

COMUNE DI BIANCAVILLA Provincia di Catania



SIN
BIANCAVILLA
DMF-468/2001

OGGETTO: INTERVENTI DI BONIFICA/MESSA IN SICUREZZA PERMANENTE E RIPRISTINO AMBIENTALE DELL'AREA DI CAVA DI "MONTE CALVARIO" PER LA FRUIBILITA' A PARCO. - C.U.P.: C84G15000000001

PROGETTO ESECUTIVO	ELABORATO	C-2.1	SCALA
	TITOLO ELABORATO	INTERVENTO PROGETTUALE "GEOSITO DI TIPO MINERALOGICO" D.A. N.105/Gab del 15/04/2015. D.Lgs 50/16 ART. 23 COMMA 8 - (DPR 207/10 art.33,lett.d – art. 36 lett.c) STRUTTURA IN ACCIAIO: RELAZIONE DI CALCOLO FASCICOLO DI CALCOLO RELAZIONE SUI MATERIALI ANALISI DEI CARICHI	

IL PROGETTISTA – RESPONSABILE DELLA V[^] P.O. – AREA TECNICA
(Ing. Placido MANCARI)

IL R.U.P.
(Geom. Antonino Ricceri)

IL COLLABORATORE
(Geom. Placido Gentile)

SPAZIO PER VISTI



SICON S.R.L.

SERVIZI INTEGRATI PER L'INGEGNERIA CIVILE



Società certificata ai sensi della norma UNI ISO 9001 : 2015

VERIFICA DELLA PROGETTAZIONE ESECUTIVA

ESITO ☒ Positivo ☐ Negativo

ALLEGATO n. _____ - ELABORATO "C-2.1" al

Rapporto di Verifica conclusivo del _____

IL PROGETTISTA
Ing. Placido Mancari

IL SOGGETTO VERIFICATORE
SICON s.r.l.
Prof. Ing. Gianni Rizzari

VISTO:
IL RESPONSABILE UNICO DEL PROCEDIMENTO
Geom. Antonino Ricceri

IL SINDACO – Antonio Bonanno

DATA	MARZO 2018	
REV.	DATA	MOTIVO DELLA REVISIONE
1	01/03/2018	RIFERIMENTO DOCUMENTO UNITARIO: Approvato con decreto del Ministero dell'Ambiente e della Tutela del Territorio e del Mare Prot. N. 316/STA del 06/06/2017. ELABORATO REVISIONATO CON LE PRESCRIZIONI DI CUI AL DECRETO Prot. N. 316/STA
2	02/08/2018	RAPPORTO DI VERIFICA INTERMEDIO N. 1
3	01/10/2018	RAPPORTO DI VERIFICA INTERMEDIO N. 2

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DESCRIZIONE GENERALE DELL'OPERA

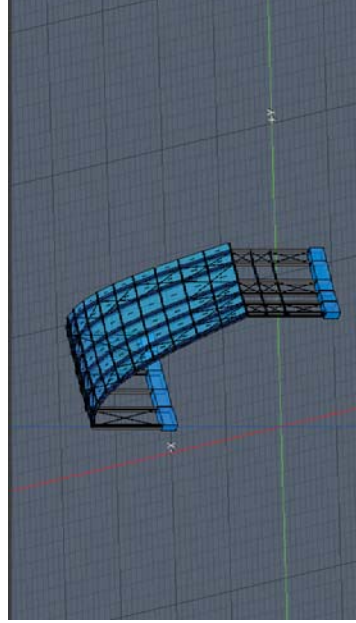
Il presente calcolo strutturale si riferisce alla realizzazione di una struttura in acciaio e vetro che intende ricoprire un versante lavico nell'ambito del progetto di "INTERVENTI DI BONIFICA/MESSA IN SICUREZZA PERMANENTE E RIPRISTINO AMBIENTALE DELL'AREA DI CAVA DEL MONTE CALVARIO PER LA FRUIBILITA' A PARCO" sito in Biancavilla (CT) ed in particolare nel settore NORD-OVEST dell'area. L'intera struttura avente una forma irregolare di una lunghezza pari a circa 70 [ml], larghezza di circa 9,40 [ml] ed altezza di 12,10 [ml] per ricoprire l'intero fronte lavico. Lo schema strutturale statico è assimilabile ad un portale zoppo incastrato alla base, che si ripete longitudinalmente per tutta la lunghezza, ed è collegato da travi poste in testa alle colonne verticali. Non potendo effettuare grandi quantità di scavi di sbancamento per le fondazioni, si è pensato di realizzare delle grosse fondazioni in c.a. che verranno successivamente ricoperte per una altezza di circa 50 [cm]. Tale soluzione si preferisce per la sua semplicità di calcolo, di fabbricazione in officina e di realizzazione in cantiere nonché per la sua versatilità di utilizzo. La struttura sarà costituita da fondazioni composte da due basamenti in c.a. delle dimensioni di L100x160 che saranno realizzati in opera dopo aver creato un opportuno piano livellato da magrone in cls. Il terreno che come si evince dalla relazione geologica sarà caratterizzato dai seguenti parametri geotecnici:

$$\gamma = 1.90 \text{ [t/mc]}$$

$$\phi = 35^\circ$$

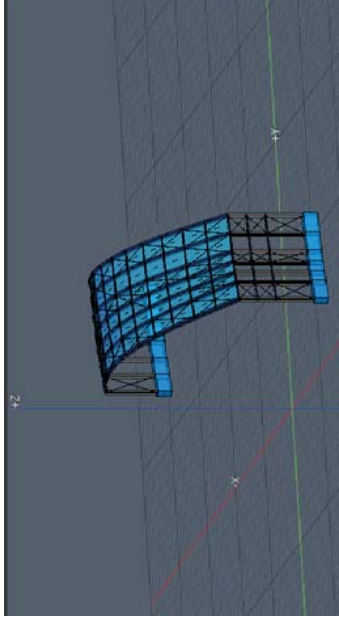
$$c = 0.00 \text{ [t/mq]}$$

In particolare il terreno di sedime è costituito da materiale vulcanico e in base al valore di VS30 trovato e secondo l'Ordinanza del Presidente del Consiglio dei Ministri n.3274 D.M. 14/01/2008 si può considerare una **categoria** di suolo pari a **B**. L'acciaio utilizzato sarà del tipo S275 ed in particolare i pilastri saranno delle dimensioni di HEA240 collegati ad incastro alle fondazioni di base. Le travi di collegamento longitudinali saranno costituite da IPE100, mentre l'intera travata del portale è in HEA240 con forma approssimabile ad un arco ma composto da elementi saldati a completa penetrazione per garantire la continuità strutturale. Inoltre verranno disposti degli opportuni controventi trasversali con tondini di dimensioni variabili per poter ben ripartire le azioni orizzontali agenti. Vista la forma particolarmente irregolare, e le differenze di quote tra i punti di valle e tra i punti di monte, sempre per evitare eccessivi scavi, si è ritenuto opportuno andare a studiare l'intera opera suddividendola in 5 blocchi di dimensioni differenti e considerando tra di loro degli opportuni giunti tecnici. La struttura in acciaio dovrà sostenere dei pannelli in vetro delle dimensioni di 1,50 x 1,50 m e composto da due lastre di vetro dello spessore di 10 [mm] unite tra loro mediante un plastico (polivinilbutirale) da 1,52 [mm] che ne garantisce l'integrità anche dopo le eventuali rotture, questi sono attaccati ai portali di interasse 1,50 [m] tramite dei supporti del tipo "a ragno". La struttura è stata calcolata considerando una analisi lineare dinamica ed un fattore di struttura unitario ($q = 1$) cioè considerando la struttura **non dissipativa** e pertanto nella verifica degli elementi non si terrà conto della gerarchia delle resistenze. Vengono riportate di seguito delle viste assonometriche contrapposte, dei rispettivi blocchi, allo scopo di consentire una migliore comprensione della struttura oggetto della presente relazione:

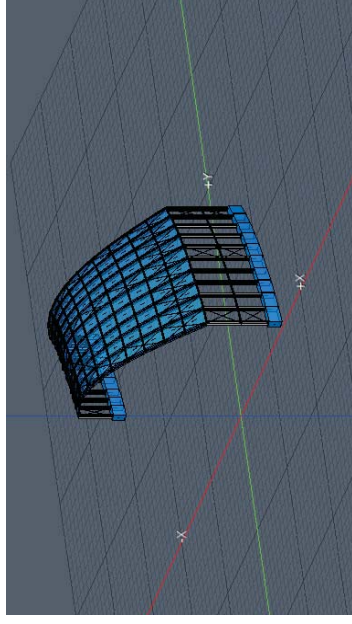


Vista Assonometrica blocco "A"

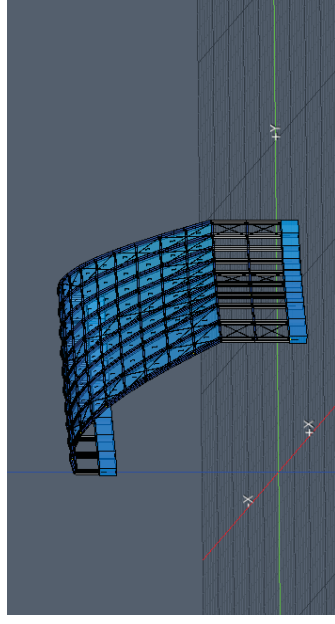
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Vista Assonometrica blocco "B"



Vista Assonometrica blocco "C"



Vista Assonometrica blocco "D"

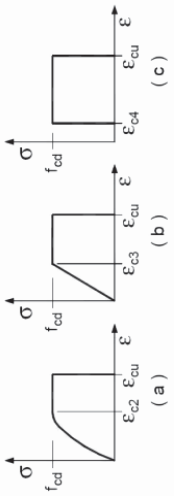
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MATERIALI IMPIEGATI E RESISTENZE DI CALCOLO

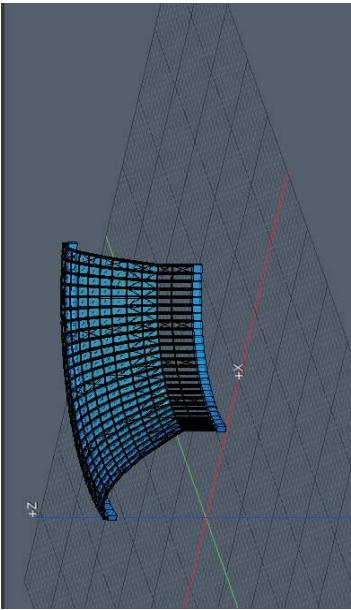
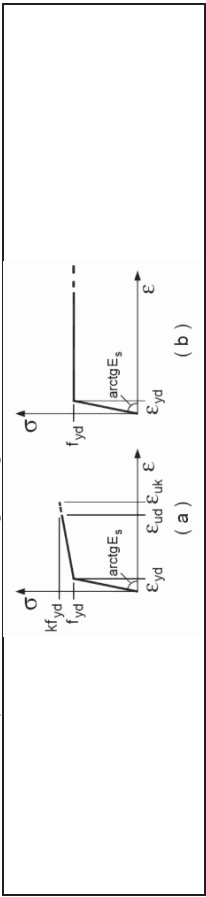
Per la realizzazione dell'opera in oggetto saranno impiegati i seguenti materiali, di cui si riportano nell' ordine le proprietà meccaniche adottate nel calcolo elastico e le resistenze di calcolo per le verifiche di sicurezza:

Materiali			
Materiale: C25/30			
Peso specifico	kg/mc		2500
Modulo di Young E	kg/cmq		3105
Modulo di Poisson v			0.13
Coefficiente di dilatazione termica λ	1/°C		1e-005
Materiale: Acciaio			
Peso specifico	kg/mc		7850
Modulo di Young E	kg/cmq		2106
Modulo di Poisson v			0.30
Coefficiente di dilatazione termica λ	1/°C		1.2e-005
Parti in calcestruzzo armato			
Classe calcestruzzo	Clis C25/30		
Resistenza cubica Rck	kg/cmq		300
Resistenza di calcolo fcd	kg/cmq		141
Resistenza a trazione di calcolofetd	kg/cmq		12
Resistenza cilindrica fck	kg/cmq		249
Resistenza a trazione mediafcim	kg/cmq		26
Classe acciaio			
Resistenza allo snervamento fyk	kg/cmq		Acciaio B450C
Resistenza alla rottura ftk	kg/cmq		>=4500
			>=5400
Parti in acciaio			
Classe acciaio			S275
fyd (<=40mm)	kg/cmq		2750
fyd (>=40mm)	kg/cmq		2550
ft (<=40mm)	kg/cmq		4300
ft (>=40mm)	kg/cmq		4100
Classe acciaio			FE430
fyd (<=40mm)	kg/cmq		2750
fyd (>=40mm)	kg/cmq		2500
ft (<=40mm)	kg/cmq		4300
ft (>=40mm)	kg/cmq		4100

I diagrammi costitutivi del calcestruzzo e dell'acciaio per calcestruzzo sono stati adottati in conformità alle indicazioni riportate al punto 4.1.2.1.2.2 del D.M. 14 gennaio 2008; in particolare per le verifiche delle sezioni in calcestruzzo armato è stato adottato il modello di calcestruzzo riportato in a) della figura seguente



Diagrammi di calcolo tensione/deformazione del calcestruzzo. ed il modello di acciaio riportato in a) o b) della figura seguente



Vista Assonometrica blocco "E"

NORMATIVA DI RIFERIMENTO

Nel seguente elenco sono riportate le norme di riferimento secondo le quali sono state condotte le fasi di calcolo e verifica degli elementi strutturali:

- Legge 5 novembre 1971 n. 1086** (G. U. 21 dicembre 1971 n. 321)
- "Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica"
- Legge 2 febbraio 1974 n. 64** (G. U. 21 marzo 1974 n. 76)
- "Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche"
- D.M. 14.01.2008 (nuove norme tecniche per le costruzioni)**
- Nel seguito denominate NT (norme tecniche)
- Il calcolo delle sollecitazioni e la loro combinazione è stato eseguito seguendo le Indicazioni delle NT secondo l'APPROCCIO 2.*

VITA NOMINALE, CLASSI D'USO E PERIODO DI RIFERIMENTO

La costruzione in oggetto è definita dalla seguente tipologia (p.to 2.4 delle NT) :

Vita della struttura	
Tipo	Ponti imp. strategica (>100) >= 100 anni
Vita nominale(anni)	100.0
Classe d'uso	Classe IV
Coefficiente d'uso	2.000
Periodo di riferimento(anni)	200.000
Stato limite di esercizio - SLO	PVR=81.0%
Stato limite ultimo - SLV	PVR=10.0%
Periodo di ritorno SLO(anni)	TR=120.4
Periodo di ritorno SLV(anni)	TR=1898.2

Per maggiori dettagli riguardo l'azione sismica si veda la definizione degli spettri di risposta

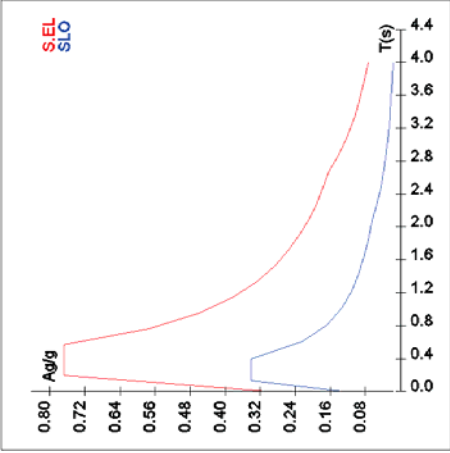
VALUTAZIONE DELL'AZIONE SISMICA

L'azione sismica è stata valutata in conformità alle indicazioni riportate al capitolo 3.2 del D.M. 14 gennaio 2008 "Norme tecniche per le Costruzioni"

- La valutazione degli spettri di risposta per un dato Stato Limite avviene attraverso le seguenti fasi:
- definizione della Vita Nominale e della Classe d'Uso della struttura, in base ai quali si determina il Periodo di Riferimento dell'azione sismica.
 - Determinazione attraverso latitudine e longitudine dei parametri sismici di base a_b , F_0 e T_c per lo Stato Limite di interesse; l'individuazione è stata effettuata interpolando tra i 4 punti più vicini al punto di riferimento dell'edificio secondo quanto disposto dall'allegato alle NTC "Pericolosità Sismica", dove:
 - ag** accelerazione orizzontale massima al sito;
 - F₀** valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale.
 - T^{*c}** periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale
 - Determinazione dei coefficienti di amplificazione stratigrafica e topografica.
 - Calcolo del periodo T_c corrispondente all'inizio del tratto a velocità costante dello Spettro.
- I dati così calcolati sono stati utilizzati per determinare gli Spettri di Progetto nelle verifiche agli Stati Limite considerati, per ogni direzione dell'azione sismica.
- Oltre alla determinazione dei parametri sismici del sito si è considerata la tipologia di terreno, la posizione topografica e la tipologia strutturale (classe di duttilità, regolarità, ecc..) che ha condotto alla determinazione dei seguenti spettri di risposta:

Spettri di risposta	
Spettro: SpettroNT(q=1)	
Il calcolo degli spettri e del fattore di struttura sono stati calcolati per la seguente tipologia di terreno e struttura	
Vita della struttura	
Tipo	Ponti imp. strategica (>100) >= 100 anni
Vita nominale(anni)	100.0
Classe d'uso	Classe IV
Coefficiente d'uso	2.000
Periodo di riferimento(anni)	200.000
Stato limite di esercizio - SLO	PVR=81.0%
Stato limite ultimo - SLV	PVR=10.0%
Periodo di ritorno SLO(anni)	TR=120.4
Periodo di ritorno SLV(anni)	TR=1898.2
Parametri del sito	
Comune	Biancavilla - (CT)
Longitudine	14.8652
Latitudine	37.6461
Id reticolo del sito	47419-47197-47196-47418
Valori di riferimento del sito	
Ag/g (TR=120.4) SLO	0.1103
F0 (TR=120.4) SLO	2.5726
Tc (TR=120.4) SLO	0.281
Ag/g (TR=1898.2) SLV	0.2704
F0 (TR=1898.2) SLV	2.5180
Tc (TR=1898.2) SLV	0.441
Coefficiente Amplificazione Topografica	SI=1.000
Categoria terreno B	
stato limite SLV	
	S=1.13
	TB=0.19
	TC=0.57
	TD=2.68
stato limite SLO	
	S=1.20
	TB=0.13
	TC=0.40
	TD=2.04

Spettro Elastico		q=1 (struttura NON DISSIPATIVA)	
Smorzamento viscoso %		5.0	
T [s]	EL [a/g]	TSLO [s]	SLO [a/g]
0.0000	0.30491	0.00000	0.13236
0.19040	0.76076	0.13299	0.34050
0.57119	0.76776	0.39896	0.34050
0.76304	0.57472	0.60424	0.22482
0.95489	0.45925	0.80952	0.16781
1.14675	0.38242	1.01479	0.13387
1.33860	0.32761	1.22007	0.11134
1.53045	0.28654	1.42535	0.09531
1.72231	0.25462	1.63063	0.08331
1.91416	0.22910	1.83591	0.07399
2.10602	0.20823	2.04119	0.06655
2.29787	0.19084	2.25883	0.05435
2.48972	0.17614	2.47648	0.04521
2.68158	0.16354	2.69412	0.03820
2.90131	0.13970	2.91177	0.03270
3.12105	0.12072	3.12942	0.02831
3.34079	0.10537	3.34706	0.02475
3.56053	0.09276	3.56471	0.02182
3.78026	0.08229	3.78235	0.01938
4.00000	0.07350	4.00000	0.01733



ELEMENTI DI FONDAZIONE

Il calcolo della struttura di fondazione è condotto considerando le azioni che la struttura sovrastante le trasmette amplificate per un γ_{rd} pari a 1,1 in CD "B" e 1,3 in CD "A", e comunque non maggiori di quelle derivanti da una analisi elastica della struttura in elevazione eseguita con un fattore di struttura q pari a 1 e non maggiori delle resistenze degli elementi sovrastanti la fondazione.

METODO DI ANALISI E CRITERI DI VERIFICA

Il calcolo delle azioni sismiche è stato eseguito in analisi dinamica modale, considerando il comportamento della struttura in regime elastico lineare. La masse sono applicate nei nodi del modello queste vengono generate attraverso i carichi agenti sulle membrature che collegano i nodi come la massa relativa alla azione di incastro perfetto del carico considerato. La risposta massima di una generica caratteristica E; conseguente alla sovrapposizione dei modi, è valutata con la tecnica della combinazione probabilistica definita CQC (Complete Quadratic Combination - Combinazione Quadratica Completa):

E = \sqrt{\sum_{i,j=1,n} \rho_{ij} \cdot E_i \cdot E_j}

\rho_{ij} = \frac{8 \xi^2 \cdot (1 + \beta_{ij}) \cdot \beta_{ij}^2}{(1 - \beta_{ij}^2)^2 + 4 \xi^2 \cdot \beta_{ij} \cdot (1 + \beta_{ij}^2)}

\beta_{ij} = \frac{\omega_i}{\omega_j}

con:

dove:

n è il numero di modi di vibrazione considerati

ξ è il coefficiente di smorzamento viscoso equivalente espresso in percentuale;

β_{ij} è il rapporto tra le frequenze di ciascuna coppia i-j di modi di vibrazione.

Le sollecitazioni derivanti da tali azioni sono state calcolate per varie posizioni dei baricentri delle masse e composte secondo combinazioni di posizioni prestabilite, come riportato in seguito, il risultato di tali combinazioni sono state composte poi con quelle derivanti da carichi non sismici secondo le varie combinazioni di carico probabilistiche. Per tener conto della eccentricità accidentale delle masse si sono considerate varie posizioni delle masse ad ogni impalcato modificando la posizione del baricentro di una distanza, rispetto alla posizione originaria, come percentuale della dimensione della struttura nella direzione considerata. Le azioni risultanti dai calcoli per le varie posizioni delle masse, in fase di verifica vengono combinati al fine di ottenere le azioni piu' sfavorevoli: di seguito vengono riportate sia le posizioni che le combinazioni delle masse, le due tabelle vanno lette nel seguente modo:

la prima indica la percentuale delle dimensione della struttura secondo cui viene spostato il baricentro ad ogni impalcato la percentuale è assegnata nelle due direzioni ortogonali secondo cui agisce il sisma, per ognuna di tali posizioni è eseguito un calcolo modale della struttura: la seconda tabella è usata in fase di verifica per la valutazione dell'azione sismica nel seguente modo l'effetto del sisma in una direzione è combinato con quello ortogonale di un'altra posizione con i fattori specificati nelle due colonne:

Percentuali Spostamento masse impalcati			
Posizione	% Spostamento direzione X	% Spostamento direzione Y	
1	0	-5	
2	5	0	
3	0	5	
4	-5	0	

Combinazioni del Sisma in X e Y e Verticale				
Comb	Pos. SismaX	Pos. SismaY	Fx	Fy Fz
1	1	2	1	0.3 0.3
2	1	2	0.3	1 0.3
3	1	4	1	0.3 0.3
4	1	4	0.3	1 0.3
5	3	2	1	0.3 0.3
6	3	2	0.3	1 0.3
7	3	4	1	0.3 0.3

8	3	4	0.3	1	0.3
9	1	2	0.3	0.3	1
10	1	4	0.3	0.3	1
11	3	2	0.3	0.3	1
12	3	4	0.3	0.3	1

Comb.= Numero di combinazione dei sismi
Pos. Sisma X = Posizione in cui viene scelto il sisma in direzione X
Pos. Sisma Y = Posizione in cui viene scelto il sisma in direzione Y
Fx = Fattore con cui il sisma X partecipa
Fy = Fattore con cui il sisma Y partecipa
Fz = Fattore con cui il sisma Verticale partecipa (quando richiesto)
Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx, ed Fy ed Fz

AZIONI SULLA STRUTTURA

I calcoli e le verifiche sono condotti con il metodo semiprobabilistico degli stati limite secondo le indicazioni del D.M. 14 gennaio 2008. I carichi agenti sui solai, derivanti dall'analisi dei carichi, vengono assegnati alle aste in modo automatico in relazione all'influenza delle diverse aree di carico. I carichi dovuti ai tamponamenti, sia sulle travi di fondazione che su quelle di piano, sono schematizzati come carichi lineari agenti esclusivamente sulle aste. In presenza di platee il tamponamento è inserito considerando delle speciali aste (aste a sezione nulla) che hanno la sola funzione di riportare il carico su di esse agente nei nodi degli elementi della platea ad esse collegati. Su tutti gli elementi strutturali è inoltre possibile applicare direttamente ulteriori azioni concentrate e/o distribuite. Le azioni introdotte direttamente sono combinate con le altre (carichi permanenti, accidentali e sisma) mediante le combinazioni di carico di seguito descritte: da esse si ottengono i valori probabilistici da impiegare successivamente nelle verifiche.

I solai, oltre a generare le condizioni di carico per carichi fissi e variabili, generano anche altre condizioni di carico che derivano dal carico accidentale moltiplicati per i coefficienti ψ0, ψ1 e ψ2 da utilizzare per le varie combinazioni di carico e per la determinazione delle masse sismiche.

Le azioni sono state assegnate su aste e piastre, definendo le seguenti condizioni di carico

Descrizione	Tipo
Peso Proprio	Automatica
QP Solai	Automatica
OFissi Solai	Automatica
QV Solai	Automatica
QV Solaiψs0	Automatica
QV Solaiψs1	Automatica
QV Solaiψs2	Automatica
Tamponamento	Automatica
Neve	Utenie
Vento X	Utenie
Vento Y	Utenie
Carichi termici	Utenie
Vetro	Utenie

In fase di combinazione delle condizioni di carico si è agito su coefficienti moltiplicatori delle condizioni per definire l'esatto contributo sia in termini di carico che di massa, e sono stati infine definiti gli scenari di calcolo come gruppi omogenei di combinazioni di carico. Di seguito vengono riportate le combinazioni di carico usate per lo Stato Limite Ultimo e per lo Stato Limite di Esercizio. Le verifiche sono riportate nel fascicolo dei calcoli.

Le tabelle riportano nell'ordine:

- il nome della combinazione di carico
- il tipo di analisi svolta: STR=Strutturale, Statica STR=Sismica statica Strutturale, Modale STR=Sismica modale strutturale, SLE Rara=Stato Limite Esercizio combinazione rara, SLE Freq=Stato Limite Esercizio combinazione frequente, SLE Q.Perm=Stato Limite Esercizio combinazione quasi Permanente, GEO=Geotecnica, Statica GEO=Sismica Statica Geotecnica, Modale GEO=Sismica modale Geotecnica, STR+GEO=Strutturale+Geotecnica, Statica STR+GEO=Sismica Statica Strutturale+Geotecnica, Modale STR+GEO=Sismica modale Strutturale+Geotecnica, Modale SLE= Combinazione sismica modale con spettro di progetto SLD, Statica SLE=Combinazione sismica statica con spettro di progetto SLD. I termini **"Strutturale"**, **"Geotecnica"** e **"Strutturale+ Geotecnica"** indicano che la combinazione è usata dal programma per la determinazione delle verifiche di resistenza degli elementi strutturali, delle sole verifiche geotecniche, sia per le verifiche strutturali che geotecniche.
- lo spettro usato, se sismica
- il fattore amplificativo del sisma
- l'angolo di ingresso del sisma, se trattasi di analisi sismica

- il nome della condizione di carico e per ogni condizione di carico
- il fattore di combinazione per i carichi verticali
- se la condizione (con il suo coefficiente di peso) è inclusa nella combinazione (colonna Attiva)
- se la condizione partecipa alla formazione della massa (colonna Massa)
- il fattore con cui partecipa alla formazione della massa (se non è esclusa dalla formazione della massa)

Scenario di calcolo

Scenario : Set NT SLV A2 STR GEO									
Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Fattore m.
1) Solo Permanenti	STR				1.00	Peso Proprio	1.3	Si	1
						QF Solai	1.3	Si	1
						QFissi Solai	1.5	Si	1
						QV Solai	1	No	1
						QV SolaiPs0	1	No	No
						QV SolaiPs1	1	No	No
						QV SolaiPs2	1	No	Si
						Tamponamento	1.5	Si	Si
						Neve	1	No	No
						Vento X	1	No	No
						Vento Y	1	No	No
						Carichi termici	1	No	No
						Vetro	1.5	Si	1
2) AD QV/Solai	STR+GEO				1.00	Peso Proprio	1.3	Si	1
						QF Solai	1.3	Si	1
						QFissi Solai	1.5	Si	1
						QV Solai	1.5	Si	No
						QV SolaiPs0	1	No	No
						QV SolaiPs1	1	No	No
						QV SolaiPs2	1	No	Si
						Tamponamento	1.5	Si	Si
						Neve	0.75	Si	No
						Vento X	1	No	No
						Vento Y	0.9	Si	No
						Carichi termici	0.9	Si	No
						Vetro	1.5	Si	1
3) AD QV/Solai	STR+GEO				1.00	Peso Proprio	1.3	Si	1
						QF Solai	1.3	Si	1
						QFissi Solai	1.5	Si	1
						QV Solai	1.5	Si	No
						QV SolaiPs0	1	No	No
						QV SolaiPs1	1	No	No
						QV SolaiPs2	1	No	Si
						Tamponamento	1.5	Si	Si
						Neve	0.75	Si	No
						Vento X	0.9	Si	No
						Vento Y	1	No	No
						Carichi termici	0.9	Si	No
						Vetro	1.5	Si	1
4) AD Neve	STR+GEO				1.00	Peso Proprio	1.3	Si	1
						QF Solai	1.3	Si	1
						QFissi Solai	1.5	Si	1
						QV Solai	1	No	No
						QV SolaiPs0	1.5	Si	No
						QV SolaiPs1	1	No	No
						QV SolaiPs2	1	No	Si
						Tamponamento	1.5	Si	Si
						Neve	1	No	No

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. ev.	Attiva	Massa	Fattore m.	
5) AD Neve	STR+GEO				1.00	Vento X	1	No	No		
							Vento Y	0.9	Si	No	1
							Carichi termici	0.9	Si	No	1
							Vetro	1.5	Si	Si	1
6) AD VentoX Vert. Slav	STR+GEO				1.00	Peso Proprio	1.3	Si	Si	1	
							QP Solai	1.3	Si	Si	1
							QFissi Solai	1.5	Si	Si	1
							QV Solai	1	No	No	1
							QV SolaiPsi0	1.5	Si	No	1
							QV SolaiPsi1	1	No	No	1
							QV SolaiPsi2	1	No	Si	1
							Tamponamento	1.5	Si	Si	1
							Neve	1.5	Si	No	1
							Vento X	0.9	Si	No	1
7) AD VentoY Vert. Slav	STR+GEO				1.00	Vento Y	1	No	No	1	
							Carichi termici	0.9	Si	No	1
							Vetro	1.5	Si	Si	1
8) AD Termici	STR+GEO				1.00	Peso Proprio	1.3	Si	Si	1	
							QP Solai	1.3	Si	Si	1
							QFissi Solai	1.5	Si	Si	1
							QV Solai	1	No	No	1
							QV SolaiPsi0	1.5	Si	No	1
							QV SolaiPsi1	1	No	No	1
							QV SolaiPsi2	1	No	Si	1
							Tamponamento	1.5	Si	Si	1
							Neve	0.75	Si	No	1
							Vento X	1	No	No	1
				Vento Y	1.5	Si	No	1			
				Carichi termici	0.9	Si	No	1			
				Vetro	1.5	Si	Si	1			

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
9) AD Termici	STR+GEO				1.00	Vetro	1.5	Si	Si	1
						Peso Proprio	1.3	Si	Si	1
						OP Solai	1.3	Si	Si	1
						QFissi Solai	1.5	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1.5	Si	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Tamponamento	1.5	Si	Si	1
						Neve	0.75	Si	No	1
						Vento X	1	No	No	1
						Vento Y	0.9	Si	No	1
						Carichi termici	1.5	Si	No	1
						Vetro	1.5	Si	Si	1
10) AD VentoX Vert fav	STR+GEO				1.00	Peso Proprio	1	Si	Si	1
						OP Solai	1	Si	Si	1
						QFissi Solai	1	No	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Tamponamento	1	No	Si	1
						Neve	1	No	No	1
						Vento X	1.5	Si	No	1
						Vento Y	1	No	No	1
						Carichi termici	1	No	No	1
						Vetro	1	Si	Si	1
11) AD VentoY Vert fav	STR+GEO				1.00	Peso Proprio	1	Si	Si	1
						OP Solai	1	Si	Si	1
						QFissi Solai	1	No	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	No	Si	1
						Tamponamento	1	No	Si	1
						Neve	1	No	No	1
						Vento X	1	No	No	1
						Vento Y	1.5	Si	No	1
						Carichi termici	1	No	No	1
						Vetro	1	Si	Si	1
12) SISMAX_SLV	Modale STR+GEO	SpetroNT (q=1)	1	0	1.00	Peso Proprio			Si	1
						OP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Tamponamento	1	Si	Si	1
						Neve	1	No	No	1
						Vento X	1	No	No	1
						Vento Y	1	No	No	1
						Carichi termici	1	No	No	1
						Vetro	1	Si	Si	1

Combinazione	Tipo	Spettro	F.Sisma	α	K mod	Cond.Carico	Fatt. cv.	Attiva	Massa	Fattore m.
13) SISMAX_SLV	Modale STR+GEO	SpetroNT (q=1)	1	90	1.00					
						Peso Proprio	1	Si	Si	1
						QP Solai	1	Si	Si	1
						QFissi Solai	1	Si	Si	1
						QV Solai	1	No	No	1
						QV SolaiPsi0	1	No	No	1
						QV SolaiPsi1	1	No	No	1
						QV SolaiPsi2	1	Si	Si	1
						Tamponamento	1	Si	Si	1
						Neve	1	No	No	1
						Vento X	1	No	No	1
						Vento Y	1	No	No	1
						Carichi termici	1	No	No	1
						Vetro	1	Si	Si	1

CODICE DI CALCOLO IMPIEGATO	
Autori:	dott. ing. Dario PICA prof. ing. Paolo BISEGNA dott. ing. Donato Sista
Produzione e distribuzione	SOFT.LAB srl via Borgo II - 82030 PONTE (BN) tel. ++39 (824) 874392 fax ++39 (824) 874431 internet: http://www.soft.lab.it e.mail: info@soft.lab.it
Sigla:	IperSpaceMax 9.0.2

Il modello di calcolo assunto è di tipo spaziale e l'analisi condotta è una Analisi Elastica Lineare, esso è fondamentalmente definito dalla posizione dei nodi collegati da elementi di tipo Beam o elementi di tipo shell a comportamento sia flessionale che membranale, l'elemento finito shell utilizzato è anche in grado di esprimere una rigidità rotazionale in direzione ortogonale al piano dello shell.

L'analisi sismica utilizzata è l'analisi modale con Combinazione Quadratica Completa degli effetti del sisma. Il modello è stato analizzato sia per le combinazioni dei carichi verticali sia per le combinazioni di carico verticale e sisma. Un particolare chiarimento richiede la definizione delle masse nell'analisi sismica. Pur avendo considerato il modello con impalcati rigidi non si rende necessario calcolare il modello con la metodologia del MASTER-SLAVE, in quanto gli impalcati rigidi sono stati modellati con elementi di tipo shell a comportamento membranale in corrispondenza dei campi di solaio. Per ottenere tale modellazione il programma inserisce in automatico elementi di tipo shell a comportamento membranale in corrispondenza del campo di solaio intercluso tra una maglia di travi. la loro rigidità membranale è sufficientemente alta da rendere il campo di solaio rigido nel proprio piano, ma tale da non mal condizionare la matrice di rigidità della struttura. Qualora una maglia di travi non è collegata da solaio lo shell non viene inserito rendendo tale campo libero di deformarsi con il solo vincolo dato dalle travi della. La loro rigidità flessionale è trascurabile rispetto a quella degli elementi che contornano il campo, per cui lo shell impone un vincolo orizzontale solo nel piano dell'impalcato tra i nodi collegati, quindi non è necessario definire preventivamente definire il centro di massa e momento d'inerzia delle masse, questo perché le masse sono trasferite direttamente nei nodi del modello (modello Lumped Mass) dal codice di calcolo, il metodo per calcolare le masse nei nodi può essere quello per aree di influenza, ma questa richiederebbe l'intervento diretto dell'operatore; il codice di calcolo utilizza una metodologia leggermente più raffinata per tener conto del fatto che su un elemento il carico portato non è uniforme, quindi il codice di calcolo considera i carichi presenti sull'asta che sono stati indicati come quelli che contribuiscono alla formazione della massa (tipicamente $G + \sqrt{2} \cdot Q$) e calcola le reazioni di incastro perfetto verticali, tali reazioni divise per l'accelerazione di gravità g danno il contributo dell'elemento alla massa del nodo, sommando i contributi di tutti gli elementi che convergono nel nodo si ottiene la massa complessiva nel nodo; per gli elementi shell invece si utilizza il metodo delle aree di influenza ossia in ognuno dei 3 oppure 4 nodi che definiscono lo shell si assegna $1/3$ oppure $1/4$ del peso dello shell e $1/3$ oppure $1/4$ dell'eventuale carico variabile ridotto, sommando su tutti gli shell che convergono nel nodo si ottiene la massa da assegnare al nodo.

VERIFICA DEGLI ELEMENTI STRUTTURALI

La verifiche di resistenza degli elementi è condotta considerando le sollecitazioni di calcolo ed imponendo che le resistenze siano superiori alle azioni. Gli elementi sono verificati e/o progettati applicando la gerarchia delle resistenze in particolare la gerarchia flessione-taglio per la verifica/progetto dell'elemento e la gerarchia pilastro-trave per la determinazione delle resistenze del pilastro. Le verifiche sono condotte secondo i seguenti criteri di verifica validi sia per lo SLU che per lo SLD. I criteri di verifica sono una raccolta di parametri che vengono usati in fase di verifica secondo le esigenze strutturali, ognuno di essi contiene i dati per tutti gli elementi, è sottinteso che nella verifica di un elemento (es. trave) non sono presi in considerazione i dati relativi agli altri elementi (ad es. se si verifica una trave non sono presi in considerazione i dati relativi a pilastri e shell, così come se si esegue una verifica agli SLU non sono presi in considerazione i dati relativi agli SLE). Ognuno di essi è identificato da un nome a scelta dell'operatore, per cui nei tabulati di verifica il nome del criterio ne identifica i parametri usati. Riguardo alle verifiche agli SLU le resistenze sono determinate in base a quanto specificato dalla norma attraverso il modello plastico-incrudente o elastico-perfettamente plastico. la verifica consiste nel verificare che assegnate le sollecitazioni di verifica le deformazioni massime nel calcestruzzo e nell'acciaio siano inferiori a quelle ultime di' equivale ad affermare che nello spazio tridimensionale N,My,Mz il punto rappresentativo delle sollecitazioni è interno al dominio di resistenza della sezione.

Le verifiche agli SLE riguardano le verifiche di:

- deformabilità degli impalcati con $\delta \leq 0.005 \cdot h$
- fessurazione
- tensioni in esercizio

Criteri di verifica

Criterio di verifica: CLS Travifondazione			
Generici			
Resistenza caratteristica Rck	kg/cmq		300
Tensione caratteristica snervamento acciaio fyk	kg/cmq		4500
Deformazione unitaria ϵ_{c0}			0.002
Deformazione ultima ϵ_{cu}			0.0035
ϵ_{fu} (solo incrudimento)			0.0019
Modulo elastico E acciaio	kg/cmq		2E06
Copri ferro di calcolo	cm		4.1
Copri ferro di disegno	cm		2.5
Coefficiente di sicurezza γ_{ClS}			1.5
Coefficiente di sicurezza γ_{Acc}			1.15
Riduzione fcd calcestruzzo			0.85
Usa staffe minime in assenza di sisma			No
Usa staffe minime di normativa in presenza di sisma			No
Generici N.T.			
Inclinazione bielle compresse $\cos(\theta)$			1.00
Modello acciaio			Incudente
Incrudimento Ey/E0			0.000
Elemento esistente			No
Generici D.M. 96 T.A.			
Tensione ammissibile σ_c	kg/cmq		97.5
Tensione ammissibile σ_c in trazione	kg/cmq		21.8
Tensione ammissibile σ_c acciaio	kg/cmq		2600.0
Tensione tangenziale ammissibile τ_{c0}	kg/cmq		6.0
Tensione tangenziale massima τ_{c1}	kg/cmq		18.3
Coefficiente di omogeneizzazione n			15
Coefficiente di omogeneizzazione n in trazione			0.5
Sezione interamente reagente			No
Fessurazioni			
Verifica a decompressione			No
Verifica formazione fessure			No
Verifica aperture fessure			Si
Classe di esposizione			XC2
Tipo armatura			Poco sensibile
Combinazione Rara			No
Combinazione QP			Si
W ammissibile Combinazione QP		mm	0.300
Combinazione Freq.			Si
W ammissibile Combinazione Freq.		mm	0.400
Valore caratteristico apertura fessure w_k (*wm)			1

fc efficace	kg/cmq	25.99
Coefficiente di breve o lunga durata kt		0.40
Coefficiente di aderenza k1		0.80
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σ_{ClS}	kg/cmq	149
Tensione ammissibile $\sigma_{Acciaio}$	kg/cmq	3600
Verifica Combinazione QP		Si
Tensione ammissibile σ_{ClS}	kg/cmq	112
Tensione ammissibile $\sigma_{Acciaio}$	kg/cmq	3600
Verifica Combinazione Freq		No
Coefficienti di omogeneizzazione		
Acciaio - Cls compresso		15
ClS teso - Cls compresso		0.5
Armatura travi		
Numero di bracci delle staffe		2
Numero minimo di ferri superiori		2
Numero minimo di ferri inferiori		2
Numero minimo di ferri di parete		1
Numero reggistaffe superiori		0
Numero reggistaffe intermedi		4
Numero reggistaffe inferiori		2
Diametro ferri superiori	mm	16
Diametro ferri inferiori	mm	16
Diametro staffe	mm	8
Percentuale armatura rispetto alla base per verifica a taglio	%	100.00
Minima percentuale armatura compressa rispetto alla tesa	%	50.00
Minima percentuale armatura rispetto al Cls	%	0.20
Massima percentuale armatura rispetto al Cls	%	1.55
Calcolo travi		
Traslazione momento		Si
Verifica travi		
Verifica a torsione		No
Verifica a pressoflessione retta		No
Trave a spessore		No
Verifica N.T. travi		
Trave tozza		No
Gerarchia Flessione- Taglio		Si
Escludi dalla gerarchia trave-pilastro		No
Verifica a taglio travi		
Coefficiente di sovrarresistenza γ_{Rd}		1.2
Includi effetto spinotto nel taglio		Si
Includi effetto della pressoflessione nel taglio		Si
Verifica a taglio N.T. travi		
Coefficiente di sovrarresistenza γ_{Rd} (CDA)		1.2
Coefficiente di sovrarresistenza γ_{Rd} (CDB)		1
Verifica a taglio D.M. 96 T.A. travi		
Percentuale taglio alle staffe	%	60
Percentuale taglio ferri parete	%	40
Considera la resistenza a taglio VRDns		NO
Stampa travi		
Stampa informazioni relative all'asse neutro		Si

Criterio di verifica: Acciaio Flessione

Verifiche		
Tipo di acciaio		
σ_{amm} (T<40mm)	kg/cmq	8275
σ_{amm} (T>40mm)	kg/cmq	1800
Fy (T<40mm)	kg/cmq	1700
Fy (T>40mm)	kg/cmq	2750
Ft (T<40mm)	kg/cmq	2550
Ft (T>40mm)	kg/cmq	4300
Piano di verifica	kg/cmq	4100
Tipo di istabilità		ε
λ. Max		Nessuna
		250

Coefficiente di sicurezza γ_s		1.5
Coefficiente di adattamento plastico Ψ_x		1
Coefficiente di adattamento plastico Ψ_y		1
Costante di ingobbimento J_w		1
Usa β		No
Escludi momento flettente trasversale M_z		No
Verifica come pendolo		No
Carichi estradossati		No
Verifiche N.T. S.I.U		
Coefficiente di sicurezza γ_M		1.05
Usa CNR 10011		No
Stampe		
Combinazioni di verifica		Più gravosa
Verifiche N.T. S.I.E		
Verifica degli spostamenti verticali		Si
Monta iniziale della trave δc	cm	0.0
Limite spostamento nello stato finale finale	mm	L/250.00
Limite spostamento dovuto ai soli carichi variabili	mm	L/300.00

Criterio di verifica: Acciaio Tirante		
Verifiche		
Tipo di acciaio		FE430
σ ann (T<40mm)	kg/cmq	1900
σ ann (T>40mm)	kg/cmq	1700
F _y (T<40mm)	kg/cmq	2750
F _y (T>40mm)	kg/cmq	2500
F _t (T<40mm)	kg/cmq	4300
F _t (T>40mm)	kg/cmq	4100
Piano di verifica	altro	
Tipo di stabilità		Nessuna
λ Max		200
Coefficiente di sicurezza γ_s		1.5
Coefficiente di adattamento plastico Ψ_x		1
Coefficiente di adattamento plastico Ψ_y		1
Costante di ingobbimento J_w		1
Usa β		No
Escludi momento flettente trasversale M_z		No
Verifica come pendolo		Si
Carichi estradossati		No
Verifiche N.T. S.I.U		
Coefficiente di sicurezza γ_M		1.05
Usa CNR 10011		No
Stampe		
Combinazioni di verifica		Più gravosa
Verifiche N.T. S.I.E		
Verifica degli spostamenti verticali		No

Criterio di verifica: Acciaio Pressiflessione		
Verifiche		
Tipo di acciaio		FE430
σ ann (T<40mm)	kg/cmq	1900
σ ann (T>40mm)	kg/cmq	1700
F _y (T<40mm)	kg/cmq	2750
F _y (T>40mm)	kg/cmq	2500
F _t (T<40mm)	kg/cmq	4300
F _t (T>40mm)	kg/cmq	4100
Piano di verifica		η
Tipo di stabilità		Pressoflessione senza svergolamento
λ Max		200
Coefficiente di sicurezza γ_s		1.5
Coefficiente di adattamento plastico Ψ_x		1
Coefficiente di adattamento plastico Ψ_y		1
Costante di ingobbimento J_w		1
Usa β		No

Escludi momento flettente trasversale M_z		No
Verifica come pendolo		No
Carichi estradossati		No
Verifiche N.T. S.I.U		
Coefficiente di sicurezza γ_M		1.05
Usa CNR 10011		No
Stampe		
Combinazioni di verifica		Più gravosa
Verifiche N.T. S.I.E		
Verifica degli spostamenti verticali		Si
Monta iniziale della trave δc	cm	0.0
Limite spostamento nello stato finale finale	mm	L/250.00
Limite spostamento dovuto ai soli carichi variabili	mm	L/300.00

INFORMAZIONI SULL'ELABORAZIONE

Il calcolo automatico è stato eseguito su un elaboratore con le seguenti caratteristiche:

- Tipo: Intel Pentium
 - Capacità di memoria: 4095 MB
 - Unità di memoria di massa: Disco C 458.45 GB
 - Sistema operativo e sua versione: Microsoft Windows NT 6.1 (Build: 7601)
- La valutazione sulla correttezza dei dati in ingresso e sulla accuratezza dei risultati è stata effettuata sia mediante le visualizzazioni grafiche del post-processore sia mediante il controllo dei tabulati numerici. La verifica che la soluzione ottenuta non sia viziata da errori di tipo numerico, legati all'algoritmo risolutivo ed alle caratteristiche dell'elaboratore, è stata effettuata considerando che il numero di cifre significative utilizzate nei procedimenti numerici è [cifre significative], e che all'interno della matrice di rigidezza il rapporto tra il pivot massimo e minimo è: [pivot]. Tale valore è accettabile quando risulta minore di 10 elevato al numero di cifre significative. Nel caso dell'elaborazione in oggetto si ha:
- Max/Min=5.024749e+005<1.0000000e+016

Si riporta la tabella relativa alle statistiche sulla matrice di rigidezza

Risultati Analisi Dinamica - Statistiche matrice di rigidezza	
Scenario di calcolo: Set_NT_SLV_A2_STRGEO	
Minimo della diag.	1.687792e+004
Massimo della diag.	1.276787e+009
Rapporto Max/Min	7.564836e+004
Media della diag.	7.313588e+007
Densita'	3.154206e+001

Pertanto i risultati si ritengono accettabili per quanto riguarda la correttezza del calcolo automatico.

Il Progettista

MODELLAZIONE

La struttura è costituita da diversi elementi distinti, in base alla loro funzione, in

- Fondazione in c.a. costituita da: graticcio di travi
- Travi in acciaio
- Pilastrini in acciaio
- Solaio per Vetro strutturale

I livelli di sicurezza scelti dal Committente e dal Progettista in funzione del tipo e dell'uso della struttura, nonché in funzione delle conseguenze del danno, con riguardo a persone, beni, e possibile turbativa sociale, compreso il costo delle opere necessarie per la riduzione del rischio di danno o di collasso, hanno indirizzato al progetto di una struttura con i seguenti requisiti:

- sicurezza nei confronti degli Stati Limite Ultimi (SLU)
- sicurezza nei confronti degli Stati Limite di Esercizio (SLE)
- sicurezza nei confronti di deformazioni permanenti inaccettabili: Stato Limite di Danno (SLD).

La struttura è stata schematizzata con un modello spaziale agli elementi finiti che tengono conto dell'effettivo stato deformativo e di sollecitazione, secondo l'effettiva realizzazione. I vincoli esterni della struttura sono stati caratterizzati, a seconda degli elementi in fondazione se presenti, con: travi winkler, plinti diretti, plinti su pali, platee; ovvero con vincoli perfetti di incastro, appoggio, carrello, ecc. I vincoli interni sono stati schematizzati secondo le sollecitazioni mutuamente scambiate tra gli elementi strutturali, inserendo, ove opportuno, il rilascio di alcune caratteristiche della sollecitazione per schematizzare il comportamento di vincoli interni non iperstatici (cerniere, carrelli, ecc.). Il modello agli elementi finiti è stato calcolato tenendo conto dell'interazione tra strutture in fondazione e strutture in elevazione, consentendo un'accurata distribuzione delle azioni statiche e sismiche; il calcolo viene eseguito considerando il comportamento elastico lineare della struttura. I solai sono schematizzati come aree di carico, sulle quali vengono definiti i carichi permanenti (QP Solai), carichi fissi (QFissi Solai) e variabili (QV Solai); tali carichi vengono assegnati alle aste in modo automatico in relazione all'influenza delle diverse aree di carico. Le masse corrispondenti ai carichi variabili sui solai nelle combinazioni sismiche vengono trattate in maniera automatica mediante un coefficiente moltiplicativo definito insieme alla tipologia del solaio.

Il modello utilizzato è stato valutato alla luce dei diversi scenari di carico a cui viene sottoposta la struttura durante la sua costruzione e la sua vita, atto a garantire la sicurezza e la durabilità della stessa. Per la tipologia strutturale affrontata non è stato necessario definire scenari di contingenza, quindi non è stata schematizzata la struttura durante le fasi costruttive, e si ritiene che non ci siano variazioni del modello di calcolo e degli schemi di vincolo, durante la vita dell'opera. Per il dettaglio degli scenari di calcolo si faccia riferimento alla "Relazione di Calcolo".

Il progetto e la verifica degli elementi strutturali è stato effettuato seguendo la teoria degli Stati limite. I parametri relativi alle verifiche effettuate sono riportati nella Relazione di Calcolo.

Il solutore agli elementi finiti impiegato nell'analisi è SpaceSolver, per il calcolo di strutture piane e spaziali schematizzabili da un insieme di elementi finiti tipo

- BEAM,
- PLATE-SHELL,
- WINK,
- BOUNDARY,

interagenti tra loro attraverso i nodi, con la possibilità di tenere in conto tutti i possibili disassamenti, mediante l'introduzione di concetti rigidi e traslazioni degli elementi bidimensionali. Il solutore lavora in campo elastico lineare, si basa sulle routines di Matlab ed è stato sviluppato in collaborazione con l'Università di Roma – Tor Vergata. Il solutore offre la possibilità di risolvere anche travi su suolo alla Winkler con molle spalmate sull'intera suola, anziché sul solo asse, plinti diretti e su pali, pali singoli, platee, piastre sottili e spesse con controllo delle rotazioni attorno all'asse normale alla piastra (drilling). Inoltre, per gli elementi BEAM considera il centro di taglio e non il baricentro.

L'affidabilità del solutore è stata testata su una serie di esempi campioni calcolati con altri procedimenti o con formule note, di cui si rende disponibile la documentazione.

AFFIDABILITA' DEI CODICI UTILIZZATI

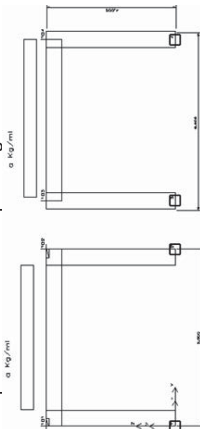
Il programma è dotato di una serie di filtri di auto diagnostica che segnalano i seguenti eventi:

- labilità della struttura
- assenza di masse
- nodi collegati ad aste nulle
- mancanza di terreno sugli elementi in fondazione
- controllo sull'assegnazione dei nodi all'impalcato
- correttezza degli spettri di progetto
- fattori di partecipazione modali
- assegnazione dei criteri di verifica agli elementi
- numerazione degli elementi strutturali
- congruenza delle connessioni tra elementi shell
- congruenza delle aree di carico
- definizione delle caratteristiche d'inerzia delle sezioni
- presenza del magrone sotto la travi tipo wink
- elementi non verificati per semi progetto allo SLU, con inserimento automatico delle armature secondo i criteri di verifica.
- elementi non verificati allo SLU per armature già inserite nell'elemento strutturale
- elementi non verificati allo SLE per armature già inserite nell'elemento strutturale

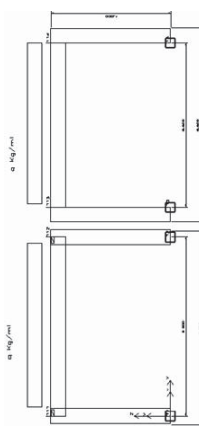
CASI PROVA

L'affidabilità dei codici utilizzati è stata testata attraverso la risoluzione di alcuni casi prova, che il Produttore fornisce all'Utente, e vengono di seguito documentati.

CASO PROVA 1 - Influenza della posizione dei nodi rispetto agli assi delle aste



I due portali sono due strutture identiche, ma il primo ha la luce teorica (da nodo a nodo) del traverso di lunghezza maggiore (5.50>5.00) e i risultati di calcolo sono diversi; se però si introducono nel traverso del primo telaio dei concetti rigidi pari a 25 cm, cioè mezzo pilastro, allora la luce flessibile dei due telai coincide praticamente e i risultati sono perfettamente coincidenti.

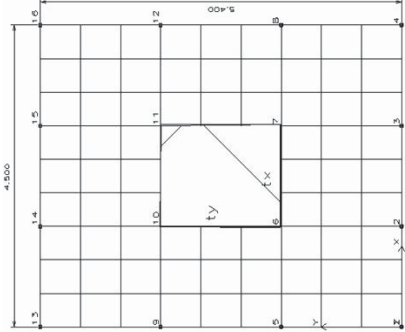


Anche in questo esempio i portali sono due strutture identiche, però il traverso del primo è più lungo e quindi i risultati saranno gli stessi se vengono introdotti sul traverso del primo portale dei concetti rigidi pari a metà pilastro.

In entrambi gli esempi (anziché introdurre i concetti rigidi) si potevano avere gli stessi risultati modificando il filo fisso del traverso del primo portale rispettivamente 8585 per l'esempio I e 8684 per l'esempio II.

Concludendo qualunque sia la posizione dei nodi rispetto agli assi delle travi e dei pilastri, le sollecitazioni (vengono prese sugli assi delle aste) sono sempre le stesse se la geometria 3D è la stessa e si scelgono oculatamente i fili fissi o si introducono i conc. rigidi. Al riguardo si ribadisce che lo schema di calcolo è quello 3D e NON lo schema unifilare. Infine si fa notare che l'equilibrio nel nodo (ad esempio N° 101) non sussiste in quanto le sollecitazione nel travverso vengono prese sull'asse dello stesso, mentre le sollecitazioni del pilastro vengono prese nel nodo e quindi in punti diversi. Per l'equilibrio quindi non bisogna prendere in considerazione solo i momenti, ma anche gli effetti delle altre sollecitazioni sul nodo rigido.

CASO PROVA 2 - Piastra rettangolare



Siano L_x ed L_y i lati della piastra ($L_y \geq L_x$) e t_x t_y i corrispondenti lati del rettangolo caricato, si ha:

p carico uniforme;
 $P = p \cdot t_x \cdot t_y$ carico totale;
 $M_{xm} = axm \cdot P$ momento al centro, agente parallelamente al lato L_x (cioè nella sezione di mezzeria parallela al lato L_y);
 $M_{ym} = aym \cdot P$ momento al centro, agente parallelamente al lato L_y (cioè nella sezione di mezzeria parallela al lato L_x).

Nel caso in esame essendo:
 $L_x = 4.5$ [m]; $L_y = 5.4$ [m]; $t_x = 1.5$ [m]; $t_y = 1.8$ [m]; $p = 5000$ [dN/mq]; si ha:
 $P = 13500$ [dN]
e per $n = 0$ sarà: $axm = 0.1377$; $aym = 0.1050$ e pertanto si ha:
 $M_{xm} = 1860$ [dNm]; $M_{ym} = 1418$ [dNm].

Se consideriamo la piastra discretizzata come in figura (9 x 9) con IperSpace si hanno i seguenti valori:

$M_{xx} = 1731$ [dNm]; $M_{yy} = 1314$ [dNm] con un errore < 8 %
Se la discretizzazione è di 15 x 15 elementi i valori sono:
 $M_{xx} = 1810$ [dNm]; $M_{yy} = 1382$ [dNm] con un errore < 3 %
Se la discretizzazione è di 21 x 21 elementi i valori sono:
 $M_{xx} = 1832$ [dNm]; $M_{yy} = 1400$ [dNm] con un errore < 1.5 %.

CASO PROVA 3 - Mensola inflessa

Prendiamo in considerazione la mensola di acciaio ($E = 20.000$ kN/cmq. e $n = 0.25$) delle dimensioni 48x4x1 cm, sollecitata all'estremità da un taglio di 40 kN, riportata a pag. 121 del testo di C.A. BREBBIA e J.J. CONNOR.

Il limite superiore dello spostamento all'estremo caricato, ottenuto con la Teoria delle travi è: cm 0.53374. Nella tabella che segue vengono riportati i valori dello spostamento per vari tipi di elementi finiti e varie discretizzazioni.

Risultati estratti dal Testo di Trebbia e Connor

Tipo di elemento	Numero elementi	Freccia di estremità	Errore %
Elemento triangolare a deformazione costante	160	0.45834	14.59
	576	0.51282	3.92
Elemento triangolare a deformazione lineare	160	0.53259	0.22
	576	0.53353	0.04
Elemento triangolare a deformazione quadratica	68	0.53059	0.17
	214	0.53259	0.22
Elemento rettangolare di primo ordine	160	0.51679	3.18
Elemento rettangolare del terzo ordine	52	0.52807	1.25

Risultati del solutore di IperSpace

Tipo di elemento	Numero elementi	Freccia di estremità	Errore %
Elemento rettangolare	16	0.5198	2.60
"	36	0.5298	0.74
"	64	0.5311	0.49
"	100	0.5322	0.29
"	144	0.5328	0.18

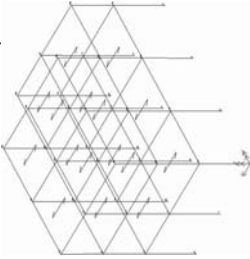
L'elemento piastra consente, con una discretizzazione molto piccola ($12 \times 3 = 36$ elementi), di avere un errore inferiore all'1%. Per ottenere risultati simili occorre eseguire non solo discretizzazioni più spinte, ma scegliere anche elementi a deformazione quadratica o di ordine superiore. L'impiego di tale elemento risulta particolarmente indicato per seguire le prescrizioni delle Norme Tecniche (D.M. 2005), che impongono la sostituzione ai pilastri snelli delle pareti. La risoluzione di questo problema di modellazione consente di evitare errori grossolani sulla stima di sforzi e deformazioni degli elementi bidimensionali.

CASO PROVA 4 - Analisi Dinamica

Si consideri la struttura a telaio riportata nelle successive figure, costituita da un materiale con modulo elastico $E=250.000$ dN/mq, nella quale le dimensioni delle sezioni trasversali dei pilastri sono:

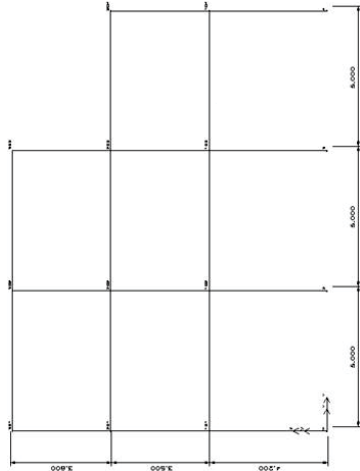
- 50x50 al primo piano
- 40x40 al secondo piano
- 35x35 al terzo piano

e le dimensioni delle sezioni trasversali delle travi sono tutte 25x60. I carichi gravitazionali sono tutti nulli a meno di un carico uniformemente distribuito, dato attraverso le aree di carico costituite dai solai, sulla struttura è di 850 dN/mq.

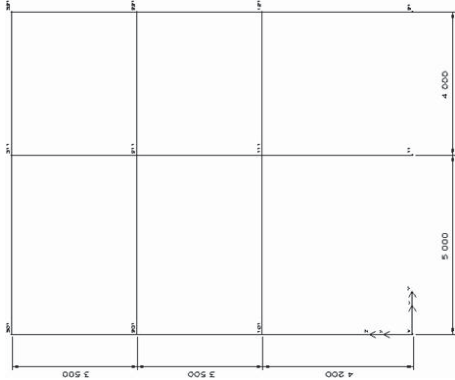




Pianta



Telaio 1



Telaio 4

Nell'ipotesi di telai shear-type, cioè con traversi infinitamente rigidi, il calcolo eseguito a mano dai prof.

Carlo Greco e Roberto Ramasco dell' Università di Napoli (esempio riportato nella pubblicazione PROGETTAZIONE E PARTICOLARI ESECUTIVI IN ZONA SISMICA – ed. ANCE), fornisce, per S=12, i seguenti risultati:

Modo	Periodo in sec.	Spostamenti dir y dei nodi del telaio 4 in mm
1	0.3227	piano primo 1.204
2	0.3160	piano secondo 2.667
3	0.2175	piano terzo 4.332
4	0.1466	
5	0.1450	

I momenti nei pilastri del telaio 4, dovuti solo al primo modo di vibrare, (uguali al piede ed in testa di ogni pilastro, essendo i traversi infinitamente rigidi) sono:
M1=5309 dNm; M2=3840 dNm; M3=2622 dNm.

Risultati di IperSpace:

a) traversi deformabili, cioè travi di sezione effettiva (25x60)

Modo	Periodo in sec	Spostamenti in mm dei nodi del pilastro N° 1
1	0.431	piano primo 2.157
2	0.416	piano secondo 5.000
3	0.326	piano terzo 7.300
4	0.173	
5	0.170	

I momenti nel pilastro N° 1 (telaio N° 4), dovuti al primo modo (non più uguali in testa e piede come nel modello shear-type) sono :
M1 max=6633 dNm; M2max=3210 dNm; M3max=2045 dNm.

Dai risultati si evince che ci sono le seguenti variazioni:

- 25 % circa sul periodo del primo modo di vibrare;
- 40 % sullo spostamento del terzo piano;
- 20 % sul momento d'incastro al piede del piano primo.

b) traversi rigidi (travi di sezione 200x200 e modulo 21000000 dN/mq)

Modo	Periodo in sec.	Spostamenti in mm dei nodi del pilastro N° 1
1	0.326	piano primo 1.244
2	0.317	piano secondo 2.728
3	0.251	piano terzo 4.203
4	0.151	
5	0.148	

I momenti nel pilastro N° 1, dovuti al primo modo (uguali in testa e piede) sono:

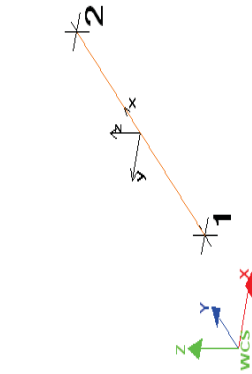
M1=5509 dNm; M2=3878 dNm; M3=2258 dNm.

In questo caso le variazioni sono contenute entro il 3 %. E' da presupporre che esse siano dovute essenzialmente al differente tipo di arrotondamento praticato tra il calcolo manuale ed il calcolo numerico, nonché al fatto che il calcolo eseguito da IperSpace è di tipo spaziale.

Si può concludere che il test su IperSpace è nettamente positivo. Inoltre la e che la qualità della soluzione il modello shear-type fornisce risultati tanto più piuttosto grossolani quanto più ci si allontana dall'ipotesi di traversi infinitamente rigidi.

PRESENTAZIONE DEI RISULTATI

I disegni dello schema statico adottato sono riportati nel fascicolo allegato alla presente relazione. E' stato impiegato il Sistema Internazionale per le unità di misura, con riferimento al daN per le forze.



Il sistema di riferimento globale rispetto al quale è stata riferita l'intera struttura è una terna di assi cartesiani sinistrorsa OXYZ (X,Y, e Z sono disposti e orientati rispettivamente secondo il pollice, l'indice ed il medio della mano destra, una volta posizionati questi ultimi a 90° tra loro).

La terna di riferimento locale per un'asta è pure una terna sinistrorsa Oxyz che ha l'asse x orientato dal nodo iniziale I dell'asta verso il nodo finale J e gli assi y e z diretti secondo gli assi geometrici della sezione con l'asse y orizzontale e orientato in modo da portarsi a coincidere con l'asse x a mezzo di una rotazione oraria di 90° e l'asse z di conseguenza.

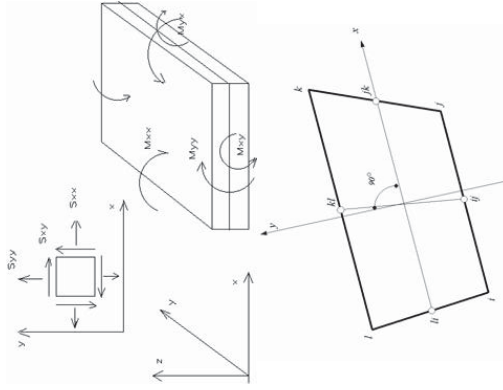
Per un'asta comunque disposta nello spazio la sua terna locale è orientata in modo tale da portarsi a coincidere con la terna globale a mezzo di rotazioni orarie degli assi locali inferiori a 180°.

- Le forze, sia sulle aste che sulle pareti o lastre, sono positive se opposte agli assi locali;
- Le forze nodali sono positive se opposte agli assi globali;
- Le coppie sono positive se sinistrorse.

Le caratteristiche di sollecitazione sono positive se sulla faccia di normale positiva sono rappresentate da vettori equiversi agli assi di riferimento locali; in particolare il vettore momento positivo rappresenta una coppia che ruota come le dita della mano destra che si chiudono quando il pollice è equi verso all'asse locale.

- Le traslazioni sono positive se concorde con gli assi globali;
- Le rotazioni sono positive se sinistrorse.

Il sistema di riferimento locale per gli elementi bidimensionali è quello riportato in figura



La terna locale per l'elemento shell è costituita dall'asse x locale che va dal nodo i al nodo j, l'asse y è diretto secondo il piano dell'elemento e orientato verso il nodo l e l'asse z di conseguenza in modo da formare la solita terna sinistrorsa. L'asse z locale rappresenta la normale positiva all'elemento.

Le sollecitazioni dell'elemento sono:

a) sforzi membranali.

$$S_{xx} = s_x$$

$$S_{yy} = s_y$$

$$S_{xy} = s_{xy}$$

b) sforzi flessionali:

$$M_{xx} \text{ momento flettente che genera } s_x, \text{ cioè intorno ad } y.$$

M_{yy} momento flettente che genera s_y , cioè intorno ad x
 M_{xy} momento torcente che genera s_{xy} .

Le sollecitazioni principali dell'elemento sono:

$$M_{1,2} = \frac{M_{xx} + M_{yy}}{2} \pm \sqrt{\left(\frac{M_{xx} - M_{yy}}{2}\right)^2 + M_{xy}^2}$$

$$S_{1,2} = \frac{S_{xx} + S_{yy}}{2} \pm \sqrt{\left(\frac{S_{xx} - S_{yy}}{2}\right)^2 + S_{xy}^2}$$

$$t_2^2 \theta = \frac{M_{xy}}{M_{xx} - M_{yy}}$$

dove q è l'angolo formato dagli assi principali di M_1 e M_2 con quelli di riferimento e

$$t_2^2 \psi = \frac{S_{xy}}{S_{xx} - S_{yy}}$$

dove ψ è l'angolo formato dagli assi principali di S_1 e S_2 con quelli di riferimento

L'elemento shell usato come piastra dà i momenti flettenti e non i tagli in direzione ortogonale all'elemento che possono ottenersi come derivazione dei momenti flettenti;

$$T_{zx} = M_{xx,x} + M_{xy,y}$$

$$T_{zy} = M_{xy,x} + M_{yy,y}$$

quando invece viene usato come lastra ci restituisce una s_x costante ed una t costante non adatti a rappresentare momenti flettenti, ma solo sforzi normali e tagli nel piano della lastra.

I tabulati di calcolo contengono due sezioni principali: la descrizione del modello di calcolo e la presentazione dei risultati.

La descrizione del modello di calcolo contiene:

- i dati generali (dimensioni)
- le coordinate nodali;
- i vincoli dei nodi e i vincoli interni delle aste, con le eventuali sconnessioni;
- le caratteristiche sezionali;
- le caratteristiche dei solai;
- le caratteristiche delle aste;
- i carichi sulle aste, sui nodi e sui muri (inclusa la distribuzione delle distorsioni imprresse, e delle variazioni e dei gradienti di temperatura);
- configurazione di sistemi che introducono stati coattivi;
- le caratteristiche dei materiali;
- legami costitutivi e criteri di verifica;
- le condizioni di carico;

La stampa dei risultati contiene:

- le combinazioni dei carichi;
- le forze sismiche agenti sulla struttura;
- gli spostamenti d'impalcato, se l'impalcato è rigido;
- gli spostamenti nodali;
- le sollecitazioni sulle membrature per ogni combinazione di carico;
- la sollecitazione sul terreno sotto travi di fondazione o platee;
- deformate;
- diagrammi sollecitazioni;

TABULATI DI INPUT - *Portali DA 1 a 7*

Dati generali	
Nome struttura	
Temperatura di riferimento [°C]	0
Fattore rigidezza assiale pilastri	1
Numero di frequenze	45
% Filtro masse libere	0.1
% Coefficiente di smorzamento viscoso	5
Spostamenti modalì con segno	SI
Deformabilità a taglio delle aste	SI
Impalcati deformabili, per carichi termici	No
Spostamento ammissibile impalcati	0.0050°h

Impalcati			
N°	Quota	Rigido	Incr.Soil.Pil
0	mm		
	0	No	1.000
1	5420	No	1.000
2	8370	No	1.000
3	13230	No	1.000

Percentuali Spostamento masse impalcati	
Posizione	% Spostamento direzione X
1	0
2	5
3	0
4	-5

Combinazioni del Sisma in X e Y e Verticale				
Comb	Pos. SismaX	Pos. SismaY	Fx	Fy
1	1	2	1	0.3
2	1	2	0.3	1
3	1	4	1	0.3
4	1	4	0.3	1
5	3	2	1	0.3
6	3	2	0.3	1
7	3	4	1	0.3
8	3	4	0.3	1
9	1	2	0.3	0.3
10	1	4	0.3	0.3
11	3	2	0.3	0.3
12	3	4	0.3	0.3

Comb. = Numero di combinazione dei sismi
Pos. SismaX = Posizione in cui viene scelto il sisma in direzione X
Pos. SismaY = Posizione in cui viene scelto il sisma in direzione Y
Fx = Fattore con cui il sisma X partecipa
Fy = Fattore con cui il sisma Y partecipa
Fz = Fattore con cui il sisma Verticale partecipa (quando richiesto)
Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx ed Fy ed Fz

Spettri di risposta

Spetro :SpetroNT(q=1)	
Il calcolo degli spettri e del fattore di struttura sono stati calcolati per la seguente tipologia di terreno e struttura	
Vita della struttura	
Tipo	Ponti imp. strategica (>100) >= 100 anni
Vita nominale(anni)	100.0
Classe d'uso	Classe IV

Coefficiente d'uso	2.000
Periodo di riferimento(anni)	200.000
Stato limite di esercizio - SLO	PVR=81.0%
Stato limite ultimo - SLV	PVR=10.0%
Periodo di ritorno SLO(anni)	TR=120.4
Periodo di ritorno SLV(anni)	TR=1898.2
Parametri del sito	
Comune	Biancavilla - (CT)
Longitudine	14.865
Latitudine	37.646
Id reticolo del sito	47419-47197-47196-47418
Valori di riferimento del sito	
Agg(TR=120.4) SLO	0.1103
F0(TR=120.4) SLO	2.5726
T°C(TR=120.4) SLO	0.281
Agg(TR=1898.2) SLV	0.2704
F0(TR=1898.2) SLV	2.5180
T°C(TR=1898.2) SLV	0.441
Coefficiente Amplificazione Topografica	SI=1.000
Categoria terreno B	
stato limite SLV	
	S=1.13
	TB=0.19
	TC=0.57
	TD=2.68
stato limite SLO	
	S=1.20
	TB=0.13
	TC=0.40
	TD=2.04
Spettro Elastico	q=1 (struttura NON dissipativa)
Smorzamento viscoso %	5.0

T	EL	EL	TSLO	SLO@q
0.00000	0.30491	0.00000	0.00000	0.13236
0.19040	0.76776	0.13299	0.13299	0.34050
0.57119	0.76776	0.39896	0.39896	0.34050
0.76304	0.57472	0.60434	0.60434	0.22482
0.95489	0.45925	0.80952	0.80952	0.16781
1.14675	0.38242	1.01479	1.01479	0.13387
1.33860	0.32761	1.22007	1.22007	0.11134
1.53045	0.28654	1.42535	1.42535	0.09531
1.72231	0.25462	1.63063	1.63063	0.08331
1.91416	0.22910	1.83591	1.83591	0.07399
2.10602	0.20823	2.04119	2.04119	0.06655
2.29787	0.19084	2.25883	2.25883	0.05435
2.48972	0.17614	2.47648	2.47648	0.04521
2.68158	0.16354	2.69412	2.69412	0.03820
2.90131	0.13970	2.91177	2.91177	0.03270
3.12105	0.12072	3.12942	3.12942	0.02831
3.34079	0.10537	3.34706	3.34706	0.02475
3.56053	0.09276	3.56471	3.56471	0.02182
3.78026	0.08229	3.78235	3.78235	0.01938
4.00000	0.07350	4.00000	4.00000	0.01733

[illegible]

Input - Aste - Tabella sezioni tipo

Nome	Raggio
cm	
1	
1	

Typo	Nome	Area	lx	ly	lt	Fx	Fy	Lx	Lx
G	IPE 140	0.0	5.412E-06	4.492E-07	2.450E-08	1.000	1.000	7	14
	IPE 100	0.0	1.710E-06	1.592E-07	8.826E-09	1.000	1.000	6	10
	HE 240 A	0.0	7.763E-05	2.769E-05	4.155E-07	1.000	1.000	24	23
	21.D 60x30x5d10	0.0	3.140E-07	1.746E-07	9.211E-09	3.785	1.660	7	6

Nome	Base	Altezza	Largezza
F60x100	60 cm	100 cm	120 cm

Aste - Geometria e vincoli

	Ni	Nf	Vinc.	Sez.	Mat.	Crit. pr.	Rot.	f.f.	xi	yi	zi	x'	y'	z'	Tiplo	L2	L3	cm
	1	1	17	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	271	271	cm
	1	17	25	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	271	271	cm
	1	17	25	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	271	271	cm
	2	19	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	0	271	271	cm
	2	19	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	0	271	271	cm
	2	19	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	0	271	271	cm
	2	19	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	0	271	271	cm
	2	19	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	0	271	271	cm
	3	20	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	0	271	271	cm
	3	20	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	0	271	271	cm
	3	20	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	0	271	271	cm
	3	20	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	0	271	271	cm
	3	20	1-1	HE 240 A	Acciao	Pressiflessione	128	5050	0	0	0	0	0	0	0	271	271	cm
	4	15	1-1	HE 240 A	Acciao	Pressiflessione	120	5050	0	0	0	0	0	0	0	271	271	cm
	4	15	1-1	HE 240 A	Acciao	Pressiflessione	120	5050	0	0	0	0	0	0	0	271	271	cm
	4	15	24	1-1	HE 240 A	Acciao	Pressiflessione	120	5050	0	0	0	0	0	0	271	271	cm

[illegible]

[illegible]

708	1116	1019	Cs-Cy	2LD 60x30x5d10	Acetario	0	8580	0	0	0	0	0	Gem.	237	307
709	1099	1118	Cs-Cy	2LD 60x30x5d10	Acetario	0	8085	0	0	0	0	0	Gem.	307	307
710	1118	1117	Cs-Cy	2LD 60x30x5d10	Acetario	0	8582	0	0	0	0	0	Gem.	243	243
711	317	1116	Cs-Cy	2LD 60x30x5d10	Acetario	0	8385	0	0	0	0	0	Gem.	314	314
712	1116	220	Cs-Cy	2LD 60x30x5d10	Acetario	0	8585	0	0	0	0	0	Gem.	278	278
713	1116	221	Cs-Cy	2LD 60x30x5d10	Acetario	0	8585	0	0	0	0	0	Gem.	278	278
714	1116	222	Cs-Cy	2LD 60x30x5d10	Acetario	0	8585	0	0	0	0	0	Gem.	222	222
715	1116	1122	Cs-Cy	2LD 60x30x5d10	Acetario	0	8585	0	0	0	0	0	Gem.	292	292
716	1122	1124	Cs-Cy	2LD 60x30x5d10	Acetario	0	8385	0	0	0	0	0	Gem.	121	121

Aste - Carichi	
Descrizione carichi aste	
UnifG	Uniforme globale
UnifL	Uniforme locale
VarG	Variabile lineare globale
VarL	Variabile lineare locale
PolG	Poligonale globale
Termico	Distorsione termica
Torcente	Carico torcente
Precomp.	Carico da precompressione
PolL	Poligonale locale

Sezione	Ni	N°	Cond.	Tipo c.	Xi	OXi	OYi	OZi	Xf	OXf	OYf	OZf
					cm	car. dist. kg/m coppie torc.			cm	car. dist. kg/m coppie torc.		
Pilastro 1												
HE 240 A	1	17	Peso Proprio	UnifG	0	0	0	60	271	0	0	60
HE 240 A	1	17	Vento X	UnifL	0	0	0	-225	271	0	0	-225
HE 240 A	1	17	Vento Y	UnifL	0	0	0	113	271	0	0	113
HE 240 A	1	17	Cantichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	17	25	Peso Proprio	UnifG	0	0	0	60	135	0	0	60
HE 240 A	17	25	Vento X	UnifL	0	0	0	-225	135	0	0	-225
HE 240 A	17	25	Vento Y	UnifL	0	0	0	113	135	0	0	113
HE 240 A	17	25	Cantichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	25	101	Peso Proprio	UnifG	0	0	0	60	136	0	0	60
HE 240 A	25	101	Vento X	UnifL	0	0	0	-225	136	0	0	-225
HE 240 A	25	101	Vento Y	UnifL	0	0	0	113	136	0	0	113
Pilastro 2												
HE 240 A	2	19	Peso Proprio	UnifG	0	0	0	60	271	0	0	60
HE 240 A	2	19	Vento X	UnifL	0	0	0	-225	271	0	0	-225
HE 240 A	2	19	Vento Y	UnifL	0	0	0	113	271	0	0	113
HE 240 A	2	19	Cantichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	19	26	Peso Proprio	UnifG	0	0	0	60	135	0	0	60
HE 240 A	19	26	Vento X	UnifL	0	0	0	-225	135	0	0	-225
HE 240 A	19	26	Vento Y	UnifL	0	0	0	113	135	0	0	113
HE 240 A	19	26	Cantichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	26	102	Peso Proprio	UnifG	0	0	0	60	136	0	0	60
HE 240 A	26	102	Vento X	UnifL	0	0	0	-225	136	0	0	-225
HE 240 A	26	102	Vento Y	UnifL	0	0	0	113	136	0	0	113
Pilastro 3												
HE 240 A	3	20	Peso Proprio	UnifG	0	0	0	60	271	0	0	60
HE 240 A	3	20	Vento X	UnifL	0	0	0	-225	271	0	0	-225
HE 240 A	3	20	Vento Y	UnifL	0	0	0	113	271	0	0	113
HE 240 A	3	20	Cantichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	20	23	Peso Proprio	UnifG	0	0	0	60	135	0	0	60
HE 240 A	20	23	Vento X	UnifL	0	0	0	-225	135	0	0	-225
HE 240 A	20	23	Vento Y	UnifL	0	0	0	113	135	0	0	113
HE 240 A	20	23	Cantichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	23	103	Peso Proprio	UnifG	0	0	0	60	136	0	0	60
HE 240 A	23	103	Vento X	UnifL	0	0	0	-225	136	0	0	-225
HE 240 A	23	103	Vento Y	UnifL	0	0	0	113	136	0	0	113
Pilastro 4												
HE 240 A	4	15	Peso Proprio	UnifG	0	0	0	60	271	0	0	60
HE 240 A	4	15	Vento X	UnifL	0	0	0	-225	271	0	0	-225
HE 240 A	4	15	Vento Y	UnifL	0	0	0	113	271	0	0	113
HE 240 A	4	15	Cantichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	15	24	Peso Proprio	UnifG	0	0	0	60	135	0	0	60
HE 240 A	15	24	Vento X	UnifL	0	0	0	-225	135	0	0	-225
HE 240 A	15	24	Vento Y	UnifL	0	0	0	113	135	0	0	113
HE 240 A	15	24	Cantichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	24	104	Peso Proprio	UnifG	0	0	0	60	136	0	0	60
HE 240 A	24	104	Vento X	UnifL	0	0	0	-225	136	0	0	-225
HE 240 A	24	104	Vento Y	UnifL	0	0	0	113	136	0	0	113
Pilastro 5												
HE 240 A	5	16	Peso Proprio	UnifG	0	0	0	60	271	0	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	OZi	Xf	QXf	OYf	OZf
HE 240 A	5	16	Vento X	UnifL	0	0	0	-225	271	0	0	-225
HE 240 A	5	16	Vento Y	UnifL	0	0	0	113	271	0	0	113
HE 240 A	5	16	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	16	21	Peso Proprio	UnifG	0	0	0	60	135	0	0	60
HE 240 A	16	21	Vento X	UnifL	0	0	0	-225	135	0	0	-225
HE 240 A	16	21	Vento Y	UnifL	0	0	0	113	135	0	0	113
HE 240 A	16	21	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	21	105	Peso Proprio	UnifG	0	0	0	60	136	0	0	60
HE 240 A	21	105	Vento X	UnifL	0	0	0	-225	136	0	0	-225
HE 240 A	21	105	Vento Y	UnifL	0	0	0	113	136	0	0	113
Pilastro 6												
HE 240 A	6	18	Peso Proprio	UnifG	0	0	0	60	271	0	0	60
HE 240 A	6	18	Vento X	UnifL	0	0	0	-225	271	0	0	-225
HE 240 A	6	18	Vento Y	UnifL	0	0	0	113	271	0	0	113
HE 240 A	6	18	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	18	22	Peso Proprio	UnifG	0	0	0	60	135	0	0	60
HE 240 A	18	22	Vento X	UnifL	0	0	0	126	135	0	0	126
HE 240 A	18	22	Vento Y	UnifL	0	0	0	-225	135	0	0	-225
HE 240 A	18	22	Vento X	UnifL	0	0	0	113	135	0	0	113
HE 240 A	18	22	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	22	106	Peso Proprio	UnifG	0	0	0	60	136	0	0	60
HE 240 A	22	106	Vento X	UnifL	0	0	0	126	136	0	0	126
HE 240 A	22	106	Vento Y	UnifL	0	0	0	-225	136	0	0	-225
HE 240 A	22	106	Vento X	UnifL	0	0	0	113	136	0	0	113
Pilastro 7												
HE 240 A	7	1001	Peso Proprio	UnifG	0	0	0	60	542	0	0	60
HE 240 A	7	1001	Vento Y	UnifL	0	0	-270	0	542	0	-270	0
HE 240 A	1001	118	Peso Proprio	UnifG	0	0	0	60	146	0	0	60
HE 240 A	1001	118	Vento Y	UnifL	0	0	-270	0	146	0	-270	0
Pilastro 8												
IPE 140	1002	117	Peso Proprio	UnifG	0	0	0	13	249	0	0	13
IPE 140	1002	117	Vento Y	UnifL	0	0	0	270	249	0	0	270
Pilastro 9												
IPE 140	1003	1111	Peso Proprio	UnifG	0	0	0	13	249	0	0	13
IPE 140	1003	1111	Vento Y	UnifL	0	0	0	270	249	0	0	270
IPE 140	1111	224	Peso Proprio	UnifG	0	0	0	13	92	0	0	13
IPE 140	1111	224	Vento Y	UnifL	0	0	0	270	92	0	0	270
Pilastro 10												
IPE 140	1004	1112	Peso Proprio	UnifG	0	0	0	13	249	0	0	13
IPE 140	1004	1112	Vento Y	UnifL	0	0	0	270	249	0	0	270
IPE 140	1112	223	Peso Proprio	UnifG	0	0	0	13	170	0	0	13
IPE 140	1112	223	Vento Y	UnifL	0	0	0	270	170	0	0	270
Pilastro 11												
IPE 140	1005	1113	Peso Proprio	UnifG	0	0	0	13	249	0	0	13
IPE 140	1005	1113	Vento Y	UnifL	0	0	0	270	249	0	0	270
IPE 140	1113	222	Peso Proprio	UnifG	0	0	0	13	233	0	0	13
IPE 140	1113	222	Vento Y	UnifL	0	0	0	270	233	0	0	270
Pilastro 12												
IPE 140	1006	1114	Peso Proprio	UnifG	0	0	0	13	249	0	0	13
IPE 140	1006	1114	Vento Y	UnifL	0	0	0	270	249	0	0	270
IPE 140	1114	221	Peso Proprio	UnifG	0	0	0	13	274	0	0	13
IPE 140	1114	221	Vento Y	UnifL	0	0	0	270	274	0	0	270
Pilastro 13												
IPE 140	1007	1115	Peso Proprio	UnifG	0	0	0	13	249	0	0	13
IPE 140	1007	1115	Vento Y	UnifL	0	0	0	270	249	0	0	270
IPE 140	1115	220	Peso Proprio	UnifG	0	0	0	13	294	0	0	13
IPE 140	1115	220	Vento Y	UnifL	0	0	0	270	294	0	0	270
Pilastro 14												
IPE 140	1008	1116	Peso Proprio	UnifG	0	0	0	13	249	0	0	13
IPE 140	1008	1116	Vento Y	UnifL	0	0	0	270	249	0	0	270
IPE 140	1116	318	Peso Proprio	UnifG	0	0	0	13	290	0	0	13
IPE 140	1116	318	Vento Y	UnifL	0	0	0	270	290	0	0	270
Pilastro 157												
IPE 140	1009	1117	Peso Proprio	UnifG	0	0	0	13	249	0	0	13
IPE 140	1009	1117	Vento Y	UnifL	0	0	0	270	249	0	0	270
IPE 140	1117	317	Peso Proprio	UnifG	0	0	0	13	256	0	0	13

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	OZi	Xf	QXf	OYf	OZf
IPE 140	1117	317	Vento Y	UnifL	0	0	0	270	256	0	0	270
Pilastro 207												
HE 240 A	207	1010	Peso Proprio	UnifG	0	0	0	60	50	0	0	60
HE 240 A	207	1010	Vento X	UnifL	0	0	0	-113	50	0	0	-113
HE 240 A	207	1010	Vento Y	UnifL	0	0	0	225	50	0	0	225
HE 240 A	207	1010	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	207	1010	Peso Proprio	UnifG	0	0	0	60	187	0	0	60
HE 240 A	207	1010	Vento Y	UnifL	0	0	0	225	187	0	0	225
Pilastro 208												
HE 240 A	208	308	Peso Proprio	UnifG	0	0	0	60	486	0	0	60
HE 240 A	208	308	Vento X	UnifL	0	0	0	-113	486	0	0	-113
HE 240 A	208	308	Vento Y	UnifL	0	0	0	225	486	0	0	225
HE 240 A	208	308	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Pilastro 209												
HE 240 A	209	309	Peso Proprio	UnifG	0	0	0	60	486	0	0	60
HE 240 A	209	309	Vento X	UnifL	0	0	0	-113	486	0	0	-113
HE 240 A	209	309	Vento Y	UnifL	0	0	0	225	486	0	0	225
HE 240 A	209	309	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Pilastro 210												
HE 240 A	210	310	Peso Proprio	UnifG	0	0	0	60	486	0	0	60
HE 240 A	210	310	Vento X	UnifL	0	0	0	-113	486	0	0	-113
HE 240 A	210	310	Vento Y	UnifL	0	0	0	225	486	0	0	225
HE 240 A	210	310	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Pilastro 211												
HE 240 A	211	311	Peso Proprio	UnifG	0	0	0	60	486	0	0	60
HE 240 A	211	311	Vento X	UnifL	0	0	0	-113	486	0	0	-113
HE 240 A	211	311	Vento Y	UnifL	0	0	0	225	486	0	0	225
HE 240 A	211	311	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Pilastro 212												
HE 240 A	212	312	Peso Proprio	UnifG	0	0	0	60	486	0	0	60
HE 240 A	212	312	Vento X	UnifL	0	0	0	-113	486	0	0	-113
HE 240 A	212	312	Vento Y	UnifL	0	0	0	225	486	0	0	225
HE 240 A	212	312	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Pilastro 1228												
HE 240 A	1010	1118	Peso Proprio	UnifG	0	0	0	60	249	0	0	60
HE 240 A	1010	1118	Vento Y	UnifL	0	0	0	225	249	0	0	225
Trave 707												
2LD	117	1111	Peso Proprio	UnifG	0	0	0	7	115	0	0	7
60x30x5d10												
Trave 708												
2LD	1111	1112	Peso Proprio	UnifG	0	0	0	7	115	0	0	7
60x30x5d10												
Trave 709												
2LD	1112	1113	Peso Proprio	UnifG	0	0	0	7	115	0	0	7
60x30x5d10												
Trave 710												
2LD	1113	1114	Peso Proprio	UnifG	0	0	0	7	115	0	0	7
60x30x5d10												
Trave 711												
2LD	1114	1115	Peso Proprio	UnifG	0	0	0	7	115	0	0	7
60x30x5d10												
Trave 712												
2LD	1115	1116	Peso Proprio	UnifG	0	0	0	7	115	0	0	7
60x30x5d10												
Trave 713												
2LD	1116	1117	Peso Proprio	UnifG	0	0	0	7	115	0	0	7
60x30x5d10												
Trave 714												
2LD	1117	1118	Peso Proprio	UnifG	0	0	0	7	115	0	0	7
60x30x5d10												
Trave 1001												
IPE 100	118	116	Peso Proprio	UnifG	0	0	0	8	95	0	0	8
IPE 100	118	116	QP Solai	PolG	35	0	0	88	35	0	0	140
					66	0	0	140	95	0	0	89
IPE 100	118	116	QV Solai	PolG	0	0	0	28	35	0	0	45

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					35	0	0	45	66	0	0	45
IPE 100	118	116	Neve	PolG	66	0	0	45	95	0	0	29
IPE 100	118	116	Neve	PolG	35	0	0	44	95	0	0	44
IPE 100	118	116	Vento X	PolG	66	0	0	43	95	0	0	11
IPE 100	118	116	Vento X	PolG	66	0	0	67	66	0	0	67
IPE 100	118	116	Vento X	PolG	66	0	0	67	95	0	0	17
IPE 100	118	116	Carichi termici	Termico	35	0	0	68	95	0	0	68
Trave 1002												
IPE 100	117	115	Peso Proprio	UnitG	0	0	0	8	101	0	0	8
IPE 100	117	115	QP Solai	PolG	0	0	0	85	35	0	0	135
IPE 100	117	115	QV Solai	PolG	72	0	0	135	101	0	0	88
IPE 100	117	115	Neve	PolG	35	0	0	27	35	0	0	43
IPE 100	117	115	Neve	PolG	72	0	0	43	101	0	0	28
IPE 100	117	115	Neve	PolG	35	0	0	12	35	0	0	43
IPE 100	117	115	Neve	PolG	35	0	0	43	101	0	0	43
IPE 100	117	115	Vento X	PolG	72	0	0	41	72	0	0	41
IPE 100	117	115	Vento X	PolG	0	0	0	18	35	0	0	67
IPE 100	117	115	Vento X	PolG	35	0	0	67	101	0	0	67
IPE 100	117	115	Carichi termici	Termico	72	0	0	64	72	0	0	64
Trave 1003												
IPE 100	224	219	Peso Proprio	UnitG	0	0	0	8	107	0	0	8
IPE 100	224	219	QP Solai	PolG	0	0	0	81	35	0	0	128
IPE 100	224	219	QV Solai	PolG	35	0	0	128	78	0	0	128
IPE 100	224	219	Neve	PolG	78	0	0	26	35	0	0	85
IPE 100	224	219	Neve	PolG	35	0	0	41	78	0	0	41
IPE 100	224	219	Neve	PolG	78	0	0	41	107	0	0	27
IPE 100	224	219	Neve	PolG	0	0	0	38	78	0	0	38
IPE 100	224	219	Vento X	PolG	78	0	0	12	35	0	0	41
IPE 100	224	219	Vento X	PolG	35	0	0	41	107	0	0	41
IPE 100	224	219	Vento X	PolG	78	0	0	59	78	0	0	59
IPE 100	224	219	Vento X	PolG	78	0	0	59	107	0	0	18
IPE 100	224	219	Carichi termici	Termico	35	0	0	19	35	0	0	64
Trave 1004												
IPE 100	223	218	Peso Proprio	UnitG	0	0	0	8	113	0	0	8
IPE 100	223	218	QP Solai	PolG	0	0	0	77	35	0	0	119
IPE 100	223	218	QV Solai	PolG	35	0	0	119	84	0	0	119
IPE 100	223	218	Neve	PolG	84	0	0	119	113	0	0	80
IPE 100	223	218	Neve	PolG	0	0	0	25	35	0	0	38
IPE 100	223	218	Neve	PolG	35	0	0	38	84	0	0	38
IPE 100	223	218	Neve	PolG	84	0	0	38	113	0	0	26
IPE 100	223	218	Vento X	PolG	0	0	0	12	35	0	0	38
IPE 100	223	218	Vento X	PolG	35	0	0	38	113	0	0	38
IPE 100	223	218	Vento X	PolG	84	0	0	36	84	0	0	36
IPE 100	223	218	Vento X	PolG	0	0	0	18	35	0	0	59
IPE 100	223	218	Vento X	PolG	35	0	0	59	113	0	0	59
IPE 100	223	218	Carichi termici	Termico	84	0	0	55	113	0	0	17
Trave 1005												
IPE 100	222	217	Peso Proprio	UnitG	0	0	0	8	119	0	0	8
IPE 100	222	217	QP Solai	PolG	0	0	0	71	35	0	0	110
IPE 100	222	217	QV Solai	PolG	35	0	0	110	90	0	0	110

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	222	217	QV Solai	PolG	90	0	0	110	119	0	0	75
IPE 100	222	217	Neve	PolG	35	0	0	35	90	0	0	35
IPE 100	222	217	Neve	PolG	90	0	0	33	90	0	0	33
IPE 100	222	217	Neve	PolG	90	0	0	33	119	0	0	11
IPE 100	222	217	Vento X	PolG	35	0	0	12	35	0	0	36
IPE 100	222	217	Vento X	PolG	90	0	0	50	90	0	0	50
IPE 100	222	217	Vento X	PolG	90	0	0	50	119	0	0	17
IPE 100	222	217	Carichi termici	Termico	35	0	0	18	35	0	0	55
Trave 1006												
IPE 100	221	216	Peso Proprio	UnitG	0	0	0	8	125	0	0	8
IPE 100	221	216	QP Solai	PolG	35	0	0	66	35	0	0	100
IPE 100	221	216	QV Solai	PolG	96	0	0	100	125	0	0	69
IPE 100	221	216	Neve	PolG	35	0	0	32	96	0	0	32
IPE 100	221	216	Neve	PolG	96	0	0	32	125	0	0	22
IPE 100	221	216	Neve	PolG	0	0	0	11	35	0	0	33
IPE 100	221	216	Vento X	PolG	35	0	0	30	96	0	0	30
IPE 100	221	216	Vento X	PolG	96	0	0	30	125	0	0	10
IPE 100	221	216	Vento X	PolG	0	0	0	17	35	0	0	50
IPE 100	221	216	Vento X	PolG	35	0	0	50	125	0	0	50
IPE 100	221	216	Carichi termici	Termico	96	0	0	46	96	0	0	46
Trave 1007												
IPE 100	220	215	Peso Proprio	UnitG	0	0	0	8	131	0	0	8
IPE 100	220	215	QP Solai	PolG	0	0	0	61	35	0	0	92
IPE 100	220	215	QV Solai	PolG	35	0	0	92	102	0	0	92
IPE 100	220	215	Neve	PolG	102	0	0	20	35	0	0	29
IPE 100	220	215	Neve	PolG	35	0	0	29	102	0	0	29
IPE 100	220	215	Neve	PolG	102	0	0	29	131	0	0	20
IPE 100	220	215	Vento X	PolG	0	0	0	27	102	0	0	27
IPE 100	220	215	Vento X	PolG	102	0	0	27	131	0	0	10
IPE 100	220	215	Vento X	PolG	0	0	0	11	35	0	0	30
IPE 100	220	215	Vento X	PolG	35	0	0	30	131	0	0	30
IPE 100	220	215	Vento X	PolG	0	0	0	16	35	0	0	46
IPE 100	220	215	Vento X	PolG	35	0	0	46	131	0	0	46
IPE 100	220	215	Carichi termici	Termico	102	0	0	42	102	0	0	42
Trave 1008												
IPE 100	318	316	Peso Proprio	UnitG	0	0	0	8	137	0	0	8
IPE 100	318	316	QP Solai	PolG	0	0	0	59	35	0	0	86
IPE 100	318	316	QV Solai	PolG	35	0	0	86	108	0	0	86
IPE 100	318	316	Neve	PolG	108	0	0	86	137	0	0	60
IPE 100	318	316	Neve	PolG	0	0	0	19	35	0	0	28
IPE 100	318	316	Neve	PolG	35	0	0	28	108	0	0	28
IPE 100	318	316	Neve	PolG	108	0	0	28	137	0	0	19
IPE 100	318	316	Neve	PolG	0	0	0	26	108	0	0	26
IPE 100	318	316	Vento X	PolG	108	0	0	26	137	0	0	10
IPE 100	318	316	Vento X	PolG	0	0	0	10	35	0	0	27
IPE 100	318	316	Vento X	PolG	35	0	0	27	137	0	0	27
IPE 100	318	316	Vento X	PolG	0	0	0	16	35	0	0	42
IPE 100	318	316	Vento X	PolG	35	0	0	42	137	0	0	42
IPE 100	318	316	Carichi termici	Termico	108	0	0	41	108	0	0	41
Trave 1009												
IPE 100	317	315	Peso Proprio	UnitG	0	0	0	8	143	0	0	8

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	317	315	QP Solai	PolG	0	0	0	60	35	0	0	86
				35	0	0	86	114	0	0	86	
				114	0	0	86	143	0	0	60	
IPE 100	317	315	QV Solai	PolG	0	0	0	19	35	0	0	28
				35	0	0	28	114	0	0	28	
				114	0	0	28	143	0	0	19	
IPE 100	317	315	Neve	PolG	0	0	0	10	35	0	0	26
				35	0	0	26	143	0	0	26	
				PolG	0	0	0	27	114	0	0	27
IPE 100	317	315	Neve	PolG	0	0	0	27	143	0	0	11
				114	0	0	16	35	0	0	41	
				35	0	0	41	143	0	0	41	
IPE 100	317	315	Vento X	PolG	0	0	0	42	114	0	0	42
				114	0	0	42	143	0	0	17	
				Termico	AXY=15°C,AXZ=15°C							
Trave 1010	307	308	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
	307	308		PolG	0	0	0	18	35	0	0	44
			QP Solai	35	0	0	44	149	0	0	44	
			QV Solai	PolG	0	0	0	6	35	0	0	14
				35	0	0	14	149	0	0	14	
			Neve	PolG	0	0	0	11	35	0	0	27
				35	0	0	27	149	0	0	27	
			Vento X	PolG	0	0	0	17	35	0	0	42
				35	0	0	42	149	0	0	42	
			Termico	AXY=15°C,AXZ=15°C								
Trave 1011	101	102	Peso Proprio	UnifG	0	0	0	8	89	0	0	8
	101	102		PolG	0	0	0	71	60	0	0	71
			QP Solai	60	0	0	71	89	0	0	17	
			QV Solai	PolG	0	0	0	23	60	0	0	23
				60	0	0	23	89	0	0	6	
			Neve	PolG	0	0	0	44	60	0	0	44
				60	0	0	44	89	0	0	11	
			Vento X	PolG	0	0	0	68	60	0	0	68
				60	0	0	68	89	0	0	17	
			Termico	AXY=15°C,AXZ=15°C								
Trave 1012	116	124	Peso Proprio	UnifG	0	0	0	8	96	0	0	8
	116	124		PolG	0	0	0	84	29	0	0	140
			QP Solai	29	0	0	140	73	0	0	140	
				73	0	0	140	96	0	0	85	
			QV Solai	PolG	0	0	0	27	29	0	0	45
				29	0	0	45	73	0	0	45	
			Neve	PolG	73	0	0	45	96	0	0	27
				29	0	0	9	29	0	0	44	
			Neve	PolG	0	0	0	44	96	0	0	44
				29	0	0	43	73	0	0	43	
Trave 1013	116	124	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
	116	124		PolG	0	0	0	81	29	0	0	135
			QP Solai	29	0	0	135	79	0	0	135	
				79	0	0	135	102	0	0	84	
			QV Solai	PolG	0	0	0	26	29	0	0	43
				29	0	0	43	79	0	0	43	
				79	0	0	43	102	0	0	27	
			Neve	PolG	0	0	0	41	79	0	0	41
				79	0	0	41	102	0	0	9	
			Neve	PolG	0	0	0	9	29	0	0	43

Sezione	Ni	Nf	Cond	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	115	123	Vento X	PolG	0	0	0	15	29	0	0	67
					29	0	0	67	102	0	0	67
IPE 100	115	123	Vento X	PolG	0	0	0	64	79	0	0	64
					79	0	0	64	102	0	0	14
IPE 100	115	123	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1014												
IPE 100	219	239	Peso Proprio	UnifG	0	0	0	8	108	0	0	8
			QP Solai	PolG	0	0	0	77	29	0	0	128
IPE 100	219	239		PolG	29	0	0	128	85	0	0	128
					85	0	0	128	108	0	0	81
IPE 100	219	239	QV Solai	PolG	0	0	0	25	29	0	0	41
					29	0	0	41	85	0	0	41
IPE 100	219	239	Neve	PolG	85	0	0	41	108	0	0	26
					29	0	0	10	29	0	0	41
IPE 100	219	239	Neve	PolG	0	0	0	41	108	0	0	41
					85	0	0	38	85	0	0	38
IPE 100	219	239	Vento X	PolG	0	0	0	38	108	0	0	9
					85	0	0	59	85	0	0	59
IPE 100	219	239	Vento X	PolG	0	0	0	59	108	0	0	14
					29	0	0	15	29	0	0	64
IPE 100	219	239	Vento X	PolG	0	0	0	64	108	0	0	64
					29	0	0	64	108	0	0	64
IPE 100	219	239	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1015												
IPE 100	218	238	Peso Proprio	UnifG	0	0	0	8	114	0	0	8
			QP Solai	PolG	0	0	0	73	29	0	0	119
IPE 100	218	238		PolG	29	0	0	119	91	0	0	119
					91	0	0	119	114	0	0	76
IPE 100	218	238	QV Solai	PolG	0	0	0	23	29	0	0	38
					29	0	0	38	91	0	0	38
IPE 100	218	238	Neve	PolG	91	0	0	38	114	0	0	24
					91	0	0	36	91	0	0	36
IPE 100	218	238	Neve	PolG	0	0	0	36	114	0	0	9
					91	0	0	9	29	0	0	38
IPE 100	218	238	Neve	PolG	0	0	0	38	114	0	0	38
					29	0	0	15	29	0	0	59
IPE 100	218	238	Vento X	PolG	0	0	0	59	114	0	0	59
					29	0	0	55	91	0	0	55
IPE 100	218	238	Vento X	PolG	0	0	0	55	91	0	0	14
					91	0	0	55	114	0	0	14
IPE 100	218	238	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1016												
IPE 100	217	237	Peso Proprio	UnifG	0	0	0	8	120	0	0	8
			QP Solai	PolG	0	0	0	67	29	0	0	110
IPE 100	217	237		PolG	29	0	0	110	97	0	0	110
					97	0	0	110	120	0	0	71
IPE 100	217	237	QV Solai	PolG	0	0	0	22	29	0	0	35
					29	0	0	35	97	0	0	35
IPE 100	217	237	Neve	PolG	97	0	0	35	120	0	0	23
					97	0	0	33	97	0	0	33
IPE 100	217	237	Neve	PolG	0	0	0	33	120	0	0	9
					29	0	0	9	29	0	0	36
IPE 100	217	237	Vento X	PolG	0	0	0	36	120	0	0	36
					29	0	0	50	97	0	0	50
IPE 100	217	237	Vento X	PolG	0	0	0	50	120	0	0	13
					97	0	0	14	29	0	0	55
IPE 100	217	237	Vento X	PolG	0	0	0	14	29	0	0	55
					29	0	0	55	120	0	0	55
IPE 100	217	237	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1017												
IPE 100	216	236	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
			QP Solai	PolG	0	0	0	62	29	0	0	100
IPE 100	216	236		PolG	29	0	0	100	103	0	0	100
					103	0	0	100	126	0	0	66
IPE 100	216	236	QV Solai	PolG	0	0	0	20	29	0	0	32
					29	0	0	32	103	0	0	32
IPE 100	216	236	Neve	PolG	103	0	0	32	126	0	0	21
					103	0	0	32	126	0	0	21
IPE 100	216	236	Neve	PolG	0	0	0	9	29	0	0	33
					29	0	0	33	126	0	0	33

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	216	236	Neve	PolG	0	0	0	0	30	103	0	0
IPE 100	216	236	Vento X	PolG	103	0	0	0	30	126	0	0
IPE 100	216	236	Vento X	PolG	29	0	0	0	14	29	0	0
IPE 100	216	236	Vento X	PolG	0	0	0	0	50	126	0	0
IPE 100	216	236	Vento X	PolG	0	0	0	0	46	103	0	0
IPE 100	216	236	Carichi termici	Termico	103	0	0	0	46	126	0	0
Trave 1018 AXY=15°C,AXZ=15°C												
IPE 100	215	235	Peso Proprio	UnifG	0	0	0	0	8	132	0	0
IPE 100	215	235	QP Solai	PolG	0	0	0	0	58	29	0	0
IPE 100	215	235	Neve	PolG	29	0	0	0	92	109	0	0
IPE 100	215	235	QV Solai	PolG	109	0	0	0	92	132	0	0
IPE 100	215	235	Neve	PolG	0	0	0	0	19	29	0	0
IPE 100	215	235	QP Solai	PolG	29	0	0	0	29	109	0	0
IPE 100	215	235	Neve	PolG	109	0	0	0	29	132	0	0
IPE 100	215	235	QV Solai	PolG	0	0	0	0	27	109	0	0
IPE 100	215	235	Neve	PolG	109	0	0	0	27	132	0	0
IPE 100	215	235	Vento X	PolG	29	0	0	0	30	132	0	0
IPE 100	215	235	Vento X	PolG	0	0	0	0	42	109	0	0
IPE 100	215	235	Vento X	PolG	109	0	0	0	42	132	0	0
IPE 100	215	235	Vento X	PolG	0	0	0	0	13	29	0	0
IPE 100	215	235	Carichi termici	Termico	29	0	0	0	46	132	0	0
Trave 1019 AXY=15°C,AXZ=15°C												
IPE 100	316	324	Peso Proprio	UnifG	0	0	0	0	8	138	0	0
IPE 100	316	324	QP Solai	PolG	0	0	0	0	55	29	0	0
IPE 100	316	324	Neve	PolG	29	0	0	0	86	115	0	0
IPE 100	316	324	QV Solai	PolG	115	0	0	0	86	138	0	0
IPE 100	316	324	Neve	PolG	0	0	0	0	18	29	0	0
IPE 100	316	324	Vento X	PolG	29	0	0	0	28	115	0	0
IPE 100	316	324	Vento X	PolG	115	0	0	0	28	138	0	0
IPE 100	316	324	Carichi termici	Termico	115	0	0	0	28	138	0	0
Trave 1020 AXY=15°C,AXZ=15°C												
IPE 100	315	323	Peso Proprio	UnifG	0	0	0	0	8	144	0	0
IPE 100	315	323	QP Solai	PolG	0	0	0	0	57	29	0	0
IPE 100	315	323	Neve	PolG	29	0	0	0	86	121	0	0
IPE 100	315	323	QV Solai	PolG	121	0	0	0	86	144	0	0
IPE 100	315	323	Neve	PolG	0	0	0	0	18	29	0	0
IPE 100	315	323	Vento X	PolG	29	0	0	0	28	121	0	0
IPE 100	315	323	Vento X	PolG	121	0	0	0	28	144	0	0
IPE 100	315	323	Carichi termici	Termico	121	0	0	0	28	144	0	0
Trave 1021 AXY=15°C,AXZ=15°C												
IPE 100	308	309	Peso Proprio	UnifG	0	0	0	0	8	147	0	0
IPE 100	308	309	QP Solai	PolG	0	0	0	0	14	29	0	0
IPE 100	308	309	QV Solai	PolG	29	0	0	0	44	149	0	0
IPE 100	308	309	Neve	PolG	0	0	0	0	5	29	0	0
IPE 100	308	309	Carichi termici	Termico	29	0	0	0	14	149	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	308	309	Vento X	PolG	0	0	0	0	14	29	0	0
IPE 100	308	309	Carichi termici	Termico	29	0	0	0	42	149	0	0
Trave 1022 AXY=15°C,AXZ=15°C												
IPE 100	102	103	Peso Proprio	UnifG	0	0	0	0	8	90	0	0
IPE 100	102	103	QP Solai	PolG	0	0	0	0	71	67	0	0
IPE 100	102	103	QV Solai	PolG	67	0	0	0	23	67	0	0
IPE 100	102	103	Neve	PolG	67	0	0	0	23	90	0	0
IPE 100	102	103	Vento X	PolG	0	0	0	0	44	67	0	0
IPE 100	102	103	Carichi termici	Termico	67	0	0	0	68	67	0	0
Trave 1023 AXY=15°C,AXZ=15°C												
IPE 100	124	122	Peso Proprio	UnifG	0	0	0	0	8	95	0	0
IPE 100	124	122	QP Solai	PolG	0	0	0	0	81	22	0	0
IPE 100	124	122	QV Solai	PolG	22	0	0	0	140	79	0	0
IPE 100	124	122	Neve	PolG	79	0	0	0	140	95	0	0
IPE 100	124	122	Vento X	PolG	0	0	0	0	26	22	0	0
IPE 100	124	122	Carichi termici	Termico	22	0	0	0	45	79	0	0
Trave 1024 AXY=15°C,AXZ=15°C												
IPE 100	123	121	Peso Proprio	UnifG	0	0	0	0	8	101	0	0
IPE 100	123	121	QP Solai	PolG	0	0	0	0	78	22	0	0
IPE 100	123	121	QV Solai	PolG	22	0	0	0	135	85	0	0
IPE 100	123	121	Neve	PolG	85	0	0	0	135	101	0	0
IPE 100	123	121	Vento X	PolG	0	0	0	0	25	22	0	0
IPE 100	123	121	Carichi termici	Termico	22	0	0	0	43	85	0	0
Trave 1025 AXY=15°C,AXZ=15°C												
IPE 100	123	121	Peso Proprio	UnifG	0	0	0	0	8	101	0	0
IPE 100	123	121	QP Solai	PolG	0	0	0	0	7	22	0	0
IPE 100	123	121	QV Solai	PolG	22	0	0	0	43	101	0	0
IPE 100	123	121	Neve	PolG	85	0	0	0	41	85	0	0
IPE 100	123	121	Vento X	PolG	0	0	0	0	41	101	0	0
IPE 100	123	121	Carichi termici	Termico	85	0	0	0	64	85	0	0
Trave 1026 AXY=15°C,AXZ=15°C												
IPE 100	239	234	Peso Proprio	UnifG	0	0	0	0	8	107	0	0
IPE 100	239	234	QP Solai	PolG	0	0	0	0	74	22	0	0
IPE 100	239	234	QV Solai	PolG	22	0	0	0	128	91	0	0
IPE 100	239	234	Neve	PolG	91	0	0	0	128	107	0	0
IPE 100	239	234	Vento X	PolG	0	0	0	0	24	22	0	0
IPE 100	239	234	Carichi termici	Termico	22	0	0	0	41	91	0	0
Trave 1027 AXY=15°C,AXZ=15°C												
IPE 100	239	234	Peso Proprio	UnifG	0	0	0	0	8	107	0	0
IPE 100	239	234	QP Solai	PolG	0	0	0	0	7	22	0	0
IPE 100	239	234	QV Solai	PolG	22	0	0	0	12	22	0	0
IPE 100	239	234	Neve	PolG	22	0	0	0	64	107	0	0
IPE 100	239	234	Vento X	PolG	0	0	0	0	59	91	0	0
IPE 100	239	234	Carichi termici	Termico	91	0	0	0	59	107	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	238	233	Peso Proprio	UnifG	0	0	0	8	113	0	0	8
IPE 100	238	233	QP Solai	PolG	0	0	0	70	22	0	0	119
					22	0	0	119	97	0	0	119
IPE 100	238	233	QV Solai	PolG	97	0	0	119	113	0	0	73
					0	0	0	22	22	0	0	38
					22	0	0	38	97	0	0	38
IPE 100	238	233	Neve	PolG	97	0	0	38	113	0	0	23
					0	0	0	7	22	0	0	38
IPE 100	238	233	Neve	PolG	22	0	0	38	113	0	0	38
					0	0	0	36	97	0	0	36
IPE 100	238	233	Vento X	PolG	97	0	0	36	113	0	0	7
					0	0	0	11	22	0	0	59
IPE 100	238	233	Vento X	PolG	22	0	0	59	113	0	0	59
					0	0	0	55	97	0	0	55
IPE 100	238	233		PolG	97	0	0	55	113	0	0	11
					0	0	0	55	113	0	0	11
Trave 1027			Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
IPE 100	237	232	Peso Proprio	UnifG	0	0	0	8	119	0	0	8
IPE 100	237	232	QP Solai	PolG	0	0	0	64	22	0	0	110
					22	0	0	110	103	0	0	110
IPE 100	237	232	QV Solai	PolG	103	0	0	110	119	0	0	68
					0	0	0	21	22	0	0	35
					22	0	0	35	103	0	0	35
IPE 100	237	232	Neve	PolG	103	0	0	35	119	0	0	22
					0	0	0	7	22	0	0	36
IPE 100	237	232	Neve	PolG	22	0	0	36	119	0	0	36
					0	0	0	33	103	0	0	33
IPE 100	237	232	Vento X	PolG	103	0	0	33	119	0	0	7
					0	0	0	11	22	0	0	55
IPE 100	237	232	Vento X	PolG	22	0	0	55	119	0	0	55
					0	0	0	50	103	0	0	50
IPE 100	237	232		PolG	103	0	0	50	119	0	0	10
					0	0	0	50	119	0	0	10
Trave 1028			Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
IPE 100	236	231	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	236	231	QP Solai	PolG	0	0	0	59	22	0	0	100
					22	0	0	100	109	0	0	100
IPE 100	236	231	QV Solai	PolG	109	0	0	100	126	0	0	63
					0	0	0	19	22	0	0	32
					22	0	0	32	109	0	0	32
IPE 100	236	231	Neve	PolG	109	0	0	32	126	0	0	20
					0	0	0	7	22	0	0	33
IPE 100	236	231	Neve	PolG	22	0	0	33	126	0	0	33
					0	0	0	30	109	0	0	30
IPE 100	236	231	Vento X	PolG	109	0	0	30	126	0	0	6
					0	0	0	11	22	0	0	50
IPE 100	236	231	Vento X	PolG	22	0	0	50	126	0	0	50
					0	0	0	46	109	0	0	46
IPE 100	236	231		PolG	109	0	0	46	126	0	0	10
					0	0	0	46	126	0	0	10
Trave 1029			Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
IPE 100	235	230	Peso Proprio	UnifG	0	0	0	8	132	0	0	8
IPE 100	235	230	QP Solai	PolG	0	0	0	55	22	0	0	92
					22	0	0	92	115	0	0	92
IPE 100	235	230	QV Solai	PolG	115	0	0	92	132	0	0	58
					0	0	0	18	22	0	0	29
					22	0	0	29	115	0	0	29
IPE 100	235	230	Neve	PolG	115	0	0	29	132	0	0	19
					0	0	0	27	115	0	0	27
IPE 100	235	230	Neve	PolG	115	0	0	27	132	0	0	6
					0	0	0	7	22	0	0	30
IPE 100	235	230	Vento X	PolG	22	0	0	30	132	0	0	30
					0	0	0	42	115	0	0	42
IPE 100	235	230	Vento X	PolG	115	0	0	42	132	0	0	10
					0	0	0	10	22	0	0	46
IPE 100	235	230		PolG	22	0	0	46	132	0	0	46
					0	0	0	46	132	0	0	46

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	235	230		Termico	ΔXY=15°C, ΔXZ=15°C							
Trave 1030												
IPE 100	324	322	Peso Proprio	UnifG	0	0	0	8	138	0	0	8
IPE 100	324	322	QP Solai	PolG	0	0	0	52	22	0	0	86
					22	0	0	86	121	0	0	86
IPE 100			QV Solai	PolG	121	0	0	86	138	0	0	54
					0	0	0	17	22	0	0	28
IPE 100	324	322	Neve	PolG	22	0	0	28	121	0	0	28
					121	0	0	26	121	0	0	17
IPE 100	324	322		PolG	121	0	0	26	138	0	0	26
					0	0	0	6	22	0	0	6
IPE 100	324	322	Neve	PolG	22	0	0	6	22	0	0	27
					22	0	0	10	22	0	0	42
IPE 100	324	322	Vento X	PolG	22	0	0	42	138	0	0	42
					22	0	0	41	121	0	0	41
IPE 100	324	322	Vento X	PolG	121	0	0	41	138	0	0	10
					0	0	0	41	138	0	0	10
Trave 1031			Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
IPE 100	324	322	Peso Proprio	UnifG	0	0	0	8	144	0	0	8
IPE 100	323	321	QP Solai	PolG	0	0	0	54	22	0	0	86
					22	0	0	86	127	0	0	86
IPE 100			QV Solai	PolG	127	0	0	86	144	0	0	53
					0	0	0	17	22	0	0	28
IPE 100	323	321	Neve	PolG	22	0	0	28	127	0	0	28
					127	0	0	28	144	0	0	17
IPE 100	323	321	Vento X	PolG	127	0	0	27	127	0	0	27
					0	0	0	27	144	0	0	7
IPE 100	323	321		PolG	127	0	0	6	22	0	0	26
					22	0	0	26	144	0	0	26
IPE 100	323	321	Vento X	PolG	22	0	0	42	127	0	0	42
					127	0	0	42	144	0	0	10
IPE 100	323	321	Vento X	PolG	127	0	0	10	22	0	0	41
					22	0	0	41	144	0	0	41
Trave 1032			Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
IPE 100	309	310	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	309	310	QP Solai	PolG	0	0	0	11	22	0	0	44
					22	0	0	44	150	0	0	44
IPE 100	309	310	QV Solai	PolG	0	0	0	4	22	0	0	14
					22	0	0	14	150	0	0	14
IPE 100	309	310	Neve	PolG	0	0	0	7	22	0	0	27
					22	0	0	27	150	0	0	27
IPE 100	309	310	Vento X	PolG	0	0	0	11	22	0	0	42
					22	0	0	42	150	0	0	42
Trave 1033			Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
IPE 100	103	104	Peso Proprio	UnifG	0	0	0	8	89	0	0	8
IPE 100	103	104	QP Solai	PolG	0	0	0	71	73	0	0	71
					73	0	0	71	89	0	0	11
IPE 100	103	104	QV Solai	PolG	0	0	0	23	73	0	0	23
					73	0	0	23	89	0	0	3
IPE 100	103	104	Neve	PolG	0	0	0	44	73	0	0	44
					73	0	0	44	89	0	0	7
IPE 100	103	104	Vento X	PolG	0	0	0	68	73	0	0	68
					73	0	0	68	89	0	0	10
Trave 1034			Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
IPE 100	122	120	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	122	120	QP Solai	PolG	0	0	0	84	16	0	0	140
					16	0	0	140	133	0	0	140
IPE 100	122	120	QV Solai	PolG	133	0	0	140	149	0	0	86
					0	0	0	27	16	0	0	45
IPE 100	122	120	Vento X	PolG	16	0	0	45	133	0	0	45
					133	0	0	45	149	0	0	27
IPE 100	122	120		PolG	133	0	0	9	16	0	0	44
					0	0	0	9	16	0	0	44

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	122	120	Neve	PolG	16	0	0	44	149	0	0	44
IPE 100	122	120	Neve	PolG	0	0	0	43	133	0	0	43
IPE 100	122	120	Vento X	PolG	133	0	0	43	149	0	0	9
IPE 100	122	120	Vento X	PolG	0	0	0	15	16	0	0	68
IPE 100	122	120	Vento X	PolG	16	0	0	68	149	0	0	67
IPE 100	122	120	Vento X	PolG	133	0	0	67	133	0	0	14
Trave 1035												
IPE 100	121	119	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	121	119	QP Solai	PolG	16	0	0	81	16	0	0	136
IPE 100	121	119	QP Solai	PolG	133	0	0	136	133	0	0	135
IPE 100	121	119	QV Solai	PolG	0	0	0	26	16	0	0	83
IPE 100	121	119	QV Solai	PolG	16	0	0	43	133	0	0	43
IPE 100	121	119	QV Solai	PolG	133	0	0	43	149	0	0	27
IPE 100	121	119	Neve	PolG	0	0	0	41	133	0	0	41
IPE 100	121	119	Neve	PolG	133	0	0	41	149	0	0	9
IPE 100	121	119	Neve	PolG	0	0	0	9	16	0	0	43
IPE 100	121	119	Neve	PolG	16	0	0	43	149	0	0	43
IPE 100	121	119	Vento X	PolG	0	0	0	14	16	0	0	67
IPE 100	121	119	Vento X	PolG	16	0	0	67	149	0	0	67
IPE 100	121	119	Vento X	PolG	0	0	0	64	133	0	0	64
IPE 100	121	119	Vento X	PolG	133	0	0	64	149	0	0	14
Trave 1036												
IPE 100	234	229	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	234	229	QP Solai	PolG	0	0	0	76	16	0	0	128
IPE 100	234	229	QP Solai	PolG	16	0	0	128	133	0	0	128
IPE 100	234	229	QV Solai	PolG	133	0	0	128	149	0	0	79
IPE 100	234	229	QV Solai	PolG	0	0	0	24	16	0	0	41
IPE 100	234	229	QV Solai	PolG	16	0	0	41	133	0	0	41
IPE 100	234	229	Neve	PolG	133	0	0	41	149	0	0	25
IPE 100	234	229	Neve	PolG	0	0	0	38	133	0	0	38
IPE 100	234	229	Neve	PolG	133	0	0	38	149	0	0	8
IPE 100	234	229	Neve	PolG	0	0	0	9	16	0	0	41
IPE 100	234	229	Neve	PolG	16	0	0	41	149	0	0	41
IPE 100	234	229	Vento X	PolG	0	0	0	59	133	0	0	59
IPE 100	234	229	Vento X	PolG	133	0	0	59	149	0	0	13
IPE 100	234	229	Vento X	PolG	0	0	0	13	16	0	0	64
IPE 100	234	229	Vento X	PolG	16	0	0	64	149	0	0	64
Trave 1037												
IPE 100	233	228	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	233	228	QP Solai	PolG	0	0	0	71	16	0	0	120
IPE 100	233	228	QP Solai	PolG	16	0	0	120	133	0	0	119
IPE 100	233	228	QV Solai	PolG	133	0	0	119	149	0	0	74
IPE 100	233	228	QV Solai	PolG	0	0	0	23	16	0	0	38
IPE 100	233	228	QV Solai	PolG	16	0	0	38	133	0	0	38
IPE 100	233	228	Neve	PolG	133	0	0	38	149	0	0	24
IPE 100	233	228	Neve	PolG	0	0	0	36	133	0	0	36
IPE 100	233	228	Neve	PolG	133	0	0	36	149	0	0	8
IPE 100	233	228	Neve	PolG	0	0	0	8	16	0	0	38
IPE 100	233	228	Neve	PolG	16	0	0	38	149	0	0	38
IPE 100	233	228	Vento X	PolG	0	0	0	13	16	0	0	59
IPE 100	233	228	Vento X	PolG	16	0	0	59	149	0	0	59
IPE 100	233	228	Vento X	PolG	0	0	0	55	133	0	0	55
IPE 100	233	228	Vento X	PolG	133	0	0	55	149	0	0	12
Trave 1038												
IPE 100	232	227	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	232	227	QP Solai	PolG	0	0	0	65	16	0	0	110
IPE 100	232	227	QP Solai	PolG	16	0	0	110	133	0	0	110
IPE 100	232	227	QV Solai	PolG	133	0	0	110	149	0	0	69
IPE 100	232	227	QV Solai	PolG	0	0	0	21	16	0	0	35
IPE 100	232	227	QV Solai	PolG	16	0	0	35	133	0	0	35

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	232	227	Neve	PolG	133	0	0	35	149	0	0	22
	231	226		PolG	0	0	0	36	149	0	0	36
	232	227	Neve	PolG	16	0	0	3	16	0	0	33
	231	226		PolG	0	0	0	33	149	0	0	7
IPE 100	232	227	Vento X	PolG	0	0	0	12	16	0	0	55
IPE 100	232	227	Vento X	PolG	16	0	0	55	149	0	0	55
IPE 100	232	227	Vento X	PolG	0	0	0	50	133	0	0	50
IPE 100	232	227	Vento X	PolG	133	0	0	50	149	0	0	11
Trave 1039												
IPE 100	231	226	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	231	226	QP Solai	PolG	0	0	0	59	16	0	0	100
IPE 100	231	226	QP Solai	PolG	16	0	0	100	133	0	0	100
IPE 100	231	226	QV Solai	PolG	133	0	0	100	149	0	0	62
IPE 100	231	226	QV Solai	PolG	0	0	0	19	16	0	0	32
IPE 100	231	226	Neve	PolG	16	0	0	32	133	0	0	32
IPE 100	231	226	Neve	PolG	133	0	0	32	149	0	0	20
IPE 100	231	226	Neve	PolG	0	0	0	30	133	0	0	30
IPE 100	231	226	Neve	PolG	133	0	0	30	149	0	0	6
IPE 100	231	226	Neve	PolG	0	0	0	7	16	0	0	33
IPE 100	231	226	Vento X	PolG	16	0	0	33	149	0	0	33
IPE 100	231	226	Vento X	PolG	0	0	0	11	16	0	0	50
IPE 100	231	226	Vento X	PolG	16	0	0	50	149	0	0	50
IPE 100	231	226	Vento X	PolG	0	0	0	46	133	0	0	46
IPE 100	231	226	Vento X	PolG	133	0	0	46	149	0	0	10
Trave 1040												
IPE 100	230	225	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	230	225	QP Solai	PolG	0	0	0	54	16	0	0	92
IPE 100	230	225	QP Solai	PolG	16	0	0	92	133	0	0	92
IPE 100	230	225	QV Solai	PolG	133	0	0	92	149	0	0	57
IPE 100	230	225	QV Solai	PolG	0	0	0	17	16	0	0	29
IPE 100	230	225	QV Solai	PolG	16	0	0	29	133	0	0	29
IPE 100	230	225	Neve	PolG	133	0	0	29	149	0	0	18
IPE 100	230	225	Neve	PolG	0	0	0	27	133	0	0	27
IPE 100	230	225	Neve	PolG	133	0	0	27	149	0	0	6
IPE 100	230	225	Neve	PolG	0	0	0	6	16	0	0	30
IPE 100	230	225	Vento X	PolG	16	0	0	30	149	0	0	30
IPE 100	230	225	Vento X	PolG	0	0	0	42	133	0	0	42
IPE 100	230	225	Vento X	PolG	133	0	0	42	149	0	0	9
IPE 100	230	225	Vento X	PolG	0	0	0	10	16	0	0	46
IPE 100	230	225	Vento X	PolG	16	0	0	46	149	0	0	46
Trave 1041												
IPE 100	320	320	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	320	320	QP Solai	PolG	0	0	0	51	16	0	0	86
IPE 100	320	320	QP Solai	PolG	16	0	0	86	133	0	0	86
IPE 100	320	320	QV Solai	PolG	133	0	0	86	149	0	0	53
IPE 100	320	320	QV Solai	PolG	0	0	0	16	16	0	0	28
IPE 100	320	320	QV Solai	PolG	16	0	0	28	133	0	0	28
IPE 100	320	320	Neve	PolG	133	0	0	28	149	0	0	17
IPE 100	320	320	Neve	PolG	0	0	0	26	133	0	0	26
IPE 100	320	320	Neve	PolG	133	0	0	26	149	0	0	5
IPE 100	320	320	Neve	PolG	0	0	0	6	16	0	0	27
IPE 100	320	320	Vento X	PolG	16	0	0	27	149	0	0	27
IPE 100	320	320	Vento X	PolG	0	0	0	9	16	0	0	42
IPE 100	320	320	Vento X	PolG	16	0	0	42	149	0	0	42
IPE 100	320	320	Vento X	PolG	0	0	0	41	133	0	0	41
IPE 100	320	320	Vento X	PolG	133	0	0	41	149	0	0	8
Trave 1042												
IPE 100	320	320	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	320	320	QP Solai	PolG	0	0	0	53	16	0	0	86
IPE 100	320	320	QP Solai	PolG	16	0	0	86	133	0	0	86
IPE 100	320	320	QV Solai	PolG	133	0	0	86	149	0	0	51
IPE 100	320	320	QV Solai	PolG	0	0	0	16	16	0	0	28
IPE 100	320	320	QV Solai	PolG	16	0	0	28	133	0	0	28
IPE 100	320	320	Neve	PolG	133	0	0	28	149	0	0	17
IPE 100	320	320	Neve	PolG	0	0	0	26	133	0	0	26
IPE 100	320	320	Neve	PolG	133	0	0	26	149	0	0	5
IPE 100	320	320	Neve	PolG	0	0	0	6	16	0	0	27
IPE 100	320	320	Vento X	PolG	16	0	0	27	149	0	0	27
IPE 100	320	320	Vento X	PolG	0	0	0	9	16	0	0	42
IPE 100	320	320	Vento X	PolG	16	0	0	42	149	0	0	42
IPE 100	320	320	Vento X	PolG	0	0	0	41	133	0	0	41
IPE 100	320	320	Vento X	PolG	133	0	0	41	149	0	0	8
Trave 1043												
IPE 100	320	320	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	320	320	QP Solai	PolG	0	0	0	53	16	0	0	86
IPE 100	320	320	QP Solai	PolG	16	0	0	86	133	0	0	86
IPE 100	320	320	QV Solai	PolG	133	0	0	86	149	0	0	51
IPE 100	320	320	QV Solai	PolG	0	0	0	16	16	0	0	28
IPE 100	320	320	QV Solai	PolG	16	0	0	28	133	0	0	28
IPE 100	320	320	Neve	PolG	133	0	0	28	149	0	0	17
IPE 100	320	320	Neve	PolG	0	0	0	26	133	0	0	26
IPE 100	320	320	Neve	PolG	133	0	0	26	149	0	0	5
IPE 100	320	320	Neve	PolG	0	0	0	6	16	0	0	27
IPE 100	320	320	Vento X	PolG	16	0	0	27	149	0	0	27
IPE 100	320	320	Vento X	PolG	0	0	0	9	16	0	0	42
IPE 100	320	320	Vento X	PolG	16	0	0	42	149	0	0	42
IPE 100	320	320	Vento X	PolG	0	0	0	41	133	0	0	41
IPE 100	320	320	Vento X	PolG	133	0	0	41	149	0	0	8
Trave 1044												
IPE 100	320	320	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	320	320	QP Solai	PolG	0	0	0	53	16	0	0	86
IPE 100	320	320	QP Solai	PolG	16	0	0	86	133	0	0	86
IPE 100	320	320	QV Solai	PolG	133	0	0	86	149	0	0	51
IPE 100	320	320	QV Solai	PolG	0	0	0	16	16	0	0	28
IPE 100	320	320	QV Solai	PolG	16	0	0	28	133	0	0	28
IPE 100	320	320	Neve	PolG	133	0	0	28	149	0	0	17
IPE 100	320	320	Neve	PolG	0	0	0	26	133	0	0	26
IPE 100	320	320	Neve	PolG	133	0	0	26	149	0	0	5
IPE 100	320	320	Neve	PolG	0	0	0	6	16	0	0	27
IPE 100	320	320	Vento X	PolG	16	0	0	27	149	0	0	27
IPE 100	320	320	Vento X	PolG	0	0	0	9	16	0	0	42
IPE 100	320	320	Vento X	PolG	16	0	0	42	149	0	0	42
IPE 100	320	320	Vento X	PolG	0	0	0	41	133	0	0	41
IPE 100	320	320	Vento X	PolG	133	0	0	41	149	0	0	8
Trave 1045												
IPE 100	320	320	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	320	320	QP Solai	PolG	0	0	0	53	16	0	0	86
IPE 100	320	320	QP Solai	PolG	16	0	0	86	133	0	0	86
IPE 100	320	320	QV Solai	PolG	133	0	0	86	149	0	0	51
IPE 100	320	320	QV Solai	PolG	0	0	0	16	16	0	0	28
IPE 100	320	320	QV Solai	PolG	16	0	0	28	133	0	0	28
IPE 100	320	320	Neve	PolG	133	0	0	28	149	0	0	17
IPE 100	320	320	Neve	PolG	0	0	0	26	133	0	0	26
IPE 100	320	320	Neve	PolG	133	0	0	26	149	0	0	5
IPE 100	320	320	Neve	PolG	0	0	0	6	16	0	0	27
IPE 100	320	320	Vento X	PolG	16	0	0	27	149	0	0	27
IPE 100	320	320	Vento X	PolG	0	0	0	9	16	0	0	42
IPE 100	320	320	Vento X	PolG	16	0	0	42	149	0	0	42
IPE 100	320	320	Vento X	PolG	0	0	0	41	133	0	0	41
IPE 100	320	320	Vento X	PolG	133	0	0	41	149	0	0	8
Trave 1046												
IPE 100	320	320	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	320	320	QP Solai	PolG	0	0	0	53	16	0	0	86
IPE 100	320	320	QP Solai	PolG	16	0	0	86	133	0	0	86
IPE 100	320	320	QV Solai	PolG	133	0	0	86	149	0	0	51
IPE 100	320	320	QV Solai	PolG	0	0	0	16	16	0	0	28
IPE 100	320	320	QV Solai	PolG	16	0	0	28	133	0	0	28
IPE 100	320	320	Neve	PolG	133	0	0	28	149	0	0	17
IPE 100	320	320	Neve	PolG	0	0	0	26	133	0	0	26
IPE 100	320	320	Neve	PolG	133	0	0	26	149	0	0	5
IPE 100	320	320	Neve	PolG	0	0	0	6	16	0	0	27
IPE 100	320	320	Vento X	PolG	16	0	0	27	149	0	0	27
IPE 100	320	320	Vento X	PolG	0	0	0	9	16	0	0	42
IPE 100	320	320	Vento X	PolG	16	0	0	42				

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	321	319		PolG	0	0	0	17	16	0	0	28
			QV Solai		16	0	0	28	133	0	0	28
IPE 100	321	319		PolG	133	0	0	28	149	0	0	16
			Neve		133	0	0	27	149	0	0	27
IPE 100	321	319		PolG	0	0	0	5	16	0	0	6
			Neve		16	0	0	5	16	0	0	26
IPE 100	321	319		PolG	0	0	0	26	149	0	0	26
			Vento X		133	0	0	42	133	0	0	42
IPE 100	321	319		PolG	0	0	0	42	149	0	0	9
			Vento X		133	0	0	8	16	0	0	41
IPE 100	321	319		PolG	16	0	0	41	149	0	0	41
			Carichi termici		16	0	0	41	149	0	0	41
Trave 1043												
IPE 100	310	311		UnitG	0	0	0	8	149	0	0	8
			Peso Proprio		0	0	0	9	16	0	0	44
IPE 100	310	311		PolG	16	0	0	44	149	0	0	44
			QV Solai		16	0	0	3	16	0	0	14
IPE 100	310	311		PolG	16	0	0	14	149	0	0	14
			Neve		16	0	0	6	16	0	0	27
IPE 100	310	311		PolG	16	0	0	27	149	0	0	27
			Vento X		16	0	0	9	16	0	0	42
IPE 100	310	311		PolG	16	0	0	42	149	0	0	42
			Carichi termici		16	0	0	42	149	0	0	42
Trave 1044												
IPE 100	104	105		UnitG	0	0	0	8	149	0	0	8
			Peso Proprio		0	0	0	71	133	0	0	71
IPE 100	104	105		PolG	133	0	0	71	149	0	0	15
			QV Solai		133	0	0	23	133	0	0	23
IPE 100	104	105		PolG	133	0	0	23	149	0	0	5
			Neve		133	0	0	44	133	0	0	44
IPE 100	104	105		PolG	133	0	0	44	149	0	0	9
			Vento X		133	0	0	68	133	0	0	68
IPE 100	104	105		PolG	133	0	0	68	149	0	0	15
			Carichi termici		133	0	0	68	149	0	0	15
Trave 1046												
IPE 100	119	125		UnitG	0	0	0	8	102	0	0	8
			Peso Proprio		0	0	0	74	16	0	0	135
IPE 100	119	125		PolG	16	0	0	135	91	0	0	135
			QV Solai		91	0	0	135	102	0	0	77
IPE 100	119	125		PolG	0	0	0	24	16	0	0	43
			Neve		16	0	0	43	91	0	0	43
IPE 100	119	125		PolG	91	0	0	43	102	0	0	25
			Vento X		91	0	0	41	91	0	0	41
IPE 100	119	125		PolG	91	0	0	41	102	0	0	5
			Neve		16	0	0	5	16	0	0	43
IPE 100	119	125		PolG	16	0	0	43	102	0	0	64
			Vento X		16	0	0	64	91	0	0	8
IPE 100	119	125		PolG	91	0	0	64	102	0	0	67
			Vento X		16	0	0	8	16	0	0	67
IPE 100	119	125		PolG	16	0	0	67	102	0	0	67
			Carichi termici		16	0	0	67	102	0	0	67
Trave 1047												
IPE 100	229	244		UnitG	0	0	0	8	107	0	0	8
			Peso Proprio		0	0	0	70	16	0	0	128
IPE 100	229	244		PolG	16	0	0	128	97	0	0	128
			QV Solai		97	0	0	128	108	0	0	74
IPE 100	229	244		PolG	0	0	0	22	16	0	0	41
			Neve		16	0	0	41	97	0	0	41
IPE 100	229	244		PolG	97	0	0	41	108	0	0	24
			Neve		97	0	0	38	97	0	0	38
IPE 100	229	244		PolG	97	0	0	38	108	0	0	5
			Neve		16	0	0	5	16	0	0	41
IPE 100	229	244		PolG	16	0	0	41	108	0	0	41
			Vento X		97	0	0	59	97	0	0	59
IPE 100	229	244		PolG	97	0	0	59	108	0	0	7
			Vento X		16	0	0	8	16	0	0	64

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	229	244		PolG	16	0	0	64	108	0	0	64
			Carichi termici		16	0	0	64	108	0	0	64
Trave 1048												
IPE 100	228	243		UnitG	0	0	0	8	113	0	0	8
			Peso Proprio		0	0	0	66	16	0	0	119
IPE 100	228	243		PolG	16	0	0	119	103	0	0	119
			QV Solai		103	0	0	119	114	0	0	69
IPE 100	228	243		PolG	0	0	0	21	16	0	0	38
			Neve		16	0	0	38	103	0	0	38
IPE 100	228	243		PolG	103	0	0	38	114	0	0	22
			Carichi termici		103	0	0	5	16	0	0	38
IPE 100	228	243		PolG	16	0	0	36	103	0	0	36
			Neve		103	0	0	36	114	0	0	5
IPE 100	228	243		PolG	0	0	0	8	16	0	0	59
			Vento X		16	0	0	59	114	0	0	59
IPE 100	228	243		PolG	0	0	0	55	103	0	0	55
			Carichi termici		103	0	0	55	114	0	0	7
Trave 1049												
IPE 100	227	242		UnitG	0	0	0	8	119	0	0	8
			Peso Proprio		0	0	0	60	16	0	0	110
IPE 100	227	242		PolG	16	0	0	110	109	0	0	110
			QV Solai		109	0	0	110	120	0	0	65
IPE 100	227	242		PolG	0	0	0	19	16	0	0	35
			Neve		16	0	0	35	109	0	0	35
IPE 100	227	242		PolG	109	0	0	35	120	0	0	21
			Vento X		109	0	0	5	16	0	0	36
IPE 100	227	242		PolG	16	0	0	36	120	0	0	36
			Carichi termici		16	0	0	33	109	0	0	33
IPE 100	227	242		PolG	109	0	0	33	120	0	0	5
			Neve		109	0	0	8	16	0	0	55
IPE 100	227	242		PolG	16	0	0	55	120	0	0	55
			Vento X		109	0	0	50	109	0	0	50
IPE 100	227	242		PolG	109	0	0	50	120	0	0	7
			Carichi termici		109	0	0	50	120	0	0	7
Trave 1050												
IPE 100	226	241		UnitG	0	0	0	8	126	0	0	8
			Peso Proprio		0	0	0	55	16	0	0	100
IPE 100	226	241		PolG	16	0	0	100	115	0	0	100
			QV Solai		115	0	0	100	126	0	0	59
IPE 100	226	241		PolG	0	0	0	18	16	0	0	32
			Neve		16	0	0	32	115	0	0	32
IPE 100	226	241		PolG	115	0	0	32	126	0	0	19
			Vento X		16	0	0	5	16	0	0	33
IPE 100	226	241		PolG	16	0	0	33	126	0	0	33
			Carichi termici		16	0	0	30	115	0	0	30
IPE 100	226	241		PolG	115	0	0	30	126	0	0	4
			Vento X		115	0	0	46	115	0	0	46
IPE 100	226	241		PolG	115	0	0	46	126	0	0	7
			Carichi termici		115	0	0	7	16	0	0	50
IPE 100	226	241		PolG	16	0	0	50	126	0	0	50
			Carichi termici		16	0	0	50	126	0	0	50
Trave 1051												
IPE 100	225	240		UnitG	0	0	0	8	132	0	0	8
			Peso Proprio		0	0	0	51	16	0	0	92
IPE 100	225	240		PolG	16	0	0	92	121	0	0	92
			QV Solai		121	0	0	92	132	0	0	54
IPE 100	225	240		PolG	0	0	0	16	16	0	0	29
			Neve		16	0	0	29	121	0	0	17
IPE 100	225	240		PolG	121	0	0	29	132	0	0	27
			Vento X		121	0	0	27	132	0	0	4
IPE 100	225	240		PolG	16	0	0	4	16	0	0	30
			Carichi termici		16	0	0	30	132	0	0	30
IPE 100	225	240		PolG	16	0	0	42	121	0	0	42

Sezione	Ni	Nf	Cond.	Tipico c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	225	240	Vento X	PolG	121	0	0	42	132	0	0	6
				PolG	0	0	0	7	16	0	0	46
IPE 100	225	240	Carichi termici	Termico	16	0	0	46	132	0	0	46
Trave 1052												
IPE 100	320	326	Peso Proprio	UnitG	0	0	0	8	137	0	0	8
IPE 100	320	326	QP Solai	PolG	0	0	0	49	16	0	0	86
				PolG	16	0	0	86	127	0	0	86
				PolG	127	0	0	86	137	0	0	51
IPE 100	320	326	QV Solai	PolG	0	0	0	16	16	0	0	28
				PolG	16	0	0	28	127	0	0	28
IPE 100	320	326	Neve	PolG	127	0	0	28	137	0	0	16
				PolG	0	0	0	26	127	0	0	26
IPE 100	320	326	Neve	PolG	127	0	0	26	137	0	0	4
				PolG	0	0	0	4	16	0	0	27
IPE 100	320	326	Vento X	PolG	16	0	0	27	137	0	0	27
				PolG	0	0	0	41	127	0	0	41
IPE 100	320	326	Vento X	PolG	127	0	0	41	137	0	0	6
				PolG	0	0	0	7	16	0	0	42
IPE 100	320	326	Carichi termici	Termico	16	0	0	42	137	0	0	42
Trave 1053												
IPE 100	319	325	Peso Proprio	UnitG	0	0	0	8	143	0	0	8
IPE 100	319	325	QP Solai	PolG	0	0	0	51	16	0	0	86
				PolG	16	0	0	86	133	0	0	86
				PolG	133	0	0	86	143	0	0	49
IPE 100	319	325	QV Solai	PolG	0	0	0	16	16	0	0	28
				PolG	16	0	0	28	133	0	0	28
IPE 100	319	325	Neve	PolG	133	0	0	28	143	0	0	16
				PolG	0	0	0	4	16	0	0	26
IPE 100	319	325	Neve	PolG	16	0	0	26	143	0	0	26
				PolG	0	0	0	27	133	0	0	27
IPE 100	319	325	Vento X	PolG	133	0	0	27	143	0	0	5
				PolG	0	0	0	42	133	0	0	42
IPE 100	319	325	Vento X	PolG	133	0	0	42	143	0	0	7
				PolG	0	0	0	7	16	0	0	41
IPE 100	319	325	Carichi termici	Termico	16	0	0	41	143	0	0	41
Trave 1054												
IPE 100	311	312	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	311	312	QP Solai	PolG	0	0	0	8	16	0	0	44
				PolG	16	0	0	44	149	0	0	44
IPE 100	311	312	QV Solai	PolG	0	0	0	2	16	0	0	14
				PolG	16	0	0	14	149	0	0	14
IPE 100	311	312	Neve	PolG	0	0	0	5	16	0	0	27
				PolG	16	0	0	27	149	0	0	27
IPE 100	311	312	Vento X	PolG	0	0	0	7	16	0	0	42
				PolG	16	0	0	42	149	0	0	42
IPE 100	311	312	Carichi termici	Termico	16	0	0	42	149	0	0	42
Trave 1055												
IPE 100	105	106	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	105	106	QP Solai	PolG	0	0	0	71	80	0	0	71
				PolG	80	0	0	71	90	0	0	7
IPE 100	105	106	QV Solai	PolG	0	0	0	23	80	0	0	23
				PolG	80	0	0	23	90	0	0	2
IPE 100	105	106	Neve	PolG	0	0	0	44	80	0	0	44
				PolG	80	0	0	44	90	0	0	5
IPE 100	105	106	Vento X	PolG	0	0	0	68	80	0	0	68
				PolG	0	0	0	68	80	0	0	68
IPE 100	105	106	Carichi termici	Termico	80	0	0	68	90	0	0	7
Trave 1056												
IPE 100	120	126	Peso Proprio	UnitG	0	0	0	8	96	0	0	8
IPE 100	120	126	QP Solai	PolG	0	0	0	77	16	0	0	140
				PolG	16	0	0	140	86	0	0	140
				PolG	86	0	0	140	96	0	0	79
IPE 100	120	126	QV Solai	PolG	0	0	0	25	16	0	0	45

Sezione	Ni	Nf	Cond.	Tiplo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					16	0	0	45	86	0	0	45
					86	0	0	45	96	0	0	25
IPE 100	120	126	Neve	PolG	0	0	0	5	16	0	0	44
					16	0	0	44	96	0	0	44
IPE 100	120	126	Neve	PolG	0	0	0	43	86	0	0	43
					86	0	0	43	96	0	0	5
IPE 100	120	126	Vento X	PolG	0	0	0	8	16	0	0	68
					16	0	0	68	96	0	0	67
IPE 100	120	126	Vento X	PolG	0	0	0	67	86	0	0	67
					86	0	0	67	96	0	0	7
IPE 100	120	126	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1057												
IPE 100	244	245	Peso Proprio	UnifG	0	0	0	8	70	0	0	8
IPE 100	244	245	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1058												
IPE 100	125	128	Peso Proprio	UnifG	0	0	0	8	70	0	0	8
IPE 100	125	128	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1059												
IPE 100	243	246	Peso Proprio	UnifG	0	0	0	8	70	0	0	8
IPE 100	243	246	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1060												
IPE 100	242	247	Peso Proprio	UnifG	0	0	0	8	70	0	0	8
IPE 100	242	247	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1061												
IPE 100	241	248	Peso Proprio	UnifG	0	0	0	8	70	0	0	8
IPE 100	241	248	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1062												
IPE 100	240	249	Peso Proprio	UnifG	0	0	0	8	70	0	0	8
IPE 100	240	249	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1063												
IPE 100	326	327	Peso Proprio	UnifG	0	0	0	8	70	0	0	8
IPE 100	326	327	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1064												
IPE 100	325	328	Peso Proprio	UnifG	0	0	0	8	70	0	0	8
IPE 100	325	328	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1065												
IPE 100	312	313	Peso Proprio	UnifG	0	0	0	8	70	0	0	8
IPE 100	312	313	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1066												
IPE 100	106	114	Peso Proprio	UnifG	0	0	0	8	82	0	0	8
IPE 100	106	114	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1067												
IPE 100	126	127	Peso Proprio	UnifG	0	0	0	8	70	0	0	8
IPE 100	126	127	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 2001												
IPE 100	17	19	Peso Proprio	UnifG	0	0	0	8	89	0	0	8
IPE 100	17	19	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 2002												
IPE 100	19	20	Peso Proprio	UnifG	0	0	0	8	89	0	0	8
IPE 100	19	20	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 2003												
IPE 100	20	15	Peso Proprio	UnifG	0	0	0	8	102	0	0	8
IPE 100	20	15	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 2004												
IPE 100	15	16	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	15	16	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 2005												
IPE 100	16	18	Peso Proprio	UnifG	0	0	0	8	90	0	0	8
IPE 100	16	18	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 2006												
IPE 100	25	26	Peso Proprio	UnifG	0	0	0	8	89	0	0	8
Trave 2007												
IPE 100	26	23	Peso Proprio	UnifG	0	0	0	8	85	0	0	8
Trave 2008												
IPE 100	23	24	Peso Proprio	UnifG	0	0	0	8	89	0	0	8

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Trave 2009												
HE 240 A	24	21	Peso Proprio	UnifG	0	0	0	0	8	162	0	8
Trave 2010												
IPE 100	21	22	Peso Proprio	UnifG	0	0	0	0	8	90	0	8
Trave 8000												
HE 240 A	117	118	Peso Proprio	UnifG	0	0	0	0	60	178	0	60
HE 240 A	117	118	QP Solai	PolG	0	0	0	0	39	131	0	47
HE 240 A	117	118	QV Solai	PolG	131	0	0	0	47	178	0	14
HE 240 A	117	118	Neve	PolG	131	0	0	0	15	178	0	15
HE 240 A	117	118	Neve	PolG	131	0	0	0	24	131	0	29
HE 240 A	117	118	Vento X	PolG	131	0	0	0	29	178	0	9
HE 240 A	117	118	Vento X	PolG	131	0	0	0	37	131	0	45
HE 240 A	117	118	Carchi termini	Termico	AXY=15°C, AXZ=15°C	131	0	0	45	178	0	13
HE 240 A	118	101	Peso Proprio	UnifG	0	0	0	0	60	182	0	60
HE 240 A	118	101	QP Solai	PolG	0	0	0	0	37	137	0	45
HE 240 A	118	101	QV Solai	PolG	137	0	0	0	45	182	0	14
HE 240 A	118	101	Neve	PolG	137	0	0	0	14	182	0	4
HE 240 A	118	101	Neve	PolG	137	0	0	0	23	137	0	28
HE 240 A	118	101	Vento X	PolG	137	0	0	0	28	182	0	9
HE 240 A	118	101	Vento X	PolG	137	0	0	0	35	137	0	43
HE 240 A	118	101	Carchi termini	Termico	AXY=15°C, AXZ=15°C	137	0	0	43	182	0	13
HE 240 A	220	221	Peso Proprio	UnifG	0	0	0	0	60	123	0	60
HE 240 A	220	221	QP Solai	PolG	0	0	0	0	50	80	0	58
HE 240 A	220	221	QV Solai	PolG	80	0	0	0	58	123	0	14
HE 240 A	220	221	Neve	PolG	80	0	0	0	16	80	0	19
HE 240 A	220	221	Neve	PolG	80	0	0	0	19	123	0	4
HE 240 A	220	221	Vento X	PolG	80	0	0	0	31	80	0	36
HE 240 A	220	221	Vento X	PolG	80	0	0	0	36	123	0	9
HE 240 A	220	221	Carchi termini	Termico	AXY=15°C, AXZ=15°C	80	0	0	48	80	0	56
HE 240 A	220	221	Peso Proprio	UnifG	0	0	0	0	60	134	0	13
HE 240 A	221	222	QP Solai	PolG	0	0	0	0	48	90	0	60
HE 240 A	221	222	QV Solai	PolG	90	0	0	0	56	134	0	56
HE 240 A	221	222	Neve	PolG	90	0	0	0	15	90	0	14
HE 240 A	221	222	Neve	PolG	90	0	0	0	18	134	0	18
HE 240 A	221	222	Vento X	PolG	90	0	0	0	30	90	0	35
HE 240 A	221	222	Vento X	PolG	90	0	0	0	35	134	0	9
HE 240 A	221	222	Carchi termini	Termico	AXY=15°C, AXZ=15°C	90	0	0	46	90	0	54
HE 240 A	221	222	Peso Proprio	UnifG	0	0	0	0	60	148	0	60
HE 240 A	222	223	QP Solai	PolG	0	0	0	0	46	102	0	54
HE 240 A	222	223	QV Solai	PolG	102	0	0	0	54	148	0	14
HE 240 A	222	223	Neve	PolG	102	0	0	0	15	102	0	17
HE 240 A	222	223	Neve	PolG	102	0	0	0	17	148	0	4
HE 240 A	222	223	Vento X	PolG	102	0	0	0	28	102	0	33
HE 240 A	222	223	Vento X	PolG	102	0	0	0	33	148	0	9
HE 240 A	222	223	Carchi termini	Termico	AXY=15°C, AXZ=15°C	102	0	0	44	102	0	52
HE 240 A	222	223	Peso Proprio	UnifG	0	0	0	0	52	148	0	13
HE 240 A	223	224	QP Solai	PolG	0	0	0	0	60	158	0	60
HE 240 A	223	224	QV Solai	PolG	112	0	0	0	43	112	0	52
HE 240 A	223	224	Neve	PolG	112	0	0	0	52	158	0	14
HE 240 A	223	224	Neve	PolG	112	0	0	0	14	112	0	17
HE 240 A	223	224	Vento X	PolG	112	0	0	0	27	112	0	32
HE 240 A	223	224	Vento X	PolG	112	0	0	0	32	158	0	9
HE 240 A	223	224	Carchi termini	Termico	AXY=15°C, AXZ=15°C	112	0	0	42	112	0	50
HE 240 A	223	224	Peso Proprio	UnifG	0	0	0	0	60	170	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	224	117	QP Solai	PolG	0	0	0	0	41	122	0	49
HE 240 A	224	117	QV Solai	PolG	122	0	0	0	49	170	0	14
HE 240 A	224	117	Neve	PolG	122	0	0	0	13	122	0	16
HE 240 A	224	117	Neve	PolG	0	0	0	0	16	170	0	4
HE 240 A	224	117	Neve	PolG	0	0	0	0	26	122	0	31
HE 240 A	224	117	Vento X	PolG	122	0	0	0	31	170	0	9
HE 240 A	224	117	Vento X	PolG	0	0	0	0	40	122	0	47
HE 240 A	224	117	Vento X	PolG	122	0	0	0	47	170	0	13
HE 240 A	224	117	Carchi termini	Termico	AXY=15°C, AXZ=15°C	122	0	0	0	0	0	0
HE 240 A	307	317	Peso Proprio	UnifG	0	0	0	0	60	112	0	60
HE 240 A	307	317	QP Solai	PolG	0	0	0	0	57	68	0	64
HE 240 A	307	317	QP Solai	PolG	68	0	0	0	64	112	0	14
HE 240 A	307	317	QV Solai	PolG	0	0	0	0	18	68	0	21
HE 240 A	307	317	QV Solai	PolG	68	0	0	0	21	112	0	4
HE 240 A	307	317	Neve	PolG	0	0	0	0	36	68	0	40
HE 240 A	307	317	Neve	PolG	0	0	0	0	40	112	0	9
HE 240 A	307	317	Vento X	PolG	68	0	0	0	55	68	0	62
HE 240 A	307	317	Vento X	PolG	0	0	0	0	62	112	0	13
HE 240 A	307	317	Carchi termini	Termico	AXY=15°C, AXZ=15°C	68	0	0	0	0	0	0
HE 240 A	317	318	Peso Proprio	UnifG	0	0	0	0	60	108	0	60
HE 240 A	317	318	QP Solai	PolG	0	0	0	0	55	67	0	62
HE 240 A	317	318	QP Solai	PolG	67	0	0	0	62	108	0	14
HE 240 A	317	318	QV Solai	PolG	0	0	0	0	18	67	0	20
HE 240 A	317	318	QV Solai	PolG	67	0	0	0	20	108	0	4
HE 240 A	317	318	Neve	PolG	0	0	0	0	34	67	0	39
HE 240 A	317	318	Neve	PolG	67	0	0	0	39	108	0	9
HE 240 A	317	318	Vento X	PolG	0	0	0	0	53	67	0	60
HE 240 A	317	318	Vento X	PolG	67	0	0	0	60	108	0	13
HE 240 A	317	318	Carchi termini	Termico	AXY=15°C, AXZ=15°C	67	0	0	0	0	0	0
HE 240 A	318	220	Peso Proprio	UnifG	0	0	0	0	60	113	0	60
HE 240 A	318	220	QP Solai	PolG	0	0	0	0	53	72	0	60
HE 240 A	318	220	QP Solai	PolG	72	0	0	0	60	113	0	14
HE 240 A	318	220	QV Solai	PolG	0	0	0	0	17	72	0	19
HE 240 A	318	220	QV Solai	PolG	72	0	0	0	19	113	0	4
HE 240 A	318	220	Neve	PolG	0	0	0	0	33	72	0	37
HE 240 A	318	220	Neve	PolG	72	0	0	0	37	113	0	9
HE 240 A	318	220	Vento X	PolG	0	0	0	0	51	72	0	58
HE 240 A	318	220	Vento X	PolG	72	0	0	0	58	113	0	13
HE 240 A	318	220	Carchi termini	Termico	AXY=15°C, AXZ=15°C	72	0	0	0	0	0	0
Trave 8001												
HE 240 A	115	116	Peso Proprio	UnifG	0	0	0	0	60	178	0	60
HE 240 A	115	116	QP Solai	PolG	0	0	0	0	50	49	0	89
HE 240 A	115	116	QP Solai	PolG	49	0	0	0	89	141	0	87
HE 240 A	115	116	QV Solai	PolG	141	0	0	0	87	178	0	49
HE 240 A	115	116	QV Solai	PolG	0	0	0	0	16	49	0	29
HE 240 A	115	116	QV Solai	PolG	49	0	0	0	29	141	0	28
HE 240 A	115	116	Neve	PolG	141	0	0	0	28	178	0	16
HE 240 A	115	116	Neve	PolG	0	0	0	0	24	141	0	29
HE 240 A	115	116	Neve	PolG	141	0	0	0	29	178	0	7
HE 240 A	115	116	Neve	PolG	0	0	0	0	7	49	0	30
HE 240 A	115	116	Vento X	PolG	49	0	0	0	30	178	0	24
HE 240 A	115	116	Vento X	PolG	0	0	0	0	11	49	0	46
HE 240 A	115	116	Vento X	PolG	49	0	0	0	46	178	0	36
HE 240 A	115	116	Vento X	PolG	0	0	0	0	38	141	0	44
HE 240 A	115	116	Vento X	PolG	141	0	0	0	44	178	0	11
HE 240 A	115	116	Carchi termini	Termico	AXY=15°C, AXZ=15°C	141	0	0	0	0	0	0
HE 240 A	115	116	Peso Proprio	UnifG	0	0	0	0	60	182	0	60
HE 240 A	116	102	QP Solai	PolG	0	0	0	0	48	47	0	85
HE 240 A	116	102	QP Solai	PolG	47	0	0	0	85	146	0	82
HE 240 A	116	102	QV Solai	PolG	146	0	0	0	82	182	0	47
HE 240 A	116	102	QV Solai	PolG	0	0	0	0	15	47	0	27
HE 240 A	116	102	QV Solai	PolG	47	0	0	0	27	146	0	26
HE 240 A	116	102	Neve	PolG	146	0	0	0	26	182	0	15
HE 240 A	116	102	Neve	PolG	0	0	0	0	23	146	0	27
HE 240 A	116	102	Neve	PolG	146	0	0	0	27	182	0	7
HE 240 A	116	102	Neve	PolG	0	0	0	0	7	47	0	28

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	116	102	Vento X	PolG	47	0	0	28	182	0	0	22
HE 240 A	116	102	Vento X	PolG	47	0	0	11	47	0	0	44
HE 240 A	116	102	Vento X	PolG	146	0	0	35	146	0	0	42
HE 240 A	116	102	Carichi termici Peso Proprio QP Solai	Termico UnifG	44	0	0	60	123	0	0	11
HE 240 A	215	216	QV Solai	PolG	44	0	0	20	44	0	0	36
HE 240 A	215	216	Neve	PolG	89	0	0	35	123	0	0	20
HE 240 A	215	216	Neve	PolG	44	0	0	7	44	0	0	36
HE 240 A	215	216	Neve	PolG	89	0	0	31	89	0	0	35
HE 240 A	215	216	Vento X	PolG	89	0	0	49	89	0	0	55
HE 240 A	215	216	Vento X	PolG	89	0	0	55	123	0	0	11
HE 240 A	215	216	Vento X	PolG	44	0	0	56	123	0	0	48
HE 240 A	216	217	Carichi termici Peso Proprio QP Solai	Termico UnifG	46	0	0	60	134	0	0	60
HE 240 A	216	217	QV Solai	PolG	46	0	0	35	99	0	0	34
HE 240 A	216	217	Neve	PolG	99	0	0	30	99	0	0	34
HE 240 A	216	217	Neve	PolG	99	0	0	34	134	0	0	7
HE 240 A	216	217	Vento X	PolG	46	0	0	35	134	0	0	29
HE 240 A	216	217	Vento X	PolG	99	0	0	53	134	0	0	11
HE 240 A	216	217	Vento X	PolG	46	0	0	54	134	0	0	46
HE 240 A	217	218	Carichi termici Peso Proprio QP Solai	Termico UnifG	48	0	0	60	148	0	0	60
HE 240 A	217	218	QV Solai	PolG	48	0	0	33	111	0	0	32
HE 240 A	217	218	Neve	PolG	111	0	0	32	148	0	0	18
HE 240 A	217	218	Neve	PolG	48	0	0	34	148	0	0	28
HE 240 A	217	218	Neve	PolG	111	0	0	29	111	0	0	33
HE 240 A	217	218	Vento X	PolG	111	0	0	44	111	0	0	51
HE 240 A	217	218	Vento X	PolG	111	0	0	51	148	0	0	11
HE 240 A	217	218	Vento X	PolG	48	0	0	52	148	0	0	43
HE 240 A	218	219	Carichi termici Peso Proprio QP Solai	Termico UnifG	49	0	0	60	158	0	0	60
HE 240 A	218	219	QV Solai	PolG	49	0	0	99	121	0	0	96
HE 240 A	218	219	Neve	PolG	121	0	0	96	158	0	0	54
HE 240 A	218	219	Neve	PolG	49	0	0	32	121	0	0	31
HE 240 A	218	219	Neve	PolG	121	0	0	31	158	0	0	17
HE 240 A	218	219	Neve	PolG	121	0	0	27	121	0	0	31
HE 240 A	218	219	Neve	PolG	49	0	0	32	158	0	0	26
HE 240 A	218	219	Vento X	PolG	0	0	0	11	49	0	0	50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	218	219	Vento X	PolG	49	0	0	50	158	0	0	41
HE 240 A	218	219	Carichi termici Peso Proprio QP Solai	Termico UnifG	121	0	0	49	158	0	0	11
HE 240 A	219	115	QV Solai	PolG	49	0	0	30	132	0	0	29
HE 240 A	219	115	Neve	PolG	132	0	0	29	170	0	0	16
HE 240 A	219	115	Neve	PolG	132	0	0	26	132	0	0	30
HE 240 A	219	115	Neve	PolG	49	0	0	94	132	0	0	94
HE 240 A	219	115	Neve	PolG	132	0	0	92	170	0	0	51
HE 240 A	219	115	Vento X	PolG	49	0	0	40	132	0	0	46
HE 240 A	219	115	Vento X	PolG	132	0	0	46	170	0	0	11
HE 240 A	219	115	Carichi termici Peso Proprio QP Solai	Termico UnifG	49	0	0	48	170	0	0	39
HE 240 A	308	315	QV Solai	PolG	46	0	0	60	112	0	0	60
HE 240 A	308	315	Neve	PolG	46	0	0	126	77	0	0	125
HE 240 A	308	315	Neve	PolG	77	0	0	125	112	0	0	68
HE 240 A	308	315	Neve	PolG	46	0	0	22	46	0	0	40
HE 240 A	308	315	Vento X	PolG	77	0	0	40	112	0	0	7
HE 240 A	308	315	Vento X	PolG	77	0	0	55	77	0	0	61
HE 240 A	308	315	Vento X	PolG	77	0	0	61	112	0	0	11
HE 240 A	308	315	Carichi termici Peso Proprio QP Solai	Termico UnifG	46	0	0	62	112	0	0	55
HE 240 A	315	316	QV Solai	PolG	42	0	0	60	108	0	0	60
HE 240 A	315	316	Neve	PolG	42	0	0	121	75	0	0	120
HE 240 A	315	316	Neve	PolG	75	0	0	120	108	0	0	66
HE 240 A	315	316	QV Solai	PolG	42	0	0	21	42	0	0	39
HE 240 A	315	316	Neve	PolG	75	0	0	39	75	0	0	38
HE 240 A	315	316	Neve	PolG	42	0	0	38	108	0	0	21
HE 240 A	315	316	Vento X	PolG	42	0	0	39	108	0	0	39
HE 240 A	315	316	Vento X	PolG	42	0	0	34	75	0	0	38
HE 240 A	315	316	Vento X	PolG	75	0	0	53	75	0	0	59
HE 240 A	315	316	Vento X	PolG	75	0	0	59	108	0	0	11
HE 240 A	315	316	Carichi termici Peso Proprio QP Solai	Termico UnifG	42	0	0	60	108	0	0	52
HE 240 A	316	215	QV Solai	PolG	42	0	0	37	81	0	0	37
HE 240 A	316	215	Neve	PolG	81	0	0	37	113	0	0	20
HE 240 A	316	215	Neve	PolG	81	0	0	33	81	0	0	37
HE 240 A	316	215	Neve	PolG	81	0	0	37	113	0	0	7
HE 240 A	316	215	Vento X	PolG	42	0	0	38	113	0	0	32
HE 240 A	316	215	Vento X	PolG	81	0	0	51	81	0	0	57
HE 240 A	316	215	Vento X	PolG	0	0	0	11	42	0	0	58

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	QXf	OYf	QZf
HE 240 A	316	215			42	0	0	0	58	113	0	50
Trave 8002												
HE 240 A	123	124	Peso Proprio	UnifG	0	0	0	0	60	178	0	60
HE 240 A	123	124	QP Solai	PolG	39	0	0	0	48	39	0	87
					149	0	0	0	84	178	0	84
HE 240 A	123	124	QV Solai	PolG	0	0	0	0	15	39	0	47
					39	0	0	0	28	149	0	27
					149	0	0	0	27	178	0	15
HE 240 A	123	124	Neve	PolG	0	0	0	0	5	39	0	29
					39	0	0	0	29	178	0	23
HE 240 A	123	124	Neve	PolG	0	0	0	0	24	149	0	28
					149	0	0	0	28	178	0	5
HE 240 A	123	124	Vento X	PolG	0	0	0	0	38	149	0	43
					149	0	0	0	43	178	0	8
HE 240 A	123	124	Vento X	PolG	0	0	0	0	8	39	0	45
					39	0	0	0	45	178	0	36
Trave 8003												
HE 240 A	123	124	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	182	0	60
HE 240 A	124	103	Peso Proprio	UnifG	0	0	0	0	46	37	0	82
HE 240 A	124	103	QP Solai	PolG	37	0	0	0	82	154	0	79
					154	0	0	0	79	182	0	44
HE 240 A	124	103	QV Solai	PolG	0	0	0	0	15	37	0	26
					37	0	0	0	26	154	0	25
					154	0	0	0	25	182	0	14
HE 240 A	124	103	Neve	PolG	0	0	0	0	23	154	0	26
					154	0	0	0	26	182	0	5
HE 240 A	124	103	Neve	PolG	0	0	0	0	5	37	0	28
					37	0	0	0	28	182	0	22
HE 240 A	124	103	Vento X	PolG	0	0	0	0	35	154	0	41
					154	0	0	0	41	182	0	8
HE 240 A	124	103	Vento X	PolG	0	0	0	0	8	37	0	43
					37	0	0	0	43	182	0	34
Trave 8004												
HE 240 A	124	103	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	123	0	60
HE 240 A	235	236	Peso Proprio	UnifG	0	0	0	0	60	35	0	110
HE 240 A	235	236	QP Solai	PolG	35	0	0	0	110	96	0	108
					96	0	0	0	108	123	0	58
HE 240 A	235	236	QV Solai	PolG	0	0	0	0	19	35	0	35
					35	0	0	0	35	96	0	35
					96	0	0	0	35	123	0	19
HE 240 A	235	236	Neve	PolG	0	0	0	0	32	96	0	35
					96	0	0	0	35	123	0	5
HE 240 A	235	236	Neve	PolG	0	0	0	0	5	35	0	36
					35	0	0	0	36	123	0	31
HE 240 A	235	236	Vento X	PolG	0	0	0	0	9	35	0	55
					35	0	0	0	55	123	0	48
HE 240 A	235	236	Vento X	PolG	0	0	0	0	49	96	0	54
					96	0	0	0	54	123	0	8
Trave 8005												
HE 240 A	235	236	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	134	0	60
HE 240 A	236	237	Peso Proprio	UnifG	0	0	0	0	57	37	0	106
HE 240 A	236	237	QP Solai	PolG	37	0	0	0	106	107	0	103
					107	0	0	0	103	134	0	56
					37	0	0	0	18	37	0	34
HE 240 A	236	237	QV Solai	PolG	0	0	0	0	34	107	0	33
					107	0	0	0	33	134	0	18
HE 240 A	236	237	Neve	PolG	0	0	0	0	30	107	0	33
					107	0	0	0	33	134	0	5
HE 240 A	236	237	Neve	PolG	0	0	0	0	5	37	0	34
					37	0	0	0	34	134	0	29
HE 240 A	236	237	Vento X	PolG	0	0	0	0	47	107	0	51
					107	0	0	0	51	134	0	8
HE 240 A	236	237	Vento X	PolG	0	0	0	0	9	37	0	53
					37	0	0	0	53	134	0	45

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	QXf	OYf	QZf
HE 240 A	236	237	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	148	0	60
HE 240 A	237	238	Peso Proprio	UnifG	0	0	0	0	55	38	0	101
HE 240 A	237	238	QP Solai	PolG	38	0	0	0	101	119	0	98
					119	0	0	0	98	148	0	54
HE 240 A	237	238	QV Solai	PolG	0	0	0	0	18	38	0	32
					38	0	0	0	32	119	0	32
					119	0	0	0	32	148	0	17
HE 240 A	237	238	Neve	PolG	0	0	0	0	5	38	0	33
					38	0	0	0	33	148	0	28
HE 240 A	237	238	Neve	PolG	0	0	0	0	29	119	0	32
					119	0	0	0	32	148	0	5
HE 240 A	237	238	Vento X	PolG	0	0	0	0	9	38	0	51
					38	0	0	0	51	148	0	43
HE 240 A	237	238	Vento X	PolG	0	0	0	0	44	119	0	49
					119	0	0	0	49	148	0	8
Trave 8006												
HE 240 A	237	238	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	158	0	60
HE 240 A	238	239	Peso Proprio	UnifG	0	0	0	0	53	39	0	96
HE 240 A	238	239	QP Solai	PolG	39	0	0	0	96	129	0	94
					129	0	0	0	94	158	0	51
HE 240 A	238	239	QV Solai	PolG	0	0	0	0	17	39	0	31
					39	0	0	0	31	129	0	30
					129	0	0	0	30	158	0	16
HE 240 A	238	239	Neve	PolG	0	0	0	0	27	129	0	30
					129	0	0	0	30	158	0	5
HE 240 A	238	239	Neve	PolG	0	0	0	0	5	39	0	32
					39	0	0	0	32	158	0	26
HE 240 A	238	239	Vento X	PolG	0	0	0	0	9	39	0	49
					39	0	0	0	49	158	0	41
HE 240 A	238	239	Vento X	PolG	0	0	0	0	42	129	0	47
					129	0	0	0	47	158	0	8
Trave 8007												
HE 240 A	238	239	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	170	0	60
HE 240 A	239	123	Peso Proprio	UnifG	0	0	0	0	50	39	0	92
HE 240 A	239	123	QP Solai	PolG	39	0	0	0	92	141	0	89
					141	0	0	0	89	170	0	49
HE 240 A	239	123	QV Solai	PolG	0	0	0	0	16	39	0	29
					39	0	0	0	29	141	0	28
					141	0	0	0	28	170	0	16
HE 240 A	239	123	Neve	PolG	0	0	0	0	26	141	0	29
					141	0	0	0	29	170	0	5
HE 240 A	239	123	Neve	PolG	0	0	0	0	5	39	0	30
					39	0	0	0	30	170	0	25
HE 240 A	239	123	Vento X	PolG	0	0	0	0	8	39	0	47
					39	0	0	0	47	170	0	39
HE 240 A	239	123	Vento X	PolG	0	0	0	0	40	141	0	45
					141	0	0	0	45	170	0	8
Trave 8008												
HE 240 A	239	123	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	112	0	60
HE 240 A	309	323	Peso Proprio	UnifG	0	0	0	0	67	36	0	124
HE 240 A	309	323	QP Solai	PolG	36	0	0	0	124	85	0	122
					85	0	0	0	122	112	0	65
HE 240 A	309	323	QV Solai	PolG	0	0	0	0	21	36	0	40
					36	0	0	0	40	85	0	39
					85	0	0	0	39	112	0	21
HE 240 A	309	323	Neve	PolG	0	0	0	0	5	36	0	40
					36	0	0	0	40	112	0	35
HE 240 A	309	323	Neve	PolG	0	0	0	0	36	85	0	39
					85	0	0	0	39	112	0	5
HE 240 A	309	323	Vento X	PolG	0	0	0	0	9	36	0	62
					36	0	0	0	62	112	0	55
HE 240 A	309	323	Vento X	PolG	0	0	0	0	56	85	0	60
					85	0	0	0	60	112	0	8
HE 240 A	309	323	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	108	0	60
HE 240 A	323	324	Peso Proprio	UnifG	0	0	0	0	60	108	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf	
HE 240 A	323	324	QP Solai	PolG	0	0	0	64	34	0	0	119	
						34	0	0	119	83	0	0	117
						83	0	0	117	108	0	0	63
HE 240 A	323	324	QV Solai	PolG	0	0	0	21	34	0	0	38	
						34	0	0	38	83	0	0	38
						83	0	0	38	108	0	0	20
HE 240 A	323	324	Neve	PolG	0	0	0	34	83	0	0	38	
						83	0	0	38	108	0	0	5
						PolG	0	0	0	5	34	0	0
HE 240 A	323	324	Vento X	PolG	34	0	0	39	108	0	0	34	
						0	0	0	9	34	0	0	60
						34	0	0	60	108	0	0	52
HE 240 A	323	324	Vento X	PolG	0	0	0	53	83	0	0	58	
						83	0	0	58	108	0	0	8
						Termico AXY=15°C, AXZ=15°C							
HE 240 A	323	324	Carichi termici	Termico	0	0	0	60	113	0	0	60	
						0	0	0	62	34	0	0	115
						PolG	34	0	0	115	88	0	0
HE 240 A	324	235	QP Solai	PolG	88	0	0	113	113	0	0	61	
						0	0	0	20	34	0	0	37
						PolG	0	0	0	37	88	0	0
HE 240 A	324	235	QV Solai	PolG	34	0	0	30	113	0	0	19	
						88	0	0	36	113	0	0	36
						PolG	0	0	0	5	34	0	0
HE 240 A	324	235	Neve	PolG	88	0	0	36	113	0	0	5	
						0	0	0	5	34	0	0	37
						PolG	34	0	0	37	113	0	0
HE 240 A	324	235	Vento X	PolG	0	0	0	51	88	0	0	56	
						88	0	0	56	113	0	0	8
						PolG	0	0	0	9	34	0	0
HE 240 A	324	235	Vento X	PolG	0	0	0	58	113	0	0	50	
						34	0	0	58	113	0	0	50
						Termico AXY=15°C, AXZ=15°C							
Trave 8003													
HE 240 A	121	122	Peso Proprio	UnitG	0	0	0	60	178	0	0	60	
						0	0	0	65	30	0	0	104
						PolG	30	0	0	104	140	0	0
HE 240 A	121	122	QV Solai	PolG	140	0	0	103	178	0	0	44	
						0	0	0	21	30	0	0	33
						30	0	0	33	140	0	0	33
HE 240 A	121	122	Neve	PolG	140	0	0	33	178	0	0	14	
						0	0	0	36	140	0	0	39
						PolG	140	0	0	39	178	0	0
HE 240 A	121	122	Neve	PolG	0	0	0	4	30	0	0	28	
						30	0	0	28	178	0	0	23
						PolG	0	0	0	6	30	0	0
HE 240 A	121	122	Vento X	PolG	0	0	0	56	140	0	0	36	
						30	0	0	43	178	0	0	61
						PolG	0	0	0	56	140	0	0
HE 240 A	121	122	Vento X	PolG	140	0	0	61	178	0	0	6	
						0	0	0	61	178	0	0	6
						Termico AXY=15°C, AXZ=15°C							
HE 240 A	121	122	Carichi termici	Termico	0	0	0	60	182	0	0	60	
						0	0	0	65	29	0	0	102
						PolG	29	0	0	102	143	0	0
HE 240 A	122	104	QV Solai	PolG	143	0	0	100	182	0	0	41	
						0	0	0	21	29	0	0	33
						29	0	0	33	143	0	0	32
HE 240 A	122	104	Neve	PolG	143	0	0	32	182	0	0	13	
						0	0	0	36	143	0	0	39
						PolG	143	0	0	39	182	0	0
HE 240 A	122	104	Neve	PolG	0	0	0	4	29	0	0	26	
						29	0	0	26	182	0	0	22
						PolG	0	0	0	6	29	0	0
HE 240 A	122	104	Vento X	PolG	29	0	0	41	182	0	0	34	
						0	0	0	56	143	0	0	61
						PolG	143	0	0	61	182	0	0
HE 240 A	122	104	Vento X	PolG	0	0	0	61	182	0	0	60	
						0	0	0	65	27	0	0	116
						Termico AXY=15°C, AXZ=15°C							
HE 240 A	122	104	Carichi termici	Termico	0	0	0	60	123	0	0	60	
						0	0	0	65	27	0	0	116
						PolG	0	0	0	60	123	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					27	0	0	116	97	0	0	114
					97	0	0	114	123	0	0	56
HE 240 A	230	231	QV Solai	PolG	0	0	0	21	27	0	0	37
					27	0	0	37	97	0	0	37
					97	0	0	37	123	0	0	18
HE 240 A	230	231	Neve	PolG	0	0	0	4	27	0	0	35
					27	0	0	35	123	0	0	31
HE 240 A	230	231	Neve	PolG	0	0	0	36	97	0	0	39
					97	0	0	39	123	0	0	4
HE 240 A	230	231	Vento X	PolG	0	0	0	6	27	0	0	54
					27	0	0	54	123	0	0	48
HE 240 A	230	231	Vento X	PolG	0	0	0	56	97	0	0	61
					97	0	0	61	123	0	0	6
					ΔXY=15°C,ΔXZ=15°C							
HE 240 A	230	231	Carichi termici	Termico	0	0	0	60	134	0	0	60
HE 240 A	231	232	Peso Proprio	UnitG	0	0	0	65	29	0	0	114
HE 240 A	231	232	QP Solai	PolG	0	0	0	114	106	0	0	112
					29	0	0	112	134	0	0	53
HE 240 A	231	232	QV Solai	PolG	0	0	0	21	29	0	0	36
					106	0	0	36	106	0	0	36
					29	0	0	36	134	0	0	17
HE 240 A	231	232	Neve	PolG	0	0	0	36	106	0	0	39
					106	0	0	39	134	0	0	4
HE 240 A	231	232	Neve	PolG	0	0	0	4	29	0	0	34
					29	0	0	34	134	0	0	29
HE 240 A	231	232	Vento X	PolG	0	0	0	6	29	0	0	52
					29	0	0	52	134	0	0	45
HE 240 A	231	232	Vento X	PolG	0	0	0	56	106	0	0	61
					106	0	0	61	134	0	0	6
					ΔXY=15°C,ΔXZ=15°C							
HE 240 A	231	232	Carichi termici	Termico	0	0	0	60	148	0	0	60
HE 240 A	232	233	Peso Proprio	UnitG	0	0	0	65	30	0	0	111
HE 240 A	232	233	QP Solai	PolG	0	0	0	111	117	0	0	110
					30	0	0	110	148	0	0	51
HE 240 A	232	233	QV Solai	PolG	117	0	0	21	30	0	0	36
					30	0	0	36	117	0	0	35
					117	0	0	35	148	0	0	16
HE 240 A	232	233	Neve	PolG	0	0	0	4	30	0	0	32
					30	0	0	32	148	0	0	28
HE 240 A	232	233	Neve	PolG	0	0	0	36	117	0	0	39
					117	0	0	39	148	0	0	4
HE 240 A	232	233	Vento X	PolG	0	0	0	6	30	0	0	50
					30	0	0	50	148	0	0	43
HE 240 A	232	233	Vento X	PolG	0	0	0	56	117	0	0	61
					117	0	0	61	148	0	0	6
					ΔXY=15°C,ΔXZ=15°C							
HE 240 A	232	233	Carichi termici	Termico	0	0	0	60	159	0	0	60
HE 240 A	233	234	Peso Proprio	UnitG	0	0	0	65	30	0	0	109
HE 240 A	233	234	QP Solai	PolG	0	0	0	109	125	0	0	107
					30	0	0	107	159	0	0	49
					125	0	0	125	0	0	0	35
HE 240 A	233	234	QV Solai	PolG	0	0	0	21	30	0	0	35
					30	0	0	35	125	0	0	34
					125	0	0	34	159	0	0	16
HE 240 A	233	234	Neve	PolG	0	0	0	36	125	0	0	39
					125	0	0	39	159	0	0	4
HE 240 A	233	234	Neve	PolG	0	0	0	4	30	0	0	31
					30	0	0	31	159	0	0	26
HE 240 A	233	234	Vento X	PolG	0	0	0	56	125	0	0	61
					125	0	0	61	159	0	0	6
HE 240 A	233	234	Vento X	PolG	0	0	0	6	30	0	0	47
					30	0	0	47	159	0	0	41
					ΔXY=15°C,ΔXZ=15°C							
HE 240 A	233	234	Carichi termici	Termico	0	0	0	60	170	0	0	60
HE 240 A	234	121	Peso Proprio	UnitG	0	0	0	65	31	0	0	106
HE 240 A	234	121	QP Solai	PolG	0	0	0	106	134	0	0	105
					31	0	0	105	170	0	0	46
					134	0	0	106	170	0	0	46

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	234	121	QV Solai	PolG	0	0	0	21	31	0	0	34
					31	0	0	34	134	0	0	34
HE 240 A	234	121	Neve	PolG	134	0	0	34	170	0	0	15
					0	0	0	4	31	0	0	29
HE 240 A	234	121	Neve	PolG	31	0	0	29	170	0	0	25
					0	0	0	36	134	0	0	39
HE 240 A	234	121	Vento X	PolG	134	0	0	39	170	0	0	4
					0	0	0	56	134	0	0	61
HE 240 A	234	121	Vento X	PolG	134	0	0	61	170	0	0	6
					0	0	0	6	31	0	0	45
HE 240 A	234	121	Carichi termici	Termico	31	0	0	45	170	0	0	38
					AXY=15°C,AXZ=15°C							
HE 240 A	310	321	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
					0	0	0	65	29	0	0	123
HE 240 A	310	321	QV Solai	PolG	29	0	0	123	89	0	0	122
					89	0	0	122	112	0	0	63
HE 240 A	310	321	Neve	PolG	0	0	0	21	29	0	0	39
					29	0	0	39	89	0	0	39
HE 240 A	310	321	Neve	PolG	89	0	0	39	112	0	0	20
					0	0	0	36	89	0	0	39
HE 240 A	310	321	Neve	PolG	89	0	0	39	112	0	0	4
					0	0	0	4	29	0	0	39
HE 240 A	310	321	Vento X	PolG	29	0	0	39	112	0	0	35
					0	0	0	56	89	0	0	61
HE 240 A	310	321	Vento X	PolG	89	0	0	61	112	0	0	6
					0	0	0	6	29	0	0	61
HE 240 A	310	322	Carichi termici	Termico	29	0	0	61	112	0	0	54
					AXY=15°C,AXZ=15°C							
HE 240 A	321	322	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
					0	0	0	65	26	0	0	121
HE 240 A	321	322	QV Solai	PolG	26	0	0	121	86	0	0	119
					86	0	0	119	108	0	0	61
HE 240 A	321	322	Neve	PolG	0	0	0	21	26	0	0	39
					26	0	0	39	86	0	0	38
HE 240 A	321	322	Neve	PolG	86	0	0	38	108	0	0	19
					0	0	0	4	26	0	0	38
HE 240 A	321	322	Neve	PolG	26	0	0	38	108	0	0	34
					0	0	0	36	86	0	0	39
HE 240 A	321	322	Vento X	PolG	86	0	0	39	108	0	0	4
					0	0	0	56	86	0	0	61
HE 240 A	321	322	Vento X	PolG	86	0	0	61	108	0	0	6
					0	0	0	6	26	0	0	58
HE 240 A	322	322	Carichi termici	Termico	26	0	0	58	108	0	0	52
					AXY=15°C,AXZ=15°C							
HE 240 A	322	230	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
					0	0	0	65	27	0	0	118
HE 240 A	322	230	QV Solai	PolG	27	0	0	118	90	0	0	117
					90	0	0	117	113	0	0	58
HE 240 A	322	230	Neve	PolG	0	0	0	21	27	0	0	38
					27	0	0	38	90	0	0	37
HE 240 A	322	230	Neve	PolG	90	0	0	37	113	0	0	19
					0	0	0	36	90	0	0	39
HE 240 A	322	230	Neve	PolG	90	0	0	39	113	0	0	4
					0	0	0	4	27	0	0	36
HE 240 A	322	230	Vento X	PolG	27	0	0	36	113	0	0	32
					0	0	0	56	90	0	0	61
HE 240 A	322	230	Vento X	PolG	90	0	0	61	113	0	0	6
					0	0	0	6	27	0	0	56
HE 240 A	322	230	Carichi termici	Termico	27	0	0	56	113	0	0	50
					AXY=15°C,AXZ=15°C							
Trave 8004												
HE 240 A	119	120	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
					0	0	0	46	38	0	0	104
HE 240 A	119	120	QV Solai	PolG	38	0	0	104	158	0	0	102
					158	0	0	102	178	0	0	65
HE 240 A	119	120	Neve	PolG	0	0	0	15	38	0	0	33

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					38	0	0	33	158	0	0	33
HE 240 A	119	120	Neve	PolG	158	0	0	33	178	0	0	21
					0	0	0	25	158	0	0	27
HE 240 A	119	120	Neve	PolG	158	0	0	27	178	0	0	4
					0	0	0	4	38	0	0	39
HE 240 A	119	120	Vento X	PolG	38	0	0	39	178	0	0	36
					0	0	0	6	38	0	0	61
HE 240 A	119	120	Vento X	PolG	38	0	0	61	178	0	0	56
					0	0	0	38	158	0	0	41
HE 240 A	119	120	Carichi termici	Termico	158	0	0	41	178	0	0	6
					AXY=15°C,AXZ=15°C							
HE 240 A	120	105	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
					0	0	0	43	39	0	0	101
HE 240 A	120	105	QV Solai	PolG	39	0	0	101	163	0	0	100
					163	0	0	100	182	0	0	65
HE 240 A	120	105	Neve	PolG	0	0	0	14	39	0	0	32
					39	0	0	32	163	0	0	32
HE 240 A	120	105	Neve	PolG	163	0	0	32	182	0	0	21
					0	0	0	4	39	0	0	39
HE 240 A	120	105	Neve	PolG	39	0	0	39	182	0	0	36
					0	0	0	23	163	0	0	25
HE 240 A	120	105	Vento X	PolG	163	0	0	25	182	0	0	4
					0	0	0	36	163	0	0	39
HE 240 A	120	105	Vento X	PolG	163	0	0	39	182	0	0	6
					0	0	0	6	39	0	0	61
HE 240 A	120	105	Carichi termici	Termico	39	0	0	61	182	0	0	56
					AXY=15°C,AXZ=15°C							
HE 240 A	225	226	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
					0	0	0	57	26	0	0	115
HE 240 A	225	226	QV Solai	PolG	26	0	0	115	105	0	0	113
					105	0	0	113	123	0	0	65
HE 240 A	225	226	Neve	PolG	0	0	0	18	26	0	0	37
					26	0	0	37	105	0	0	36
HE 240 A	225	226	Neve	PolG	105	0	0	32	105	0	0	21
					0	0	0	34	123	0	0	4
HE 240 A	225	226	Neve	PolG	105	0	0	34	123	0	0	39
					0	0	0	39	123	0	0	36
HE 240 A	225	226	Vento X	PolG	26	0	0	49	105	0	0	52
					0	0	0	52	123	0	0	6
HE 240 A	225	226	Vento X	PolG	105	0	0	6	26	0	0	61
					0	0	0	61	123	0	0	56
HE 240 A	225	226	Carichi termici	Termico	26	0	0	61	123	0	0	56
					AXY=15°C,AXZ=15°C							
HE 240 A	226	227	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
					0	0	0	55	28	0	0	113
HE 240 A	226	227	QV Solai	PolG	28	0	0	113	116	0	0	111
					116	0	0	111	134	0	0	65
HE 240 A	226	227	Neve	PolG	0	0	0	18	28	0	0	36
					28	0	0	36	116	0	0	36
HE 240 A	226	227	Neve	PolG	116	0	0	36	134	0	0	21
					0	0	0	4	28	0	0	39
HE 240 A	226	227	Neve	PolG	28	0	0	39	134	0	0	36
					0	0	0	30	116	0	0	32
HE 240 A	226	227	Vento X	PolG	116	0	0	32	134	0	0	4
					0	0	0	6	28	0	0	61
HE 240 A	226	227	Vento X	PolG	28	0	0	61	134	0	0	56
					0	0	0	47	116	0	0	50
HE 240 A	226	227	Carichi termici	Termico	116	0	0	50	134	0	0	6
					AXY=15°C,AXZ=15°C							
HE 240 A	227	228	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
					0	0	0	53	31	0	0	110
HE 240 A	227	228	QV Solai	PolG	31	0	0	110	128	0	0	109
					128	0	0	109	148	0	0	65
HE 240 A	227	228	Neve	PolG	0	0	0	17	31	0	0	35
					31	0	0	35	128	0	0	35
HE 240 A	227	228	Neve	PolG	128	0	0	35	148	0	0	21

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	227	228	Neve	PolG	0	0	0	4	31	0	0	39
HE 240 A	227	228	Neve	PolG	31	0	0	39	148	0	0	36
HE 240 A	227	228	Vento X	PolG	128	0	0	31	148	0	0	4
HE 240 A	227	228	Vento X	PolG	0	0	0	6	31	0	0	61
HE 240 A	227	228	Vento X	PolG	31	0	0	61	148	0	0	56
HE 240 A	227	228	Vento X	PolG	128	0	0	45	128	0	0	48
HE 240 A	227	228	Carichi termici	Termico	0	0	0	60	158	0	0	60
HE 240 A	228	229	Peso Proprio	UnifG	0	0	0	50	33	0	0	108
HE 240 A	228	229	QP Solai	PolG	33	0	0	108	139	0	0	107
HE 240 A	228	229	QV Solai	PolG	139	0	0	107	158	0	0	65
HE 240 A	228	229	QV Solai	PolG	33	0	0	16	33	0	0	35
HE 240 A	228	229	QV Solai	PolG	33	0	0	35	139	0	0	34
HE 240 A	228	229	Neve	PolG	139	0	0	34	158	0	0	21
HE 240 A	228	229	Neve	PolG	0	0	0	27	139	0	0	30
HE 240 A	228	229	Neve	PolG	139	0	0	30	158	0	0	4
HE 240 A	228	229	Neve	PolG	0	0	0	4	33	0	0	39
HE 240 A	228	229	Vento X	PolG	33	0	0	39	158	0	0	36
HE 240 A	228	229	Vento X	PolG	0	0	0	42	139	0	0	46
HE 240 A	228	229	Vento X	PolG	139	0	0	46	158	0	0	6
HE 240 A	228	229	Vento X	PolG	0	0	0	6	33	0	0	61
HE 240 A	228	229	Carichi termici	Termico	33	0	0	61	158	0	0	56
HE 240 A	229	119	Peso Proprio	UnifG	0	0	0	60	170	0	0	60
HE 240 A	229	119	QP Solai	PolG	0	0	0	48	36	0	0	106
HE 240 A	229	119	QP Solai	PolG	36	0	0	106	150	0	0	104
HE 240 A	229	119	QP Solai	PolG	150	0	0	104	170	0	0	65
HE 240 A	229	119	QV Solai	PolG	0	0	0	15	36	0	0	34
HE 240 A	229	119	QV Solai	PolG	36	0	0	34	150	0	0	33
HE 240 A	229	119	QV Solai	PolG	150	0	0	33	170	0	0	21
HE 240 A	229	119	Neve	PolG	0	0	0	4	36	0	0	39
HE 240 A	229	119	Neve	PolG	36	0	0	39	170	0	0	36
HE 240 A	229	119	Neve	PolG	0	0	0	26	150	0	0	28
HE 240 A	229	119	Vento X	PolG	150	0	0	28	170	0	0	4
HE 240 A	229	119	Vento X	PolG	0	0	0	6	36	0	0	61
HE 240 A	229	119	Vento X	PolG	36	0	0	61	170	0	0	56
HE 240 A	229	119	Vento X	PolG	0	0	0	40	150	0	0	44
HE 240 A	229	119	Vento X	PolG	150	0	0	44	170	0	0	6
HE 240 A	229	119	Carichi termici	Termico	0	0	0	60	112	0	0	60
HE 240 A	311	319	Peso Proprio	UnifG	0	0	0	64	23	0	0	122
HE 240 A	311	319	QP Solai	PolG	23	0	0	122	94	0	0	120
HE 240 A	311	319	QP Solai	PolG	94	0	0	120	112	0	0	64
HE 240 A	311	319	QV Solai	PolG	0	0	0	21	23	0	0	39
HE 240 A	311	319	QV Solai	PolG	23	0	0	39	94	0	0	39
HE 240 A	311	319	QV Solai	PolG	94	0	0	39	112	0	0	21
HE 240 A	311	319	Neve	PolG	0	0	0	36	94	0	0	38
HE 240 A	311	319	Neve	PolG	94	0	0	38	112	0	0	4
HE 240 A	311	319	Neve	PolG	0	0	0	4	23	0	0	39
HE 240 A	311	319	Vento X	PolG	23	0	0	39	112	0	0	36
HE 240 A	311	319	Vento X	PolG	0	0	0	6	23	0	0	61
HE 240 A	311	319	Vento X	PolG	23	0	0	61	112	0	0	56
HE 240 A	311	319	Vento X	PolG	0	0	0	56	94	0	0	59
HE 240 A	311	319	Carichi termici	Termico	94	0	0	59	112	0	0	6
HE 240 A	319	320	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
HE 240 A	319	320	QP Solai	PolG	0	0	0	62	22	0	0	120
HE 240 A	319	320	QP Solai	PolG	22	0	0	120	91	0	0	118
HE 240 A	319	320	QP Solai	PolG	91	0	0	118	108	0	0	64
HE 240 A	319	320	QV Solai	PolG	0	0	0	20	22	0	0	38
HE 240 A	319	320	QV Solai	PolG	22	0	0	38	91	0	0	38
HE 240 A	319	320	QV Solai	PolG	91	0	0	38	108	0	0	21
HE 240 A	319	320	Neve	PolG	0	0	0	4	22	0	0	39
HE 240 A	319	320	Neve	PolG	22	0	0	39	108	0	0	36

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	319	320	Neve	PolG	0	0	0	35	91	0	0	37
HE 240 A	319	320	Vento X	PolG	91	0	0	37	108	0	0	4
HE 240 A	319	320	Vento X	PolG	0	0	0	53	91	0	0	57
HE 240 A	319	320	Vento X	PolG	91	0	0	57	108	0	0	6
HE 240 A	319	320	Vento X	PolG	0	0	0	6	22	0	0	61
HE 240 A	319	320	Vento X	PolG	22	0	0	61	108	0	0	56
HE 240 A	319	320	Carichi termici	Termico	0	0	0	60	113	0	0	60
HE 240 A	320	225	Peso Proprio	UnifG	0	0	0	60	23	0	0	117
HE 240 A	320	225	QP Solai	PolG	23	0	0	117	96	0	0	116
HE 240 A	320	225	QP Solai	PolG	96	0	0	116	113	0	0	65
HE 240 A	320	225	QV Solai	PolG	0	0	0	19	23	0	0	38
HE 240 A	320	225	QV Solai	PolG	23	0	0	38	96	0	0	37
HE 240 A	320	225	Neve	PolG	96	0	0	37	113	0	0	21
HE 240 A	320	225	Neve	PolG	0	0	0	4	23	0	0	39
HE 240 A	320	225	Neve	PolG	23	0	0	39	113	0	0	36
HE 240 A	320	225	Neve	PolG	0	0	0	33	96	0	0	35
HE 240 A	320	225	Vento X	PolG	96	0	0	35	113	0	0	4
HE 240 A	320	225	Vento X	PolG	0	0	0	6	23	0	0	61
HE 240 A	320	225	Vento X	PolG	23	0	0	61	113	0	0	56
HE 240 A	320	225	Vento X	PolG	0	0	0	51	96	0	0	54
HE 240 A	320	225	Vento X	PolG	96	0	0	54	113	0	0	6
HE 240 A	320	225	Carichi termici	Termico	0	0	0	60	178	0	0	60
HE 240 A	320	225	Peso Proprio	UnifG	0	0	0	4	21	0	0	43
HE 240 A	320	225	QP Solai	PolG	21	0	0	43	178	0	0	38
HE 240 A	320	225	QP Solai	PolG	0	0	0	1	21	0	0	14
HE 240 A	320	225	QV Solai	PolG	21	0	0	14	178	0	0	12
HE 240 A	320	225	QV Solai	PolG	0	0	0	3	21	0	0	27
HE 240 A	320	225	Neve	PolG	21	0	0	27	178	0	0	23
HE 240 A	320	225	Vento X	PolG	0	0	0	4	21	0	0	42
HE 240 A	320	225	Vento X	PolG	21	0	0	42	178	0	0	36
HE 240 A	320	225	Carichi termici	Termico	0	0	0	60	182	0	0	60
HE 240 A	320	225	Peso Proprio	UnifG	0	0	0	4	20	0	0	41
HE 240 A	320	225	QP Solai	PolG	20	0	0	41	182	0	0	35
HE 240 A	320	225	QP Solai	PolG	0	0	0	1	20	0	0	13
HE 240 A	320	225	QV Solai	PolG	20	0	0	13	182	0	0	11
HE 240 A	320	225	QV Solai	PolG	0	0	0	3	20	0	0	25
HE 240 A	320	225	Neve	PolG	20	0	0	25	182	0	0	22
HE 240 A	320	225	Vento X	PolG	0	0	0	4	20	0	0	39
HE 240 A	320	225	Vento X	PolG	20	0	0	39	182	0	0	34
HE 240 A	320	225	Carichi termici	Termico	0	0	0	60	123	0	0	60
HE 240 A	320	225	Peso Proprio	UnifG	0	0	0	4	19	0	0	55
HE 240 A	320	225	QP Solai	PolG	19	0	0	55	123	0	0	49
HE 240 A	320	225	QP Solai	PolG	0	0	0	1	19	0	0	18
HE 240 A	320	225	QV Solai	PolG	19	0	0	18	123	0	0	16
HE 240 A	320	225	QV Solai	PolG	0	0	0	3	19	0	0	34
HE 240 A	320	225	Neve	PolG	19	0	0	34	123	0	0	31
HE 240 A	320	225	Vento X	PolG	0	0	0	4	19	0	0	53
HE 240 A	320	225	Vento X	PolG	19	0	0	53	123	0	0	47
HE 240 A	320	225	Carichi termici	Termico	0	0	0	60	134	0	0	60
HE 240 A	320	225	Peso Proprio	UnifG	0	0	0	4	19	0	0	52
HE 240 A	320	225	QP Solai	PolG	19	0	0	52	134	0	0	47
HE 240 A	320	225	QP Solai	PolG	0	0	0	1	19	0	0	17
HE 240 A	320	225	QV Solai	PolG	19	0	0	17	134	0	0	15
HE 240 A	320	225	QV Solai	PolG	0	0	0	3	19	0	0	33
HE 240 A	320	225	Neve	PolG	19	0	0	33	134	0	0	29
HE 240 A	320	225	Vento X	PolG	0	0	0	4	19	0	0	50
HE 240 A	320	225	Vento X	PolG	19	0	0	50	134	0	0	45
HE 240 A	320	225	Carichi termici	Termico	0	0	0	60	148	0	0	60
HE 240 A	320	225	Peso Proprio	UnifG	0	0	0	4	20	0	0	50
HE 240 A	320	225	QP Solai	PolG	0	0	0	4	20	0	0	50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf		
HE 240 A	242	243	QV Solai	PolG	20	0	0	0	50	148	0	45		
				PolG	0	0	0	0	1	20	0	16		
				PolG	20	0	0	0	16	148	0	14		
HE 240 A	242	243	Neve	PolG	0	0	0	0	3	20	0	31		
				PolG	20	0	0	0	31	148	0	28		
HE 240 A	242	243	Vento X	PolG	0	0	0	0	4	20	0	48		
				PolG	20	0	0	0	48	148	0	43		
HE 240 A	242	243	Carichi termici	Termico	AXY=15°C,AXZ=15°C									
	HE 240 A	243	Peso Proprio	UnitG	0	0	0	0	60	158	0	60		
	HE 240 A	243	Qp Solai	PolG	0	0	0	0	4	21	0	48		
	HE 240 A	243	Qp Solai	PolG	21	0	0	0	48	158	0	42		
HE 240 A	243	244	QV Solai	PolG	0	0	0	0	1	21	0	15		
				PolG	21	0	0	0	15	158	0	14		
	HE 240 A	243	Neve	PolG	0	0	0	0	3	21	0	30		
				PolG	21	0	0	0	30	158	0	26		
HE 240 A	243	244	Vento X	PolG	0	0	0	0	4	21	0	46		
				PolG	21	0	0	0	46	158	0	41		
HE 240 A	243	244	Carichi termici	Termico	AXY=15°C,AXZ=15°C									
	HE 240 A	244	Peso Proprio	UnitG	0	0	0	0	60	170	0	60		
	HE 240 A	125	Qp Solai	PolG	0	0	0	0	4	21	0	46		
	HE 240 A	244	125	Qp Solai	PolG	21	0	0	0	46	170	0	40	
HE 240 A	244	125	QV Solai	PolG	0	0	0	0	1	21	0	15		
				PolG	21	0	0	0	15	170	0	13		
	HE 240 A	244	Neve	PolG	0	0	0	0	3	21	0	28		
				PolG	21	0	0	0	28	170	0	25		
HE 240 A	244	125	Vento X	PolG	0	0	0	0	4	21	0	44		
				PolG	21	0	0	0	44	170	0	38		
HE 240 A	244	125	Carichi termici	Termico	AXY=15°C,AXZ=15°C									
	HE 240 A	312	325	UnitG	0	0	0	0	60	112	0	60		
	HE 240 A	312	325	Peso Proprio	UnitG	0	0	0	4	19	0	62		
	HE 240 A	312	325	Qp Solai	PolG	19	0	0	0	62	112	0	56	
HE 240 A	312	325	QV Solai	PolG	0	0	0	0	1	19	0	20		
				PolG	19	0	0	0	20	112	0	18		
	HE 240 A	312	325	Neve	PolG	0	0	0	3	19	0	38		
				PolG	19	0	0	0	38	112	0	35		
HE 240 A	312	325	Vento X	PolG	0	0	0	0	4	19	0	59		
				PolG	19	0	0	0	59	112	0	54		
HE 240 A	312	325	Carichi termici	Termico	AXY=15°C,AXZ=15°C									
	HE 240 A	325	326	UnitG	0	0	0	0	60	108	0	60		
	HE 240 A	325	326	Peso Proprio	UnitG	0	0	0	4	18	0	59		
	HE 240 A	325	326	Qp Solai	PolG	18	0	0	0	59	108	0	54	
HE 240 A	325	326	QV Solai	PolG	0	0	0	0	1	18	0	19		
				PolG	18	0	0	0	19	108	0	17		
	HE 240 A	325	326	Neve	PolG	0	0	0	3	18	0	37		
				PolG	18	0	0	0	37	108	0	34		
HE 240 A	325	326	Vento X	PolG	0	0	0	0	4	18	0	57		
				PolG	18	0	0	0	57	108	0	52		
HE 240 A	325	326	Carichi termici	Termico	AXY=15°C,AXZ=15°C									
	HE 240 A	326	240	UnitG	0	0	0	0	60	113	0	60		
	HE 240 A	326	240	Peso Proprio	UnitG	0	0	0	4	18	0	57		
	HE 240 A	326	240	Qp Solai	PolG	18	0	0	0	57	113	0	52	
HE 240 A	326	240	QV Solai	PolG	0	0	0	0	1	18	0	18		
				PolG	18	0	0	0	18	113	0	17		
	HE 240 A	326	240	Neve	PolG	0	0	0	3	18	0	35		
				PolG	18	0	0	0	35	113	0	32		
HE 240 A	326	240	Vento X	PolG	0	0	0	0	4	18	0	55		
				PolG	18	0	0	0	55	113	0	50		
Trave 8006	HE 240 A	326	240	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C								
	HE 240 A	1002	1001	Peso Proprio	UnitG	0	0	0	0	60	115	0	60	
	HE 240 A	1002	1001	Vetro	UnitL	0	0	0	0	200	0	115	0	200
	HE 240 A	1003	1002	Peso Proprio	UnitG	0	0	0	0	60	115	0	60	
HE 240 A	1003	1002	Vetro	UnitL	0	0	0	0	200	0	115	0	200	
	HE 240 A	1004	1003	Peso Proprio	UnitG	0	0	0	0	60	115	0	60	
	HE 240 A	1004	1003	Vetro	UnitL	0	0	0	0	200	0	115	0	200
	HE 240 A	1005	1004	Peso Proprio	UnitG	0	0	0	0	60	115	0	60	

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	QXf	OYf	QZf
HE 240 A	1005	1004	Vetro	UnitL	0	0	0	200	0	115	0	200
HE 240 A	1006	1005	Peso Proprio	UnitG	0	0	0	0	60	115	0	0
HE 240 A	1006	1005	Vetro	UnitL	0	0	0	200	0	115	0	200
HE 240 A	1007	1006	Peso Proprio	UnitG	0	0	0	0	60	115	0	0
HE 240 A	1007	1006	Vetro	UnitL	0	0	0	200	0	115	0	200
HE 240 A	1008	1007	Peso Proprio	UnitG	0	0	0	0	60	115	0	0
HE 240 A	1008	1007	Vetro	UnitL	0	0	0	200	0	115	0	200
HE 240 A	1009	1008	Peso Proprio	UnitG	0	0	0	0	60	115	0	0
HE 240 A	1009	1008	Vetro	UnitL	0	0	0	200	0	115	0	200
HE 240 A	1010	1009	Peso Proprio	UnitG	0	0	0	0	60	115	0	0
HE 240 A	1010	1009	Vetro	UnitL	0	0	0	200	0	115	0	200
Fondazione 318												
F60x100	1	7	Peso Proprio	UnitG	0	0	0	0	1500	108	0	1500
Fondazione 9001												
F60x100	2	1	Peso Proprio	UnitG	0	0	0	0	1500	101	0	1500
F60x100	3	2	Peso Proprio	UnitG	0	0	0	0	1500	90	0	1500
F60x100	4	3	Peso Proprio	UnitG	0	0	0	0	1500	89	0	1500
F60x100	5	4	Peso Proprio	UnitG	0	0	0	0	1500	149	0	1500
F60x100	6	5	Peso Proprio	UnitG	0	0	0	0	1500	102	0	1500
Fondazione 9002												
F60x100	207	208	Peso Proprio	UnitG	0	0	0	0	1500	161	0	1500
F60x100	208	209	Peso Proprio	UnitG	0	0	0	0	1500	149	0	1500
F60x100	209	210	Peso Proprio	UnitG	0	0	0	0	1500	150	0	1500
F60x100	210	211	Peso Proprio	UnitG	0	0	0	0	1500	149	0	1500
F60x100	211	212	Peso Proprio	UnitG	0	0	0	0	1500	161	0	1500
Generica 701												
2LD 60x30x5d10	1001	117	Peso Proprio	UnitG	0	0	0	0	7	307	0	7
Generica 702												
2LD 60x30x5d10	117	1003	Peso Proprio	UnitG	0	0	0	0	7	236	0	7
Generica 703												
2LD 60x30x5d10	1003	1112	Peso Proprio	UnitG	0	0	0	0	7	307	0	7
Generica 704												
2LD 60x30x5d10	1112	1005	Peso Proprio	UnitG	0	0	0	0	7	237	0	7
Generica 705												
2LD 60x30x5d10	1005	1114	Peso Proprio	UnitG	0	0	0	0	7	307	0	7
Generica 706												
2LD 60x30x5d10	1114	1007	Peso Proprio	UnitG	0	0	0	0	7	237	0	7
Generica 707												
2LD 60x30x5d10	1007	1116	Peso Proprio	UnitG	0	0	0	0	7	307	0	7
Generica 708												
2LD 60x30x5d10	1116	1009	Peso Proprio	UnitG	0	0	0	0	7	237	0	7
Generica 709												
2LD 60x30x5d10	1009	1118	Peso Proprio	UnitG	0	0	0	0	7	307	0	7
Generica 710												
2LD 60x30x5d10	1118	317	Peso Proprio	UnitG	0	0	0	0	7	243	0	7
Generica 711												
2LD 60x30x5d10	317	1116	Peso Proprio	UnitG	0	0	0	0	7	314	0	7
Generica 712												
2LD 60x30x5d10	1116	220	Peso Proprio	UnitG	0	0	0	0	7	278	0	7
Generica 713												
2LD 60x30x5d10	220	1114	Peso Proprio	UnitG	0	0	0	0	7	349	0	7
Generica 714												
2LD 60x30x5d10	1114	222	Peso Proprio	UnitG	0	0	0	0	7	222	0	7

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Generica 715												
60x30x5d10												
2LD	222	1112	Peso Proprio	UnifG	0	0	0	7	292	0	0	7
60x30x5d10												
Generica 716												
2LD	1112	224	Peso Proprio	UnifG	0	0	0	7	121	0	0	7
60x30x5d10												
Generica 7001												
Fi16	101	115	Peso Proprio	UnifG	0	0	0	2	371	0	0	2
Fi16	101	115	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7002												
Fi16	115	223	Peso Proprio	UnifG	0	0	0	2	345	0	0	2
Fi16	115	223	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7003												
Fi16	223	216	Peso Proprio	UnifG	0	0	0	2	306	0	0	2
Fi16	223	216	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7004												
Fi16	216	318	Peso Proprio	UnifG	0	0	0	2	269	0	0	2
Fi16	216	318	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7005												
Fi16	318	308	Peso Proprio	UnifG	0	0	0	2	260	0	0	2
Fi16	318	308	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7006												
Fi18	308	207	Peso Proprio	UnifG	0	0	0	2	508	0	0	2
Fi18	308	207	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7007												
Fi18	208	307	Peso Proprio	UnifG	0	0	0	2	508	0	0	2
Fi18	208	307	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7008												
Fi16	307	316	Peso Proprio	UnifG	0	0	0	2	260	0	0	2
Fi16	307	316	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7009												
Fi16	316	221	Peso Proprio	UnifG	0	0	0	2	269	0	0	2
Fi16	316	221	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7010												
Fi16	221	218	Peso Proprio	UnifG	0	0	0	2	306	0	0	2
Fi16	221	218	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7011												
Fi16	218	117	Peso Proprio	UnifG	0	0	0	2	345	0	0	2
Fi16	218	117	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7012												
Fi16	117	102	Peso Proprio	UnifG	0	0	0	2	372	0	0	2
Fi16	117	102	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7013												
Fi16	17	2	Peso Proprio	UnifG	0	0	0	2	285	0	0	2
Fi16	17	2	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7014												
Fi16	19	1	Peso Proprio	UnifG	0	0	0	2	285	0	0	2
Fi16	19	1	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7015												
Fi16	5	18	Peso Proprio	UnifG	0	0	0	2	286	0	0	2
Fi16	5	18	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7016												
Fi16	105	125	Peso Proprio	UnifG	0	0	0	2	372	0	0	2
Fi16	105	125	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7017												
Fi16	125	228	Peso Proprio	UnifG	0	0	0	2	345	0	0	2
Fi16	125	228	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7018												
Fi16	228	241	Peso Proprio	UnifG	0	0	0	2	306	0	0	2
Fi16	228	241	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7019												
Fi16	241	320	Peso Proprio	UnifG	0	0	0	2	269	0	0	2
Fi16	241	320	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7020												

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Generica 7021												
Fi16	320	312	Peso Proprio	UnifG	0	0	0	2	261	0	0	2
Fi16	320	312	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7022												
Fi18	312	211	Peso Proprio	UnifG	0	0	0	2	508	0	0	2
Fi18	312	211	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7023												
Fi16	212	311	Peso Proprio	UnifG	0	0	0	2	508	0	0	2
Fi18	212	311	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7024												
Fi16	311	326	Peso Proprio	UnifG	0	0	0	2	260	0	0	2
Fi16	311	326	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7025												
Fi16	326	226	Peso Proprio	UnifG	0	0	0	2	269	0	0	2
Fi16	326	226	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7026												
Fi16	226	243	Peso Proprio	UnifG	0	0	0	2	306	0	0	2
Fi16	226	243	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7027												
Fi16	243	119	Peso Proprio	UnifG	0	0	0	2	345	0	0	2
Fi16	243	119	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7028												
Fi16	119	106	Peso Proprio	UnifG	0	0	0	2	372	0	0	2
Fi16	119	106	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7029												
Fi16	16	6	Peso Proprio	UnifG	0	0	0	2	286	0	0	2
Fi16	16	6	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7030												
Fi16	324	310	Peso Proprio	UnifG	0	0	0	2	261	0	0	2
Fi16	324	310	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7031												
Fi16	310	320	Peso Proprio	UnifG	0	0	0	2	264	0	0	2
Fi16	310	320	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7032												
Fi16	320	311	Peso Proprio	UnifG	0	0	0	2	218	0	0	2
Fi16	320	311	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7033												
Fi16	311	322	Peso Proprio	UnifG	0	0	0	2	264	0	0	2
Fi16	311	322	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7034												
Fi16	322	309	Peso Proprio	UnifG	0	0	0	2	260	0	0	2
Fi16	322	309	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7035												
Fi16	309	316	Peso Proprio	UnifG	0	0	0	2	260	0	0	2
Fi16	309	316	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7036												
Fi16	324	308	Peso Proprio	UnifG	0	0	0	2	261	0	0	2
Fi16	324	308	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7037												
Fi16	102	123	Peso Proprio	UnifG	0	0	0	2	371	0	0	2
Fi16	102	123	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7038												
Fi16	123	104	Peso Proprio	UnifG	0	0	0	2	371	0	0	2
Fi16	123	104	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7039												
Fi16	104	119	Peso Proprio	UnifG	0	0	0	2	389	0	0	2
Fi16	104	119	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7040												
Fi16	105	121	Peso Proprio	UnifG	0	0	0	2	389	0	0	2
Fi16	105	121	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7041												
Fi16	121	103	Peso Proprio	UnifG	0	0	0	2	372	0	0	2
Fi16	121	103	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7042												
Fi16	103	115	Peso Proprio	UnifG	0	0	0	2	372	0	0	2
Fi16	103	115	Carichi termici	Termico	AXY=15°C, AXZ=15°C							

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Generica 7042												
Fi16	17	26	Peso Proprio	UnifG	0	0	0	2	162	0	0	2
Generica 7043												
Fi16	26	101	Peso Proprio	UnifG	0	0	0	2	162	0	0	2
Generica 7044												
Fi16	25	19	Peso Proprio	UnifG	0	0	0	2	162	0	0	2
Generica 7045												
Fi16	16	22	Peso Proprio	UnifG	0	0	0	2	163	0	0	2
Generica 7046												
Fi16	22	105	Peso Proprio	UnifG	0	0	0	2	163	0	0	2
Generica 7047												
Fi16	106	21	Peso Proprio	UnifG	0	0	0	2	163	0	0	2
Generica 7048												
Fi16	21	18	Peso Proprio	UnifG	0	0	0	2	163	0	0	2
Generica 7049												
Fi16	25	102	Peso Proprio	UnifG	0	0	0	2	162	0	0	2
Generica 7050												
Fi16	104	23	Peso Proprio	UnifG	0	0	0	2	162	0	0	2
Generica 7051												
Fi16	23	15	Peso Proprio	UnifG	0	0	0	2	162	0	0	2
Generica 7052												
Fi16	15	3	Peso Proprio	UnifG	0	0	0	2	285	0	0	2
Generica 7053												
Fi16	4	20	Peso Proprio	UnifG	0	0	0	2	285	0	0	2
Generica 7054												
Fi16	20	24	Peso Proprio	UnifG	0	0	0	2	162	0	0	2
Generica 7055												
Fi16	24	103	Peso Proprio	UnifG	0	0	0	2	162	0	0	2

Dati solai		
Solaiο n°	Nodi	Tipo
1	323-309-308-315	Vetro strutturale
1	321-310-309-323	Vetro strutturale
1	319-311-310-321	Vetro strutturale
1	325-312-311-319	Vetro strutturale
1	313-312-325-328	Vetro strutturale
1	315-308-307-317	Vetro strutturale
2	316-315-317-318	Vetro strutturale
2	326-325-319-320	Vetro strutturale
2	324-323-315-316	Vetro strutturale
2	327-328-325-326	Vetro strutturale
2	322-321-323-324	Vetro strutturale
2	320-319-321-322	Vetro strutturale
3	327-326-240-249	Vetro strutturale
3	230-322-324-235	Vetro strutturale
3	240-326-320-225	Vetro strutturale
3	225-320-322-230	Vetro strutturale
3	235-324-316-215	Vetro strutturale
3	215-316-318-220	Vetro strutturale
4	241-240-225-226	Vetro strutturale
4	231-230-235-236	Vetro strutturale
4	226-225-230-231	Vetro strutturale
4	249-240-241-248	Vetro strutturale
4	216-215-220-221	Vetro strutturale
4	236-235-215-216	Vetro strutturale
5	242-241-226-227	Vetro strutturale
5	232-231-236-237	Vetro strutturale
5	237-236-216-217	Vetro strutturale
5	248-241-242-247	Vetro strutturale
5	227-226-231-232	Vetro strutturale
5	217-216-221-222	Vetro strutturale
6	218-217-222-223	Vetro strutturale
6	104-122-124-103	Vetro strutturale
6	121-234-239-123	Vetro strutturale
6	234-233-238-239	Vetro strutturale

6	233-232-237-238	Vetro strutturale
6	219-218-223-224	Vetro strutturale
6	238-237-217-218	Vetro strutturale
6	239-238-218-219	Vetro strutturale
6	123-239-219-115	Vetro strutturale
6	124-123-115-116	Vetro strutturale
6	103-124-116-102	Vetro strutturale
6	105-120-122-104	Vetro strutturale
6	120-119-121-122	Vetro strutturale
6	119-229-234-121	Vetro strutturale
6	229-228-233-234	Vetro strutturale
6	243-242-227-228	Vetro strutturale
6	244-243-228-229	Vetro strutturale
6	125-244-229-119	Vetro strutturale
6	126-125-119-120	Vetro strutturale
6	106-126-120-105	Vetro strutturale
6	228-227-232-233	Vetro strutturale
6	115-219-224-117	Vetro strutturale
6	102-116-118-101	Vetro strutturale
6	247-242-243-246	Vetro strutturale
6	246-243-244-245	Vetro strutturale
6	245-244-125-128	Vetro strutturale
6	128-125-126-127	Vetro strutturale
6	127-126-106-114	Vetro strutturale
6	116-115-117-118	Vetro strutturale
6	122-121-123-124	Vetro strutturale

TABULATI DI VERIFICA

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Forze sismiche e masse
- Spostamenti Relativi dei nodi (SLD)
- Fattori di partecipazione e masse modali
- Massime tensioni sul terreno aste
- Massime reazioni vincolari
- Massime sollecitazioni travi
- Massime sollecitazioni pilastri
- Massime sollecitazioni aste generiche

Risultati Analisi Dinamica - Baricentri masse e masse

Scenario di calcolo : Set_NT_SLV_A2_STRGEO

Combinazione masse 1

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	11587	727	840	38
1	No	23617	347	560	973
2	No	0	0	0	0
3	No	3120	-209	322	1323

Combinazione masse 2

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	11587	728	841	38
1	No	23617	374	592	973
2	No	0	0	0	0
3	No	3120	-207	324	1323

Combinazione masse 3

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	11587	727	842	38
1	No	23617	347	624	973
2	No	0	0	0	0
3	No	3120	-209	326	1323

Combinazione masse 4

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	11587	727	841	38
1	No	23617	320	592	973
2	No	0	0	0	0
3	No	3120	-210	324	1323

Verifica Degli Spostamenti Relativi

Scenario di calcolo : Set_NT_SLV_A2_STRGEO

Attenzione calcolo agli SLU: Gli spostamenti dovuti al sisma sono stati calcolati in via approssimata moltiplicando gli spostamenti derivanti dagli spettri al limite ultimo per il coefficiente c=Sd(T0)/Su(T0),dove T0 è il periodo fondamentale nella direzione considerata, Sd(T0) e Su(T0) il valore dello spettro in T0 rispettivamente di danno e ultimo

Combinazione		Spettro		c=0.417						
		SpetroNT(q=1)								
SISMAX_SLV		SpetroNT(q=1)		c=0.417						
Interp.	Comb.	ηXv mm	ηXh mm	ηYv mm	ηYh mm	Nodo1	Nodo2	η mm	ηAmm mm	Cs
0-1	(12+13)+V-3	0.46	6.02	0.21	3.63	1	101	6.48	27.10	4.18
0-1	(12+13)+V-3	1.60	6.55	0.64	3.33	2	102	8.15	27.10	3.33
0-1	(12+13)+V-4	2.49	7.82	1.23	0.27	3	103	10.31	27.10	2.63
0-1	(12+13)+V-4	2.89	9.33	1.49	0.50	4	104	12.22	27.10	2.22
0-1	(12+13)+V-4	2.99	10.42	1.58	2.39	5	105	13.41	27.10	2.02
0-1	(12+13)+V-4	2.92	10.68	1.55	2.40	6	106	13.60	27.10	1.99
0-1	(12+13)+I-3	0.36	6.46	0.25	4.77	7	1001	6.81	27.10	3.98
1-1	(12+13)+V-3	0.55	0.86	0.07	0.76	1001	118	1.41	7.30	5.19
1-1	(12+13)+I-4	0.83	0.52	1.47	1.02	1002	117	2.49	12.43	4.99
1-1	(12+13)+III-3	1.67	1.41	2.28	1.80	1003	224	4.08	17.07	4.18
1-1	(12+13)+III-3	2.14	1.83	3.01	2.55	1004	223	5.56	20.95	3.77
1-1	(12+13)+IV-3	2.31	2.75	3.36	3.08	1005	222	6.44	24.08	3.74
1-1	(12+13)+V-3	2.18	2.76	3.29	3.32	1006	221	6.61	26.17	3.96
1-1	(12+13)+III-3	1.72	1.42	2.83	2.74	1007	220	5.57	27.15	4.88
1-1	(12+13)+I-4	1.19	0.26	2.14	1.97	1008	318	4.11	26.93	6.55
1-1	(12+13)+VI-3	0.60	3.52	1.31	4.08	1009	317	5.39	25.27	4.69
1-3	(12+13)+I-3	0.73	3.53	0.17	7.19	1010	307	7.36	21.80	2.96
2-1	(12+13)+V-4	0.12	0.45	0.09	0.27	207	1010	0.57	2.50	4.36
2-3	(12+13)+I-4	1.88	0.56	0.98	7.62	208	1009	8.59	24.30	2.83
2-3	(12+13)+V-3	2.63	7.46	1.39	1.12	209	309	10.09	24.30	2.41
2-3	(12+13)+V-3	3.17	8.81	1.65	0.52	210	310	11.98	24.30	2.03
2-3	(12+13)+V-3	3.54	10.21	1.80	0.08	211	311	13.75	24.30	1.77
2-3	(12+13)+V-3	3.94	11.67	1.98	0.77	212	312	15.61	24.30	1.56
Minimo										
2-3	(12+13)+V-3	3.94	11.67	1.98	0.77	212	312	15.61	24.30	1.56

Periodi di vibrazione e Masse modali

Scenario di calcolo : Set_NT_SLV_A2_STRGEO

Posizione masse 1

Numero di Frequenze calcolate =45, filtrate=18

N		T(s)	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
			Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3691	45.904	-18.405	3322	20664	73.58	11.83	
2(2)	0.3340	-15.775	-44.499	19418	2440	8.69	69.15	
3(3)	0.3087	-0.461	12.255	2	2	0.01	5.24	
4(5)	0.2022	16.692	11.476	2732	2732	9.73	4.60	
5(6)	0.1760	6.763	-6.534	449	419	1.60	1.49	
6(7)	0.1443	2.001	5.848	39	335	0.14	1.19	
7(8)	0.1340	-1.969	-4.306	38	182	0.14	0.65	
8(9)	0.1322	6.838	-4.631	459	210	1.63	0.75	
9(10)	0.1189	1.419	6.331	20	393	0.07	1.40	
10(11)	0.1031	7.564	3.050	561	91	2.00	0.32	
11(12)	0.1009	1.647	-2.381	27	56	0.09	0.20	
12(13)	0.0923	-1.101	3.339	12	109	0.04	0.39	
13(14)	0.0851	2.019	2.558	40	64	0.14	0.23	
14(22)	0.0583	14.625	-2.115	26	44	0.09	0.16	
15(23)	0.0574	-0.193	1.741	0	30	0.00	0.11	
16(30)	0.0464	1.474	-2.371	21	55	0.08	0.20	
17(42)	0.0343	1.631	-2.101	26	43	0.09	0.15	
18(44)	0.0318	-1.750	-2.006	30	39	0.11	0.14	
Somma delle Masse Modali [kgm*g]								
					27587	27576		
Masse strutturali libere [kgm*g]					28083	28083		
Percentuale					98.23	98.19		

Posizione masse 2

Numero di Frequenze calcolate =45, filtrate=17

TABULATI DI VERIFICA

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Forze sismiche e masse
- Spostamenti Relativi dei nodi (SLD)
- Fattori di partecipazione e masse modali
- Massime tensioni sul terreno aste
- Massime reazioni vincolari
- Massime sollecitazioni travi
- Massime sollecitazioni pilastri
- Massime sollecitazioni aste generiche

Risultati Analisi Dinamica - Baricentri masse e masse

Scenario di calcolo : Set_NT_SLV_A2_STRGEO

Combinazione masse 1

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	11587	727	840	38
1	No	23617	347	560	973
2	No	0	0	0	0
3	No	3120	-209	322	1323

Combinazione masse 2

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	11587	728	841	38
1	No	23617	374	592	973
2	No	0	0	0	0
3	No	3120	-207	324	1323

Combinazione masse 3

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	11587	727	842	38
1	No	23617	347	624	973
2	No	0	0	0	0
3	No	3120	-209	326	1323

Combinazione masse 4

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	11587	727	841	38
1	No	23617	320	592	973
2	No	0	0	0	0
3	No	3120	-210	324	1323

Verifica Degli Spostamenti Relativi

Scenario di calcolo : Set_NT_SLV_A2_STRGEO

Attenzione calcolo agli SLU: Gli spostamenti dovuti al sisma sono stati calcolati in via approssimata moltiplicando gli spostamenti derivanti dagli spettri al limite ultimo per il coefficiente c=Sd(T0)/Su(T0),dove T0 è il periodo fondamentale nella direzione considerata, Sd(T0) e Su(T0) il valore dello spettro in T0 rispettivamente di danno e ultimo

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3675	47.049	-15.214	21708	2270	77.30	8.08
2(2)	0.3318	-12.043	-47.251	1422	21895	5.06	77.96
3(5)	0.2027	16.589	11.592	2699	1318	9.61	4.69
4(6)	0.1783	6.602	-7.026	427	484	1.52	1.72
5(7)	0.1440	-1.547	-6.304	23	390	0.08	1.39
6(8)	0.1339	0.624	-5.478	4	294	0.01	1.05
7(9)	0.1329	7.280	-2.831	520	79	1.85	0.28
8(10)	0.1205	10.027	5.884	10	340	0.04	1.21
9(11)	0.1024	7.795	3.337	596	109	2.12	0.39
10(13)	0.0922	-0.733	3.520	5	121	0.02	0.43
11(14)	0.0843	1.635	2.199	26	47	0.09	0.17
12(17)	0.0756	-0.752	1.704	6	28	0.02	0.10
13(24)	0.0555	1.724	-2.311	29	52	0.10	0.19
14(27)	0.0500	1.414	-1.853	20	34	0.07	0.12
15(30)	0.0464	1.216	-1.953	14	37	0.05	0.13
16(42)	0.0343	1.582	-2.218	25	48	0.09	0.17
17(44)	0.0321	0.914	1.760	8	30	0.03	0.11
Somma delle Masse Modali [kgm*g]		27543		27577			
Masse strutturali libere [kgm*g]		28083		28083			
Percentuale		98.08		98.20		98.08	

Posizione masse 3

Numero di Frequenze calcolate =45, filtrate=17

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3730	48.173	-7.744	22758	588	81.04	2.09
2(2)	0.3390	-4.394	-48.758	189	23314	0.67	83.02
3(5)	0.2714	-2.228	2.212	49	48	0.17	0.17
4(5)	0.2007	16.649	12.236	2718	1468	9.68	5.23
5(6)	0.1837	6.675	-7.099	437	494	1.56	1.76
6(7)	0.1475	2.106	5.769	44	326	0.15	1.16
7(8)	0.1349	-3.583	7.261	126	517	0.45	1.84
8(9)	0.1333	6.510	0.234	416	1	1.48	0.00
9(10)	0.1206	1.753	5.545	30	302	0.11	1.07
10(11)	0.1054	7.818	2.140	599	45	2.13	0.16
11(12)	0.0938	-2.638	-3.783	68	140	0.24	0.50
12(13)	0.0912	-2.365	-1.102	55	12	0.20	0.04
13(14)	0.0897	0.894	-3.100	8	94	0.03	0.34
14(17)	0.0758	-1.059	1.848	11	33	0.04	0.12
15(28)	0.0487	-1.129	1.884	13	35	0.04	0.12
16(29)	0.0482	-1.543	2.240	49	240	0.08	0.18
17(43)	0.0338	-0.570	2.142	3	45	0.01	0.16
Somma delle Masse Modali [kgm*g]		27546		27512			
Masse strutturali libere [kgm*g]		28083		28083			
Percentuale		98.09		97.96		98.09	

Posizione masse 4

Numero di Frequenze calcolate =45, filtrate=20

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3733	47.844	-10.527	22448	1087	79.93	3.87
2(2)	0.3409	-7.115	-47.858	496	22461	1.77	79.98
3(3)	0.3054	-0.334	6.765	1	449	0.00	1.60
4(5)	0.2005	16.746	12.138	2750	1445	9.79	5.14
5(6)	0.1817	6.910	-6.568	468	423	1.67	1.51
6(7)	0.1479	2.461	5.431	59	289	0.21	1.03
7(8)	0.1343	-0.270	-6.476	411	11	0.00	1.46
8(9)	0.1331	7.277	-3.412	519	114	1.85	0.41
9(10)	0.1192	2.219	5.989	48	352	0.17	1.25

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
10(11)	0.1058	7.605	1.831	567	33	2.02	0.12
11(12)	0.0949	-2.719	-1.754	73	30	0.26	0.11
12(13)	0.0923	-1.248	-4.593	15	207	0.05	0.74
13(14)	0.0913	-2.310	1.517	52	23	0.19	0.08
14(15)	0.0829	-0.627	1.946	4	37	0.01	0.13
15(17)	0.0755	-1.001	1.912	10	36	0.03	0.13
16(25)	0.0550	-1.560	2.043	24	41	0.08	0.15
17(29)	0.0484	-0.727	1.745	5	30	0.02	0.11
18(30)	0.0479	1.702	-2.298	28	52	0.10	0.18
19(42)	0.0344	-1.592	1.704	25	28	0.09	0.10
20(45)	0.0321	-1.818	-0.713	32	5	0.12	0.02
Somma delle Masse Modali [kgm*g]				27627	27552		
Masse strutturali libere [kgm*g]				98.38	28083		
Percentuale					98.38		98.11

Risultati Analisi Dinamica - Masse tensioni sul terreno aste

Scenario di calcolo : Set NT SLV A2 STRGEO

Asta	N in.	N fin.	0/5	1/5	2/5	3/5	4/5	5/5
	318	1	7	1.51(12-1-3)	1.34(12-1-3)	1.18(12-1-3)	1.03(12-1-2)	1.04(8)
	9001	3	2	1.07(12-1-3)	1.12(12-1-3)	1.17(12-1-3)	1.23(12-1-3)	1.34(12-1-3)
	9001	4	3	1.01(13-1-2)	0.98(13-1-2)	0.96(13-1-2)	0.99(12-1-3)	1.08(12-1-3)
	9001	5	4	1.29(13-1-3)	1.22(13-1-3)	1.16(13-1-3)	1.10(13-1-3)	1.01(13-1-2)
	9001	2	1	1.33(12-1-3)	1.41(12-1-3)	1.49(12-1-3)	1.58(12-1-3)	1.66(12-1-3)
	9001	6	5	1.62(12-11-3)	1.55(12-11-3)	1.48(12-11-3)	1.41(12-11-3)	1.35(13-1-3)
	9002	210	211	1.70(12-11-3)	1.70(12-11-3)	1.70(12-11-3)	1.71(12-11-3)	1.73(12-11-3)
	9002	207	208	1.64(13-11-2)	1.57(13-11-2)	1.54(6)	1.56(6)	1.60(6)
	9002	211	212	1.76(12-11-3)	1.76(12-11-3)	1.77(12-11-3)	1.81(12-11-3)	1.84(12-11-3)
	9002	209	210	1.63(6)	1.63(12-11-3)	1.64(12-11-3)	1.65(12-11-3)	1.70(12-11-3)
	9002	208	209	1.60(6)	1.59(6)	1.59(6)	1.60(6)	1.61(6)

Risultati Analisi Dinamica - Reazioni massime - Nodi

Scenario di calcolo : Set NT SLV A2 STRGEO

Nodo	Rx	Ry	Rz	Mx	My	Mz
	kg	kg	kg	kg*m	kg*m	kg*m
1	-1012(12-1-2)	993(12-1-2)	0	0	0	3(13-1-3)
2	-1287(12-1-3)	-1257(11)	0	0	0	3(2)
3	-1306(12-1-3)	-1410(11)	0	0	0	2(12-1-3)
4	-1509(12-1-3)	-1415(7)	0	0	0	2(13-1-3)
5	-1422(12-1-3)	-1497(7)	0	0	0	2(13-1-3)
6	-1356(12-1-3)	-1616(7)	0	0	0	-2(13-11-3)
7	1563(11)	-2393(7)	0	0	0	-14(3)
207	5563(12-11-4)	-6468(7)	0	0	0	-388(12-11-3)
208	1309(12-11-2)	2094(13-11-3)	0	0	0	-2(8)
209	1602(6)	851(10)	0	0	0	-2(12-11-3)
210	1909(6)	957(6)	0	0	0	-2(12-11-3)
211	2399(12-11-2)	2257(13-11-3)	0	0	0	-2(12-11-3)
212	2976(12-11-3)	2402(13-11-3)	0	0	0	-2(8)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Travi

Asta	N in.	N fin.	N	Ty	Tz	Mt	My	Mz
	kg	kg	kg	kg	kg	kg*m	kg*m	kg*m
707	117	2927(12-1-1)	30(8)	0	0	0	-25(11)	0
	1111	2929(12-1-1)	30(8)	5(3)	0	0	0	-12(8)
708	1111	2893(12-1-1)	-17(8)	-5(6)	0	0	0	-10(8)
	1112	2896(12-1-1)	-17(8)	5(7)	0	0	0	10(8)
709	1112	2656(12-1-1)	-32(11)	-5(5)	0	0	14(12-11-1)	0
	1113	2658(12-1-1)	-32(11)	5(7)	0	0	41(11)	0
710	1113	2656(12-1-1)	33(11)	-5(6)	0	0	37(11)	0
	1114	2659(12-1-1)	5(7)	0	0	0	10(8)	0

711	1114	2496(12-1-1)	-32(11)	0	-5(6)	0	0	20(7)
712	1115	2499(12-1-1)	-32(11)	0	5(7)	0	0	54(11)
713	1116	2503(12-1-1)	34(11)	0	-5(6)	0	0	52(11)
714	1117	2506(12-1-1)	34(11)	0	5(1)	0	0	15(7)
1001	1118	2573(12-1-4)	-59(11)	0	-5(6)	0	0	18(7)
1002	1119	2576(12-1-4)	-59(11)	0	5(7)	0	0	85(11)
1003	1120	2579(12-1-4)	193(11)	0	-5(6)	0	0	83(11)
1004	1121	2582(12-1-4)	193(11)	0	5(7)	0	0	-138(11)
1005	1122	2585(12-1-4)	193(11)	0	-158(6)	0	0	-57(13-11-4)
1006	1123	2588(12-1-4)	193(11)	0	137(6)	0	0	-37(7)
1007	1124	2591(12-1-4)	193(11)	0	-140(6)	0	0	-53(12-1-1)
1008	1125	2594(12-1-4)	193(11)	0	143(6)	0	0	-35(12-11-2)
1009	1126	2597(12-1-4)	193(11)	0	-142(6)	0	0	-46(12-1-4)
1010	1127	2600(12-1-4)	193(11)	0	145(6)	0	0	-35(12-11-3)
1011	1128	2603(12-1-4)	193(11)	0	-146(6)	0	0	-35(12-1-3)
1012	1129	2606(12-1-4)	193(11)	0	147(6)	0	0	-35(12-1-3)
1013	1130	2609(12-1-4)	193(11)	0	-148(6)	0	0	-35(12-1-3)
1014	1131	2612(12-1-4)	193(11)	0	149(6)	0	0	-35(12-1-3)
1015	1132	2615(12-1-4)	193(11)	0	-150(6)	0	0	-35(12-1-3)
1016	1133	2618(12-1-4)	193(11)	0	151(6)	0	0	-35(12-1-3)
1017	1134	2621(12-1-4)	193(11)	0	-152(6)	0	0	-35(12-1-3)
1018	1135	2624(12-1-4)	193(11)	0	153(6)	0	0	-35(12-1-3)
1019	1136	2627(12-1-4)	193(11)	0	-154(6)	0	0	-35(12-1-3)
1020	1137	2630(12-1-4)	193(11)	0	155(6)	0	0	-35(12-1-3)
1021	1138	2633(12-1-4)	193(11)	0	-156(6)	0	0	-35(12-1-3)
1022	1139	2636(12-1-4)	193(11)	0	157(6)	0	0	-35(12-1-3)
1023	1140	2639(12-1-4)	193(11)	0	-158(6)	0	0	-35(12-1-3)
1024	1141	2642(12-1-4)	193(11)	0	159(6)	0	0	-35(12-1-3)
1025	1142	2645(12-1-4)	193(11)	0	-160(6)	0	0	-35(12-1-3)
1026	1143	2648(12-1-4)	193(11)	0	161(6)	0	0	-35(12-1-3)
1027	1144	2651(12-1-4)	193(11)	0	-162(6)	0	0	-35(12-1-3)
1028	1145	2654(12-1-4)	193(11)	0	163(6)	0	0	-35(12-1-3)
1029	1146	2657(12-1-4)	193(11)	0	-164(6)	0	0	-35(12-1-3)
1030	1147	2660(12-1-4)	193(11)	0	165(6)	0	0	-35(12-1-3)

	322	-1397(7)	-25(13-1-3)	189(6)	0	0	0	17(7)
1031	323	-352(7)	-26(13-1-3)	-195(6)	0	0	0	-19(13-1-3)
	321	-352(7)	-26(13-1-3)	197(6)	0	0	0	33(9)
1032	309	2703(6)	-23(8)	-102(6)	0	0	0	-5(13-11-3)
	310	2703(6)	-23(8)	112(6)	0	0	0	33(8)
1033	103	1208(3)	133(9)	-105(6)	0	0	0	76(9)
	104	1208(3)	133(9)	91(6)	0	0	0	58(12-1-4)
1034	122	-857(7)	-208(6)	-233(6)	0	0	0	-37(10)
	120	-857(7)	258(6)	233(6)	0	0	0	-67(6)
1035	121	722(12-11-3)	-194(6)	-225(6)	0	0	0	-41(12-1-3)
	119	723(12-11-3)	256(6)	225(6)	0	0	0	-70(6)
1036	234	-147(7)	-185(6)	-213(6)	0	0	0	-45(13-1-4)
	229	-147(7)	240(6)	213(6)	0	0	0	-65(6)
1037	233	-517(11)	-186(6)	-199(6)	0	0	0	-48(13-1-4)
	228	-517(11)	211(6)	199(6)	0	0	0	-53(13-1-4)
1038	232	-269(7)	-185(6)	-184(6)	0	0	0	-49(13-1-3)
	227	-270(7)	182(6)	184(6)	0	0	0	-53(13-11-3)
1039	231	-1162(7)	-176(6)	-168(6)	0	0	0	-59(13-1-3)
	226	-1162(7)	160(6)	168(6)	0	0	0	-63(13-11-3)
1040	230	-397(7)	-164(6)	-154(6)	0	0	0	-67(13-1-3)
	225	-397(7)	145(6)	155(6)	0	0	0	-70(13-11-3)
1041	322	-2224(13-1-3)	-21(13-1-3)	-205(6)	0	0	0	19(8)
	320	-2224(13-1-3)	-21(13-1-3)	206(6)	0	0	0	19(7)
1042	321	-228(7)	-27(7)	-205(6)	0	0	0	-19(13-1-3)
	319	-228(7)	204(6)	204(6)	0	0	0	35(9)
1043	310	3859(13-11-3)	-28(8)	-104(6)	0	0	0	-10(13-11-3)
	311	3859(13-11-3)	-28(8)	112(6)	0	0	0	37(8)
1044	104	1128(12-1-2)	54(8)	-177(6)	0	0	0	57(8)
	105	1128(12-1-2)	54(8)	164(6)	0	0	0	-24(8)
1046	119	749(12-11-3)	-108(10)	-149(6)	0	0	0	37(9)
	125	749(12-11-3)	199(6)	153(6)	0	0	0	-43(8)
1047	229	63(12-1-3)	-109(6)	-149(6)	0	0	0	25(9)
	244	63(12-1-3)	194(6)	153(6)	0	0	0	-40(6)
1048	228	-420(12-11-2)	-133(6)	-148(6)	0	0	0	-18(12-1-3)
	243	-420(12-11-2)	167(6)	152(6)	0	0	0	-31(10)
1049	227	-185(9)	-153(6)	-145(6)	0	0	0	-25(6)
	242	-183(9)	140(6)	148(6)	0	0	0	-30(10)
1050	226	-71(7)	-161(6)	-139(6)	0	0	0	-34(8)
	241	-71(7)	121(6)	142(6)	0	0	0	30(9)
1051	225	-252(7)	-153(6)	-135(6)	0	0	0	-33(6)
	240	-252(7)	119(6)	137(6)	0	0	0	28(9)
1052	320	1482(13-1-3)	-24(13-1-3)	-188(6)	0	0	0	26(9)
	326	1482(13-1-3)	-24(13-1-3)	191(6)	0	0	0	16(13-11-3)
1053	319	-106(11)	-188(8)	-196(6)	0	0	0	-13(13-11-3)
	325	-106(11)	-188(8)	199(6)	0	0	0	30(8)
1054	311	2416(13-11-4)	-32(13-11-3)	-104(6)	0	0	0	-24(13-11-3)
	312	2416(13-11-4)	-32(13-11-3)	112(6)	0	0	0	37(8)
1055	105	990(12-1-3)	202(9)	-106(6)	0	0	0	109(9)
	106	990(12-1-3)	202(9)	97(6)	0	0	0	-72(9)
1056	120	-272(11)	-110(10)	-145(6)	0	0	0	43(9)
	126	-272(11)	197(8)	148(6)	0	0	0	-44(9)
1057	244	-2(13-1-3)	-5(13-1-2)	-8(12-1-2)	0	0	0	-2(13-1-2)
	245	2(13-1-3)	-1(13-1-2)	4(12-1-2)	0	0	0	0
1058	125	2(13-1-4)	-6(13-1-4)	-8(12-1-4)	0	0	0	-3(13-1-4)
	128	2(13-1-4)	-2(13-1-4)	-4(12-1-4)	0	0	0	0
1059	243	-2(13-1-3)	-5(13-1-2)	-7(12-1-2)	0	0	0	-2(13-1-2)
	246	2(13-1-3)	-1(13-1-2)	-4(12-1-2)	0	0	0	0
1060	242	-2(13-1-3)	-5(13-1-2)	-7(12-1-2)	0	0	0	-2(13-1-2)
	247	-2(13-1-3)	-1(13-1-2)	-4(12-1-2)	0	0	0	0
1061	241	2(13-1-3)	-5(12-1-3)	-7(12-1-3)	0	0	0	-2(12-1-3)
	248	-2(13-1-3)	1(12-1-3)	3(12-1-3)	0	0	0	0
1062	240	2(13-1-3)	-6(12-1-3)	-6(12-1-3)	0	0	0	-2(12-1-3)
	249	-2(13-1-3)	2(12-1-3)	2(12-1-3)	0	0	0	0
1063	326	2(13-1-3)	2(12-11-3)	-7(6)	0	3(2)	0	-2(12-1-3)
	327	2(13-1-3)	2(12-11-3)	0	0	0	0	0
1064	325	2(13-1-3)	-7(6)	-7(6)	0	0	0	2(12-11-3)
	328	2(13-1-3)	2(12-11-3)	0	0	0	0	0

1065	312	2(13-13)	-3(12-13)	-7(7)	0	3(7)	-2(12-13)
1066	313	-2(13-13)	-3(12-13)	0	0	0	0
1066	106	-1(13-13)	-3(13-13)	9(1)	0	-4(1)	-3(13-13)
1067	114	1(13-13)	-3(13-13)	0	0	0	0
1067	126	-2(13-13)	-6(13-13)	-7(12-13)	0	3(12-13)	-3(13-13)
1067	127	-2(13-13)	2(13-13)	-3(12-13)	0	0	0
2001	17	162(8)	-2(18)	-5(7)	0	0	4(9)
2001	19	162(8)	-2(18)	5(1)	0	0	22(8)
2002	19	210(8)	11(13-13)	-5(2)	0	0	21(8)
2002	20	210(8)	11(13-13)	5(5)	0	0	16(9)
2003	20	188(8)	-7(13-13)	-5(1)	0	0	17(9)
2003	15	188(8)	-7(13-13)	5(8)	0	0	22(8)
2004	15	108(8)	-5(12-14)	-8(9)	0	0	17(8)
2004	16	108(8)	-5(12-14)	8(1)	0	0	18(9)
2005	16	134(8)	14(13-13)	-5(1)	0	0	22(9)
2005	18	134(8)	14(13-13)	5(8)	0	0	14(8)
2006	25	-128(7)	-38(13-14)	-5(5)	0	0	-10(13-14)
2006	26	-128(7)	-38(13-14)	5(7)	0	0	24(13-14)
2007	26	-280(13-14)	-14(13-13)	-4(1)	0	0	7(13-12)
2007	23	-280(13-14)	-14(13-13)	4(7)	0	0	7(13-13)
2008	23	64(6)	-2(12-13)	-5(1)	0	0	9(7)
2008	24	64(6)	-2(12-13)	5(7)	0	0	13(12-13)
2009	24	-122(11)	8(12-13)	-9(1)	0	0	10(12-13)
2009	21	-122(11)	8(12-13)	9(2)	0	0	-4(12-13)
2010	21	-118(13-13)	27(7)	-5(4)	0	0	16(7)
2010	22	-118(13-13)	27(7)	5(6)	0	0	-9(9)
8000	117	-280(9)(3-14)	175(7)	2446(12-13)	0	-363(9)	564(8)
8000	118	-2950(13-14)	175(7)	2554(12-13)	-11(7)	2685(12-13)	-545(11)
8000	118	4100(13-13)	-398(11)	-130(12-13)	-34(11)	2684(12-13)	-718(11)
8000	101	3957(13-13)	-398(11)	1208(8)	-34(11)	-739(13-12)	-105(13-13)
8000	220	-1447(13-12)	-370(11)	-486(13-14)	-15(11)	-1917(8)	-736(11)
8000	221	-1509(13-12)	-370(11)	-370(13-14)	-15(11)	-2184(8)	-283(11)
8000	221	-5635(13-13)	654(11)	418(13-14)	31(7)	-218(8)	-251(11)
8000	222	-5720(13-13)	654(11)	533(13-14)	31(7)	-185(9)	-1130(11)
8000	222	-5479(13-13)	-399(11)	-316(13-12)	10(8)	-1866(8)	-1156(11)
8000	223	-5585(13-13)	-399(11)	234(13-12)	10(8)	-2020(8)	-566(11)
8000	223	-7167(13-13)	-194(8)	-229(13-12)	31(11)	-2029(8)	-551(11)
8000	224	-7287(13-13)	-194(8)	287(13-12)	31(11)	-1895(8)	-740(11)
8000	224	-6369(13-13)	258(12-14)	-1303(7)	7(12-11)	-1883(8)	-732(11)
8000	307	-6502(13-13)	258(12-14)	-1139(7)	7(12-11)	-3751(9)	554(8)
8000	317	2242(13-12)	227(11)	-1556(9)	18(7)	593(12-14)	-71(7)
8000	317	-1283(12-11)	-315(11)	-1372(9)	18(7)	-2027(9)	-333(11)
8000	318	-1289(12-11)	-315(11)	-420(6)	-22(13-13)	-2039(8)	-33(11)
8000	318	2235(13-12)	652(11)	184(6)	-20(13-13)	-2176(8)	163(13-13)
8000	220	2198(13-12)	652(11)	439(6)	-20(13-13)	-1864(9)	-735(11)
8001	115	-3538(10)	365(7)	811(8)	-14(9)	-239(8)	453(9)
8001	116	-3998(6)	365(7)	1159(3)	-14(9)	799(12-12)	-494(11)
8001	116	-4284(6)	-328(11)	1337(3)	-16(8)	798(12-12)	-510(11)
8001	102	-4751(6)	-328(11)	1675(3)	-16(8)	2575(3)	-176(13-14)
8001	215	-3301(2)	183(7)	-975(13-13)	-12(11)	-2156(8)	223(7)
8001	216	-3511(3)	183(7)	-807(13-13)	-12(11)	-2663(8)	-175(13-12)
8001	216	-4270(6)	-289(13-13)	-749(13-13)	19(8)	-2664(8)	-242(13-13)
8001	217	-4570(6)	-289(13-13)	-584(13-13)	19(8)	-3152(8)	148(13-13)
8001	217	-4780(6)	133(12-13)	-466(13-13)	10(8)	-3152(8)	204(9)
8001	218	-5148(6)	133(12-13)	-305(13-13)	10(8)	-3418(8)	-92(13-13)
8001	218	4412(13-14)	117(13-13)	-227(13-12)	7(7)	-3418(8)	-113(12-13)
8001	219	-4581(13-14)	117(13-13)	288(8)	7(7)	-3223(8)	-210(13-13)
8001	219	-4756(6)	-236(12-13)	371(9)	8(13-13)	-3225(8)	-156(13-13)
8001	115	-5205(6)	-236(12-13)	657(3)	8(13-13)	-2390(8)	481(8)
8001	308	-2363(7)	-25(12-13)	-2258(13-13)	16(13-13)	3027(13-12)	-30(13-13)
8001	315	-2281(7)	-25(12-13)	-2079(13-13)	16(13-13)	1917(12-12)	32(13-12)
8001	315	-2571(13-13)	-162(13-13)	-1616(13-13)	-23(13-13)	1917(12-12)	31(9)
8001	316	-2579(13-13)	-162(13-13)	-1441(13-13)	-23(13-13)	1797(13-13)	171(13-13)
8001	316	-3232(2)	-150(13-13)	-889(12-12)	-26(13-13)	1797(13-13)	184(13-13)
8002	215	-3325(2)	-150(13-13)	-717(12-12)	-26(13-13)	-2155(8)	124(7)
8002	123	-4212(6)	328(7)	1015(3)	-15(9)	-2160(8)	38(112-13)

8002	124	-467(6)	328(7)	1370(6)	-15(9)	1288(12-13)	-477(11)
8002	124	-4980(6)	-289(11)	1540(6)	-14(8)	1288(12-13)	-474(11)
8002	103	-5443(6)	-289(11)	1833(6)	-14(8)	3466(3)	-185(12-14)
8002	235	-2224(6)	100(7)	-1094(6)	9(8)	-2706(9)	159(7)
8002	236	-2449(6)	100(7)	-864(12-13)	9(8)	-3548(8)	-164(13-13)
8002	236	-2515(6)	-259(13-11-3)	-835(12-13)	16(8)	-3548(8)	-256(13-13)
8002	237	-2816(6)	-259(13-11-3)	-669(12-11-3)	16(8)	-4014(8)	-98(13-13)
8002	237	-3015(6)	135(12-13)	-566(12-11-3)	11(8)	-4013(8)	172(12-13)
8002	238	-3384(6)	135(12-13)	463(12-13)	11(8)	-4016(8)	-80(11)
8002	238	-3658(6)	-266(13-11-3)	270(12-13)	10(9)	-4016(8)	-101(12-13)
8002	239	-4069(6)	-266(13-11-3)	548(8)	10(9)	-3409(8)	-363(13-13)
8002	239	-4388(6)	-311(12-11-3)	577(8)	12(13-13)	-3408(8)	308(8)
8002	123	-4836(6)	-311(12-11-3)	934(3)	12(13-13)	-2159(8)	488(12-11-3)
8002	309	-1880(6)	-24(13-11-2)	-1815(6)	16(13-13)	3610(12-11-3)	32(8)
8002	323	-1749(6)	-24(13-11-2)	-1360(6)	16(13-13)	2788(12-11-3)	44(13-11-3)
8002	323	-1246(3)	-154(13-13)	-1460(6)	-26(13-13)	2788(12-11-3)	37(9)
8002	324	-1266(3)	-154(13-13)	-1017(6)	-26(13-13)	2012(12-11-3)	174(13-13)
8002	324	-2166(6)	142(13-13)	-1449(6)	-31(13-13)	2012(12-11-3)	212(13-13)
8002	235	-2302(6)	142(13-13)	-1018(6)	-31(13-13)	-2706(9)	67(12-13)
8003	121	-4710(6)	377(7)	1212(3)	-16(8)	-2313(8)	482(8)
8003	122	-5245(6)	377(7)	1615(6)	-16(8)	1784(12-13)	-473(11)
8003	122	-5722(6)	-307(11)	1844(6)	-16(8)	1784(12-13)	-467(11)
8003	104	-6266(6)	-307(11)	2247(6)	-16(8)	4291(3)	187(9)
8003	230	-2185(6)	-55(12-11-3)	-1305(12-11-3)	12(8)	-2908(9)	-139(13-11-4)
8003	231	-2423(6)	-55(12-11-3)	-1128(12-11-3)	12(8)	-3832(8)	-135(13-11-3)
8003	231	-2506(6)	212(13-13)	-1072(12-11-3)	15(8)	-3832(8)	-217(13-11-3)
8003	232	-2829(6)	212(13-13)	-897(12-11-3)	15(8)	-4413(8)	-102(12-11-3)
8003	232	-3068(6)	88(12-13)	-736(12-11-3)	15(8)	-4413(8)	-158(12-11-3)
8003	233	-3470(6)	88(12-13)	616(12-13)	15(8)	-4448(8)	107(8)
8003	233	-3823(6)	165(13-13)	379(12-13)	6(8)	-4448(8)	128(8)
8003	234	-4278(6)	165(13-13)	609(3)	6(8)	-3766(8)	-272(13-13)
8003	234	-4716(6)	-290(12-11-3)	678(3)	11(12-12)	-3767(8)	-203(13-13)
8003	121	-5221(6)	-290(12-11-3)	1084(3)	11(12-12)	-2315(8)	518(8)
8003	310	-1991(6)	31(9)	-2096(6)	15(13-13)	4476(12-11-3)	39(8)
8003	321	-1859(6)	31(9)	-1634(6)	15(13-13)	3609(12-11-3)	-43(13-13)
8003	321	-1262(6)	-166(13-13)	-1742(6)	-26(13-13)	3609(12-11-3)	35(9)
8003	322	-1283(6)	-166(13-13)	-1286(6)	-26(13-13)	2678(12-11-3)	181(13-13)
8003	322	-2141(6)	154(13-13)	-1697(6)	-30(13-13)	2678(12-11-3)	212(13-13)
8003	230	-2282(6)	154(13-13)	-1248(6)	-30(13-13)	-2909(9)	-55(13-11-4)
8004	119	-4336(6)	333(7)	1309(3)	-17(9)	-2818(12-11-3)	444(9)
8004	120	-4875(6)	333(7)	1722(6)	-17(9)	2081(13-13)	-402(11)
8004	120	-5312(6)	-279(11)	1961(6)	20(11)	2082(13-13)	-415(11)
8004	105	-5860(6)	-279(11)	2366(6)	20(11)	4524(3)	211(9)
8004	225	-3059(13-11-3)	-62(12-11-3)	-13400(13-11-2)	12(8)	-3609(9)	-117(13-11-3)
8004	226	-3155(13-11-3)	-62(12-11-3)	-1162(13-11-2)	12(8)	-3999(9)	-177(13-11-3)
8004	226	-2818(6)	196(13-13)	-1252(13-11-4)	-16(13-13)	-4000(9)	-180(13-11-3)
8004	227	-3145(6)	196(13-13)	-1076(13-11-4)	-16(13-13)	-4518(8)	-134(12-11-2)
8004	227	-3401(6)	-100(12-11-3)	-973(13-11-4)	11(8)	-4517(8)	-172(12-11-2)
8004	228	-3806(6)	-100(12-11-3)	835(13-14)	11(8)	-4578(8)	115(8)
8004	228	-3168(6)	-177(13-11-3)	539(13-14)	-5(13-14)	-4578(8)	101(9)
8004	229	-3627(6)	-177(13-11-3)	711(13-14)	-5(13-14)	-3869(8)	327(8)
8004	229	-4037(6)	-263(12-11-3)	713(8)	-9(12-12)	-3869(8)	258(8)
8004	119	-4547(6)	-263(12-11-3)	1117(3)	-9(12-12)	-2818(12-11-2)	524(8)
8004	311	-1471(13-11-3)	31(8)	-2792(13-11-3)	15(13-13)	5737(12-11-2)	44(13-11-3)
8004	319	-1418(13-11-3)	31(8)	-2607(13-11-3)	15(13-13)	3983(12-11-3)	36(13-11-2)
8004	319	-1555(13-11-3)	189(13-11-3)	-2086(13-11-3)	-24(13-11-3)	3983(12-11-3)	38(8)
8004	320	-1564(13-11-3)	189(13-11-3)	-1903(13-11-3)	-24(13-11-3)	3311(13-11-3)	183(13-11-3)
8004	320	-3262(13-11-3)	161(13-13)	-1654(6)	-25(13-13)	3311(13-11-3)	188(13-11-3)
8004	225	-3319(13-11-3)	161(13-11-3)	-1235(12-11-3)	-25(13-13)	-3608(9)	-59(6)
8005	125	-2340(6)	165(12-11-3)	1209(2)	-16(8)	-2108(12-11-3)	400(8)
8005	126	-2625(6)	165(12-11-3)	1390(3)	-16(8)	-2364(13-11-3)	285(8)
8005	126	-2866(6)	-196(13-14)	1467(3)	13(13-13)	4028(13-11-3)	-251(11)
8005	106	-3151(6)	-196(13-14)	1674(3)	13(13-13)	4028(13-11-3)	159(9)
8005	240	1069(6)	-100(13-13)	-1782(12-11-3)	14(8)	-3404(8)	-87(6)
8005	241	1205(6)	-100(13-13)	-1664(12-11-3)	14(8)	-4514(8)	75(13-13)
8005	241	2627(13-13)	-125(13-11-3)	-1064(12-11-3)	-17(13-13)	-4514(8)	100(9)
8005	242	2542(13-13)	-125(13-11-3)	-949(12-11-3)	-17(13-13)	-4823(8)	87(12-12)

8005	242	2399(13-1-3)	-111(8)	-475(12-1-3)	15(8)	-482(3-8)	-102(12-11-2)
8005	243	2293(13-1-3)	-111(8)	572(12-1-3)	15(8)	-4479(8)	175(8)
8005	244	-2815(13-1-3)	-139(13-11-3)	641(13-1-3)	-6(12-1-3)	-4479(8)	163(8)
8005	244	-2935(13-1-3)	-139(13-11-3)	765(2)	-6(12-1-3)	-349(18)	297(8)
8005	244	-2893(13-1-3)	-204(12-11-3)	930(7)	-9(12-1-2)	-3492(8)	263(8)
8005	125	-3025(13-1-3)	-204(12-11-3)	1106(2)	-9(12-1-2)	-2107(12-1-3)	442(8)
8005	312	-1986(12-1-4)	-19(13-11-2)	-267(66)	-14(13-1-3)	7191(12-11-3)	37(8)
325	312	-1950(12-1-4)	-19(13-11-2)	-2403(6)	-14(13-1-3)	5258(12-11-3)	38(13-1-2)
8005	325	-1185(12-1-4)	-186(13-1-3)	-2469(6)	-24(13-1-3)	5258(12-11-3)	47(8)
8005	326	-1191(12-1-4)	-186(13-1-3)	-2202(6)	-24(13-1-3)	3058(12-11-3)	179(13-1-3)
8005	326	1070(6)	193(13-1-3)	-2206(12-11-2)	-19(13-1-3)	3058(12-11-3)	170(13-1-3)
8006	240	989(6)	193(13-1-3)	-2086(12-11-2)	-19(13-1-3)	-3404(8)	-80(6)
8006	1002	471(2)	957(12-1-3)	3188(7)	-43(7)	-3653(7)	272(12-11-4)
8006	1001	441(2)	1272(9)	3188(7)	-43(7)	0	-1359(12-1-4)
8006	1003	766(7)	-392(12-11-1)	2687(7)	28(7)	-6700(7)	277(12-1-1)
8006	1004	3943(7)	-90(8)	2038(7)	28(7)	-362(17)	261(12-1-4)
8006	1003	3913(7)	445(7)	2038(7)	26(7)	-8723(11)	288(3)
8006	1005	4041(7)	-428(8)	1215(11)	22(7)	-10107(11)	-108(11)
8006	1004	4010(7)	81(11)	1215(11)	22(7)	-8716(11)	261(3)
8006	1006	4854(7)	39(11)	283(7)	27(7)	-10342(11)	237(6)
8006	1005	4824(7)	458(7)	283(7)	27(7)	-10021(11)	-168(7)
8006	1007	4885(7)	-370(1)	-742(7)	-13(13-11-1)	-9501(11)	98(13-11-1)
8006	1006	4855(7)	184(7)	-742(7)	-13(13-11-1)	-10342(11)	227(6)
8006	1008	4496(7)	-239(13-11-1)	-1821(11)	-18(13-11-1)	-7430(11)	212(7)
8006	1007	4466(7)	353(13-1-1)	-1821(11)	-18(13-11-1)	-9516(11)	178(13-11-1)
8006	1009	4468(7)	-604(6)	-287(7)	-21(6)	-4150(11)	-365(12-1-3)
8006	1008	4438(7)	-210(13-11-1)	-287(7)	-21(6)	-7437(11)	253(7)
8006	1010	-3667(12-1-4)	-2152(13-11-1)	-3793(7)	77(13-11-1)	0	-2584(13-11-1)
	1009	-3690(12-1-4)	-1858(13-11-1)	-3793(7)	77(13-11-1)	-4346(7)	-306(12-11-3)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Pilastri

Scenario di calcolo : Set NT SLV_A2 STR/GEO									
Asta	N.in.	N.fin.	N	ky	Tz	My	Mz		
			kg	kg	kg	kg	kg	kg	kg
1	1	1	-10351(12-1-2)	-697(12-1-2)	1248(6)	-3(13-1-3)	-2473(8)	-1464(12-1-2)	628(8)
	17	17	-10187(12-1-2)	-697(12-1-2)	333(6)	-3(13-1-3)	-1286(9)	628(8)	
1	17	5936(12-1-2)	276(12-1-2)	347(6)	-5(8)	-1287(9)	636(8)		
25	25	6018(12-1-2)	276(12-1-2)	311(12-1-2)	311(12-1-2)	-5(8)	-1063(9)	363(9)	
1	25	-3354(8)	230(8)	309(12-1-1)	10(13-11-4)	-1064(9)	359(9)		
101	101	-3248(8)	230(8)	-667(10)	10(13-11-4)	739(13-1-2)	-86(13-11-3)		
2	2	-13155(12-1-2)	-712(12-1-2)	-1108(11)	-3(2)	1800(11)	-1499(12-1-2)		
19	19	-12992(12-1-2)	-712(12-1-2)	-699(13-1-2)	-3(2)	-1344(9)	626(8)		
2	19	-8772(12-1-2)	-285(12-1-2)	-676(13-1-2)	-3(13-1-4)	-1344(9)	628(8)		
26	26	-8691(12-1-2)	-285(12-1-2)	-800(10)	-3(13-1-4)	-1807(2)	366(8)		
2	26	-4795(6)	167(8)	-853(10)	-7(9)	-1808(2)	355(8)		
102	102	-4689(6)	167(8)	-1310(10)	-7(9)	-2572(3)	224(7)		
3	3	-12601(12-1-2)	-744(12-1-2)	-1274(11)	-2(12-1-3)	2321(11)	-1556(12-1-2)		
20	20	-12437(12-1-2)	-744(12-1-2)	-848(2)	-2(12-1-3)	-1223(9)	640(8)		
3	20	-8062(12-1-2)	338(12-1-2)	-824(2)	-4(12-1-3)	-1223(9)	639(8)		
23	23	-7980(12-1-2)	338(12-1-2)	-1052(6)	-4(12-1-3)	-2088(2)	351(9)		
3	23	-5888(6)	-194(10)	-1015(6)	-6(9)	-2088(2)	358(9)		
103	103	-5782(6)	-194(10)	-1472(6)	-6(9)	-3442(3)	389(6)		
4	4	-14032(12-1-2)	-680(12-1-2)	-1438(7)	-2(13-1-3)	3322(12-1-3)	-1417(12-1-2)		
15	15	-13868(12-1-2)	-680(12-1-2)	-1068(2)	-2(13-1-3)	-1282(9)	648(8)		
4	15	-9651(12-1-2)	-297(12-1-2)	-1066(2)	-3(12-1-3)	-1282(9)	642(8)		
24	24	-9569(12-1-2)	-297(12-1-2)	-1267(6)	-3(12-1-3)	-2495(2)	352(8)		
4	24	-6576(6)	133(8)	-1269(6)	-7(9)	-2495(2)	348(8)		
104	104	-6469(6)	133(8)	-1726(6)	-7(9)	-4289(3)	194(7)		
5	5	-11485(12-1-2)	-646(12-1-2)	-1647(7)	-2(13-1-3)	3501(13-1-2)	-1367(12-1-2)		
16	16	-11322(12-1-2)	-646(12-1-2)	-1214(2)	-2(13-1-3)	-1541(12-1-3)	627(8)		
5	16	-8111(13-1-3)	-263(12-1-2)	-1217(2)	-3(13-1-3)	-1541(12-1-3)	627(8)		
21	21	-8030(13-1-3)	-263(12-1-2)	-1316(6)	-3(13-1-3)	-2642(2)	367(8)		
5	21	-7068(6)	128(8)	-1325(6)	-9(9)	-2642(2)	367(8)		
105	105	-6902(6)	128(8)	-1782(6)	-9(9)	-4519(3)	226(9)		
6	6	-13075(12-1-2)	-630(12-1-2)	-1772(7)	2(13-11-3)	4380(13-1-3)	-1338(12-1-2)		

6	18	-12911(12-1-2)	-630(12-1-2)	-1595(13-1-3)	2(13-11-3)	-1542(12-1-3)	622(8)
18	18	-9099(12-1-2)	-280(12-1-2)	-1526(13-1-3)	2(13-11-3)	-1542(12-1-3)	614(8)
22	22	-892(12-1-2)	-280(12-1-2)	-1526(13-1-3)	2(13-11-3)	-2711(7)	347(8)
6	22	-5154(7)	-291(13-1-3)	-1464(13-1-3)	-9(9)	-2711(7)	
106	106	-5048(7)	-291(13-1-3)	-1464(13-1-3)	-9(9)	-4008(13-1-3)	427(7)
7	7	-11429(12-1-3)	2758(11)	-622(12-1-2)	14(3)	1565(12-1-2)	4915(11)
1001	1001	-1102(12-1-3)	563(11)	-622(12-1-2)	14(3)	-1808(12-1-2)	-4086(11)
7	1001	-6031(12-1-3)	-2652(7)	-5100(12-1-2)	-62(7)	745(12-1-2)	-4166(7)
118	118	-5943(12-1-3)	-3243(7)	-5100(12-1-2)	-62(7)	138(7)	0
8	1002	-653(7)	-28(7)	-504(7)	0	-37(7)	0
117	117	-611(7)	-28(7)	504(11)	0	0	33(7)
9	1003	-2611(12-1-3)	-18(7)	-689(7)	0	-29(7)	0
1111	1111	-2579(12-1-3)	-18(7)	327(11)	0	-460(7)	16(7)
9	1111	-2551(12-1-3)	33(9)	312(7)	1(11)	-461(7)	15(7)
224	224	-2539(12-1-3)	33(9)	686(7)	1(11)	0	-17(9)
10	1004	111(13-1-1)	-38(7)	-834(7)	-1(7)	0	-45(7)
1112	1112	143(13-11-1)	-38(7)	188(11)	-1(7)	-822(7)	51(7)
10	1112	-411(12-1-2)	-68(7)	118(7)	2(11)	-786(7)	-71(7)
223	223	-389(12-1-2)	-68(7)	806(7)	2(11)	0	45(7)
1005	1005	844(12-1-4)	-6(8)	-949(7)	-1(7)	0	-15(7)
1113	1113	876(12-1-4)	-6(8)	66(11)	-1(7)	-1109(7)	-6(11)
11	1113	887(12-1-4)	-8(11)	21(13-1-4)	0	-1112(7)	-6(11)
222	222	917(12-1-4)	-8(11)	949(7)	0	0	13(11)
1006	1006	145(7)	-16(13-11-4)	-1027(7)	-2(7)	0	-13(13-11-4)
1114	1114	187(7)	-16(13-11-4)	-40(13-1-4)	-2(7)	-1301(7)	28(13-11-4)
12	1114	-445(7)	-9(13-11-4)	-136(11)	0	-1179(7)	-20(13-11-4)
221	221	-399(7)	-9(13-11-4)	985(7)	0	0	15(11)
13	1007	696(12-1-4)	7(11)	-1067(7)	-1(7)	0	-6(12-1-3)
1115	1115	728(12-1-4)	7(11)	-58(7)	-1(7)	-1401(7)	-16(11)
13	1115	738(12-1-4)	-12(11)	-121(11)	0	-1405(7)	-15(11)
220	220	776(12-1-4)	-12(11)	1073(7)	0	0	19(11)
14	1008	196(7)	51(11)	-1052(7)	0	0	42(11)
1116	1116	238(7)	51(11)	-43(7)	0	-1363(7)	-85(11)
14	1116	-1041(7)	18(11)	-153(11)	-1(7)	-1271(7)	41(11)
318	318	-992(7)	18(11)	1025(7)	-1(7)	0	-17(13-1-4)
157	1009	612(8)	17(7)	-894(7)	0	0	23(7)
157	1117	653(8)	17(7)	-137(11)	0	-969(7)	-21(11)
317	317	707(8)	-16(11)	903(7)	-2(11)	0	20(11)
207	207	-10658(13-11-3)	4046(7)	6145(13-11-1)	387(12-11-4)	3709(13-1-2)	2770(7)
1010	1010	-10628(13-11-3)	4046(7)	6145(13-11-1)	387(12-11-4)	1616(7)	1183(13-1-3)
207	1118	-5398(13-1-3)	197(13-1-3)	1438(12-1-3)	-45(11)	2804(13-1-1)	342(13-1-3)
307	307	-5285(13-1-3)	197(13-1-3)	1438(12-1-3)	-45(11)	593(12-1-4)	-42(7)
208	208	-5226(13-1-3)	259(7)	1257(6)	2(12-11-3)	-2772(6)	1313(9)
308	308	-4933(13-1-3)	259(7)	1077(13-11-2)	2(12-11-3)	3024(13-11-2)	-148(12-11-3)
209	209	-3203(6)	287(9)	1807(6)	2(12-11-3)	-3999(6)	1388(9)
309	309	-2822(6)	287(9)	1444(12-11-3)	2(12-11-3)	3608(12-11-3)	110(12-11-3)
210	210	-3526(6)	292(7)	2132(6)	2(12-11-3)	-4767(6)	1386(9)
310	310	-3144(6)	292(7)	1869(12-11-3)	2(12-11-3)	4474(12-11-3)	-11(12-11-3)
211	211	-6039(13-11-3)	295(7)	2397(6)	2(12-11-3)	-5917(12-11-3)	-1376(9)
311	311	-5745(13-11-3)	295(7)	2395(12-11-3)	2(12-11-3)	5735(12-11-2)	-142(12-11-2)
212	212	-7264(13-1-3)	325(7)	2992(12-11-3)	2(12-11-3)	-7375(12-11-3)	1398(7)
312	312	-6971(13-1-3)	325(7)	2992(12-11-3)	2(12-11-3)	7168(12-11-3)	-567(12-11-3)
1228	1010	-9810(13-11-3)	-309(13-11-3)	2119(13-11-1)	-700(13-11-1)	-2518(13-11-1)	1072(13-1-3)
1118	1118	-9660(13-11-3)	-309(13-11-3)	2119(13-11-1)	-700(13-11-1)	2768(13-11-1)	316(13-1-3)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi -ASTE generiche

Scenario di calcolo : Set NT SLV_A2 STR/GEO									
Asta	N.in.	N.fin.	N	Iy	Iz	My	Mz		
			kg	kg	kg	kg	kg	kg	kg
701	1001	-4325(12-1-3)	-20(2)	-5(7)	0	0	-40(3)		
117	117	-4306(12-1-3)	5(1)	0	0	0	29(7)		
702	117	4608(7)	-33(11)	-5(1)	0	0	-20(11)		
1003	1003	4590(7)	-33(11)	5(7)	0	0	62(7)		
703	1003	-2979(7)	14(12-11-1)	-5(6)	0	0	30(12-11-1)		
1112	1112	-2955(7)	14(12-11-1)	5(1)	0	0	-14(12-11-1)		

704	1112	1373(12-1-3)	-39(1)	0	-5(7)	0	0	39(11)
	1005	1359(12-1-3)	-39(1)	0	5(3)	0	0	80(7)
705	1005	-1262(11)	18(1)	0	-5(3)	0	0	38(1)
	1114	-1243(11)	18(1)	0	5(7)	0	0	19(11)
706	1114	-1770(13-II-2)	-32(1)	0	-5(6)	0	0	73(11)
	1007	-1784(13-II-2)	-32(1)	0	5(1)	0	0	51(9)
707	1007	2011(13-II-3)	15(1)	0	-5(2)	0	0	32(1)
	1116	2030(13-II-3)	15(1)	0	5(1)	0	0	34(11)
708	1116	-2612(6)	47(11)	0	-5(1)	0	0	85(11)
	1009	-2630(6)	47(11)	0	5(1)	0	0	-39(12-II-3)
709	1009	2926(7)	-18(13-II-1)	0	-5(1)	0	0	33(7)
	1118	2950(7)	-18(13-II-1)	0	5(7)	0	0	29(13-II-1)
710	1118	-4777(13-II-1)	-30(11)	0	-5(1)	0	0	-58(11)
	317	-4762(13-II-1)	-30(11)	0	5(3)	0	0	19(13-II-3)
711	317	3009(13-II-4)	55(11)	0	-5(7)	0	0	97(11)
	1116	2989(13-II-4)	55(11)	0	5(1)	0	0	-77(11)
712	1116	-3190(13-II-2)	-95(11)	0	-5(6)	0	0	-142(11)
	220	-3173(13-II-2)	-95(11)	0	5(7)	0	0	123(11)
713	220	1995(13-II-4)	44(11)	0	-5(7)	0	0	78(11)
	1114	1973(13-II-4)	44(11)	0	5(1)	0	0	-75(11)
714	1114	-2230(13-II-2)	-131(11)	0	-5(1)	0	0	-143(11)
	222	-2217(13-II-2)	-131(11)	0	5(7)	0	0	149(11)
715	222	-961(7)	31(11)	0	-5(3)	0	0	45(11)
	1112	-985(7)	31(11)	0	5(1)	0	0	-46(11)
716	1112	-1080(12-II-4)	-110(11)	0	-5(5)	0	0	-51(11)
	224	-1076(12-II-4)	-110(11)	0	5(7)	0	0	82(11)
7001	101	-2528(13-II-3)	0	0	-2(1)	0	0	1(9)
	115	-2523(13-II-3)	0	0	2(1)	0	0	1(9)
7002	115	2498(12-1-3)	0	0	-2(1)	0	0	2(8)
	223	2502(12-1-3)	0	0	2(1)	0	0	1(9)
7003	223	-1791(13-1-3)	0	0	-3(1)	0	0	2(9)
	216	-1788(13-1-3)	0	0	3(1)	0	0	1(8)
7004	216	-3199(13-II-3)	0	0	-3(1)	0	0	1(8)
	318	-3197(13-II-3)	0	0	3(1)	0	0	1(9)
7005	318	1629(6)	0	0	-3(1)	0	0	1(9)
	308	1628(6)	0	0	3(1)	0	0	1(8)
7006	308	6031(13-1-3)	0	0	-2(8)	0	0	3(8)
	207	6019(13-1-3)	0	0	2(1)	0	0	3(9)
7007	208	-6001(13-1-3)	0	0	-2(1)	0	0	3(9)
	307	-5989(13-1-3)	0	0	2(1)	0	0	3(8)
7008	307	-1849(6)	0	0	-3(8)	0	0	1(9)
	316	3374(13-II-3)	0	0	3(1)	0	0	1(8)
7009	316	3372(13-II-3)	0	0	-3(1)	0	0	1(9)
	221	3372(13-II-3)	0	0	3(1)	0	0	1(8)
7010	221	1755(13-1-3)	0	0	-3(8)	0	0	2(8)
	218	1752(13-1-3)	0	0	3(1)	0	0	3(1)
7011	218	-2479(12-1-3)	0	0	-2(1)	0	0	1(9)
	117	-2483(12-1-3)	0	0	2(1)	0	0	1(8)
7012	117	2534(13-II-3)	0	0	-2(1)	0	0	1(9)
	102	2529(13-II-3)	0	0	2(1)	0	0	1(8)
7013	17	2197(12-1-2)	0	0	0	0	0	1(9)
	2	2192(12-1-2)	0	0	0	0	0	1(8)
7014	19	-2204(12-1-2)	0	0	0	0	0	1(8)
	1	-2208(12-1-2)	0	0	0	0	0	1(9)
7015	5	-1958(12-1-2)	0	0	0	0	0	1(8)
	18	-1953(12-1-2)	0	0	0	0	0	1(8)
7016	105	1717(13-1-3)	0	0	-2(1)	0	0	1(9)
	125	1722(13-1-3)	0	0	2(2)	0	0	1(9)
7017	125	-1329(12-II-3)	0	0	-2(1)	0	0	2(9)
	228	-1325(12-II-3)	0	0	2(1)	0	0	1(8)
7018	228	966(13-II-3)	0	0	-3(1)	0	0	2(8)
	241	968(13-II-3)	0	0	3(1)	0	0	1(9)
7019	241	2126(13-1-3)	0	0	-3(1)	0	0	1(8)
	320	2127(13-1-3)	0	0	3(1)	0	0	1(9)
7020	320	-1492(6)	0	0	-3(8)	0	0	1(9)
	312	-1493(6)	0	0	3(1)	0	0	1(8)
7021	312	-6100(13-II-3)	0	0	-2(1)	0	0	3(8)

7022	211	-6112(13-II-3)	0	2(1)	0	0	2(9)
	212	-6248(13-1-3)	0	-2(8)	0	0	2(9)
7023	311	-6236(13-1-3)	0	2(1)	0	0	3(8)
	311	710(13-II-3)	0	-3(8)	0	0	1(9)
7024	326	710(13-II-3)	0	3(1)	0	0	1(8)
	326	-1592(13-1-3)	0	-3(1)	0	0	1(8)
	226	-1593(13-1-3)	0	3(1)	0	0	1(9)
7025	226	956(13-1-3)	0	-3(1)	0	0	1(8)
	243	953(13-1-3)	0	3(1)	0	0	0
7026	243	1677(12-II-3)	0	-2(1)	0	0	1(8)
	119	1674(12-II-3)	0	2(1)	0	0	1(8)
7027	119	-1865(13-1-3)	0	-2(1)	0	0	1(8)
	106	-1870(13-1-3)	0	2(1)	0	0	1(8)
7028	16	-1969(12-II-2)	0	0	0	0	1(9)
	6	-1973(12-II-2)	0	0	0	0	1(8)
7029	324	-2461(13-1-3)	0	-3(2)	0	0	1(8)
	310	-2462(13-1-3)	0	3(1)	0	0	1(8)
7030	310	2262(13-1-3)	0	-3(1)	0	0	1(9)
	320	2262(13-1-3)	0	3(1)	0	0	1(8)
7031	320	-940(12-II-3)	0	-2(1)	0	0	1(9)
	311	-940(12-II-3)	0	2(8)	0	0	1(8)
7032	311	-2198(7)	0	-3(1)	0	0	1(9)
	322	-2198(7)	0	3(1)	0	0	1(8)
7033	322	2519(13-1-3)	0	-3(1)	0	0	1(9)
	309	2518(13-1-3)	0	3(1)	0	0	1(8)
7034	309	2668(13-1-3)	0	-3(1)	0	0	1(9)
	316	2668(13-1-3)	0	3(1)	0	0	1(8)
7035	324	-2976(13-II-3)	0	-3(1)	0	0	1(9)
	308	-2977(13-II-3)	0	3(1)	0	0	1(8)
7036	102	-3584(12-1-3)	0	-2(1)	0	0	1(8)
	123	-3579(12-1-3)	0	2(1)	0	0	1(9)
7037	123	-2703(12-II-3)	0	-2(8)	0	0	1(8)
	104	-2708(12-II-3)	0	2(1)	0	0	1(8)
7038	104	2732(12-II-3)	0	-3(1)	0	0	2(8)
	119	2736(12-II-3)	0	3(1)	0	0	1(9)
7039	105	-2795(12-II-3)	0	-3(1)	0	0	1(8)
	121	-2790(12-II-3)	0	3(1)	0	0	1(9)
7040	121	-2720(12-1-3)	0	-2(1)	0	0	1(8)
	103	-2724(12-1-3)	0	2(8)	0	0	1(9)
7041	103	3514(12-1-3)	0	-2(1)	0	0	1(8)
	115	3518(12-1-3)	0	2(1)	0	0	1(9)
7042	17	-3141(12-1-2)	0	0	0	0	0
	26	-3139(12-1-2)	0	0	0	0	0
7043	26	2581(12-1-2)	0	0	0	0	0
	101	2583(12-1-2)	0	0	0	0	0
7044	25	3138(12-1-2)	0	0	0	0	0
	19	3136(12-1-2)	0	0	0	0	0
7045	16	-2674(12-1-2)	0	0	0	0	0
	22	-2672(12-1-2)	0	0	0	0	0
7046	22	-2194(12-II-2)	0	0	0	0	0
	105	-2192(12-II-2)	0	0	0	0	0
7047	106	-2078(12-1-2)	0	0	0	0	0
	21	-2080(12-1-2)	0	0	0	0	0
7048	21	2635(12-1-2)	0	0	0	0	0
	18	2633(12-1-2)	0	0	0	0	0
7049	25	-2617(12-1-2)	0	0	0	0	0
	102	-2615(12-1-2)	0	0	0	0	0
7050	104	-2434(12-1-2)	0	0	0	0	0
	23	-2436(12-1-2)	0	0	0	0	0
7051	23	2889(12-1-2)	0	0	0	0	0
	15	2887(12-1-2)	0	0	0	0	0
7052	15	-2140(12-1-2)	0	0	0	0	0
	3	-2144(12-1-2)	0	0	0	0	0
7053	4	-2090(12-II-2)	0	0	0	0	0
	20	-2086(12-II-2)	0	0	0	0	0
7054	20	-2869(12-1-2)	0	0	0	0	0
	24	-2867(12-1-2)	0	0	0	0	0

7055	24	-2484(12-II-2)	0	0	0	0	0	0
	103	-2482(12-II-2)	0	0	0	0	0	0

VERIFICHE STATO LIMITE ULTIMO

Scenario di calcolo : Set NT_SIV_A2_STR/CEO								
Verifica delle travi								

Trave di Fond.: 318 [1, 7] | Pilastrate [1, 7]

Sez. R: By= 60.0 cm Bz=100.0 cm L=108.0 cm Ln=108.0 cm Terreno: **Terreno1**

Criterio : CLS Travifondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8538	733	--	--	12.06	12.06	42365	42365	(12+13)-VI-1	(12+13)-VI-4	4.96
10.8	7639	354	899	380	12.06	12.06	42365	42365	(12+13)-VI-1	(12+13)-VI-4	4.96
CAMP	5706	-249	2832	2071	12.06	12.06	42365	42365	(12+13)-VI-1	(12+13)-I-1	4.96
97.2	-595	684	4925	1138	12.06	12.06	42365	42365	(12+13)-V-1	(12+13)-I-1	9.78
FLN	-1798	1822	5071	--	12.06	12.06	42365	42365	(12+13)-V-1	(12+13)-I-1	12.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.3	95.9	0.201	19.2	95.9	0.200	42365	42365	(12+13)-VI-1	(12+13)-VI-4	Parz.	Parz.
10.8	19.3	95.9	0.201	19.2	95.9	0.200	42365	42365	(12+13)-VI-1	(12+13)-VI-4	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.2	95.9	0.200	42365	42365	(12+13)-VI-1	(12+13)-I-1	Parz.	Parz.
97.2	19.3	95.9	0.201	19.2	95.9	0.200	42365	42365	(12+13)-V-1	(12+13)-I-1	Parz.	Parz.
FLN	19.2	95.9	0.201	19.2	95.9	0.200	42365	42365	(12+13)-V-1	(12+13)-I-1	Parz.	Parz.

Verifica a taglio:cof(0) ≈2.500

Comb=(12+13)-V-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	11993	--	125983	84882	84882		0	42365	108.0	7.08
Des								42365		

Trave di Fond.: 9001 [2, 1] | Pilastrate [2, 1]

Sez. R: By= 60.0 cm Bz=100.0 cm L=89.4 cm Ln=101.4 cm Terreno: **Terreno1**

Criterio : CLS Travifondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10290	8744	--	--	12.06	12.06	42365	42365	(12+13)-I-2	(12+13)-I-3	4.12
10.1	9785	8141	505	603	12.06	12.06	42365	42365	(12+13)-I-2	(12+13)-I-3	4.12
CAMP	7742	6171	2548	2573	12.06	12.06	42365	42365	(12+13)-I-2	(12+13)-I-3	4.12
91.3	2368	5561	4751	195	12.06	12.06	42365	42365	(12+13)-III-2	7	5.95
FLN	1109	5756	5065	--	12.06	12.06	42365	42365	(12+13)-III-2	7	6.86

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)-I-2	(12+13)-I-3	Parz.	Parz.
10.1	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)-I-2	(12+13)-I-3	Parz.	Parz.
CAMP	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)-I-2	(12+13)-I-3	Parz.	Parz.
91.3	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-III-2	7	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-III-2	7	Parz.	Parz.

Verifica a taglio:cof(0) ≈2.500

Comb=(12+13)-V-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	16200	--	125983	84882	84882		0	42365	101.4	5.24

89

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
Des							42365			

Trave di Fond.: 9001 [3, 2] | Pilastrate [3, 2]

Sez. R: By= 60.0 cm Bz=100.0 cm L=89.6 cm Ln=89.6 cm Terreno: **Terreno1**

Criterio : CLS Travifondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1617	-42	5855	5109	12.06	12.06	42365	42365	(12+13)-V-2	(12+13)-V-3	5.67
9.0	2642	744	5797	5262	12.06	12.06	42365	42365	(12+13)-V-2	(12+13)-V-3	5.02
CAMP	10522	8181	1736	2014	12.06	12.06	42365	42365	(12+13)-V-2	(12+13)-V-3	3.46
80.6	11416	9191	842	1004	12.06	12.06	42365	42365	(12+13)-V-2	(12+13)-V-3	3.46
FLN	12258	10195	--	--	12.06	12.06	42365	42365	(12+13)-V-2	(12+13)-V-3	3.46

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-V-2	(12+13)-V-3	Parz.	Parz.
9.0	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-V-2	(12+13)-V-3	Parz.	Parz.
CAMP	19.4	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)-V-2	(12+13)-V-3	Parz.	Parz.
80.6	19.4	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)-V-2	(12+13)-V-3	Parz.	Parz.
FLN	19.4	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)-V-2	(12+13)-V-3	Parz.	Parz.

Verifica a taglio:cof(0) ≈2.500

Comb=(12+13)-V-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	14613	--	125983	84882	84882		0	42365	89.6	5.81
Des								42365		

Trave di Fond.: 9001 [4, 3] | Pilastrate [4, 3]

Sez. R: By= 60.0 cm Bz=100.0 cm L=89.2 cm Ln=89.2 cm Terreno: **Terreno1**

Criterio : CLS Travifondazione - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5103	2992	--	--	12.06	12.06	42365	42365	(12+13)-V-1	(12+13)-V-4	8.30
8.9	5115	2836	--	156	12.06	12.06	42365	42365	(12+13)-V-1	(12+13)-V-4	8.28
CAMP	5121	2571	--	422	12.06	12.06	42365	42365	(12+13)-V-1	(12+13)-V-4	8.27
80.3	4772	2672	328	81	12.06	12.06	42365	42365	(12+13)-V-1	(12+13)-I-4	8.31
FLN	4636	2753	432	--	12.06	12.06	42365	42365	(12+13)-V-1	(12+13)-I-4	8.36

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-V-1	(12+13)-V-4	Parz.	Parz.
8.9	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-V-1	(12+13)-V-4	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-V-1	(12+13)-V-4	Parz.	Parz.
80.3	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-V-1	(12+13)-I-4	Parz.	Parz.
FLN	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-V-1	(12+13)-I-4	Parz.	Parz.

Verifica a taglio:cof(0) ≈2.500

Comb=8

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	4248	--	125983	84882	84882		0	42365	89.2	20.0
Des								42365		

Trave di Fond.: 9001 [5, 4] | Pilastrate [5, 4]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.5 cm Ln=149.5 cm Terreno: **Terreno1**

90

Criterio : *CLS Travifondazione - Verifica a flessione - Verificato*

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	12157	11034	--	--	12.06	12.06	42365	42365	(12+13)-III-3	(12+13)-III-2	3.48
ILN	11390	9608	768	1426	12.06	12.06	42365	42365	(12+13)-III-3	(12+13)-III-2	3.48
CAMP	10417	8101	1741	2932	12.06	12.06	42365	42365	(12+13)-III-3	(12+13)-III-2	3.48
134.5	4053	1378	2430	2850	12.06	12.06	42365	42365	(12+13)-V-2	(12+13)-V-3	6.53
FLN	6483	4228	--	--	12.06	12.06	42365	42365	(12+13)-V-2	(12+13)-V-3	6.53

X	x-	d-	x-d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)-III-3	(12+13)-III-2	Parz.	Parz.
ILN	14.9	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)-III-3	(12+13)-III-2	Parz.
CAMP	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)-III-3	(12+13)-III-2	Parz.	Parz.
134.5	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-V-2	(12+13)-V-3	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-V-2	(12+13)-V-3	Parz.	Parz.

Verifica a taglio cot(0) =2,500

Comb =(12+13)-V-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg	kg	kg	cm	cmq/m	
Sin	15506	--	125983	88275	88275	0	42365	149.5	10.45	5.69
Des							42365			

Trave di Fond.: 9001 | 6, 5 | Pilastrate [6, 5]

Sez. R: By= 60.0 cm Bz=100.0 cm L=89.9 cm Ln=101.9 cm Terreno: Terreno1

Criterio : CLS Travifondazione - Verifica a flessione - Verificato

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	-565	-59	6298	4833	12.06	12.06	42365	42365	(12+13)-III-3	(12+13)-III-2	7.39
ILN	10.2	1158	1213	5710	12.06	12.06	42365	42365	(12+13)-III-3	(12+13)-III-2	6.17
CAMP	9382	8050	1272	1424	12.06	12.06	42365	42365	(12+13)-III-3	(12+13)-III-2	3.98
91.7	10071	8786	582	688	12.06	12.06	42365	42365	(12+13)-III-3	(12+13)-III-2	3.98
FLN	10654	9474	--	--	12.06	12.06	42365	42365	(12+13)-III-3	(12+13)-III-2	3.98

X	x-	d-	x-d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-III-3	(12+13)-III-2	Parz.	Parz.
ILN	10.2	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-III-3	(12+13)-III-2	Parz.
CAMP	19.3	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)-III-3	(12+13)-III-2	Parz.	Parz.
91.7	19.3	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)-III-3	(12+13)-III-2	Parz.	Parz.
FLN	19.3	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)-III-3	(12+13)-III-2	Parz.	Parz.

Verifica a taglio cot(0) =2,500

Comb =(12+13)-V-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg	kg	kg	cm	cmq/m	
Sin	17789	--	125983	84882	84882	0	42365	101.9	10.05	4.77
Des							42365			

Trave di Fond.: 9002 | 207, 208 | Pilastrate [207, 208]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.4 cm Ln=161.4 cm Terreno: Terreno1

Criterio : CLS Travifondazione - Verifica a flessione - Verificato

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	-168	832	6540	3950	12.06	12.06	42365	42365	(12+13)-IV-2	(12+13)-IV-3	6.65
ILN	16.1	2447	2376	5991	12.06	12.06	42365	42365	(12+13)-IV-2	(12+13)-IV-3	5.02
CAMP	15247	10825	2177	1873	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3	2.43
145.3	16404	11781	1020	917	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3	2.43

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X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr+	Mr-	C-	C+	CS
FLN	17424	12699	--	--	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3	2.43

X	x-	d-	x-d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-IV-2	(12+13)-IV-3	Parz.	Parz.
ILN	16.1	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-IV-2	(12+13)-IV-3	Parz.
CAMP	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
145.3	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
FLN	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.

Verifica a taglio cot(0) =2,500

Comb =(12+13)-II-2

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg	kg	kg	cm	cmq/m	
Sin	17547	--	125983	84882	84882	0	42365	161.4	10.05	4.84
Des							42365			

Trave di Fond.: 9002 | 208, 209 | Pilastrate [208, 209]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.5 cm Ln=149.5 cm Terreno: Terreno1

Criterio : CLS Travifondazione - Verifica a flessione - Verificato

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	18767	14216	--	--	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3	2.26
ILN	14.9	18230	13223	537	993	12.06	12.06	42365	(12+13)-II-2	(12+13)-II-3	2.26
CAMP	17595	12213	1172	2003	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3	2.26
134.5	9975	4048	3976	3781	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3	3.04
FLN	9136	3409	3437	3045	12.06	12.06	42365	42365	(12+13)-VI-2	(12+13)-VI-3	3.37

X	x-	d-	x-d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.5	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
ILN	14.9	19.5	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.
CAMP	19.5	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
134.5	19.4	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
FLN	19.4	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)-VI-2	(12+13)-VI-3	Parz.	Parz.

Verifica a taglio cot(0) =2,500

Comb =(12+13)-II-2

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg	kg	kg	cm	cmq/m	
Sin	8475	--	125983	84882	84882	0	42365	149.5	10.05	10.0
Des							42365			

Trave di Fond.: 9002 | 209, 210 | Pilastrate [209, 210]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.7 cm Ln=149.7 cm Terreno: Terreno1

Criterio : CLS Travifondazione - Verifica a flessione - Verificato

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg·m	kg·m	kg·m	kg·m	cmq	cmq	kg·m	kg·m			
ILN	11219	5668	--	--	12.06	12.06	42365	42365	(12+13)-II-4	(12+13)-II-1	3.78
ILN	15.0	10287	4571	933	1096	12.06	12.06	42365	(12+13)-II-4	(12+13)-II-1	3.78
CAMP	9364	3550	1856	2118	12.06	12.06	42365	42365	(12+13)-II-4	(12+13)-II-1	3.78
134.8	7552	2749	491	868	12.06	12.06	42365	42365	(12+13)-I-3	(12+13)-I-2	5.27
FLN	8042	3617	--	--	12.06	12.06	42365	42365	(12+13)-I-3	(12+13)-I-2	5.27

X	x-	d-	x-d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				

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X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
ILN	19.4	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)>IL-4	(12+13)>IL-1	Parz.	Parz.
15.0	19.4	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)>IL-4	(12+13)>IL-1	Parz.	Parz.
CAMP	19.4	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)>IL-4	(12+13)>IL-1	Parz.	Parz.
134.8	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.
FLN	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.

Verifica a taglio:cot(0) =2,500

Comb =(12+13)>IL-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
	kg	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	9534	--	125983	87910	87910	0	42365	149.7	10.41	9.22
Des							42365			

Trave di Fond.: 9002 | 210. 211 | Pilastrate [210. 211]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.0 cm Ln=149.0 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione - Verifica a flessione :Verificato

X	Mr-	Mr+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*	kg*	kg*	kg*	cmq	cmq	kg*	kg*	kg*	kg*	
ILN	6993	2703	1985	2040	12.06	12.06	42365	42365	(12+13)>I-3	(12+13)>I+2	4.72
14.9	6478	2154	3249	3463	12.06	12.06	42365	42365	(12+13)>IL-3	(12+13)>IL-2	4.36
CAMP	13731	10685	1557	2198	12.06	12.06	42365	42365	(12+13)>IL-3	(12+13)>IL-2	2.77
134.1	14547	11895	741	1188	12.06	12.06	42365	42365	(12+13)>IL-3	(12+13)>IL-2	2.77
FLN	15288	13083	--	--	12.06	12.06	42365	42365	(12+13)>IL-3	(12+13)>IL-2	2.77

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*	kg*	kg*	kg*		
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.
14.9	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.
CAMP	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.
134.1	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.
FLN	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.

Verifica a taglio:cot(0) =2,500

Comb =(12+13)>IL-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
	kg	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	8643	--	125983	84882	84882	0	42365	149.0	10.05	9.82
Des							42365			

Trave di Fond.: 9002 | 211. 212 | Pilastrate [211. 212]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.4 cm Ln=161.4 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione - Verifica a flessione :Verificato

X	Mr-	Mr+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*	kg*	kg*	kg*	cmq	cmq	kg*	kg*	kg*	kg*	
ILN	13909	11713	--	--	12.06	12.06	42365	42365	(12+13)>IL-3	(12+13)>IL-2	3.05
16.1	13119	10908	789	806	12.06	12.06	42365	42365	(12+13)>IL-3	(12+13)>IL-2	3.05
CAMP	12220	10054	1688	1660	12.06	12.06	42365	42365	(12+13)>IL-3	(12+13)>IL-2	3.05
145.2	1861	1701	4909	3801	12.06	12.06	42365	42365	(12+13)>IL-3	(12+13)>IL-2	6.26
FLN	-376	-8	5462	4193	12.06	12.06	42365	42365	(12+13)>IL-3	(12+13)>IL-2	8.33

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*	kg*	kg*	kg*		
ILN	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.
16.1	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.
CAMP	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.
145.2	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>IL-3	(12+13)>IL-2	Parz.	Parz.

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Verifica a taglio:cot(0) =2,500

Comb =(12+13)>IL-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
	kg	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	14449	--	125983	84882	84882	0	42365	161.4	10.05	5.87
Des							42365			

Verifica Stabilità aste Metalliche

Scenario di calcolo : Set_NT_SILV_A2_STR/GEO

Asta : 1 | 1 , 17 |

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq:Verificato

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*	kg*	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*			
-12117	629	-1720	211298	20492	9673	27	45	0.960	0.832	--	0.672	0.299	0.403
													0.499

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
kg	kg	kg	kg*	kg*	kg	kg*	kg*		
1	Y	12117	422	515	193231	19516	9213	(12+13)>VII-2	7.13
1	Z	12117	253	858	167375	19516	9213	(12+13)>VII-2	5.60

Asta : 1 | 17 , 25 |

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq:Verificato

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*	kg*	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*			
-4607	-870	636	211298	20492	9673	13	23	0.975	0.964	--	0.881	0.495	0.528
													0.825

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
kg	kg	kg	kg*	kg*	kg	kg*	kg*		
1	Y	4607	766	315	196194	19516	9213	8	10.3
1	Z	4607	460	525	194055	19516	9213	8	9.59

Asta : 1 | 25 , 101 |

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq:Verificato

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*	kg*	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*			
-1727	-1064	359	211298	20492	9673	13	23	0.975	0.964	--	0.851	0.401	0.511
													0.668

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
kg	kg	kg	kg*	kg*	kg	kg*	kg*		
1	Y	1727	905	144	196194	19516	9213	9	14.1
1	Z	1727	543	240	194055	19516	9213	9	15.9

Asta : 2 | 2 , 19 |

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq:Verificato

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*	kg*	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*			
-15042	-481	1603	211298	20492	9673	27	45	0.960	0.832	--	0.536	0.306	0.321
													0.510

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
kg	kg	kg	kg*	kg*	kg	kg*	kg*		
1	Y	15042	258	491	193231	19516	9213	(12+13)>VII-3	6.93
1	Z	15042	155	818	167375	19516	9213	(12+13)>VII-3	5.36

Asta : 2 | 19 , 26 |

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq:Verificato

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N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3655	-1605	501	211298	20492	9673	13	23	0.975	0.964	--	0.936	0.527	0.562
													0.879
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	3655	1502	264	196194	19516	9213				9		8.05
1	Z	3655	901	440	194055	19516	9213				9		8.86

Asia : 2 [26 , 102]

Sez. G: HE 240 A L=135,5 cm Ln1=135,5 cm Ln2=135,5 cm Crit.: Acciaio_Pressflessione γM=1,05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4422	-2572	250	211298	20492	9673	13	23	0.975	0.964	--	0.821	0.451	0.493
													0.752

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	4422	2113	113	196194	19516	9213				3		6.99
1	Z	4422	1268	188	194055	19516	9213				3		9.25

Asia : 3 [3 , 20]

Sez. G: HE 240 A L=271,0 cm Ln1=271,0 cm Ln2=271,0 cm Crit.: Acciaio_Pressflessione γM=1,05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-14775	1883	-1819	211298	20492	9673	27	45	0.960	0.832	--	0.665	0.299	0.399
													0.498

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	14775	1253	544	193231	19516	9213				(12+13)-VII-2		5.01
1	Z	14775	752	906	167375	19516	9213				(12+13)-VII-2		4.44

Asia : 3 [20 , 23]

Sez. G: HE 240 A L=135,5 cm Ln1=135,5 cm Ln2=135,5 cm Crit.: Acciaio_Pressflessione γM=1,05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5771	-1624	639	211298	20492	9673	13	23	0.975	0.964	--	0.833	0.479	0.500
													0.799

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	5771	1352	306	196194	19516	9213				8		7.58
1	Z	5771	811	510	194055	19516	9213				8		7.89

Asia : 3 [23 , 103]

Sez. G: HE 240 A L=135,5 cm Ln1=135,5 cm Ln2=135,5 cm Crit.: Acciaio_Pressflessione γM=1,05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5610	-3442	382	211298	20492	9673	13	23	0.975	0.964	--	0.828	0.498	0.497
													0.830

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	5610	2850	190	196194	19516	9213				3		5.12
1	Z	5610	1710	317	194055	19516	9213				3		6.62

Asia : 4 [4 , 15]

Sez. G: HE 240 A L=271,0 cm Ln1=271,0 cm Ln2=271,0 cm Crit.: Acciaio_Pressflessione γM=1,05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-15972	-1122	1625	211298	20492	9673	27	45	0.960	0.832	--	0.761	0.300	0.456
													0.500

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	15972	853	488	193231	19516	9213				(12+13)-VII-3		5.58
1	Z	15972	512	813	167375	19516	9213				(12+13)-VII-3		4.76

Asia : 4 [15 , 24]

Sez. G: HE 240 A L=135,5 cm Ln1=135,5 cm Ln2=135,5 cm Crit.: Acciaio_Pressflessione γM=1,05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-10775	-1672	-489	211298	20492	9673	13	23	0.975	0.964	--	0.871	0.363	0.523
													0.606

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	10775	1457	178	196194	19516	9213				(12+13)-VII-3		6.72
1	Z	10775	874	296	194055	19516	9213				(12+13)-VII-3		7.55

Asia : 4 [24 , 104]

Sez. G: HE 240 A L=135,5 cm Ln1=135,5 cm Ln2=135,5 cm Crit.: Acciaio_Pressflessione γM=1,05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6215	-4289	220	211298	20492	9673	13	23	0.975	0.964	--	0.828	0.522	0.497
													0.871

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	6215	3549	115	196194	19516	9213				3		4.42
1	Z	6215	2129	192	194055	19516	9213				3		6.18

Asia : 5 [5 , 16]

Sez. G: HE 240 A L=271,0 cm Ln1=271,0 cm Ln2=271,0 cm Crit.: Acciaio_Pressflessione γM=1,05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-8459	4119	-1054	211298	20492	9673	27	45	0.960	0.832	--	0.709	0.301	0.425
													0.502

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	8459	2920	317	193231	19516	9213				(12+13)-V-1		4.39
1	Z	8459	1752	529	167375	19516	9213				(12+13)-V-1		5.06

Asia : 5 [16 , 21]

Sez. G: HE 240 A L=135,5 cm Ln1=135,5 cm Ln2=135,5 cm Crit.: Acciaio_Pressflessione γM=1,05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-7114	-2557	384	211298	20492	9673	13	23	0.975	0.964	--	0.756	0.509	0.453
													0.848

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	7114	1932	196	196194	19516	9213				3		6.39
1	Z	7114	1159	326	194055	19516	9213				3		7.61

Asia : 5 [21 , 105]

Sez. G: HE 240 A L=135,5 cm Ln1=135,5 cm Ln2=135,5 cm Crit.: Acciaio_Pressflessione γM=1,05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6821	-4519	241	211298	20492	9673	13	23	0.975	0.964	--	0.828	0.537	0.497
													0.896

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	6821	3743	130	196194	19516	9213				3		4.16
1	Z	6821	2246	216	194055	19516	9213				3		5.76

Asia : 6 [6 , 18]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-14178	3762	1271	211298	20492	9673	27	45	0.960	0.832	--	0.588	0.295	0.353	0.492

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	14178	2213	376	19231	19516	9213	(12+13)-IV-3	4.39
	Z	14178	1328	626	167375	19516	9213	(12+13)-IV-3	4.53

Asia : 6 [18 , 22]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-10693	-2133	-461	211298	20492	9673	13	23	0.975	0.964	--	0.865	0.365	0.519	0.608

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	10693	1846	168	196194	19516	9213	(12+13)-VII-3	5.98
	Z	10693	1108	280	194055	19516	9213	(12+13)-VII-3	7.03

Asia : 6 [22 , 106]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-5154	-3937	427	211298	20492	9673	13	23	0.975	0.964	--	0.877	0.480	0.526	0.801

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5154	3453	205	196194	19516	9213	7	4.44
	Z	5154	2072	342	194055	19516	9213	7	5.89

Asia : 7 [1001 , 118]

Sez. G: HE 240 A L=146.0 cm Ln1=146.0 cm Ln2=146.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-3039	2	-4140	211298	20492	9673	15	24	0.968	0.955	--	0.601	0.353	0.361	0.588

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3039	1	1460	194812	19516	9213	11	5.74
	Z	3039	1	2433	192117	19516	9213	11	3.57

Asia : 7 [7 , 1001]

Sez. G: HE 240 A L=542.0 cm Ln1=542.0 cm Ln2=542.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-7222	1004	4901	211298	20492	9673	54	90	0.826	0.517	--	0.407	0.263	0.244	0.439

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7222	409	1291	166287	19516	9213	7	4.89
	Z	7222	245	2151	104054	19516	9213	7	3.17

Asia : 8 [1002 , 117]

Sez. G: IPE 140 L=248.7 cm Ln1=248.7 cm Ln2=248.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MyRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-653	-313	-37	45172	2431	529	43	150	0.925	0.269	--	1.005	0.259	0.603	0.432

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	653	315	10	39776	2315	504	7	5.83
	Z	653	189	16	11586	2315	504	7	5.89

Asia : 9 [1003 , 1111]

Sez. G: IPE 140 L=249.0 cm Ln1=249.0 cm Ln2=249.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MyRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz	
kg	kg*m	kg	kg	kg*m	kg*m									
-1685	-586	-29	45172	2431	529	43	151	0.924	0.269	--	1.002	0.289	0.601	0.482

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1685	587	8	39767	2315	504	7	3.20
	Z	1685	352	14	11559	2315	504	7	3.07

Asia : 9 [1111 , 224]

Sez. G: IPE 140 L=92.3 cm Ln1=92.3 cm Ln2=92.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MyRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz	
kg	kg ^m	kg ^m	kg	kg ^m	kg ^m									
-1617	-461	-14	45172	2431	529	16	56	1.000	0.815	--	0.600	0.248	0.360	0.413

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1617	277	4	43021	2315	504	7	6.09
	Z	1617	166	6	35053	2315	504	7	7.72

Asia : 10 [1004 , 1112]

Sez. G: IPE 140 L=249.0 cm Ln1=249.0 cm Ln2=249.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MyRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-7	-21	27	45172	2431	529	43	151	0.924	0.269	--	0.600	0.240	0.360	0.400

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7	13	7	39767	2315	504	(12+13)-VII-1	53.5
	Z	7	8	11	11559	2315	504	(12+13)-VII-1	39.2

Asia : 10 [1112 , 223]

Sez. G: IPE 140 L=170.0 cm Ln1=170.0 cm Ln2=170.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	k _{yz}	k _{zy}	k _{zz}	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-211	-786	-71	45172	2431	529	30	103	0.968	0.487	--	0.600	0.243	0.360	0.406

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	211	472	17	41630	2315	504	7	4.11
	Z	211	283	29	20942	2315	504	7	5.28

Asia : 11 [1005 , 1113]

Sez. G: IPE 140 L=249.0 cm Ln1=249.0 cm Ln2=249.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MyRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-4621	4	-10	45172	2431	529	43	151	0.924	0.269	--	0.603	0.283	0.362	0.471

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	621	2	3	39767	2315	504	(12+13)+I-1	45.1
1	Z	621	1	5	11559	2315	504	(12+13)+I-1	15.7

Asta : 11 [1113 , 222.1]

Sez. G: IPE 140 L=232.7 cm L_{n1}=232.7 cm L_{n2}=232.7 cm L_{n2}=232.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-555	24	-7	45172	2431	529	41	141	0.934	0.301	--	0.602	0.254	0.361

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	555	14	2	40192	2315	504	(12+13)+III-2	42.3
1	Z	555	9	3	12966	2315	504	(12+13)+III-2	19.0

Asta : 12 [1006 , 1114.1]

Sez. G: IPE 140 L=249.0 cm L_{n1}=249.0 cm L_{n2}=249.0 cm L_{n2}=249.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-19	-92	-15	45172	2431	529	43	151	0.924	0.269	--	0.600	0.389	0.360

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	19	55	6	39767	2315	504	(12+13)+VIII-1	27.7
1	Z	19	33	10	11559	2315	504	(12+13)+VIII-1	27.9

Asta : 12 [1114 , 221.1]

Sez. G: IPE 140 L=274.3 cm L_{n1}=274.3 cm L_{n2}=274.3 cm L_{n2}=274.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-445	-1199	14	45172	2431	529	48	166	0.908	0.227	--	1.003	0.306	0.602

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	445	1203	4	39055	2315	504		1.85
1	Z	445	722	7	9768	2315	504		2.69

Asta : 13 [1007 , 1115.1]

Sez. G: IPE 140 L=249.0 cm L_{n1}=249.0 cm L_{n2}=249.0 cm L_{n2}=249.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-279	-58	-6	45172	2431	529	43	151	0.924	0.269	--	0.601	0.409	0.361

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	279	55	3	39767	2315	504	(12+13)+VI-1	36.7
1	Z	279	21	4	11559	2315	504	(12+13)+VI-1	23.9

Asta : 13 [1115 , 220.1]

Sez. G: IPE 140 L=294.0 cm L_{n1}=294.0 cm L_{n2}=294.0 cm L_{n2}=294.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-245	-57	3	45172	2431	529	51	178	0.894	0.201	--	0.601	0.330	0.361

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	245	34	1	38450	2315	504	(12+13)+VI-1	42.9
1	Z	245	20	2	8639	2315	504	(12+13)+VI-1	24.4

Asta : 14 [1008 , 1116.1]

Sez. G: IPE 140 L=249.0 cm L_{n1}=249.0 cm L_{n2}=249.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-0	-96	-47	45172	2431	529	43	151	0.924	0.269	--	0.600	0.289	0.360

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	57	14	39767	2315	504	(12+13)+IV-1	19.4
1	Z	0	34	23	11559	2315	504	(12+13)+IV-1	16.8

Asta : 14 [1116 , 318.1]

Sez. G: IPE 140 L=289.7 cm L_{n1}=289.7 cm L_{n2}=289.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-1041	-1296	39	45172	2431	529	50	175	0.897	0.206	--	1.009	0.338	0.606

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	1041	1309	13	38587	2315	504		1.62
1	Z	1041	785	22	8871	2315	504		2.00

Asta : 157 [1009 , 1117.1]

Sez. G: IPE 140 L=249.0 cm L_{n1}=249.0 cm L_{n2}=249.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-115	38	-5	45172	2431	529	43	151	0.924	0.269	--	0.601	0.243	0.360

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	115	23	1	39767	2315	504	(12+13)+VI-1	66.3
1	Z	115	14	2	11559	2315	504	(12+13)+VI-1	50.4

Asta : 157 [1117 , 317.1]

Sez. G: IPE 140 L=256.3 cm L_{n1}=256.3 cm L_{n2}=256.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-83	36	-4	45172	2431	529	45	155	0.920	0.256	--	0.600	0.243	0.360

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	83	21	1	39568	2315	504	(12+13)+VI-1	74.4
1	Z	83	13	2	10996	2315	504	(12+13)+VI-1	60.2

Asta : 207 [207 , 1010.1]

Sez. G: HE 240 A L=50.0 cm L_{n1}=50.0 cm L_{n2}=50.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-1261	3545	2770	211298	20492	9673	5	8	1.000	1.000	--	0.782	0.424	0.469

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	1261	2773	1175	201236	19516	9213		3.62
1	Z	1261	1664	1958	201236	19516	9213		3.29

Asta : 207 [1118 , 307.1]

Sez. G: HE 240 A L=187.0 cm L_{n1}=187.0 cm L_{n2}=187.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
	kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m								
-4149	3499	-243	211298	20492	9673	19	31	0.942	0.919	--		0.645	0.343	0.387 0.572
Clis	Dir	N	Mvseq	NRd	MvRd	MzRd	Comb.							
		kg	kg* ^m	kg	kg* ^m	kg* ^m								SF
1	Y	4149	2256	83	189561	19516	9213					(12+13)-V14	6.82	
1	Z	4149	1354	139	184881	19516	9213					(12+13)-V14	9.35	

Asia : 208 [208 , 308]

Sez. G: HE 240 A L=486.0 cm Ln1=486.0 cm Ln2=486.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
	kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m								
-2749	-1875	1313	211298	20492	9673	48	81	0.858	0.580	--		0.999	0.384	0.600 0.640
Clis	Dir	N	Mvseq	NRd	MvRd	MzRd	Comb.							
		kg	kg* ^m	kg	kg* ^m	kg* ^m								SF
1	Y	2749	1873	504	172679	19516	9213					9	6.00	
1	Z	2749	1124	841	116709	19516	9213					9	5.80	

Asia : 209 [209 , 309]

Sez. G: HE 240 A L=486.0 cm Ln1=486.0 cm Ln2=486.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
	kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m								
-2276	-1813	1388	211298	20492	9673	48	81	0.858	0.580	--		0.601	0.368	0.361 0.613
Clis	Dir	N	Mvseq	NRd	MvRd	MzRd	Comb.							
		kg	kg* ^m	kg	kg* ^m	kg* ^m								SF
1	Y	2276	1089	511	172679	19516	9213					9	8.04	
1	Z	2276	654	851	116709	19516	9213					9	6.88	

Asia : 210 [210 , 310]

Sez. G: HE 240 A L=486.0 cm Ln1=486.0 cm Ln2=486.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
	kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m								
-2525	-1984	1386	211298	20492	9673	48	81	0.858	0.580	--		0.504	0.367	0.303 0.612
Clis	Dir	N	Mvseq	NRd	MvRd	MzRd	Comb.							
		kg	kg* ^m	kg	kg* ^m	kg* ^m								SF
1	Y	2525	1001	508	172679	19516	9213					9	8.26	
1	Z	2525	600	847	116709	19516	9213					9	6.93	

Asia : 211 [211 , 311]

Sez. G: HE 240 A L=486.0 cm Ln1=486.0 cm Ln2=486.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
	kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m								
-4503	-2134	-1327	211298	20492	9673	48	81	0.858	0.580	--		0.651	0.382	0.391 0.637
Clis	Dir	N	Mvseq	NRd	MvRd	MzRd	Comb.							
		kg	kg* ^m	kg	kg* ^m	kg* ^m								SF
1	Y	6503	1390	507	172679	19516	9213					(12+13)-H-2	6.10	
1	Z	6503	834	846	116709	19516	9213					(12+13)-H-2	5.26	

Asia : 212 [212 , 312]

Sez. G: HE 240 A L=486.0 cm Ln1=486.0 cm Ln2=486.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
	kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m								
-4624	6753	1067	211298	20492	9673	48	81	0.858	0.580	--		0.405	0.256	0.243 0.427

Clis	Dir	N	Mvseq	NRd	MvRd	MzRd	Comb.							
		kg	kg* ^m	kg	kg* ^m	kg* ^m								SF
1	Y	6274	2736	274	172679	19516	9213					(12+13)-V1L-3	4.85	
1	Z	6274	1642	456	116709	19516	9213					(12+13)-V1L-3	5.34	

Asia : 1228 [1010 , 1118]

Sez. G: HE 240 A L=249.0 cm Ln1=249.0 cm Ln2=249.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
	kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m								
-10563	2034	-1155	211298	20492	9673	25	41	0.969	0.855	--		0.402	0.440	0.241 0.733
Clis	Dir	N	Mvseq	NRd	MvRd	MzRd	Comb.							
		kg	kg* ^m	kg	kg* ^m	kg* ^m								SF
1	Y	10563	817	508	195090	19516	9213					(12+13)-H-2	6.62	
1	Z	10563	490	846	172122	19516	9213					(12+13)-H-2	5.61	

Asia : 8000 [307 , 317]

Sez. G: HE 240 A L=112.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
	kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m								
-114	-2027	-67	211298	20492	9673	11	19	0.990	0.986	--		0.677	0.547	0.406 0.911
Clis	Dir	N	Mvseq	NRd	MvRd	MzRd	Comb.							
		kg	kg* ^m	kg	kg* ^m	kg* ^m								SF
1	Y	114	1372	37	199302	19516	9213					9	13.4	
1	Z	114	823	61	198461	19516	9213					9	20.2	

Asia : 8000 [317 , 318]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	N	My	Mz	NRk	MvRk
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Asia : 8000 [221 , 222]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1702	-1872	-331	211298	20492	9673	13	22	0.976	0.965	--	1.000	0.386	0.600

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1702	1872	128	196343	19516	9213	9	8.44				
1	Z	1702	1123	213	194265	19516	9213	9	11.2				

Asia : 8000 [222 , 223]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-279	-2020	355	211298	20492	9673	15	25	0.967	0.953	--	0.969	0.567	0.582

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	279	1959	201	194571	19516	9213	8	8.09				
1	Z	279	1175	335	191780	19516	9213	8	10.2				

Asia : 8000 [223 , 224]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2256	-2031	632	211298	20492	9673	16	26	0.960	0.943	--	1.001	0.483	0.601

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2256	2033	305	193190	19516	9213	8	6.71				
1	Z	2256	1220	509	189861	19516	9213	8	7.72				

Asia : 8000 [224 , 117]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1628	-3475	628	211298	20492	9673	17	28	0.953	0.934	--	0.818	0.572	0.491

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1628	2841	359	191741	19516	9213	8	5.18				
1	Z	1628	1705	598	187860	19516	9213	8	6.21				

Asia : 8000 [117 , 118]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1400	-3229	547	211298	20492	9673	18	30	0.948	0.927	--	0.601	0.360	0.360

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1400	1940	197	190746	19516	9213	8	7.80				
1	Z	1400	1164	329	186496	19516	9213	8	9.73				

Asia : 8000 [118 , 101]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-487	2033	-249	211298	20492	9673	18	30	0.945	0.923	--	0.772	0.319	0.463

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	487	1571	79	190241	19516	9213	(12+13)-V1-1	10.9				
1	Z	487	942	152	185807	19516	9213	(12+13)-V1-1	15.3				

Asia : 8001 [308 , 315]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-714	3278	-12	211298	20492	9673	11	19	0.990	0.986	--	0.818	0.476	0.491

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	714	2681	6	199298	19516	9213	(12+13)-V11-4	7.06				
1	Z	714	1609	10	198455	19516	9213	(12+13)-V11-4	11.5				

Asia : 8001 [315 , 316]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1732	2035	140	211298	20492	9673	11	18	0.993	0.990	--	0.968	0.327	0.581

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1732	1971	46	199876	19516	9213	(12+13)-L3	8.72				
1	Z	1732	1183	76	199282	19516	9213	(12+13)-L3	12.9				

Asia : 8001 [316 , 215]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2807	-2155	52	211298	20492	9673	11	19	0.990	0.985	--	0.888	0.459	0.533

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2807	1913	24	199180	19516	9213	8	8.72				
1	Z	2807	1148	40	198287	19516	9213	8	12.9				

Asia : 8001 [215 , 216]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3025	-2663	117	211298	20492	9673	12	20	0.984	0.976	--	0.924	0.334	0.555

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	3025	2462	39	197916	19516	9213	8	6.86				
1	Z	3025	1477	65	196488	19516	9213	8	10.2				

Asia : 8001 [216 , 217]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3614	-3152	102	211298	20492	9673	13	22	0.976	0.965	--	0.939	0.495	0.564

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3614	2961	50	196340	19516	9213	8	5.70
1	Z	3614	1776	84	194260	19516	9213	8	8.42

Asta : 8001 [217 , 218]

Sez. G: HE 240 A L=147,9 cm Ln1=147,9 cm Ln2=147,9 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-4116	-3418	170	211298	20492	9673	15	25	0.967	0.953	--	0.971	0.454	0.582

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4116	3318	77	194568	19516	9213	8	5.01
1	Z	4116	1991	129	191776	19516	9213	8	7.28

Asta : 8001 [218 , 219]

Sez. G: HE 240 A L=158,5 cm Ln1=158,5 cm Ln2=158,5 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-2867	-3422	148	211298	20492	9673	16	26	0.960	0.943	--	1.002	0.518	0.601

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2867	3428	77	193188	19516	9213	8	5.03
1	Z	2867	2057	128	189857	19516	9213	8	7.44

Asta : 8001 [219 , 115]

Sez. G: HE 240 A L=169,8 cm Ln1=169,8 cm Ln2=169,8 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-3508	-3225	481	211298	20492	9673	17	28	0.953	0.934	--	0.899	0.428	0.539

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3508	2898	206	191738	19516	9213	8	5.29
1	Z	3508	1739	344	187857	19516	9213	8	6.89

Asta : 8001 [115 , 116]

Sez. G: HE 240 A L=177,6 cm Ln1=177,6 cm Ln2=177,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-2496	-2391	453	211298	20492	9673	18	30	0.948	0.927	--	0.714	0.522	0.429

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2496	1708	236	190743	19516	9213	8	7.92
1	Z	2496	1025	394	186493	19516	9213	8	9.21

Asta : 8001 [116 , 102]

Sez. G: HE 240 A L=181,6 cm Ln1=181,6 cm Ln2=181,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-4751	2510	211	211298	20492	9673	18	30	0.945	0.923	--	0.572	0.354	0.343

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4751	1436	75	190239	19516	9213	6	9.38
1	Z	4751	861	125	185804	19516	9213	6	12.0

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Asta : 8002 [309 , 323]

Sez. G: HE 240 A L=12,4 cm Ln1=112,4 cm Ln2=112,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-1377	3949	-5	211298	20492	9673	11	19	0.990	0.986	--	0.922	0.394	0.657

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1377	3641	2	199297	19516	9213	(12+13)-V-4	5.16
1	Z	1377	2185	3	198454	19516	9213	(12+13)-V-4	8.39

Asta : 8002 [323 , 324]

Sez. G: HE 240 A L=108,1 cm Ln1=108,1 cm Ln2=108,1 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-989	3177	25	211298	20492	9673	11	18	0.993	0.990	--	0.904	0.240	0.542

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	989	2871	6	199876	19516	9213	(12+13)-V-4	6.55
1	Z	989	1723	10	199282	19516	9213	(12+13)-V-4	10.6

Asta : 8002 [324 , 235]

Sez. G: HE 240 A L=113,2 cm Ln1=113,2 cm Ln2=113,2 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-1264	-2706	103	211298	20492	9673	11	19	0.990	0.985	--	0.882	0.484	0.529

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1264	2387	50	199180	19516	9213	9	7.46
1	Z	1264	1432	83	198287	19516	9213	9	11.3

Asta : 8002 [235 , 236]

Sez. G: HE 240 A L=22,6 cm Ln1=22,6 cm Ln2=122,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-1891	-3548	80	211298	20492	9673	12	20	0.983	0.976	--	0.903	0.422	0.542

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1891	3202	34	197915	19516	9213	8	5.64
1	Z	1891	1921	56	196487	19516	9213	8	8.76

Asta : 8002 [236 , 237]

Sez. G: HE 240 A L=134,4 cm Ln1=134,4 cm Ln2=134,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-2209	-4014	88	211298	20492	9673	13	22	0.976	0.965	--	0.954	0.520	0.573

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2209	3830	46	196339	19516	9213	8	4.71
1	Z	2209	2298	76	194259	19516	9213	8	7.28

Asta : 8002 [237 , 238]

Sez. G: HE 240 A L=147,9 cm Ln1=147,9 cm Ln2=147,9 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$

kg/cm² ft=4300 kg/cm²;**Verificato**

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N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m	kg	kg	kg
-2688	-4081	120	211298	20492	9673	15	25	0.967	0.953	--	1.000	0.394	0.600
Cls	Dir	N	Mvseq	Mzseq	MzRk	NRd	MvRd	MzRd	Comb.				
		kg	kg*m	kg*m	kg*m	kg	kg*m	kg*m					
1	Y	2688	4083	47	194567	19516	9213	9213	8				
1	Z	2688	2450	79	191775	19516	9213	9213	8				

Asia : 8002 [238 , 239]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m	kg	kg	kg
-3269	-4016	340	211298	20492	9673	16	26	0.960	0.943	--	0.941	0.386	0.565

Cls	Dir	N	Mvseq	Mzseq	MzRk	NRd	MvRd	MzRd	Comb.				
		kg	kg*m	kg*m	kg*m	kg	kg*m	kg*m					
1	Y	3269	3780	131	193187	19516	9213	9213	8				
1	Z	3269	2268	219	189856	19516	9213	9213	8				

Asia : 8002 [239 , 123]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m	kg	kg	kg
-3917	-3408	412	211298	20492	9673	17	28	0.953	0.934	--	0.856	0.540	0.513

Cls	Dir	N	Mvseq	Mzseq	MzRk	NRd	MvRd	MzRd	Comb.				
		kg	kg*m	kg*m	kg*m	kg	kg*m	kg*m					
1	Y	3917	2916	223	191738	19516	9213	9213	8				
1	Z	3917	1750	371	187856	19516	9213	9213	8				

Asia : 8002 [123 , 124]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m	kg	kg	kg
-3646	-2160	362	211298	20492	9673	18	30	0.948	0.927	--	0.634	0.566	0.381

Cls	Dir	N	Mvseq	Mzseq	MzRk	NRd	MvRd	MzRd	Comb.				
		kg	kg*m	kg*m	kg*m	kg	kg*m	kg*m					
1	Y	3646	1370	205	190743	19516	9213	9213	8				
1	Z	3646	822	342	186492	19516	9213	9213	8				

Asia : 8002 [124 , 103]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m	kg	kg	kg
-5443	3413	172	211298	20492	9673	18	30	0.945	0.923	--	0.603	0.361	0.362

Cls	Dir	N	Mvseq	Mzseq	MzRk	NRd	MvRd	MzRd	Comb.				
		kg	kg*m	kg*m	kg*m	kg	kg*m	kg*m					
1	Y	5443	2056	62	190238	19516	9213	9213	6				
1	Z	5443	1234	104	185803	19516	9213	9213	6				

Asia : 8003 [310 , 321]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m	kg	kg	kg
-1625	4856	11	211298	20492	9673	11	19	0.990	0.986	--	0.935	0.240	0.561

Cls	Dir	N	Mvseq	Mzseq	MzRk	NRd	MvRd	MzRd	Comb.				
		kg	kg*m	kg*m	kg*m	kg	kg*m	kg*m					
1	Y	1625	4543	3	199289	19516	9213	9213	(12+13)-V-4				
1	Z	1625	2726	4	198442	19516	9213	9213	(12+13)-V-4				

Asia : 8003 [321 , 322]

Sez. G: HE 240 A L=108.2 cm Ln1=108.2 cm Ln2=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m	kg	kg	kg
-1113	4070	15	211298	20492	9673	11	18	0.993	0.990	--	0.911	0.240	0.547

Cls	Dir	N	Mvseq	Mzseq	MzRk	NRd	MvRd	MzRd	Comb.				
		kg	kg*m	kg*m	kg*m	kg	kg*m	kg*m					
1	Y	1113	3709	4	199867	19516	9213	9213	(12+13)-V-4				
1	Z	1113	2226	6	199269	19516	9213	9213	(12+13)-V-4				

Asia : 8003 [322 , 230]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m	kg	kg	kg
-2199	3167	-65	211298	20492	9673	11	19	0.990	0.985	--	0.805	0.299	0.483

Cls	Dir	N	Mvseq	Mzseq	MzRk	NRd	MvRd	MzRd	Comb.				
		kg	kg*m	kg*m	kg*m	kg	kg*m	kg*m					
1	Y	2199	2549	19	199171	19516	9213	9213	(12+13)-V-4				
1	Z	2199	1530	32	198275	19516	9213	9213	(12+13)-V-4				

Asia : 8003 [230 , 231]

Sez. G: HE 240 A L=22.6 cm Ln1=22.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m	kg	kg	kg
-1843	-3832	42	211298	20492	9673	12	20	0.983	0.976	--	0.892	0.578	0.535

Cls	Dir	N	Mvseq	Mzseq	MzRk	NRd	MvRd	MzRd	Comb.				
		kg	kg*m	kg*m	kg*m	kg	kg*m	kg*m					
1	Y	1843	3418	24	197908	19516	9213	9213	8				
1	Z	1843	2051	40	196476	19516	9213	9213	8				

Asia : 8003 [231 , 232]

Sez. G: HE 240 A L=134.5 cm Ln1=134.5 cm Ln2=134.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m	kg	kg	kg
-2187	-4413	100	211298	20492	9673	13	22	0.976	0.965	--	0.948	0.400	0.569

Cls	Dir	N	Mvseq	Mzseq	MzRk	NRd	MvRd	MzRd	Comb.				
		kg	kg*m	kg*m	kg*m	kg	kg*m	kg*m					
1	Y	2187	4184	40	196352	19516	9213	9213	8				
1	Z	2187	2510	67	194250	19516	9213	9213	8				

Asia : 8003 [232 , 233]

Asia : 8003 [233 , 234]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3408	-4448	200	211298	20492	9673	16	26	0.960	0.943	--	0.941	0.514	0.564
													0.857

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3408	4184	103	193181	19516	9213	8	4.11
1	Z	3408	2510	171	189848	19516	9213	8	6.05

Asia : 8003 [234 , 121]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4210	-3767	518	211298	20492	9673	17	28	0.953	0.933	--	0.848	0.444	0.509
													0.740

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4210	3195	230	191733	19516	9213	8	4.75
1	Z	4210	1917	383	187849	19516	9213	8	6.16

Asia : 8003 [121 , 122]

Sez. G: HE 240 A L=177.7 cm Ln1=177.7 cm Ln2=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2365	-2630	402	211298	20492	9673	18	30	0.948	0.927	--	0.753	0.350	0.452
													0.583

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2365	1981	140	190738	19516	9213	(12+13)-V-4	7.74
1	Z	2365	1189	234	186485	19516	9213	(12+13)-V-4	10.1

Asia : 8003 [122 , 104]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5972	4291	102	211298	20492	9673	18	30	0.945	0.923	--	0.658	0.574	0.395
													0.956

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5972	2822	59	190234	19516	9213	3	5.48
1	Z	5972	1693	98	185797	19516	9213	3	7.72

Asia : 8004 [311 , 319]

Sez. G: HE 240 A L=112.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-303	5523	11	211298	20492	9673	11	19	0.990	0.986	--	0.938	0.247	0.563
													0.412

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	303	5181	3	199300	19516	9213	(12+13)-V-4	3.74
1	Z	303	3108	4	198459	19516	9213	(12+13)-V-4	6.20

Asia : 8004 [319 , 320]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1251	4049	-150	211298	20492	9673	11	18	0.993	0.990	--	0.961	0.320	0.576
													0.534

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1251	3891	48	199879	19516	9213	(12+13)-VIII-4	4.74
1	Z	1251	2334	80	199286	19516	9213	(12+13)-VIII-4	7.43

Asia : 8004 [320 , 225]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2932	4049	-142	211298	20492	9673	11	19	0.990	0.985	--	0.867	0.453	0.520
													0.756

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2932	3511	64	199183	19516	9213	(12+13)-VIII-4	4.96
1	Z	2932	2107	107	198291	19516	9213	(12+13)-VIII-4	7.44

Asia : 8004 [225 , 226]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-472	-3999	41	211298	20492	9673	12	20	0.984	0.976	--	0.961	0.598	0.577
													0.996

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	472	3843	24	197918	19516	9213	9	4.95
1	Z	472	2306	41	196491	19516	9213	9	8.00

Asia : 8004 [226 , 227]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2435	-4518	53	211298	20492	9673	13	22	0.976	0.965	--	0.950	0.521	0.570
													0.869

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2435	4293	28	196342	19516	9213	8	4.25
1	Z	2435	2576	46	194263	19516	9213	8	6.69

Asia : 8004 [227 , 228]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3005	-4623	115	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.477	0.601
													0.795

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3005	4628	35	194569	19516	9213	8	3.87
1	Z	3005	2777	91	191778	19516	9213	8	5.96

Asia : 8004 [228 , 229]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3169	-4578	327	211298	20492	9673	16	26	0.960	0.943	--	0.940	0.427	0.564
													0.711

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3169	4302	139	193189	19516	9213	8	3.97
1	Z	3169	2581	232	189859	19516	9213	8	5.74

Asta : 8004 [229 , 119]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg				
-3938	-3869	524	211298	20492	9673	17	28	0.953	0.934	--	0.846	0.479	0.508
													0.798

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	3938	3274	251	191740	19516	9213	8	4.64
1	Z	3938	1964	418	187859	19516	9213	8	5.99

Asta : 8004 [119 , 120]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg				
-2576	2557	-317	211298	20492	9673	18	30	0.948	0.927	--	0.976	0.364	0.586
													0.606

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	2576	2497	115	190745	19516	9213	(12+13)-VII-1	6.50
1	Z	2576	1498	192	186494	19516	9213	(12+13)-VII-1	8.98

Asta : 8004 [120 , 105]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg				
-5666	4524	131	211298	20492	9673	18	30	0.945	0.923	--	0.660	0.600	0.396
													1.000

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	5666	2984	78	190240	19516	9213	3	5.23
1	Z	5666	1791	131	185806	19516	9213	3	7.33

Asta : 8005 [312 , 325]

Sez. G: HE 240 A L=112.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg				
-1793	7737	5	211298	20492	9673	11	19	0.990	0.986	--	0.894	0.489	0.536
													0.815

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	1793	6913	3	199301	19516	9213	(12+13)-V-4	2.75
1	Z	1793	4148	4	198459	19516	9213	(12+13)-V-4	4.50

Asta : 8005 [325 , 326]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg				
-970	5674	12	211298	20492	9673	11	18	0.993	0.990	--	0.836	0.464	0.501
													0.773

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	970	4741	6	199879	19516	9213	(12+13)-V-4	4.03
1	Z	970	2845	10	199287	19516	9213	(12+13)-V-4	6.59

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Asta : 8005 [326 , 240]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg				
-165	-2871	-34	211298	20492	9673	11	19	0.990	0.985	--	0.869	0.240	0.522
													0.400

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	165	2495	8	199183	19516	9213	(12+13)-V-1	7.72
1	Z	165	1497	13	198291	19516	9213	(12+13)-V-1	12.7

Asta : 8005 [240 , 241]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg				
-557	-1937	-50	211298	20492	9673	12	20	0.984	0.976	--	0.776	0.463	0.466
													0.772

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	557	1504	23	197919	19516	9213	(12+13)-VII-1	12.1
1	Z	557	902	39	196492	19516	9213	(12+13)-VII-1	18.8

Asta : 8005 [241 , 242]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg				
-2361	756	105	211298	20492	9673	13	22	0.976	0.965	--	0.578	0.240	0.347
													0.400

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	2361	436	25	196342	19516	9213	(12+13)-III-2	26.9
1	Z	2361	262	42	194263	19516	9213	(12+13)-III-2	33.2

Asta : 8005 [242 , 243]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg				
-2586	1305	100	211298	20492	9673	15	25	0.967	0.953	--	0.827	0.530	0.496
													0.883

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	2586	1080	53	194570	19516	9213	(12+13)-I-2	13.4
1	Z	2586	648	89	191779	19516	9213	(12+13)-I-2	17.8

Asta : 8005 [243 , 244]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg				
-426	-4153	230	211298	20492	9673	16	26	0.960	0.943	--	0.905	0.460	0.543
													0.766

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	426	3757	106	193189	19516	9213	6	4.85
1	Z	426	2254	176	189859	19516	9213	6	7.31

Asta : 8005 [244 , 125]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

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N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-396	-3492	442	211298	20492	9673	17	28	0.953	0.934	--	0.817	0.503	0.490
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	396	2851	222	191740	19516	9213	8					
1	Z	396	1711	370	187859	19516	9213	8					

Asia : 8005 [125 , 126]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-304	2202	-330	211298	20492	9673	18	30	0.948	0.927	--	0.964	0.462	0.578
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	304	2122	152	190745	19516	9213	(12+13)÷VII-1					
1	Z	304	1273	254	186495	19516	9213	(12+13)÷VII-1					

Asia : 8005 [126 , 106]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-800	3901	-268	211298	20492	9673	18	30	0.945	0.923	--	0.887	0.252	0.532
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	800	3458	67	190240	19516	9213	(12+13)÷VIII-1					
1	Z	800	2075	112	185806	19516	9213	(12+13)÷VIII-1					

Asia : 8006 [1010 , 1009]

Sez. G: HE 240 A L=114.6 cm Ln1=114.6 cm Ln2=114.6 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4258	933	-2969	211298	20492	9673	11	19	0.989	0.984	--	0.600	0.386	0.360
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	4258	560	1147	198998	19516	9213	(12+13)÷VIII-4					
1	Z	4258	336	1912	198027	19516	9213	(12+13)÷VIII-4					

Asia : 8006 [1009 , 1008]

Sez. G: HE 240 A L=114.6 cm Ln1=114.6 cm Ln2=114.6 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1517	2793	-259	211298	20492	9673	11	19	0.989	0.984	--	0.813	0.278	0.488
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	1517	2270	72	198998	19516	9213	(12+13)÷IV-2					
1	Z	1517	1362	120	198027	19516	9213	(12+13)÷IV-2					

Asia : 8006 [1008 , 1007]

Sez. G: HE 240 A L=114.6 cm Ln1=114.6 cm Ln2=114.6 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1462	3754	180	211298	20492	9673	11	19	0.989	0.984	--	0.899	0.596	0.539

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	1462	3373	108	198998	19516	9213	(12+13)÷IV-2					
1	Z	1462	2024	179	198027	19516	9213	(12+13)÷IV-2					

Asia : 8006 [1007 , 1006]

Sez. G: HE 240 A L=114.6 cm Ln1=114.6 cm Ln2=114.6 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-866	-3809	143	211298	20492	9673	11	19	0.989	0.984	--	0.946	0.584	0.568
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	866	3603	83	198998	19516	9213	(12+13)÷III-3					
1	Z	866	2162	139	198027	19516	9213	(12+13)÷III-3					

Asia : 8006 [1006 , 1005]

Sez. G: HE 240 A L=114.6 cm Ln1=114.6 cm Ln2=114.6 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-793	-3852	-92	211298	20492	9673	11	19	0.989	0.984	--	0.995	0.240	0.597
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	793	3833	22	198998	19516	9213	(12+13)÷III-3					
1	Z	793	2300	37	198027	19516	9213	(12+13)÷III-3					

Asia : 8006 [1005 , 1004]

Sez. G: HE 240 A L=114.6 cm Ln1=114.6 cm Ln2=114.6 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-167	-3817	-94	211298	20492	9673	11	19	0.989	0.984	--	0.959	0.240	0.576
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	167	3662	22	198998	19516	9213	(12+13)÷III-3					
1	Z	167	2197	37	198027	19516	9213	(12+13)÷III-3					

Asia : 8006 [1004 , 1003]

Sez. G: HE 240 A L=114.6 cm Ln1=114.6 cm Ln2=114.6 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-110	-3423	69	211298	20492	9673	11	19	0.989	0.984	--	0.903	0.240	0.542
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	110	3091	16	198998	19516	9213	(12+13)÷III-3					
1	Z	110	1854	27	198027	19516	9213	(12+13)÷III-3					

Asia : 8006 [1003 , 1002]

Sez. G: HE 240 A L=114.6 cm Ln1=114.6 cm Ln2=114.6 cm Crit.: Acciaio_PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
Asta tesa													

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1								I					

Asta : 8006 [1002 , 1001]

Sez. G: HE 240 A L=114.6 cm Ln1=114.6 cm Ln2=114.6 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq

Verificato											
N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m					

Asta tesa

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.			
		kg	kg*m	kg*m	kg	kg*m	kg*m				
1								1			--

Verifica Resistenza aste Metalliche

Scenario di calcolo : Set_NT_SLV_A2_STR/GEO

Asta : [1 , 17]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-12117	-820	-196	-1	629	-1720	--	--	(12+13)+VII-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87004	38027	19516	9213	462	>100	3.58	>100	3.58

Asta : [17 , 25]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-4607	204	331	-5	-870	636	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86715	37901	19516	9213	462	>100	7.32	91.3	7.32

Asta : [25 , 101]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1727	220	224	-8	-1064	359	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86507	37810	19516	9213	462	>100	9.79	59.2	9.79

Asta : 2 [2 , 19]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	11538	-836	-488	-2	1376	-1757	--	--	(12+13)+VII-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86965	38010	19516	9213	462	77.9	3.14	>100	3.14

Asta : 2 [19 , 26]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
135	1	-5882	-41	-341	-2	-1801	230	--	--	7	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
135	1	201236	86926	37993	19516	9213	462	>100	6.82	>100	6.82

Asta : 2 [26 , 102]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
136	1	-4316	114	-992	-1	-2572	95	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
136	1	201236	87018	38034	19516	9213	462	38.4	6.11	>100	6.11

Asta : 3 [3 , 20]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-14775	-873	-599	-2	1883	-1819	--	--	(12+13)+VII-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86974	38014	19516	9213	462	63.4	2.72	>100	2.72

Asta : 3 [20 , 23]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
135	1	-6064	162	-1001	-2	-1950	207	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
135	1	201236	86965	38010	19516	9213	462	38.0	6.56	>100	6.56

Asta : 3 [23 , 103]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
136	1	-5504	-119	-1240	-2	-3442	382	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
136	1	201236	86964	38010	19516	9213	462	30.7	4.08	>100	4.08

Asta : 4 [4 , 15]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	10663	-804	-914	-1	2944	-1678	--	--	(12+13)+VII-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87050	38048	19516	9213	462	41.6	2.59	>100	2.59

Asia : 4 [15 , 24]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
135	1	-6481	15	-929	-2	-2495	217	--	--	2
X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
135	1	201236	86935	37997	19516	9213	462	40.9	5.45	>100
135	1	201236	86935	37997	19516	9213	462	40.9	5.45	>100

Asia : 4 [24 , 104]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
136	1	-6109	52	-1516	-4	-4289	150	--	--	3
X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
136	1	201236	86816	37945	19516	9213	462	25.0	3.75	>100
136	1	201236	86816	37945	19516	9213	462	25.0	3.75	>100

Asia : 5 [5 , 16]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-13177	-762	-867	1	2795	-1614	--	--	(12+13)-VII-2
X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	201236	87042	38044	19516	9213	462	43.9	2.61	>100
0	1	201236	87042	38044	19516	9213	462	43.9	2.61	>100

Asia : 5 [16 , 21]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
135	1	-7007	106	-1299	-0	-2557	240	--	--	3
X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
135	1	201236	87097	38068	19516	9213	462	29.3	5.21	>100
135	1	201236	87097	38068	19516	9213	462	29.3	5.21	>100

Asia : 5 [21 , 105]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
136	1	-6715	46	-1587	-5	-4519	180	--	--	3
X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
136	1	201236	86692	37891	19516	9213	462	23.9	3.52	86.2
136	1	201236	86692	37891	19516	9213	462	23.9	3.52	86.2

Asia : 6 [6 , 18]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-14178	616	-1440	-1	3762	1271	--	--	(12+13)-IV-3
X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86692	37891	19516	9213	462	23.9	3.52	86.2
0	1	201236	86692	37891	19516	9213	462	23.9	3.52	86.2

X	cls	Nr	Vyr	Vzr	Mrv	Mzr	MTrd	SF V.	SF M	SF Mt
0	1	201236	87013	38031	19516	9213	462	26.4	2.49	>100
0	1	201236	87013	38031	19516	9213	462	26.4	2.49	>100

Asia : 6 [18 , 22]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
135	1	-7747	-80	-1049	0	-2711	215	--	--	7
X	cls	Nr	Vyr	Vzr	Mrv	Mzr	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
135	1	201236	87094	38067	19516	9213	462	36.3	4.98	>100
135	1	201236	87094	38067	19516	9213	462	36.3	4.98	>100

Asia : 6 [22 , 106]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
136	1	-5527	-303	-1340	-3	-4130	426	--	--	(12+13)-IV-3
X	cls	Nr	Vyr	Vzr	Mrv	Mzr	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
136	1	201236	86858	37964	19516	9213	462	28.3	3.50	>100
136	1	201236	86858	37964	19516	9213	462	28.3	3.50	>100

Asia : 7 [1001 , 118]

Sez. G: HE 240 A L=146.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-2604	-2652	19	-62	-28	-4166	--	--	7
X	cls	Nr	Vyr	Vzr	Mrv	Mzr	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	201236	82505	35973	19516	9213	462	31.0	2.14	7.47
0	1	201236	82505	35973	19516	9213	462	31.0	2.14	7.47

Asia : 7 [7 , 1001]

Sez. G: HE 240 A L=542.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-7222	2752	-364	5	1004	4901	--	--	7
X	cls	Nr	Vyr	Vzr	Mrv	Mzr	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86684	37888	19516	9213	462	31.5	1.61	84.5
0	1	201236	86684	37888	19516	9213	462	31.5	1.61	84.5

Asia : 8 [1002 , 117]

Sez. G: IPE 140 L=248.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
99	1	-636	-28	-101	-0	-301	-9	--	--	7
X	cls	Nr	Vyr	Vzr	Mrv	Mzr	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
99	1	43021	15231	11554	2315	504	46	>100	6.15	>100
99	1	43021	15231	11554	2315	504	46	>100	6.15	>100

Asia : 9 [1003 , 1111]

Sez. G: IPE 140 L=249.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
199	1	-1652	-18	118	-1	-569	7	--	--	7
X	cls	Nr	Vyr	Vzr	Mrv	Mzr	MTrd	SF V.	SF M	SF Mt
cm	kg	kg	kg	kg	kg*	kg*	kg*			
199	1	43021	15231	11554	2315	504	46	>100	6.15	>100
199	1	43021	15231	11554	2315	504	46	>100	6.15	>100

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
199	1	43021	15128	11476	2315	504	46	97.4	3.36	58.1	3.36

Asta : 9 [1111 , 224]

Sez. G: IPE 140 L=92.3 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1617	30	312	1	-461	13	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	43021	15148	11492	2315	504	46	36.8	3.79	72.1	3.79

Asta : 10 [1004 , 1112]

Sez. G: IPE 140 L=249.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
249	1	77	-38	174	-1	-822	51	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
249	1	43021	15042	11411	2315	504	46	65.6	2.19	32.2	2.19

Asta : 10 [1112 , 223]

Sez. G: IPE 140 L=170.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-211	-68	118	1	-786	-71	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	43021	15043	11412	2315	504	46	96.8	2.06	32.2	2.06

Asta : 11 [1005 , 1113]

Sez. G: IPE 140 L=249.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
224	1	689	-5	-42	-1	-1111	-5	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
224	1	43021	15036	11407	2315	504	46	>100	1.98	31.2	1.98

Asta : 11 [1113 , 222]

Sez. G: IPE 140 L=232.7 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	702	-6	7	1	-1112	-4	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	43021	15161	11501	2315	504	46	>100	1.98	84.6	1.98

Asta : 12 [1006 , 1114]

Sez. G: IPE 140 L=249.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
249	1	187	4	-18	-2	-1301	-16	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
249	1	43021	15012	11388	2315	504	46	>100	1.67	27.7	1.67

Asta : 12 [1114 , 221]

Sez. G: IPE 140 L=274.3 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
27	1	-440	-7	-14	1	-1199	-2	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
27	1	43021	15156	11498	2315	504	46	>100	1.88	79.7	1.88

Asta : 13 [1007 , 1115]

Sez. G: IPE 140 L=294.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
249	1	692	7	-58	-1	-1401	-15	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
249	1	43021	15072	11434	2315	504	46	>100	1.54	38.1	1.54

Asta : 13 [1115 , 220]

Sez. G: IPE 140 L=294.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
29	1	700	-11	1	-0	-1422	-11	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
29	1	43021	15186	11520	2315	504	46	>100	1.53	>100	1.53

Asta : 14 [1008 , 1116]

Sez. G: IPE 140 L=249.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
249	1	203	51	-58	-1	-1351	-85	--	--	11	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
249	1	43021	15130	11478	2315	504	46	>100	1.32	59.6	1.32

Asta : 14 [1116 , 318]

Sez. G: IPE 140 L=289.7 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
29	1	-1036	18	-31	-1	-1296	34	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
29	1	43021	15099	11454	2315	504	46	>100	1.53	45.7	1.53

Asta : 157 [1009 , 1117]

Sez. G: IPE 140 L=249.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
249	1	469	17	115	0	-969	-21	--	--	7	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
249	1	43021	15172	11509	2315	504	46	>100	2.13	99.5	2.13

Asta : 157 [1117 , 317]

Sez. G: IPE 140 L=256.3 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
26	1	467	-14	-32	-2	-1004	-16	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
26	1	43021	14907	11309	2315	504	46	>100	2.10	18.9	2.10

Asta : 207 [207 , 1010]

Sez. G: HE 240 A L=50.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2539	294	7597	384	-3440	271	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	35002	15299	19516	9213	462	2.01	4.58	1.200	1.200

Asta : 207 [1118 , 307]

Sez. G: HE 240 A L=187.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4149	-139	-1692	0	3499	-243	--	--	(12+13)-V1-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87064	38054	19516	9213	462	22.5	4.42	>100	4.42

Asta : 208 [208 , 308]

Sez. G: HE 240 A L=486.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	3400	-230	899	1	-1819	-1229	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86999	38025	19516	9213	462	42.3	4.11	>100	4.11

Asta : 209 [209 , 309]

Sez. G: HE 240 A L=486.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2871	165	1259	2	-3661	845	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86976	38015	19516	9213	462	30.2	3.41	>100	3.41

Asta : 210 [210 , 310]

Sez. G: HE 240 A L=486.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1976	-195	1633	2	-4145	-1013	--	--	(12+13)-V1-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86928	37994	19516	9213	462	23.3	3.01	>100	3.01

Asta : 211 [211 , 311]

Sez. G: HE 240 A L=486.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-5634	-192	1788	2	-4761	-985	--	--	(12+13)-V1-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86941	38000	19516	9213	462	21.3	2.64	>100	2.64

Asta : 212 [212 , 312]

Sez. G: HE 240 A L=486.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6274	331	2764	2	-6669	1067	--	--	(12+13)-VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86957	38007	19516	9213	462	13.8	2.05	>100	2.05

Asta : 701 [1001 , 117]

Sez. G: 2LD 60x30x5d10 L=306.6 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	3	-4773	--	--	--	--	--	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	3	22262	--	--	--	--	--	>100	4.66	>100	4.66

Asta : 702 [117 , 1003]

Sez. G: 2LD 60x30x5d10 L=236.4 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	4608	--	--	--	--	--	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	22262	--	--	--	--	--	>100	4.83	>100	4.83

Asta : 703 [1003 , 1112]

Sez. G: 2LD 60x30x5d10 L=306.9 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	3	-2979	--	--	--	--	--	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	3	22262	--	--	--	--	--	>100	7.47	>100	7.47

Asta : 704 [1112 , 1005]

Sez. G: 2LD 60x30x5d10 L=236.7 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Non verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	1649	--	--	--	--	--	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	22262	--	--	--	--	--	>100	13.5	>100	13.5

Asia : 705 [1005 , 1114]
Sez. G: 2LD 60x30x5d10 L=306.9 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	--	--	(12+13)+I-4
307	1	1431	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--
307	1	22262	--	--	--	--	--	>100	15.6	>100	15.6

Asia : 706 [1114 , 1007]
Sez. G: 2LD 60x30x5d10 L=236.7 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	--	--	(12+13)+VI-4
237	3	-2052	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--
237	3	22262	--	--	--	--	--	>100	10.8	>100	10.8

Asia : 707 [1117 , 1111]
Sez. G: 2LD 60x30x5d10 L=114.7 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	--	--	(12+13)+I-2
115	1	3125	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--
115	1	22262	--	--	--	--	--	>100	7.12	>100	7.12

Asia : 707 [1007 , 1116]
Sez. G: 2LD 60x30x5d10 L=306.9 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	--	--	(12+13)+II-4
307	1	2178	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--
307	1	22262	--	--	--	--	--	>100	10.2	>100	10.2

Asia : 708 [1111 , 1112]
Sez. G: 2LD 60x30x5d10 L=114.6 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	--	--	(12+13)+I-2
115	1	3092	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--
115	1	22262	--	--	--	--	--	>100	7.20	>100	7.20

Asia : 708 [1116 , 1009]
Sez. G: 2LD 60x30x5d10 L=236.7 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
237	3	-2630								6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
237	3	22262	--	--	--	--	--	>100	8.46	>100	8.46

Asia : 709 [1112 , 1113]

Sez. G: 2LD 60x30x5d10 L=114.6 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	--	--	(12+13)+I-1
115	1	2925	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--
115	1	22262	--	--	--	--	--	>100	7.61	>100	7.61

Asia : 709 [1009 , 1118]

Sez. G: 2LD 60x30x5d10 L=306.9 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m	--	--	--
307	1	2950	--	--	--	--	--	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--
307	1	22262	--	--	--	--	--	>100	7.55	>100	7.55

Asia : 710 [1113 , 1114]

Sez. G: 2LD 60x30x5d10 L=114.6 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	--	--	(12+13)+I-1
115	1	2929	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--
115	1	22262	--	--	--	--	--	>100	7.60	>100	7.60

Asia : 710 [1118 , 317]

Sez. G: 2LD 60x30x5d10 L=243.3 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	--	--	(12+13)+II-4
0	3	-5281	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--
0	3	22262	--	--	--	--	--	>100	4.22	>100	4.22

Asia : 711 [1114 , 1115]

Sez. G: 2LD 60x30x5d10 L=114.6 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	--	--	(12+13)+I-1
115	1	2855	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	--	--	--	--
115	1	22262	--	--	--	--	--	>100	7.80	>100	7.80

Asia : 711 [317 , 1116]

Sez. G: 2LD 60x30x5d10 L=313.8 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	--	--	(12+13)+IV-4
0	1	3274	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	22262	--	--	--	--	--	>100	6.80	>100	6.80

Asia : 712 [1115, 1116]

Sez. G: 2LD 60x30x5d10 L=114.6 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	2866	--	--	--	--	--	--	--	(12+13)+I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	22262	--	--	--	--	--	>100	7.77	>100	7.77

Asia : 712 [1116, 220]

Sez. G: 2LD 60x30x5d10 L=277.5 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	3	-3502	--	--	--	--	--	--	--	(12+13)+II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	3	22262	--	--	--	--	--	>100	6.36	>100	6.36

Asia : 713 [1116, 1117]

Sez. G: 2LD 60x30x5d10 L=114.6 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	3069	--	--	--	--	--	--	--	(12+13)+I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	22262	--	--	--	--	--	>100	7.25	>100	7.25

Asia : 713 [220, 1114]

Sez. G: 2LD 60x30x5d10 L=349.4 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2171	--	--	--	--	--	--	--	(12+13)+IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	22262	--	--	--	--	--	>100	10.3	>100	10.3

Asia : 714 [1117, 1118]

Sez. G: 2LD 60x30x5d10 L=114.6 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	3089	--	--	--	--	--	--	--	(12+13)+I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	22262	--	--	--	--	--	>100	7.21	>100	7.21

Asia : 714 [1114, 222]

Sez. G: 2LD 60x30x5d10 L=222.3 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	3	-2528	--	--	--	--	--	--	--	(12+13)+VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	3	22262	--	--	--	--	--	>100	8.81	>100	8.81

Asia : 715 [222, 1112]

Sez. G: 2LD 60x30x5d10 L=291.7 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1031	--	--	--	--	--	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	22262	--	--	--	--	--	>100	21.6	>100	21.6

Asia : 716 [1112, 224]

Sez. G: 2LD 60x30x5d10 L=120.7 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	3	-1317	--	--	--	--	--	--	--	(12+13)+V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	3	22262	--	--	--	--	--	>100	16.9	>100	16.9

Asia : 1001 [118, 116]

Sez. G: IPE 100 L=95.4 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2747	14	-76	-0	0	49	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9461	7672	1033	240	27	>100	3.28	>100	3.28

Asia : 1002 [117, 115]

Sez. G: IPE 100 L=101.4 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	929	-135	-45	0	0	-60	--	--	(12+13)+III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9474	7684	1033	240	27	70.4	3.53	>100	3.53

Asia : 1003 [224, 219]

Sez. G: IPE 100 L=107.4 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-112	-117	-46	-0	0	-49	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9473	7682	1033	240	27	80.7	4.77	>100	4.77

Asia : 1004 [223, 218]

Sez. G: IPE 100 L=113.4 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
68	1	-113	3	26	-0	-34	30	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
68	1	27037	9471	7681	1033	240	27	>100	6.11	>100	6.11

Asta : 1005 [222 , 217]

Sez. G: IPE 100 L=119.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-149	-143	-78	0	0	-50	--	--		7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9475	7684	1033	240	27	66.1	4.69	>100	4.69

Asta : 1006 [221 , 216]

Sez. G: IPE 100 L=125.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1510	-135	-76	0	0	-48	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9467	7677	1033	240	27	70.0	3.89	>100	3.89

Asta : 1007 [220 , 215]

Sez. G: IPE 100 L=131.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-231	-158	-74	0	0	-70	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9469	7679	1033	240	27	60.0	3.33	>100	3.33

Asta : 1008 [318 , 316]

Sez. G: IPE 100 L=137.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1944	27	-104	0	0	35	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9476	7685	1033	240	27	74.1	4.62	>100	4.62

Asta : 1009 [317 , 315]

Sez. G: IPE 100 L=143.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
72	1	-145	3	-0	0	-60	16	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
72	1	27037	9475	7684	1033	240	27	>100	7.59	>100	7.59

Asta : 1010 [307 , 308]

Sez. G: IPE 100 L=149.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
149	1	2324	31	38	0	0	-24	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9480	7688	1033	240	27	>100	5.42	>100	5.42

Asta : 1011 [101 , 102]

Sez. G: IPE 100 L=89.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/M=2619 kg/cmq ft=4300 kg/cmq .Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-211	-181	-34	-0	0	-82	---		(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9471	7681	1033	240	27	52.3	2.85	>100	2.85

Asta : 1012 [116 , 124]

Sez. G: IPE 100 L=95.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/M=2619 kg/cmq ft=4300 kg/cmq .Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	27	-174	-45	0	0	-70	---		(12+13)+V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9469	7679	1033	240	27	54.4	3.40	>100	3.40

Asta : 1013 [115 , 123]

Sez. G: IPE 100 L=101.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	944	-193	-46	-0	0	-83	--		(12+13)-VII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9477	7685	1033	240	27	49.1	2.62	>100	2.62

Asta : 1014 [219 , 239]

Sez. G: IPE 100 L=107.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	63	-192	-47	-0	0	-87	--		(12+13)-VII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9471	7681	1033	240	27	49.3	2.73	>100	2.73

Asta : 1015 [218 , 238]

Sez. G: IPE 100 L=113.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	665	-170	-47	-0	0	-79	---		(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9467	7677	1033	240	27	55.7	2.82	>100	2.82

Asta : 1016 [217 , 237]

Sez. G: IPE 100 L=119.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq: Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	191	-155	-46	-0	0	-75	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9463	7675	1033	240	27	61.1	3.13	>100	3.13

Asia : 1017 [216 , 236]

Sez. G: IPE 100 L=125,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm			kg	kg	kg*	kg*						
0	1	396	-156	-44	0	-81	--	--	(12+13)-VIII-1			

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9466	7677	1033	240	27	60.6	2.85	>100	2.85

Asia : 1018 [215 , 235]

Sez. G: IPE 100 L=131,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
0	1	-20	-156	-43	0	-85	--	--	(12+13)-VIII-1			

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9476	7685	1033	240	27	60.7	2.82	>100	2.82

Asia : 1019 [316 , 324]

Sez. G: IPE 100 L=137,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
96	1	-3239	-13	45	0	-32	13	--	--	--	7	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
96	1	27037	9474	7683	1033	240	27	>100	4.90	>100	4.90

Asia : 1020 [315 , 323]

Sez. G: IPE 100 L=143,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
144	1	-347	-24	110	0	33	--	--	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
144	1	27037	9472	7682	1033	240	27	69.6	6.56	>100	6.56

Asia : 1021 [308 , 309]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
147	1	2009	-18	64	0	29	--	--	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
147	1	27037	9475	7684	1033	240	27	>100	5.09	>100	5.09

Asia : 1022 [102 , 103]

Sez. G: IPE 100 L=89,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
0	1	-380	-128	-35	0	-58	--	--	(12+13)-V-1			

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9464	7675	1033	240	27	74.1	3.93	>100	3.93

Asia : 1023 [124 , 122]

Sez. G: IPE 100 L=95,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
95	1	-247	150	46	0	-59	--	--	(12+13)-V-3			

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
95	1	27037	9471	7681	1033	240	27	63.0	3.90	>100	3.90

Asia : 1024 [123 , 121]

Sez. G: IPE 100 L=101,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
101	1	-255	173	48	0	-74	--	--	(12+13)-VII-4			

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	27037	9480	7688	1033	240	27	54.9	3.15	>100	3.15

Asia : 1025 [239 , 234]

Sez. G: IPE 100 L=107,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
107	1	-112	169	49	0	-75	--	--	(12+13)-VII-4			

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9477	7686	1033	240	27	55.9	3.17	>100	3.17

Asia : 1026 [238 , 233]

Sez. G: IPE 100 L=113,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
113	1	-352	149	48	0	-66	--	--	(12+13)-VII-4			

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27037	9470	7680	1033	240	27	63.7	3.45	>100	3.45

Asia : 1027 [237 , 232]

Sez. G: IPE 100 L=119,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
119	1	-280	128	47	0	-58	--	--	(12+13)-VIII-4			

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9471	7681	1033	240	27	73.7	3.95	>100	3.95

Asia : 1028 [236 , 231]

Sez. G: IPE 100 L=125,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
126	1	-724	124	46	0	-59	--	--	(12+13)-VIII-4			

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
126	1	27037	9472	7682	1033	240	27	76.4	3.67	>100	3.67

Asia : 1029 [235 , 230]

Sez. G: IPE 100 L=131,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.			
cm		kg	kg	kg	kg*	kg*						
132	1	-161	118	44	0	-58	--	--	(12+13)-VIII-4			

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9479	7687	1033	240	27	80.6	4.00	>100	4.00

Asta : 1030 [324 , 322]

Sez. G: IPE 100 L=137,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
55	1	-1162	10	-33	0	-53	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
55	1	27037	9478	7687	1033	240	27	>100	5.96	>100	5.96

Asta : 1031 [323 , 321]

Sez. G: IPE 100 L=143,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
144	1	-258	-24	112	0	0	33	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
144	1	27037	9479	7687	1033	240	27	68.8	6.70	>100	6.70

Asta : 1032 [309 , 310]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	2180	-23	93	0	0	33	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9481	7689	1033	240	27	82.2	4.55	>100	4.55

Asta : 1033 [103 , 104]

Sez. G: IPE 100 L=89,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	762	133	-60	-0	0	76	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9481	7689	1033	240	27	71.2	2.88	>100	2.88

Asta : 1034 [122 , 120]

Sez. G: IPE 100 L=149,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	-57	258	233	-0	0	-67	--	--	6	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9478	7687	1033	240	27	33.0	3.54	>100	3.54

Asta : 1035 [121 , 119]

Sez. G: IPE 100 L=149,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	-1	256	225	-0	0	-70	--	--	6	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9479	7687	1033	240	27	34.1	3.42	>100	3.42

Asta : 1036 [234 , 229]

Sez. G: IPE 100 L=149,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	-17	240	213	-0	0	-65	--	--	6	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9480	7688	1033	240	27	36.1	3.70	>100	3.70

Asta : 1037 [233 , 228]

Sez. G: IPE 100 L=149,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	-60	124	65	0	0	-61	--	--	(12+13)-VII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9472	7682	1033	240	27	76.5	3.91	>100	3.91

Asta : 1038 [232 , 227]

Sez. G: IPE 100 L=149,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	-172	121	60	0	0	-61	--	--	(12+13)-VII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9472	7682	1033	240	27	78.6	3.86	>100	3.86

Asta : 1039 [231 , 226]

Sez. G: IPE 100 L=149,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	-619	125	55	0	0	-66	--	--	(12+13)-IV-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9475	7684	1033	240	27	76.0	3.33	>100	3.33

Asta : 1040 [230 , 225]

Sez. G: IPE 100 L=149,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	-60	131	51	-0	0	-74	--	--	(12+13)-IV-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9478	7686	1033	240	27	72.1	3.22	>100	3.22

Asta : 1041 [230 , 320]

Sez. G: IPE 100 L=149,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	2156	-24	68	0	0	18	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9472	7682	1033	240	27	>100	6.49	>100	6.49

Asta : 1042 [321 , 319]

Sez. G: IPE 100 L=149,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
149	1	-159	-25	116	0	0	35	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9474	7683	1033	240	27	66.2	6.52	>100	6.52

Asia : 1043 [310 , 311]

Sez. G: IPE 100 L=149,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
149	1	1671	-28	93	0	0	37	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9480	7688	1033	240	27	82.3	4.65	>100	4.65

Asia : 1044 [104 , 105]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	594	54	-147	-0	0	57	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9480	7688	1033	240	27	52.4	3.84	>100	3.84

Asia : 1046 [119 , 125]

Sez. G: IPE 100 L=101,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
102	1	21	198	126	-0	0	-43	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
102	1	27037	9476	7685	1033	240	27	47.9	5.53	>100	5.53

Asia : 1047 [229 , 244]

Sez. G: IPE 100 L=107,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
107	1	-6	194	153	-0	0	-40	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9472	7682	1033	240	27	48.9	5.92	>100	5.92

Asia : 1048 [228 , 243]

Sez. G: IPE 100 L=113,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
57	1	-23	8	-0	-0	-37	29	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
57	1	27037	9469	7679	1033	240	27	>100	6.43	>100	6.43

Asia : 1049 [227 , 242]

Sez. G: IPE 100 L=119,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
72	1	-169	-2	25	-0	-36	31	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
72	1	27037	9472	7682	1033	240	27	>100	5.91	>100	5.91

Asia : 1050 [226 , 241]

Sez. G: IPE 100 L=125,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
75	1	-402	-17	24	-0	-36	34	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	27037	9477	7686	1033	240	27	>100	5.25	>100	5.25

Asia : 1051 [225 , 240]

Sez. G: IPE 100 L=131,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
79	1	-189	-12	23	0	-37	33	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
79	1	27037	9481	7689	1033	240	27	>100	5.58	>100	5.58

Asia : 1052 [320 , 326]

Sez. G: IPE 100 L=137,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
27	1	537	13	-67	-0	-24	22	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
27	1	27037	9480	7688	1033	240	27	>100	7.38	>100	7.38

Asia : 1053 [319 , 325]

Sez. G: IPE 100 L=143,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
100	1	7	-18	68	0	-51	22	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
100	1	27037	9481	7689	1033	240	27	>100	7.14	>100	7.14

Asia : 1054 [311 , 312]

Sez. G: IPE 100 L=149,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	2606	-34	-36	0	0	-26	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9476	7685	1033	240	27	>100	4.93	>100	4.93

Asia : 1055 [105 , 106]

Sez. G: IPE 100 L=89,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	82	202	-61	-0	0	109	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9480	7688	1033	240	27	46.9	2.17	>100	2.17

Asta : 1056 [120 , 126]

Sez. G: IPE 100 L=95.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
96	1	-146	174	83	-0	0	-44	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
96	1	27037	9476	7685	1033	240	27	54.4	5.26	>100	5.26

Asta : 1057 [244 , 245]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	2	-6	-5	0	2	-3	--	--	(12+13)-V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	75.6	>100	75.6

Asta : 1058 [125 , 128]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	2	-6	-5	-0	2	-3	--	--	(12+13)-VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	67.4	>100	67.4

Asta : 1059 [243 , 246]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	2	-6	-5	0	2	-3	--	--	(12+13)-V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	77.2	>100	77.2

Asta : 1060 [242 , 247]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	2	-6	-5	-0	2	-3	--	--	(12+13)-V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9475	7684	1033	240	27	>100	78.1	>100	78.1

Asta : 1061 [241 , 248]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1	-6	-1	0	-1	-3	--	--	(12+13)-V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	84.4	>100	84.4

Asta : 1062 [240 , 249]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-1	-6	-1	0	-0	-3	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	84.3	>100	84.3

Asta : 1063 [326 , 327]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-0	-3	-6	0	2	-2	--	--	(12+13)-V-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	90.4	>100	90.4

Asta : 1064 [325 , 328]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-0	-3	-6	0	2	-2	--	--	(12+13)-V-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	90.6	>100	90.6

Asta : 1065 [312 , 313]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	0	4	-6	0	2	3	--	--	(12+13)-V-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	77.5	>100	77.5

Asta : 1066 [106 , 114]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	1	4	7	0	-3	3	--	--	(12+13)-VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	66.5	>100	66.5

Asta : 1067 [126 , 127]

Sez. G: IPE 100 L=70.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	1	-6	-1	0	-1	-3	--	--	(12+13)-VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	74.1	>100	74.1

Asta : 1228 [1010 , 1118]

Sez. G: HE 240 A L=249.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-8542	-273	2609	-86	-3033	-880	--	--	(12+13)-V1-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	80332	35111	19516	9213	462	13.5	3.41	5.36	3.41

Asta : 2001 [17 , 19]

Sez. G: IPE 100 L=89.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	162	-21	5	0	0	22	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	27037	9472	7682	1033	240	27	>100	10.1	>100	10.1

Asta : 2002 [19 , 20]

Sez. G: IPE 100 L=89.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	210	6	-5	0	0	21	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9474	7683	1033	240	27	>100	10.3	>100	10.3

Asta : 2003 [20 , 15]

Sez. G: IPE 100 L=89.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
102	1	188	-6	5	0	0	22	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
102	1	27037	9477	7686	1033	240	27	>100	10.0	>100	10.0

Asta : 2004 [15 , 16]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	108	-0	2	0	-3	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9480	7688	1033	240	27	>100	12.7	>100	12.7

Asta : 2005 [16 , 18]

Sez. G: IPE 100 L=89.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	112	11	-5	0	0	22	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9481	7689	1033	240	27	>100	10.6	>100	10.6

Asta : 2006 [25 , 26]

Sez. G: IPE 100 L=89.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	-118	-41	4	-0	0	26	--	--	(12+13)+IV-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	27037	9480	7688	1033	240	27	>100	8.89	>100	8.89

Asta : 2007 [26 , 23]

Sez. G: IPE 100 L=89.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-276	12	-3	-0	0	9	--	--	(12+13)+VI-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9470	7680	1033	240	27	>100	20.9	>100	20.9

Asta : 2008 [23 , 24]

Sez. G: IPE 100 L=89.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	-45	-24	4	0	0	14	--	--	(12+13)+V-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	27037	9471	7681	1033	240	27	>100	16.1	>100	16.1

Asta : 2009 [24 , 21]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	25	9	-7	0	0	11	--	--	(12+13)+V-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9479	7688	1033	240	27	>100	21.5	>100	21.5

Asta : 2010 [21 , 22]

Sez. G: IPE 100 L=89.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-68	27	-5	-0	0	16	--	--	7	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9480	7689	1033	240	27	>100	14.1	>100	14.1

Asta : 2001 [101 , 115]

Sez. G: Fil16 L=371.4 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2877	--	--	--	--	--	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	1.83	>100	1.83

Asta : 2002 [115 , 223]

Sez. G: Fil16 L=345.3 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
345	1	2765	--	--	--	--	--	--	--	(12+13)+V-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
345	1	5266	--	--	--	--	--	>100	1.90	>100	1.90

Asta : 2003 [223 , 216]

Sez. G: Fil16 L=305.9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-2033	--	--	--	--	--	--	--	(12+13)+V-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	2.59	>100	2.59

Asia : 7004 [216 , 318]

Sez. G: Fil16 L=269.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	-3340	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.58	>100	1.58

Asia : 7005 [318 , 308]

Sez. G: Fil16 L=269.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	1629	--	--	--	--	--	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	3.23	>100	3.23

Asia : 7006 [308 , 207]

Sez. G: Fil18 L=508.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	6639	--	--	--	--	--	--	--	(12+13)+II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	6665	--	--	--	--	--	>100	1.00	>100	1.00

Asia : 7007 [208 , 307]

Sez. G: Fil18 L=508.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	-6605	--	--	--	--	--	--	--	(12+13)+II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	6665	--	--	--	--	--	>100	1.01	>100	1.01

Asia : 7008 [307 , 316]

Sez. G: Fil16 L=260.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	-1849	--	--	--	--	--	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	2.85	>100	2.85

Asia : 7009 [316 , 221]

Sez. G: Fil16 L=268.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	3532	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.49	>100	1.49

Asia : 7010 [221 , 218]

Sez. G: Fil16 L=306.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	1991	--	--	--	--	--	--	--	(12+13)+V-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	2.64	>100	2.64

Asia : 7011 [218 , 117]

Sez. G: Fil16 L=345.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
345	1	-2732	--	--	--	--	--	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
345	1	5266	--	--	--	--	--	>100	1.93	>100	1.93

Asia : 7012 [117 , 102]

Sez. G: Fil16 L=371.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	2894	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.82	>100	1.82

Asia : 7013 [17 , 2]

Sez. G: Fil16 L=285.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	2586	--	--	--	--	--	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	2.04	>100	2.04

Asia : 7014 [19 , 1]

Sez. G: Fil16 L=285.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
285	1	-2596	--	--	--	--	--	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
285	1	5266	--	--	--	--	--	>100	2.03	>100	2.03

Asia : 7015 [5 , 18]

Sez. G: Fil16 L=285.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	-2319	--	--	--	--	--	--	--	(12+13)+V-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	2.27	>100	2.27

Asia : 7016 [105 , 125]

Sez. G: F16 L=371.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato										
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m				
372	1	1903	--	--	--	--	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
372	1	5266	--	--	--	--	--	>100	2.77	>100	2.77

Asia : 7017 [125 , 228]

Sez. G: Fil6 L=345.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato										
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m				
0	1	-1490	---	---	---	---	---	---	---	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	3.53	>100	3.53

Asia : 7018 [228 , 241]

Sez. G: F16 L=306.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato										
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m				
306	1	1023	---	---	---	---	---	---	---	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
306	1	5266	--	--	--	--	--	>100	5.15	>100	5.15

Asia : 7019 [241 , 320]

Sez. G: F16 L=268.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
269	1	2325	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
269	1	5266	--	--	--	--	--	>100	2.26	>100	2.26

Asia : 7020 [320 , 312]

Sez. G: Fil6 L=260.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
261	1	-1712	---	---	---	---	---	---	---	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
261	1	5266	--	--	--	--	--	>100	3.08	>100	3.08

Asia : 7021 [312 , 211]

Sez. G: F18 L=508.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato										
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m				
508	1	-6623	---	---	---	---	---	---	---	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
508	1	6665	--	--	--	--	--	>100	1.01	>100	1.01

Asia : 7022 [212 , 311]

Sez. G: F18 L=508.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq <i>Non verificato</i>										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-6167	--	--	--	--	--	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	6665	--	--	--	--	--	>100	1.080	>100	1.080

Asia : 7023 [311 , 326]

Sez. G: Fil6 L=260.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
260	1	782	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
260	1	5266	--	--	--	--	--	>100	6.73	>100	6.73

Asia : 7024 [326 , 226]

Sez. G: Fil6 L=269.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
269	1	-1839	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
269	1	5266	--	--	--	--	--	>100	2.86	>100	2.86

Asia : 7025 [226 , 243]

Sez. G: Fil6 L=306.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1023	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	5.15	>100	5.15

Asia : 7026 [243 , 119]

Sez. G: Fil6 L=345.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq <i>Verificato</i>										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1837	--	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.87	>100	2.87

Asia : 7027 [119 , 106]

Sez. G: F16 L=371.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
372	1	-2046	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
372	1	5266	--	--	--	--	--	>100	2.57	>100	2.57

Asia : 7028 [16 , 6]

Sez. G: F16 L=285.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
		kg	kg	kg	kg*m	kg*m	kg*m			
286	1	-2349	--	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.24	>100	2.24
286	1	5266	--	--	--	--	--				

Asia : 7029 [324 , 310]

Sez. G: F116 L=261.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
261	1	-2691	--	--	--	--	--	--	--		(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.96	>100	1.96
261	1	5266	--	--	--	--	--				

Asia : 7030 [310 , 320]

Sez. G: F116 L=264.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
264	1	2413	--	--	--	--	--	--	--		(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.18	>100	2.18
264	1	5266	--	--	--	--	--				

Asia : 7031 [320 , 311]

Sez. G: F116 L=217.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
218	1	-1078	--	--	--	--	--	--	--		(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	4.89	>100	4.89
218	1	5266	--	--	--	--	--				

Asia : 7032 [311 , 322]

Sez. G: F116 L=263.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2501	--	--	--	--	--	--	--		(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.11	>100	2.11
0	1	5266	--	--	--	--	--				

Asia : 7033 [322 , 309]

Sez. G: F116 L=260.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	2651	--	--	--	--	--	--	--		(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.99	>100	1.99
0	1	5266	--	--	--	--	--				

Asia : 7034 [309 , 316]

Sez. G: F116 L=260.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
260	1	2841	--	--	--	--	--	--	--		(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.85	>100	1.85
260	1	5266	--	--	--	--	--				

Asia : 7035 [324 , 308]

Sez. G: F116 L=260.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
261	1	-3103	--	--	--	--	--	--	--		(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.70	>100	1.70
261	1	5266	--	--	--	--	--				

Asia : 7036 [102 , 123]

Sez. G: F116 L=371.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-3912	--	--	--	--	--	--	--		(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.35	>100	1.35
0	1	5266	--	--	--	--	--				

Asia : 7037 [123 , 104]

Sez. G: F116 L=371.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
371	1	-3007	--	--	--	--	--	--	--		(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.75	>100	1.75
371	1	5266	--	--	--	--	--				

Asia : 7038 [104 , 119]

Sez. G: F116 L=389.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
389	1	3096	--	--	--	--	--	--	--		(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.70	>100	1.70
389	1	5266	--	--	--	--	--				

Asia : 7039 [105 , 121]

Sez. G: F116 L=388.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-3167	--	--	--	--	--	--	--		(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.66	>100	1.66
0	1	5266	--	--	--	--	--				

Asia : 7040 [121 , 103]

Sez. G: F116 L=371.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
372	1	-3022	--	--	--	--	--	--	--		(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.74	>100	1.74
372	1	5266	--	--	--	--	--				

Asia : 7041 [103 , 115]

Sez. G: F116 L=371.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
372	1	3845	--	--	--	--	--	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
372	1	5266	--	--	--	--	--	>100	1.37	>100	1.37

Asia : 7042 [17 , 26]

Sez. G: Fil16 L=162.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3682	--	--	--	--	--	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.43	>100	1.43

Asia : 7043 [26 , 101]

Sez. G: Fil16 L=162.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
162	1	3023	--	--	--	--	--	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
162	1	5266	--	--	--	--	--	>100	1.74	>100	1.74

Asia : 7044 [25 , 19]

Sez. G: Fil16 L=162.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	3680	--	--	--	--	--	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.43	>100	1.43

Asia : 7045 [16 , 22]

Sez. G: Fil16 L=162.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3191	--	--	--	--	--	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.65	>100	1.65

Asia : 7046 [22 , 105]

Sez. G: Fil16 L=162.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2659	--	--	--	--	--	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.98	>100	1.98

Asia : 7047 [106 , 21]

Sez. G: Fil16 L=162.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
163	1	-2539	--	--	--	--	--	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
163	1	5266	--	--	--	--	--	>100	2.07	>100	2.07

Asia : 7048 [21 , 18]

Sez. G: Fil16 L=162.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	3154	--	--	--	--	--	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.67	>100	1.67

Asia : 7049 [25 , 102]

Sez. G: Fil16 L=162.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3065	--	--	--	--	--	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.72	>100	1.72

Asia : 7050 [104 , 23]

Sez. G: Fil16 L=162.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
162	1	-2909	--	--	--	--	--	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
162	1	5266	--	--	--	--	--	>100	1.81	>100	1.81

Asia : 7051 [23 , 15]

Sez. G: Fil16 L=162.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	3429	--	--	--	--	--	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.54	>100	1.54

Asia : 7052 [15 , 3]

Sez. G: Fil16 L=285.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
285	1	-2535	--	--	--	--	--	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
283	1	5266	--	--	--	--	--	>100	2.08	>100	2.08

Asia : 7053 [4 , 20]

Sez. G: Fil16 L=285.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2478	--	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	2.13	>100	2.13

Asia : 7054 [20 , 24]

Sez. G: F16 L=162.2 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-3405	--	--	--	--	--	--	--	(12+13)-V-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	1.55	>100	1.55

Asia : 7055 [24 , 103]

Sez. G: F16 L=162.2 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-2950	--	--	--	--	--	--	--	(12+13)-VII-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	1.78	>100	1.78

Asia : 8000 [307 , 317]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq											
: Verificato											

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	-61	13	-1372	17	-2027	-67	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	85800	37501	19516	9213	462	27.3	8.97	27.1	8.97

Asia : 8000 [317 , 318]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq											
: Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	-233	28	-171	1	-2179	67	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	201236	86989	38021	19516	9213	462	>100	8.33	>100	8.33

Asia : 8000 [318 , 220]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq											
: Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	414	338	197	2	-1864	-347	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	201236	86972	38013	19516	9213	462	>100	7.39	>100	7.39

Asia : 8000 [220 , 221]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq											
: Verificato											

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	216	-193	-43	1	-1884	-319	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87020	38034	19516	9213	462	>100	7.57	>100	7.57

Asia : 8000 [221 , 222]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq											
: Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
134	1	-2402	551	-44	31	-1054	-921	--	--	7	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
134	1	201236	84763	37048	19516	9213	462	>100	6.03	15.1	6.03

Asia : 8000 [222 , 223]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq											
: Verificato											

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-2223	-387	-3	1	-1040	-924	--	--	7	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87014	38032	19516	9213	462	>100	6.08	>100	6.08

Asia : 8000 [223 , 224]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq											
: Verificato											

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
158	1	-2256	-194	184	-12	-1895	632	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
158	1	201236	86211	37681	19516	9213	462	>100	5.65	39.5	5.65

Asia : 8000 [224 , 117]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq											
: Verificato											

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	-1628	43	-840	-3	-3475	554	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	86838	37955	19516	9213	462	452	4.06	>100	4.06

Asia : 8000 [117 , 118]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq											
: Verificato											

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1142	92	1083	-3	-3423	564	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86849	37960	19516	9213	462	35.1	4.13	>100	4.13

Asia : 8000 [118 , 101]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq											
: Verificato											

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4361	196	-1318	9	2447	284	--	--	(12+13)-III-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
0	1	201236	86431	37777	19516	9213	462	28.7	5.62	52.4	5.62

Asta : 8001 [308 , 315]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	456	-11	-2366	-14	3553	17	--	--	(12+13)+V-III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86014	37595	19516	9213	462	15.9	5.37	32.4	5.37

Asta : 8001 [315 , 316]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
108	1	-2696	-177	1064	24	2073	185	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
108	1	201236	85248	37260	19516	9213	462	35.0	7.16	19.0	7.16

Asta : 8001 [316 , 215]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2946	135	-846	-27	2073	197	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	85013	37157	19516	9213	462	43.9	7.03	16.9	7.03

Asta : 8001 [215 , 216]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
123	1	-3025	106	-235	6	-2663	-13	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
123	1	201236	86607	37854	19516	9213	462	>100	6.54	71.2	6.54

Asta : 8001 [216 , 217]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
134	1	-3614	-33	-188	19	-3152	102	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
134	1	201236	85660	37440	19516	9213	462	>100	5.25	24.4	5.25

Asta : 8001 [217 , 218]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

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:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
89	1	-3991	70	-143	10	-3375	108	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	201236	86313	37725	19516	9213	462	>100	4.89	44.6	4.89

Asta : 8001 [218 , 219]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
63	1	-2651	-32	86	6	-3406	118	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
63	1	201236	86671	37882	19516	9213	462	>100	4.99	81.9	4.99

Asta : 8001 [219 , 115]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
68	1	-3271	-203	456	-1	-2960	274	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
68	1	201236	87018	38034	19516	9213	462	83.3	5.06	>100	5.06

Asta : 8001 [115 , 116]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2092	84	811	-13	-2391	453	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86079	37623	19516	9213	462	46.4	5.49	34.4	5.49

Asta : 8001 [116 , 102]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
182	1	-4173	117	1675	-10	2575	-14	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
182	1	201236	86314	37726	19516	9213	462	22.5	6.49	44.7	6.49

Asta : 8002 [309 , 323]

Sez. G: HE 240 A L=12.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1377	6	-367	-0	3949	-1	--	--	(12+13)+V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87081	38061	19516	9213	462	>100	4.78	>100	4.78

Asia : 8002 [323 , 324]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4			Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-980	-37	-994	1	3177	-13	--	--	(12+13)-V-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87021	38035	19516	9213	462	38.3	5.92	>100	5.92

Asia : 8002 [324 , 235]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4			Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	-1264	44	-568	-15	-2706	53	--	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	201236	85944	37564	19516	9213	462	66.2	6.63	30.4	6.63

Asia : 8002 [235 , 236]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4			Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
123	1	-1891	48	-527	9	-3548	21	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
123	1	201236	86396	37761	19516	9213	462	71.7	5.17	49.8	5.17

Asia : 8002 [236 , 237]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4			Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
134	1	-2209	22	-171	16	-4014	59	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
134	1	201236	85887	37539	19516	9213	462	>100	4.48	29.0	4.48

Asia : 8002 [237 , 238]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4			Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	-2426	70	-112	11	-4056	100	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	201236	86241	37694	19516	9213	462	>100	4.34	40.9	4.34

Asia : 8002 [238 , 239]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4			Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	-3130	-191	419	9	-3718	219	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	201236	86384	37757	19516	9213	462	90.2	4.35	49.1	4.35

Asia : 8002 [239 , 123]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4			Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-3532	-61	577	-7	-3408	308	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86553	37830	19516	9213	462	65.6	4.43	64.1	4.43

Asia : 8002 [123 , 124]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4			Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-3245	30	964	-14	-2160	362	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86004	37590	19516	9213	462	39.0	6.02	32.1	6.02

Asia : 8002 [124 , 103]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4			Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
182	1	-5443	68	1883	-7	3413	61	--	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
182	1	201236	86564	37835	19516	9213	462	20.1	4.80	65.5	4.80

Asia : 8003 [310 , 321]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4			Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1625	14	-406	-1	4856	11	--	--	(12+13)-V-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87036	38041	19516	9213	462	93.7	3.87	>100	3.87

Asia : 8003 [321 , 322]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1105	-19	-1084	0	4070	-8	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87081	38061	19516	9213	462	35.1	4.65	>100	4.65

Asia.: 8003 [322 , 230]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2143	57	-1494	-4	3167	16	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86758	37920	19516	9213	462	25.4	5.72	>100	5.72

Asia.: 8003 [230 , 231]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
123	1	-1843	3	-660	12	-3832	38	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
123	1	201236	86225	37687	19516	9213	462	57.1	4.77	40.1	4.77

Asia.: 8003 [231 , 232]

Sez. G: HE 240 A L=134.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
134	1	-2187	62	-248	15	-4413	17	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
134	1	201236	85954	37569	19516	9213	462	>100	4.19	30.7	4.19

Asia.: 8003 [232 , 233]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
104	1	-2630	-23	56	15	-4498	97	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
104	1	201236	85991	37585	19516	9213	462	>100	3.94	31.7	3.94

Asia.: 8003 [233 , 234]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3018	-45	246	6	-4448	128	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86613	37856	19516	9213	462	>100	3.89	72.1	3.89

Asia.: 8003 [234 , 121]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3777	-199	673	-3	-3767	180	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86849	37960	19516	9213	462	56.4	4.32	>100	4.32

Asia.: 8003 [121 , 122]

Sez. G: HE 240 A L=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2148	170	874	-3	-2630	402	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86834	37953	19516	9213	462	43.4	5.29	>100	5.29

Asia.: 8003 [122 , 104]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
182	1	-5972	-7	2231	-11	4291	102	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
182	1	201236	86292	37716	19516	9213	462	16.9	3.84	43.5	3.84

Asia.: 8004 [311 , 319]

Sez. G: HE 240 A L=12.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	262	25	-2219	7	6056	-11	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86532	37821	19516	9213	462	17.0	3.20	61.8	3.20

Asia.: 8004 [319 , 320]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	301	-1	-1041	-0	4561	1	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87079	38060	19516	9213	462	36.6	4.25	>100	4.25

Asta : 8004 [320 , 225]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-2875	-81	-1314	15	4049	-142	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	85954	37568	19516	9213	462	28.6	4.22	30.7	4.22

Asta : 8004 [225 , 226]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
123	1	-1660	-20	-581	12	-3946	15	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
123	1	201236	86156	37657	19516	9213	462	64.9	4.72	37.2	4.72

Asta : 8004 [226 , 227]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
134	1	-2435	13	-233	15	-4518	36	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
134	1	201236	85941	37563	19516	9213	462	>100	4.04	30.3	4.04

Asta : 8004 [227 , 228]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
133	1	-2976	-40	116	11	-4598	109	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
133	1	201236	86251	37698	19516	9213	462	>100	3.81	41.3	3.81

Asta : 8004 [228 , 229]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
32	1	-2842	-149	329	4	-4484	138	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
32	1	201236	86780	37929	19516	9213	462	>100	3.86	>100	3.86

Asta : 8004 [229 , 119]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-3502	-156	713	-9	-3869	258	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	86445	37783	19516	9213	462	53.0	4.10	53.6	4.10

Asta : 8004 [119 , 120]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-4673	143	1207	-0	-3422	380	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	87062	38053	19516	9213	462	31.5	4.55	>100	4.55

Asta : 8004 [120 , 105]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
182	1	-5666	1	2341	-2	4524	130	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
182	1	201236	86982	38018	19516	9213	462	16.2	3.65	>100	3.65

Asta : 8005 [312 , 325]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-1793	5	-1926	-1	7737	3	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	87012	38031	19516	9213	462	19.8	2.46	>100	2.46

Asta : 8005 [325 , 326]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-964	-4	-2242	-2	5674	5	--	--	(12+13)-V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	86950	38004	19516	9213	462	17.0	3.38	>100	3.38

Asta : 8005 [326 , 240]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
113	1	861	96	-1338	-6	-3404	-75	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	201236	86646	37871	19516	9213	462	28.3	5.35	77.3	5.35

Asta : 8005 [240 , 241]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
123	1	935	-93	-791	14	-4514	54	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
123	1	201236	85997	37587	19516	9213	462	47.5	4.14	31.9	4.14

Asta : 8005 [241 , 242]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
134	1	1009	57	-119	12	-4823	-2	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
134	1	201236	86223	37686	19516	9213	462	>100	3.96	40.0	3.96

Asta : 8005 [242 , 243]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
74	1	828	-111	233	15	-4692	92	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
74	1	201236	85928	37557	19516	9213	462	>100	3.93	30.0	3.93

Asta : 8005 [243 , 244]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	307	-84	523	5	-4479	163	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86697	37893	19516	9213	462	72.5	4.02	87.1	4.02

Asta : 8005 [244 , 125]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-154	-105	846	-8	-3492	263	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86507	37810	19516	9213	462	44.7	4.80	59.2	4.80

Asta : 8005 [125 , 126]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2078	143	837	-1	-2413	393	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87059	38052	19516	9213	462	45.5	5.66	>100	5.66

Asta : 8005 [126 , 106]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
182	1	-881	-178	1171	13	4151	103	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
182	1	201236	86082	37624	19516	9213	462	32.1	4.38	34.5	4.38

Asta : 8006 [1010 , 1009]

Sez. G: HE 240 A L=14.6 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-4550	-2479	330	95	0	-3016	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	79582	34783	19516	9213	462	32.1	2.86	4.84	2.86

Asta : 8006 [1009 , 1008]

Sez. G: HE 240 A L=14.6 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	4438	83	-2871	-16	-7397	253	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	201236	85845	37521	19516	9213	462	13.1	2.33	28.0	2.33

Asta : 8006 [1008 , 1007]

Sez. G: HE 240 A L=14.6 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	4466	323	-1819	7	-9472	87	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	201236	86568	37837	19516	9213	462	20.8	1.93	66.0	1.93

Asta : 8006 [1007 , 1006]

Sez. G: HE 240 A L=14.6 cm Crit.: Acciaio_PressSverg $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
115	1	4855	184	-742	10	-10276	105	--	--	7

VERIFICHE STATO LIMITE DI ESERCIZIO

Verifica spostamenti laterali delle colonne in acciaio secondo NTC 2008

Scenario di calcolo : Set_NT_SLD_A2_STR/GEO

Verifica spostamenti orizzontali relativi di piano (§4.2.4.2.2 - NTC 2008)												
Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup.	SpostX sup.	SpostY sup.	SpostX inf.	SpostY inf.	δ	h/300.00	Verifica	
0-1	105 (Nodo_105)	5 (Nodo_5)	6	7.20	9.14	0.00	0.00	0.00	11.64	18.07	Si	
0-1	106 (Nodo_106)	6 (Nodo_6)	6	7.31	9.19	0.00	0.00	0.00	11.74	18.07	Si	
0-1	103 (Nodo_103)	3 (Nodo_3)	6	4.08	7.35	0.00	0.00	0.00	8.41	18.07	Si	
0-1	104 (Nodo_104)	4 (Nodo_4)	6	5.26	8.04	0.00	0.00	0.00	9.61	18.07	Si	
0-1	101 (Nodo_101)	1 (Nodo_1)	6	0.34	4.76	0.00	0.00	0.00	4.77	18.07	Si	
0-1	102 (Nodo_102)	2 (Nodo_2)	6	1.87	5.90	0.00	0.00	0.00	6.19	18.07	Si	
0-1	1001 (Nodo_1001)	7 (Nodo_7)	6	-7.83	14.65	0.00	0.00	0.00	16.61	18.07	Si	
2-3	308 (Nodo_308)	208 (Nodo_208)	6	-3.20	6.28	0.00	0.00	0.00	7.05	16.20	Si	
2-3	309 (Nodo_309)	209 (Nodo_209)	5	-6.28	-4.86	0.00	0.00	0.00	7.94	16.20	Si	
2-3	310 (Nodo_310)	210 (Nodo_210)	5	-7.73	-5.56	0.00	0.00	0.00	9.52	16.20	Si	
2-3	311 (Nodo_311)	211 (Nodo_211)	5	-8.76	-6.00	0.00	0.00	0.00	10.62	16.20	Si	
2-3	312 (Nodo_312)	212 (Nodo_212)	5	-9.72	-6.43	0.00	0.00	0.00	11.65	16.20	Si	
2-3	307 (Nodo_307)	207 (Nodo_207)	6	-1.73	7.27	0.00	0.00	0.00	7.47	16.20	Si	

Verifica spostamenti orizzontali in sommità (§4.2.4.2.2 - NTC 2008)

Verifica spostamenti orizzontali in sommità (§4.2.4.2.2 - NTC 2008)						
Nodo	Comb.	SpostX mm	SpostY mm	Δ mm	H/500.00 mm	Verifica
308 (Nodo_308)	6	-3.20	6.28	7.05	26.46	Si
309 (Nodo_309)	5	-6.28	-4.86	7.94	26.46	Si
310 (Nodo_310)	5	-7.73	-5.56	9.52	26.46	Si
311 (Nodo_311)	5	-8.76	-6.00	10.62	26.46	Si
312 (Nodo_312)	5	-9.72	-6.43	11.65	26.46	Si
307 (Nodo_307)	6	-1.73	7.27	7.47	26.46	Si

Verifica spostamenti verticali delle aste in Acciaio secondo NTC 2008

Scenario di calcolo : Set_NT_SLD_A2_STR/GEO

Travata: 8000 (Travata 8000) [307 (Nodo 307) ,101 (Nodo 101)]
L = 1425.8cm Crit.Prog: Acciaio_Pressflessione δx = 0.0cm Verifica: Verificata
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax mm	L/250.00 mm	Cs
cm		mm	mm	
620.1	2	11.64	57.03	4.90

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ2 mm	L/300.00 mm	Cs
cm		mm	mm	
605.3	2	4.76	47.53	9.97

Travata: 8001 (Travata 8001) [308 (Nodo 308) ,102 (Nodo 102)]

L = 1426.0cm Crit.Prog: Acciaio_Pressflessione δx = 0.0cm Verifica: Verificata
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax mm	L/250.00 mm	Cs
cm		mm	mm	

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
115	1	201236	86362	37747	19516	9213	462	50.9	1.78	47.6	1.78

Asia - 8006 [1006 ,1005]

Sez. G: HE 240 A L=114.6 cm Crit.: Acciaio PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq :Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	4854	30	283	27	-10275	112	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	85071	37182	19516	9213	462	>100	1.78	17.4	1.78

Asia - 8006 [1005 ,1004]

Sez. G: HE 240 A L=114.6 cm Crit.: Acciaio PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq :Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	4041	-350	1207	22	-10043	-101	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	85438	37343	19516	9213	462	30.9	1.83	21.2	1.83

Asia - 8006 [1004 ,1003]

Sez. G: HE 240 A L=114.6 cm Crit.: Acciaio PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq :Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	3943	16	2038	26	-8668	100	--	--	7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	85110	37199	19516	9213	462	18.3	2.11	17.7	2.11

Asia - 8006 [1003 ,1002]

Sez. G: HE 240 A L=114.6 cm Crit.: Acciaio PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq :Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m			
0	1	555	-264	2675	19	-6681	-67	--	--	11

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	85677	37447	19516	9213	462	14.0	2.84	24.7	2.84

Asia - 8006 [1002 ,1001]

Sez. G: HE 240 A L=114.6 cm Crit.: Acciaio PressSverg γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq :Verificato

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	464	771	3188	-43	-3653	114	--		7

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	83829	36640	19516	9213	462	11.5	4.95	10.9	4.95

x		Comb.	δ_{max}	L/250.00	Cs
649.8		2	13.17	57.04	4.33

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ₂	L/300.00	Cs
cm			mm	mm	
649.8		2	5.45	47.53	8.72

Travata: 8002 (Travata 8002) [309 (Nodo 309) , 103 (Nodo 103)]

L = 1426.1cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
649.9		2	14.17	57.04	4.03

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ₂	L/300.00	Cs
cm			mm	mm	
649.9		2	6.02	47.54	7.90

Travata: 8003 (Travata 8003) [310 (Nodo 310) , 104 (Nodo 104)]

L = 1426.6cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
650.2		2	14.91	57.06	3.83

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ₂	L/300.00	Cs
cm			mm	mm	
650.2		2	6.44	47.55	7.38

Travata: 8004 (Travata 8004) [311 (Nodo 311) , 105 (Nodo 105)]

L = 1425.9cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
664.5		2	14.48	57.04	3.94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ₂	L/300.00	Cs
cm			mm	mm	
649.7		2	6.29	47.53	7.56

Travata: 8005 (Travata 8005) [312 (Nodo 312) , 106 (Nodo 106)]

L = 1425.9cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
590.6		6	13.40	57.03	4.26

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ₂	L/300.00	Cs
cm			mm	mm	
563.7		6	6.07	47.53	7.83

Travata: 1001 (Travata 1001) [118 (Nodo 118) , 116 (Nodo 116)]

L = 95.4cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
76.3		7	-0.11	3.82	33.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ₂	L/300.00	Cs
cm			mm	mm	
66.8		7	-0.16	3.18	19.6

Travata: 1012 (Travata 1012) [116 (Nodo 116) , 124 (Nodo 124)]

L = 95.6cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
76.5		7	-0.10	3.82	36.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ₂	L/300.00	Cs
cm			mm	mm	
66.9		7	-0.16	3.19	19.7

Travata: 1023 (Travata 1023) [124 (Nodo 124) , 122 (Nodo 122)]

L = 95.2cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
76.2		7	-0.13	3.81	29.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ₂	L/300.00	Cs
cm			mm	mm	
66.7		7	-0.17	3.17	18.3

Travata: 1034 (Travata 1034) [122 (Nodo 122) , 120 (Nodo 120)]

L = 149.4cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
74.7		5	0.80	5.98	7.51

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ₂	L/300.00	Cs
cm			mm	mm	
59.8		5	0.33	4.98	15.0

Travata: 1002 (Travata 1002) [117 (Nodo 117) , 115 (Nodo 115)]

L = 101.4cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
81.1		7	-0.14	4.06	29.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ₂	L/300.00	Cs
cm			mm	mm	
71.0		7	-0.19	3.38	17.4

Travata: 1013 (Travata 1013) [115 (Nodo 115) , 123 (Nodo 123)]

L = 101.3cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
81.0	7	-0.11	4.05	36.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ ₂	L/300.00	Cs
cm		mm	mm	
70.9	7	-0.18	3.38	19.2

Travata: 1024 (Travata 1024) [123 (Nodo 123), 121 (Nodo 121)]

L = 101.3cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
81.0	7	-0.15	4.05	27.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ ₂	L/300.00	Cs
cm		mm	mm	
70.9	7	-0.20	3.38	17.2

Travata: 1035 (Travata 1035) [121 (Nodo 121), 119 (Nodo 119)]

L = 149.4cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
74.7	5	0.75	5.97	7.97

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ ₂	L/300.00	Cs
cm		mm	mm	
59.7	5	0.32	4.98	15.8

Travata: 1046 (Travata 1046) [119 (Nodo 119), 125 (Nodo 125)]

L = 101.6cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
81.3	7	-0.15	4.06	26.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ ₂	L/300.00	Cs
cm		mm	mm	
71.1	7	-0.22	3.39	15.2

Travata: 1003 (Travata 1003) [124 (Nodo 224), 219 (Nodo 219)]

L = 107.4cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
42.9	5	0.12	4.29	36.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ ₂	L/300.00	Cs
cm		mm	mm	
75.2	7	-0.18	3.58	19.5

Travata: 1014 (Travata 1014) [219 (Nodo 219), 239 (Nodo 239)]

L = 107.6cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
53.8	5	0.11	4.30	40.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ ₂	L/300.00	Cs
cm		mm	mm	
64.5	7	-0.18	3.59	20.2

Travata: 1025 (Travata 1025) [239 (Nodo 239), 234 (Nodo 234)]

L = 107.3cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
42.9	5	0.11	4.29	37.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ ₂	L/300.00	Cs
cm		mm	mm	
75.1	7	-0.17	3.58	20.7

Travata: 1036 (Travata 1036) [234 (Nodo 234), 229 (Nodo 229)]

L = 149.1cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
74.6	5	0.66	5.96	9.09

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ ₂	L/300.00	Cs
cm		mm	mm	
74.6	5	0.26	4.97	19.1

Travata: 1047 (Travata 1047) [229 (Nodo 229), 244 (Nodo 244)]

L = 107.3cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
85.8	7	-0.12	4.29	34.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ ₂	L/300.00	Cs
cm		mm	mm	
75.1	7	-0.20	3.58	18.2

Travata: 1004 (Travata 1004) [223 (Nodo 223), 218 (Nodo 218)]

L = 113.4cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
56.7	5	0.15	4.54	30.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ ₂	L/300.00	Cs
cm		mm	mm	
56.7	7	-0.16	3.78	23.8

Travata: 1037 (Travata 1037) [233 (Nodo 233), 228 (Nodo 228)]

L = 149.1cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
74.5	5	0.58	5.96	10.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
59.6	7	-0.27	4.97	18.7

Travata: 1048 (Travata 1048) [228 (Nodo 228) - 243 (Nodo 243)]

L = 113.5cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
56.7	5	0.14	4.54	31.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
56.7	7	-0.17	3.78	21.9

Travata: 1015 (Travata 1015) [218 (Nodo 218) - 238 (Nodo 238)]

L = 113.6cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
68.1	5	0.14	4.54	32.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
45.4	7	-0.19	3.79	20.1

Travata: 1026 (Travata 1026) [238 (Nodo 238) - 233 (Nodo 233)]

L = 113.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
56.7	5	0.15	4.54	31.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
45.4	7	-0.17	3.78	21.8

Travata: 1005 (Travata 1005) [222 (Nodo 222) - 217 (Nodo 217)]

L = 119.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
71.6	5	0.19	4.78	25.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
35.8	7	-0.22	3.98	18.0

Travata: 1016 (Travata 1016) [217 (Nodo 217) - 237 (Nodo 237)]

L = 119.5cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
71.7	5	0.19	4.78	24.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
35.9	7	-0.26	3.98	15.6

Travata: 1027 (Travata 1027) [237 (Nodo 237) - 232 (Nodo 232)]

L = 119.2cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
71.5	5	0.18	4.77	26.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
35.8	7	-0.25	3.97	16.1

Travata: 1038 (Travata 1038) [232 (Nodo 232) - 227 (Nodo 227)]

L = 149.2cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
74.6	5	0.53	5.97	11.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
44.8	7	-0.35	4.97	14.4

Travata: 1049 (Travata 1049) [227 (Nodo 227) - 242 (Nodo 242)]

L = 119.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
59.7	5	0.17	4.78	28.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
35.8	7	-0.23	3.98	17.6

Travata: 1006 (Travata 1006) [221 (Nodo 221) - 216 (Nodo 216)]

L = 125.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
25.1	7	-0.20	5.02	24.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
37.6	7	-0.31	4.18	13.7

Travata: 1017 (Travata 1017) [216 (Nodo 216) ,236 (Nodo 236)]

$L = 125.5\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max} mm	L/250.00 mm	Cs
cm		0.22	5.02	22.4
75.3	5			

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2 mm	L/300.00 mm	Cs
cm		-0.31	4.18	13.7
37.7	7			

Travata: 1028 (Travata 1028) [236 (Nodo 236) ,231 (Nodo 231)]

$L = 125.5\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max} mm	L/250.00 mm	Cs
cm		0.21	5.02	23.7
75.3	5			

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2 mm	L/300.00 mm	Cs
cm		-0.30	4.18	14.1
37.7	7			

Travata: 1039 (Travata 1039) [231 (Nodo 231) ,226 (Nodo 226)]

$L = 149.2\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max} mm	L/250.00 mm	Cs
cm		0.47	5.97	12.7
74.6	5			

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2 mm	L/300.00 mm	Cs
cm		-0.40	4.97	12.5
44.8	7			

Travata: 1050 (Travata 1050) [226 (Nodo 226) ,241 (Nodo 241)]

$L = 125.6\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max} mm	L/250.00 mm	Cs
cm		0.21	5.02	23.4
75.3	5			

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2 mm	L/300.00 mm	Cs
cm		-0.26	4.19	15.9
37.7	7			

Travata: 1007 (Travata 1007) [220 (Nodo 220) ,215 (Nodo 215)]

$L = 131.4\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max} mm	L/250.00 mm	Cs
cm		0.22	5.26	23.5
78.8	5			

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2 mm	L/300.00 mm	Cs
cm		-0.33	4.38	13.2
39.4	7			

Travata: 1018 (Travata 1018) [215 (Nodo 215) ,235 (Nodo 235)]

$L = 131.5\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max} mm	L/250.00 mm	Cs
cm		-0.26	5.26	20.6
26.3	7			

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2 mm	L/300.00 mm	Cs
cm		-0.35	4.38	12.5
39.5	7			

Travata: 1029 (Travata 1029) [235 (Nodo 235) ,230 (Nodo 230)]

$L = 131.6\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max} mm	L/250.00 mm	Cs
cm		0.22	5.26	24.0
78.9	5			

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2 mm	L/300.00 mm	Cs
cm		-0.33	4.39	13.3
39.5	7			

Travata: 1040 (Travata 1040) [230 (Nodo 230) ,225 (Nodo 225)]

$L = 149.1\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max} mm	L/250.00 mm	Cs
cm		0.41	5.97	14.4
74.6	5			

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2 mm	L/300.00 mm	Cs
cm		-0.41	4.97	12.0
44.7	7			

Travata: 1051 (Travata 1051) [225 (Nodo 225) ,240 (Nodo 240)]

$L = 131.5\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max} mm	L/250.00 mm	Cs
cm		0.23	5.26	23.3
78.9	5			

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2 mm	L/300.00 mm	Cs
cm		-0.29	4.38	15.3
39.5	7			

Travata: 1008 (Travata 1008) [318 (Nodo 318) ,316 (Nodo 316)]

$L = 137.4\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max} mm	L/250.00 mm	Cs
cm		-0.27	5.50	20.5
68.7	7			

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2 mm	L/300.00 mm	Cs
cm		-0.39	4.58	11.7
68.7	7			

Travata: 1019 (Travata 1019) [316 (Nodo 316), 324 (Nodo 324)]
L = 137.5cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δmax	L/250.00	Cs
cm			mm	mm	
68.8		7	-0.27	5.50	20.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	$\delta 2$	L/300.00	Cs
cm			mm	mm	
68.8		7	-0.39	4.58	11.7

Travata: 1030 (Travata 1030) [324 (Nodo 324), 322 (Nodo 322)]
L = 137.6cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δmax	L/250.00	Cs
cm			mm	mm	
68.8		7	-0.27	5.50	20.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	$\delta 2$	L/300.00	Cs
cm			mm	mm	
68.8		7	-0.39	4.59	11.7

Travata: 1041 (Travata 1041) [322 (Nodo 322), 320 (Nodo 320)]
L = 149.1cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δmax	L/250.00	Cs
cm			mm	mm	
74.5		7	-0.28	5.96	21.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	$\delta 2$	L/300.00	Cs
cm			mm	mm	
74.5		7	-0.45	4.97	11.0

Travata: 1052 (Travata 1052) [320 (Nodo 320), 326 (Nodo 326)]
L = 137.5cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δmax	L/250.00	Cs
cm			mm	mm	
68.7		7	-0.27	5.50	20.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	$\delta 2$	L/300.00	Cs
cm			mm	mm	
68.7		7	-0.39	4.58	11.8

Travata: 1009 (Travata 1009) [317 (Nodo 317), 315 (Nodo 315)]
L = 143.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δmax	L/250.00	Cs
cm			mm	mm	
71.7		7	-0.28	5.74	20.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	$\delta 2$	L/300.00	Cs
cm			mm	mm	
71.7		7	-0.42	4.78	11.3

Travata: 1020 (Travata 1020) [315 (Nodo 315), 323 (Nodo 323)]
L = 143.5cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δmax	L/250.00	Cs
cm			mm	mm	
71.8		7	-0.28	5.74	20.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	$\delta 2$	L/300.00	Cs
cm			mm	mm	
71.8		7	-0.42	4.78	11.3

Travata: 1031 (Travata 1031) [323 (Nodo 323), 321 (Nodo 321)]
L = 143.7cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δmax	L/250.00	Cs
cm			mm	mm	
71.8		7	-0.28	5.75	20.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	$\delta 2$	L/300.00	Cs
cm			mm	mm	
71.8		7	-0.42	4.79	11.3

Travata: 1042 (Travata 1042) [321 (Nodo 321), 319 (Nodo 319)]
L = 149.1cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δmax	L/250.00	Cs
cm			mm	mm	
74.5		7	-0.28	5.96	21.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	$\delta 2$	L/300.00	Cs
cm			mm	mm	
74.5		7	-0.45	4.97	11.0

Travata: 1053 (Travata 1053) [319 (Nodo 319), 325 (Nodo 325)]
L = 143.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δmax	L/250.00	Cs
cm			mm	mm	
71.7		7	-0.27	5.74	20.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	$\delta 2$	L/300.00	Cs
cm			mm	mm	
71.7		7	-0.42	4.78	11.3

Travata: 1010 (Travata 1010) [307 (Nodo 307), 308 (Nodo 308)]
L = 149.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δmax	L/250.00	Cs
cm			mm	mm	
74.7		7	-0.38	5.98	15.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	$\delta 2$	L/300.00	Cs
cm			mm	mm	
74.7		7	-0.48	4.98	10.4

Travata: 1021 (Travata 1021) [308 (Nodo 308) , 309 (Nodo 309)]
*L = 147.4cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata***

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
73.7	7	-0.38	5.89	15.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
73.7	7	-0.47	4.91	10.6

Travata: 1032 (Travata 1032) [309 (Nodo 309) , 310 (Nodo 310)]
*L = 149.3cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata***

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.7	7	-0.38	5.97	15.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.7	7	-0.48	4.98	10.4

Travata: 1043 (Travata 1043) [310 (Nodo 310) , 311 (Nodo 311)]
*L = 148.9cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata***

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.4	7	-0.38	5.95	15.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.4	7	-0.47	4.96	10.5

Travata: 1054 (Travata 1054) [311 (Nodo 311) , 312 (Nodo 312)]
*L = 149.4cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata***

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.7	7	-0.38	5.98	15.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.7	7	-0.48	4.98	10.4

Travata: 1011 (Travata 1011) [101 (Nodo 101) , 102 (Nodo 102)]
*L = 89.4cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata***

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.7	7	-0.16	3.58	22.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
44.7	7	-0.17	2.98	17.0

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Travata: 1022 (Travata 1022) [102 (Nodo 102) , 103 (Nodo 103)]
*L = 89.6cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata***

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.8	7	-0.16	3.58	22.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
44.8	7	-0.18	2.99	17.0

Travata: 1033 (Travata 1033) [103 (Nodo 103) , 104 (Nodo 104)]
*L = 89.1cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata***

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.5	7	-0.15	3.56	23.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
44.5	7	-0.17	2.97	17.1

Travata: 1044 (Travata 1044) [104 (Nodo 104) , 105 (Nodo 105)]
*L = 149.5cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata***

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.7	7	-0.32	5.98	18.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.7	7	-0.46	4.98	10.8

Travata: 1055 (Travata 1055) [105 (Nodo 105) , 106 (Nodo 106)]
*L = 89.9cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata***

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.9	7	-0.16	3.60	22.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
44.9	7	-0.18	3.00	17.0

Travata: 1067 (Travata 1067) [126 (Nodo 126) , 127 (Nodo 127)]
*L = 70.0cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata***

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
35.0	7	-0.23	2.80	12.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
35.0	7	-0.22	2.33	10.6

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Travata: 1057 (Travata 1057) [244 (Nodo 244) , 245 (Nodo 245)]

L = 69.8cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x		mm		
cm	34.9	-0.22	2.79	12.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		δ_2	L/300.00	Cs
x		mm		
cm	34.9	-0.22	2.33	10.7

Travata: 1058 (Travata 1058) [125 (Nodo 125) , 128 (Nodo 128)]

L = 70.0cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x		mm		
cm	35.0	-0.23	2.80	12.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		δ_2	L/300.00	Cs
x		mm		
cm	35.0	-0.22	2.33	10.6

Travata: 1059 (Travata 1059) [243 (Nodo 243) , 246 (Nodo 246)]

L = 69.8cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x		mm		
cm	34.9	-0.22	2.79	12.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		δ_2	L/300.00	Cs
x		mm		
cm	34.9	-0.22	2.33	10.7

Travata: 1060 (Travata 1060) [242 (Nodo 242) , 247 (Nodo 247)]

L = 70.0cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x		mm		
cm	35.0	-0.23	2.80	12.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		δ_2	L/300.00	Cs
x		mm		
cm	35.0	-0.22	2.33	10.6

Travata: 1061 (Travata 1061) [241 (Nodo 241) , 248 (Nodo 248)]

L = 70.0cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x		mm		
cm	35.0	-0.23	2.80	12.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		δ_2	L/300.00	Cs
x		mm		
cm				

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Comb.		δ_2	L/300.00	Cs
x		mm		
cm	35.0	-0.22	2.33	10.6

Travata: 1062 (Travata 1062) [240 (Nodo 240) , 249 (Nodo 249)]

L = 70.0cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x		mm		
cm	35.0	-0.23	2.80	12.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		δ_2	L/300.00	Cs
x		mm		
cm	35.0	-0.22	2.33	10.6

Travata: 1063 (Travata 1063) [326 (Nodo 326) , 327 (Nodo 327)]

L = 70.0cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x		mm		
cm	35.0	-0.11	2.80	25.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		δ_2	L/300.00	Cs
x		mm		
cm	35.0	-0.11	2.33	21.2

Travata: 1064 (Travata 1064) [325 (Nodo 325) , 328 (Nodo 328)]

L = 70.0cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x		mm		
cm	35.0	-0.11	2.80	25.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		δ_2	L/300.00	Cs
x		mm		
cm	35.0	-0.11	2.33	21.2

Travata: 1065 (Travata 1065) [312 (Nodo 312) , 313 (Nodo 313)]

L = 70.0cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x		mm		
cm	35.0	-0.11	2.80	25.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		δ_2	L/300.00	Cs
x		mm		
cm	35.0	-0.11	2.33	21.2

Travata: 1066 (Travata 1066) [106 (Nodo 106) , 114 (Nodo 114)]

L = 82.0cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x		mm		
cm	41.0	0.15	3.28	21.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

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x	Comb.	82	L/300.00	Cs
cm		mm	mm	
41.0	8	0.15	2.73	18.1

Travata: 1056 (Travata 1056) [120 (Nodo 120), 126 (Nodo 126)]

L = 95.8cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
67.1	7	-0.16	3.83	24.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
67.1	7	-0.21	3.19	15.2

Travata: 2001 (Travata 2001) [17 (Nodo 17), 19 (Nodo 19)]

L = 89.0cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.5	8	-0.18	3.56	20.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
44.5	8	-0.18	2.97	16.6

Travata: 2002 (Travata 2002) [19 (Nodo 19), 20 (Nodo 20)]

L = 89.2cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.6	8	-0.18	3.57	20.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
44.6	8	-0.18	2.97	16.6

Travata: 2003 (Travata 2003) [20 (Nodo 20), 15 (Nodo 15)]

L = 101.8cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
50.9	8	-0.23	4.07	17.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
50.9	8	-0.23	3.39	14.5

Travata: 2004 (Travata 2004) [15 (Nodo 15), 16 (Nodo 16)]

L = 149.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.7	7	-0.49	5.98	12.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
74.7	8	-0.50	4.98	9.91

Travata: 2005 (Travata 2005) [16 (Nodo 16), 18 (Nodo 18)]

L = 89.8cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.9	8	-0.18	3.59	20.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
44.9	8	-0.18	2.99	16.5

Travata: 2006 (Travata 2006) [25 (Nodo 25), 26 (Nodo 26)]

L = 89.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.7	4	0.00	3.58	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
0.0	8	-0.00	2.98	>100

Travata: 2007 (Travata 2007) [26 (Nodo 26), 23 (Nodo 23)]

L = 85.2cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
42.6	2	0.00	3.41	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
0.0	8	-0.00	2.84	>100

Travata: 2008 (Travata 2008) [23 (Nodo 23), 24 (Nodo 24)]

L = 88.8cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.4	6	0.00	3.55	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
0.0	8	-0.00	2.96	>100

Travata: 2009 (Travata 2009) [24 (Nodo 24), 21 (Nodo 21)]

L = 161.6cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
80.8	8	0.02	6.47	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
0.0	8	-0.00	5.39	>100

Travata: 2010 (Travata 2010) [21 (Nodo 21) , 22 (Nodo 22)]

L = 89.9cm Crit.Prog: Acciaio Flessione δc = 0.0cm Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
44.9	1	0.00	3.60	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
0.0	8	-0.00	3.00	>100

Verifica delle travi (Stati limite esercizio)

scenario di calcolo : Set_NT_SLD A2 STR/GEO

Trave di Fond. : 9001 | 2 , 1 | Pilastrate [2 , 1]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.4 cm Ln= 101.4 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: scalc[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σc-	σf+	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	3741	1374	12.06	12.06	-6	345	-2	127	6	8	Si	10.4
10.1	3408	1368	12.06	12.06	-5	314	-2	126	6	8	Si	11.5
50.7	2097	874	12.06	12.06	-3	193	-1	81	6	5	Si	18.6
91.3	793	--	12.06	12.06	-1	73	--	--	6	5	Si	49.3
101.4	887	--	12.06	12.06	-1	82	--	--	8	6	Si	44.0

Combinazione QP: scalc[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σc-	σf+	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	103	12.06	12.06	--	--	9	-0	14	14	Si	>100
10.1	--	232	12.06	12.06	--	--	21	-0	14	14	Si	>100
50.7	--	408	12.06	12.06	--	--	1	-1	38	14	Si	95.7
91.3	19	--	12.06	12.06	-0	2	--	--	14	14	Si	>100
101.4	229	--	12.06	12.06	-0	21	--	--	14	14	Si	>100

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	M	Act	Aft	pAft	S_rmax	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	97	0.1	12.06	30.16	22.4	9	0.001	0.001	10(Fr)	Si	>100
0.0	103	0.1	12.06	30.16	22.4	9	0.001	0.001	14(Op)	Si	>100
10.1	232	0.1	12.06	30.16	22.4	21	0.001	0.001	14(Op)	Si	>100
10.1	232	0.1	12.06	30.16	22.4	21	0.001	0.001	9(Fr)	Si	>100
50.7	408	0.1	12.06	30.16	22.4	38	0.002	0.002	14(Op)	Si	>100
50.7	-132	0.1	12.06	30.16	22.4	12	0.001	0.001	12(Fr)	Si	>100
91.3	-19	0.1	12.06	30.16	22.4	2	0.000	0.000	14(Op)	Si	>100
91.3	-17	0.1	12.06	30.16	22.4	2	0.000	0.000	11(Fr)	Si	>100
101.4	-229	0.1	12.06	30.16	22.4	21	0.001	0.001	14(Op)	Si	>100
101.4	-201	0.1	12.06	30.16	22.4	19	0.001	0.001	12(Fr)	Si	>100

Trave di Fond. : 9001 | 3 , 2 | Pilastrate [3 , 2]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.6 cm Ln= 89.6 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: scalc[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σc-	σf+	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	404	1213	12.06	12.06	-1	37	-2	112	6	8	Si	32.2
9.0	787	1364	12.06	12.06	-1	72	-2	126	6	8	Si	28.6
44.8	2420	1608	12.06	12.06	-4	223	-2	148	6	8	Si	16.1
80.6	4175	1268	12.06	12.06	-6	385	-2	117	6	8	Si	9.35
89.6	4627	1090	12.06	12.06	-7	426	-2	100	6	8	Si	8.44

Combinazione QP: scalc[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σc-	σf+	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	7	--	12.06	12.06	-0	1	--	--	14	14	Si	>100
9.0	--	106	12.06	12.06	--	--	-0	10	14	14	Si	>100
44.8	--	338	12.06	12.06	--	--	-1	31	14	14	Si	>100
80.6	--	204	12.06	12.06	--	--	-0	19	14	14	Si	>100
89.6	--	110	12.06	12.06	--	--	-0	10	14	14	Si	>100

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	M	Act	Mq	Afup	Afntf	pAft	S _{max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m			cmq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-7	0.1	12.06	30.16	22.4	1	0.000	1	0.000	0.000	9(Fr)	Si	>100
0.0	-7	0.1	12.06	30.16	22.4	1	0.000	1	0.000	0.000	14(Qp)	Si	>100
9.0	106	0.1	12.06	30.16	22.4	10	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
9.0	84	0.1	12.06	30.16	22.4	8	0.000	0.000	0.000	0.000	10(Fr)	Si	>100
44.8	338	0.1	12.06	30.16	22.4	31	0.002	0.002	0.002	0.002	14(Qp)	Si	>100
44.8	-329	0.1	12.06	30.16	22.4	30	0.002	0.002	0.002	0.002	12(Fr)	Si	>100
80.6	204	0.1	12.06	30.16	22.4	19	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
80.6	203	0.1	12.06	30.16	22.4	19	0.001	0.001	0.001	0.001	10(Fr)	Si	>100
89.6	110	0.1	12.06	30.16	22.4	10	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
89.6	106	0.1	12.06	30.16	22.4	10	0.001	0.001	0.001	0.001	10(Fr)	Si	>100

Trave di Fond.: 9001 | 4. 3 | Pilastro [4. 3]

Sez. R: By= 60.0 cm Bz= 100.0 cm L=89.2 cm Ln=89.2 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Act	Mq	Afup	Afntf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m			cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1109	1913	12.06	12.06	-2	102	-3	176	6	8	8	8	Si	20.4
8.9	1044	1969	12.06	12.06	-2	96	-3	181	6	8	8	8	Si	19.8
44.6	1018	1852	12.06	12.06	-2	94	-3	171	6	8	8	8	Si	21.1
80.3	1297	1185	12.06	12.06	-2	120	-2	109	6	8	8	8	Si	30.1
89.2	1404	931	12.06	12.06	-2	129	-1	86	6	8	8	8	Si	27.8

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	Act	Mq	Afup	Afntf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m			cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	233	12.06	12.06	--	--	--	21	14	14	14	14	Si	>100
8.9	--	296	12.06	12.06	--	--	--	27	14	14	14	14	Si	>100
44.6	--	342	12.06	12.06	--	--	--	32	14	14	14	14	Si	>100
80.3	--	58	12.06	12.06	--	--	--	5	14	14	14	14	Si	>100
89.2	65	--	12.06	12.06	-0	6	--	--	14	14	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Mq	Afup	Afntf	pAft	S _{max}	σfmed	Wd	Wk	Cb+	Cb-	Ver.	Cs
cm	kg*m			cmq	cmq	cm	cm	kg/cmq	mm	mm				
0.0	-192	0.1	12.06	30.16	22.4	18	0.001	18	0.001	0.001	12(Fr)	Si	>100	
0.0	233	0.1	12.06	30.16	22.4	21	0.001	21	0.001	0.001	14(Qp)	Si	>100	
8.9	296	0.1	12.06	30.16	22.4	27	0.002	0.002	0.002	0.002	14(Qp)	Si	>100	
8.9	-125	0.1	12.06	30.16	22.4	12	0.001	0.001	0.001	0.001	12(Fr)	Si	>100	
44.6	342	0.1	12.06	30.16	22.4	32	0.002	0.002	0.002	0.002	14(Qp)	Si	>100	
44.6	-59	0.1	12.06	30.16	22.4	5	0.000	0.000	0.000	0.000	12(Fr)	Si	>100	
80.3	58	0.1	12.06	30.16	22.4	5	0.000	0.000	0.000	0.000	14(Qp)	Si	>100	
80.3	31	0.1	12.06	30.16	22.4	3	0.000	0.000	0.000	0.000	10(Fr)	Si	>100	
89.2	-65	0.1	12.06	30.16	22.4	6	0.000	0.000	0.000	0.000	14(Qp)	Si	>100	
89.2	27	0.1	12.06	30.16	22.4	2	0.000	0.000	0.000	0.000	11(Fr)	Si	>100	

Trave di Fond.: 9001 | 5. 4 | Pilastro [5. 4]

Sez. R: By= 60.0 cm Bz= 100.0 cm L=149.5 cm Ln=149.5 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Act	Mq	Afup	Afntf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m			cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	6222	12.06	12.06	--	--	--	573	5	6	6	6	Si	6.28
14.9	--	5941	12.06	12.06	--	--	--	548	5	6	6	6	Si	6.58
74.7	--	3460	12.06	12.06	--	--	--	319	4	6	6	6	Si	11.3
134.5	802	1886	12.06	12.06	-1	74	-3	174	6	8	8	8	Si	20.7
149.5	2089	1514	12.06	12.06	-3	193	-2	140	6	8	8	8	Si	18.7

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	Act	Mq	Afup	Afntf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m			cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				

X	M+	M-	Act	Mq	Afup	Afntf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
0.0	--	399	12.06	12.06	12.06	12.06	--	--	-1	37	14	14	Si	98.0
14.9	--	662	12.06	12.06	12.06	12.06	--	--	-1	61	14	14	Si	59.0
74.7	--	1076	12.06	12.06	12.06	12.06	--	--	-2	99	14	14	Si	36.3
134.5	--	508	12.06	12.06	12.06	12.06	--	--	-1	47	14	14	Si	77.0
149.5	--	218	12.06	12.06	12.06	12.06	--	--	-0	20	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Mq	Afup	Afntf	pAft	S _{max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m			cmq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	360	0.1	12.06	30.16	22.4	33	0.002	0.002	0.002	0.002	11(Fr)	Si	>100
0.0	399	0.1	12.06	30.16	22.4	37	0.002	0.002	0.002	0.002	14(Qp)	Si	>100
14.9	662	0.1	12.06	30.16	22.4	61	0.004	0.004	0.004	0.004	14(Qp)	Si	76.9
14.9	662	0.1	12.06	30.16	22.4	61	0.004	0.004	0.004	0.004	9(Fr)	Si	>100
74.7	1076	0.1	12.06	30.16	22.4	99	0.006	0.006	0.006	0.006	14(Qp)	Si	47.3
74.7	1076	0.1	12.06	30.16	22.4	99	0.006	0.006	0.006	0.006	9(Fr)	Si	63.1
134.5	508	0.1	12.06	30.16	22.4	47	0.003	0.003	0.003	0.003	14(Qp)	Si	>100
134.5	131	0.1	12.06	30.16	22.4	12	0.001	0.001	0.001	0.001	12(Fr)	Si	>100
149.5	218	0.1	12.06	30.16	22.4	20	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
149.5	198	0.1	12.06	30.16	22.4	18	0.001	0.001	0.001	0.001	10(Fr)	Si	>100

Trave di Fond.: 9001 | 6. 5 | Pilastro [6. 5]

Sez. R: By= 60.0 cm Bz= 100.0 cm L=89.9 cm Ln=101.9 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Act	Mq	Afup	Afntf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m			cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	131	120	12.06	12.06	12.06	12.06	-0	12	-0	11	5	7	Si	>100
10.2	--	827	12.06	12.06	12.06	12.06	--	--	-1	76	5	6	Si	47.2
50.9	--	3652	12.06	12.06	12.06	12.06	--	--	-6	337	5	6	Si	10.7
91.7	--	5068	12.06	12.06	12.06	12.06	--	--	-8	467	5	6	Si	7.71
101.9	--	5228	12.06	12.06	12.06	12.06	--	--	-8	482	5	6	Si	7.47

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	Act	Mq	Afup	Afntf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m			cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	230	--	12.06	12.06	12.06	12.06	-0	21	--	--	14	14	Si	>100
10.2	13	--	12.06	12.06	12.06	12.06	-0	1	--	--	14	14	Si	>100
50.9	--	497	12.06	12.06	12.06	12.06	--	--	-1	46	14	14	Si	78.6
91.7	--	467	12.06	12.06	12.06	12.06	--	--	-1	43	14	14	Si	83.7
101.9	--	379	12.06	12.06	12.06	12.06	--	--	-1	35	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	cm	M ⁺ kg·m	Act	mq	Aft	cmq	cm	S _{max}	σ _f med	Wd	Wk	Cb	Ver.	Cs
					pAft	cm	cm		kg/cmq	mm	mm			
	0.0	-144	0.1	12.06	30.16	22.4	13	0.001	0.001	0.001	0.001	13(Fr)	Si	>100
	0.0	-230	0.1	12.06	30.16	22.4	21	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
	10.2	-13	0.1	12.06	30.16	22.4	1	0.000	0.000	0.000	0.000	14(Qp)	Si	>100
	10.2	-12	0.1	12.06	30.16	22.4	1	0.000	0.000	0.000	0.000	10(Fr)	Si	>100
	50.9	497	0.1	12.06	30.16	22.4	46	0.003	0.003	0.003	0.003	14(Qp)	Si	>100
	50.9	495	0.1	12.06	30.16	22.4	46	0.003	0.003	0.003	0.003	11(Fr)	Si	>100
	91.7	467	0.1	12.06	30.16	22.4	43	0.003	0.003	0.003	0.003	14(Qp)	Si	>100
	91.7	451	0.1	12.06	30.16	22.4	42	0.003	0.003	0.003	0.003	11(Fr)	Si	>100
	101.9	379	0.1	12.06	30.16	22.4	35	0.002	0.002	0.002	0.002	14(Qp)	Si	>100
	101.9	355	0.1	12.06	30.16	22.4	33	0.002	0.002	0.002	0.002	11(Fr)	Si	>100

X	M+	M-	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
16.1	1208	--	--	12.06	12.06	-2	111	--	--	6	5	Si	32.3
80.7	3199	1425	-5	12.06	12.06	-2	295	-2	131	6	5	Si	12.2
145.3	4831	2660	12.06	12.06	12.06	-7	445	-4	245	6	8	Si	8.08
161.4	5220	2864	12.06	12.06	12.06	-8	481	-4	264	6	8	Si	7.48

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cm	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	161	--	--	12.06	12.06	-4	15	--	--	14	14	Si	>100
16.1	--	58	12.06	12.06	12.06	--	--	-0	5	14	14	Si	>100
80.7	--	684	12.06	12.06	12.06	--	--	-1	63	14	14	Si	57.1
145.3	--	855	12.06	12.06	12.06	--	--	-1	79	14	14	Si	45.7
161.4	--	818	12.06	12.06	12.06	--	--	-1	75	14	14	Si	47.8

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Mq	cmq	pAlt	S _{max}	σf _{ed}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	mm	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-161	0.1	12.06	30.16	22.4	15	0.001	0.001	0.001	9(Fr)	Si	>100
0.0	-161	0.1	12.06	30.16	22.4	15	0.001	0.001	0.001	14(Qp)	Si	>100
16.1	58	0.1	12.06	30.16	22.4	5	0.000	0.000	0.000	14(Qp)	Si	>100
16.1	-30	0.1	12.06	30.16	22.4	3	0.000	0.000	0.000	13(Fr)	Si	>100
80.7	684	0.1	12.06	30.16	22.4	63	0.004	0.004	0.004	14(Qp)	Si	74.4
80.7	-156	0.1	12.06	30.16	22.4	14	0.001	0.001	0.001	12(Fr)	Si	>100
145.3	855	0.1	12.06	30.16	22.4	79	0.005	0.005	0.005	14(Qp)	Si	59.6
145.3	-452	0.1	12.06	30.16	22.4	42	0.003	0.003	0.003	12(Fr)	Si	>100
161.4	818	0.1	12.06	30.16	22.4	75	0.005	0.005	0.005	14(Qp)	Si	62.3
161.4	-584	0.1	12.06	30.16	22.4	54	0.003	0.003	0.003	12(Fr)	Si	>100

Trave di Fond.: 9002 | 208, 209 | Pilastro [208, 209]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.5 cm Terreno: TerrenoI

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg* π m	kg* π m	cm μ	cm μ	kg/cm μ	kg/cm μ	kg/cm μ	kg/cm μ				
0.0	6371	2465	12.06	12.06	-10	587	-4	227	6	8	Si	6.13
14.9	5798	2863	12.06	12.06	-9	534	-4	264	6	5	Si	6.74
74.7	3568	4029	12.06	12.06	-6	329	-6	371	6	5	Si	9.69
134.5	1536	4285	12.06	12.06	-2	142	-7	395	6	5	Si	9.11
149.5	1073	4196	12.06	12.06	-2	99	-6	387	6	5	Si	9.31

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	817	12.06	12.06	--	--	--	-1	75	14	14	Si	47.8
14.9	--	1004	12.06	12.06	--	--	--	-2	93	14	14	Si	38.9
74.7	--	1456	12.06	12.06	--	--	--	-2	134	14	14	Si	26.8
134.5	--	1426	12.06	12.06	--	--	--	-2	131	14	14	Si	27.4
149.5	--	1341	12.06	12.06	--	--	--	-2	124	14	14	Si	29.1

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAlt	S _{max}	σ _f	Wd	Wk	Cb	Ver.	Cs
cm	kg·m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-764	0.1	12.06	30.16	22.4	70	0.005	0.005	12(Fr)	Si	88.9
0.0	817	0.1	12.06	30.16	22.4	75	0.005	0.005	14(Qp)	Si	62.3
14.9	1004	0.1	12.06	30.16	22.4	93	0.006	0.006	14(Qp)	Si	50.7
14.9	-509	0.1	12.06	30.16	22.4	47	0.003	0.003	12(Fr)	Si	>100
74.7	1456	0.1	12.06	30.16	22.4	134	0.009	0.009	14(Qp)	Si	35.0
74.7	273	0.1	12.06	30.16	22.4	25	0.002	0.002	12(Fr)	Si	>100
134.5	1426	0.1	12.06	30.16	22.4	131	0.008	0.008	14(Qp)	Si	35.7
134.5	648	0.1	12.06	30.16	22.4	60	0.004	0.004	12(Fr)	Si	>100
149.5	1341	0.1	12.06	30.16	22.4	124	0.008	0.008	14(Qp)	Si	38.0
149.5	674	0.1	12.06	30.16	22.4	62	0.004	0.004	12(Fr)	Si	>100

Trave di Fond.: 9002 | 209, 210 | Pilastro [209, 210]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.7 cm Terreno: TerrenoI

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	2240	3812	12.06	12.06	12.06	-3	206	-6	351	6	5	Si	10.2
15.0	1532	4074	12.06	12.06	12.06	-2	141	-6	375	6	5	Si	9.59
74.9	--	4491	12.06	12.06	--	--	--	-7	414	6	5	Si	8.70
134.8	--	3930	12.06	12.06	--	--	--	-6	362	7	5	Si	9.94
149.7	--	3674	12.06	12.06	--	--	--	-6	339	7	6	Si	10.6

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	1332	12.06	12.06	12.06	--	--	-2	123	14	14	Si	29.3
15.0	--	1468	12.06	12.06	12.06	--	--	-2	135	14	14	Si	26.6
74.9	--	1700	12.06	12.06	12.06	--	--	-3	157	14	14	Si	23.0
134.8	--	1445	12.06	12.06	12.06	--	--	-2	133	14	14	Si	27.0
149.7	--	1306	12.06	12.06	12.06	--	--	-2	120	14	14	Si	29.9

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	cm	M	kg*m	Act	mq	Alt	cmq	pAlt	cm	S _{max}	cm	kg/cmq	Wd	mm	Wk	mm	Cb	Ver.	Cs
	0.0	502	0.1	12.06	30.16	22.4	46	0.003	0.003	0.003	0.003	12(Fr)	Si	>100					
	0.0	1332	0.1	12.06	30.16	22.4	123	0.008	0.008	0.008	0.008	14(Qp)	Si	38.2	0.009	0.009	14(Qp)	Si	34.7
	15.0	1468	0.1	12.06	30.16	22.4	135	0.009	0.009	0.009	0.009	14(Qp)	Si	91.0	0.004	0.004	12(Fr)	Si	30.0
	74.9	1700	0.1	12.06	30.16	22.4	157	0.010	0.010	0.010	0.010	14(Qp)	Si	30.0	0.008	0.008	12(Fr)	Si	47.1
	74.9	1441	0.1	12.06	30.16	22.4	133	0.008	0.008	0.008	0.008	14(Qp)	Si	35.2	0.009	0.009	14(Qp)	Si	35.2
	134.8	1445	0.1	12.06	30.16	22.4	133	0.009	0.009	0.009	0.009	9(Fr)	Si	47.0	0.008	0.008	9(Fr)	Si	47.0
	149.7	1306	0.1	12.06	30.16	22.4	120	0.008	0.008	0.008	0.008	14(Qp)	Si	39.0	0.008	0.008	14(Qp)	Si	39.0
	149.7	1306	0.1	12.06	30.16	22.4	120	0.008	0.008	0.008	0.008	9(Fr)	Si	52.0	0.008	0.008	9(Fr)	Si	52.0

Trave di Fond.: 9002 | 210, 211 | Pilastro [210, 211]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.0 cm Terreno: TerrenoI

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	3309	12.06	12.06	12.06	--	--	-5	305	7	5	Si	11.8
14.9	--	3365	12.06	12.06	12.06	--	--	-5	310	7	5	Si	11.6
74.5	--	5641	12.06	12.06	12.06	--	--	-9	520	8	6	Si	6.92
134.1	--	7343	12.06	12.06	12.06	--	--	-11	677	8	6	Si	5.32
149.0	--	7635	12.06	12.06	12.06	--	--	-12	704	8	6	Si	5.12

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	1288	12.06	12.06	12.06	--	--	-2	119	14	14	Si	30.3
14.9	--	1367	12.06	12.06	12.06	--	--	-2	126	14	14	Si	28.6
74.5	--	1386	12.06	12.06	12.06	--	--	-2	128	14	14	Si	28.2
134.1	--	948	12.06	12.06	12.06	--	--	-1	87	14	14	Si	41.2
149.0	--	768	12.06	12.06	12.06	--	--	-1	71	14	14	Si	50.9

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	σ _{f_{ed}}	Wd	Wk	Cb	Ver.	Cs
cm	kg·m	mq	cmq	cm	cm	mm	mm	mm			
0.0	1288	0.1	12.06	30.16	22.4	119	0.008	0.008	9(Fr)	Si	52.7
0.0	1288	0.1	12.06	30.16	22.4	119	0.008	0.008	14(Qp)	Si	39.5
14.9	1367	0.1	12.06	30.16	22.4	126	0.008	0.008	14(Qp)	Si	37.3
14.9	1367	0.1	12.06	30.16	22.4	126	0.008	0.008	9(Fr)	Si	49.7

X	M	Act	Aft	pAft	S _{max}	σfmed	Wd	Wk	Cb	Ver.	Cs
74.5	1386	0.1	12.06	30.16	22.4	128	0.008	0.008	14(Qp)	Si	36.8
74.5	1379	0.1	12.06	30.16	22.4	127	0.008	0.008	13(Fr)	Si	49.2
134.1	948	0.1	12.06	30.16	22.4	87	0.006	0.006	14(Qp)	Si	53.8
134.1	919	0.1	12.06	30.16	22.4	85	0.005	0.005	13(Fr)	Si	73.9
149.0	768	0.1	12.06	30.16	22.4	71	0.005	0.005	14(Qp)	Si	66.3
149.0	732	0.1	12.06	30.16	22.4	67	0.004	0.004	13(Fr)	Si	92.7

Trave di Fond. : 9002 | 211 . 212 | Pilastro [211 . 212]

Sec. R: By= 60.0 cm Bz= 100.0 cm Bz= 100.0 cm L= 149.4 cm Ln= 161.4 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Alsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	6527	12.06	12.06	--	--	-10	602	8	6	Si	5.98
16.1	--	6313	12.06	12.06	--	--	-10	582	8	6	Si	6.19
80.7	--	4635	12.06	12.06	--	--	-7	427	8	6	Si	8.43
145.2	--	1342	12.06	12.06	--	--	-2	124	5	6	Si	29.1
161.4	--	431	12.06	12.06	--	--	-1	40	5	7	Si	90.5

Combinazione OP: σca[kg/cmq]= 112 σfa[kg/cmq]=3600

X	M+	M-	Alsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	781	12.06	12.06	--	--	-1	72	14	14	Si	50.0
16.1	--	828	12.06	12.06	--	--	-1	76	14	14	Si	47.2
80.7	--	695	12.06	12.06	--	--	-1	64	14	14	Si	56.2
145.2	--	67	12.06	12.06	--	--	-0	6	14	14	Si	>100
161.4	166	--	12.06	12.06	-0	15	--	--	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	647	0.1	12.06	30.16	22.4	60	0.004	0.004	13(Fr)	Si	>100
0.0	781	0.1	12.06	30.16	22.4	72	0.005	0.005	14(Qp)	Si	65.2
16.1	828	0.1	12.06	30.16	22.4	76	0.005	0.005	14(Qp)	Si	61.5
16.1	717	0.1	12.06	30.16	22.4	66	0.004	0.004	13(Fr)	Si	94.7
80.7	695	0.1	12.06	30.16	22.4	64	0.004	0.004	14(Qp)	Si	73.3
80.7	677	0.1	12.06	30.16	22.4	62	0.004	0.004	13(Fr)	Si	>100
145.2	67	0.1	12.06	30.16	22.4	6	0.000	0.000	14(Qp)	Si	>100
145.2	65	0.1	12.06	30.16	22.4	6	0.000	0.000	11(Fr)	Si	>100
161.4	-166	0.1	12.06	30.16	22.4	15	0.001	0.001	14(Qp)	Si	>100
161.4	-57	0.1	12.06	30.16	22.4	5	0.000	0.000	13(Fr)	Si	>100

TABULATI DI INPUT - Portali DA 8 a 14

Dati generali											
Nome struttura											
Temperatura di riferimento [°C]											
Fattore rigidità assiale pilastri											
Numero di frequenze											
% Filtro masse libere											
% Coefficiente di smorzamento viscoso											
Spostamenti nodali con segno											
Deformabilità a taglio delle aste											
Impalcati deformabili per carichi termici											
Spostamento ammissibile impalcati											
0.0050*h											

Impalcati					
N°	Quota	mm	Rigido	Incr Soil Pil	Inc Soil Par.
0			0	No	1.000
1		5420	No	No	1.000
2		9510	No	No	1.000
3		13230	No	No	1.000

Percentuali Spostamento masse impalcati		
Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0

Combinazioni del Sisma in X e Y e Verticale					
Comb	Pos. SismaX	Pos. SismaY	Fx	Fy	Fz
1	1	2	1	0.3	0.3
2	1	2	0.3	1	0.3
3	1	4	1	0.3	0.3
4	1	4	0.3	1	0.3
5	3	2	1	0.3	0.3
6	3	2	0.3	1	0.3
7	3	4	1	0.3	0.3
8	3	4	0.3	1	0.3
9	1	2	0.3	0.3	1
10	1	4	0.3	0.3	1
11	3	2	0.3	0.3	1
12	3	4	0.3	0.3	1

Comb = Numero di combinazione dei sismi

Pos. SismaX = Posizione in cui viene scelto il sisma in direzione X

Pos. SismaY = Posizione in cui viene scelto il sisma in direzione Y

Fx = Fattore con cui il sisma X partecipa

Fy = Fattore con cui il sisma Y partecipa

Fz = Fattore con cui il sisma Verticale partecipa (quando richiesto)

Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx ed Fy ed Fz

Spettri di risposta

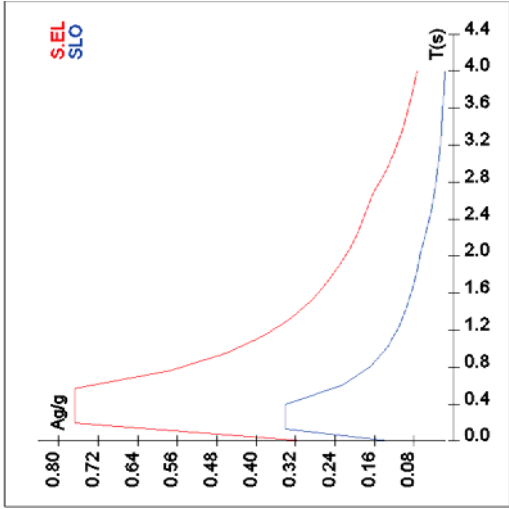
Spettro :SpettroNT(q=1)

Il calcolo degli spettri e del fattore di struttura sono stati calcolati per la seguente tipologia di terreno e struttura

Vita della struttura	Ponti imp. strategica (>100) >=100 anni
Tipo	100.0
Vita nominale(anni)	Classe IV
Classe d'uso	2.000
Coefficiente d'uso	200.000
Periodo di riferimento(anni)	PVR=81.0%
Stato limite di esercizio - SLO	PVR=10.0%
Stato limite ultimo - SLV	TR=120.4
Periodo di ritorno SLO(anni)	TR=1898.2
Periodo di ritorno SLV(anni)	
Parametri del sito	
Comune	Biancavilla - (CT)
Longitudine	14.865
Latitudine	37.646
Id reticolo del sito	47419-47197-47196-47418
Valori di riferimento del sito	
Agg(TR=120.4) SLO	0.1103
F0(TR=120.4) SLO	2.5726
T°C(TR=120.4) SLO	0.281
Agg(TR=1898.2) SLV	0.2704
F0(TR=1898.2) SLV	2.5180
T°C(TR=1898.2) SLV	0.441
Coefficiente Amplificazione Topografica	SI=1.000
Categoria terreno B	
stato limite SLV	
	S=1.13
	TB=0.19
	TC=0.57
	TD=2.68
stato limite SLO	
	S=1.20
	TB=0.13
	TC=0.40
	TD=2.04
Spettro Elastico	
Smorzamento viscoso %	q=1 (struttura NON dissipativa)
	5.0

T	EL [s]	EL [a.g]	TSLO [s]	SLO [a.g]
0.00000	0.30491	0.00000	0.00000	0.13236
0.19040	0.76776	0.13299	0.13299	0.34050
0.57119	0.76776	0.39896	0.39896	0.34050
0.76304	0.57472	0.60424	0.22482	0.22482
0.95489	0.45925	0.80952	0.16781	0.16781
1.14675	0.38242	1.01479	0.13387	0.13387
1.33860	0.32761	1.22007	0.11134	0.11134
1.53045	0.28654	1.42535	0.09531	0.09531
1.72231	0.25462	1.63063	0.08331	0.08331
1.91416	0.22910	1.83591	0.07399	0.07399
2.10602	0.20823	2.04119	0.06655	0.06655
2.29787	0.19084	2.25883	0.05435	0.05435
2.48972	0.17614	2.47648	0.04521	0.04521
2.68158	0.16354	2.69412	0.03870	0.03870
2.90131	0.13970	2.91177	0.03270	0.03270
3.12105	0.12072	3.12942	0.02831	0.02831
3.34079	0.10537	3.34706	0.02475	0.02475

3.56053	0.09276	3.56471	0.02182
3.78026	0.08229	3.78235	0.01938
4.00000	0.07350	4.00000	0.01733



Caratteristiche del terreno

Terreno1- Cost. Winkler=10.00 kg/cm2 Falda assente									
Strato n°	Spessore cm	γ kg/mc	γSat kg/mc	φ °	Addensato	OCR	Coesione kg/cmq	Cu kg/cmq	v
1	100	1900	1900	35	No	--	0.00	0.00	2E02 0.30

Materiali

Materiale: C25/30		
Peso specifico	kg/mc	2500
Modulo di Young E	kg/cmq	3E05
Modulo di Poisson ν		0.13
Coefficiente di dilatazione termica λ	1/°C	1e-005
Materiale: Acciaio		
Peso specifico	kg/mc	7850
Modulo di Young E	kg/cmq	2E06
Modulo di Poisson ν		0.30
Coefficiente di dilatazione termica λ	1/°C	1.2e-005

Nodi - Geometria e vincoli

Nodo	Coordinate [mm]			Tx			Ty			Tz			Rx			Ry			Rz			Impalcato
	X	Y	Z	V	W	U	V	W	U	V	W	U	V	W	U	V	W	U	V	W	U	
1	9390	5450	0	1	1	0	0	0	0	1	1	0	0	0	1	1	0	0	1	1	0	0
2	8830	6840	0	1	1	0	0	0	0	1	1	0	0	0	1	1	0	0	1	1	0	0
3	8510	7670	0	1	1	0	0	0	0	1	1	0	0	0	1	1	0	0	1	1	0	0
4	8240	8530	0	1	1	0	0	0	0	1	1	0	0	0	1	1	0	0	1	1	0	0
5	8020	9390	0	1	1	0	0	0	0	1	1	0	0	0	1	1	0	0	1	1	0	0
6	7700	10850	0	1	1	0	0	0	0	1	1	0	0	0	1	1	0	0	1	1	0	0

7	7370	12310	0	1	1	0	0	0	0	1	0	0
15	8830	6840	2710	0	0	0	0	0	0	0	0	0
16	8830	6840	4065	0	0	0	0	0	0	0	0	0
17	8510	7670	2710	0	0	0	0	0	0	0	0	0
18	8510	7670	4065	0	0	0	0	0	0	0	0	0
19	9390	5450	2710	0	0	0	0	0	0	0	0	0
20	9390	5450	4065	0	0	0	0	0	0	0	0	0
21	8020	9390	2710	0	0	0	0	0	0	0	0	0
22	8020	9390	4065	0	0	0	0	0	0	0	0	0
23	7700	10850	2710	0	0	0	0	0	0	0	0	0
24	7700	10850	4065	0	0	0	0	0	0	0	0	0
25	8240	8530	2710	0	0	0	0	0	0	0	0	0
26	8240	8530	4065	0	0	0	0	0	0	0	0	0
27	7370	12310	2710	0	0	0	0	0	0	0	0	0
28	7370	12310	4065	0	0	0	0	0	0	0	0	0
101	9390	5450	5420	0	0	0	0	0	0	0	1	1
102	8830	6840	5420	0	0	0	0	0	0	0	0	1
103	8510	7670	5420	0	0	0	0	0	0	0	0	1
104	8240	8530	5420	0	0	0	0	0	0	0	0	1
105	8020	9390	5420	0	0	0	0	0	0	0	0	1
106	7700	10850	5420	0	0	0	0	0	0	0	0	1
107	7370	12310	5420	0	0	0	0	0	0	0	0	1
115	7201	8234	6880	0	0	0	0	0	0	0	0	1
116	6162	7938	8290	0	0	0	0	0	0	0	0	1
117	6316	12073	6880	0	0	0	0	0	0	0	0	1
118	5262	11836	8290	0	0	0	0	0	0	0	0	1
119	8391	5042	6880	0	0	0	0	0	0	0	0	1
120	7392	4634	8290	0	0	0	0	0	0	0	0	1
121	7489	7318	6880	0	0	0	0	0	0	0	0	1
122	6468	6966	8290	0	0	0	0	0	0	0	0	1
123	7830	6431	6880	0	0	0	0	0	0	0	0	1
124	6830	6022	8290	0	0	0	0	0	0	0	0	1
125	6967	9153	6880	0	0	0	0	0	0	0	0	1
126	5914	8916	8290	0	0	0	0	0	0	0	0	1
127	6646	10613	6880	0	0	0	0	0	0	0	0	1
128	5592	10376	8290	0	0	0	0	0	0	0	0	1
208	-600	1370	9510	1	1	0	0	0	0	1	1	2
209	-1170	2750	9510	1	1	0	0	0	0	1	1	2
210	-1700	4150	9510	1	1	0	0	0	0	1	1	2
211	-2150	5570	9510	1	1	0	0	0	0	1	1	2
212	-2510	7020	9510	1	1	0	0	0	0	1	1	2
213	-2840	8480	9510	1	1	0	0	0	0	1	1	2
214	-3170	9940	9510	1	1	0	0	0	0	1	1	2
215	5123	7642	9600	0	0	0	0	0	0	0	0	1
216	4084	7346	10760	0	0	0	0	0	0	0	0	1
217	3045	7050	11770	0	0	0	0	0	0	0	0	1
218	2006	6754	12570	0	0	0	0	0	0	0	0	1
219	967	6458	13150	0	0	0	0	0	0	0	0	1
220	4208	11599	9600	0	0	0	0	0	0	0	0	1
221	3154	11362	10760	0	0	0	0	0	0	0	0	1
222	2100	11125	11770	0	0	0	0	0	0	0	0	1
223	1046	10888	12570	0	0	0	0	0	0	0	0	1
224	-8	10651	13150	0	0	0	0	0	0	0	0	1
225	6393	4226	9600	0	0	0	0	0	0	0	0	1
226	5394	3818	10760	0	0	0	0	0	0	0	0	1
227	4395	3410	11770	0	0	0	0	0	0	0	0	1
228	3396	3002	12570	0	0	0	0	0	0	0	0	1
229	2397	2594	13150	0	0	0	0	0	0	0	0	1
230	5447	6614	9600	0	0	0	0	0	0	0	0	1
231	4426	6262	10760	0	0	0	0	0	0	0	0	1
232	3405	5910	11770	0	0	0	0	0	0	0	0	1
233	2384	5558	12570	0	0	0	0	0	0	0	0	1
234	1363	5206	13150	0	0	0	0	0	0	0	0	1
235	5830	5613	9600	0	0	0	0	0	0	0	0	1
236	4830	5204	10760	0	0	0	0	0	0	0	0	1
237	3830	4795	11770	0	0	0	0	0	0	0	0	1
238	2830	4386	12570	0	0	0	0	0	0	0	0	1

239	1830	3977	13150	0	0	0	0	0	0	0	0	1
240	4861	8679	9600	0	0	0	0	0	0	0	0	1
241	3808	8442	10760	0	0	0	0	0	0	0	0	1
242	2755	8205	11770	0	0	0	0	0	0	0	0	1
243	1702	7968	12570	0	0	0	0	0	0	0	0	1
244	649	7731	13150	0	0	0	0	0	0	0	0	1
245	4538	10139	9600	0	0	0	0	0	0	0	0	1
246	3484	9902	10760	0	0	0	0	0	0	0	0	1
247	2430	9665	11770	0	0	0	0	0	0	0	0	1
248	1376	9428	12570	0	0	0	0	0	0	0	0	1
249	322	9191	13150	0	0	0	0	0	0	0	0	1
308	-600	1370	13230	0	0	0	0	0	0	0	0	3
309	-1170	2750	13230	0	0	0	0	0	0	0	0	3
310	-1700	4150	13230	0	0	0	0	0	0	0	0	3
311	-2510	5570	13230	0	0	0	0	0	0	0	0	3
312	-2840	7020	13230	0	0	0	0	0	0	0	0	3
313	-3170	8480	13230	0	0	0	0	0	0	0	0	3
314	-372	9940	13230	0	0	0	0	0	0	0	0	3
315	-72	6162	13490	0	0	0	0	0	0	0	0	1
316	-1111	5866	13540	0	0	0	0	0	0	0	0	1
317	-1062	10414	13490	0	0	0	0	0	0	0	0	1
318	-2116	10177	13540	0	0	0	0	0	0	0	0	1
319	1398	2186	13490	0	0	0	0	0	0	0	0	1
320	399	1778	13540	0	0	0	0	0	0	0	0	1
321	342	4854	13490	0	0	0	0	0	0	0	0	1
322	-679	4502	13540	0	0	0	0	0	0	0	0	1
323	830	3568	13490	0	0	0	0	0	0	0	0	1
324	-170	3159	13490	0	0	0	0	0	0	0	0	1
325	-404	7494	13490	0	0	0	0	0	0	0	0	1
326	-1457	7257	13540	0	0	0	0	0	0	0	0	1
327	-732	8954	13490	0	0	0	0	0	0	0	0	1
328	-1786	8717	13540	0	0	0	0	0	0	0	0	1

Nodi - Carichi

Nodi - Carichi

N°	C. Car.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	At
				kg			kg·m			mm			mmrad	°C
101	QP Solai	0	0	0	-0	0	0	0						
101	QV Solai	0	0	0	-0	0	0	0						
101	Neve	0	0	0	-0	0	0	0						
103	QP Solai	0	0	0	-0	0	0	0						
103	QV Solai	-0	-0	0	-0	0	0	0						
103	Neve	0	0	0	-0	0	0	0						
103	Neve	0	0	0	-0	0	0	0						
105	QP Solai	-0	-0	0	-0	0	0	0						
105	QV Solai	0	0	0	-0	0	0	0						
105	Neve	0	0	0	-0	0	0	0						
106	QP Solai	-0	-0	0	-0	0	0	0						
106	QV Solai	-0	-0	0	-0	0	0	0						
106	Neve	0	0	0	-0	0	0	0						
106	Neve	0	0	0	-0	0	0	0						
119	QP Solai	-0	-0	0	-0	0	0	0						
119	QV Solai	0	0	0	-0	0	0	0						
119	Neve	0	0	0	-0	0	0	0						
120	QP Solai	-0	-0	0	-0	0	0	0						
120	QV Solai	0	0	0	-0	0	0	0						
120	Neve	-0	0	0	-0	0	0	0						
121	QP Solai	0	0	0	-0	0	0	0						
121	QV Solai	0	0	0	-0	0	0	0						
121	Neve	0	0	0	-0	0	0	0						
121	Neve	0	0	0	-0	0	0	0						
122	QP Solai	0	0	0	-0	0	0	0						
122	QV Solai	-0	-0	0	-0	0	0	0						
122	Neve	0	0	0	-0	0	0	0						
122	Neve	-0	0	0	-0	0	0	0						
125	QP Solai	0	0	0	-0	0	0	0						
125	QV Solai	0	0	0	-0	0	0	0						
125	Neve	-0	-0	0	-0	0	0	0						
125	Neve	0	0	0	-0	0	0	0						
126	QP Solai	0	0	0	-0	0	0	0						
126	QV Solai	0	0	0	-0	0	0	0						
126	Neve	-0	-0	0	-0	0	0	0						
126	Neve	-0	-0	0	-0	0	0	0						
127	QP Solai	-0	-0	0	-0	0	0	0						
127	QV Solai	-0	-0	0	-0	0	0	0						

[illegible]

320	Nevse	-0	-0	0	0	-0	0	-0	0
321	QP Solia	-0	-0	0	0	-0	0	-0	-0
321	QV Solia	0	0	0	0	0	-0	-0	-0
321	Nevse	-0	-0	0	0	-0	0	-0	-0
321	Nevse	-0	-0	0	0	-0	0	-0	-0
322	QP Solia	-0	-0	0	0	-0	0	-0	-0
322	QV Solia	0	0	0	0	0	-0	-0	-0
322	Nevse	0	0	0	0	0	-0	-0	-0
322	Nevse	0	0	0	0	0	-0	-0	-0
322	Nevse	0	-0	0	0	0	-0	0	0
325	QP Solia	0	0	0	0	-0	0	0	0
325	QV Solia	0	0	0	0	-0	0	0	0
325	Nevse	0	0	0	0	-0	0	0	0
325	Nevse	-0	-0	0	0	-0	0	0	0
326	QP Solia	0	0	0	0	-0	0	0	0
326	QV Solia	0	0	0	0	-0	0	0	0
326	Nevse	0	0	0	0	-0	0	0	0
326	Nevse	-0	0	0	0	-0	0	0	0
327	QP Solia	-0	0	0	0	-0	0	0	0
327	QV Solia	-0	0	0	0	-0	0	0	0
327	Nevse	-0	0	0	0	-0	0	0	0
327	Nevse	-0	-0	0	0	-0	0	0	0
327	Nevse	-0	-0	0	0	-0	0	-0	-0
328	QP Solia	0	0	0	0	-0	0	-0	-0
328	QV Solia	-0	0	0	0	-0	0	-0	-0
328	Nevse	0	0	0	0	-0	0	0	-0

Input - Aste - Tabella sezioni tipo

Input - Aste - Tabella sezioni tipo		
Tipo	Nome	Raggio
C		cm
	F16	1

Tiplo	Nome	Area	lx	ly	lt	Fx	Fy	Lx	Lx
G		m ²			m ²			cm	cm
	IPE 100	0.0	1.710E-06	1.592E-07	8.826E-09	1.000	1.000	6	10
	HE 240 A	0.0	7.763E-05	2.769E-05	4.155E-07	1.000	1.000	24	23

Tiplo	Nome	Base	Altezza	Large mag.
R		cm	cm	cm
	F60x100	60	100	120

Aste - Geometria e vincoli

Aste - Geometria e vincoli

Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	°	f.f.	x1	y1	z1	x'	y'	z'	Tipo	L2	L3	cm	
1	1	I-1	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	112	5050	0	0	0	0	0	0	Pila	271	271	271
1	19	I-20	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	112	5050	0	0	0	0	0	0	Pila	136	136	136
1	20	I-1	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	112	5050	0	0	0	0	0	0	Pila	135	135	135
2	1	I-1	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	112	5050	0	0	0	0	0	0	Pila	135	135	135
2	15	I-1	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	112	5050	0	0	0	0	0	0	Pila	271	271	271
2	16	I-1	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	112	5050	0	0	0	0	0	0	Pila	136	136	136
2	16	I-2	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	109	5050	0	0	0	0	0	0	Pila	135	135	135
3	1	I-1	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	109	5050	0	0	0	0	0	0	Pila	271	271	271
3	17	I-1	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	109	5050	0	0	0	0	0	0	Pila	136	136	136
3	18	I-1	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	109	5050	0	0	0	0	0	0	Pila	135	135	135
4	4	I-25	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	106	5050	0	0	0	0	0	0	Pila	136	136	136
4	25	I-26	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	106	5050	0	0	0	0	0	0	Pila	135	135	135
4	26	I-24	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	106	5050	0	0	0	0	0	0	Pila	135	135	135
5	5	21	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	271	271	271
5	21	22	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	136	136	136
5	22	105	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	135	135	135
6	6	I-1	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	136	136	136
6	24	I-1	HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	136	136	136
6	24	106	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	135	135	135
7	7	27	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	271	271	271
7	27	28	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	136	136	136
7	28	107	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	135	135	135
208	208	308	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	112	5050	0	0	0	0	0	0	Pila	372	372	372
209	209	309	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	112	5050	0	0	0	0	0	0	Pila	372	372	372
210	210	310	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	109	5050	0	0	0	0	0	0	Pila	372	372	372
211	211	311	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	106	5050	0	0	0	0	0	0	Pila	372	372	372
212	212	312	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	372	372	372
213	213	313	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	372	372	372
214	214	314	I-1 HE 240 A	Acciaio	Acciaio	Acciaio	Pressi flessione	103	5050	0	0	0	0	0	0	Pila	372	372	372
101	101	IPE 100	IPE 100	Acciaio	Acciaio	Acciaio	Pressi flessione	45	5050	0	0	0	0	0	0	Trave	150	150	150
101	119	I35	Cy-Cy	Acciaio	Acciaio	Acciaio	Flessione	45	5050	0	0	0	0	0	0	Trave	95	95	95
101	123	I115	Cy-Cy	Acciaio	Acciaio	Acciaio	Flessione	45	5050	0	0	0	0	0	0	Trave	96	96	96
101	125	I125	Cy-Cy	Acciaio	Acciaio	Acciaio	Flessione	45	5050	0	0	0	0	0	0	Trave	95	95	95
101	125	I27	Cy-Cy	Acciaio	Acciaio	Acciaio	Flessione	45	5050	0	0	0	0	0	0	Trave	149	149	149
101	127	I17	Cy-Cy	Acciaio	Acciaio	Acciaio	Flessione	45	5050	0	0	0	0	0	0	Trave	150	150	150
102	120	I24	Cy-Cy	Acciaio	Acciaio	Acciaio	Flessione	45	5050	0	0	0	0	0	0	Trave	150	150	150

[illegible]

Aste - Carichi

	Sezione	Ni	Nf	Cond.	Tipo c.	Xi	OXi	OYi	QZi	Xf	OXf	OYf	QZf
						cm	car. dist. kg/m	car. dist. kg/m	car. dist. kg/m	cm	car. dist. kg/m	car. dist. kg/m	car. dist. kg/m
							coppie torc. kg°m/m	coppie torc. kg°m/m			coppie torc. kg°m/m	coppie torc. kg°m/m	
Uniforme globale Uniforme locale Variabile lineare globale Variabile lineare locale Poligonale globale Distorsione termica Carico torcente	Carico da precompressione												
	Poligonale locale												
	Pilastrino 1												
	HE 240 A	1	19	Peso Proprio	UnifG	0	0	0	60	271	0	0	60
	HE 240 A	1	19	Vento X	UnifL	0	0	0	-225	271	0	0	-225
	HE 240 A	1	19	Vento Y	UnifL	0	0	0	113	271	0	0	113
	HE 240 A	1	19	Carichi termici	Termico	0	0	0	60	136	0	0	60
	HE 240 A	19	20	Peso Proprio	UnifG	0	0	0	-225	136	0	0	-225
	HE 240 A	19	20	Vento X	UnifL	0	0	0	113	136	0	0	113
	HE 240 A	19	20	Vento Y	UnifL	0	0	0	113	136	0	0	113
PolG Termico Torcente	HE 240 A	19	20	Carichi termici	Termico	0	0	0	60	135	0	0	60
	HE 240 A	20	101	Peso Proprio	UnifG	0	0	0	-225	135	0	0	-225
	HE 240 A	20	101	Vento X	UnifL	0	0	0	113	135	0	0	113
	HE 240 A	20	101	Vento Y	UnifL	0	0	0	113	135	0	0	113
	HE 240 A	20	101	Carichi termici	Termico	0	0	0	60	135	0	0	60
	HE 240 A	20	101	Peso Proprio	UnifG	0	0	0	-225	135	0	0	-225
	HE 240 A	20	101	Vento X	UnifL	0	0	0	113	135	0	0	113
	HE 240 A	20	101	Vento Y	UnifL	0	0	0	113	135	0	0	113
Pilastrino 2													
HE 240 A	2	15		Peso Proprio	UnifG	0	0	0	60	271	0	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	OXf	QYf	QZf
HE 240 A	7	27	Vento X	UnifL	0	0	0	-225	271	0	0	-225
HE 240 A	7	27	Vento Y	UnifL	0	0	0	113	271	0	0	113
HE 240 A	7	27	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	27	28	Peso Proprio	UnifG	0	0	0	60	136	0	0	60
HE 240 A	27	28	Vento X	UnifL	0	0	0	-225	136	0	0	-225
HE 240 A	27	28	Vento Y	UnifL	0	0	0	113	136	0	0	113
HE 240 A	27	28	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	28	107	Peso Proprio	UnifG	0	0	0	60	135	0	0	60
HE 240 A	28	107	Vento X	UnifL	0	0	0	-225	135	0	0	-225
HE 240 A	28	107	Vento Y	UnifL	0	0	0	113	135	0	0	113
HE 240 A	28	107	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastrino 208												
HE 240 A	208	308	Peso Proprio	UnifG	0	0	0	60	372	0	0	60
HE 240 A	208	308	Vento X	UnifL	0	0	0	-113	372	0	0	-113
HE 240 A	208	308	Vento Y	UnifL	0	0	0	225	372	0	0	225
HE 240 A	208	308	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastrino 209												
HE 240 A	209	309	Peso Proprio	UnifG	0	0	0	60	372	0	0	60
HE 240 A	209	309	Vento X	UnifL	0	0	0	-113	372	0	0	-113
HE 240 A	209	309	Vento Y	UnifL	0	0	0	225	372	0	0	225
HE 240 A	209	309	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastrino 210												
HE 240 A	210	310	Peso Proprio	UnifG	0	0	0	60	372	0	0	60
HE 240 A	210	310	Vento X	UnifL	0	0	0	-113	372	0	0	-113
HE 240 A	210	310	Vento Y	UnifL	0	0	0	225	372	0	0	225
HE 240 A	210	310	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastrino 211												
HE 240 A	211	311	Peso Proprio	UnifG	0	0	0	60	372	0	0	60
HE 240 A	211	311	Vento X	UnifL	0	0	0	-113	372	0	0	-113
HE 240 A	211	311	Vento Y	UnifL	0	0	0	225	372	0	0	225
HE 240 A	211	311	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastrino 212												
HE 240 A	212	312	Peso Proprio	UnifG	0	0	0	60	372	0	0	60
HE 240 A	212	312	Vento X	UnifL	0	0	0	-113	372	0	0	-113
HE 240 A	212	312	Vento Y	UnifL	0	0	0	225	372	0	0	225
HE 240 A	212	312	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastrino 213												
HE 240 A	213	313	Peso Proprio	UnifG	0	0	0	60	372	0	0	60
HE 240 A	213	313	Vento X	UnifL	0	0	0	-113	372	0	0	-113
HE 240 A	213	313	Vento Y	UnifL	0	0	0	225	372	0	0	225
HE 240 A	213	313	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastrino 214												
HE 240 A	214	314	Peso Proprio	UnifG	0	0	0	60	372	0	0	60
HE 240 A	214	314	Vento X	UnifL	0	0	0	-113	372	0	0	-113
HE 240 A	214	314	Vento Y	UnifL	0	0	0	225	372	0	0	225
HE 240 A	214	314	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 101												
IPE 100	115	125	Peso Proprio	UnifG	0	0	0	8	95	0	0	8
IPE 100	115	125	QP Solai	PolG	90	0	0	141	90	0	0	140
IPE 100	115	125	QV Solai	PolG	0	0	0	45	90	0	0	45
IPE 100	115	125	Neve	PolG	90	0	0	44	90	0	0	44
IPE 100	115	125	Neve	PolG	90	0	0	44	95	0	0	43
IPE 100	115	125	Neve	PolG	0	0	0	44	95	0	0	43
IPE 100	115	125	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	119	123	Peso Proprio	UnifG	0	0	0	81	14	0	0	140
IPE 100	119	123	QP Solai	PolG	14	0	0	140	136	0	0	140
IPE 100	119	123	QV Solai	PolG	136	0	0	140	150	0	0	83
IPE 100	119	123	QV Solai	PolG	0	0	0	26	14	0	0	45
IPE 100	119	123	Neve	PolG	136	0	0	45	136	0	0	26
IPE 100	119	123	Neve	PolG	0	0	0	43	136	0	0	43

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	OXf	QYf	QZf
IPE 100	119	123	Neve	PolG	0	0	0	7	14	0	0	44
IPE 100	119	123	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	121	115	Peso Proprio	UnifG	0	0	0	8	96	0	0	8
IPE 100	121	115	QP Solai	PolG	8	0	0	140	94	0	0	140
IPE 100	121	115	QV Solai	PolG	94	0	0	71	96	0	0	71
IPE 100	121	115	QV Solai	PolG	0	0	0	23	8	0	0	45
IPE 100	121	115	Neve	PolG	94	0	0	45	94	0	0	45
IPE 100	121	115	Neve	PolG	94	0	0	23	96	0	0	23
IPE 100	121	115	Neve	PolG	0	0	0	43	94	0	0	43
IPE 100	121	115	Neve	PolG	0	0	0	2	8	0	0	44
IPE 100	121	115	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	123	121	Peso Proprio	UnifG	0	0	0	8	95	0	0	8
IPE 100	123	121	QP Solai	PolG	14	0	0	76	14	0	0	140
IPE 100	123	121	QV Solai	PolG	87	0	0	140	95	0	0	77
IPE 100	123	121	QV Solai	PolG	0	0	0	24	14	0	0	45
IPE 100	123	121	Neve	PolG	14	0	0	45	87	0	0	45
IPE 100	123	121	Neve	PolG	87	0	0	45	95	0	0	25
IPE 100	123	121	Neve	PolG	0	0	0	4	14	0	0	44
IPE 100	123	121	Neve	PolG	14	0	0	44	95	0	0	44
IPE 100	123	121	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	125	127	Peso Proprio	UnifG	0	0	0	43	87	0	0	43
IPE 100	125	127	QP Solai	PolG	87	0	0	43	95	0	0	4
IPE 100	125	127	QV Solai	PolG	0	0	0	24	4	0	0	45
IPE 100	125	127	QV Solai	PolG	4	0	0	45	145	0	0	45
IPE 100	125	127	Neve	PolG	145	0	0	45	149	0	0	24
IPE 100	125	127	Neve	PolG	0	0	0	3	4	0	0	43
IPE 100	125	127	Neve	PolG	4	0	0	43	149	0	0	43
IPE 100	125	127	Neve	PolG	0	0	0	44	145	0	0	44
IPE 100	125	127	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	127	117	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	127	117	QP Solai	PolG	0	0	0	75	4	0	0	140
IPE 100	127	117	QV Solai	PolG	4	0	0	140	145	0	0	140
IPE 100	127	117	QV Solai	PolG	145	0	0	140	150	0	0	73
IPE 100	127	117	Neve	PolG	0	0	0	24	4	0	0	45
IPE 100	127	117	Neve	PolG	4	0	0	45	145	0	0	45
IPE 100	127	117	Neve	PolG	145	0	0	45	150	0	0	23
IPE 100	127	117	Neve	PolG	0	0	0	44	145	0	0	44
IPE 100	127	117	Neve	PolG	145	0	0	44	150	0	0	2
IPE 100	127	117	Neve	PolG	0	0	0	2	4	0	0	43
IPE 100	127	117	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 102												
IPE 100	116	126	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	116	126	QP Solai	PolG	97	0	0	135	101	0	0	67
IPE 100	116	126	QV Solai	PolG	0	0	0	44	97	0	0	43
IPE 100	116	126	QV Solai	PolG	97	0	0	43	101	0	0	21
IPE 100	116	126	Neve	PolG	0	0	0	42	101	0	0	41
IPE 100	116	126	Neve	PolG	0	0	0	43	97	0	0	43
IPE 100	116	126	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	120	124	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	120	124	QP Solai	PolG	14	0	0	78	14	0	0	135
IPE 100	120	124	QV Solai	PolG	136	0	0	135	150	0	0	81
IPE 100	120	124	QV Solai	PolG	0	0	0	25	14	0	0	43

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	OXf	QYf	QZf
IPE 100	120	124	Neve	PolG	136	0	0	43	150	0	0	26
IPE 100	120	124	Neve	PolG	136	0	0	41	136	0	0	41
IPE 100	120	124	Neve	PolG	14	0	0	7	14	0	0	7
IPE 100	120	124	Carichi termici	Termico	14	0	0	43	150	0	0	43
IPE 100	122	116	Peso Proprio	UnitG	AXY=15°C,AXZ=15°C	0	0	0	8	102	0	8
IPE 100	122	116	QP Solai	PolG	8	0	0	69	8	0	0	135
IPE 100	122	116	QP Solai	PolG	100	0	0	135	100	0	0	135
IPE 100	122	116	QP Solai	PolG	8	0	0	69	102	0	0	69
IPE 100	122	116	QV Solai	PolG	0	0	0	22	8	0	0	43
IPE 100	122	116	QV Solai	PolG	8	0	0	43	100	0	0	43
IPE 100	122	116	QV Solai	PolG	100	0	0	22	102	0	0	22
IPE 100	122	116	Neve	PolG	0	0	0	41	100	0	0	41
IPE 100	122	116	Neve	PolG	0	0	0	2	8	0	0	43
IPE 100	122	116	Neve	PolG	8	0	0	43	102	0	0	43
IPE 100	122	116	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	101	0	8
IPE 100	124	122	Peso Proprio	UnitG	0	0	0	0	8	101	0	8
IPE 100	124	122	QP Solai	PolG	14	0	0	73	14	0	0	135
IPE 100	124	122	QP Solai	PolG	93	0	0	135	101	0	0	135
IPE 100	124	122	QV Solai	PolG	0	0	0	23	14	0	0	43
IPE 100	124	122	QV Solai	PolG	14	0	0	43	93	0	0	43
IPE 100	124	122	Neve	PolG	93	0	0	43	101	0	0	43
IPE 100	124	122	Neve	PolG	14	0	0	43	101	0	0	43
IPE 100	124	122	Neve	PolG	93	0	0	41	101	0	0	41
IPE 100	124	122	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	150	0	8
IPE 100	126	128	Peso Proprio	UnitG	0	0	0	73	4	0	0	135
IPE 100	126	128	QP Solai	PolG	4	0	0	135	145	0	0	135
IPE 100	126	128	QV Solai	PolG	145	0	0	135	150	0	0	71
IPE 100	126	128	QV Solai	PolG	4	0	0	24	4	0	0	43
IPE 100	126	128	QV Solai	PolG	4	0	0	43	145	0	0	43
IPE 100	126	128	Neve	PolG	145	0	0	43	150	0	0	23
IPE 100	126	128	Neve	PolG	0	0	0	43	145	0	0	43
IPE 100	126	128	Neve	PolG	145	0	0	43	150	0	0	3
IPE 100	126	128	Neve	PolG	4	0	0	3	4	0	0	41
IPE 100	126	128	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	41	150	0	41
IPE 100	128	118	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	128	118	QP Solai	PolG	4	0	0	73	4	0	0	135
IPE 100	128	118	QP Solai	PolG	145	0	0	135	145	0	0	135
IPE 100	128	118	QV Solai	PolG	0	0	0	23	4	0	0	43
IPE 100	128	118	QV Solai	PolG	4	0	0	43	145	0	0	43
IPE 100	128	118	QV Solai	PolG	145	0	0	43	150	0	0	22
IPE 100	128	118	Neve	PolG	0	0	0	43	145	0	0	43
IPE 100	128	118	Neve	PolG	145	0	0	43	150	0	0	2
IPE 100	128	118	Neve	PolG	4	0	0	2	4	0	0	41
IPE 100	128	118	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	41	150	0	41
IPE 100	128	118	Peso Proprio	UnitG	0	0	0	8	107	0	0	8
IPE 100	128	118	QP Solai	PolG	103	0	0	128	107	0	0	63
IPE 100	128	118	QP Solai	PolG	0	0	0	41	103	0	0	41
IPE 100	128	118	QV Solai	PolG	103	0	0	41	107	0	0	20
IPE 100	128	118	QV Solai	PolG	0	0	0	39	107	0	0	38
IPE 100	128	118	Neve	PolG	0	0	0	41	103	0	0	41
IPE 100	128	118	Neve	PolG	103	0	0	41	107	0	0	1
IPE 100	128	118	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	150	0	8
IPE 100	128	118	Peso Proprio	UnitG	0	0	0	73	14	0	0	128
IPE 100	128	118	QP Solai	PolG	14	0	0	128	136	0	0	128

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	OZi	Xf	QXf	QYf	OZf	
IPE 100	225	235	QV Solai	PolG	136	0	0	23	150	0	0	77	
					0	0	0	128	14	0	0	41	
					14	0	0	41	136	0	0	41	
IPE 100	225	235	Neve	PolG	136	0	0	41	150	0	0	25	
					0	0	0	38	136	0	0	38	
					136	0	0	0	38	150	0	7	
IPE 100	225	235	Neve	PolG	0	0	0	7	14	0	0	41	
					14	0	0	41	150	0	0	41	
					Termico AXY=15°C,AXZ=15°C								
IPE 100	225	235	Carichi termici	UnitG	0	0	0	8	108	0	0	8	
	IPE 100	230	215	Peso Proprio	PolG	0	0	0	65	8	0	0	128
		230	215	QP Solai	PolG	8	0	0	128	106	0	0	128
IPE 100	230	215	QP Solai	PolG	106	0	0	66	108	0	0	66	
					0	0	0	21	8	0	0	41	
					8	0	0	41	106	0	0	41	
IPE 100	230	215	QV Solai	PolG	106	0	0	21	108	0	0	21	
					0	0	0	38	106	0	0	38	
					0	0	0	2	8	0	0	41	
IPE 100	235	230	Neve	PolG	8	0	0	41	108	0	0	41	
					Termico AXY=15°C,AXZ=15°C								
					UnitG	0	0	0	8	107	0	0	8
IPE 100	235	230	Peso Proprio	PolG	0	0	0	69	14	0	0	128	
	IPE 100	240	245	QP Solai	PolG	14	0	0	128	100	0	0	128
		240	245	QP Solai	PolG	100	0	0	128	107	0	0	73
IPE 100	240	245	QP Solai	PolG	0	0	0	22	14	0	0	41	
					14	0	0	41	100	0	0	41	
					100	0	0	41	107	0	0	23	
IPE 100	240	245	Neve	PolG	0	0	0	38	100	0	0	38	
	IPE 100	245	245	Neve	PolG	100	0	0	38	107	0	0	4
		245	245	Neve	PolG	0	0	0	4	14	0	0	41
IPE 100	245	245	Neve	PolG	14	0	0	41	107	0	0	41	
					Termico AXY=15°C,AXZ=15°C								
					UnitG	0	0	0	8	150	0	0	8
IPE 100	245	245	Peso Proprio	PolG	0	0	0	70	4	0	0	128	
	IPE 100	245	245	QP Solai	PolG	4	0	0	128	145	0	0	128
		245	245	QP Solai	PolG	145	0	0	128	150	0	0	66
IPE 100	245	245	QV Solai	PolG	0	0	0	22	4	0	0	41	
					4	0	0	41	145	0	0	41	
					145	0	0	41	150	0	0	21	
IPE 100	245	245	Neve	PolG	0	0	0	2	4	0	0	38	
	IPE 100	245	245	Neve	PolG	4	0	0	38	150	0	0	38
		245	245	Neve	PolG	0	0	0	41	145	0	0	41
IPE 100	245	245	Neve	PolG	145	0	0	41	150	0	0	3	
					Termico AXY=15°C,AXZ=15°C								
					UnitG	0	0	0	8	150	0	0	8
IPE 100	245	220	Carichi termici	PolG	0	0	0	70	4	0	0	128	
	IPE 100	245	220	Peso Proprio	PolG	0	0	0	128	145	0	0	128
		245	220	QP Solai	PolG	4	0	0	22	4	0	0	65
IPE 100	245	220	QV Solai	PolG	145	0	0	128	150	0	0	65	
					0	0	0	22	4	0	0	41	
					4	0	0	41	145	0	0	41	
IPE 100	245	220	Neve	PolG	145	0	0	41	150	0	0	21	
	IPE 100	245	220	Neve	PolG	0	0	0	2	4	0	0	38
		245	220	Neve	PolG	4	0	0	38	150	0	0	38
IPE 100	245	220	Neve	PolG	0	0	0	2	4	0	0	38	
	IPE 100	245	220	Neve	PolG	4	0	0	38	150	0	0	38
		245	220	Neve	PolG	0	0	0	41	145	0	0	41
IPE 100	245	220	Neve	PolG	145	0	0	41	150	0	0	2	
					Termico AXY=15°C,AXZ=15°C								
					UnitG	0	0	0	41	150	0	0	2
Trave 104													
IPE 100	216	241	Peso Proprio	UnitG	0	0	0	8	113	0	0	8	
	IPE 100	216	241	QP Solai	PolG	0	0	0	120	109	0	0	119
		216	241	QP Solai	PolG	109	0	0	119	113	0	0	59
IPE 100	216	241	QV Solai	PolG	0	0	0	39	109	0	0	38	
					109	0	0	38	113	0	0	19	
					0	0	0	38	109	0	0	38	
IPE 100	216	241	Neve	PolG	0	0	0	38	113	0	0	1	
	IPE 100	216	241	Neve	PolG	109	0	0	38	113	0	0	36
		216	241	Carichi termici	PolG	0	0	0	36	113	0	0	36
IPE 100	216	241	Neve	PolG	0	0	0	36	113	0	0	36	
	IPE 100	216	241	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	36	113	0	36
		216	241	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	36	113	0	36

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	226	236	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	226	236	QP Solai	PolG	0	0	0	68	14	0	0	119
					14	0	0	119	136	0	0	119
IPE 100	226	236	QV Solai	PolG	0	0	0	119	150	0	0	72
					136	0	0	22	14	0	0	38
IPE 100	226	236			14	0	0	38	136	0	0	38
					136	0	0	38	150	0	0	23
IPE 100	226	236	Neve	PolG	0	0	0	7	14	0	0	38
					14	0	0	38	150	0	0	38
IPE 100	226	236	Neve	PolG	0	0	0	36	136	0	0	36
					136	0	0	36	150	0	0	6
IPE 100	226	236	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	231	216	Peso Proprio	UnifG	0	0	0	8	114	0	0	8
IPE 100	231	216	QP Solai	PolG	8	0	0	60	8	0	0	119
					8	0	0	119	112	0	0	119
IPE 100	231	216	QV Solai	PolG	112	0	0	62	114	0	0	62
					0	0	0	19	8	0	0	38
					8	0	0	38	112	0	0	38
IPE 100	231	216	Neve	PolG	112	0	0	20	114	0	0	20
IPE 100	231	216	Neve	PolG	0	0	0	36	112	0	0	36
					106	0	0	2	8	0	0	38
IPE 100	231	216	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	231	216	Peso Proprio	UnifG	0	0	0	8	113	0	0	8
IPE 100	236	231	QP Solai	PolG	0	0	0	64	14	0	0	119
					14	0	0	119	106	0	0	119
IPE 100	236	231	QV Solai	PolG	106	0	0	119	113	0	0	68
					0	0	0	21	14	0	0	38
					14	0	0	38	106	0	0	38
IPE 100	236	231	Neve	PolG	106	0	0	38	113	0	0	22
					0	0	0	4	14	0	0	38
IPE 100	236	231	Neve	PolG	14	0	0	38	113	0	0	38
					106	0	0	36	106	0	0	36
IPE 100	236	231	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	241	246	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	241	246	QP Solai	PolG	0	0	0	65	4	0	0	119
					4	0	0	119	145	0	0	119
IPE 100	241	246	QV Solai	PolG	145	0	0	119	150	0	0	61
					0	0	0	21	4	0	0	38
					4	0	0	38	145	0	0	38
IPE 100	241	246	Neve	PolG	145	0	0	38	150	0	0	20
					0	0	0	38	145	0	0	38
IPE 100	241	246	Neve	PolG	145	0	0	38	150	0	0	2
					0	0	0	2	4	0	0	36
IPE 100	241	246	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	246	221	Peso Proprio	UnifG	4	0	0	36	150	0	0	36
IPE 100	246	221	QP Solai	PolG	0	0	0	8	150	0	0	8
					4	0	0	65	4	0	0	119
IPE 100	246	221	QV Solai	PolG	4	0	0	119	145	0	0	119
					145	0	0	119	150	0	0	61
IPE 100	246	221			0	0	0	21	4	0	0	38
					4	0	0	38	145	0	0	38
IPE 100	246	221	Neve	PolG	4	0	0	38	145	0	0	38
					145	0	0	38	150	0	0	20
IPE 100	246	221	Neve	PolG	145	0	0	38	145	0	0	38
					0	0	0	2	4	0	0	36
IPE 100	246	221	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	246	221	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	246	221	QP Solai	PolG	4	0	0	65	4	0	0	119
IPE 100	246	221	QV Solai	PolG	4	0	0	119	145	0	0	119
					145	0	0	119	150	0	0	61
IPE 100	246	221			0	0	0	21	4	0	0	38
					4	0	0	38	145	0	0	38
IPE 100	246	221	Neve	PolG	145	0	0	38	145	0	0	38
					145	0	0	38	150	0	0	20
IPE 100	246	221	Neve	PolG	4	0	0	36	150	0	0	36
					4	0	0	38	145	0	0	38
IPE 100	246	221	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	246	221	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	246	221	QP Solai	PolG	4	0	0	65	4	0	0	119
IPE 100	246	221	QV Solai	PolG	4	0	0	119	145	0	0	119
					145	0	0	119	150	0	0	61
IPE 100	246	221			0	0	0	21	4	0	0	38
					4	0	0	38	145	0	0	38
IPE 100	246	221	Neve	PolG	145	0	0	38	145	0	0	38
					145	0	0	38	150	0	0	20
IPE 100	246	221	Neve	PolG	4	0	0	36	150	0	0	36
					4	0	0	38	145	0	0	38
IPE 100	246	221	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	246	221	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	246	221	QP Solai	PolG	4	0	0	65	4	0	0	119
IPE 100	246	221	QV Solai	PolG	4	0	0	119	145	0	0	119
					145	0	0	119	150	0	0	61
IPE 100	246	221			0	0	0	21	4	0	0	38
					4	0	0	38	145	0	0	38
IPE 100	246	221	Neve	PolG	145	0	0	38	145	0	0	38
					145	0	0	38	150	0	0	20
IPE 100	246	221	Neve	PolG	4	0	0	36	150	0	0	36
					4	0	0	38	145	0	0	38
IPE 100	246	221	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	246	221	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	246	221	QP Solai	PolG	4	0	0	65	4	0	0	119
IPE 100	246	221	QV Solai	PolG	4	0	0	119	145	0	0	119
					145	0	0	119	150	0	0	61
IPE 100	246	221			0	0	0	21	4	0	0	38
					4	0	0	38	145	0	0	38
IPE 100	246	221	Neve	PolG	145	0	0	38	145	0	0	38
					145	0	0	38	150	0	0	20
IPE 100	246	221	Neve	PolG	4	0	0	36	150	0	0	36
					4	0	0	38	145	0	0	38
IPE 100	246	221	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	246	221	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	246	221	QP Solai	PolG	4	0	0	65	4	0	0	119
IPE 100	246	221	QV Solai	PolG	4	0	0	119	145	0	0	119
					145	0	0	119	150	0	0	61
IPE 100	246	221			0	0	0	21	4	0	0	38
					4	0	0	38	145	0	0	38
IPE 100	246	221	Neve	PolG	145	0	0	38	145	0	0	38
					145	0	0	38	150	0	0	20
IPE 100	246	221	Neve	PolG	4	0	0	36	150	0	0	36
					4	0	0	38	145	0	0	38
IPE 100	246	221	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	246	221	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	246	221	QP Solai	PolG	4	0	0	65	4	0	0	119
IPE 100	246	221	QV Solai	PolG	4	0	0	119	145	0	0	119
					145	0	0	119	150	0	0	61
IPE 100	246	221			0	0	0	21	4	0	0	38
					4	0	0	38	145	0	0	38
IPE 100	246	221	Neve	PolG	145	0	0	38	145	0	0	38
					145	0	0	38	150	0	0	20
IPE 100	246	221	Neve	PolG	4	0	0	36	150	0	0	36
					4	0	0	38	145	0	0	38
IPE 100	246	221	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	246	221	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	246	221	QP Solai	PolG	4	0	0	65	4	0	0	119
IPE 100	246	221	QV Solai	PolG	4	0	0	119	145	0	0	119
					145	0	0	119	150	0	0	61
IPE 100	246	221			0	0	0	21	4	0	0	38
					4	0	0	38	145	0	0	38
IPE 100	246	221	Neve	PolG	145	0	0	38	145	0	0	38
					145	0	0	38	150	0	0	20
IPE 100	246	221	Neve	PolG	4	0	0	36	150	0	0	36
					4	0	0	38	145	0	0	38
IPE 100	246	221	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	246	221	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	246	221	QP Solai	PolG	4	0	0	65	4	0	0	119
IPE 100	246	221	QV Solai	PolG	4	0	0	119	145			

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	249	224	Carichi termici	Termico	4	0	0	0	27	150	0	27
Trave 108												
IPE 100	315	325	Peso Proprio	UnitG	0	0	0	0	8	137	0	8
IPE 100	315	325	QV Solai	PolG	133	0	0	0	87	133	0	86
IPE 100	315	325	QV Solai	PolG	0	0	0	0	28	133	0	28
IPE 100	315	325	Neve	PolG	133	0	0	0	28	137	0	14
IPE 100	315	325	Neve	PolG	0	0	0	0	27	133	0	27
IPE 100	315	325	Neve	PolG	133	0	0	0	27	137	0	1
IPE 100	315	325	Carichi termici	Termico	0	0	0	0	8	149	0	8
IPE 100	319	323	Peso Proprio	UnitG	0	0	0	0	50	14	0	86
IPE 100	319	323	QV Solai	PolG	14	0	0	0	86	136	0	86
IPE 100	319	323	QV Solai	PolG	136	0	0	0	86	149	0	52
IPE 100	319	323	QV Solai	PolG	0	0	0	0	16	14	0	28
IPE 100	319	323	Neve	PolG	14	0	0	0	28	136	0	28
IPE 100	319	323	Neve	PolG	136	0	0	0	28	149	0	17
IPE 100	319	323	Neve	PolG	0	0	0	0	5	14	0	27
IPE 100	319	323	Neve	PolG	14	0	0	0	27	149	0	27
IPE 100	319	323	Neve	PolG	0	0	0	0	26	136	0	26
IPE 100	319	323	Neve	PolG	136	0	0	0	26	149	0	5
IPE 100	319	323	Carichi termici	Termico	0	0	0	0	8	137	0	8
IPE 100	321	315	Peso Proprio	UnitG	0	0	0	0	45	8	0	86
IPE 100	321	315	QV Solai	PolG	8	0	0	0	86	135	0	86
IPE 100	321	315	QV Solai	PolG	135	0	0	0	44	137	0	44
IPE 100	321	315	QV Solai	PolG	0	0	0	0	14	8	0	28
IPE 100	321	315	QV Solai	PolG	8	0	0	0	28	135	0	28
IPE 100	321	315	QV Solai	PolG	135	0	0	0	14	137	0	14
IPE 100	321	315	Neve	PolG	0	0	0	0	26	135	0	26
IPE 100	321	315	Neve	PolG	0	0	0	0	2	8	0	27
IPE 100	321	315	Neve	PolG	8	0	0	0	27	137	0	27
IPE 100	321	315	Carichi termici	Termico	0	0	0	0	8	138	0	8
IPE 100	323	321	Peso Proprio	UnitG	0	0	0	0	48	14	0	86
IPE 100	323	321	QV Solai	PolG	14	0	0	0	86	130	0	86
IPE 100	323	321	QV Solai	PolG	130	0	0	0	86	138	0	50
IPE 100	323	321	QV Solai	PolG	0	0	0	0	15	14	0	28
IPE 100	323	321	QV Solai	PolG	14	0	0	0	28	130	0	28
IPE 100	323	321	QV Solai	PolG	130	0	0	0	28	138	0	16
IPE 100	323	321	Neve	PolG	0	0	0	0	26	130	0	26
IPE 100	323	321	Neve	PolG	130	0	0	0	26	138	0	3
IPE 100	323	321	Neve	PolG	0	0	0	0	4	14	0	27
IPE 100	323	321	Neve	PolG	14	0	0	0	27	138	0	27
IPE 100	323	321	Carichi termici	Termico	0	0	0	0	8	150	0	8
IPE 100	325	327	Peso Proprio	UnitG	0	0	0	0	47	4	0	86
IPE 100	325	327	QV Solai	PolG	4	0	0	0	86	145	0	86
IPE 100	325	327	QV Solai	PolG	145	0	0	0	86	150	0	45
IPE 100	325	327	QV Solai	PolG	0	0	0	0	15	4	0	28
IPE 100	325	327	QV Solai	PolG	4	0	0	0	28	145	0	28
IPE 100	325	327	QV Solai	PolG	145	0	0	0	1	4	0	26
IPE 100	325	327	QV Solai	PolG	4	0	0	0	26	150	0	26
IPE 100	325	327	QV Solai	PolG	0	0	0	0	27	145	0	27
IPE 100	325	327	QV Solai	PolG	145	0	0	0	27	150	0	2
IPE 100	325	327	Carichi termici	Termico	0	0	0	0	8	150	0	8
IPE 100	327	317	Peso Proprio	UnitG	0	0	0	0	46	4	0	86
IPE 100	327	317	QV Solai	PolG	4	0	0	0	86	145	0	86
IPE 100	327	317	QV Solai	PolG	145	0	0	0	86	150	0	45
IPE 100	327	317	QV Solai	PolG	4	0	0	0	15	4	0	28
IPE 100	327	317	QV Solai	PolG	0	0	0	0	28	145	0	28
IPE 100	327	317	QV Solai	PolG	4	0	0	0	28	145	0	4
IPE 100	327	317	QV Solai	PolG	145	0	0	0	28	150	0	14
IPE 100	327	317	QV Solai	PolG	0	0	0	0	2	4	0	27
IPE 100	327	317	QV Solai	PolG	4	0	0	0	27	150	0	27
IPE 100	327	317	QV Solai	PolG	0	0	0	0	26	145	0	26
IPE 100	327	317	QV Solai	PolG	145	0	0	0	26	150	0	1
IPE 100	327	317	QV Solai	PolG	0	0	0	0	8	150	0	8
IPE 100	327	317	QV Solai	PolG	4	0	0	0	86	145	0	86
IPE 100	327	317	QV Solai	PolG	145	0	0	0	86	150	0	46
IPE 100	327	317	QV Solai	PolG	0	0	0	0	14	4	0	28
IPE 100	327	317	QV Solai	PolG	4	0	0	0	28	145	0	28
IPE 100	327	317	QV Solai	PolG	145	0	0	0	28	150	0	15
IPE 100	327	317	QV Solai	PolG	4	0	0	0	4	14	0	26
IPE 100	327	317	QV Solai	PolG	14	0	0	0	26	144	0	26
IPE 100	327	317	QV Solai	PolG	0	0	0	0	27	136	0	27
IPE 100	327	317	QV Solai	PolG	0	0	0	0	27	144	0	4
IPE 100	327	317	QV Solai	PolG	136	0	0	0	8	150	0	8
IPE 100	327	317	QV Solai	PolG	0	0	0	0	45	4	0	86
IPE 100	327	317	QV Solai	PolG	4	0	0	0	86	145	0	86
IPE 100	327	317	QV Solai	PolG	145	0	0	0	86	150	0	46
IPE 100	327	317	QV Solai	PolG	0	0	0	0	14	4	0	28
IPE 100	327	317	QV Solai	PolG	4	0	0	0	28	145	0	28
IPE 100	327	317	QV Solai	PolG	145	0	0	0	28	150	0	15
IPE 100	327	317	QV Solai	PolG	4	0	0	0	4	14	0	26
IPE 100	327	317	QV Solai	PolG	14	0	0	0	26	144	0	26
IPE 100	327	317	QV Solai	PolG	0	0	0	0	27	136	0	27
IPE 100	327	317	QV Solai	PolG	0	0	0	0	27	144	0	4
IPE 100	327	317	QV Solai	PolG	136	0	0	0	8	150	0	8
IPE 100	327	317	QV Solai	PolG	0	0	0	0	45	4	0	86
IPE 100	327	317	QV Solai	PolG	4	0	0	0	86	145	0	86
IPE 100	327	317	QV Solai	PolG	145	0	0	0	86	150	0	46
IPE 100	327	317	QV Solai	PolG	0	0	0	0	14	4	0	28
IPE 100	327	317	QV Solai	PolG	4	0	0	0	28	145	0	28
IPE 100	327	317	QV Solai	PolG	145	0	0	0	28	150	0	15
IPE 100	327	317	QV Solai	PolG	4	0	0	0	4	14	0	26
IPE 100	327	317	QV Solai	PolG	14	0	0	0	26	144	0	26
IPE 100	327	317	QV Solai	PolG	0	0	0	0	27	136	0	27
IPE 100	327	317	QV Solai	PolG	0	0	0	0	27	144	0	4
IPE 100	327	317	QV Solai	PolG	136	0	0	0	8	150	0	8
IPE 100	327	317	QV Solai	PolG	0	0	0	0	45	4	0	86
IPE 100	327	317	QV Solai	PolG	4	0	0	0	86	145	0	86
IPE 100	327	317	QV Solai	PolG	145	0	0	0	86	150	0	46
IPE 100	327	317	QV Solai	PolG	0	0	0	0	14	4	0	28
IPE 100	327	317	QV Solai	PolG	4	0	0	0	28	145	0	28
IPE 100	327	317	QV Solai	PolG	145	0	0	0	28	150	0	15
IPE 100	327	317	QV Solai	PolG	4	0	0	0	4	14	0	26
IPE 100	327	317	QV Solai	PolG	14	0	0	0	26	144	0	26
IPE 100	327	317	QV Solai	PolG	0	0	0	0	27	136	0	27
IPE 100	327	317	QV Solai	PolG	0	0	0	0	27	144	0	4
IPE 100	327	317	QV Solai	PolG	136	0	0	0	8	150	0	8
IPE 100	327	317	QV Solai	PolG	0	0	0	0	45	4	0	86
IPE 100	327	317	QV Solai	PolG	4	0	0	0	86	145	0	86
IPE 100	327	317	QV Solai	PolG	145	0	0	0	86	150	0	46
IPE 100	327	317	QV Solai	PolG	0	0	0	0	14	4	0	28
IPE 100	327	317	QV Solai	PolG	4	0	0	0	28	145	0	28
IPE 100	327	317	QV Solai	PolG	145	0	0	0	28	150	0	15
IPE 100	327	317	QV Solai	PolG	4	0	0	0	4	14	0	26
IPE 100	327	317	QV Solai	PolG	14	0	0	0	26	144	0	26
IPE 100	327	317	QV Solai	PolG	0	0	0	0	27	136	0	27
IPE 100	327	317	QV Solai	PolG	0	0	0	0	27	144	0	4
IPE 100	327	317	QV Solai	PolG	136	0	0	0	8	150	0	8
IPE 100	327	317	QV Solai	PolG	0	0	0	0	45	4	0	86
IPE 100	327	317	QV Solai	PolG	4	0	0	0	86	145	0	86
IPE 100	327	317	QV Solai	PolG	145	0	0	0	86	150	0	46
IPE 100	327	317	QV Solai	PolG	0	0	0	0	14	4	0	28
IPE 100	327	317	QV Solai	PolG	4	0	0	0	28	145	0	28
IPE 100	327	317	QV Solai	PolG	145	0	0	0	28	150	0	15</

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	QXf	QYf	QZf
IPE 100	328	318	QV Solai	PolG	0	0	0	14	4	0	0	28
					4	0	0	28	145	0	0	28
IPE 100	328	318	Neve	PolG	145	0	0	28	150	0	0	15
					0	0	0	1	4	0	0	27
IPE 100	328	318	Neve	PolG	4	0	0	27	150	0	0	27
					0	0	0	26	145	0	0	26
IPE 100	328	318	Carichi termici	Termico	145	0	0	26	150	0	0	1
					AXY=15°C,AXZ=15°C							
Trave 110												
IPE 100	101	102	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	101	102	QP Solai	PolG	0	0	0	71	136	0	0	71
					136	0	0	71	150	0	0	12
IPE 100	101	102	QV Solai	PolG	0	0	0	23	136	0	0	23
					136	0	0	23	150	0	0	4
IPE 100	101	102	Neve	PolG	0	0	0	44	136	0	0	44
					136	0	0	44	150	0	0	7
IPE 100	101	102	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	102	103	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	102	103	QP Solai	PolG	0	0	0	71	81	0	0	71
					81	0	0	71	89	0	0	6
IPE 100	102	103	QV Solai	PolG	0	0	0	23	81	0	0	23
					81	0	0	23	89	0	0	2
IPE 100	102	103	Neve	PolG	0	0	0	44	81	0	0	44
					81	0	0	44	89	0	0	4
IPE 100	102	103	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	103	104	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	103	104	QP Solai	PolG	0	0	0	71	88	0	0	71
IPE 100	103	104	QV Solai	PolG	0	0	0	23	88	0	0	23
IPE 100	103	104	Neve	PolG	0	0	0	44	88	0	0	44
IPE 100	103	104	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	104	105	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	104	105	QP Solai	PolG	0	0	0	71	89	0	0	71
IPE 100	104	105	QV Solai	PolG	0	0	0	23	89	0	0	23
IPE 100	104	105	Neve	PolG	0	0	0	44	89	0	0	44
IPE 100	104	105	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	105	106	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	105	106	QP Solai	PolG	0	0	0	5	4	0	0	71
					4	0	0	71	149	0	0	71
IPE 100	105	106	QV Solai	PolG	0	0	0	1	4	0	0	23
					4	0	0	23	149	0	0	23
IPE 100	105	106	Neve	PolG	0	0	0	3	4	0	0	44
					4	0	0	44	149	0	0	44
IPE 100	105	106	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	106	107	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	106	107	QP Solai	PolG	0	0	0	4	4	0	0	71
					4	0	0	71	150	0	0	71
IPE 100	106	107	QV Solai	PolG	0	0	0	1	4	0	0	23
					4	0	0	23	150	0	0	23
IPE 100	106	107	Neve	PolG	0	0	0	2	4	0	0	44
					4	0	0	44	150	0	0	44
IPE 100	106	107	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 301												
IPE 100	308	309	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	308	309	QP Solai	PolG	0	0	0	8	14	0	0	44
					14	0	0	44	149	0	0	44
IPE 100	308	309	QV Solai	PolG	0	0	0	3	14	0	0	14
					14	0	0	14	149	0	0	14
IPE 100	308	309	Neve	PolG	0	0	0	5	14	0	0	27
					14	0	0	27	149	0	0	27
IPE 100	308	309	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	309	310	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	309	310	QP Solai	PolG	0	0	0	6	14	0	0	44
					14	0	0	44	150	0	0	44
IPE 100	309	310	QV Solai	PolG	0	0	0	2	14	0	0	14

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	QXf	QYf	QZf
IPE 100	309	310	Neve	PolG	0	0	0	4	14	0	0	27
					14	0	0	27	150	0	0	27
IPE 100	309	310	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	310	311	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	310	311	QP Solai	PolG	0	0	0	3	8	0	0	44
					8	0	0	44	149	0	0	44
IPE 100	310	311	QV Solai	PolG	0	0	0	1	8	0	0	14
					8	0	0	14	149	0	0	14
IPE 100	310	311	Neve	PolG	0	0	0	2	8	0	0	27
					8	0	0	27	149	0	0	27
IPE 100	310	311	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	311	312	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	311	312	QP Solai	PolG	0	0	0	44	145	0	0	44
					145	0	0	44	149	0	0	1
IPE 100	311	312	QV Solai	PolG	0	0	0	14	145	0	0	14
					145	0	0	14	149	0	0	0
IPE 100	311	312	Neve	PolG	0	0	0	27	145	0	0	27
					145	0	0	27	149	0	0	1
IPE 100	311	312	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	312	313	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	312	313	QP Solai	PolG	0	0	0	44	145	0	0	44
					145	0	0	44	150	0	0	2
IPE 100	312	313	QV Solai	PolG	0	0	0	14	145	0	0	14
					145	0	0	14	150	0	0	1
IPE 100	312	313	Neve	PolG	0	0	0	27	145	0	0	27
					145	0	0	27	150	0	0	1
IPE 100	312	313	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	313	314	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	313	314	QP Solai	PolG	0	0	0	44	145	0	0	44
					145	0	0	44	150	0	0	2
IPE 100	313	314	QV Solai	PolG	0	0	0	14	145	0	0	14
					145	0	0	14	150	0	0	1
IPE 100	313	314	Neve	PolG	0	0	0	27	145	0	0	27
					145	0	0	27	150	0	0	1
IPE 100	313	314	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 8000												
HE 240 A	101	119	Peso Proprio	UnitG	0	0	0	60	181	0	0	60
HE 240 A	101	119	QP Solai	PolG	0	0	0	5	31	0	0	63
					31	0	0	63	182	0	0	58
HE 240 A	101	119	QV Solai	PolG	0	0	0	2	31	0	0	20
					31	0	0	20	182	0	0	19
HE 240 A	101	119	Neve	PolG	0	0	0	3	31	0	0	39
					31	0	0	39	182	0	0	36
HE 240 A	101	119	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	119	120	Peso Proprio	UnitG	0	0	0	60	177	0	0	60
HE 240 A	119	120	QP Solai	PolG	0	0	0	5	30	0	0	63
					30	0	0	63	178	0	0	58
HE 240 A	119	120	QV Solai	PolG	0	0	0	2	30	0	0	20
					30	0	0	20	178	0	0	19
HE 240 A	119	120	Neve	PolG	0	0	0	3	30	0	0	39
					30	0	0	39	178	0	0	36
HE 240 A	119	120	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	120	225	Peso Proprio	UnitG	0	0	0	60	170	0	0	60
HE 240 A	120	225	QP Solai	PolG	0	0	0	5	29	0	0	63
					29	0	0	63	170	0	0	58
HE 240 A	120	225	QV Solai	PolG	0	0	0	2	29	0	0	20
					29	0	0	20	170	0	0	19
HE 240 A	120	225	Neve	PolG	0	0	0	3	29	0	0	39
					29	0	0	39	170	0	0	36
HE 240 A	120	225	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	225	226	Peso Proprio	UnitG	0	0	0	60	158	0	0	60
HE 240 A	225	226	QP Solai	PolG	0	0	0	5	27	0	0	63
					27	0	0	63	158	0	0	58
HE 240 A	225	226	QV Solai	PolG	0	0	0	2	27	0	0	20
					27	0	0	20	158	0	0	19

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	OXf	QYf	QZf
HE 240 A	225	226	Neve	PolG	27	0	0	0	3	27	0	39
HE 240 A	225	226	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	148	0	60
HE 240 A	226	227	Peso Proprio	UnitG	27	0	0	0	5	26	0	63
HE 240 A	226	227	QP Solai	PolG	0	0	0	0	63	148	0	58
HE 240 A	226	227	QV Solai	PolG	26	0	0	0	2	26	0	19
HE 240 A	226	227	Neve	PolG	26	0	0	0	20	148	0	39
HE 240 A	226	227	Neve	PolG	26	0	0	0	3	148	0	36
HE 240 A	226	227	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	134	0	60
HE 240 A	227	228	Peso Proprio	UnitG	0	0	0	0	5	23	0	63
HE 240 A	227	228	QP Solai	PolG	23	0	0	0	63	134	0	58
HE 240 A	227	228	QV Solai	PolG	0	0	0	0	2	23	0	20
HE 240 A	227	228	Neve	PolG	23	0	0	0	20	134	0	39
HE 240 A	227	228	Neve	PolG	23	0	0	0	3	23	0	36
HE 240 A	227	228	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	122	0	60
HE 240 A	228	229	Peso Proprio	UnitG	0	0	0	0	5	22	0	63
HE 240 A	228	229	QP Solai	PolG	22	0	0	0	63	123	0	58
HE 240 A	228	229	QV Solai	PolG	0	0	0	0	2	22	0	20
HE 240 A	228	229	Neve	PolG	22	0	0	0	20	123	0	39
HE 240 A	228	229	Neve	PolG	22	0	0	0	3	22	0	36
HE 240 A	228	229	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	113	0	60
HE 240 A	229	319	Peso Proprio	UnitG	0	0	0	0	5	19	0	63
HE 240 A	229	319	QP Solai	PolG	20	0	0	0	63	113	0	58
HE 240 A	229	319	QV Solai	PolG	0	0	0	0	2	20	0	20
HE 240 A	229	319	Neve	PolG	20	0	0	0	20	113	0	39
HE 240 A	229	319	Neve	PolG	20	0	0	0	3	20	0	36
HE 240 A	229	319	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	108	0	60
HE 240 A	319	320	Peso Proprio	UnitG	0	0	0	0	5	19	0	63
HE 240 A	319	320	QP Solai	PolG	19	0	0	0	63	108	0	58
HE 240 A	319	320	QV Solai	PolG	0	0	0	0	2	19	0	20
HE 240 A	319	320	Neve	PolG	19	0	0	0	20	108	0	39
HE 240 A	319	320	Neve	PolG	19	0	0	0	3	19	0	36
HE 240 A	319	320	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	112	0	60
HE 240 A	320	308	Peso Proprio	UnitG	0	0	0	0	5	20	0	63
HE 240 A	320	308	QP Solai	PolG	20	0	0	0	63	112	0	58
HE 240 A	320	308	QV Solai	PolG	0	0	0	0	2	20	0	20
HE 240 A	320	308	Neve	PolG	20	0	0	0	20	112	0	39
HE 240 A	320	308	Neve	PolG	20	0	0	0	3	20	0	36
HE 240 A	320	308	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	182	0	60
HE 240 A	102	123	Peso Proprio	UnitG	0	0	0	0	64	16	0	98
HE 240 A	102	123	QP Solai	PolG	16	0	0	0	98	151	0	100
HE 240 A	102	123	QV Solai	PolG	151	0	0	0	100	182	0	42
HE 240 A	102	123	Neve	PolG	0	0	0	0	20	16	0	32
HE 240 A	102	123	Neve	PolG	151	0	0	0	32	151	0	34
HE 240 A	102	123	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	178	0	60
HE 240 A	102	123	QP Solai	PolG	15	0	0	0	64	15	0	113
HE 240 A	102	123	QV Solai	PolG	151	0	0	0	39	182	0	3
HE 240 A	102	123	Neve	PolG	0	0	0	0	3	16	0	25
HE 240 A	102	123	Neve	PolG	16	0	0	0	25	182	0	23
HE 240 A	102	123	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	178	0	60
HE 240 A	123	124	Peso Proprio	UnitG	0	0	0	0	60	178	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf	
HE 240 A	123	124	QP Solai	PolG	0	0	0	0	64	17	0	101	
		17			0	0	101	147	0	0	103		
		147			0	0	103	178	0	0	45		
HE 240 A	123	124	QV Solai	PolG	0	0	0	20	17	0	0	32	
		17			0	0	32	147	0	0	33		
		147			0	0	33	178	0	0	14		
HE 240 A	123	124	Neve	PolG	0	0	0	3	17	0	0	26	
		17			0	0	26	178	0	0	24		
					0	0	36	147	0	0	39		
HE 240 A	123	124	Neve	PolG	0	0	0	3	178	0	0	3	
		147			0	0	39	178	0	0			
					Termico ΔXY=15°C,ΔXZ=15°C								
HE 240 A	123	124	Carichi termici	UnitG	0	0	0	60	170	0	0	60	
	124	235			Peso Proprio	PolG	0	0	0	64	17	0	103
	124	235					QP Solai	17	0	0	103	141	0
			QV Solai	PolG	141	0	0	105	170	0	0	47	
					0	0	0	20	17	0	0	33	
					17	0	0	33	141	0	0	34	
HE 240 A	124	235	Neve	PolG	141	0	0	34	170	0	0	15	
					0	0	3	17	0	0	28		
					17	0	0	28	170	0	0	26	
HE 240 A	124	235	Neve	PolG	0	0	0	36	141	0	0	39	
					141	0	0	39	170	0	0	3	
					Termico ΔXY=15°C,ΔXZ=15°C								
HE 240 A	124	235	Carichi termici	UnitG	0	0	0	60	159	0	0	60	
	235	236			Peso Proprio	PolG	0	0	0	64	16	0	106
	235	236					QP Solai	16	0	0	106	131	0
			QV Solai	PolG	131	0	0	107	159	0	0	49	
					0	0	0	20	16	0	0	34	
					16	0	0	34	131	0	0	34	
HE 240 A	235	236	Neve	PolG	131	0	0	34	159	0	0	16	
					0	0	0	36	131	0	0	39	
					131	0	0	39	159	0	0	3	
HE 240 A	235	236	Neve	PolG	0	0	0	29	159	0	0	29	
					16	0	0	3	16	0	0	27	
					Termico ΔXY=15°C,ΔXZ=15°C								
HE 240 A	235	236	Carichi termici	UnitG	0	0	0	60	148	0	0	60	
	236	237			Peso Proprio	PolG	0	0	0	64	16	0	108
	236	237					QP Solai	16	0	0	108	122	0
			QV Solai	PolG	122	0	0	110	148	0	0	52	
					0	0	0	20	16	0	0	35	
					16	0	0	35	122	0	0	35	
HE 240 A	236	237	Neve	PolG	122	0	0	35	148	0	0	17	
					0	0	0	36	122	0	0	39	
					122	0	0	39	148	0	0	3	
HE 240 A	236	237	Neve	PolG	0	0	0	3	16	0	0	30	
					0	0	0	30	148	0	0	29	
					Termico ΔXY=15°C,ΔXZ=15°C								
HE 240 A	236	237	Carichi termici	UnitG	0	0	0	60	134	0	0	60	
	237	238			Peso Proprio	PolG	0	0	0	64	15	0	110
	237	238					QP Solai	15	0	0	110	111	0
			QV Solai	PolG	111	0	0	112	134	0	0	54	
					0	0	0	20	15	0	0	35	
					15	0	0	35	111	0	0	36	
HE 240 A	237	238	Neve	PolG	111	0	0	36	134	0	0	17	
					0	0	0	36	111	0	0	39	
					111	0	0	39	134	0	0	3	
HE 240 A	237	238	Neve	PolG	0	0	0	3	15	0	0	32	
					15	0	0	32	134	0	0	30	
					Termico ΔXY=15°C,ΔXZ=15°C								
HE 240 A	237	238	Carichi termici	UnitG	0	0	0	60	123	0	0	60	
	238	239			Peso Proprio	PolG	0	0	0	64	15	0	113
	238	239					QP Solai	15	0	0	113	101	0
			QV Solai	PolG	101	0	0	114	123	0	0	56	
					0	0	0	20	15	0	0	36	
					15	0	0	36	101	0	0	37	
					101	0	0	37	123	0	0	18	

Sezione	Ni	NF	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	234	321	Neve	PolG	99	0	0	35	113	0	0	18
HE 240 A	234	321	Neve	PolG	99	0	0	35	113	0	0	2
HE 240 A	234	321	Carichi termici	Termico	6	0	0	34	113	0	0	33
HE 240 A	321	322	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
	321	322	QP Solai	PolG	6	0	0	111	94	0	0	114
	321	322										
HE 240 A	321	322	QV Solai	PolG	94	0	0	114	108	0	0	59
HE 240 A	321	322	Neve	PolG	6	0	0	35	94	0	0	37
HE 240 A	321	322	Neve	PolG	94	0	0	37	108	0	0	19
HE 240 A	321	322	Neve	PolG	6	0	0	35	108	0	0	35
HE 240 A	321	322	Neve	PolG	0	0	0	34	94	0	0	36
HE 240 A	321	322	Carichi termici	Termico	94	0	0	36	108	0	0	2
HE 240 A	322	310	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
	322	310	QP Solai	PolG	0	0	0	59	7	0	0	115
	322	310			7	0	0	115	97	0	0	119
HE 240 A	322	310	QV Solai	PolG	97	0	0	119	112	0	0	61
HE 240 A	322	310	Neve	PolG	7	0	0	37	97	0	0	38
HE 240 A	322	310	Neve	PolG	97	0	0	38	112	0	0	20
HE 240 A	322	310	Neve	PolG	97	0	0	38	112	0	0	38
HE 240 A	322	310	Neve	PolG	0	0	0	2	7	0	0	36
HE 240 A	322	310	Carichi termici	Termico	7	0	0	36	112	0	0	36
Trave 8003												
HE 240 A	104	115	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
	104	115	QP Solai	PolG	0	0	0	70	175	0	0	74
					175	0	0	74	180	0	0	47
HE 240 A	104	115	QV Solai	PolG	180	0	0	10	182	0	0	0
HE 240 A	104	115	Neve	PolG	175	0	0	22	175	0	0	24
HE 240 A	104	115	Neve	PolG	180	0	0	24	180	0	0	15
HE 240 A	104	115	Neve	PolG	175	0	0	3	182	0	0	0
HE 240 A	104	115	Neve	PolG	175	0	0	22	175	0	0	23
HE 240 A	104	115	Neve	PolG	175	0	0	23	182	0	0	0
HE 240 A	104	115	Carichi termici	Termico	0	0	0	22	180	0	0	23
HE 240 A	104	115	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
	115	116	QP Solai	PolG	0	0	0	75	170	0	0	79
	115	116			170	0	0	79	175	0	0	51
HE 240 A	115	116	QV Solai	PolG	175	0	0	51	178	0	0	0
HE 240 A	115	116	Neve	PolG	170	0	0	24	170	0	0	25
HE 240 A	115	116	Neve	PolG	170	0	0	25	175	0	0	16
HE 240 A	115	116	Neve	PolG	175	0	0	16	178	0	0	0
HE 240 A	115	116	Neve	PolG	175	0	0	23	175	0	0	24
HE 240 A	115	116	Neve	PolG	175	0	0	24	178	0	0	0
HE 240 A	115	116	Carichi termici	Termico	170	0	0	23	170	0	0	25
HE 240 A	115	116	Peso Proprio	UnifG	0	0	0	25	178	0	0	0
	116	215	QP Solai	PolG	0	0	0	80	162	0	0	60
	116	215			162	0	0	84	167	0	0	56
HE 240 A	116	215	QV Solai	PolG	167	0	0	56	170	0	0	1
HE 240 A	116	215	Neve	PolG	167	0	0	26	162	0	0	27
HE 240 A	116	215	Neve	PolG	167	0	0	18	170	0	0	18
HE 240 A	116	215	Neve	PolG	167	0	0	25	162	0	0	27
HE 240 A	116	215	Neve	PolG	162	0	0	27	170	0	0	0
HE 240 A	116	215	Neve	PolG	167	0	0	25	167	0	0	26
HE 240 A	116	215	Carichi termici	Termico	167	0	0	26	170	0	0	0

Sezione	Ni	Nf	Cond.	Tiplo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A HE 240 A	215	216	Peso Proprio QP Solai	UnifG PolG	0	0	0	0	60	159	0	60
	215	216			0	0	0	85	151	0	89	
	215	216			151	0	0	89	156	0	60	
HE 240 A	215	216	QV Solai	PolG	156	0	0	60	159	0	1	
	215	216			0	0	0	27	151	0	29	
	215	216			151	0	0	29	156	0	19	
HE 240 A	215	216	Nevve	PolG	156	0	0	19	159	0	0	
	215	216			0	0	0	26	151	0	28	
	215	216			151	0	0	28	159	0	0	
HE 240 A	215	216	Nevve	PolG	0	0	0	26	156	0	0	
	215	216			156	0	0	27	159	0	0	
	215	216			0	0	0	27	159	0	0	
HE 240 A HE 240 A HE 240 A	215	216	Carichi termici Peso Proprio QP Solai	Termico UnifG PolG	0	0	0	60	148	0	0	
	216	217			0	0	89	141	0	94		
	216	217			141	0	0	94	145	0	63	
HE 240 A	216	217	QV Solai	PolG	145	0	0	63	148	0	1	
	216	217			0	0	0	29	141	0	30	
	216	217			141	0	0	30	145	0	20	
HE 240 A	216	217	Nevve	PolG	145	0	0	20	148	0	0	
	216	217			0	0	0	28	141	0	0	
	216	217			141	0	0	29	148	0	0	
HE 240 A	216	217	Nevve	PolG	0	0	0	28	145	0	0	
	216	217			145	0	0	29	148	0	0	
	216	217			0	0	0	29	148	0	0	
HE 240 A HE 240 A HE 240 A	216	217	Carichi termici Peso Proprio QP Solai	Termico UnifG PolG	0	0	0	60	134	0	0	
	217	218			0	0	94	128	0	98		
	217	218			128	0	0	98	132	0	67	
HE 240 A	217	218	QV Solai	PolG	132	0	0	67	134	0	1	
	217	218			0	0	0	30	128	0	32	
	217	218			128	0	0	32	132	0	22	
HE 240 A	217	218	Nevve	PolG	132	0	0	22	134	0	0	
	217	218			0	0	29	132	0	30		
	217	218			132	0	0	30	134	0	0	
HE 240 A HE 240 A HE 240 A	217	218	Nevve	PolG	0	0	0	29	128	0	0	
	217	218			128	0	0	31	134	0	0	
	217	218			0	0	0	31	134	0	0	
HE 240 A HE 240 A HE 240 A	217	218	Carichi termici Peso Proprio QP Solai	Termico UnifG PolG	0	0	0	60	123	0	0	
	218	219			0	0	99	116	0	103		
	218	219			116	0	0	103	120	0	71	
HE 240 A	218	219	QV Solai	PolG	120	0	0	71	123	0	1	
	218	219			0	0	32	116	0	33		
	218	219			116	0	0	33	120	0	23	
HE 240 A	218	219	Nevve	PolG	120	0	0	23	123	0	0	
	218	219			0	0	31	120	0	32		
	218	219			120	0	0	32	123	0	0	
HE 240 A	218	219	Nevve	PolG	0	0	0	30	116	0	0	
	218	219			116	0	0	32	123	0	32	
	218	219			0	0	0	32	123	0	0	
HE 240 A HE 240 A HE 240 A	218	219	Carichi termici Peso Proprio QP Solai	Termico UnifG PolG	0	0	0	60	113	0	0	
	219	315			0	0	108	107	0	108		
	219	315			107	0	0	108	111	0	75	
HE 240 A	219	315	QV Solai	PolG	111	0	0	75	113	0	1	
	219	315			0	0	0	33	107	0	34	
	219	315			107	0	0	34	111	0	24	
HE 240 A	219	315	Nevve	PolG	111	0	0	24	113	0	0	
	219	315			0	0	32	107	0	34		
	219	315			107	0	0	34	113	0	0	
HE 240 A	219	315	Nevve	PolG	0	0	0	32	111	0	0	
	219	315			111	0	0	33	113	0	33	
	219	315			0	0	0	33	113	0	0	
HE 240 A HE 240 A HE 240 A	219	315	Carichi termici Peso Proprio QP Solai	Termico UnifG PolG	0	0	0	60	108	0	0	
	315	316			0	0	108	102	0	112		
	315	316			102	0	0	112	106	0	79	
HE 240 A	315	316	QV Solai	PolG	106	0	0	79	108	0	1	
	315	316			102	0	0	35	102	0	36	
	315	316			102	0	0	36	106	0	25	

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	315	316	Neve	PolG	106	0	0	0	25	108	0	0
					PolG	0	0	0	34	106	0	35
					PolG	106	0	0	35	108	0	0
HE 240 A	315	316	Neve	PolG	0	0	0	33	102	0	0	35
					102	0	0	0	35	108	0	0
ΔXY=15°C,ΔXZ=15°C												
HE 240 A	315	316	Canchi termici	Termico								
HE 240 A	316	311	Peso Proprio	UnifG	0	0	0	0	60	112	0	60
HE 240 A	316	311	QP Solai	PolG	0	0	0	0	117	105	0	117
HE 240 A	316	311			105	0	0	0	117	110	0	83
					110	0	0	83	112	0	0	1
HE 240 A	316	311	QV Solai	PolG	0	0	0	36	105	0	0	37
					105	0	0	37	110	0	0	27
HE 240 A	316	311	Neve	PolG	0	0	0	27	112	0	0	0
					110	0	0	35	105	0	0	36
HE 240 A	316	311	Neve	PolG	0	0	0	36	112	0	0	0
HE 240 A	316	311	Neve	PolG	0	0	0	35	110	0	0	36
					110	0	0	36	112	0	0	0
ΔXY=15°C,ΔXZ=15°C												
HE 240 A	316	311	Canchi termici	Termico								
Trave 8004												
HE 240 A	105	125	Peso Proprio	UnifG	0	0	0	0	60	181	0	60
HE 240 A	105	125	QP Solai	PolG	0	0	0	0	95	170	0	97
					170	0	0	97	182	0	39	
HE 240 A	105	125	QV Solai	PolG	0	0	0	30	170	0	0	31
					170	0	0	31	182	0	0	12
HE 240 A	105	125	Neve	PolG	0	0	0	23	182	0	0	23
HE 240 A	105	125	Neve	PolG	0	0	0	36	170	0	0	37
					170	0	0	37	182	0	0	1
ΔXY=15°C,ΔXZ=15°C												
HE 240 A	105	125	Canchi termici	Termico								
HE 240 A	125	126	Peso Proprio	UnifG	0	0	0	0	60	177	0	60
HE 240 A	125	126	QP Solai	PolG	0	0	0	97	166	0	0	99
					166	0	0	99	178	0	0	41
HE 240 A	125	126	QV Solai	PolG	0	0	0	31	166	0	0	32
					166	0	0	32	178	0	0	13
HE 240 A	125	126	Neve	PolG	0	0	0	36	166	0	0	37
					166	0	0	37	178	0	0	1
HE 240 A	125	126	Neve	PolG	0	0	0	24	178	0	0	24
ΔXY=15°C,ΔXZ=15°C												
HE 240 A	125	126	Canchi termici	Termico								
HE 240 A	125	126	Peso Proprio	UnifG	0	0	0	0	60	170	0	60
HE 240 A	126	240	QP Solai	PolG	0	0	0	60	2	0	0	99
HE 240 A	126	240			2	0	0	99	159	0	0	102
					159	0	0	102	170	0	0	43
HE 240 A	126	240	QV Solai	PolG	0	0	0	19	2	0	0	32
					2	0	0	32	159	0	0	33
					159	0	0	33	170	0	0	14
HE 240 A	126	240	Neve	PolG	0	0	0	1	2	0	0	26
					2	0	0	26	170	0	0	26
HE 240 A	126	240	Neve	PolG	0	0	0	36	159	0	0	37
					159	0	0	37	170	0	0	1
ΔXY=15°C,ΔXZ=15°C												
HE 240 A	126	240	Canchi termici	Termico								
HE 240 A	126	240	Peso Proprio	UnifG	0	0	0	0	60	158	0	60
HE 240 A	240	241	QP Solai	PolG	0	0	0	60	2	0	0	102
HE 240 A	240	241			2	0	0	102	149	0	0	104
					149	0	0	104	158	0	0	46
HE 240 A	240	241	QV Solai	PolG	0	0	0	19	2	0	0	33
					2	0	0	33	149	0	0	33
					149	0	0	33	158	0	0	15
HE 240 A	240	241	Neve	PolG	0	0	0	1	2	0	0	15
					2	0	0	27	158	0	0	27
HE 240 A	240	241	Neve	PolG	0	0	0	36	149	0	0	37
					149	0	0	37	158	0	0	1
ΔXY=15°C,ΔXZ=15°C												
HE 240 A	240	241	Canchi termici	Termico								
HE 240 A	240	241	Peso Proprio	UnifG	0	0	0	0	60	148	0	60
HE 240 A	241	242	QP Solai	PolG	0	0	0	60	2	0	0	104
HE 240 A	241	242			2	0	0	104	139	0	0	106
					139	0	0	106	148	0	0	48
HE 240 A	241	242	QV Solai	PolG	0	0	0	19	142	0	0	33

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					2	0	0	33	139	0	0	33
					139	0	0	0	34	148	0	15
HE 240 A	241	242	Neve	PolG	0	0	0	1	2	0	0	28
					2	0	0	28	148	0	0	29
HE 240 A	241	242	Neve	PolG	139	0	0	36	139	0	0	37
					AXY=15°C,ΔXZ=15°C			37	148	0	0	1
					139	0	0	0	0	0	0	60
HE 240 A	241	242	Carichi termici	Termico	0	0	0	60	134	0	0	60
HE 240 A	242	243	Peso Proprio	UnifG	0	0	0	60	2	0	0	106
HE 240 A	242	243	QP Solai	PolG	2	0	0	106	126	0	0	109
					126	0	0	109	134	0	0	50
HE 240 A	242	243	QV Solai	PolG	2	0	0	19	2	0	0	34
					2	0	0	34	126	0	0	35
					126	0	0	35	134	0	0	16
HE 240 A	242	243	Neve	PolG	0	0	0	36	126	0	0	37
					126	0	0	37	134	0	0	1
HE 240 A	242	243	Neve	PolG	0	0	0	1	2	0	0	30
					2	0	0	30	134	0	0	30
					AXY=15°C,ΔXZ=15°C							
HE 240 A	242	243	Carichi termici	Termico	0	0	0	60	122	0	0	60
HE 240 A	243	244	Peso Proprio	UnifG	0	0	0	60	2	0	0	109
HE 240 A	243	244	QP Solai	PolG	2	0	0	109	115	0	0	111
					115	0	0	111	123	0	0	53
HE 240 A	243	244	QV Solai	PolG	0	0	0	19	2	0	0	35
					2	0	0	35	115	0	0	36
					115	0	0	36	123	0	0	17
HE 240 A	243	244	Neve	PolG	0	0	0	1	2	0	0	31
					2	0	0	31	123	0	0	32
HE 240 A	243	244	Neve	PolG	0	0	0	36	115	0	0	37
					115	0	0	37	123	0	0	1
					AXY=15°C,ΔXZ=15°C							
HE 240 A	243	244	Carichi termici	Termico	0	0	0	60	113	0	0	60
HE 240 A	244	325	Peso Proprio	UnifG	0	0	0	60	2	0	0	111
HE 240 A	244	325	QP Solai	PolG	2	0	0	111	107	0	0	113
					107	0	0	113	113	0	0	55
HE 240 A	244	325	QV Solai	PolG	0	0	0	19	2	0	0	36
					2	0	0	36	107	0	0	36
					107	0	0	36	113	0	0	18
HE 240 A	244	325	Neve	PolG	0	0	0	1	2	0	0	33
					2	0	0	33	113	0	0	33
HE 240 A	244	325	Neve	PolG	0	0	0	36	107	0	0	37
					107	0	0	37	113	0	0	1
					AXY=15°C,ΔXZ=15°C							
HE 240 A	244	325	Carichi termici	Termico	0	0	0	60	108	0	0	60
HE 240 A	325	326	Peso Proprio	UnifG	0	0	0	60	2	0	0	114
HE 240 A	325	326	QP Solai	PolG	2	0	0	114	102	0	0	116

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	326	312		Termico	0	0	0	0	60	181	0	60
Trave 8005												
HE 240 A	106	127	Peso Proprio	UnifG	0	0	0	0	60	181	0	60
HE 240 A	106	127	QP Solai	PolG	12	0	0	0	60	172	0	118
					172	0	0	0	118	182	0	60
HE 240 A	106	127	QV Solai	PolG	0	0	0	0	19	12	0	38
					12	0	0	0	38	172	0	38
					172	0	0	0	38	182	0	19
HE 240 A	106	127	Neve	PolG	0	0	0	0	36	172	0	37
					172	0	0	0	37	182	0	1
HE 240 A	106	127	Neve	PolG	0	0	0	0	1	12	0	37
					12	0	0	0	37	182	0	36
HE 240 A	106	127	Carichi termici	Termico	0	0	0	0	60	177	0	60
HE 240 A	127	128	Peso Proprio	UnifG	0	0	0	0	60	11	0	118
HE 240 A	127	128	QP Solai	PolG	0	0	0	0	118	168	0	118
					11	0	0	0	118	178	0	60
HE 240 A	127	128	QV Solai	PolG	0	0	0	0	19	11	0	38
					11	0	0	0	38	168	0	38
					168	0	0	0	38	178	0	19
HE 240 A	127	128	Neve	PolG	0	0	0	0	1	11	0	37
					11	0	0	0	37	178	0	36
HE 240 A	127	128	Neve	PolG	0	0	0	0	36	168	0	37
					168	0	0	0	37	178	0	1
HE 240 A	127	128	Carichi termici	Termico	0	0	0	0	60	170	0	60
HE 240 A	128	245	Peso Proprio	UnifG	0	0	0	0	60	11	0	118
HE 240 A	128	245	QP Solai	PolG	0	0	0	0	118	160	0	118
					11	0	0	0	118	170	0	60
HE 240 A	128	245	QV Solai	PolG	0	0	0	0	19	11	0	38
					11	0	0	0	38	160	0	38
					160	0	0	0	38	170	0	19
HE 240 A	128	245	Neve	PolG	0	0	0	0	36	160	0	37
					160	0	0	0	37	170	0	1
HE 240 A	128	245	Neve	PolG	0	0	0	0	1	11	0	37
					11	0	0	0	37	170	0	36
HE 240 A	128	245	Carichi termici	Termico	0	0	0	0	60	158	0	60
HE 240 A	245	246	Peso Proprio	UnifG	0	0	0	0	60	10	0	118
HE 240 A	245	246	QP Solai	PolG	0	0	0	0	118	150	0	60
					10	0	0	0	118	159	0	60
HE 240 A	245	246	QV Solai	PolG	0	0	0	0	19	10	0	38
					10	0	0	0	38	150	0	38
					150	0	0	0	38	159	0	19
HE 240 A	245	246	Neve	PolG	0	0	0	0	36	150	0	37
					10	0	0	0	37	159	0	36
HE 240 A	245	246	Neve	PolG	0	0	0	0	36	150	0	37
					150	0	0	0	37	159	0	1
HE 240 A	245	246	Carichi termici	Termico	0	0	0	0	60	148	0	60
HE 240 A	246	247	Peso Proprio	UnifG	0	0	0	0	60	9	0	118
HE 240 A	246	247	QP Solai	PolG	0	0	0	0	118	140	0	118
					9	0	0	0	118	148	0	60
HE 240 A	246	247	QV Solai	PolG	0	0	0	0	19	9	0	38
					9	0	0	0	38	140	0	38
					140	0	0	0	38	148	0	19
HE 240 A	246	247	Neve	PolG	0	0	0	0	36	140	0	37
					140	0	0	0	37	148	0	1
HE 240 A	246	247	Neve	PolG	0	0	0	0	1	9	0	37
					9	0	0	0	37	148	0	36
HE 240 A	246	247	Carichi termici	Termico	0	0	0	0	60	134	0	60
HE 240 A	247	248	Peso Proprio	UnifG	0	0	0	0	60	8	0	118
HE 240 A	247	248	QP Solai	PolG	0	0	0	0	118	127	0	118
					127	0	0	0	118	134	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	247	248	QV Solai	PolG	0	0	0	0	19	8	0	38
					127	0	0	0	38	127	0	38
HE 240 A	247	248	Neve	PolG	0	0	0	0	36	127	0	37
					127	0	0	0	37	134	0	1
HE 240 A	247	248	Neve	PolG	0	0	0	0	1	8	0	37
					8	0	0	0	37	134	0	36
HE 240 A	247	248	Carichi termici	Termico	0	0	0	0	60	123	0	60
HE 240 A	248	249	Peso Proprio	UnifG	0	0	0	0	60	7	0	118
HE 240 A	248	249	QP Solai	PolG	0	0	0	0	118	116	0	118
					7	0	0	0	118	123	0	60
HE 240 A	248	249	QV Solai	PolG	0	0	0	0	19	7	0	38
					7	0	0	0	38	116	0	38
HE 240 A	248	249	Neve	PolG	0	0	0	0	1	7	0	37
					7	0	0	0	37	123	0	36
HE 240 A	248	249	Neve	PolG	0	0	0	0	36	116	0	37
					116	0	0	0	37	123	0	1
HE 240 A	248	249	Carichi termici	Termico	0	0	0	0	60	113	0	60
HE 240 A	249	327	Peso Proprio	UnifG	0	0	0	0	60	7	0	118
HE 240 A	249	327	QP Solai	PolG	0	0	0	0	118	107	0	60
					107	0	0	0	118	113	0	60
HE 240 A	249	327	QV Solai	PolG	0	0	0	0	19	7	0	38
					7	0	0	0	38	107	0	38
					107	0	0	0	38	113	0	19
HE 240 A	249	327	Neve	PolG	0	0	0	0	1	7	0	37
					7	0	0	0	37	113	0	36
HE 240 A	249	327	Neve	PolG	0	0	0	0	36	107	0	37
					107	0	0	0	37	113	0	1
HE 240 A	249	327	Carichi termici	Termico	0	0	0	0	60	108	0	60
HE 240 A	327	328	Peso Proprio	UnifG	0	0	0	0	60	6	0	118
HE 240 A	327	328	QP Solai	PolG	0	0	0	0	118	102	0	118
					6	0	0	0	118	108	0	60
HE 240 A	327	328	QV Solai	PolG	0	0	0	0	19	6	0	38
					6	0	0	0	38	102	0	38
HE 240 A	327	328	Neve	PolG	0	0	0	0	38	108	0	19
					102	0	0	0	1	6	0	37
HE 240 A	327	328	Neve	PolG	0	0	0	0	37	108	0	36
					6	0	0	0	36	102	0	37
HE 240 A	327	328	QV Solai	PolG	0	0	0	0	37	108	0	1
					102	0	0	0	37	108	0	0
HE 240 A	327	328	Carichi termici	Termico	0	0	0	0	60	112	0	60
HE 240 A	328	313	Peso Proprio	UnifG	0	0	0	0	60	6	0	118
HE 240 A	328	313	QP Solai	PolG	0	0	0	0	118	106	0	118
					6	0	0	0	118	112	0	60
HE 240 A	328	313	QV Solai	PolG	0	0	0	0	19	6	0	38
					106	0	0	0	38	106	0	38
HE 240 A	328	313	Neve	PolG	0	0	0	0	38	112	0	19
					106	0	0	0	1	6	0	37
HE 240 A	328	313	Neve	PolG	0	0	0	0	37	112	0	36
					6	0	0	0	36	106	0	37
HE 240 A	328	313	Carichi termici	Termico	0	0	0	0	37	112	0	1
Trave 8006												
HE 240 A	107	117	Peso Proprio	UnifG	0	0	0	0	60	182	0	60
HE 240 A	107	117	QP Solai	PolG	0	0	0	0	2	10	0	60
					10	0	0	0	60	182	0	58
HE 240 A	107	117	QV Solai	PolG	0	0	0	0	1	10	0	19
					10	0	0	0	19	182	0	19
HE 240 A	107	117	Neve	PolG	0	0	0	0	1	10	0	37
					10	0	0	0	37	182	0	36
HE 240 A	107	117	Carichi termici	Termico	0	0	0	0	60	178	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	OXf	QYf	QZf
HE 240 A	117	118	QP Solai	PolG	0	0	0	2	10	0	0	60
HE 240 A	117	118	QV Solai	PolG	10	0	0	60	178	0	0	58
HE 240 A	117	118	Neve	PolG	0	0	0	1	10	0	0	19
HE 240 A	117	118	Neve	PolG	10	0	0	19	178	0	0	19
HE 240 A	117	118	Carichi termici	Termico	10	0	0	37	178	0	0	36
HE 240 A	117	118	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	170	0	60
HE 240 A	118	220	QP Solai	PolG	0	0	0	2	9	0	0	60
HE 240 A	118	220	QV Solai	PolG	9	0	0	60	170	0	0	58
HE 240 A	118	220	Neve	PolG	0	0	0	1	9	0	0	19
HE 240 A	118	220	Carichi termici	Termico	9	0	0	19	170	0	0	19
HE 240 A	118	220	Neve	PolG	9	0	0	1	9	0	0	37
HE 240 A	118	220	Carichi termici	Termico	9	0	0	37	170	0	0	36
HE 240 A	220	221	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	159	0	60
HE 240 A	220	221	QP Solai	PolG	0	0	0	2	9	0	0	60
HE 240 A	220	221	QV Solai	PolG	9	0	0	60	159	0	0	58
HE 240 A	220	221	Neve	PolG	0	0	0	1	9	0	0	19
HE 240 A	220	221	Carichi termici	Termico	9	0	0	19	159	0	0	19
HE 240 A	220	221	Neve	PolG	9	0	0	1	9	0	0	37
HE 240 A	220	221	Carichi termici	Termico	9	0	0	37	159	0	0	36
HE 240 A	221	222	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	148	0	60
HE 240 A	221	222	QP Solai	PolG	0	0	0	2	8	0	0	60
HE 240 A	221	222	QV Solai	PolG	8	0	0	60	148	0	0	58
HE 240 A	221	222	Neve	PolG	0	0	0	1	8	0	0	19
HE 240 A	221	222	Carichi termici	Termico	8	0	0	19	148	0	0	19
HE 240 A	221	222	Neve	PolG	8	0	0	1	8	0	0	37
HE 240 A	221	222	Carichi termici	Termico	8	0	0	37	148	0	0	36
HE 240 A	222	223	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	134	0	60
HE 240 A	222	223	QP Solai	PolG	0	0	0	2	7	0	0	60
HE 240 A	222	223	QV Solai	PolG	7	0	0	60	134	0	0	58
HE 240 A	222	223	Neve	PolG	0	0	0	1	7	0	0	19
HE 240 A	222	223	Carichi termici	Termico	7	0	0	19	134	0	0	19
HE 240 A	222	223	Neve	PolG	7	0	0	1	7	0	0	37
HE 240 A	222	223	Carichi termici	Termico	7	0	0	37	134	0	0	36
HE 240 A	223	224	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	123	0	60
HE 240 A	223	224	QP Solai	PolG	0	0	0	2	7	0	0	60
HE 240 A	223	224	QV Solai	PolG	7	0	0	60	123	0	0	58
HE 240 A	223	224	Neve	PolG	0	0	0	1	7	0	0	19
HE 240 A	223	224	Carichi termici	Termico	7	0	0	19	123	0	0	19
HE 240 A	223	224	Neve	PolG	7	0	0	1	7	0	0	37
HE 240 A	223	224	Carichi termici	Termico	7	0	0	37	123	0	0	36
HE 240 A	224	317	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	113	0	60
HE 240 A	224	317	QP Solai	PolG	0	0	0	2	6	0	0	60
HE 240 A	224	317	QV Solai	PolG	6	0	0	60	113	0	0	58
HE 240 A	224	317	Neve	PolG	0	0	0	1	6	0	0	19
HE 240 A	224	317	Carichi termici	Termico	6	0	0	19	113	0	0	19
HE 240 A	224	317	Neve	PolG	6	0	0	1	6	0	0	37
HE 240 A	224	317	Carichi termici	Termico	6	0	0	37	113	0	0	36
HE 240 A	317	318	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	108	0	60
HE 240 A	317	318	QP Solai	PolG	0	0	0	2	6	0	0	60
HE 240 A	317	318	QV Solai	PolG	6	0	0	60	108	0	0	58
HE 240 A	317	318	Neve	PolG	0	0	0	1	6	0	0	19
HE 240 A	317	318	Carichi termici	Termico	6	0	0	19	108	0	0	19
HE 240 A	317	318	Neve	PolG	6	0	0	1	6	0	0	37
HE 240 A	317	318	Carichi termici	Termico	6	0	0	37	108	0	0	36
HE 240 A	318	314	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	112	0	60
HE 240 A	318	314	QP Solai	PolG	0	0	0	2	6	0	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	OXf	QYf	QZf
HE 240 A	318	314	QV Solai	PolG	6	0	0	0	60	112	0	58
HE 240 A	318	314	Neve	PolG	6	0	0	0	1	6	0	19
HE 240 A	318	314	Carichi termici	Termico	6	0	0	0	37	112	0	36
Trave 8007	318	314	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	77	0	8
IPE 100	16	18	Peso Proprio	UnifG	0	0	0	0	8	77	0	8
IPE 100	16	18	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	18	26	Peso Proprio	UnifG	0	0	0	0	8	90	0	8
IPE 100	18	26	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	162	0	8
IPE 100	20	16	Peso Proprio	UnifG	0	0	0	0	8	162	0	8
IPE 100	20	16	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	149	0	8
IPE 100	22	24	Peso Proprio	UnifG	0	0	0	0	8	149	0	8
IPE 100	22	24	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	150	0	8
IPE 100	24	28	Peso Proprio	UnifG	0	0	0	0	8	150	0	8
IPE 100	24	28	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	26	22	Peso Proprio	UnifG	0	0	0	0	8	89	0	8
IPE 100	26	22	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	77	0	8
Trave 8008	15	17	Peso Proprio	UnifG	0	0	0	0	8	77	0	8
IPE 100	15	17	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	17	25	Peso Proprio	UnifG	0	0	0	0	8	90	0	8
IPE 100	17	25	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	150	0	8
IPE 100	19	15	Peso Proprio	UnifG	0	0	0	0	8	150	0	8
IPE 100	19	15	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	149	0	8
IPE 100	21	23	Peso Proprio	UnifG	0	0	0	0	8	149	0	8
IPE 100	21	23	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	150	0	8
IPE 100	23	27	Peso Proprio	UnifG	0	0	0	0	8	150	0	8
IPE 100	23	27	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	25	21	Peso Proprio	UnifG	0	0	0	0	8	89	0	8
IPE 100	25	21	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	162	0	1500
Fondazione 9003	1	2	Peso Proprio	UnifG	0	0	0	0	1500	162	0	1500
F60x100	2	3	Peso Proprio	UnifG	0	0	0	0	1500	89	0	1500
F60x100	3	4	Peso Proprio	UnifG	0	0	0	0	1500	90	0	1500
F60x100	4	5	Peso Proprio	UnifG	0	0	0	0	1500	89	0	1500
F60x100	5	6	Peso Proprio	UnifG	0	0	0	0	1500	149	0	1500
F60x100	6	7	Peso Proprio	UnifG	0	0	0	0	1500	162	0	1500
Fondazione 9004	208	209	Peso Proprio	UnifG	0	0	0	0	1500	161	0	1500
F60x100	209	210	Peso Proprio	UnifG	0	0	0	0	1500	150	0	1500
F60x100	210	211	Peso Proprio	UnifG	0	0	0	0	1500	149	0	1500
F60x100	211	212	Peso Proprio	UnifG	0	0	0	0	1500	149	0	1500
F60x100	212	213	Peso Proprio	UnifG	0	0	0	0	1500	150	0	1500
F60x100	213	214	Peso Proprio	UnifG	0	0	0	0	1500	162	0	1500
Generica 7001	1	15	Peso Proprio	UnifG	0	0	0	0	2	310	0	2
Fil6	1	15	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	2	202	0	2
Generica 7002	15	20	Peso Proprio	UnifG	0	0	0	0	2	202	0	2
Fil6	15	20	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	2	202	0	2
Generica 7003	20	102	Peso Proprio	UnifG	0	0	0	0	2	202	0	2
Fil6	20	102	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	2	390	0	2
Generica 7004	102	120	Peso Proprio	UnifG	0	0	0	0	2	390	0	2
Fil6	102	120	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	2	360	0	2
Generica 7005	120	236	Peso Proprio	UnifG	0	0	0	0	2	360	0	2
Fil6	120	236	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	2	319	0	2
Generica 7006	236	228	Peso Proprio	UnifG	0	0	0	0	2	319	0	2
Fil6	236	228	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	2	202	0	2
Generica 7007	236	228	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	2	202	0	2

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	OXf	OYf	QZf
Fil6	228	323	Peso Proprio	UnitG	0	0	0	2	278	0	0	2
	228	323	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7008												
Fil6	323	308	Peso Proprio	UnitG	0	0	0	2	264	0	0	2
Fil6	323	308	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7009												
Fil6	308	209	Peso Proprio	UnitG	0	0	0	2	401	0	0	2
Fil6	308	209	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7010												
Fil6	208	309	Peso Proprio	UnitG	0	0	0	2	401	0	0	2
Fil6	208	309	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7011												
Fil6	309	319	Peso Proprio	UnitG	0	0	0	2	264	0	0	2
Fil6	309	319	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7012												
Fil6	319	238	Peso Proprio	UnitG	0	0	0	2	278	0	0	2
Fil6	319	238	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7013												
Fil6	238	226	Peso Proprio	UnitG	0	0	0	2	319	0	0	2
Fil6	238	226	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7014												
Fil6	226	124	Peso Proprio	UnitG	0	0	0	2	361	0	0	2
Fil6	226	124	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7015												
Fil6	124	101	Peso Proprio	UnitG	0	0	0	2	389	0	0	2
Fil6	124	101	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7016												
Fil6	101	16	Peso Proprio	UnitG	0	0	0	2	202	0	0	2
Fil6	101	16	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7017												
Fil6	16	19	Peso Proprio	UnitG	0	0	0	2	202	0	0	2
Fil6	16	19	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7018												
Fil6	19	2	Peso Proprio	UnitG	0	0	0	2	310	0	0	2
Fil6	19	2	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7019												
Fil6	102	122	Peso Proprio	UnitG	0	0	0	2	372	0	0	2
Fil6	102	122	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7020												
Fil6	122	104	Peso Proprio	UnitG	0	0	0	2	372	0	0	2
Fil6	122	104	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7021												
Fil6	104	126	Peso Proprio	UnitG	0	0	0	2	371	0	0	2
Fil6	104	126	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7022												
Fil6	126	106	Peso Proprio	UnitG	0	0	0	2	389	0	0	2
Fil6	126	106	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7023												
Fil6	106	118	Peso Proprio	UnitG	0	0	0	2	389	0	0	2
Fil6	106	118	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7024												
Fil6	118	246	Peso Proprio	UnitG	0	0	0	2	361	0	0	2
Fil6	118	246	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7025												
Fil6	246	223	Peso Proprio	UnitG	0	0	0	2	319	0	0	2
Fil6	246	223	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7026												
Fil6	223	327	Peso Proprio	UnitG	0	0	0	2	278	0	0	2
Fil6	223	327	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7027												
Fil6	327	314	Peso Proprio	UnitG	0	0	0	2	264	0	0	2
Fil6	327	314	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7028												
Fil6	314	213	Peso Proprio	UnitG	0	0	0	2	401	0	0	2
Fil6	314	213	Carichi termici	Termico	AXY=15°C,AXZ=15°C							

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	OXf	OYf	QZf
Generica 7029												
Fil6	214	313	Peso Proprio	UnitG	0	0	0	2	401	0	0	2
Fil6	214	313	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7030												
Fil6	313	317	Peso Proprio	UnitG	0	0	0	2	264	0	0	2
Fil6	313	317	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7031												
Fil6	317	248	Peso Proprio	UnitG	0	0	0	2	279	0	0	2
Fil6	317	248	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7032												
Fil6	248	221	Peso Proprio	UnitG	0	0	0	2	319	0	0	2
Fil6	248	221	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7033												
Fil6	221	128	Peso Proprio	UnitG	0	0	0	2	361	0	0	2
Fil6	221	128	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7034												
Fil6	128	107	Peso Proprio	UnitG	0	0	0	2	389	0	0	2
Fil6	128	107	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7035												
Fil6	107	24	Peso Proprio	UnitG	0	0	0	2	202	0	0	2
Fil6	107	24	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7036												
Fil6	24	27	Peso Proprio	UnitG	0	0	0	2	202	0	0	2
Fil6	24	27	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7037												
Fil6	27	6	Peso Proprio	UnitG	0	0	0	2	310	0	0	2
Fil6	27	6	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7038												
Fil6	7	23	Peso Proprio	UnitG	0	0	0	2	310	0	0	2
Fil6	7	23	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7039												
Fil6	23	28	Peso Proprio	UnitG	0	0	0	2	202	0	0	2
Fil6	23	28	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7040												
Fil6	28	106	Peso Proprio	UnitG	0	0	0	2	202	0	0	2
Fil6	28	106	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7041												
Fil6	124	103	Peso Proprio	UnitG	0	0	0	2	371	0	0	2
Fil6	124	103	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7042												
Fil6	103	116	Peso Proprio	UnitG	0	0	0	2	372	0	0	2
Fil6	103	116	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7043												
Fil6	116	105	Peso Proprio	UnitG	0	0	0	2	371	0	0	2
Fil6	116	105	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7044												
Fil6	105	128	Peso Proprio	UnitG	0	0	0	2	389	0	0	2
Fil6	105	128	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7045												
Fil6	309	321	Peso Proprio	UnitG	0	0	0	2	260	0	0	2
Fil6	309	321	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7046												
Fil6	321	311	Peso Proprio	UnitG	0	0	0	2	261	0	0	2
Fil6	321	311	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7047												
Fil6	311	325	Peso Proprio	UnitG	0	0	0	2	261	0	0	2
Fil6	311	325	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7048												
Fil6	325	313	Peso Proprio	UnitG	0	0	0	2	264	0	0	2
Fil6	325	313	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7049												
Fil6	327	312	Peso Proprio	UnitG	0	0	0	2	264	0	0	2
Fil6	327	312	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Generica 7050												
Fil6	312	315	Peso Proprio	UnitG	0	0	0	2	260	0	0	2

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	Oxi	Oxi	OZi	Xf	QXf	QVf	QZf
File6	312	315	Carichi termici	Termico	ΔXY=15°C	ΔXZ=15°C						
Generica 7051												
File6	315	310	Peso Proprio	UnitG	0	0	0	2	260	0	0	2
File6	315	310	Carichi termici	Termico	ΔXY=15°C	ΔXZ=15°C						
Generica 7052												
File6	310	323	Peso Proprio	UnitG	0	0	0	2	261	0	0	2
File6	310	323	Carichi termici	Termico	ΔXY=15°C	ΔXZ=15°C						
Generica 7053												
File6	105	26	Peso Proprio	UnitG	0	0	0	2	162	0	0	2
Generica 7054												
File6	26	21	Peso Proprio	UnitG	0	0	0	2	162	0	0	2
Generica 7055												
File6	21	4	Peso Proprio	UnitG	0	0	0	2	284	0	0	2
Generica 7056												
File6	5	25	Peso Proprio	UnitG	0	0	0	2	285	0	0	2
Generica 7057												
File6	25	22	Peso Proprio	UnitG	0	0	0	2	162	0	0	2
Generica 7058												
File6	22	104	Peso Proprio	UnitG	0	0	0	2	162	0	0	2
Generica 7059												
File6	116	241	Peso Proprio	UnitG	0	0	0	2	345	0	0	2
Generica 7060												
File6	241	218	Peso Proprio	UnitG	0	0	0	2	306	0	0	2
Generica 7061												
File6	218	325	Peso Proprio	UnitG	0	0	0	2	268	0	0	2
Generica 7062												
File6	315	243	Peso Proprio	UnitG	0	0	0	2	269	0	0	2
Generica 7063												
File6	243	216	Peso Proprio	UnitG	0	0	0	2	306	0	0	2
Generica 7064												
File6	216	126	Peso Proprio	UnitG	0	0	0	2	345	0	0	2

Dati solai		
Solaiο n°	Nodi	Tipo
1 102-123-119-101		Vetro strutturale
1 103-121-123-102		Vetro strutturale
1 104-115-121-103		Vetro strutturale
1 105-125-115-104		Vetro strutturale
1 106-127-125-105		Vetro strutturale
1 107-117-127-106		Vetro strutturale
1 115-116-122-121		Vetro strutturale
1 116-215-230-122		Vetro strutturale
1 215-216-231-230		Vetro strutturale
1 216-217-232-231		Vetro strutturale
1 241-242-217-216		Vetro strutturale
1 240-241-216-215		Vetro strutturale
1 126-240-215-116		Vetro strutturale
1 125-126-116-115		Vetro strutturale
1 127-128-126-125		Vetro strutturale
1 117-118-128-127		Vetro strutturale
1 118-220-245-128		Vetro strutturale
1 220-221-246-245		Vetro strutturale
1 221-232-247-246		Vetro strutturale
1 236-237-227-226		Vetro strutturale
1 235-236-226-225		Vetro strutturale
1 124-235-225-120		Vetro strutturale
1 123-124-120-119		Vetro strutturale
1 246-247-242-241		Vetro strutturale
1 121-122-124-123		Vetro strutturale
1 122-230-235-124		Vetro strutturale
1 230-231-236-235		Vetro strutturale
1 231-232-237-236		Vetro strutturale
1 128-245-240-126		Vetro strutturale
1 245-246-241-240		Vetro strutturale
2 237-238-228-227		Vetro strutturale

2 232-233-238-237	Vetro strutturale
2 247-248-243-242	Vetro strutturale
2 217-218-233-232	Vetro strutturale
2 222-223-248-247	Vetro strutturale
2 242-243-218-217	Vetro strutturale
3 223-224-249-248	Vetro strutturale
3 233-234-239-238	Vetro strutturale
3 238-239-229-228	Vetro strutturale
3 218-219-234-233	Vetro strutturale
3 248-249-244-243	Vetro strutturale
3 243-244-219-218	Vetro strutturale
4 219-315-321-234	Vetro strutturale
4 239-323-319-229	Vetro strutturale
4 224-317-327-249	Vetro strutturale
4 249-327-325-244	Vetro strutturale
4 234-321-323-239	Vetro strutturale
4 244-325-315-219	Vetro strutturale
5 321-322-324-323	Vetro strutturale
5 325-326-316-315	Vetro strutturale
5 315-316-322-321	Vetro strutturale
5 323-324-320-319	Vetro strutturale
5 317-318-328-327	Vetro strutturale
5 327-328-326-325	Vetro strutturale
6 322-310-309-324	Vetro strutturale
6 316-311-310-322	Vetro strutturale
6 326-312-311-316	Vetro strutturale
6 324-309-308-320	Vetro strutturale
6 318-314-313-328	Vetro strutturale
6 328-313-312-326	Vetro strutturale

TABULATI DI VERIFICA

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Forze sismiche e masse
- Taglienti di piano
- Spostamenti Relativi dei nodi (SLD)
- Fattori di partecipazione e masse modali
- Massime tensioni sul terreno aste
- Massime reazioni vincolari
- Massime sollecitazioni travi
- Massime sollecitazioni pilastri
- Massime sollecitazioni aste generiche

Risultati Analisi Dinamica - Baricentri masse e masse									
Scenario di calcolo : Set NT SLV A2 STR/GEO									

Combinazione masse 1					
Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	13250	826	878	39
1	No	23545	382	710	1042
2	No	0	0	0	0
3	No	1898	-203	557	1323

Combinazione masse 2					
Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	13250	827	882	39
1	No	23545	394	744	1042

Piano	Rigido	Massa	X	Y	Z
2	No	0	0	0	0
3	No	1898	-202	562	1323

Combinazione masse 3

Piano	Rigido	Massa	X	Y	Z
0	No	kg	cm	cm	cm
1	No	13250	826	886	39
2	No	23545	382	778	1042
3	No	0	0	0	0
3	No	1898	-203	567	1323

Combinazione masse 4

Piano	Rigido	Massa	X	Y	Z
0	No	kg	cm	cm	cm
1	No	13250	825	882	39
2	No	23545	369	744	1042
3	No	0	0	0	0
3	No	1898	-205	562	1323

Taglianti di piano

Scenario di calcolo: **Set_NT_SLV_A2_STR/GEO**

I taglianti sono dati per combinazioni di calcolo C-S-Pm con C=Combinazione(1,2,...) S=Sisma(1,II) Pm=posizione masse(1,2,...) Azioni complessive, riferite al sistema WCS,con origine in (0,0,0),i momenti sono comprensivi dei momenti di trasporto

con:

Fz=forza verticale,

dr=spost medio del piano rispetto al piano inferiore,

Fh=tagliante,

H=altezza del piano

$$\Theta = Fz * dr / (Fh * H)$$

Combinazione 12-1-1 (SISMAX SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
0	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	mm
1	-9552	-100	16501	7789	-13701	-1462	8278	8801	4065	--
2	16483	-463	-21388	4792	1691	-3014	3155	7204	10223	0.000246
3	9305	179	-7418	4511	-5509	-1206	-1993	5620	13230	0.003721

Piano	FxPIU/Isol.	FyPIU/Isol.	FzPIU/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
0	kg	kg	kg	kg	kg	kg	kg	kg	kg
1	-8694	-2757	0	0	0	0	0	-9552	-100
2	8694	2757	0	0	0	0	0	16483	-463
3	8756	1849	0	0	0	0	0	9305	179

Percentuali assorbite in direzione X

Piano	%aPIU/Isol.FX	%Par.FX	%Shell.FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%aPIU/Isol.FY	%Par.FY	%Shell.FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 12-1-2 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
0	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	mm
1	-9715	-185	16703	-14102	8059	-1519	8278	8801	4065	--
2	16525	-425	-22376	4078	-2664	-4255	3155	7204	10223	0.000213
3	9155	216	-7431	4240	-5317	-2074	-1993	5620	13230	0.003764

Piano	FxPIU/Isol.	FyPIU/Isol.	FzPIU/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
0	kg	kg	kg	kg	kg	kg	kg	kg	kg
1	-8870	-2788	0	0	0	0	0	-9715	-185
2	8870	2788	0	0	0	0	0	16525	-425
3	8629	1823	0	0	0	0	0	9155	216

Percentuali assorbite in direzione X

Piano	%aPIU/Isol.FX	%Par.FX	%Shell.FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%aPIU/Isol.FY	%Par.FY	%Shell.FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 12-1-3 (SISMAX SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
0	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	mm
1	-9694	-151	16771	-15195	7749	-1166	8278	8801	4065	--
2	18650	2343	-22119	-4833	6184	-13763	3155	7204	10223	0.000181
3	9115	284	-7298	4852	-5105	-3187	-1993	5620	13230	0.003704

Piano	FxPIU/Isol.	FyPIU/Isol.	FzPIU/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
0	kg	kg	kg	kg	kg	kg	kg	kg	kg
1	-8843	-2754	0	0	0	0	0	-9694	-151
2	8843	2754	0	0	0	0	0	18650	2343
3	8615	1827	0	0	0	0	0	9115	284

Percentuali assorbite in direzione X

Piano	%aPIU/Isol.FX	%Par.FX	%Shell.FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%aPIU/Isol.FY	%Par.FY	%Shell.FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 12-1-4 (SISMAX SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
0	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	mm
1	-9524	-111	16601	-14458	7170	-1325	8278	8801	4065	--
2	17154	473	-22149	745	1378	-5666	3155	7204	10223	0.000244
3	9285	280	-7674	4620	-5535	-2361	-1993	5620	13230	0.003854

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-8666	-2748	0	0	0	0	-9524	-1111
1	8666	2748	0	0	0	0	17154	473
2	0	0	0	0	0	0	0	0
3	8766	1868	0	0	0	0	9285	280

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 13-I-1 (SISMAY SLV)

Piano	Fx	Fy	Fz	Mx	Mv	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	mm
0	-3195	-9598	17227	24741	16859	6010	8278	8801	4065	--
1	-1926	16413	-22430	5024	13357	3155	7204	10223	0.001683	--
2	0	0	0	0	0	0	0	0	0	0.000000
3	-4408	7619	-7610	-14426	4182	20048	-1993	5620	13230	0.002615

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-5761	-1220	0	0	0	0	-3195	-9598
1	5761	1220	0	0	0	0	-1926	16413
2	0	0	0	0	0	0	0	0
3	-2710	2236	0	0	0	0	-4408	7619

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 13-I-2 (SISMAY SLV)

Piano	Fx	Fy	Fz	Mx	Mv	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	mm
0	-3293	-9501	17312	23916	16678	5879	8278	8801	4065	--
1	-1781	16375	-22530	-18106	4374	12363	3155	7204	10223	0.001711
2	0	0	0	0	0	0	0	0	0	0.000000
3	-4434	7643	-7643	-14436	4193	19900	-1993	5620	13230	0.002622

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-5815	-1263	0	0	0	0	-3293	-9501
1	5815	1263	0	0	0	0	-1781	16375
2	0	0	0	0	0	0	0	0

225

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
3	-2728	2237	0	0	0	0	-4434	7643

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 13-I-3 (SISMAY SLV)

Piano	Fx	Fy	Fz	Mx	Mv	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	mm
0	-3318	-9518	17377	23626	17104	5937	8278	8801	4065	--
1	-1683	16370	-22603	-17947	4763	12405	3155	7204	10223	0.001717
2	0	0	0	0	0	0	0	0	0	0.000000
3	-4450	7677	-7631	-14548	4138	19765	-1993	5620	13230	0.002679

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-5843	-1268	0	0	0	0	-3318	-9518
1	5843	1268	0	0	0	0	-1683	16370
2	0	0	0	0	0	0	0	0
3	-2737	2245	0	0	0	0	-4450	7677

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 13-I-4 (SISMAY SLV)

Piano	Fx	Fy	Fz	Mx	Mv	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	mm
0	-3221	-9617	17289	24663	16846	6071	8278	8801	4065	--
1	-1814	16516	-22494	-18472	5443	12924	3155	7204	10223	0.001677
2	0	0	0	0	0	0	0	0	0	0.000000
3	-4410	7660	-7647	-14520	4103	19924	-1993	5620	13230	0.002626

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-5790	-1225	0	0	0	0	-3221	-9617
1	5790	1225	0	0	0	0	-1814	16516
2	0	0	0	0	0	0	0	0
3	-2703	2249	0	0	0	0	-4410	7660

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00

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Piano	%PI/I/Isol. FX	%Par. FX	%Shell. FX
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%PI/I/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Verifica Degli Spostamenti Relativi

Scenario di calcolo : **Set NT_SIV_A2_STR/GEO**
Attenzione calcolo agli SLU: Gli spostamenti dovuti al sisma sono stati calcolati in via approssimata moltiplicando gli spostamenti derivanti dagli spettri al limite ultimo per il coefficiente e=Sd(T0)/Su(T0),dove T0 è il periodo fondamentale nella direzione considerata, Sd(T0) e Su(T0) il valore dello spettro in T0 rispettivamente di danno e ultimo

Combinazione	Spettro
SISMAX_SIV	SpettroNT(q=1)
SISMAX_SIV	SpettroNT(q=1)
	e=0.417
	e=0.417

Interp.	Comb.	nXh mm	nXh mm	nYh mm	nYv mm	ηYh mm	Nodo1	Nodo2	η mm	ηAmm mm	Cs
0-1	(12+13)+V-4	5.57	9.77	1.49	3.51	1.01	101	15.34	27.10	1.77	
0-1	(12+13)+V-4	6.16	9.73	1.74	3.61	2	102	15.89	27.10	1.71	
0-1	(12+13)+V-4	6.42	9.65	1.84	3.60	3	103	16.06	27.10	1.69	
0-1	(12+13)+V-4	6.54	9.71	1.89	3.38	4	104	16.25	27.10	1.67	
0-1	(12+13)+V-4	6.57	9.78	1.91	3.39	5	105	16.34	27.10	1.66	
0-1	(12+13)+V-4	6.26	10.09	1.85	3.49	6	106	16.36	27.10	1.66	
0-1	(12+13)+V-4	5.74	10.12	1.74	3.53	7	107	15.87	27.10	1.71	
2-3	(12+13)+V-4	0.79	7.83	0.26	3.66	208	308	8.62	18.60	2.16	
2-3	(12+13)+V-4	0.97	7.90	0.31	3.55	209	309	8.87	18.60	2.10	
2-3	(12+13)+V-4	1.02	7.99	0.31	3.50	210	310	9.01	18.60	2.06	
2-3	(12+13)+V-4	1.09	8.06	0.31	3.45	211	311	9.15	18.60	2.03	
2-3	(12+13)+V-4	1.13	8.24	0.29	3.55	212	312	9.36	18.60	1.99	
2-3	(12+13)+V-3	1.15	8.51	0.28	0.94	213	313	9.66	18.60	1.92	
2-3	(12+13)+V-3	1.02	8.89	0.23	1.01	214	314	9.91	18.60	1.88	
Minimo											
0-1	(12+13)+V-4	6.26	10.09	1.85	3.49	6	106	16.36	27.10	1.66	

Periodi di vibrazione e Masse modali

Scenario di calcolo : **Set NT_SIV_A2_STR/GEO**

Posizione masse 1

Numero di Frequenze calcolate =45, filtrate=18											
N	T(s)	Coeff. Partecipazione				Masse Modali				Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3649	48.736	13.894	73293	1893	86.18	7.00	86.61	6.54		
2(2)	0.3171	13.290	-46.645	21337	641	6.41	78.94	5.54	79.27		
3(3)	0.2250	-1.924	8.001	36	628	0.13	2.32	0.97	1.61		
4(7)	0.1498	-4.056	12.629	161	1564	0.60	5.79	0.00	0.15		
5(8)	0.1401	0.394	-2.030	2	40	0.01	0.15	0.08	0.21		
6(9)	0.1208	-2.411	7.888	57	610	0.21	2.26	0.00	0.13		
7(10)	0.1141	-1.852	-0.766	34	6	0.12	0.02	0.02	0.25		
8(11)	0.1118	3.949	2.051	153	41	0.57	0.15	0.02	0.29		
9(12)	0.1004	-4.625	-1.457	210	21	0.78	0.08	0.24	0.00		
10(13)	0.0933	9.833	1.755	948	30	3.51	0.11	0.21	0.04		
11(14)	0.0885	1.209	5.085	14	254	0.05	0.94				
12(15)	0.0852	-1.943	1.619	37	26	0.14	0.10				
13(17)	0.0673	-0.804	2.937	6	85	0.02	0.31				

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N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
14(27)	0.0435	-1.205	4.080	14	163	0.05	0.60
15(28)	0.0419	0.666	-2.084	4	43	0.02	0.16
16(34)	0.0319	2.333	-0.056	53	0	0.20	0.00
17(35)	0.0314	-1.680	-0.601	28	4	0.10	0.01
18(36)	0.0312	-2.770	-1.174	75	14	0.28	0.05
Somma delle Masse Modali [kgm*g]							
				26859	26757		
Masse strutturali libere [kgm*g]							
				27028	27028		
Percentuale							
				99.37	99.00	99.37	99.00

Posizione masse 2

Numero di Frequenze calcolate =45, filtrate=19

N	T(s)	Coeff. Partecipazione				Masse Modali				Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3616	48.872	13.740	23423	1851	86.66	6.85	86.66	6.85		
2(2)	0.3141	12.874	-46.575	1625	21273	6.01	78.71	6.01	78.71		
3(3)	0.2218	-3.273	7.306	105	523	0.39	1.94	0.39	1.94		
4(6)	0.1529	3.867	-13.183	147	1704	0.54	6.31	0.54	6.31		
5(7)	0.1521	-0.674	2.645	4	69	0.02	0.25	0.02	0.25		
6(9)	0.1204	-2.322	8.756	53	752	0.20	2.78	0.20	2.78		
7(10)	0.1101	-3.227	-0.065	102	0	0.38	0.00	0.38	0.00		
8(11)	0.1090	2.679	0.591	70	2679	0.01	3	0.26	70	0.01	0.01
9(12)	0.0994	-4.436	-0.979	193	9	0.71	0.03	0.71	0.03		
10(13)	0.0904	9.864	2.703	954	72	3.53	0.27				
11(14)	0.0872	-0.511	4.364	3	187	0.01	0.69				
12(15)	0.0850	0.344	-2.130	1	45	0.00	0.16				
13(17)	0.0680	1.080	-2.660	11	69	0.04	0.26				
14(22)	0.0517	-0.599	1.907	4	36	0.01	0.13				
15(25)	0.0463	0.739	-2.709	5	72	0.02	0.27				
16(26)	0.0456	-0.726	2.428	5	58	0.02	0.21				
17(27)	0.0441	-0.656	1.844	4	33	0.02	0.12				
18(34)	0.0328	-2.143	0.575	3	0.17	0.01	0.01				
19(37)	0.0309	3.085	0.999	93	10	0.35	0.04				
Somma delle Masse Modali [kgm*g]											
				26849	26769						
Masse strutturali libere [kgm*g]											
				27028	27028						
Percentuale											
				99.34	99.04	99.34	99.04				

Posizione masse 3

Numero di Frequenze calcolate =45, filtrate=18

N	T(s)	Coeff. Partecipazione				Masse Modali				Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3628	48.857	13.428	23409	1768	86.61	6.54	86.61	6.54		
2(2)	0.3145	12.362	-46.740	1499	21424	5.54	79.27	5.54	79.27		
3(3)	0.2219	-5.170	6.655	262	434	0.97	1.61	0.97	1.61		
4(4)	0.1889	0.034	-2.061	0	42	0.00	0.15	0.00	0.15		
5(6)	0.1543	2.212	-8.091	48	642	0.18	2.38	0.18	2.38		
6(7)	0.1515	-2.726	10.901	73	1165	0.27	4.31	0.27	4.31		
7(9)	0.1208	-1.894	8.325	35	680	0.13	2.51	0.13	2.51		
8(10)	0.1113	-4.313	0.942	182	9	0.67	0.03	0.67	0.03		
9(12)	0.0995	-4.325	-0.228	183	1	0.68	0.00	0.68	0.00		
10(13)	0.0921	9.124	3.387	816	112	3.02	0.42	3.02	0.42		
11(14)	0.0869	-2.065	3.849	42	145	0.15	0.54	0.15	0.54		
12(15)	0.0842	3.162	2.650	98	69	0.36	0.25	0.36	0.25		
13(17)	0.0683	-1.442	2.386	20	56	0.08	0.21	0.08	0.21		
14(23)	0.0516	-0.264	1.862	1	34	0.00	0.13	0.00	0.13		
15(25)	0.0461	-0.684	2.602	5	66	0.02	0.25	0.02	0.25		
16(26)	0.0453	2.810	-0.864	7	77	0.03	0.29	0.03	0.29		
17(35)	0.0321	-2.561	-0.218	64	0	0.24	0.00	0.24	0.00		
18(37)	0.0310	2.418	0.983	57	9	0.21	0.04	0.21	0.04		
Somma delle Masse Modali [kgm*g]											
				26802	26734						
Masse strutturali libere [kgm*g]											
				99.16	27028						
Percentuale											
				98.91	98.91	99.16	98.91			98.91	

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Posizione masse 4

Numero di Frequenze calcolate =45, filtrate=17

N	T(s)	Coeff. Partecipazione		Masse Modali kgm* ^g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3655	48.780	18.610	23335	1816	86.34	6.72
2(2)	0.3175	12.772	-46.813	1600	21491	5.92	79.52
3(3)	0.2254	-3.765	7.385	139	535	0.51	1.98
4(7)	0.1498	-3.621	12.845	129	1618	0.48	5.99
5(8)	0.1389	0.236	-1.793	1	32	0.00	0.12
6(9)	0.1209	-1.748	7.811	30	598	0.11	2.21
7(10)	0.1143	-2.602	-0.537	66	3	0.25	0.01
8(11)	0.1127	4.312	-0.305	182	0.00	0.67	0.00
9(12)	0.1007	-4.790	-0.923	225	8	0.83	0.03
10(13)	0.0930	9.764	3.207	935	101	3.46	0.37
11(14)	0.0894	-1.634	3.968	26	154	0.10	0.57
12(15)	0.0855	2.438	3.087	2	93	0.01	0.35
13(17)	0.0671	1.166	-2.781	13	76	0.05	0.28
14(23)	0.0516	-0.390	1.864	1	34	0.01	0.13
15(27)	0.0432	-1.180	3.972	14	155	0.05	0.57
16(28)	0.0419	-0.663	2.263	4	55	0.02	0.20
17(35)	0.0313	-3.473	-1.306	118	17	0.44	0.06
Somma delle Masse Modali [kgm* ^g]							
Masse strutturali libere [kgm* ^g]				26820		26787	
Percentuale				99.23		99.11	
				99.23		99.23	

Risultati Analisi Dinamica - Massime tensioni sul terreno aste

Scenario di calcolo: Set NT SLV A2 STR/GEO									
Asta	N in.	N fin.	0/5	1/5	2/5	3/5	4/5	5/5	
			kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
9003	1	2	2.45(12-1-3)	2.34(12-1-3)	2.24(12-1-3)	2.15(12-1-3)	2.06(12-1-3)	1.97(12-1-3)	
9003	2	3	1.98(12-1-3)	1.93(12-1-3)	1.89(12-1-3)	1.85(12-1-3)	1.81(12-1-3)	1.78(12-1-3)	
9003	3	4	1.78(12-1-3)	1.77(12-1-3)	1.75(12-1-3)	1.74(12-1-3)	1.73(12-1-3)	1.71(12-1-3)	
9003	4	5	1.71(12-1-2)	1.72(12-1-2)	1.73(12-1-2)	1.73(12-1-2)	1.74(12-1-2)	1.75(12-1-2)	
9003	5	6	1.75(12-1-2)	1.78(12-1-2)	1.81(12-1-2)	1.84(12-1-2)	1.88(12-1-2)	1.92(12-1-2)	
9003	6	7	1.92(12-1-2)	1.95(12-1-2)	1.98(12-1-2)	2.01(12-1-2)	2.06(12-1-2)	2.11(12-1-2)	
9004	209	210	1.79(12-1-1)	1.81(12-1-1)	1.84(12-1-1)	1.87(12-1-1)	1.91(12-1-1)	1.95(12-1-1)	
9004	210	211	1.96(12-1-1)	1.95(12-1-1)	1.95(12-1-1)	1.96(12-1-1)	1.97(12-1-1)	2.00(12-1-1)	
9004	211	212	2.00(12-1-1)	1.96(12-1-1)	1.94(12-1-1)	1.92(12-1-1)	1.91(12-1-1)	1.91(12-1-1)	
9004	212	213	1.91(12-1-1)	1.88(12-1-1)	1.86(12-1-1)	1.84(12-1-1)	1.83(12-1-1)	1.83(12-1-1)	
9004	213	214	1.83(12-1-1)	1.81(12-1-1)	1.80(12-1-1)	1.79(12-1-1)	1.79(12-1-1)	1.79(12-1-1)	
9004	208	209	-1.75(12-1-1)	-1.68(12-1-1)	1.62(12-1-1)	1.67(12-1-1)	1.72(12-1-1)	1.78(12-1-1)	

Risultati Analisi Dinamica - Reazioni massime - Nodi

Nodo	Scenario di calcolo: Set NT SLV_A2 STR/CEO										Mz
	Rx	Ry	Rz	kg	kg ^m	Mix	My	kg ^m			
1	-1596(13-II-1)	-1347(13-I-4)	0	0	0	0	0	0	2(13-I-1)		
2	-1661(7)	-1600(13-I-4)	0	0	0	0	0	0	0		
3	-1634(7)	-675(13-I-4)	0	0	0	0	0	0	0		
4	-1662(7)	-1157(13-I-4)	0	0	0	0	0	0	0		
5	-1711(7)	-1242(13-I-4)	0	0	0	0	0	0	1(13-II-1)		
6	-1693(7)	-1818(13-I-4)	0	0	0	0	0	0	0		
7	-1454(7)	-1934(13-I-4)	0	0	0	0	0	0	-1(13-II-3)		
208	2260(12-II-1)	2451(13-II-3)	0	0	0	0	0	0	-2(13-II-3)		
209	2344(12-II-1)	2294(13-II-3)	0	0	0	0	0	0	0		
210	2463(12-II-1)	801(12-II-4)	0	0	0	0	0	0	0		
211	2577(12-II-1)	709(12-II-4)	0	0	0	0	0	0	0		
212	2682(12-II-3)	621(12-II-3)	0	0	0	0	0	0	0		
213	2662(12-II-4)	1735(13-II-3)	0	0	0	0	0	0	0		
214	2782(12-II-3)	1646(13-II-3)	0	0	0	0	0	0	0		

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Travi

Scenario di calcolo : Set NT SILV A2 STRGEO											
Asta	N.in.	N	Ty			Tz	kg	Mt	My	Mz	
			kg	kg	kg						
101	115	-221(9)	-144(9)	-109(2)	0	0	-29(13-11-4)	0	0	-30(13-1-4)	
	125	-221(9)	94(13-1-4)	107(3)	0	0	-183(2)	0	0	-45(3)	
101	119	-74(13-11-3)	149(3)	166(2)	0	0	-138(3)	0	0	-25(13-1-4)	
	123	-74(13-1-3)	149(3)	166(2)	0	0	-138(3)	0	0	-34(13-11-1)	
101	121	-229(9)	102(13-1-1)	108(2)	0	0	-103(3)	0	0	-33(13-1-1)	
	115	-229(9)	102(13-1-1)	108(2)	0	0	-103(3)	0	0	-33(13-1-1)	
101	123	-188(9)	-142(3)	105(2)	0	0	29(8)	0	0	-40(2)	
	121	-188(9)	90(13-1-1)	170(3)	0	0	-170(3)	0	0	-30(13-1-2)	
101	125	-178(13-11-3)	-180(2)	160(3)	0	0	-170(3)	0	0	-45(3)	
	127	-178(13-1-3)	160(3)	170(2)	0	0	-170(2)	0	0	-27(13-1-4)	
101	127	-101(13-1-1)	153(2)	112(3)	0	0	-113(2)	0	0	-32(8)	
	117	-101(13-1-1)	153(2)	112(3)	0	0	-113(2)	0	0	-34(8)	
102	116	248(13-11-1)	-155(9)	110(3)	0	0	161(2)	0	0	-45(3)	
	126	248(13-1-1)	89(13-1-1)	110(3)	0	0	161(2)	0	0	-26(13-1-2)	
102	120	418(13-11-1)	-180(3)	161(3)	0	0	161(3)	0	0	-30(13-11-2)	
	124	418(13-1-1)	142(2)	161(3)	0	0	-110(2)	0	0	32(8)	
102	122	187(12-11-4)	-147(8)	112(3)	0	0	164(2)	0	0	-42(2)	
	122	187(12-11-4)	92(13-1-2)	112(3)	0	0	164(3)	0	0	-30(12-11-3)	
102	116	528(13-11-1)	-150(3)	106(3)	0	0	-165(2)	0	0	-48(2)	
	124	528(13-11-1)	-150(3)	106(3)	0	0	164(3)	0	0	-26(13-1-2)	
103	215	90(12-1-4)	-141(2)	111(3)	0	0	-113(2)	0	0	-25(2)	
	240	90(12-1-4)	84(3)	111(3)	0	0	-113(2)	0	0	-28(3)	
103	225	800(13-1-3)	-167(3)	152(2)	0	0	109(2)	0	0	25(8)	
	235	800(13-1-3)	137(2)	152(3)	0	0	-156(3)	0	0	-41(3)	
103	230	92(12-1-4)	-136(3)	112(3)	0	0	152(3)	0	0	-23(1)	
	230	92(12-1-4)	86(2)	112(3)	0	0	-110(2)	0	0	-25(13-1-2)	
103	235	75(12-1-4)	-139(3)	107(3)	0	0	112(3)	0	0	-25(13-1-2)	
	235	75(12-1-4)	107(3)	112(3)	0	0	-107(3)	0	0	-28(3)	
103	230	75(12-1-4)	79(2)	109(2)	0	0	156(3)	0	0	25(8)	
	240	71(12-1-1)	-166(2)	156(3)	0	0	-156(3)	0	0	-37(2)	
103	245	71(12-1-1)	146(3)	155(2)	0	0	155(2)	0	0	-30(12-11-3)	
	245	108(13-1-1)	-170(2)	156(2)	0	0	-156(2)	0	0	-40(2)	
103	220	108(13-1-1)	142(3)	156(2)	0	0	156(2)	0	0	-23(1)	
	220	108(13-1-1)	142(3)	156(2)	0	0	-156(2)	0	0	-19(13-11-2)	
104	216	-213(12-11-4)	110(3)	110(2)	0	0	-112(3)	0	0	-19(13-1-2)	
	241	-213(12-11-4)	110(3)	110(2)	0	0	110(2)	0	0	-19(13-1-2)	
104	226	-322(13-11-3)	-144(3)	142(3)	0	0	-142(3)	0	0	-28(3)	
	236	-322(13-1-3)	141(2)	142(3)	0	0	142(3)	0	0	-28(3)	
104	231	207(12-1-1)	-108(3)	109(3)	0	0	-109(3)	0	0	-26(2)	
	216	207(12-1-1)	111(2)	110(3)	0	0	111(2)	0	0	-22(13-11-2)	
104	236	440(13-1-3)	-110(3)	106(3)	0	0	-106(3)	0	0	-23(13-1-2)	
	231	440(13-1-3)	106(2)	108(2)	0	0	108(2)	0	0	-19(13-11-2)	
104	241	-337(13-1-1)	-141(2)	146(2)	0	0	-146(2)	0	0	-26(12-1-3)	
	246	-337(13-1-1)	151(3)	146(2)	0	0	151(3)	0	0	-31(3)	
104	246	-336(13-1-1)	-143(2)	146(2)	0	0	-146(2)	0	0	-25(2)	
	221	-336(13-1-1)	149(3)	146(3)	0	0	146(3)	0	0	-29(3)	
105	217	-147(12-11-1)	-87(2)	129(3)	0	0	-109(2)	0	0	21(8)	
	232	-147(12-11-1)	129(3)	107(3)	0	0	107(3)	0	0	-25(3)	
105	242	-147(12-11-1)	119(3)	131(2)	0	0	-131(2)	0	0	-21(1)	
	227	-91(13-11-3)	144(2)	132(3)	0	0	132(3)	0	0	-33(2)	
105	237	-91(13-11-3)	-84(3)	106(3)	0	0	-106(3)	0	0	22(9)	
	232	-147(12-11-1)	129(2)	108(2)	0	0	108(2)	0	0	-25(2)	
105	217	-147(12-11-1)	129(2)	103(2)	0	0	-103(2)	0	0	-22(13-1-1)	
	237	-117(12-11-1)	-86(3)	106(3)	0	0	106(3)	0	0	-22(2)	
105	232	-117(12-11-1)	124(2)	135(2)	0	0	-135(2)	0	0	-24(12-1-3)	
	242	-119(12-11-1)	-116(2)	134(3)	0	0	134(3)	0	0	-39(3)	
105	247	-119(12-11-1)	154(3)	135(2)	0	0	-135(2)	0	0	-19(1)	
	247	-116(13-1-2)	-117(2)	135(2)	0	0	135(2)	0	0	-37(3)	
106	222	-116(13-1-2)	152(3)	105(3)	0	0	-105(3)	0	0	29(9)	
	218	-329(13-1-2)	-76(2)	103(3)	0	0	103(3)	0	0	-30(8)	
106	243	-329(13-1-2)	132(3)	103(3)	0	0	-103(3)	0	0	-30(8)	
	243	-329(13-1-2)	132(3)	103(3)	0	0	-103(3)	0	0	-30(8)	

106	228	-232(3-II-3)	-102(3)	0	0	-24(13-I-4)
238	-232(13-II-3)	139(2)	120(2)	0	0	-34(2)
233	-470(13-I-1)	-74(3)	-102(2)	0	0	28(9)
218	-470(13-I-1)	131(2)	103(3)	0	0	-30(9)
238	-373(12-II-1)	-79(3)	-100(2)	0	0	-30(13-I-4)
233	-373(12-II-1)	124(9)	102(2)	0	0	-28(9)
243	-352(12-II-4)	-98(2)	-123(3)	0	0	-35(13-I-4)
248	-352(12-II-4)	149(3)	123(2)	0	0	-40(3)
248	-256(2)	-102(2)	-123(2)	0	0	-23(13-I-4)
223	-256(2)	145(3)	123(3)	0	0	-37(3)
219	-129(13-II-3)	-69(3)	-101(2)	0	0	33(9)
244	-129(13-II-3)	132(2)	99(3)	0	0	-35(8)
229	-52(2)	-89(2)	-110(2)	0	0	-26(13-I-4)
229	-52(2)	132(3)	111(3)	0	0	-34(3)
234	-94(2)	-79(13-I-4)	-98(3)	0	0	-32(13-I-4)
219	-78(2)	128(2)	100(2)	0	0	-33(8)
239	-78(2)	-86(13-I-4)	-97(3)	0	0	-30(13-I-4)
234	-78(2)	121(9)	98(2)	0	0	-30(13-II-4)
244	-112(13-II-4)	-89(13-I-4)	-113(2)	0	0	-41(13-I-4)
249	-112(13-II-4)	145(3)	113(3)	0	0	-47(13-II-4)
249	-47(2)	-87(3)	-114(2)	0	0	25(9)
224	-47(2)	140(2)	113(3)	0	0	-39(9)
315	-784(13-II-3)	-77(13-I-4)	-100(2)	0	0	34(9)
325	-784(13-II-3)	130(2)	98(3)	0	0	-37(9)
319	-120(13-I-4)	-78(13-I-4)	-104(2)	0	0	-34(13-I-4)
323	-120(13-I-4)	130(3)	104(3)	0	0	-37(8)
321	-396(13-I-4)	-109(13-I-4)	-97(3)	0	0	-54(13-I-4)
315	-396(13-I-4)	127(2)	98(2)	0	0	-55(13-I-4)
323	-1412(13-I-4)	-110(13-I-4)	-95(3)	0	0	-55(13-I-4)
321	-1412(13-I-4)	120(9)	97(2)	0	0	-51(13-I-4)
325	-118(13-II-4)	-110(13-I-4)	-107(2)	0	0	-58(13-I-4)
327	-118(13-II-4)	138(3)	107(3)	0	0	-62(13-II-4)
327	-1016(13-II-4)	-82(2)	-107(3)	0	0	-33(13-I-4)
317	-1016(13-II-4)	132(3)	107(2)	0	0	-39(8)
316	-142(12-I-1)	-89(3)	-104(2)	0	0	-21(13-I-2)
326	-142(12-I-1)	118(2)	102(3)	0	0	-26(2)
320	-79(12-I-1)	-90(2)	-104(2)	0	0	-20(13-II-2)
324	-79(12-I-1)	120(3)	104(2)	0	0	-28(3)
322	-141(12-I-1)	-88(2)	-101(3)	0	0	-20(13-I-4)
316	-141(12-I-1)	115(3)	102(2)	0	0	-24(3)
324	-118(12-I-1)	-91(2)	-100(2)	0	0	-21(13-I-2)
322	-118(12-I-1)	111(3)	101(3)	0	0	-22(3)
326	-118(12-I-1)	-92(3)	-106(2)	0	0	-25(13-I-1)
328	-118(12-I-1)	122(2)	106(3)	0	0	-29(2)
328	-74(12-I-3)	-99(3)	-106(3)	0	0	-24(13-I-2)
318	-74(12-I-3)	116(2)	106(2)	0	0	-24(2)
101	971(13-I-3)	-31(9)	-127(2)	0	0	-8(13-II-4)
102	971(13-I-3)	31(9)	118(2)	0	0	39(9)
102	1407(13-I-3)	-58(13-II-1)	-75(2)	0	0	-26(13-I-1)
103	1407(13-I-3)	58(13-II-1)	70(2)	0	0	41(8)
103	459(12-II-2)	-68(13-II-1)	-76(3)	0	0	-30(13-I-1)
104	459(12-II-2)	-68(13-II-1)	74(2)	0	0	41(8)
104	643(13-II-1)	-77(8)	-76(2)	0	0	-32(13-II-4)
105	643(13-II-1)	-77(8)	76(2)	0	0	51(8)
105	1069(13-II-1)	-19(9)	-124(2)	0	0	61(2-II-3)
106	1069(13-II-1)	-19(9)	127(2)	0	0	31(9)
106	968(13-II-1)	-20(8)	-124(2)	0	0	10(13-I-4)
107	968(13-II-1)	-20(8)	127(2)	0	0	31(8)
308	1633(13-I-4)	18(13-I-4)	-76(2)	0	0	25(8)
309	1633(13-I-4)	18(13-I-4)	81(2)	0	0	-13(13-I-4)
309	2443(13-I-4)	8(8)	-76(2)	0	0	22(8)
310	2443(13-I-4)	8(8)	81(2)	0	0	11(9)
310	1228(12-II-1)	7(9)	-78(2)	0	0	22(9)
311	1228(12-II-1)	7(9)	81(2)	0	0	11(8)
311	1206(13-II-4)	-12(13-II-4)	-81(2)	0	0	22(9)
312	1206(13-II-4)	-12(13-II-4)	79(2)	0	0	11(8)
312	2432(13-II-4)	7(9)	-82(2)	0	0	22(9)

301	313	2432(13-I-4)	7(9)	80(2)	0	0	11(8)
313	1735(13-I-4)	-18(13-II-4)	-82(2)	0	0	0	21(9)
314	1735(13-I-4)	-18(13-II-4)	80(2)	0	0	0	13(13-II-4)
8000	101	-3032(3)	-89(8)	-1552(2)	17(8)	3818(2)	27(13-II-4)
8000	119	-2733(3)	-89(8)	-1332(2)	17(8)	2618(12-I-1)	154(8)
8000	119	-2511(3)	-144(9)	-1234(2)	20(9)	2617(12-I-1)	193(8)
8000	120	-2222(3)	-144(9)	-1097(13-II-1)	20(9)	-2025(12-II-1)	430(8)
8000	120	-3024(13-I-4)	183(13-II-3)	-920(13-II-3)	11(13-I-3)	-2026(12-II-1)	471(8)
225	-2871(13-I-3)	-795(3-II-3)	11(13-I-3)	-2670(8)	261(8)	2670(8)	261(8)
8000	225	-2802(13-I-4)	139(13-I-4)	-766(12-I-1)	-68(8)	-2671(8)	294(8)
8000	226	-2667(13-I-4)	139(13-I-4)	-641(12-I-1)	-68(8)	-3429(9)	88(9)
8000	226	-2821(13-I-3)	152(13-II-3)	-711(12-I-1)	-12(8)	-3428(9)	101(9)
227	-2704(13-I-3)	152(13-II-3)	663(12-II-1)	-12(8)	-3846(9)	-173(13-II-2)	173(13-II-2)
8000	227	-2583(13-I-3)	182(13-I-3)	719(12-II-1)	-16(13-I-3)	-3846(9)	-155(13-II-2)
8000	228	-2490(13-I-3)	182(13-I-3)	845(12-II-1)	-16(13-I-3)	-3878(9)	-93(13-I-3)
8000	228	-829(12-II-1)	1294(13-II-4)	-11(9)	-3878(9)	-72(13-I-3)	-3878(9)
8000	229	-707(12-II-1)	1420(13-II-4)	-11(9)	-351(39)	-45(13-I-4)	-45(13-I-4)
8000	229	-1007(12-II-1)	108(13-I-3)	1555(13-II-3)	-9(13-I-3)	-351(39)	-351(39)
319	-967(12-II-1)	1680(13-II-3)	-9(13-I-3)	-2804(9)	-162(13-I-4)	-2804(9)	-162(13-I-4)
8000	319	-1531(13-I-4)	122(13-II-3)	-11(9)	-2803(9)	-133(13-I-4)	-133(13-I-4)
320	-1526(13-I-4)	1412(13-II-3)	-11(9)	3428(12-II-1)	-62(12-I-1)	-62(12-I-1)	-62(12-I-1)
8000	320	-1963(13-I-4)	-44(12-I-4)	1353(2)	-11(13-I-4)	3429(12-II-1)	-51(12-I-1)
308	-1999(13-I-4)	-44(12-I-4)	1573(2)	-11(13-I-4)	4384(13-II-2)	22(8)	22(8)
8001	102	-4681(3)	106(13-II-1)	-1985(2)	18(8)	4674(2)	66(13-II-1)
123	-4261(3)	106(13-II-1)	-1675(2)	18(8)	2711(12-I-1)	146(8)	146(8)
8001	123	-3914(3)	-158(9)	-1513(2)	20(9)	2710(12-I-1)	176(8)
124	-3502(3)	-158(9)	-197(2)	20(9)	-2569(12-II-1)	437(8)	437(8)
8001	124	-362(3)	-206(13-I-3)	-1102(2)	9(9)	-2569(12-II-1)	476(8)
235	-3234(3)	-206(13-I-3)	-789(9)	9(9)	-3020(8)	261(8)	261(8)
8001	235	-2907(3)	-123(13-II-4)	-863(12-I-1)	-68(8)	-3020(8)	290(8)
236	-2557(3)	-123(13-II-4)	-690(12-I-1)	-68(8)	-3872(9)	99(9)	99(9)
8001	236	-2469(3)	118(13-II-2)	-861(12-I-1)	-13(8)	-3871(9)	85(9)
237	-2160(3)	118(13-II-2)	939(12-II-1)	-13(8)	-4173(9)	145(13-I-2)	145(13-I-2)
8001	237	-2116(12-II-1)	-184(13-II-3)	982(12-II-1)	-16(9)	-4173(9)	-142(13-II-2)
238	-1985(12-II-1)	-184(13-II-3)	1159(12-II-1)	-16(9)	-3990(9)	107(13-II-4)	107(13-II-4)
8001	238	-2155(12-II-1)	-88(8)	1007(12-II-1)	-10(9)	-3991(9)	83(13-II-4)
239	-2059(12-II-1)	-88(8)	1186(12-II-1)	-10(9)	-3343(9)	125(9)	125(9)
8001	239	-2384(13-I-3)	923(12-II-1)	-11(13-I-3)	-3343(9)	67(9)	67(9)
323	-2327(12-II-1)	-190(13-II-3)	1244(3)	-11(13-I-3)	3207(12-II-1)	-249(13-I-4)	-249(13-I-4)
8001	323	-1516(12-II-1)	-186(13-I-3)	1478(13-II-4)	-9(9)	3209(12-II-1)	-196(13-I-4)
324	-1508(12-II-1)	-186(13-I-3)	1661(13-II-4)	-9(9)	3655(12-II-1)	89(8)	89(8)
8001	324	-1766(12-II-1)	45(8)	10(13-I-4)	3655(12-II-1)	66(8)	66(8)
309	-1819(12-II-1)	45(8)	1961(13-II-4)	10(13-I-4)	4008(13-II-4)	20(13-I-4)	20(13-I-4)
8002	103	-4070(3)	119(13-II-1)	-1843(2)	15(9)	4561(2)	115(13-II-1)
121	-3717(3)	119(13-II-1)	-1581(2)	15(9)	2679(12-I-1)	197(8)	197(8)
8002	121	-3468(3)	-133(13-II-2)	-1449(2)	19(9)	2679(12-I-1)	248(8)
122	-3113(3)	-133(13-II-2)	-1177(2)	19(9)	-2288(12-II-1)	438(8)	438(8)
8002	122	-3044(3)	205(13-II-2)	-1086(2)	9(9)	-2288(12-II-1)	501(8)
230	-2701(3)	205(13-II-2)	-804(2)	9(9)	-2889(8)	-804(2)	269(8)
8002	230	-2437(3)	139(8)	-824(12-I-1)	-5(8)	-2890(8)	317(8)
231	-2122(3)	139(8)	-666(12-I-1)	-5(8)	-3748(9)	97(9)	97(9)
8002	231	-1888(3)	117(13-II-2)	-836(12-I-1)	-12(8)	-3748(9)	94(8)
232	-1604(3)	117(13-II-2)	798(12-II-1)	-12(8)	-4163(9)	-142(13-II-2)	-142(13-II-2)
8002	232	-1479(12-II-1)	893(12-II-1)	-15(9)	-4163(9)	-132(13-II-2)	-132(13-II-2)
233	-1355(12-II-1)	182(13-I-3)	1060(12-II-1)	-15(9)	-4088(9)	-121(13-I-4)	-121(13-I-4)
8002	233	-1655(12-II-1)	-92(8)	1039(12-II-1)	-9(9)	-4088(9)	-90(13-I-4)
234	-1563(12-II-1)	-92(8)	1211(12-II-1)	-9(9)	-3561(9)	125(9)	125(9)
8002	234	-1926(12-II-1)	-255(13-I-4)	-13(13-I-4)	3036(12-I-1)	-325(13-I-4)	-325(13-I-4)
321	-1871(12-II-1)	-255(13-I-4)	1272(3)	-13(13-I-4)	3037(12-II-1)	-252(13-I-4)	-252(13-I-4)
8002	321	-1300(12-II-1)	201(13-I-3)	1204(2)	10(13-I-3)	3769(12-II-1)	82(8)
322	-1292(12-II-1)	-201(13-I-3)	1548(2)	10(13-I-3)	3769(12-II-1)	61(8)	61(8)
8002	322	-1670(12-II-1)	47(8)	1514(2)	-11(13-I-4)	4283(12-II-1)	9(8)
8003	104	-4006(3)	-120(13-I-4)	-1871(2)	15(9)	4655(2)	113(13-II-4)
115	-3658(3)	-120(13-I-4)	-1613(2)	15(9)	2697(12-I-2)	243(9)	243(9)
8003	115	-3392(3)	136(13-I-2)	-1476(2)	18(8)	2697(12-I-2)	294(9)
116	-3041(3)	136(13-I-2)	-1207(2)	18(8)	-2342(12-II-4)	444(9)	444(9)

8003	116	-2293(3)	215(13-II-2)	-1107(2)	9(8)	-2342(12-II-4)	508(9)
	215	-2598(3)	215(13-II-2)	-826(2)	9(8)	-292(18)	263(8)
8003	215	-2321(3)	141(9)	-846(12-I-4)	-6(9)	-292(18)	310(8)
	216	-2007(3)	141(9)	-688(12-I-4)	-6(9)	-377(19)	87(8)
8003	216	-2072(13-I-4)	125(13-II-2)	-859(12-I-4)	-11(9)	-377(19)	85(8)
	217	-19200(13-I-4)	125(13-II-2)	835(12-I-4)	-11(9)	-4161(9)	-155(13-I-2)
8003	217	-1814(13-I-4)	-185(13-II-3)	944(12-I-3)	16(13-II-3)	-4160(9)	-143(13-I-2)
	218	-1690(13-I-4)	-185(13-II-3)	1112(12-I-3)	16(13-II-3)	-4091(9)	108(13-II-4)
8003	218	-1622(12-I-3)	-106(8)	1070(12-I-3)	-8(9)	-4091(9)	91(13-I-4)
	219	-1530(12-I-3)	-106(8)	1243(12-I-3)	-8(9)	-143(8)	143(8)
8003	219	-1888(12-I-3)	-223(13-I-3)	1076(12-I-4)	-13(13-I-3)	-3557(9)	81(8)
	315	-1833(12-I-3)	-223(13-II-3)	1292(3)	-13(13-I-3)	3132(12-II-3)	260(13-I-4)
8003	315	-1873(13-I-4)	-191(13-I-3)	1223(2)	-10(13-II-3)	3133(12-II-3)	205(13-I-4)
	316	-1465(13-I-4)	-191(13-I-3)	1569(2)	-10(13-I-3)	3863(12-II-4)	93(9)
8003	316	-1779(12-I-3)	53(9)	1523(2)	-12(13-II-4)	3863(12-II-4)	70(9)
	311	-1833(12-I-3)	53(9)	1880(2)	-12(13-II-4)	4431(12-II-1)	14(13-I-4)
8004	105	-4487(3)	-139(13-I-4)	-2045(2)	14(9)	4884(2)	132(13-I-4)
	125	-4465(3)	-139(13-I-4)	-1733(2)	14(9)	2708(12-I-3)	296(9)
8004	125	-4154(3)	158(13-I-2)	-1559(2)	18(8)	2708(12-I-3)	358(9)
	126	-3739(3)	158(13-I-2)	-1241(2)	18(8)	-2484(12-I-4)	449(9)
8004	126	-3839(3)	216(13-II-2)	-1132(2)	9(13-I-2)	-2485(12-I-4)	520(9)
	240	-3447(3)	216(13-II-2)	-809(2)	9(13-I-2)	-3049(8)	262(9)
8004	240	-3144(3)	155(9)	-821(12-I-4)	-5(9)	-3050(8)	317(9)
	241	-2790(3)	155(9)	-647(12-I-4)	-5(9)	-3908(9)	74(8)
8004	241	-2525(13-I-3)	122(13-II-2)	-857(12-I-1)	-10(9)	-3908(9)	82(8)
	242	-2360(13-I-3)	122(13-II-2)	875(12-I-1)	-10(9)	-4243(9)	-153(13-II-2)
8004	242	-2294(13-I-3)	171(13-I-3)	984(12-I-1)	18(13-II-3)	-4242(9)	148(13-I-2)
	243	-2162(13-I-3)	171(13-I-3)	1163(12-I-1)	18(13-II-3)	-4098(9)	-86(13-I-4)
8004	243	-1738(12-II-1)	-106(8)	1155(12-II-1)	-7(8)	-4097(9)	61(13-I-4)
	244	-1640(12-II-1)	-106(8)	1336(12-I-1)	-7(8)	-3453(9)	141(9)
8004	244	-2025(13-I-4)	213(13-I-4)	1151(12-I-1)	-12(13-I-3)	-3452(9)	83(9)
	325	-1967(12-II-1)	213(13-I-4)	1335(12-I-1)	-12(13-I-3)	3291(12-II-1)	267(13-II-4)
8004	325	-1531(12-II-1)	178(13-II-3)	1193(2)	-9(13-II-3)	3292(12-II-1)	208(13-II-4)
	326	-1523(12-II-1)	178(13-II-3)	1550(2)	-9(13-II-3)	4028(12-II-4)	94(9)
8004	326	-1886(12-II-1)	54(9)	1474(2)	-12(13-I-4)	4027(12-II-3)	70(9)
	312	-1940(12-II-1)	54(9)	1837(2)	-12(13-I-4)	4532(12-II-3)	-15(13-II-4)
8005	106	-5078(3)	-147(9)	-2207(2)	18(9)	4951(2)	-38(13-I-4)
	127	-4587(3)	-147(9)	-1844(2)	18(9)	2836(12-I-3)	298(9)
8005	127	-4170(3)	152(13-I-2)	-1627(2)	17(8)	2836(12-I-3)	333(9)
	128	-3695(3)	152(13-I-2)	-1264(2)	17(8)	-2875(12-II-3)	440(9)
8005	128	-4200(3)	207(13-II-2)	-1098(2)	-10(13-II-2)	-2876(12-I-3)	489(9)
	245	-3759(3)	137(9)	-734(2)	-10(13-II-2)	-3173(8)	248(8)
8005	245	-3392(3)	137(9)	-913(12-I-3)	-7(9)	-3174(8)	281(9)
	246	-3001(3)	137(9)	-724(12-I-3)	-7(9)	-3845(9)	65(8)
8005	246	-3330(3)	-130(13-I-2)	-920(12-I-3)	-11(9)	-3847(9)	60(8)
	247	-2990(3)	-130(13-I-2)	1055(12-I-3)	-11(9)	-4044(9)	155(13-I-2)
8005	247	-2776(3)	198(13-I-3)	1090(12-I-3)	17(13-II-3)	-4044(9)	152(13-I-2)
	248	-2550(12-II-3)	198(13-I-3)	1280(12-I-3)	17(13-II-3)	-3835(9)	123(13-II-4)
8005	248	-2381(13-I-4)	-119(9)	1085(12-I-3)	8(13-II-4)	-3833(9)	94(13-II-4)
	249	-2280(13-I-4)	-119(9)	1275(12-I-3)	8(13-II-4)	-3288(9)	149(9)
8005	249	-2612(12-I-3)	179(13-I-4)	1005(12-I-4)	-10(13-I-3)	-3288(9)	88(9)
	327	-2552(13-I-3)	179(13-I-4)	1227(3)	-10(13-I-3)	3445(12-II-3)	252(13-II-4)
8005	327	-1595(13-I-4)	168(13-I-3)	1578(13-I-4)	-10(8)	3447(12-I-3)	194(13-II-4)
	328	-1587(13-I-4)	168(13-II-3)	1767(13-I-4)	-10(8)	4034(12-II-3)	89(9)
8005	328	-1873(12-I-3)	52(9)	1937(13-I-4)	-10(13-II-4)	4034(12-II-3)	66(9)
	313	-1927(12-II-3)	52(9)	2127(13-I-4)	-10(13-I-4)	4514(12-II-1)	-17(13-II-4)
8006	107	-3418(3)	-143(9)	-1605(2)	22(9)	4290(13-I-4)	-35(13-I-4)
	117	-2920(3)	147(13-I-2)	-138(12)	22(9)	2639(12-I-3)	292(9)
8006	117	-2627(3)	147(13-I-2)	-1158(13-I-4)	18(8)	2639(12-I-3)	296(9)
	118	-2627(3)	147(13-I-2)	-1158(13-I-4)	18(8)	-2203(12-II-3)	426(9)
8006	118	-2980(13-II-4)	-202(13-I-2)	-1033(13-I-3)	-11(13-I-2)	-2203(12-II-3)	438(9)
	220	-2825(13-II-4)	-202(13-I-2)	-905(13-I-3)	-11(13-II-2)	-2754(8)	226(8)
8006	220	-2658(13-II-4)	-159(13-II-1)	-743(12-I-3)	-9(9)	-2754(8)	230(9)
	221	-2658(13-II-4)	-159(13-II-1)	-616(12-I-3)	-9(9)	-3631(9)	-50(13-I-4)
8006	221	-2809(13-I-4)	-168(13-I-1)	-777(12-I-3)	-12(9)	-3632(9)	-69(13-I-1)
	222	-2690(13-I-4)	-168(13-I-1)	722(12-I-3)	-12(9)	-4062(9)	187(13-I-2)
8006	222	-2624(13-I-4)	-196(13-II-2)	883(12-I-3)	-17(13-I-3)	-4061(9)	167(13-I-2)

8006	223	-2529(13-I-4)	-196(13-II-2)	1010(12-II-3)	-17(13-I-3)	-4025(9)	105(13-II-2)
	223	-795(13-I-2)	-96(9)	198(13-I-4)	9(13-I-4)	-4024(9)	83(13-II-2)
8006	224	-726(13-I-2)	-96(9)	1326(13-I-4)	9(13-I-4)	-3462(9)	99(2)
	224	-944(12-I-3)	-97(13-II-2)	1515(13-I-1)	8(13-II-2)	-3462(9)	62(2)
8006	317	-903(12-I-3)	-97(13-II-2)	1642(13-I-1)	8(13-II-2)	3121(12-II-3)	151(13-II-4)
	317	-1679(12-I-4)	-114(13-I-3)	1365(13-I-2)	-11(8)	3120(12-II-3)	124(13-II-4)
8006	318	-1673(12-I-4)	-114(13-I-3)	1493(13-I-2)	-11(8)	4145(12-II-3)	65(2)
	318	-2049(12-I-4)	51(2)	1371(2)	11(13-I-4)	4144(12-II-3)	48(2)
8007	314	-2086(12-I-4)	51(2)	1595(2)	11(13-I-4)	4710(12-II-3)	-16(13-II-4)
	16	-402(13-I-4)	9(13-I-1)	4(3)	0	0	19(9)
8007	18	-402(13-I-4)	9(13-I-1)	4(7)	0	0	17(8)
	18	-428(2)	-10(13-I-1)	-5(8)	0	0	15(9)
8007	26	-428(2)	-10(13-I-1)	5(1)	0	0	15(9)
	20	301(8)	-11(9)	-9(1)	0	0	8(8)
8007	22	-289(2)	-5(9)	8(8)	0	0	24(9)
	24	-289(2)	-5(9)	8(1)	0	0	22(9)
8007	24	-61(7)	10(9)	-8(1)	0	0	20(9)
	28	-61(7)	10(9)	8(9)	0	0	5(8)
8007	26	-219(2)	-15(8)	-5(9)	0	0	11(9)
	22	-219(2)	-15(8)	5(1)	0	0	25(8)
8008	15	-403(12-I-3)	8(9)	-4(9)	0	0	21(9)
	17	-403(12-I-3)	8(9)	4(1)	0	0	15(9)
8008	17	-407(13-I-4)	-6(13-II-1)	-5(8)	0	0	15(9)
	25	-407(13-I-4)	-6(13-II-1)	5(1)	0	0	15(9)
8008	19	222(13-I-2)	-13(9)	-8(1)	0	0	4(8)
	15	222(13-I-2)	-13(9)	8(9)	0	0	24(9)
8008	21	-292(13-I-3)	-5(13-II-1)	-8(1)	0	0	16(8)
	23	-292(13-I-3)	-5(13-II-1)	8(8)	0	0	21(9)
8008	23	203(13-I-3)	12(8)	-8(1)	0	0	21(9)
	27	203(13-I-3)	12(8)	8(9)	0	0	3(9)
8008	25	337(13-I-4)	-8(13-I-1)	-5(9)	0	0	15(9)
	21	337(13-I-4)	-8(13-I-1)	5(1)	0	0	18(8)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Pilastri

Scenario di calcolo : Set NT SLV A2 STR/Geo										
Asia	N in	N fin	N		Ty		Tz	Mt		Mz
			kg	kg	kg	kg		kg	kg	
1	1	1	-12644(13-I-1)	-504(13-II-4)	-1507(7)	-2(13-I-1)	3985(12-I-1)	-1054(13-II-4)	671(9)	
	19	19	-12481(13-I-1)	-504(13-II-4)	-1408(12-I-2)	-2(13-I-1)	-1511(9)			
1	19	19	-8682(13-I-1)	197(13-II-1)	-1366(12-I-1)	-1(8)	-1511(9)	670(9)		
	20	20	-8600(13-I-1)	197(13-II-1)	-1366(12-I-1)	-1(8)	-2680(2)	584(9)		
1	20	20	-5332(13-I-1)	425(9)	-1328(12-I-1)	3(8)	-2678(2)	584(9)		
	101	101	-5251(13-I-1)	425(9)	-1328(12-I-1)	3(8)	-3825(2)	-39(13-II-4)		
2	2	2	-10400(13-I-4)	-518(13-II-4)	-1707(7)	0	4046(12-I-1)	-1093(13-II-4)		
	15	15	-10237(13-I-4)	-518(13-II-4)	-1408(12-I-2)	0	-1550(9)	650(9)		
2	15	15	-6816(13-I-4)	-213(13-I-1)	-1364(12-I-2)	0	-1552(9)	648(9)		
	16	16	-6734(13-I-4)	-213(13-I-1)	-1364(12-I-2)	0	-3113(2)	625(9)		
2	16	16	-4555(3)	500(9)	-1326(12-I-2)	3(8)	-3112(2)	623(9)		
	102	102	-4449(3)	500(9)	-1326(12-I-2)	3(8)	-4666(2)	-71(13-II-1)		
3	3	3	-5120(2)	-514(13-II-4)	-1716(7)	0	4134(12-I-1)	-1095(13-II-4)	655(9)	
	17	17	-4908(2)	-514(13-II-4)	-1434(12-I-2)	0	-1554(9)	655(9)		
3	17	17	-4899(2)	-210(13-I-1)	-1380(12-I-2)	0	-1554(9)	655(9)		
	18	18	-4793(2)	-210(13-I-1)	-1380(12-I-2)	0	-3055(2)	587(9)		
3	18	18	-4784(2)	463(9)	-1360(12-I-2)	-3(13-I-4)	-3055(2)	587(9)		
	103	103	-4678(2)	463(9)	-1360(12-I-2)	-3(13-I-4)	-4572(2)	-99(13-II-1)		
4	4	4	-11741(13-I-4)	515(13-I-4)	-1729(7)	0	4196(12-I-2)	1092(13-I-4)		
	25	25	-15777(13-I-4)	515(13-I-4)	-1442(12-I-2)	0	-1551(9)	652(8)		
4	25	25	-8178(13-I-4)	228(13-I-4)	-1398(12-I-2)	0	-1551(9)	652(8)		
	26	26	-8096(13-I-4)	228(13-I-4)	-1398(12-I-2)	0	-3093(2)	585(8)		
4	26	26	-5039(2)	467(8)	-1379(12-I-2)	4(8)	-3093(2)	585(8)		
	104	104	-4933(2)	467(8)	-1379(12-I-2)	4(8)	-4647(2)	-83(13-II-4)		

5	5	-12,108(13-1-4)	539(13-1-4)	-1782(7)	0	4241(12-1-3)	1138(13-1-4)
	21	-11944(13-1-4)	539(13-1-4)	-1447(12-1-3)	0	-1580(9)	665(8)
	21	-8416(13-1-4)	233(13-1-4)	-1413(2)	0	-1580(9)	664(8)
5	22	-8334(13-1-4)	233(13-1-4)	-1405(12-1-3)	0	-323(12)	594(8)
	22	-4854(2)	471(8)	-1368(12-1-3)	3(9)	-3238(2)	594(8)
	105	-4748(2)	471(8)	-1368(12-1-3)	3(9)	-488(12)	117(13-1-4)
6	6	-10707(13-1-4)	528(13-1-4)	-1769(7)	1(13-11-3)	4229(12-1-3)	1106(13-1-4)
	23	-10543(13-1-4)	528(13-1-4)	-1423(12-1-2)	1(13-11-3)	-1631(9)	658(8)
6	23	-7009(13-1-4)	-229(13-1-4)	-1418(2)	1(13-11-4)	-1629(9)	658(8)
	24	-6927(13-1-4)	-229(13-1-4)	-1383(12-1-2)	1(13-11-4)	-3309(2)	604(8)
6	24	-5810(3)	442(8)	-1335(12-1-2)	2(9)	-3310(2)	604(8)
	106	-5704(3)	442(8)	-1372(3)	2(9)	-4966(2)	561(13-1-4)
7	7	-13072(13-1-4)	505(13-1-4)	-1542(7)	2(13-11-3)	4089(12-1-3)	1056(13-1-4)
	27	-12908(13-1-4)	505(13-1-4)	-1389(12-1-3)	2(13-11-3)	-1549(9)	654(8)
7	27	-9097(13-1-4)	-208(13-1-4)	-1358(13-1-4)	1(9)	-1547(9)	654(8)
	28	-9015(13-1-4)	-208(13-1-4)	-1358(13-1-4)	1(9)	-2774(2)	615(8)
7	28	-5691(13-1-4)	454(8)	-1336(13-1-4)	6(9)	-2775(2)	615(8)
	107	-5609(13-1-4)	454(8)	-1336(13-1-4)	6(9)	-4286(13-1-4)	571(13-1-4)
208	208	-5283(13-1-3)	-340(13-11-3)	2309(12-1-1)	0	-4730(12-11-1)	1239(13-1-3)
	308	-5059(13-1-3)	-340(13-1-3)	2309(12-1-1)	0	4382(13-11-2)	30(13-11-4)
209	309	-3658(13-1-2)	-350(13-11-3)	2383(12-1-1)	0	-4993(12-11-1)	-1272(13-11-3)
	309	-3433(13-1-2)	-350(13-11-3)	2383(12-1-1)	0	4009(13-11-4)	32(13-1-4)
210	210	-2667(3)	364(13-1-3)	2586(12-1-1)	0	-5342(12-11-1)	1339(13-1-3)
	310	-2375(3)	364(13-1-3)	2586(12-1-1)	0	4281(12-11-1)	13(13-11-4)
211	211	-2701(3)	373(13-1-3)	2669(12-1-1)	0	-5498(12-11-1)	1370(13-1-3)
	311	-2409(3)	373(13-1-3)	2669(12-1-1)	0	4434(12-11-1)	-17(13-1-4)
212	212	-2673(3)	372(13-1-3)	2751(12-1-1)	0	-5680(12-11-3)	136(13-1-3)
	312	-2381(3)	372(13-1-3)	2751(12-1-1)	0	4555(12-11-3)	-25(12-11-1)
213	213	-3721(13-11-3)	362(13-1-3)	2717(12-1-4)	0	-5694(12-11-3)	1316(13-1-3)
	313	-3497(13-11-3)	362(13-1-3)	2717(12-1-4)	0	4517(12-11-1)	-334(13-1-4)
214	214	-4518(13-1-3)	354(13-1-3)	2845(12-1-3)	0	-5875(12-11-3)	1282(13-1-3)
	314	-5293(13-1-3)	354(13-1-3)	2845(12-1-3)	0	4714(12-11-3)	-37(13-1-4)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Aste generiche

Scenario di calcolo : Set_NT_SLV_A2_STR/Geo									
Asta	N.in.	N.fin.	N	Ty	Tz	Mt	My	Mz	
				kg	kg	kg*m	kg*m	kg*m	
7001			1	-2413(13-11-4)	0	-2(1)	0	1(8)	
	15		15	-2409(13-11-4)	0	2(8)	0	0	1(9)
7002			15	2600(13-11-4)	0	-2(1)	0	0	1(8)
	20		20	2602(13-11-4)	0	2(1)	0	0	1(8)
7003			20	-2292(13-11-4)	0	-2(1)	0	0	1(8)
	102		102	-2290(13-11-4)	0	2(1)	0	0	2(9)
7004			102	1488(13-11-4)	0	-3(1)	0	0	1(8)
	120		120	1493(13-11-4)	0	3(1)	0	0	2(8)
7005			120	-1054(13-11-2)	0	-3(1)	0	0	1(8)
	236		236	-1050(13-11-2)	0	3(1)	0	0	2(8)
7006			236	716(13-1-4)	0	-3(1)	0	0	1(9)
	228		228	719(13-1-4)	0	3(8)	0	0	2(9)
7007			228	1460(13-11-4)	0	-3(1)	0	0	1(8)
	323		323	1461(13-11-4)	0	3(1)	0	0	1(8)
7008			323	-862(12-11-1)	0	-3(1)	0	0	1(8)
	308		308	-863(12-11-1)	0	3(8)	0	0	1(9)
7009			308	-3749(13-1-3)	0	-2(8)	0	0	1(9)
	209		209	-3755(13-1-3)	0	2(1)	0	0	1(9)
7010			208	-3812(13-11-3)	0	-2(1)	0	0	1(8)
	309		309	-3806(13-11-3)	0	2(8)	0	0	1(9)
7011			309	404(12-1-3)	0	-3(1)	0	0	1(8)
	319		319	405(12-1-3)	0	3(8)	0	0	1(9)
7012			319	1383(13-1-4)	0	-3(1)	0	0	1(8)
	238		238	1381(13-1-4)	0	3(8)	0	0	1(9)
7013			238	-732(13-1-4)	0	-3(1)	0	0	1(9)

7014	226	-735(13-1-4)	0	3(1)	0	0	0	2(9)
	226	1216(13-1-2)	0	-3(1)	0	0	0	0
7015	124	1212(13-11-2)	0	3(1)	0	0	0	2(9)
	124	-1614(13-11-4)	0	-3(8)	0	0	0	1(8)
7016	101	-1619(13-1-4)	0	3(1)	0	0	0	1(8)
	101	-2142(13-1-1)	0	-2(1)	0	0	0	1(9)
	16	-2144(13-1-1)	0	2(1)	0	0	0	1(9)
7017	16	-2692(13-11-4)	0	-2(1)	0	0	0	1(8)
	19	-2695(13-11-4)	0	2(8)	0	0	0	1(8)
7018	19	2281(13-11-4)	0	-2(1)	0	0	0	1(9)
	2	2277(13-1-4)	0	2(8)	0	0	0	1(8)
7019	102	-2012(13-11-1)	0	-2(1)	0	0	0	1(9)
	122	-2008(13-11-1)	0	2(1)	0	0	0	1(9)
7020	122	-2266(13-1-1)	0	-2(1)	0	0	0	1(9)
	104	-2270(13-1-1)	0	2(1)	0	0	0	1(9)
7021	104	-1788(13-1-4)	0	-2(1)	0	0	0	1(9)
	126	-1784(13-1-4)	0	2(1)	0	0	0	1(9)
7022	126	-2396(13-1-4)	0	-3(1)	0	0	0	1(9)
	106	-2401(13-1-4)	0	3(1)	0	0	0	2(9)
7023	106	1667(13-1-4)	0	-3(1)	0	0	0	1(9)
	118	1672(13-1-4)	0	3(1)	0	0	0	2(9)
7024	118	-1150(13-1-2)	0	-3(1)	0	0	0	0
	246	-1146(13-1-2)	0	3(1)	0	0	0	2(9)
7025	246	691(13-11-4)	0	-3(1)	0	0	0	0
	223	693(13-11-4)	0	3(8)	0	0	0	2(8)
7026	223	1531(13-1-4)	0	-3(1)	0	0	0	1(9)
	327	1532(13-1-4)	0	3(1)	0	0	0	1(9)
7027	327	1040(12-11-3)	0	-3(8)	0	0	0	1(9)
	314	1040(12-11-3)	0	3(1)	0	0	0	1(8)
7028	314	-3885(13-11-3)	0	-2(8)	0	0	0	1(8)
	213	-3891(13-11-3)	0	2(1)	0	0	0	1(9)
7029	214	-3963(13-1-3)	0	-2(1)	0	0	0	1(9)
	313	-3958(13-1-3)	0	2(8)	0	0	0	1(8)
7030	313	367(12-1-1)	0	-3(1)	0	0	0	1(9)
	317	367(12-1-1)	0	3(1)	0	0	0	1(9)
7031	317	-1300(13-1-1)	0	-3(8)	0	0	0	1(9)
	248	-1302(13-1-1)	0	3(1)	0	0	0	2(9)
7032	248	756(13-1-4)	0	-3(1)	0	0	0	0
	221	754(13-1-4)	0	3(1)	0	0	0	2(8)
7033	221	1287(13-1-2)	0	-3(1)	0	0	0	0
	128	1284(13-1-2)	0	3(1)	0	0	0	2(8)
7034	128	-1823(13-1-4)	0	-3(1)	0	0	0	1(9)
	107	-1828(13-1-4)	0	3(1)	0	0	0	2(9)
7035	107	2189(13-1-4)	0	-2(1)	0	0	0	1(8)
	24	2187(13-1-4)	0	2(2)	0	0	0	1(8)
7036	24	-2692(13-1-4)	0	-2(8)	0	0	0	1(9)
	27	-2695(13-1-4)	0	2(1)	0	0	0	1(8)
7037	27	2290(13-1-4)	0	-2(1)	0	0	0	1(8)
	6	2285(13-1-4)	0	2(1)	0	0	0	1(9)
7038	7	-2438(13-1-4)	0	-2(1)	0	0	0	1(9)
	23	-2434(13-1-4)	0	2(8)	0	0	0	1(8)
7039	23	2620(13-1-4)	0	-2(1)	0	0	0	1(9)
	28	2622(13-1-4)	0	2(8)	0	0	0	1(9)
7040	28	-2357(13-1-4)	0	-2(1)	0	0	0	1(8)
	106	-2355(13-1-4)	0	2(1)	0	0	0	1(8)
7041	124	-2014(13-1-1)	0	-2(1)	0	0	0	1(9)
	103	-2019(13-1-1)	0	2(1)	0	0	0	1(9)
7042	103	-2354(13-1-1)	0	-2(1)	0	0	0	1(9)
	116	-2350(13-1-1)	0	2(1)	0	0	0	1(9)
7043	116	1674(13-1-4)	0	-2(1)	0	0	0	1(9)
	105	1670(13-1-4)	0	2(1)	0	0	0	1(9)
7044	105	-2381(13-11-4)	0	-3(1)	0	0	0	1(9)
	128	-2377(13-11-4)	0	3(1)	0	0	0	1(9)
7045	309	-2122(13-1-4)	0	-3(1)	0	0	0	1(8)
	321	-2121(13-1-4)	0	3(8)	0	0	0	1(9)
7046	321	-1992(13-1-4)	0	-3(1)	0	0	0	1(9)
	311	-1993(13-1-4)	0	3(8)	0	0	0	1(8)

7047	311	-1059(13-II-2)	0	-3(1)	0	0	1(8)
	325	-1058(13-II-2)	0	3(1)	0	0	1(9)
7048	325	-2198(13-I-4)	0	-3(1)	0	0	1(9)
	313	-2198(13-I-4)	0	3(2)	0	0	1(8)
7049	327	-1998(13-II-4)	0	-3(1)	0	0	1(8)
	312	-1998(13-II-4)	0	3(8)	0	0	1(8)
7050	312	-1047(13-I-2)	0	-3(1)	0	0	1(9)
	315	-1047(13-I-2)	0	3(1)	0	0	1(8)
7051	315	-2341(13-II-4)	0	-3(2)	0	0	1(8)
	310	-2341(13-II-4)	0	3(1)	0	0	1(9)
7052	310	-1778(13-I-4)	0	-3(1)	0	0	1(8)
	323	-1777(13-I-4)	0	3(1)	0	0	1(8)
7053	105	-2171(13-II-4)	0	0	0	0	0
	26	-2173(13-II-4)	0	0	0	0	0
7054	26	-2397(13-I-4)	0	0	0	0	0
	21	-2399(13-I-4)	0	0	0	0	0
7055	21	-1643(13-II-4)	0	0	0	0	0
	4	-1647(13-II-4)	0	0	0	0	0
7056	5	-1713(13-I-4)	0	0	0	0	0
	25	-1709(13-I-4)	0	0	0	0	0
7057	25	-2348(13-II-4)	0	0	0	0	0
	22	-2346(13-II-4)	0	0	0	0	0
7058	22	-2092(13-I-4)	0	0	0	0	0
	104	-2090(13-I-4)	0	0	0	0	0
7059	116	-1440(13-II-2)	0	-2(1)	0	0	0
	241	-1436(13-II-2)	0	2(1)	0	0	0
7060	241	327(12-I-3)	0	-3(1)	0	0	0
	218	330(12-I-3)	0	3(1)	0	0	0
7061	218	1616(13-II-4)	0	-3(1)	0	0	0
	325	1618(13-II-4)	0	3(1)	0	0	0
7062	315	-1632(13-II-4)	0	-3(1)	0	0	0
	243	-1633(13-II-4)	0	3(1)	0	0	0
7063	243	371(13-II-4)	0	-3(1)	0	0	0
	216	368(13-II-4)	0	3(1)	0	0	0
7064	216	1482(13-II-2)	0	-2(1)	0	0	0
	126	1478(13-II-2)	0	2(1)	0	0	0

VERIFICHE STATO LIMITE ULTIMO

Verifica delle travi
Scenario di calcolo : Set NT SLV A2 STR/CEO

Grave di: Fond. = 9003 [1., 2.] Plastreca [1., 2] Spec. R.: Fby = 60.0 cm Bz = 100.0 cm L = 149.9 cm Lp = 161.9 cm Terreno: Terreno 1 Criterio: CLS Travifondazione - Verifica a flessione: Verificato									
X	M-	M+	ΔM^-	ΔM^+	AlS	Mf-	Mf+	C-	C+
	kg·m	kg·m	kg·m	kg·m	cmq	kg·m	kg·m		
ILN	-791	-270	5790	4227	12.06	12.06	42365	(12+13)-VIII-2	(12+13)-VIII-3
16.2	1667	1423	5955	3924	12.06	12.06	42365	(12+13)-VIII-2	(12+13)-VIII-3
CAMP	10749	10485	583	2059	12.06	12.06	42365	(12+13)-IV-2	(12+13)-IV-3
145.7	11129	11532	-22	1013	12.06	12.06	42365	(12+13)-IV-2	(12+13)-IV-3
FLN	11331	12545	--	--	12.06	12.06	42365	(12+13)-IV-2	(12+13)-IV-3

X	x-	d-	x-/d-	x+	d+	Mr. g* ^{cm}	Mr. g* ^m	C-	C+	Stato-
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	(12+13)V+II-2	(12+13)V+II-3	Parz.
16.2	19.3	95.9	0.201	19.3	95.9	0.201	42365	(12+13)V+II-2	(12+13)V+II-3	Parz.
CAMP	19.4	95.9	0.202	19.4	95.9	0.202	42365	(12+13)-IV-2	(12+13)-IV-3	Parz.
145.7	19.4	95.9	0.202	19.4	95.9	0.202	42365	(12+13)-IV-2	(12+13)-IV-3	Parz.
FLN	19.4	95.9	0.202	19.4	95.9	0.202	42365	(12+13)-IV-2	(12+13)-IV-3	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$
 $\text{Comb} = (12+13) \cdot \text{VIII} \cdot 2$

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	16210	--	125983	87691	87691	0	42365	161.9	10.39	5.41
Des							42365			

Trave di Fond.: 9003 | 2, 3 | Pilastrate | 2, 3 |

Sez. R: $B_y = 60.0 \text{ cm}$ $B_z = 100.0 \text{ cm}$ $L = 89.0 \text{ cm}$ $L_n = 89.0 \text{ cm}$ **Terreno: Terreno I**
Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	M _c kg ^a m	M ₊ kg ^a m	ΔM ₋ kg ^a m	ΔM ₊ kg ^a m	Af _S cmq	Mf ^a kg ^a m	C ⁻	C ⁺	CS
com	12501	13606	--	--	12.06	42365	(12+13)IV-2	(12+13)IV-3	3.11
ILN	8.9	11793	12966	640	12.06	42365	(12+13)IV-2	(12+13)IV-3	3.11
CAMP	9411	11026	7090	2580	12.06	42365	(12+13)IV-2	(12+13)IV-3	3.11
801	4749	7833	4532	3096	12.06	42365	(12+13)IV-2	(12+13)IV-3	3.88
FLN	3744	7223	4660	3059	12.06	42365	(12+13)IV-2	(12+13)IV-3	4.12

X	x-	d-	x-/d-	x+	d+	Mr- kg* ^m	Mr+ kg* ^m	C-	C+	Stato- Stato-
ILN	19.4	95.9	0.202	19.4	95.9	0.202	423.65	(12+13)-IV-2	(12+13)-IV-3	Parz.
8.9	19.4	95.9	0.202	19.4	95.9	0.202	423.65	(12+13)-IV-2	(12+13)-IV-3	Parz.
CAMP	19.4	95.9	0.202	19.4	95.9	0.202	423.65	(12+13)-IV-2	(12+13)-IV-3	Parz.
80.1	19.4	95.9	0.202	19.4	95.9	0.202	423.65	(12+13)-IV-2	(12+13)-IV-3	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.202	423.65	(12+13)-IV-2	(12+13)-IV-3	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

$$\text{Comb} = (12+13)\text{-VIII-2}$$

Sez	Td	VRdms	VRd	VRsd	VRd	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg	cm	cmq/m	
Sin	12258	--	125983	79129	79129	0	42365	89.0	9.37
Des							42365		6.46

Trave di Fond.: 9003 [3, 4 | Pilastrate [3, 4]

Sez. R: $B_y=60.0$ cm $B_z=100.0$ cm $L=90.1$ cm $L_n=90.1$ cm Terreno: **Terreno I**
Criterio : CLS TraviFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	AfS	AfI	Mf-	Mf+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4813	8215	--	--	12.06	12.06	42365	42365	(12+13)-IV-2	(12+13)-IV-3	5.16
9.0	4047	7391	767	824	12.06	12.06	42365	42365	(12+13)-IV-2	(12+13)-IV-3	5.16
CAMP	740	4101	4073	4114	12.06	12.06	42365	42365	(12+13)-IV-2	(12+13)-IV-3	5.16
81.1	1594	4783	--	532	12.06	12.06	42365	42365	8	(12+13)-VII-2	7.97
FLN	1424	5316	--	--	12.06	12.06	42365	42365	8	(12+13)-VII-2	7.97

X	cm	x-	cm	d-	x-/d-	x+	cm	d+	x+/d+	Mr-	kg*m	C-	C+	Stato-	Stato-
ILN	193	193	95.9	0.201	19.3	95.9	0.201	423.65	423.65	(12+13)+IV-2	(12+13)+IV-3	Parz.	Parz.		
	9.0	193	95.9	0.201	19.3	95.9	0.201	423.65	423.65	(12+13)+IV-2	(12+13)+IV-3	Parz.	Parz.		
CAMP	193	95.9	0.201	19.3	95.9	0.201	423.65	423.65	(12+13)+IV-2	(12+13)+IV-3	Parz.	Parz.	Parz.		
	8.1	192	95.9	0.200	19.3	95.9	0.200	423.65	423.65	8	(12+13)+VII-2	Parz.	Parz.		
FLN	192	95.9	0.200	19.3	95.9	0.201	423.65	423.65	8	(12+13)+VII-2	Parz.	Parz.	Parz.		

Verifica a taglio: $\cot(\theta) = 2.500$

$$\text{Comb} = (12+13)\text{-VIII-2}$$

Sez	Tid	VRdms	VRcd	VRsd	VRd	Mr	Dx	Stafte	CS
	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	11710	--	125983	90651	90651	0	42365	90.1	10.74
Des							42365		7.74

Grave di Fond.: 9003 | 4, 5 | Pilastrate | 4, 5 |

Sez. R: $B_y = 60.0 \text{ cm}$ $B_z = 100.0 \text{ cm}$ $L = 88.8 \text{ cm}$ $L_n = 88.8 \text{ cm}$ **Terreno: Terreno I**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	916	4888	826	--	12.06	12.06	42365	42365	6	(12+13)-VII-2	8.67
CAMP	924	4475	776	413	12.06	12.06	42365	42365	8	(12+13)-VII-2	8.67
			--				42365	42365	8	(12+13)-VII-2	8.67

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
79.9	1912	4014	--	447	12.06	12.06	42365	42365	8	(12+13)~VII-2	9.50
FLN	1866	3931	--	434	12.06	12.06	42365	42365	8	(12+13)~VII-2	9.71

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	6	(12+13)~VII-2	Parz.
8.9	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	8	(12+13)~VII-2	Parz.
CAMP	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	8	(12+13)~VII-2	Parz.
79.9	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	8	(12+13)~VII-2	Parz.
FLN	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	8	(12+13)~VII-2	Parz.

Verifica a taglio:cof(0) =2,500

Comb =3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
kg	kg	kg	kg	kg	kg	kg	kg*m		cm	cmq/m
Sin	3262	--	125983	79359	79359	0	42365	88.8	9.40	24.3
Des							42365			

Trave di Fond.: 9003 | 5, 6 | Pilastrate | 5, 6 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.5 cm Ln= 149.5 cm Terreno: Terrenol

Criterio : CLS Travifondazione - Verifica a flessione :Verificato

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	-1831	1416	5368	3334	12.06	12.06	42365	42365	(12+13)~VIII-3	(12+13)~VIII-2	8.92
14.9	356	2810	4818	3055	12.06	12.06	42365	42365	(12+13)~VIII-3	(12+13)~VIII-2	7.22
CAMP	11002	10622	2200	2358	12.06	12.06	42365	42365	(12+13)~IV-3	(12+13)~IV-2	3.21
134.5	12164	11807	1037	1173	12.06	12.06	42365	42365	(12+13)~IV-3	(12+13)~IV-2	3.21
FLN	13201	12980	--	--	12.06	12.06	42365	42365	(12+13)~IV-3	(12+13)~IV-2	3.21

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)~VIII-3	(12+13)~VIII-2	Parz.
14.9	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)~VIII-3	(12+13)~VIII-2	Parz.
CAMP	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)~IV-3	(12+13)~IV-2	Parz.
134.5	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)~IV-3	(12+13)~IV-2	Parz.
FLN	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)~IV-3	(12+13)~IV-2	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)~IV-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
kg	kg	kg	kg	kg	kg	kg	kg*m		cm	cmq/m
Sin	13280	--	125983	88128	88128	0	42365	149.5	10.44	6.64
Des							42365			

Trave di Fond.: 9003 | 6, 7 | Pilastrate | 6, 7 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.7 cm Ln= 161.7 cm Terreno: Terrenol

Criterio : CLS Travifondazione - Verifica a flessione :Verificato

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11985	11880	--	--	12.06	12.06	42365	42365	(12+13)~IV-3	(12+13)~IV-2	3.53
16.2	11696	10972	288	909	12.06	12.06	42365	42365	(12+13)~IV-3	(12+13)~IV-2	3.53
CAMP	11228	10027	756	1854	12.06	12.06	42365	42365	(12+13)~IV-3	(12+13)~IV-2	3.53
145.5	1665	1424	5081	3805	12.06	12.06	42365	42365	(12+13)~IV-3	(12+13)~IV-2	6.28
FLN	-808	-250	5874	4144	12.06	12.06	42365	42365	(12+13)~IV-3	(12+13)~IV-2	8.36

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)~IV-3	(12+13)~IV-2	Parz.
16.2	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)~IV-3	(12+13)~IV-2	Parz.
CAMP	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)~IV-3	(12+13)~IV-2	Parz.
145.5	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)~IV-3	(12+13)~IV-2	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)~IV-3	(12+13)~IV-2	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)~IV-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
kg	kg	kg	kg	kg	kg	kg	kg*m		cm	cmq/m
Sin	16240	--	125983	87866	87866	0	42365	161.7	10.41	5.41
Des							42365			

Trave di Fond.: 9004 | 208, 209 | Pilastrate | 208, 209 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.3 cm Ln= 161.2 cm Terreno: Terrenol

Criterio : CLS Travifondazione - Verifica a flessione :Verificato

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	195	482	3610	2758	12.06	12.06	42365	42365	(12+13)~II-2	(12+13)~II-3	11.1
16.1	8662	1595	3264	2522	12.06	12.06	42365	42365	(12+13)~II-2	(12+13)~II-3	8.60
CAMP	1629	7268	1237	1281	12.06	12.06	42365	42365	(12+13)~VI-2	(12+13)~VI-3	4.29
145.1	9280	7916	586	632	12.06	12.06	42365	42365	(12+13)~VI-2	(12+13)~VI-3	4.29
FLN	9866	8548	--	--	12.06	12.06	42365	42365	(12+13)~VI-2	(12+13)~VI-3	4.29

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)~II-2	(12+13)~II-3	Parz.
16.1	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)~II-2	(12+13)~II-3	Parz.
CAMP	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)~VI-2	(12+13)~VI-3	Parz.
145.1	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)~VI-2	(12+13)~VI-3	Parz.
FLN	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)~VI-2	(12+13)~VI-3	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)~II-2

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
kg	kg	kg	kg	kg	kg	kg	kg*m		cm	cmq/m
Sin	9584	--	125983	88148	88148	0	42365	161.2	10.44	9.20
Des							42365			

Trave di Fond.: 9004 | 209, 210 | Pilastrate | 209, 210 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.7 cm Ln= 149.7 cm Terreno: Terrenol

Criterio : CLS Travifondazione - Verifica a flessione :Verificato

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11331	10000	--	--	12.06	12.06	42365	42365	(12+13)~VI-2	(12+13)~VI-3	3.74
15.0	11107	9473	224	527	12.06	12.06	42365	42365	(12+13)~VI-2	(12+13)~VI-3	3.74
CAMP	9144	7251	2187	2749	12.06	12.06	42365	42365	(12+13)~VI-2	(12+13)~VI-3	3.74
134.7	8154	5740	1313	1250	12.06	12.06	42365	42365	(12+13)~VIII-4	(12+13)~VIII-1	4.47
FLN	7627	5332	1419	1214	12.06	12.06	42365	42365	(12+13)~VIII-4	(12+13)~VIII-1	4.68

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	19.4	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)~VI-2	(12+13)~VI-3	Parz.
15.0	19.4	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)~VI-2	(12+13)~VI-3	Parz.
CAMP	19.4	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)~VI-2	(12+13)~VI-3	Parz.
134.7	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)~VIII-4	(12+13)~VIII-1	Parz.
FLN	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)~VIII-4	(12+13)~VIII-1	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)~II-2

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
kg	kg	kg	kg	kg	kg	kg	kg*m		cm	cmq/m
Sin	5372	--	125983	88205	88205	0	42365	149.7	10.45	16.4
Des							42365			

Trave di Fond.: 9004 | 210, 211 | Pilastrate | 210, 211 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.0 cm Ln= 149.0 cm Terreno: Terrenol

Criterio : CLS Travifondazione - Verifica a flessione :Verificato

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	9091	6814	--	--	12.06	12.06	42365	42365	(12+13)~VIII-1	(12+13)~VIII-1	4.66
14.9	8762	6232	330	582	12.06	12.06	42365	42365	(12+13)~VIII-4	(12+13)~VIII-1	4.66

240

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Verifica a taglio: cot(θ) =2,500

Comb =(12+13)·VI-1

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg* ^m	cm	cmq/m	
Sin	5492	--	125983	87871	87871	0	42365	149.7	10.41	16.0
Des							42365			

Trave di Fond. : 9004 | 213, 214 | Pilastrate [213, 214]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.7 cm Ln= 161.7 cm Terreno: TerrenoI

Criterio : CLS_TraviFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr+	Mr-	C-	C+	CS
cm	kg* ^m	kg* ^m	kg* ^m	kg* ^m	cmq	cmq	kg* ^m	kg* ^m			
ILN	9892	8775	--	--	12.06	12.06	42365	42365	(12+13)·II-3	(12+13)·II-2	4.28
16.2	9349	8149	543	626	12.06	12.06	42365	42365	(12+13)·II-3	(12+13)·II-2	4.28
CAMP	8733	7499	1159	1276	12.06	12.06	42365	42365	(12+13)·II-3	(12+13)·II-2	4.28
145.5	1695	1619	3327	2601	12.06	12.06	42365	42365	(12+13)·II-3	(12+13)·II-2	8.44
FLN	188	481	3690	2828	12.06	12.06	42365	42365	(12+13)·II-3	(12+13)·II-2	10.9

Verifica a taglio: cot(θ) =2,500

Comb =(12+13)·II-3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg* ^m	kg* ^m			
ILN	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)·II-3	(12+13)·II-2	Parz.
16.2	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)·II-3	(12+13)·II-2	Parz.
CAMP	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)·II-3	(12+13)·II-2	Parz.
145.5	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)·II-3	(12+13)·II-2	Parz.
FLN	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)·II-3	(12+13)·II-2	Parz.

Verifica a taglio: cot(θ) =2,500

Comb =(12+13)·II-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg* ^m	cm	cmq/m	
Sin	9824	--	125983	87866	87866	0	42365	161.7	10.41	8.94
Des							42365			

Verifica Stabilità aste Metalliche

Scenario di calcolo : Set NT_SLV_A2_STR/GEO

Asta : I | I , 19 |

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq:Verificato

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	kyY	kyZ	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m							
-9468	4343	-707	211298	20492	9673	27	45	0.960	0.832	--	0.611	0.300 0.367 0.500

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
I	Y	9468	2654	212	193231	19516	9213	(12+13)·III-2	4.81
I	Z	9468	1593	354	167375	19516	9213	(12+13)·III-2	5.66

Asta : I | I , 20 |

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq:Verificato

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	kyY	kyZ	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m							
-5336	-2451	670	211298	20492	9673	13	23	0.975	0.964	--	0.849	0.568 0.509 0.947

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
I	Y	5336	2080	381	196194	19516	9213	9	5.71
I	Z	5336	1248	635	194055	19516	9213	9	6.24

Asta : I | I , 10 |

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq:Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr+	Mr-	C-	C+	CS
CAMP	8394	5663	698	1151	12.06	12.06	42365	42365	(12+13)·VIII-4	(12+13)·VIII-1	4.66
134.1	8439	5737	309	70	12.06	12.06	42365	42365	(12+13)·VIII-4	(12+13)·III-1	4.84
FLN	8286	5807	391	--	12.06	12.06	42365	42365	(12+13)·VIII-4	(12+13)·III-1	4.88

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg* ^m	kg* ^m			
ILN	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)·VIII-4	(12+13)·VIII-1	Parz.
14.9	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)·VIII-4	(12+13)·VIII-1	Parz.
CAMP	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)·VIII-4	(12+13)·VIII-1	Parz.
134.1	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)·VIII-4	(12+13)·III-1	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)·VIII-4	(12+13)·III-1	Parz.

Verifica a taglio: cot(θ) =2,500

Comb =(12+13)·III-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg* ^m	cm	cmq/m	
Sin	5535	--	125983	81902	81902	0	42365	149.0	9.70	14.8
Des							42365			

Trave di Fond. : 9004 | 211, 212 | Pilastrate [211, 212]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.4 cm Ln= 149.4 cm Terreno: TerrenoI

Criterio : CLS_TraviFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr+	Mr-	C-	C+	CS
cm	kg* ^m	kg* ^m	kg* ^m	kg* ^m	cmq	cmq	kg* ^m	kg* ^m			
ILN	8418	5902	--	--	12.06	12.06	42365	42365	(12+13)·III-4	(12+13)·III-1	5.03
14.9	8351	5668	68	234	12.06	12.06	42365	42365	(12+13)·III-4	(12+13)·III-1	5.03
CAMP	8273	4627	145	1468	12.06	12.06	42365	42365	(12+13)·III-4	(12+13)·II-2	5.03
134.5	8020	5347	176	748	12.06	12.06	42365	42365	(12+13)·I-3	(12+13)·II-2	5.19
FLN	7903	6095	258	--	12.06	12.06	42365	42365	(12+13)·I-3	(12+13)·II-2	5.19

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg* ^m	kg* ^m			
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)·III-4	(12+13)·III-1	Parz.
14.9	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)·III-4	(12+13)·III-1	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)·III-4	(12+13)·II-2	Parz.
134.5	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)·III-3	(12+13)·II-2	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)·III-3	(12+13)·II-2	Parz.

Verifica a taglio: cot(θ) =2,500

Comb =(12+13)·VIII-4

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg* ^m	cm	cmq/m	
Sin	6419	--	125983	81611	81611	0	42365	149.4	9.67	12.7
Des							42365			

Trave di Fond. : 9004 | 212, 213 | Pilastrate [212, 213]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.7 cm Ln= 149.7 cm Terreno: TerrenoI

Criterio : CLS_TraviFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr+	Mr-	C-	C+	CS
cm	kg* ^m	kg* ^m	kg* ^m	kg* ^m	cmq	cmq	kg* ^m	kg* ^m			
ILN	6604	4659	1662	1455	12.06	12.06	42365	42365	(12+13)·III-3	(12+13)·II-2	5.13
15.0	7202	5141	1592	1514	12.06	12.06	42365	42365	(12+13)·III-3	(12+13)·II-2	4.82
CAMP	10626	8999	648	1159	12.06	12.06	42365	42365	(12+13)·III-3	(12+13)·II-2	3.76
134.7	10972	9580	301	578	12.06	12.06	42365	42365	(12+13)·III-3	(12+13)·II-2	3.76
FLN	11274	10158	--	--	12.06	12.06	42365	42365	(12+13)·III-3	(12+13)·II-2	3.76

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg* ^m	kg* ^m			
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)·III-3	(12+13)·II-2	Parz.
15.0	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)·III-3	(12+13)·II-2	Parz.
CAMP	19.4	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)·III-3	(12+13)·II-2	Parz.
134.7	19.4	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)·III-3	(12+13)·II-2	Parz.
FLN	19.4	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)·III-3	(12+13)·II-2	Parz.

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5702	-4187	50	211298	20492	9673	13	23	0.975	0.964	--	0.837	0.240	0.502

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5702	3503	12	196194	19516	9213	(12+13)-VIII-2	4.77
1	Z	5702	2102	20	194055	19516	9213	(12+13)-VIII-2	7.18

Asia : 2 [2 , 15]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-9409	2933	863	211298	20492	9673	27	45	0.960	0.832	--	0.622	0.300	0.373

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	9409	1824	259	193231	19516	9213	(12+13)-IV-1	5.87
1	Z	9409	1094	432	167375	19516	9213	(12+13)-IV-1	6.28

Asia : 2 [15 , 16]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3819	-3113	419	211298	20492	9673	13	23	0.975	0.964	--	0.781	0.597	0.468

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3819	2431	250	196194	19516	9213	2	5.84
1	Z	3819	1459	417	194055	19516	9213	2	7.16

Asia : 2 [16 , 102]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4525	-4666	417	211298	20492	9673	13	23	0.975	0.964	--	0.868	0.334	0.521

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4525	4051	139	196194	19516	9213	2	4.07
1	Z	4525	2431	232	194055	19516	9213	2	5.78

Asia : 3 [3 , 17]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3074	3966	-680	211298	20492	9673	27	45	0.960	0.832	--	0.623	0.299	0.374

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3074	2435	203	193231	19516	9213	(12+13)-III-2	6.14
1	Z	3074	1461	339	167375	19516	9213	(12+13)-III-2	7.69

Asia : 3 [17 , 18]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4059	-2729	655	211298	20492	9673	13	23	0.975	0.964	--	0.829	0.574	0.497

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4059	2262	376	196194	19516	9213	9	5.64
1	Z	4059	1357	627	194055	19516	9213	9	6.31

Asia : 3 [18 , 103]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4784	-4572	369	211298	20492	9673	13	23	0.975	0.964	--	0.869	0.341	0.521

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4784	3972	126	196194	19516	9213	2	4.14
1	Z	4784	2383	210	194055	19516	9213	2	5.90

Asia : 4 [4 , 25]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-7844	3955	-627	211298	20492	9673	27	45	0.960	0.832	--	0.627	0.300	0.376

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7844	2479	188	193231	19516	9213	(12+13)-III-2	5.32
1	Z	7844	1488	313	167375	19516	9213	(12+13)-III-2	6.37

Asia : 4 [25 , 26]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4993	-2742	648	211298	20492	9673	13	23	0.975	0.964	--	0.828	0.574	0.497

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4993	2270	372	196194	19516	9213	9	5.49
1	Z	4993	1362	620	194055	19516	9213	9	6.14

Asia : 4 [26 , 104]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5039	-4647	343	211298	20492	9673	13	23	0.975	0.964	--	0.868	0.340	0.521

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5039	4033	117	196194	19516	9213	2	4.08
1	Z	5039	2420	194	194055	19516	9213	2	5.85

Asia : 5 [5 , 21]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-11387	3146	1054	211298	20492	9673	27	45	0.960	0.832	--	0.610	0.301	0.366

Clis	Dir	N	Mvseq	Mzseq	MvRk	MzRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	11387	1919	317	193231	19516	9213	(12+13)-VIII-1	5.22
1	Z	11387	1151	529	167375	19516	9213	(12+13)-VIII-1	5.42

Asta : 5 [21 , 22]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3458	-2858	642	211298	20492	9673	13	23	0.975	0.964	--	0.822	0.572	0.493
													0.954

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3458	2349	368	196194	19516	9213	9	5.62
	Z	3458	1410	613	194055	19516	9213	9	6.39

Asta : 5 [22 , 105]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4854	-4883	308	211298	20492	9673	13	23	0.975	0.964	--	0.867	0.348	0.520
													0.579

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4854	4233	107	196194	19516	9213	2	3.95
	Z	4854	2540	178	194055	19516	9213	2	5.73

Asta : 6 [6 , 23]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-7204	3912	-538	211298	20492	9673	27	45	0.960	0.832	--	0.637	0.296	0.382
													0.494

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7204	2491	159	193231	19516	9213	(12+13)>VII-2	5.49
	Z	7204	1495	266	167375	19516	9213	(12+13)>VII-2	6.73

Asta : 6 [23 , 24]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5207	-2892	630	211298	20492	9673	13	23	0.975	0.964	--	0.827	0.583	0.496
													0.971

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5207	2391	367	196194	19516	9213	9	5.29
	Z	5207	1435	612	194055	19516	9213	9	6.00

Asta : 6 [24 , 106]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5773	-4966	331	211298	20492	9673	13	23	0.975	0.964	--	0.868	0.379	0.521
													0.632

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5773	4312	126	196194	19516	9213	2	3.79
	Z	5773	2587	209	194055	19516	9213	2	5.40

Asta : 7 [7 , 27]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-12300	4000	980	211298	20492	9673	27	45	0.960	0.832	--	0.552	0.298	0.331
													0.497

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	12300	2207	292	193231	19516	9213	(12+13)>VIII-1	4.80
	Z	12300	1324	487	167375	19516	9213	(12+13)>VIII-1	5.15

Asta : 7 [27 , 28]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2917	-2492	624	211298	20492	9673	13	23	0.975	0.964	--	0.849	0.591	0.510
													0.984

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2917	2116	368	196194	19516	9213	9	6.12
	Z	2917	1270	614	194055	19516	9213	9	6.81

Asta : 7 [28 , 107]

Sez. G: HE 240 A L=135.5 cm Ln1=135.5 cm Ln2=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5421	-4692	62	211298	20492	9673	13	23	0.975	0.964	--	0.825	0.240	0.495
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5421	3872	15	196194	19516	9213	(12+13)>VIII-1	4.39
	Z	5421	2323	25	194055	19516	9213	(12+13)>VIII-1	6.68

Asta : 208 [208 , 308]

Sez. G: HE 240 A L=372.0 cm Ln1=372.0 cm Ln2=372.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4837	5091	-989	211298	20492	9673	37	62	0.916	0.716	--	0.604	0.370	0.362
													0.617

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4837	3073	366	184232	19516	9213	(12+13)>II-4	4.48
	Z	4837	1844	610	144109	19516	9213	(12+13)>II-4	5.15

Asta : 209 [209 , 309]

Sez. G: HE 240 A L=372.0 cm Ln1=372.0 cm Ln2=372.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1464	-4769	55	211298	20492	9673	37	62	0.916	0.716	--	0.601	0.363	0.361
													0.605

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1464	2867	20	184232	19516	9213	(12+13)>II-4	6.37
	Z	1464	1720	33	144109	19516	9213	(12+13)>II-4	9.81

Asta : 210 [210 , 310]

Sez. G: HE 240 A L=372.0 cm Ln1=372.0 cm Ln2=372.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1730	3769	-1082	211298	20492	9673	37	62	0.916	0.716	--	0.601	0.364	0.361
													0.606

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	1730	2266	393	184232	19516	9213	(12+13)-IV-4	5.95
I	Z	1730	1360	656	144109	19516	9213	(12+13)-IV-4	6.54

Asta : 211 [211 , 311]

Sez. G: HE 240 A L=372.0 cm Ln1=372.0 cm Ln2=372.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-1742	4228	719	211298	20492	9673	37	62	0.916	0.716	--	0.601	0.364	0.361
													0.606

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	1742	2542	261	184232	19516	9213	(12+13)-III-3	5.95
I	Z	1742	1525	435	144109	19516	9213	(12+13)-III-3	7.27

Asta : 212 [212 , 312]

Sez. G: HE 240 A L=372.0 cm Ln1=372.0 cm Ln2=372.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-1497	4337	679	211298	20492	9673	37	62	0.916	0.716	--	0.601	0.363	0.361
													0.605

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	1497	2607	247	184232	19516	9213	(12+13)-V-3	5.94
I	Z	1497	1364	411	144109	19516	9213	(12+13)-V-3	7.40

Asta : 213 [213 , 313]

Sez. G: HE 240 A L=372.0 cm Ln1=372.0 cm Ln2=372.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-2619	4115	-652	211298	20492	9673	37	62	0.916	0.716	--	0.602	0.365	0.361
													0.609

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	2619	2477	238	184232	19516	9213	(12+13)-V-2	5.99
I	Z	2619	1486	397	144109	19516	9213	(12+13)-V-2	7.28

Asta : 214 [214 , 314]

Sez. G: HE 240 A L=372.0 cm Ln1=372.0 cm Ln2=372.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-5811	5029	1252	211298	20492	9673	37	62	0.916	0.716	--	0.604	0.372	0.363
													0.620

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	5811	3039	458	184232	19516	9213	(12+13)-VI-3	4.22
I	Z	5811	1823	764	144109	19516	9213	(12+13)-VI-3	4.62

Asta : 8000 [101 , 119]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-2450	4042	-141	211298	20492	9673	18	30	0.946	0.924	--	0.882	0.323	0.529
													0.538

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	2450	3567	46	190274	19516	9213	(12+13)-III-2	4.98
I	Z	2450	2140	76	185852	19516	9213	(12+13)-III-2	7.63

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Asta : 8000 [119 , 120]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-1716	2588	-68	211298	20492	9673	18	30	0.948	0.927	--	0.926	0.574	0.555
													0.957

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	1716	2396	39	190773	19516	9213	(12+13)-I-1	7.35
I	Z	1716	1437	65	186533	19516	9213	(12+13)-I-1	11.1

Asta : 8000 [120 , 225]

Sez. G: HE 240 A L=169.7 cm Ln1=169.7 cm Ln2=169.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-1181	-2670	471	211298	20492	9673	17	28	0.953	0.934	--	0.839	0.493	0.504
													0.822

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	1181	2241	232	191763	19516	9213	8	6.84
I	Z	1181	1345	387	187890	19516	9213	8	8.53

Asta : 8000 [225 , 226]

Sez. G: HE 240 A L=158.4 cm Ln1=158.4 cm Ln2=158.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-598	-3429	293	211298	20492	9673	16	26	0.960	0.944	--	0.901	0.432	0.541
													0.720

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	598	3089	127	193207	19516	9213	9	5.71
I	Z	598	1853	211	189884	19516	9213	9	8.26

Asta : 8000 [226 , 227]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-596	-3846	101	211298	20492	9673	15	25	0.967	0.953	--	0.957	0.470	0.574
													0.783

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	596	3680	47	194582	19516	9213	9	5.08
I	Z	596	2208	79	191796	19516	9213	9	8.01

Asta : 8000 [227 , 228]

Sez. G: HE 240 A L=134.3 cm Ln1=134.3 cm Ln2=134.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-329	-3897	38	211298	20492	9673	13	22	0.976	0.965	--	1.000	0.343	0.600
													0.571

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	329	3897	13	196355	19516	9213	9	4.93
I	Z	329	2338	21	194282	19516	9213	9	8.08

Asta : 8000 [228 , 229]

Sez. G: HE 240 A L=122.5 cm Ln1=122.5 cm Ln2=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

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N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-40	-3263	-29	211298	20492	9673	12	20	0.984	0.977	--	0.932	0.526	0.559
Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	40	3042	15	197939	19516	9213	2					
1	Z	40	1825	26	196520	19516	9213	2					

Asia : 8000 [319 , 319]

Sez. G: HE 240 A L=113.1 cm L_{n1}=113.1 cm L_{n2}=113.1 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1092	3209	-38	211298	20492	9673	11	19	0.990	0.986	--	0.824	0.529	0.494

Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	1092	2643	20	199210	19516	9213	(12+13)÷III-4		6.99			
1	Z	1092	1586	33	198330	19516	9213	(12+13)÷III-4		11.1			

Asia : 8000 [319 , 320]

Sez. G: HE 240 A L=108.0 cm L_{n1}=108.0 cm L_{n2}=108.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1741	4210	-28	211298	20492	9673	11	18	0.993	0.991	--	0.905	0.376	0.543

Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	1741	3811	11	199913	19516	9213	(12+13)÷III-4		4.87			
1	Z	1741	2287	18	199335	19516	9213	(12+13)÷III-4		7.82			

Asia : 8000 [320 , 308]

Sez. G: HE 240 A L=112.3 cm L_{n1}=112.3 cm L_{n2}=112.3 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2350	5087	-32	211298	20492	9673	11	19	0.991	0.986	--	0.926	0.463	0.556

Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2350	4712	15	199340	19516	9213	(12+13)÷IV-4		3.92			
1	Z	2350	2827	25	198515	19516	9213	(12+13)÷IV-4		6.27			

Asia : 8001 [102 , 123]

Sez. G: HE 240 A L=181.6 cm L_{n1}=181.6 cm L_{n2}=181.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4587	4674	44	211298	20492	9673	18	30	0.945	0.923	--	0.719	0.549	0.431

Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	4587	3359	24	190236	19516	9213	2		5.03			
1	Z	4587	2016	40	185800	19516	9213	2		7.56			

Asia : 8001 [123 , 124]

Sez. G: HE 240 A L=177.6 cm L_{n1}=177.6 cm L_{n2}=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2069	2889	-92	211298	20492	9673	18	30	0.948	0.927	--	0.904	0.382	0.542

Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2069	2610	35	190740	19516	9213	(12+13)÷I-1		6.74			
1	Z	2069	1566	58	186488	19516	9213	(12+13)÷I-1		10.2			

Asia : 8001 [124 , 235]

Sez. G: HE 240 A L=169.8 cm L_{n1}=169.8 cm L_{n2}=169.8 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2922	-3020	476	211298	20492	9673	17	28	0.953	0.933	--	0.834	0.492	0.501

Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg	kg*m	kg	kg*m	kg*m						
1	Y	2922	2520	235	191735	19516	9213	8		5.89			
1	Z	2922	1512	391	187852	19516	9213	8		7.38			

Asia : 8001 [235 , 236]

Sez. G: HE 240 A L=158.5 cm L_{n1}=158.5 cm L_{n2}=158.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2215	-3872	287	211298	20492	9673	16	26	0.960	0.943	--	0.903	0.443	0.542

Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg	kg*m	kg	kg*m	kg*m						
1	Y	2215	3496	127	193184	19516	9213	9		4.89			
1	Z	2215	2097	212	189852	19516	9213	9		7.03			

Asia : 8001 [236 , 237]

Sez. G: HE 240 A L=147.9 cm L_{n1}=147.9 cm L_{n2}=147.9 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1587	-4173	98	211298	20492	9673	15	25	0.967	0.953	--	0.972	0.568	0.583

Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg	kg*m	kg	kg*m	kg*m						
1	Y	1587	4055	56	194564	19516	9213	9		4.50			
1	Z	1587	2433	93	191770	19516	9213	9		6.99			

Asia : 8001 [237 , 238]

Sez. G: HE 240 A L=134.4 cm L_{n1}=134.4 cm L_{n2}=134.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1168	-4173	76	211298	20492	9673	13	22	0.976	0.965	--	1.000	0.511	0.600

Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg	kg*m	kg	kg*m	kg*m						
1	Y	1168	4174	39	196355	19516	9213	9		4.46			
1	Z	1168	2505	65	194234	19516	9213	9		7.07			

Asia : 8001 [238 , 239]

Sez. G: HE 240 A L=122.6 cm L_{n1}=122.6 cm L_{n2}=122.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1141	-3991	125	211298	20492	9673	12	20	0.983	0.976	--	0.935	0.393	0.561

Cls	Dir	N	Mvseq	Mzeq	MzRd	MvRd	MzRd	Comb.					
		kg	kg	kg*m	kg	kg*m	kg*m						
1	Y	1141	3733	49	197911	19516	9213	9		4.94			
1	Z	1141	2240	82	196481	19516	9213	9		7.73			

Asia : 8001 [239 , 323]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-1032	-3343	187	211298	20492	9673	11	19	0.990	0.985	--	0.886	0.445
											0.532	0.742

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1032	2962	83	199175	19516	9213	9	6.02
	Z	1032	1777	139	198280	19516	9213	9	8.98

Asia : 8001 [323 , 324]

Sez. G: HE 240 A L=108.2 cm Ln1=108.2 cm Ln2=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-1260	4041	39	211298	20492	9673	11	18	0.993	0.990	--	0.943	0.310
											0.566	0.517

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1260	3811	12	199871	19516	9213	(12-13)-III-4	4.93
	Z	1260	2286	20	199274	19516	9213	(12-13)-III-4	7.96

Asia : 8001 [324 , 309]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-1669	4601	22	211298	20492	9673	11	19	0.990	0.986	--	0.952	0.404
											0.571	0.674

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1669	4378	9	199292	19516	9213	(12-13)-III-4	4.28
	Z	1669	2627	15	198447	19516	9213	(12-13)-III-4	6.91

Asia : 8002 [103 , 121]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-3943	4561	101	211298	20492	9673	18	30	0.945	0.924	--	0.730	0.465
											0.438	0.775

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3943	3329	47	190268	19516	9213	2	5.09
	Z	3943	1998	79	185843	19516	9213	2	7.57

Asia : 8002 [121 , 122]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-2021	2836	-63	211298	20492	9673	18	30	0.948	0.927	--	0.894	0.428
											0.536	0.713

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2021	2535	27	190767	19516	9213	(12-13)-I-1	6.97
	Z	2021	1521	45	186525	19516	9213	(12-13)-I-1	10.7

Asia : 8002 [122 , 230]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-2400	-2889	501	211298	20492	9673	17	28	0.953	0.934	--	0.832	0.489
											0.499	0.815

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2400	2403	245	191756	19516	9213	8	6.16
	Z	2400	1442	409	187881	19516	9213	8	7.63

Asia : 8002 [230 , 231]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-1742	-3748	314	211298	20492	9673	16	26	0.960	0.944	--	0.899	0.434
											0.539	0.723

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1742	3368	136	193200	19516	9213	9	5.09
	Z	1742	2021	227	189873	19516	9213	9	7.28

Asia : 8002 [231 , 232]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-1266	-4163	93	211298	20492	9673	15	25	0.967	0.953	--	0.961	0.597
											0.576	0.996

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1266	3999	56	194574	19516	9213	9	4.60
	Z	1266	2400	93	191785	19516	9213	9	7.16

Asia : 8002 [232 , 233]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-863	-4179	70	211298	20492	9673	13	22	0.976	0.965	--	1.000	0.520
											0.600	0.867

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	863	4179	36	196346	19516	9213	9	4.50
	Z	863	2507	61	194269	19516	9213	9	7.17

Asia : 8002 [233 , 234]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-584	-4087	125	211298	20492	9673	12	20	0.984	0.976	--	0.949	0.385
											0.569	0.641

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	584	3877	48	197929	19516	9213	9	4.83
	Z	584	2326	80	196506	19516	9213	9	7.64

Asia : 8002 [234 , 321]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-477	-3560	181	211298	20492	9673	11	19	0.990	0.985	--	0.895	0.450
											0.537	0.751

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	477	3187	82	199199	19516	9213	9	5.73
1	Z	477	1912	136	198315	19516	9213	9	8.68

Asta : 8002 [321 , 322]

Sez. G: HE 240 A L=108,1 cm Ln1=108,1 cm Ln2=108,1 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	18	0.993	0.990	--	0.924	0.316	0.554
-1378	4109	30	211298	20492	9673								0.526

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1378	3796	9	199902	19516	9213	(12+13)-III-4	4.94
1	Z	1378	2278	16	199319	19516	9213	(12+13)-III-4	7.98

Asta : 8002 [322 , 310]

Sez. G: HE 240 A L=112,4 cm Ln1=112,4 cm Ln2=112,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	19	0.991	0.986	--	0.953	0.240	0.572
-1820	4656	1	211298	20492	9673								0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1820	4439	0	199329	19516	9213	(12+13)-III-4	4.23
1	Z	1820	2663	0	198500	19516	9213	(12+13)-III-4	6.86

Asta : 8003 [104 , 115]

Sez. G: HE 240 A L=181,6 cm Ln1=181,6 cm Ln2=181,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.945	0.923	--	0.730	0.441	0.438
-3896	4655	152	211298	20492	9673								0.735

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3896	3400	67	190236	19516	9213	2	4.95
1	Z	3896	2040	112	185800	19516	9213	2	7.27

Asta : 8003 [115 , 116]

Sez. G: HE 240 A L=177,6 cm Ln1=177,6 cm Ln2=177,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.948	0.927	--	0.601	0.360	0.361
-2193	2746	65	211298	20492	9673								0.601

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2193	1650	24	190741	19516	9213	(12+13)-V-1	10.1
1	Z	2193	990	39	186489	19516	9213	(12+13)-V-1	15.0

Asta : 8003 [116 , 215]

Sez. G: HE 240 A L=169,8 cm Ln1=169,8 cm Ln2=169,8 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	17	28	0.953	0.933	--	0.601	0.360	0.361
-2257	-2921	483	211298	20492	9673								0.600

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2257	1755	174	191736	19516	9213	8	8.29
1	Z	2257	1053	290	187853	19516	9213	8	10.3

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Asta : 8003 [215 , 216]

Sez. G: HE 240 A L=158,5 cm Ln1=158,5 cm Ln2=158,5 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	16	26	0.960	0.943	--	0.900	0.427	0.540
-1629	-3771	310	211298	20492	9673								0.712

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1629	3394	132	193184	19516	9213	9	5.08
1	Z	1629	2036	221	189853	19516	9213	9	7.31

Asta : 8003 [216 , 217]

Sez. G: HE 240 A L=147,9 cm Ln1=147,9 cm Ln2=147,9 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	15	25	0.967	0.953	--	0.963	0.586	0.578
-1506	-4161	90	211298	20492	9673								0.977

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1506	4008	53	194564	19516	9213	9	4.57
1	Z	1506	2405	88	191771	19516	9213	9	7.11

Asta : 8003 [217 , 218]

Sez. G: HE 240 A L=134,4 cm Ln1=134,4 cm Ln2=134,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	13	22	0.976	0.965	--	1.000	0.506	0.600
-1099	-4177	72	211298	20492	9673								0.844

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1099	4178	37	196336	19516	9213	9	4.47
1	Z	1099	2507	61	194255	19516	9213	9	7.11

Asta : 8003 [218 , 219]

Sez. G: HE 240 A L=122,6 cm Ln1=122,6 cm Ln2=122,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	12	20	0.983	0.976	--	0.948	0.383	0.569
-757	-4091	143	211298	20492	9673								0.639

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	757	3878	55	197912	19516	9213	9	4.80
1	Z	757	2327	91	196482	19516	9213	9	7.52

Asta : 8003 [219 , 315]

Sez. G: HE 240 A L=113,3 cm Ln1=113,3 cm Ln2=113,3 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	19	0.990	0.985	--	0.897	0.459	0.538
-646	-3557	196	211298	20492	9673								0.765

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	646	3192	90	199176	19516	9213	9	5.66
1	Z	646	1915	150	198281	19516	9213	9	8.50

Asta : 8003 [315 , 316]

Sez. G: HE 240 A L=108,1 cm Ln1=108,1 cm Ln2=108,1 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

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-1737	N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg*m	kg	kg*m	kg*m								
	4156	25	211298	20492	9673	11	18	0.993	0.990	--		0.942	0.557	0.565
														0.928
Clis	Dir	N		Mvseq		NRd		MyRd		MzRd		Comb.		SF
		kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m			
1	Y	1737	3915	14	199871	19516	9213						(12+13)-VII-4	4.74
1	Z	1737	2349	23	199276	19516	9213						(12+13)-VII-4	7.60

Asia : 8003 [316, 311]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	N		Mz		NRk		MvRk		MzRk		λY		λZ		χY		χZ		χLT		kyy		kyz		kzz	
		kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m
-1997		4637	3	211298	20492	9673	11	19	0.990	0.986	--																

Clis	Dir	N		Mvseq		NRd		MvRd		MzRd		λY		λZ		χY		χZ		χLT		Comb.		SF	
		kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m				
1	Y	1997	4449	1	199293	19516	9213																		4.20
1	Z	1997	2669	2	198449	19516	9213																		6.80

Asia : 8004 [105, 125]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	N		Mz		NRk		MvRk		MzRk		λY		λZ		χY		χZ		χLT		kyy		kyz		kzz	
		kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m
-4700		4516	202	211298	20492	9673	18	30	0.946	0.924	--																

Clis	Dir	N		Mvseq		NRd		MvRd		MzRd		λY		λZ		χY		χZ		χLT		Comb.		SF	
		kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m				
1	Y	4700	2720	73	190274	19516	9213																		5.82
1	Z	4700	1632	121	185851	19516	9213																		8.19

Asia : 8004 [125, 126]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	N		Mz		NRk		MyRk		MzRk		λY		λZ		χY		χZ		χLT		kyy		kyz		kzz	
		kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m
-1727		2879	123	211298	20492	9673	18	30	0.948	0.927	--																

Clis	Dir	N		Mvseq		NRd		MvRd		MzRd		λY		λZ		χY		χZ		χLT		Comb.		SF	
		kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m				
1	Y	1727	2523	53	190775	19516	9213																		6.94
1	Z	1727	1514	89	186536	19516	9213																		10.4

Asia : 8004 [126, 240]

Sez. G: HE 240 A L=169.7 cm Ln1=169.7 cm Ln2=169.7 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	N		Mz		NRk		MvRk		MzRk		λY		λZ		χY		χZ		χLT		kyy		kyz		kzz	
		kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-3061		-3049	515	211298	20492	9673	17	28	0.953	0.934	--																

Clis	Dir	N		Mvseq		NRd		MvRd		MzRd		λY		λZ		χY		χZ		χLT		Comb.		SF	
		kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m				
1	Y	3061	2543	248	191768	19516	9213																		5.77
1	Z	3061	1526	414	187897	19516	9213																		7.17

Asia : 8004 [240, 241]

Sez. G: HE 240 A L=158.4 cm Ln1=158.4 cm Ln2=158.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	N		Mz		NRk		MyRk		MzRk		λY		λZ		χY		χZ		χLT		kyy		kyz		kzz	
		kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-2335		-3908	317	211298	20492	9673	16	26	0.960	0.944	--																

Clis	Dir	N		Mveq		NRd		MvRd		MzRd		λY		λZ		χY		χZ		χLT		Comb.		SF	
		kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m				
1	Y	2335	3529	131	193215	19516	9213																		4.83
1	Z	2335	2117	219	189894	19516	9213																		6.92

Asia : 8004 [241, 242]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	N		Mz		NRk		MvRk		MzRk		λY		λZ		χY		χZ		χLT		kyy		kyz		kzz	
		kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m	kg	kg·m
-1748		-4243	83	211298	20492	9673	15	25	0.967	0.953	--																

Clis	Dir	N		Mveq		NRd		MvRd		MzRd		λY		λZ		χY		χZ		χLT		Comb.		SF	
		kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m				
1	Y	1748	4112	49	194593	19516	9213																		4.44
1	Z	1748	2467	82	191811	19516	9213																		6.92

Asia : 8004 [242, 243]

Sez. G: HE 240 A L=134.3 cm Ln1=134.3 cm Ln2=134.3 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq

Asia : 8004 [326 , 312]

Sez. G: HE 240 A L=112,3 cm Ln1=112,3 cm Ln2=112,3 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1647	4774	-17	211298	20492	9673	11	19	0,990	0,986	--	0,959	0,368	0,575 0,614

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1647	4577	6	199310	19516	9213	(12+13)>VII-4	4,11
1	Z	1647	2746	10	198472	19516	9213	(12+13)>VII-4	6,66

Asia : 8005 [106 , 127]

Sez. G: HE 240 A L=181,6 cm Ln1=181,6 cm Ln2=181,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4974	4951	201	211298	20492	9673	18	30	0,945	0,923	--	0,706	0,377	0,424 0,628

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4974	3495	76	190266	19516	9213	2	4,69
1	Z	4974	2097	126	185841	19516	9213	2	6,76

Asia : 8005 [127 , 128]

Sez. G: HE 240 A L=177,6 cm Ln1=177,6 cm Ln2=177,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2341	-3105	-72	211298	20492	9673	18	30	0,948	0,927	--	0,601	0,360	0,361 0,601

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2341	1866	26	190768	19516	9213	(12+13)>VII-4	9,03
1	Z	2341	1120	43	186526	19516	9213	(12+13)>VII-4	13,4

Asia : 8005 [128 , 245]

Sez. G: HE 240 A L=169,8 cm Ln1=169,8 cm Ln2=169,8 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3272	-3173	484	211298	20492	9673	17	28	0,953	0,934	--	0,855	0,484	0,513 0,806

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3272	2713	234	191760	19516	9213	8	5,51
1	Z	3272	1628	390	187886	19516	9213	8	6,99

Asia : 8005 [245 , 246]

Sez. G: HE 240 A L=158,5 cm Ln1=158,5 cm Ln2=158,5 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2493	-3845	281	211298	20492	9673	16	26	0,960	0,944	--	0,921	0,415	0,552 0,691

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2493	3540	117	193206	19516	9213	9	4,83
1	Z	2493	2124	194	189883	19516	9213	9	6,99

Asia : 8005 [246 , 247]

Sez. G: HE 240 A L=147,9 cm Ln1=147,9 cm Ln2=147,9 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1583	5111	-24	211298	20492	9673	11	19	0,990	0,986	--	0,883	0,282	0,530 0,469

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2545	-4045	90	211298	20492	9673	15	25	0,967	0,953	--	1,001	0,517	0,601 0,862

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2545	4050	47	194583	19516	9213	9	4,43
1	Z	2545	2430	78	191798	19516	9213	9	6,84

Asia : 8005 [247 , 248]

Sez. G: HE 240 A L=134,4 cm Ln1=134,4 cm Ln2=134,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2067	-4044	57	211298	20492	9673	13	22	0,976	0,965	--	0,980	0,564	0,588 0,940

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2067	3963	32	196352	19516	9213	9	4,61
1	Z	2067	2378	54	194277	19516	9213	9	7,23

Asia : 8005 [248 , 249]

Sez. G: HE 240 A L=122,6 cm Ln1=122,6 cm Ln2=122,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1422	-3833	149	211298	20492	9673	12	20	0,984	0,976	--	0,943	0,365	0,566 0,608

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1422	3616	54	197925	19516	9213	9	5,04
1	Z	1422	2170	91	196501	19516	9213	9	7,80

Asia : 8005 [249 , 327]

Sez. G: HE 240 A L=113,3 cm Ln1=113,3 cm Ln2=113,3 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3014	3802	56	211298	20492	9673	11	19	0,990	0,985	--	0,872	0,433	0,523 0,722

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3014	3315	24	199186	19516	9213	(12+13)>VII-4	5,33
1	Z	3014	1989	40	198295	19516	9213	(12+13)>VII-4	8,23

Asia : 8005 [327 , 328]

Sez. G: HE 240 A L=108,1 cm Ln1=108,1 cm Ln2=108,1 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1863	4319	-38	211298	20492	9673	11	18	0,993	0,990	--	0,953	0,289	0,572 0,481

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1863	4114	11	199878	19516	9213	(12+13)>VII-4	4,52
1	Z	1863	2468	18	199285	19516	9213	(12+13)>VII-4	7,26

Asia : 8005 [328 , 313]

Sez. G: HE 240 A L=112,4 cm Ln1=112,4 cm Ln2=112,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1583	5111	-24	211298	20492	9673	11	19	0,990	0,986	--	0,883	0,282	0,530 0,469

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1583	4511	7	199297	19516	9213	(12+13)>III-3	4.17
1	Z	1583	2707	11	198454	19516	9213	(12+13)>III-3	6.76

Asia : 8006 [107 , 117]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m			
-2678	4697	160	211298	20492	9673	18	30	0.945	0.923	--	0.811	0.304	0.487
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF				
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2678	3810	49	190236	19516	9213	(12+13)>VIII-1	4.66				
1	Z	2678	2286	81	185800	19516	9213	(12+13)>VIII-1	7.12				

Asia : 8006 [117 , 118]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m			
-2023	2989	97	211298	20492	9673	18	30	0.948	0.927	--	0.875	0.403	0.525

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2023	2616	39	190741	19516	9213	(12+13)>VII-1	6.72
1	Z	2023	1570	65	186489	19516	9213	(12+13)>VII-1	10.2

Asia : 8006 [118 , 220]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m			
-1519	-2754	434	211298	20492	9673	17	28	0.953	0.933	--	0.829	0.485	0.498

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1519	2285	211	191736	19516	9213	8	6.76
1	Z	1519	1371	351	187853	19516	9213	8	8.59

Asia : 8006 [220 , 221]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m			
-982	-3631	230	211298	20492	9673	16	26	0.960	0.943	--	0.893	0.408	0.536

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	982	3243	94	193185	19516	9213	9	5.51
1	Z	982	1946	156	189853	19516	9213	9	8.21

Asia : 8006 [221 , 222]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m			
-218	-4062	73	211298	20492	9673	15	25	0.967	0.953	--	0.938	0.463	0.575

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	218	3890	34	194565	19516	9213	9	4.90
1	Z	218	2334	57	191772	19516	9213	9	7.88

Asia : 8006 [222 , 223]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m			
-5	-3689	44	211298	20492	9673	13	22	0.976	0.965	--	0.976	0.412	0.586

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5	3600	18	196336	19516	9213	8	5.36
1	Z	5	2160	30	194255	19516	9213	8	8.78

Asia : 8006 [223 , 224]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m			
-64	-3467	88	211298	20492	9673	12	20	0.983	0.976	--	0.919	0.290	0.551

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	64	3187	26	197912	19516	9213	8	6.01
1	Z	64	1912	43	196483	19516	9213	8	9.72

Asia : 8006 [224 , 317]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m			
-795	3520	-35	211298	20492	9673	11	19	0.990	0.985	--	0.774	0.270	0.464

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	795	2723	9	199176	19516	9213	(12+13)>VII-3	6.92
1	Z	795	1634	16	198282	19516	9213	(12+13)>VII-3	11.2

Asia : 8006 [317 , 318]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m			
-1955	4761	-35	211298	20492	9673	11	18	0.993	0.990	--	0.896	0.329	0.538

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1955	4265	11	199872	19516	9213	(12+13)>VII-3	4.36
1	Z	1955	2559	19	199276	19516	9213	(12+13)>VII-3	6.99

Asia : 8006 [318 , 314]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg*m			
-2423	5452	10	211298	20492	9673	11	19	0.990	0.986	--	0.949	0.404	0.570

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2423	5175	4	199294	19516	9213	(12+13)>V-3	3.60
1	Z	2423	3105	7	198449	19516	9213	(12+13)>V-3	5.81

Verifica Resistenza aste Metalliche

Scenario di calcolo : **Set_NT_SILV_A2_STR/GEO**

Asta : 1 [1 , 19]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
		kg	kg	kg	kg	kg	kg		
0	1	-13768	-552	-1345	1	3135	-1158	--	--
(12+13)+IV-2									

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
0	1	201236	87004	38027	19516	9213	462	28.3	2.82	>100	2.82

Asta : 1 [19 , 20]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
		kg	kg	kg	kg*	kg*	kg*		
136	1	-5230	64	-624	-1	-2451	584	---	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
136	1	201236	87017	38033	19516	9213	462	61.0	4.65	>100	4.65

Asta : 1 [20 , 101]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
	cm	kg	kg	kg	kg*m	kg*m	kg*m			
135	1	-5620	66	-1292	0	-4187	-42	--		(12+13)+VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
135	1	201236	87081	38061	19516	9213	462	29.5	4.05	>100	4.05

Asta : 2 [2 , 15]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
em		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-9409	408	-1094	-1	2933	863	--		(12+13)+IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
0	1	201236	87046	38046	19516	9213	462	34.8	3.44	>100	3.44

Asta : 2 [15 , 16]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
em		kg	kg	kg	kg ^{*m}	kg ^{*m}	kg ^{*m}		
136	1	-3713	-3	-1197	-0	-3113	419	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
136	1	201236	87079	38060	19516	9213	462	31.8	4.48	>100	4.48

Asta : 2 [16 , 102]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
	cm	kg	kg	kg	kg ² m	kg ³ m	kg ³ m		
135	1	-4419	341	-1078	2	-4666	-45	--	--
									2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
135	1	201236	86975	38015	19516	9213	462	35.3	3.76	>100	3.76

Asta : 3 [3 , 17]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
		kg	kg	kg	kg	kg	kg		
0	1	-3074	-317	-1353	-0	3906	-680	--	--
(12+13)+III-2									

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
0	1	201236	87087	38064	19516	9213	462	28.1	3.46	>100	3.46

Asta : 3 [17 , 18]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
	cm	kg	kg	kg	kg*m	kg*m	kg*m			
136	1	-3953	51	-799	0	-2729	587	---	---	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
136	1	201236	87087	38064	19516	9213	462	47.6	4.48	>100	4.48

Asta : 3 [18 , 103]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
	cm	kg	kg	kg	kg ^{*m}	kg ^{*m}	kg ^{*m}			
135	1	-4678	293	-1052	1	-4572	-28	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
135	1	201236	87008	38029	19516	9213	462	36.2	3.84	>100	3.84

Asta : 4 [4 , 25]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
		kg	kg	kg	kg	kg	kg		
0	1	-7844	-295	-1368	-1	3955	-627	--	--
									(12+13)+III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
0	1	201236	87054	38049	19516	9213	462	27.8	3.23	>100	3.23

Asta : 4 [25 , 26]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
		kg	kg	kg	kg	kg	kg		
136	1	-4887	49	-810	-0	-2742	581	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
		kg	kg	kg	kg	kg	kg				
136	1	201236	87090	38065	19516	9213	462	47.0	4.39	>100	4.39

Asta : 4 [26 , 104]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg		
135	1	-4933	274	-1078	2	-4647	-28	--	--

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
135	1	201236	86925	37993	19516	9213	462	35.2	3.76	>100	3.76

Asta : 5 [5 , 21]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-11387	499	-1203	-1	3146	1054	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87032	38040	19516	9213	462	31.6	3.01	>100	3.01

Asta : 5 [21 , 22]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
136	1	-3352	53	-875	1	-2858	570	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
136	1	201236	87028	38038	19516	9213	462	43.5	4.45	>100	4.45

Asta : 5 [22 , 105]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
135	1	-4748	238	-1146	2	-4883	-15	--	--	2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
135	1	201236	86923	37992	19516	9213	462	33.2	3.63	>100	3.63

Asta : 6 [6 , 23]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	4433	490	-1282	-1	3367	1026	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87057	38051	19516	9213	462	29.7	3.27	>100	3.27

Asta : 6 [23 , 24]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
136	1	-5101	32	-864	0	-2892	587	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
136	1	201236	87066	38055	19516	9213	462	44.0	4.21	>100	4.21

Asta : 6 [24 , 106]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
135	1	-5667	224	-1153	1	-4966	28	--	--	2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
135	1	201236	87040	38043	19516	9213	462	33.0	3.50	>100	3.50

Asta : 7 [7 , 27]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-12300	469	-1620	-1	4000	980	--	--	(12+13)+III-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87030	38039	19516	9213	462	23.5	2.68	>100	2.68

Asta : 7 [27 , 28]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
136	1	-2811	17	-629	1	-2492	601	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
136	1	201236	87000	38026	19516	9213	462	60.4	4.83	>100	4.83

Asta : 7 [28 , 107]

Sez. G: HE 240 A L=135.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
135	1	-5339	-68	-1551	-2	-4692	62	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
135	1	201236	86983	38018	19516	9213	462	24.5	3.65	>100	3.65

Asta : 101 [119 , 123]

Sez. G: IPE 100 L=149.8 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-68	-1	27	-0	-49	36	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9476	7685	1033	240	27	>100	5.01	>100	5.01

Asta : 101 [123 , 121]

Sez. G: IPE 100 L=95.0 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
76	1	-188	-3	52	0	-13	31	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
76	1	27037	9476	7685	1033	240	27	>100	6.76	>100	6.76

Asta : 101 [121 , 115]

Sez. G: IPE 100 L=96.0 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-73	-108	-49	-0	0	-37	--	--	(12+13)÷VIII+2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9477	7686	1033	240	27	87.4	6.44	>100	6.44

Asta : 101 [115 , 125]

Sez. G: IPE 100 L=94.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
76	1	-221	-5	52	0	-13	32	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
76	1	27037	9480	7689	1033	240	27	>100	6.50	>100	6.50

Asta : 101 [125 , 127]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-144	-10	-0	-0	-64	32	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	27037	9479	7688	1033	240	27	>100	4.98	>100	4.98

Asta : 101 [127 , 117]

Sez. G: IPE 100 L=149.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-70	0	27	0	-49	36	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9476	7685	1033	240	27	>100	4.96	>100	4.96

Asta : 102 [120 , 124]

Sez. G: IPE 100 L=149.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	-77	-6	26	-0	-47	36	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9476	7685	1033	240	27	>100	5.05	>100	5.05

Asta : 102 [124 , 126]

Sez. G: IPE 100 L=101.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
81	1	-176	-11	53	0	-14	35	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
81	1	27037	9473	7683	1033	240	27	>100	6.04	>100	6.04

Asta : 102 [122 , 116]

Sez. G: IPE 100 L=101.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
82	1	-28	-5	54	0	-15	34	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
82	1	27037	9475	7684	1033	240	27	>100	6.38	>100	6.38

Asta : 102 [116 , 126]

Sez. G: IPE 100 L=100.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
81	1	30	-12	54	0	-14	35	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
81	1	27037	9476	7685	1033	240	27	>100	6.13	>100	6.13

Asta : 102 [126 , 128]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	98	-0	26	0	-47	35	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9480	7688	1033	240	27	>100	5.07	>100	5.07

Asta : 102 [128 , 118]

Sez. G: IPE 100 L=149.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	56	-8	26	0	-47	37	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9478	7687	1033	240	27	>100	4.95	>100	4.95

Asta : 103 [225 , 235]

Sez. G: IPE 100 L=149.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
90	1	7	0	25	-0	-45	34	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9479	7687	1033	240	27	>100	5.41	>100	5.41

Asta : 103 [235 , 230]

Sez. G: IPE 100 L=107.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	3	-10	36	0	-20	30	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	27037	9473	7682	1033	240	27	>100	6.89	>100	6.89

Asta : 103 [230 , 215]

Sez. G: IPE 100 L=107.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	7	-7	36	0	-20	30	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	27037	9473	7683	1033	240	27	>100	6.94	>100	6.94

Asta : 103 [215, 240]

Sez. G: IPE 100 L=107,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	10	-10	36	0	-20	30	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	27037	9474	7683	1033	240	27	>100	6.84	>100	6.84

Asta : 103 [240, 245]

Sez. G: IPE 100 L=149, 5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	13	5	25	0	-45	33	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	27037	9479	7687	1033	240	27	>100	5.46	>100	5.46

Asta : 103 [245, 220]

Sez. G: IPE 100 L=149, 7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	9	1	25	0	-45	34	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	27037	9481	7689	1033	240	27	>100	5.37	>100	5.37

Asta : 104 [226, 236]

Sez. G: IPE 100 L=149, 6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	45	0	-0	-44	31	--	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	27037	9481	7689	1033	240	27	>100	5.77	>100	5.77

Asta : 104 [236, 231]

Sez. G: IPE 100 L=113, 3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
57	1	201	2	-0	0	-25	25	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
57	1	27037	9475	7684	1033	240	27	>100	7.40	>100	7.40

Asta : 104 [231, 216]

Sez. G: IPE 100 L=113, 7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
57	1	64	3	-0	0	-25	25	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
57	1	27037	9474	7683	1033	240	27	>100	7.67	>100	7.67

Asta : 104 [216, 241]

Sez. G: IPE 100 L=113 0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
57	1	-114	1	0	0	-25	25	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
57	1	27037	9474	7683	1033	240	27	>100	7.58	>100	7.58

Asta : 104 [241, 246]

Sez. G: IPE 100 L=149 6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	-170	5	-0	0	-44	31	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	27037	9479	7687	1033	240	27	>100	5.62	>100	5.62

Asta : 104 [246, 221]

Sez. G: IPE 100 L=149 7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	-145	3	0	-0	-44	31	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	27037	9479	7687	1033	240	27	>100	5.64	>100	5.64

Asta : 105 [227, 237]

Sez. G: IPE 100 L=119 6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
60	1	-7	1	-22	0	-39	32	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
60	1	27037	9479	7687	1033	240	27	>100	5.86	>100	5.86

Asta : 105 [237, 232]

Sez. G: IPE 100 L=119 3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
36	1	-20	2	-35	0	-22	30	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
36	1	27037	9477	7686	1033	240	27	>100	6.85	>100	6.85

Asta : 105 [232, 217]

Sez. G: IPE 100 L=119 5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
36	1	-39	3	-35	0	-22	30	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
36	1	27037	9475	7684	1033	240	27	>100	6.76	>100	6.76

Asta : 105 [217, 242]

Sez. G: IPE 100 L=119 1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
36	1	-67	2	-35	0	-22	30	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
36	1	27037	9474	7683	1033	240	27	>100	6.77	>100	6.77

Asta : 105 [242, 247]

Sez. G: IPE 100 L=149,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	-73	7	-22	0	-39	33	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9480	7688	1033	240	27	>100	5.68	>100	5.68

Asta : 105 [247, 222]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	-54	5	-22	-0	-39	32	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9478	7687	1033	240	27	>100	5.74	>100	5.74

Asta : 106 [228, 238]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	-158	12	-20	0	-35	33	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9477	7686	1033	240	27	>100	5.68	>100	5.68

Asta : 106 [238, 233]

Sez. G: IPE 100 L=125,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
38	1	-86	9	-33	0	-22	32	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
38	1	27037	9479	7687	1033	240	27	>100	6.39	>100	6.39

Asta : 106 [233, 218]

Sez. G: IPE 100 L=125,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
38	1	-163	13	-33	0	-22	33	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
38	1	27037	9477	7686	1033	240	27	>100	6.11	>100	6.11

Asta : 106 [218, 243]

Sez. G: IPE 100 L=125,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
38	1	-283	13	-33	0	-22	33	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
38	1	27037	9476	7685	1033	240	27	>100	5.92	>100	5.92

Asta : 106 [243, 248]

Sez. G: IPE 100 L=149,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
150	1	-303	94	57	0	0	-42	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
150	1	27037	9475	7684	1033	240	27	>100	5.38	>100	5.38

Asta : 106 [248, 223]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	-219	15	-20	-0	-36	32	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9479	7687	1033	240	27	>100	5.63	>100	5.63

Asta : 107 [229, 239]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	-46	1	-37	0	-29	34	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	27037	9477	7686	1033	240	27	>100	5.83	>100	5.83

Asta : 107 [239, 234]

Sez. G: IPE 100 L=131,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-75	-90	-45	0	0	-40	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9479	7687	1033	240	27	>100	5.82	>100	5.82

Asta : 107 [234, 219]

Sez. G: IPE 100 L=131,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
39	1	-75	16	-32	0	-22	34	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
39	1	27037	9478	7687	1033	240	27	>100	6.04	>100	6.04

Asta : 107 [219, 244]

Sez. G: IPE 100 L=131,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
26	1	-73	3	-48	0	-17	36	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
26	1	27037	9477	7686	1033	240	27	>100	5.88	>100	5.88

Asta : 107 [244, 249]

Sez. G: IPE 100 L=149,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
150	1	-105	102	52	0	0	-51	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
150	1	27037	9479	7687	1033	240	27	92.7	4.65	>100	4.65

Asta : 107 [249., 224]

Sez. G: IPE 100 L=149.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	-36	6	-37	-0	-29	35	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	27037	9480	7688	1033	240	27	>100	5.76	>100	5.76

Asta : 108 [319., 323]

Sez. G: IPE 100 L=149.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1088	-80	-48	0	0	-36	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9472	7682	1033	240	27	>100	5.21	>100	5.21

Asta : 108 [323., 321]

Sez. G: IPE 100 L=137.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1517	-116	-44	0	0	-59	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9477	7686	1033	240	27	81.9	3.29	>100	3.29

Asta : 108 [321., 315]

Sez. G: IPE 100 L=137.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
137	1	-450	115	45	0	0	-58	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
137	1	27037	9479	7687	1033	240	27	82.4	3.84	>100	3.84

Asta : 108 [315., 325]

Sez. G: IPE 100 L=137.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
27	1	-249	4	-48	0	-17	37	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
27	1	27037	9479	7687	1033	240	27	>100	5.52	>100	5.52

Asta : 108 [325., 327]

Sez. G: IPE 100 L=149.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
150	1	-1237	122	49	-0	0	-67	--	--	(12+13)+VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
150	1	27037	9475	7684	1033	240	27	77.4	3.09	>100	3.09

Asta : 108 [327., 317]

Sez. G: IPE 100 L=149.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1174	-80	-49	0	0	-35	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9474	7683	1033	240	27	>100	5.28	>100	5.28

Asta : 109 [320., 324]

Sez. G: IPE 100 L=149.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
60	1	-28	6	-17	0	-31	30	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9481	7689	1033	240	27	>100	6.47	>100	6.47

Asta : 109 [324., 322]

Sez. G: IPE 100 L=143.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
57	1	-56	0	-17	0	-28	27	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9479	7688	1033	240	27	>100	6.94	>100	6.94

Asta : 109 [322., 316]

Sez. G: IPE 100 L=143.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
57	1	-61	5	-16	0	-28	28	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9480	7688	1033	240	27	>100	6.78	>100	6.78

Asta : 109 [316., 326]

Sez. G: IPE 100 L=143.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
57	1	-51	8	-16	0	-28	29	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9481	7689	1033	240	27	>100	6.68	>100	6.68

Asta : 109 [326., 328]

Sez. G: IPE 100 L=149.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
60	1	-34	5	-17	-0	-31	29	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9480	7688	1033	240	27	>100	6.51	>100	6.51

Asia : 109 [328 , 318]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
60	1	-22	3	-17	-0	-31	29	--	--	9		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
60	1	27037	9480	7689	1033	240	27	>100	6.64	>100	6.64

Asia : 110 [101 , 102]

Sez. G: IPE 100 L=149,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
150	1	-238	-31	95	-0	0	39	--	--	9		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
150	1	27037	9479	7688	1033	240	27	81.2	5.80	>100	5.80

Asia : 110 [102 , 103]

Sez. G: IPE 100 L=89,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
89	1	-486	-54	56	0	0	41	--	--	8		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9481	7689	1033	240	27	>100	5.30	>100	5.30

Asia : 110 [103 , 104]

Sez. G: IPE 100 L=90,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
90	1	-22	-54	59	-0	0	41	--	--	8		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	27037	9480	7688	1033	240	27	>100	5.79	>100	5.79

Asia : 110 [104 , 105]

Sez. G: IPE 100 L=88,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
89	1	200	-77	60	-0	0	51	--	--	8		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9479	7687	1033	240	27	>100	4.51	>100	4.51

Asia : 110 [105 , 106]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
135	1	259	-19	81	-0	-14	28	--	--	8		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
135	1	27037	9479	7688	1033	240	27	94.8	7.17	>100	7.17

Asia : 110 [106 , 107]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
135	1	176	-20	81	0	-14	28	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
135	1	27037	9478	7687	1033	240	27	94.7	7.22	>100	7.22

Asia : 208 [208 , 308]

Sez. G: HE 240 A L=372,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4860	-304	2825	-1	-5431	-1102	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*				
0	1	201236	87048	38046	19516	9213	462	13.5	2.37	>100	2.37

Asia : 209 [209 , 309]

Sez. G: HE 240 A L=372,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*			
0	1	788	-314	2510	-1	-4678	-1135	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*				
0	1	201236	87052	38049	19516	9213	462	15.2	2.73	>100	2.73

Asia : 210 [210 , 310]

Sez. G: HE 240 A L=372,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1752	-327	2075	-0	-3964	-1204	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*				
0	1	201236	87062	38053	19516	9213	462	18.3	2.92	>100	2.92

Asia : 211 [211 , 311]

Sez. G: HE 240 A L=372,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1755	218	2510	0	-5102	799	--	--	(12+13)-I-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*				
0	1	201236	87072	38057	19516	9213	462	15.2	2.80	>100	2.80

Asia : 212 [212 , 312]

Sez. G: HE 240 A L=372,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1519	208	2590	1	-5296	756	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*				
0	1	201236	87050	38047	19516	9213	462	14.7	2.77	>100	2.77

Asia : 213 [213 , 313]

Sez. G: HE 240 A L=372,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

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: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	41	202	3008	1	-6255	730	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	201236	87051	38048	19516	9213	462	12.6	2.50	>100	2.50

Asta : 214 [214 , 314]

Sez. G: HE 240 A L=372,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3594	198	3263	1	-4697	711	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	201236	87050	38047	19516	9213	462	11.7	2.28	>100	2.28

Asta : 301 [308 , 309]

Sez. G: IPE 100 L=149,3 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
149	1	1865	19	39	-0	0	-15	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
149	1	27037	9476	7685	1033	240	27	>100	7.66	>100	7.66

Asta : 301 [309 , 310]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
105	1	2800	4	15	0	-12	-2	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
105	1	27037	9477	7686	1033	240	27	>100	8.16	>100	8.16

Asta : 301 [310 , 311]

Sez. G: IPE 100 L=149,0 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
45	1	490	7	-26	-0	-20	19	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
45	1	27037	9480	7688	1033	240	27	>100	8.65	>100	8.65

Asta : 301 [311 , 312]

Sez. G: IPE 100 L=149,4 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
30	1	681	8	-39	-0	-16	20	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
30	1	27037	9480	7688	1033	240	27	>100	8.09	>100	8.09

Asta : 301 [312 , 313]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
45	1	822	7	-26	-0	-21	18	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
45	1	27037	9480	7688	1033	240	27	>100	7.90	>100	7.90

Asta : 301 [313 , 314]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1905	-17	-39	0	0	-13	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	27037	9477	7685	1033	240	27	>100	8.11	>100	8.11

Asta : 7001 [1 , 15]

Sez. G: IPE 100 L=202,0 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2662	--	--	--	--	--	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	5266	--	--	--	--	--	>100	1.98	>100	1.98

Asta : 7002 [15 , 20]

Sez. G: Fil16 L=202,0 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
202	1	2914	--	--	--	--	--	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
202	1	5266	--	--	--	--	--	>100	1.81	>100	1.81

Asta : 7003 [20 , 102]

Sez. G: Fil16 L=202,0 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2575	--	--	--	--	--	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	5266	--	--	--	--	--	>100	2.04	>100	2.04

Asta : 7004 [102 , 120]

Sez. G: Fil16 L=389,5 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
390	1	1648	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
390	1	5266	--	--	--	--	--	>100	3.19	>100	3.19

Asta : 7005 [120 , 236]

Sez. G: Fil16 L=360,4 cm Crit.: Acciaio_Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm²/cmq ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1143	--	--	--	--	--	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	4.61	>100	4.61
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7006 [236 , 228]

Sez. G: F116 L=319,1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
319	1	774	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	6.80	>100	6.80
319	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7007 [228 , 323]

Sez. G: F116 L=278,4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-2	
278	1	1588	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.32	>100	3.32
278	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7008 [323 , 308]

Sez. G: F116 L=263,5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-I-4	
264	1	-1006	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	5.24	>100	5.24
264	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7009 [308 , 209]

Sez. G: F116 L=400,8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
401	1	-4137	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.27	>100	1.27
401	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7010 [208 , 309]

Sez. G: F116 L=400,8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-2	
0	1	-4204	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.25	>100	1.25
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7011 [309 , 319]

Sez. G: F116 L=264,2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-VII-1	
264	1	475	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	11.1	>100	11.1
264	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7012 [319 , 238]

Sez. G: F116 L=278,2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-VIII-1	
0	1	1527	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.45	>100	3.45
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7013 [238 , 226]

Sez. G: F116 L=318,9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
319	1	-814	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	6.47	>100	6.47
319	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7014 [226 , 124]

Sez. G: F116 L=360,8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-II-2	
0	1	1308	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	4.03	>100	4.03
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7015 [124 , 101]

Sez. G: F116 L=388,8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-2	
389	1	-1791	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.94	>100	2.94
389	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7016 [101 , 16]

Sez. G: F116 L=202,0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-VIII-3	
202	1	-2407	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.19	>100	2.19
202	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7017 [16 , 19]

Sez. G: F116 L=202,0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-VIII-2	
202	1	-3008	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.75	>100	1.75
202	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7018 [19 , 2]

Sez. G: F116 L=309,7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	5257	--	--	--	--	--	--	--	(12+13)+V-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	2.08	>100	2.08

Asia : 7019 [102 , 122]

Sez. G: Fil16 L=371.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2199	--	--	--	--	--	--	--	(12+13)+V-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	2.40	>100	2.40

Asia : 7020 [122 , 104]

Sez. G: Fil16 L=371.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
372	1	-2474	--	--	--	--	--	--	--	(12+13)+V-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
372	1	5266	--	--	--	--	--	>100	2.13	>100	2.13

Asia : 7021 [104 , 126]

Sez. G: Fil16 L=389.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1924	--	--	--	--	--	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	2.74	>100	2.74

Asia : 7022 [126 , 106]

Sez. G: Fil16 L=389.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
389	1	-2621	--	--	--	--	--	--	--	(12+13)+V-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
389	1	5266	--	--	--	--	--	>100	2.01	>100	2.01

Asia : 7023 [106 , 118]

Sez. G: Fil16 L=1801 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
389	1	1801	--	--	--	--	--	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
389	1	5266	--	--	--	--	--	>100	2.92	>100	2.92

Asia : 7024 [118 , 246]

Sez. G: Fil16 L=360.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1250	--	--	--	--	--	--	--	(12+13)+V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	4.21	>100	4.21

Asia : 7025 [246 , 223]

Sez. G: Fil16 L=319.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
319	1	770	--	--	--	--	--	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
319	1	5266	--	--	--	--	--	>100	6.84	>100	6.84

Asia : 7026 [223 , 327]

Sez. G: Fil16 L=278.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
278	1	1670	--	--	--	--	--	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
278	1	5266	--	--	--	--	--	>100	3.15	>100	3.15

Asia : 7027 [327 , 314]

Sez. G: Fil16 L=264.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
264	1	-1171	--	--	--	--	--	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
264	1	5266	--	--	--	--	--	>100	4.50	>100	4.50

Asia : 7028 [314 , 213]

Sez. G: Fil16 L=401.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
401	1	-4180	--	--	--	--	--	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
401	1	5266	--	--	--	--	--	>100	1.26	>100	1.26

Asia : 7029 [214 , 313]

Sez. G: Fil16 L=401.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4261	--	--	--	--	--	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.24	>100	1.24

Asia : 7030 [313 , 317]

Sez. G: Fil16 L=264.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
264	1	421	--	--	--	--	--	--	--	(12+13)+V-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
264	1	5266	--	--	--	--	--	>100	12.5	>100	12.5

Asia : 7031 [317 , 248]

Sez. G: Fil16 L=278,6 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq fl=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
279	1	-1522	--	--	--	--	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
279	1	5266	--	--	--	--	--	>100	3.46	>100	3.46

Asia : 7032 [248 , 221]

Sez. G: Fil16 L=319,0 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/γM=2619 kg/cmq fl=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m		
0	1	835	---	---	---	---	---	---	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	6.30	>100	6.30

Asia : 7033 [221 , 128]

Sez. G: Fil16 L=360,8 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq fl=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m		
0	1	1429	---	---	---	---	---	---	(12+13)+VI+3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	3.68	>100	3.68

Asia : 7034 [128 , 107]

Sez. G: Fil16 L=389,1 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq fl=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m		
389	1	-1957	--	--	--	--	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
389	1	5266	--	--	--	--	--	>100	2.69	>100	2.69

Asia : 7035 [107 , 24]

Sez. G: Fil6 L=201,9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/γM=2619 kg/cmq fl=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m		
0	1	2364	---	---	---	---	---	---	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.23	>100	2.23

Asia : 7036 [24 , 27]

Sez. G: Fil16 L=201,9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/γM=2619 kg/cmq fl=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m		
202	1	-2901	---	---	---	---	---	---	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
202	1	5266	--	--	--	--	--	>100	1.82	>100	1.82

Asia : 7037 [27 , 6]

Sez. G: Fil16 L=309,6 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq fl=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	2468	--	--	--	--	--	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.13	>100	2.13

Asia : 7038 [7 , 23]

Sez. G: Fil6 L=309,6 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/M=2619 kg/cmq fl=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m		
0	1	-2620	--	--	--	--	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.01	>100	2.01

Asia : 7039 [23 , 28]

Sez. G: Fil6 L=201,9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/My=2619 kg/cmq fl=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
202	1	2827	--	--	--	--	--	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
202	1	5266	--	--	--	--	--	>100	1.86	>100	1.86

Asia : 7040 [28 , 106]

Sez. G: Fil6 L=201,9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/fyM=2619 kg/cmq fl=4300 kg/cmq Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m		
0	1	-2541	--	--	--	--	--	--	(12+13)/N-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.07	>100	2.07

Asia : 7041 [124 , 103]

Sez. G: Fil6 L=371,1 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/γM=2619 kg/cmq fl=4300 kg/cmq Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m		
371	1	-2188	--	--	--	--	--	--	(12+13)+VIII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
371	1	5266	--	--	--	--	--	>100	2.41	>100	2.41

Asia : 7042 [103 , 116]

Sez. G: Fil6 L=371,8 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/γM=2619 kg/cmq fl=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-2579	--	--	--	--	--	--	--	(12+13)+VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.04	>100	2.04

Asia : 7043 [116 , 105]

Sez. G: Fil16 L=371,4 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/fM=2619 kg/cmq fl=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1807	--	--	--	--	--	--	--	(12+13)+IV-2

282

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.91	>100	2.91
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7044 [105 , 128]

Sez. G: F116 L=388.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-VIII-2	
0	1	-2608	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.02	>100	2.02
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7045 [309 , 321]

Sez. G: F116 L=260.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-VIII-4	
0	1	-2311	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.28	>100	2.28
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7046 [321 , 311]

Sez. G: F116 L=260.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
261	1	-2241	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.35	>100	2.35
261	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7047 [311 , 325]

Sez. G: F116 L=264.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-VI-4	
0	1	-1187	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	4.44	>100	4.44
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7048 [325 , 313]

Sez. G: F116 L=264.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
264	1	-2497	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.11	>100	2.11
264	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7049 [327 , 312]

Sez. G: F116 L=264.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-VIII-4	
264	1	-2178	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.42	>100	2.42
264	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7050 [312 , 315]

Sez. G: F116 L=259.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-II-3	
0	1	-1236	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	4.26	>100	4.26
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7051 [315 , 310]

Sez. G: F116 L=260.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-VIII-4	
260	1	-2553	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.06	>100	2.06
260	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7052 [310 , 323]

Sez. G: F116 L=260.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
0	1	-1996	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.64	>100	2.64
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7053 [105 , 26]

Sez. G: F116 L=162.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-2	
162	1	-2338	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.25	>100	2.25
162	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7054 [26 , 21]

Sez. G: F116 L=162.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
162	1	-2585	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.04	>100	2.04
162	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7055 [21 , 4]

Sez. G: F116 L=285.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-2	
284	1	-1779	--	--	--	--	--	--	--	--	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.96	>100	2.96
284	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7056 [5 , 25]

Sez. G: F116 L=285.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm q fl=4300 kg/cm q : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-1845	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.85	>100	2.85

Asta : 7057 [25 , 22]

Sez. G: Fil16 L=162.0 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2534	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.08	>100	2.08

Asta : 7058 [22 , 104]

Sez. G: Fil16 L=344.9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2256	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.33	>100	2.33

Asta : 7059 [116 , 241]

Sez. G: Fil16 L=344.9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1607	--	--	--	--	--	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	3.28	>100	3.28

Asta : 7060 [241 , 218]

Sez. G: Fil16 L=306.1 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
306	1	404	--	--	--	--	--	--	--	(12+13)-VII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
306	1	5266	--	--	--	--	--	>100	13.0	>100	13.0

Asta : 7061 [218 , 325]

Sez. G: Fil16 L=268.4 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
268	1	1798	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
268	1	5266	--	--	--	--	--	>100	2.93	>100	2.93

Asta : 7062 [315 , 243]

Sez. G: Fil16 L=269.4 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
269	1	-1773	--	--	--	--	--	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
269	1	5266	--	--	--	--	--	>100	2.97	>100	2.97

Asta : 7063 [243 , 216]

Sez. G: Fil16 L=305.6 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	442	--	--	--	--	--	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	11.9	>100	11.9

Asta : 7064 [216 , 126]

Sez. G: Fil16 L=345.2 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1612	--	--	--	--	--	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	3.27	>100	3.27

Asta : 8000 [101 , 119]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2516	93	-1477	-11	4180	28	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86269	37706	19516	9213	462	25.5	4.35	42.3	4.35

Asta : 8000 [119 , 120]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2061	-91	-939	-3	2839	-120	--	--	(12+13)-I-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86898	37981	19516	9213	462	40.5	5.93	>100	5.93

Asta : 8000 [120 , 225]

Sez. G: HE 240 A L=169.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
170	1	-949	124	-536	9	-2670	261	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	201236	86443	37782	19516	9213	462	70.4	5.89	53.5	5.89

Asta : 8000 [225 , 226]

Sez. G: HE 240 A L=158.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
158	1	-392	130	-439	-5	-3429	88	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
158	1	201236	86682	37887	19516	9213	462	86.3	5.34	84.1	5.34

Asia : 8000 [226 , 227]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
148	1	-417	37	-184	-11	-3846	46	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
148	1	201236	86228	37688	19516	9213	462	>100	4.90	40.3	4.90

Asia : 8000 [227 , 228]

Sez. G: HE 240 A L=134.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
27	1	-305	30	-84	-16	-3874	30	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
27	1	201236	85910	37549	19516	9213	462	>100	4.92	29.5	4.92

Asia : 8000 [228 , 229]

Sez. G: HE 240 A L=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	131	-38	206	-11	-3878	-20	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86284	37713	19516	9213	462	>100	4.96	43.0	4.96

Asia : 8000 [229 , 319]

Sez. G: HE 240 A L=113.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	160	-83	535	-5	-3513	4	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86704	37896	19516	9213	462	70.8	5.52	88.8	5.52

Asia : 8000 [319 , 320]

Sez. G: HE 240 A L=108.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
108	1	-1852	103	1331	-7	4143	-40	--	--	(12+13)+IV-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	201236	86548	37828	19516	9213	462	28.4	4.43	63.6	4.43

Asia : 8000 [320 , 308]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
112	1	-2315	-28	967	-10	5093	-14	--	--	(12+13)+II-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	86372	37751	19516	9213	462	39.0	3.65	48.2	3.65

Asia : 8001 [102 , 123]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4587	-5	-1985	13	4674	34	--	--	2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86124	37643	19516	9213	462	19.0	3.76	36.0	3.76

Asia : 8001 [123 , 124]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2069	-26	-422	0	2889	-90	--	--	(12+13)+I-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87062	38053	19516	9213	462	90.1	5.95	>100	5.95

Asia : 8001 [124 , 235]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
170	1	-2595	127	-61	8	-3020	261	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	86459	37789	19516	9213	462	61.9	5.10	54.8	5.10

Asia : 8001 [235 , 236]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
159	1	-1921	119	-466	-6	-3872	99	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
159	1	201236	86630	37864	19516	9213	462	81.2	4.57	74.7	4.57

Asia : 8001 [236 , 237]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
148	1	-1327	-9	-66	-13	-4173	98	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
148	1	201236	86148	37653	19516	9213	462	>100	4.33	36.9	4.33

Asia : 8001 [237 , 238]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
13	1	-1150	-21	18	-16	-4172	51	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
13	1	201236	85850	37523	19516	9213	462	>100	4.44	28.1	4.44

Asta : 8001 [238 , 239]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1141	-88	385	-10	-3991	17	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86342	37738	19516	9213	462	98.0	4.72	46.3	4.72

Asta : 8001 [239 , 323]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
113	1	-2050	-4	1192	0	3463	-8	--	--	(12+13)-1-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	201236	87082	38061	19516	9213	462	31.9	5.31	>100	5.31

Asta : 8001 [323 , 324]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
108	1	-1252	-28	637	1	4041	27	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
108	1	201236	86988	38020	19516	9213	462	59.7	4.62	>100	4.62

Asta : 8001 [324 , 309]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	-597	-20	1768	-9	4691	-14	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	86407	37766	19516	9213	462	21.4	4.08	50.6	4.08

Asta : 8002 [103 , 121]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3943	-32	-1843	9	4561	44	--	--	2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86422	37773	19516	9213	462	20.5	3.87	51.8	3.87

Asta : 8002 [121 , 122]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2021	-4	-451	0	2836	-30	--	--	(12+13)-I-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87082	38062	19516	9213	462	84.4	6.30	>100	6.30

Asta : 8002 [122 , 230]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
170	1	-2108	137	-602	9	-2889	269	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	201236	86389	37758	19516	9213	462	62.7	5.33	49.3	5.33

Asta : 8002 [230 , 231]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
158	1	-1475	138	-481	-5	-3748	97	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
158	1	201236	86719	37903	19516	9213	462	78.7	4.77	92.2	4.77

Asta : 8002 [231 , 232]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
148	1	-1026	1	-153	-12	-4163	92	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
148	1	201236	86226	37687	19516	9213	462	>100	4.38	40.2	4.38

Asta : 8002 [232 , 233]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
54	1	-784	-17	29	-15	-4177	56	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
54	1	201236	85924	37555	19516	9213	462	>100	4.46	29.9	4.46

Asta : 8002 [233 , 234]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-584	-92	292	-9	-4087	13	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
0	1	201236	86399	37763	19516	9213	462	>100	4.68	50.1	4.68

Asia : 8002 [234 , 321]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-477	-100	684	-5	-3560	68	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86726	37906	19516	9213	462	55.4	5.20	94.1	5.20

Asia : 8002 [321 , 322]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
108	1	-1369	-11	969	0	4109	30	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	201236	87067	38055	19516	9213	462	39.3	4.53	>100	4.53

Asia : 8002 [322 , 310]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	-1820	22	589	-0	4656	-0	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	87090	38065	19516	9213	462	64.6	4.04	>100	4.04

Asia : 8003 [104 , 115]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3896	-56	-1871	9	4655	51	--	--	2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86393	37761	19516	9213	462	20.2	3.80	49.7	3.80

Asia : 8003 [115 , 116]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2212	6	-496	0	2842	68	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87089	38065	19516	9213	462	76.8	6.10	>100	6.10

Asia : 8003 [116 , 215]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
170	1	-1996	144	-605	9	-2921	263	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	86434	37778	19516	9213	462	62.4	5.32	52.7	5.32

Asia : 8003 [215 , 216]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
159	1	-1363	141	-477	-6	-3771	87	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
159	1	201236	86681	37886	19516	9213	462	79.5	4.78	83.8	4.78

Asia : 8003 [216 , 217]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
148	1	-1267	-3	-136	-11	-4161	90	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
148	1	201236	86243	37695	19516	9213	462	>100	4.36	41.0	4.36

Asia : 8003 [217 , 218]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
54	1	-1021	-21	25	-15	-4176	55	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
54	1	201236	85965	37573	19516	9213	462	>100	4.44	31.0	4.44

Asia : 8003 [218 , 219]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-757	-105	298	-8	-4091	14	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86461	37790	19516	9213	462	>100	4.65	55.0	4.65

Asia : 8003 [219 , 315]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-646	-102	663	-5	-3557	81	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86744	37914	19516	9213	462	57.2	5.15	98.8	5.15

Asia : 8003 [315 , 316]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
108	1	-1728	5	816	-0	4156	7	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	201236	87073	38057	19516	9213	462	46.6	4.50	>100	4.50

Asia : 8003 [316 , 311]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	-1997	2	359	-0	4637	0	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	87078	38060	19516	9213	462	>100	4.04	>100	4.04

Asia : 8004 [105 , 125]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4743	-77	-2045	7	4884	62	--	--	2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86580	37842	19516	9213	462	18.5	3.56	67.6	3.56

Asia : 8004 [125 , 126]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1737	23	-615	-0	2880	123	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87065	38054	19516	9213	462	61.8	5.90	>100	5.90

Asia : 8004 [126 , 240]

Sez. G: HE 240 A L=169.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
170	1	-2731	149	-619	8	-3049	262	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	86459	37789	19516	9213	462	61.1	5.05	54.8	5.05

Asia : 8004 [240 , 241]

Sez. G: HE 240 A L=158.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
158	1	-2038	155	-468	-5	-3908	72	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
158	1	201236	86685	37888	19516	9213	462	81.0	4.58	84.7	4.58

Asia : 8004 [241 , 242]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
148	1	-1485	-2	-87	-10	-4243	83	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
148	1	201236	86325	37731	19516	9213	462	>100	4.28	45.3	4.28

Asia : 8004 [242 , 243]

Sez. G: HE 240 A L=134.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
13	1	-1275	-10	-8	-15	-4245	50	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
13	1	201236	85987	37583	19516	9213	462	>100	4.36	31.6	4.36

Asia : 8004 [243 , 244]

Sez. G: HE 240 A L=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1034	-105	380	-7	-4097	13	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86556	37832	19516	9213	462	99.5	4.62	64.6	4.62

Asia : 8004 [244 , 325]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
113	1	-2149	126	1477	-7	3632	-149	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	201236	86557	37832	19516	9213	462	25.6	4.70	64.7	4.70

Asia : 8004 [325 , 326]

Sez. G: HE 240 A L=108.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
108	1	-1268	7	739	-0	4284	-33	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	201236	87063	38053	19516	9213	462	51.5	4.36	>100	4.36

Asia : 8004 [326 , 312]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	-1647	-0	696	-1	4774	-1	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	87044	38045	19516	9213	462	54.6	3.95	>100	3.95

Asia : 8005 [106 , 127]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
0	1	-4974	-103	-2207	10	4951	13	--	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg	kg	kg	kg
0	1	201236	86310	37724	19516	9213	462	17.1	3.57	44.4	3.57

Asia : 8005 [127 , 128]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
0	1	-1967	18	-558	-0	3063	113	--	--	--	(12+13)>V-1

X	cls	Nr	Vyr	Vzr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m				
0	1	201236	87064	38054	19516	9213	68.2	5.59	>100	5.59

Asia : 8005 [128 , 245]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
170	1	-2903	139	-535	7	-3173	248	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m				
170	1	201236	86584	37844	19516	9213	70.8	4.90	68.1	4.90

Asia : 8005 [245 , 246]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
158	1	-2167	137	-337	-7	-3845	64	--	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
158	1	201236	86566	37836	19516	9213	462	>100	4.66	65.8	4.66

Asia : 8005 [246 , 247]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
148	1	-2261	-21	-11	-4044	90	--	--	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
148	1	201236	86278	37710	19516	9213	462	>100	4.38	42.7	4.38

Asia : 8005 [247 , 248]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
0	1	-2067	-6	-15	-4044	48	--	--	--	--	9

X	cls	Nr	Vyr	Vzr	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m				
0	1	201236	85961	37571	19516	9213	462	>100	4.49	30.9
								4.49		4.49

Asia : 8005 [248 , 249]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
0	1	-1422	-119	293	-7	-3833	3	--	--	--	9

X	cls	Nr	Vyr	Vzr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg	kg	kg	kg	kg
0	1	201236	86565	37835	19516	9213	462	>100	4.91	65.6

Asia : 8005 [249 , 327]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
113	1	-2954	-3	1113	0	3802	15	--	--	--	(12+13)>VIL-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M.	SF Mt	SF
cm		kg	kg	kg	kg	kg	kg	kg	kg	kg	kg
113	1	201236	87078	38060	19516	9213	462	34.2	4.74	>100	4.74

Asia : 8005 [327 , 328]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
108	1	-1843	4	674	-6	4318	-39	--	--	--	(12+13)>V-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg	kg	kg	kg	kg	kg
108	1	201236	86679	37885	19516	9213	462	56.2	4.26	83.4	4.26

Asia : 8005 [328 , 313]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
112	1	-1583	-38	1600	6	5111	8	--	--	--	(12+13)>III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
112	1	201236	86637	37867	19516	9213	462	23.7	3.70	75.9	3.70

Asia : 8006 [107 , 117]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
0	1	-2678	-108	-1316	10	4697	-38	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg	kg	kg			
0	1	201236	86332	37733	19516	9213	462	28.7	3.87	45.7	3.87

Asia : 8006 [117 , 118]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg	kg	kg			
cm		kg	kg	kg	kg	kg	kg	kg			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-2023	9	-568	-0	2989	97	--	--	(12+13)+VII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	201236	87091	38065	19516	9213	462	67.0	5.76	>100	5.76

Asia : 8006 [118 , 220]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
170	1	-1283	122	-597	4	-2754	226	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
170	1	201236	86759	37920	19516	9213	462	63.6	5.81	>100	5.81

Asia : 8006 [220 , 221]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
159	1	-773	116	-516	-9	-3631	46	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
159	1	201236	86395	37761	19516	9213	462	73.2	5.13	49.8	5.13

Asia : 8006 [221 , 222]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
148	1	-36	-28	-192	-12	-4062	73	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
148	1	201236	86223	37686	19516	9213	462	>100	4.62	40.0	4.62

Asia : 8006 [222 , 223]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
27	1	130	24	-32	-15	-4075	35	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
27	1	201236	85934	37560	19516	9213	462	>100	4.69	30.1	4.69

Asia : 8006 [223 , 224]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	43	-96	363	-7	-4024	-27	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	201236	86598	37850	19516	9213	462	>100	4.78	70.0	4.78

Asia : 8006 [224 , 317]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

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: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
113	1	-755	47	1673	-5	3520	-35	--	--	(12+13)+VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
113	1	201236	86757	37920	19516	9213	462	22.7	5.32	>100	5.32

Asia : 8006 [317 , 318]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
108	1	-1949	5	1294	-1	4761	4	--	--	(12+13)+VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
108	1	201236	87007	38029	19516	9213	462	29.4	3.94	>100	3.94

Asia : 8006 [318 , 314]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	-2423	1	631	6	5452	8	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
112	1	201236	86619	37859	19516	9213	462	60.0	3.42	73.0	3.42

Asia : 8007 [20 , 16]

Sez. G: IPE 100 L=149.9 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
162	1	231	-11	9	0	0	24	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
162	1	27037	9480	7688	1033	240	27	>100	9.18	>100	9.18

Asia : 8007 [16 , 18]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	357	2	-4	-0	0	19	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	27037	9481	7689	1033	240	27	>100	10.9	>100	10.9

Asia : 8007 [18 , 26]

Sez. G: IPE 100 L=90.1 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
36	1	-254	0	-1	-0	-1	15	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
36	1	27037	9481	7689	1033	240	27	>100	13.6	>100	13.6

Asia : 8007 [26 , 22]

Sez. G: IPE 100 L=88.8 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

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X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
89	1	-125	-15	5		0	0	24	--	--	9

X	cls	Nr	Vyr	Vzr	MTrd	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*				
89	1	27037	9481	7689	1033	240	>100	9.37	>100	9.37

Asta : 8007 [22 , 24]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	-239	-5	8	-0	0	22	--	--	9	

X	cls	Nr	Vyr	Vzr	MTrd	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*				
149	1	27037	9480	7688	1033	240	>100	10.1	>100	10.1

Asta : 8007 [24 , 28]

Sez. G: IPE 100 L=149.7 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-44	10	-8	-0	0	20	--	--	9	

X	cls	Nr	Vyr	Vzr	MTrd	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*				
0	1	27037	9480	7688	1033	240	>100	11.7	>100	11.7

Asta : 8008 [19 , 15]

Sez. G: IPE 100 L=149.9 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
150	1	200	-13	8	0	0	24	--	--	9	

X	cls	Nr	Vyr	Vzr	MTrd	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*				
150	1	27037	9479	7687	1033	240	>100	9.26	>100	9.26

Asta : 8008 [15 , 17]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	349	7	-4	-0	0	21	--	--	8	

X	cls	Nr	Vyr	Vzr	MTrd	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*				
0	1	27037	9481	7689	1033	240	>100	9.92	>100	9.92

Asta : 8008 [17 , 25]

Sez. G: IPE 100 L=90.1 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
36	1	288	0	-1	-0	-1	15	--	--	8	

X	cls	Nr	Vyr	Vzr	MTrd	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*				
36	1	27037	9481	7689	1033	240	>100	13.2	>100	13.2

Asta : 8008 [25 , 21]

Sez. G: IPE 100 L=88.8 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	284	-3	5	0	0	18	--	--	8	

X	cls	Nr	Vyr	Vzr	MTrd	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*				
89	1	27037	9480	7688	1033	240	>100	11.9	>100	11.9

Asta : 8008 [21 , 23]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	142	-3	8	-0	0	21	--	--	8	

X	cls	Nr	Vyr	Vzr	MTrd	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*				
149	1	27037	9480	7688	1033	240	>100	11.0	>100	11.0

Asta : 8008 [23 , 27]

Sez. G: IPE 100 L=149.7 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	133	12	-8	-0	0	21	--	--	8	

X	cls	Nr	Vyr	Vzr	MTrd	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*				
0	1	27037	9479	7687	1033	240	>100	10.9	>100	10.9

Verifica spostamenti verticali delle aste in Acciaio secondo NTC 2008

Scenario di calcolo : Set NT_SLD_A2_STR/GEO

Travata: 8000 (Travata 8000) [101 (Nodo 101) , 308 (Nodo 308)]

L = 1424.0cm Crit.Prog: Acciaio_Pressflessione $\delta \epsilon = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
861.2	1	10.26	56.96	5.55

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
955.2	1	3.58	47.47	13.2

Travata: 8001 (Travata 8001) [102 (Nodo 102) , 309 (Nodo 309)]

L = 1426.4cm Crit.Prog: Acciaio_Pressflessione $\delta \epsilon = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
820.7	1	11.81	57.05	4.83

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
916.1	1	4.13	47.55	11.5

Travata: 8002 (Travata 8002) [103 (Nodo 103) , 310 (Nodo 310)]

L = 1424.6cm Crit.Prog: Acciaio_Pressflessione $\delta \epsilon = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
848.1	1	11.97	56.99	4.76

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	

x	Comb.	82	L/300.00	Cs
928.7	1	4.13	47.49	11.5

Travata: 8003 (Travata 8003) | 104 (Nodo 104), 311 (Nodo 311) |

L = 1426.3cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
835.5	1	12.22	57.05	4.67

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
929.6	1	4.16	47.54	11.4

Travata: 8004 (Travata 8004) | 105 (Nodo 105), 312 (Nodo 312) |

L = 1424.2cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
834.2	1	12.48	56.97	4.57

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
901.3	1	4.29	47.47	11.1

Travata: 8005 (Travata 8005) | 106 (Nodo 106), 313 (Nodo 313) |

L = 1425.0cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
805.0	1	12.17	57.00	4.68

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
901.7	1	4.06	47.50	11.7

Travata: 8006 (Travata 8006) | 107 (Nodo 107), 314 (Nodo 314) |

L = 1426.3cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
848.9	1	11.02	57.05	5.18

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
929.6	1	3.82	47.54	12.4

Travata: 101 (Travata 101) | 119 (Nodo 119), 117 (Nodo 117) |

L = 734.9cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
525.4	2	1.07	29.39	27.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	

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x	Comb.	82	L/300.00	Cs
525.4	2	0.35	24.50	70.0

Travata: 102 (Travata 102) | 120 (Nodo 120), 118 (Nodo 118) |

L = 752.8cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
543.4	2	1.76	30.11	17.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
558.3	2	0.57	25.09	43.7

Travata: 103 (Travata 103) | 225 (Nodo 225), 220 (Nodo 220) |

L = 770.8cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
546.4	2	2.11	30.83	14.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
471.6	2	0.65	25.69	39.7

Travata: 104 (Travata 104) | 236 (Nodo 226), 221 (Nodo 221) |

L = 788.8cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
564.4	2	2.10	31.55	15.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
489.6	2	0.69	26.29	38.4

Travata: 105 (Travata 105) | 227 (Nodo 227), 222 (Nodo 222) |

L = 806.8cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
567.4	2	1.85	32.27	17.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
507.5	2	0.61	26.89	43.8

Travata: 106 (Travata 106) | 228 (Nodo 228), 223 (Nodo 223) |

L = 824.8cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ _{max}	L/250.00	Cs
cm		mm	mm	
570.4	1	1.46	32.99	22.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	

302

x	Comb.	82	L/300.00	Cs
525.5	2	0.48	27.49	57.7

Travata: 107 (Travata 107) | 229 (Nodo 229) , 224 (Nodo 224) |
L = 842.8cm *Crit.Prog:* Acciaio_Flessione $\delta\epsilon = 0.0cm$ *Verifica:* **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
451.6	1	1.10	33.71	30.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
797.9	8	-0.39	28.09	71.3

Travata: 108 (Travata 108) | 319 (Nodo 319) , 317 (Nodo 317) |
L = 860.8cm *Crit.Prog:* Acciaio_Flessione $\delta\epsilon = 0.0cm$ *Verifica:* **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
465.3	2	0.75	34.43	45.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
815.9	8	-0.40	28.69	71.7

Travata: 109 (Travata 109) | 320 (Nodo 320) , 318 (Nodo 318) |

L = 878.7cm *Crit.Prog:* Acciaio_Flessione $\delta\epsilon = 0.0cm$ *Verifica:* **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
350.2	2	0.47	35.15	75.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
104.6	7	-0.33	29.29	88.8

Travata: 301 (Travata 301) | 308 (Nodo 308) , 314 (Nodo 314) |

L = 896.7cm *Crit.Prog:* Acciaio_Flessione $\delta\epsilon = 0.0cm$ *Verifica:* **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
74.7	7	-0.39	35.87	91.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
224.2	7	-0.51	29.89	58.1

Travata: 110 (Travata 110) | 101 (Nodo 101) , 107 (Nodo 107) |

L = 716.9cm *Crit.Prog:* Acciaio_Flessione $\delta\epsilon = 0.0cm$ *Verifica:* **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
492.5	7	-0.41	28.67	70.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	

303

x	Comb.	82	L/300.00	Cs
74.9	7	-0.50	23.90	47.8

Travata: 8007 (Travata 8007) | 20 (Nodo 20) , 28 (Nodo 28) |
L = 716.6cm *Crit.Prog:* Acciaio_Flessione $\delta\epsilon = 0.0cm$ *Verifica:* **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
80.8	7	-0.63	28.66	45.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
80.8	7	-0.61	23.89	39.3

Travata: 8008 (Travata 8008) | 19 (Nodo 19) , 27 (Nodo 27) |

L = 704.9cm *Crit.Prog:* Acciaio_Flessione $\delta\epsilon = 0.0cm$ *Verifica:* **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
480.4	7	-0.58	28.19	48.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
74.9	7	-0.53	23.50	44.3

Verifica delle travi (Stati limite esercizio)

Scenario di calcolo : Set NT_SLD_A2_STR/GEO

Travi di Fond. : 9003 | 1.2 | Pilastrate | 1.2 |

Sez. R: *By* = 60.0 cm *Bz* = 100.0 cm *L* = 149.9 cm *L_n* = 161.9 cm *Terreno:* **Terreno I**

Criterio : *CLS Travifondazione*

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{c-}	σ_{f+}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	911	--	12.06	12.06	-1	84	--	--	8	6	Si	42.9
16.2	253	--	12.06	12.06	-0	23	--	--	8	1	Si	>100
80.9	--	1540	12.06	12.06	--	--	-2	142	6	8	Si	25.4
145.7	--	2009	12.06	12.06	--	--	-3	185	6	8	Si	19.4
161.9	--	1921	12.06	12.06	--	--	-3	177	1	8	Si	20.3

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{c-}	σ_{f+}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	260	--	12.06	12.06	-0	24	--	--	14	14	Si	>100
16.2	--	122	12.06	12.06	--	--	-0	11	14	14	Si	>100
80.9	--	660	12.06	12.06	--	--	-1	61	14	14	Si	59.2
145.7	201	--	12.06	12.06	-0	19	--	--	14	14	Si	>100
161.9	607	--	12.06	12.06	-1	56	--	--	14	14	Si	64.4

Verifica aperture fessure: W_{amm} Freq[mm]=0.400 W_{amm} Qp[mm]=0.300

X	M	Act	mq	Aft	pAft	S _{max}	σ _f inf	Wd	Wk	Cb	Ver.	Cs
cm	kg*m		mm	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-260	0.1	12.06	30.16	30.16	22.4	24	0.002	0.002	9(Fr)	Si	>100
0.0	-260	0.1	12.06	30.16	30.16	22.4	24	0.002	0.002	14(Op)	Si	>100
16.2	122	0.1	12.06	30.16	30.16	22.4	11	0.001	0.001	14(Op)	Si	>100
16.2	49	0.1	12.06	30.16	30.16	22.4	4	0.000	0.000	13(Fr)	Si	>100
80.9	660	0.1	12.06	30.16	30.16	22.4	61	0.004	0.004	14(Op)	Si	77.2
80.9	660	0.1	12.06	30.16	30.16	22.4	61	0.004	0.004	9(Fr)	Si	>100
145.7	-201	0.1	12.06	30.16	30.16	22.4	19	0.001	0.001	14(Op)	Si	>100
145.7	-92	0.1	12.06	30.16	30.16	22.4	8	0.001	0.001	11(Fr)	Si	>100

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X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
161.9	-607	0.1	12.06	30.16	22.4	56	0.004	0.004	14(Qp)	Si	84.0
161.9	-151	0.1	12.06	30.16	22.4	14	0.001	0.001	13(Fr)	Si	>100

Trave di Fond.: 9003 | 2. 3 | Pilastro | 2. 3 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.0 cm Ln= 89.0 cm Terreno: Terreno I

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cm^2]=149 \sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	cmq	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	1534	12.06	12.06	--	--	--	-2	141	1	8	Si	25.5
8.9	--	1611	12.06	12.06	--	--	--	-2	148	1	8	Si	24.3
44.5	477	1666	12.06	12.06	-1	44	--	-3	154	6	8	Si	23.5
80.1	1372	1317	12.06	12.06	-2	126	--	-2	121	1	8	Si	28.5
89.0	1655	1166	12.06	12.06	-3	153	--	-2	107	1	8	Si	23.6

Combinazione QP: $\sigma_{cal}[kg/cm^2]=112 \sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	cmq	cmq	σf+	σc+	σf-	σc-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	553	--	12.06	12.06	-1	51	--	--	--	--	14	14	Si	70.7
8.9	586	--	12.06	12.06	-1	54	--	--	--	--	14	14	Si	66.6
44.5	919	--	12.06	12.06	-1	85	--	--	--	--	14	14	Si	42.5
80.1	1542	--	12.06	12.06	-2	142	--	--	--	--	14	14	Si	25.3
89.0	1739	--	12.06	12.06	-3	160	--	--	--	--	14	14	Si	22.5

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cmq	cm	kg/cmq	mm	mm			
0.0	-182	0.1	12.06	30.16	22.4	17	0.001	0.001	13(Fr)	Si	>100
0.0	-553	0.1	12.06	30.16	22.4	51	0.003	0.003	14(Qp)	Si	92.2
8.9	-586	0.1	12.06	30.16	22.4	54	0.003	0.003	14(Qp)	Si	86.9
8.9	-205	0.1	12.06	30.16	22.4	19	0.001	0.001	13(Fr)	Si	>100
44.5	-919	0.1	12.06	30.16	22.4	85	0.005	0.005	14(Qp)	Si	55.4
44.5	-492	0.1	12.06	30.16	22.4	45	0.003	0.003	13(Fr)	Si	>100
80.1	-1542	0.1	12.06	30.16	22.4	142	0.009	0.009	14(Qp)	Si	33.0
80.1	-1075	0.1	12.06	30.16	22.4	99	0.006	0.006	13(Fr)	Si	63.2
89.0	-1739	0.1	12.06	30.16	22.4	160	0.010	0.010	14(Qp)	Si	29.3
89.0	-1263	0.1	12.06	30.16	22.4	116	0.007	0.007	13(Fr)	Si	53.8

Trave di Fond.: 9003 | 3. 4 | Pilastro | 3. 4 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 90.1 cm Ln= 90.1 cm Terreno: Terreno I

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cm^2]=149 \sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg·m	kg·m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1848	767	12.06	12.06	-3	170	-1	71	1	8	Si	21.1
9.0	1817	875	12.06	12.06	-3	167	-1	81	1	8	Si	21.5
45.1	1911	1045	12.06	12.06	-3	176	-2	96	6	8	Si	20.4
81.1	2329	796	12.06	12.06	-4	215	-1	73	1	8	Si	16.8
90.1	2485	669	12.06	12.06	-4	229	-1	62	1	8	Si	15.7

Combinazione QP: $\sigma_{cal}[kg/cm^2]=112 \sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1701	--	12.06	12.06	-3	157	--	--	14	14	Si	23.0
9.0	1672	--	12.06	12.06	-3	154	--	--	14	14	Si	23.4
45.1	1714	--	12.06	12.06	-3	158	--	--	14	14	Si	22.8
81.1	1999	--	12.06	12.06	-3	184	--	--	14	14	Si	19.5
90.1	2107	--	12.06	12.06	-3	194	--	--	14	14	Si	18.5

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cmq	cm	kg/cmq	mm	mm			
0.0	-1311	0.1	12.06	30.16	22.4	121	0.008	0.008	13(Fr)	Si	51.8
0.0	-1701	0.1	12.06	30.16	22.4	157	0.010	0.010	14(Qp)	Si	29.9
9.0	-1672	0.1	12.06	30.16	22.4	154	0.010	0.010	14(Qp)	Si	30.5
9.0	-1275	0.1	12.06	30.16	22.4	118	0.008	0.008	13(Fr)	Si	53.3
45.1	-1714	0.1	12.06	30.16	22.4	158	0.010	0.010	14(Qp)	Si	29.7
45.1	-1296	0.1	12.06	30.16	22.4	119	0.008	0.008	13(Fr)	Si	52.4
81.1	-1999	0.1	12.06	30.16	22.4	184	0.012	0.012	14(Qp)	Si	25.5
81.1	-1573	0.1	12.06	30.16	22.4	145	0.009	0.009	13(Fr)	Si	43.2
90.1	-2107	0.1	12.06	30.16	22.4	194	0.012	0.012	14(Qp)	Si	24.2
90.1	-1681	0.1	12.06	30.16	22.4	155	0.010	0.010	13(Fr)	Si	40.4

Trave di Fond.: 9003 | 4. 5 | Pilastro | 4. 5 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 88.8 cm Ln= 88.8 cm Terreno: Terreno I

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cm^2]=149 \sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	A sup	A inf	cmq <th>cmq<th>σf+</th><th>σc+</th><th>σf-</th><th>σc-</th><th>Cb+</th><th>Cb-</th><th>Ver.</th><th>Cs</th></th>	cmq <th>σf+</th> <th>σc+</th> <th>σf-</th> <th>σc-</th> <th>Cb+</th> <th>Cb-</th> <th>Ver.</th> <th>Cs</th>	σf+	σc+	σf-	σc-	Cb+	Cb-	Ver.	Cs
cm	kg·m	kg·m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	2769	327	12.06	12.06	-4	255	--	1	30	--	1	5	Si	14.1
8.9	2579	504	12.06	12.06	-4	238	--	1	46	--	1	5	Si	15.1
44.4	2053	950	12.06	12.06	-3	189	--	1	88	--	6	8	Si	19.0
79.9	1807	1066	12.06	12.06	-3	167	--	2	98	--	6	8	Si	21.6
88.8	1787	1034	12.06	12.06	-3	165	--	2	95	--	6	8	Si	21.9

Combinazione QP: $\sigma_{cal}[kg/cm^2]=112 \sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	A _{sup}	A _{inf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	2125	--	12.06	12.06	-3	196	--	--	14	14	Si	18.4
8.9	2004	--	12.06	12.06	-3	185	--	--	14	14	Si	19.5
44.4	1665	--	12.06	12.06	-3	153	--	--	14	14	Si	23.5
79.9	1562	--	12.06	12.06	-2	144	--	--	14	14	Si	25.0
88.8	1575	--	12.06	12.06	-2	145	--	--	14	14	Si	24.8

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cmq	cm	kg/cmq	mm	mm			
0.0	-1742	0.1	12.06	30.16	22.4	161	0.010	0.010	11(Fr)	Si	39.0
0.0	-2125	0.1	12.06	30.16	22.4	196	0.013	0.013	14(Qp)	Si	24.0
8.9	-2004	0.1	12.06	30.16	22.4	185	0.012	0.012	14(Qp)	Si	25.4
8.9	-1620	0.1	12.06	30.16	22.4	149	0.010	0.010	11(Fr)	Si	41.9
44.4	-1665	0.1	12.06	30.16	22.4	153	0.010	0.010	14(Qp)	Si	30.6
44.4	-1288	0.1	12.06	30.16	22.4	119	0.008	0.008	13(Fr)	Si	52.7
79.9	-1562	0.1	12.06	30.16	22.4	144	0.009	0.009	14(Qp)	Si	32.6
79.9	-1170	0.1	12.06	30.16	22.4	108	0.007	0.007	13(Fr)	Si	58.1
88.8	-1575	0.1	12.06	30.16	22.4	145	0.009	0.009	14(Qp)	Si	32.3
88.8	-1180	0.1	12.06	30.16	22.4	109	0.007	0.007	13(Fr)	Si	57.6

Trave di Fond.: 9003 | 5. 6 | Pilastro | 5. 6 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.5 cm Ln= 149.5 cm Terreno: Terreno I

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cm^2]=149 \sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	2129	661	12.06	12.06	-3	196	-1	61	6	5	Si	18.3
14.9	1628	980	12.06	12.06	-3	150	-2	90	6	5	Si	24.0
74.7	155	1559	12.06	12.06	-0	14	-2	144	6	5	Si	25.1
134.5	--	1136	12.06	12.06	--	--	--	105	6	8	Si	34.4
149.5	--	874	12.06	12.06	--	--	-1	81	6	8	Si	44.7

Combinazione QP: $\sigma_{cal}[kg/cm^2]=112 \sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				

X	M+	M-	M-	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
0.0	1624	--	12.06	12.06	-3	150	--	--	14	--	--	14	14	Si	24.1
14.9	1227	--	12.06	12.06	-2	113	--	--	14	--	--	14	14	Si	31.8
74.7	1111	--	12.06	12.06	-0	10	--	--	14	--	--	14	14	Si	>100
134.5	--	179	12.06	12.06	--	--	--	--	16	14	14	14	14	Si	>100
149.5	--	110	12.06	12.06	--	--	--	--	10	14	14	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	kg*m	cm	cm	cm	kg/cmq	mm	mm	mm	mm	mm	mm	mm	mm
0.0	-127.5	0.1	12.06	30.16	22.4	118	0.008	0.008	11(Fr)	Si	53.3				
0.0	-1624	0.1	12.06	30.16	22.4	150	0.010	0.010	14(Qp)	Si	31.4				
14.9	-1227	0.1	12.06	30.16	22.4	113	0.007	0.007	14(Qp)	Si	41.5				
14.9	-900	0.1	12.06	30.16	22.4	83	0.005	0.005	11(Fr)	Si	75.5				
74.7	-111	0.1	12.06	30.16	22.4	10	0.001	0.001	14(Qp)	Si	>100				
74.7	103	0.1	12.06	30.16	22.4	10	0.001	0.001	13(Fr)	Si	>100				
134.5	179	0.1	12.06	30.16	22.4	16	0.001	0.001	14(Qp)	Si	>100				
134.5	134	0.1	12.06	30.16	22.4	12	0.001	0.001	12(Fr)	Si	>100				
149.5	110	0.1	12.06	30.16	22.4	10	0.001	0.001	14(Qp)	Si	>100				
149.5	84	0.1	12.06	30.16	22.4	8	0.000	0.000	12(Fr)	Si	>100				

Trave di Fond.: 9003 | 6. 7 | Pilastrate [6. 7]

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln= 149.7 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	M-	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	cm	cm	cm	kg/cmq	kg/cmq	mm	mm	mm	mm	mm	mm	mm
0.0	43	528	12.06	12.06	-0	4	-1	49	6	5	Si	74.0			
16.2	--	798	12.06	12.06	--	--	--	74	6	5	Si	49.0			
80.8	--	1326	12.06	12.06	--	--	--	122	5	1	Si	29.4			
145.5	--	561	12.06	12.06	--	--	--	52	5	7	Si	69.6			
161.7	103	156	12.06	12.06	-0	9	-0	14	2	7	Si	>100			

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M-	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	cm	cm	cm	kg/cmq	kg/cmq	mm	mm	mm	mm	mm	mm	mm
0.0	--	52	12.06	12.06	--	--	--	5	14	14	Si	>100			
16.2	--	362	12.06	12.06	--	--	--	33	14	14	Si	>100			
80.8	--	871	12.06	12.06	--	--	--	80	14	14	Si	44.8			
145.5	--	121	12.06	12.06	--	--	--	11	14	14	Si	>100			
161.7	279	--	12.06	12.06	-0	26	--	--	14	14	Si	>100			

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	kg*m	cm	cm	cm	kg/cmq	mm	mm	mm	mm	mm	mm	mm	mm
0.0	19	0.1	12.06	30.16	22.4	2	0.000	0.000	12(Fr)	Si	>100				
0.0	52	0.1	12.06	30.16	22.4	5	0.000	0.000	14(Qp)	Si	>100				
16.2	362	0.1	12.06	30.16	22.4	33	0.002	0.002	14(Qp)	Si	>100				
16.2	341	0.1	12.06	30.16	22.4	31	0.002	0.002	12(Fr)	Si	>100				
80.8	871	0.1	12.06	30.16	22.4	80	0.005	0.005	14(Qp)	Si	58.5				
80.8	871	0.1	12.06	30.16	22.4	80	0.005	0.005	9(Fr)	Si	78.0				
145.5	121	0.1	12.06	30.16	22.4	11	0.001	0.001	14(Qp)	Si	>100				
145.5	110	0.1	12.06	30.16	22.4	10	0.001	0.001	11(Fr)	Si	>100				
161.7	-279	0.1	12.06	30.16	22.4	26	0.002	0.002	14(Qp)	Si	>100				
161.7	-182	0.1	12.06	30.16	22.4	17	0.001	0.001	13(Fr)	Si	>100				

Trave di Fond.: 9004 | 208. 209 | Pilastrate [208. 209]

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln= 149.3 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	M-	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	cm	cm	cm	kg/cmq	kg/cmq	mm	mm	mm	mm	mm	mm	mm
0.0	779	--	12.06	12.06	-1	72	--	--	8	6	Si	50.1			

X	M+	M-	M-	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
16.1	396	--	12.06	12.06	-1	36	--	--	8	6	Si	98.6			
80.6	--	1033	12.06	12.06	--	--	--	95	6	8	Si	37.8			
145.1	--	2200	12.06	12.06	--	--	--	203	6	8	Si	17.8			
161.2	--	2435	12.06	12.06	--	--	--	224	6	8	Si	16.0			

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M-	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	cm	cm	cm	kg/cmq	kg/cmq	mm	mm	mm	mm	mm	mm	mm
0.0	143	--	12.06	12.06	-0	13	--	--	14	14	Si	>100			
16.1	--	34	12.06	12.06	--	--	--	-0	3	14	Si	>100			
80.6	--	535	12.06	12.06	--	--	--	-1	49	14	Si	73.0			
145.1	--	682	12.06	12.06	--	--	--	-1	63	14	Si	57.3			
161.2	--	659	12.06	12.06	--	--	--	-1	61	14	Si	59.3			

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	kg*m	cm	cm	cm	kg/cmq	kg/cmq	mm	mm	mm	mm	mm	mm	mm
0.0	-139	0.1	12.06	30.16	22.4	13	0.001	0.001	12(Fr)	Si	>100				
0.0	-143	0.1	12.06	30.16	22.4	13	0.001	0.001	14(Qp)	Si	>100				
16.1	34	0.1	12.06	30.16	22.4	3	0.000	0.000	14(Qp)	Si	>100				
16.1	27	0.1	12.06	30.16	22.4	2	0.000	0.000	11(Fr)	Si	>100				
80.6	535	0.1	12.06	30.16	22.4	49	0.003	0.003	14(Qp)	Si	95.2				
80.6	514	0.1	12.06	30.16	22.4	47	0.003	0.003	12(Fr)	Si	>100				
145.1	682	0.1	12.06	30.16	22.4	63	0.004	0.004	14(Qp)	Si	74.7				
145.1	601	0.1	12.06	30.16	22.4	55	0.004	0.004	12(Fr)	Si	>100				
161.2	659	0.1	12.06	30.16	22.4	61	0.004	0.004	14(Qp)	Si	77.3				
161.2	561	0.1	12.06	30.16	22.4	52	0.003	0.003	12(Fr)	Si	>100				

Trave di Fond.: 9004 | 209. 210 | Pilastrate [209. 210]

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln= 149.7 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	M-	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	cm	cm	cm	kg/cmq	kg/cmq	mm	mm	mm	mm	mm	mm	mm
0.0	--	1986	12.06	12.06	--	--	--	-3	183	6	8	Si	19.7		
15.0	--	2267	12.06	12.06	--	--	--	-4	209	6	8	Si	17.2		
74.8	--	3129	12.06	12.06	--	--	--	-5	288	6	8	Si	12.5		
134.7	--	3510	12.06	12.06	--	--	--	-5	324	6	8	Si	11.1		
149.7	--	3525	12.06	12.06	--	--	--	-5	325	6	5	Si	11.1		

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M-	Act	Mq	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	cm	cm	cm	kg/cmq	kg/cmq	mm	mm	mm	mm	mm	mm	mm
0.0	--	665	12.06	12.06	--	--	--	-1	61	14	14	Si	58.7		
15.0	--	817	12.06	12.06	--	--	--	-1	75	14	14	Si	47.8		
74.8	--	1199	12.06	12.06	--	--	--	-2	111	14	14	Si	32.6		
134.7	--	1207	12.06	12.06	--	--	--	-2	111	14	14	Si	32.4		
149.7	--	1147	12.06	12.06	--	--	--	-2	106	14	14	Si	34.0		

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	σ _{max}	σ _{max} defined	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cm	cm	kg/cm ²	mm	mm			
0.0	568	0.1	12.06	30.16	22.4	52	0.003	12(Fr)	Si	>100
0.0	665	0.1	12.06	30.16	22.4	61	0.004	14(Qp)	Si	76.6
15.0	817	0.1	12.06	30.16	22.4	75	0.005	14(Qp)	Si	62.3
15.0	697	0.1	12.06	30.16	22.4	64	0.004	12(Fr)	Si	97.4
74.8	1199	0.1	12.06	30.16	22.4	111	0.007	14(Qp)	Si	42.5
74.8	992	0.1	12.06	30.16	22.4	91	0.006	12(Fr)	Si	68.5
134.7	1207	0.1	12.06	30.16	22.4	111	0.007	14(Qp)	Si	42.2
134.7	926	0.1	12.06	30.16	22.4	85	0.005	12(Fr)	Si	73.3
149.7	1147	0.1	12.06	30.16	22.4	79	0.007	14(Qp)	Si	44.4
149.7	832	0.1	12.06	30.16	22.4	106	0.005	12(Fr)	Si	79.7

Verifica aperture fessure:Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	mq	cmq	pAft	S _r max	σ _{med}	Wd	Wk	Cb	Ver.	Cs
cm	kg* ³ m				cm		kg/cmq	mm	mm			
0.0	413	0.1	12.06	30.16	22.4	38	0.002	0.002	0.002	13(Fr)	Si	>100
0.0	558	0.1	12.06	30.16	22.4	51	0.003	0.003	0.003	14(Qp)	Si	91.2
16.2	600	0.1	12.06	30.16	22.4	55	0.004	0.004	0.004	14(Qp)	Si	84.9
16.2	479	0.1	12.06	30.16	22.4	44	0.003	0.003	0.003	13(Fr)	Si	>100
80.8	519	0.1	12.06	30.16	22.4	48	0.003	0.003	0.003	14(Qp)	Si	98.2
80.8	499	0.1	12.06	30.16	22.4	46	0.003	0.003	0.003	13(Fr)	Si	>100
145.5	38	0.1	12.06	30.16	22.4	3	0.000	0.000	0.000	14(Qp)	Si	>100
145.5	31	0.1	12.06	30.16	22.4	3	0.000	0.000	0.000	11(Fr)	Si	>100
161.7	-146	0.1	12.06	30.16	22.4	13	0.001	0.001	0.001	14(Qp)	Si	>100
161.7	-30	0.1	12.06	30.16	22.4	3	0.000	0.000	0.000	13(Fr)	Si	>100

VERIFICHE STATO LIMITE DI ESERCIZIO

Verifica spostamenti laterali delle colonne in acciaio secondo NTC 2008
Scenario di calcolo : Set NT_SLD_A2_STR/GEO

Verifica spostamenti orizzontali relativi di piano (§4.2.4.2.2 - NTC 2008)

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup. mm	SpostY sup. mm	SpostX inf. mm	SpostY inf. mm	δ mm	h/500.00 mm	Verifica
0-1	102 (Nodo 102)	2 (Nodo 2)	6	13.35	3.54	0.00	0.00	13.81	18.07	Si
0-1	103 (Nodo 103)	3 (Nodo 3)	6	13.53	3.60	0.00	0.00	14.00	18.07	Si
0-1	101 (Nodo 101)	1 (Nodo 1)	6	12.54	3.22	0.00	0.00	12.94	18.07	Si
0-1	105 (Nodo 105)	5 (Nodo 5)	6	13.63	3.64	0.00	0.00	14.11	18.07	Si
0-1	106 (Nodo 106)	6 (Nodo 6)	6	13.13	3.55	0.00	0.00	13.60	18.07	Si
0-1	104 (Nodo 104)	4 (Nodo 4)	6	13.58	3.62	0.00	0.00	14.05	18.07	Si
0-1	107 (Nodo 107)	7 (Nodo 7)	6	12.43	3.40	0.00	0.00	12.88	18.07	Si
2-3	308 (Nodo 308)	208 (Nodo 208)	5	-4.18	-2.19	0.00	0.00	4.72	12.40	Si
2-3	309 (Nodo 309)	209 (Nodo 209)	5	-4.51	-2.30	0.00	0.00	5.06	12.40	Si
2-3	310 (Nodo 310)	210 (Nodo 210)	5	-4.65	-2.32	0.00	0.00	5.19	12.40	Si
2-3	311 (Nodo 311)	211 (Nodo 211)	5	-4.79	-2.33	0.00	0.00	5.33	12.40	Si
2-3	312 (Nodo 312)	212 (Nodo 212)	5	-4.93	-2.33	0.00	0.00	5.45	12.40	Si
2-3	313 (Nodo 313)	213 (Nodo 213)	5	-4.99	-2.30	0.00	0.00	5.50	12.40	Si
2-3	314 (Nodo 314)	214 (Nodo 214)	5	-4.90	-2.26	0.00	0.00	5.40	12.40	Si

Verifica spostamenti orizzontali in sommità (§4.2.4.2.2 - NTC 2008)

Nodo	Comb.	SpostX mm	SpostY mm	Δ mm	H/500.00 mm	Verifica
308 (Nodo 308)	5	-4.18	-2.19	4.72	26.46	Si
309 (Nodo 309)	5	-4.51	-2.30	5.06	26.46	Si
310 (Nodo 310)	5	-4.65	-2.32	5.19	26.46	Si
311 (Nodo 311)	5	-4.79	-2.33	5.33	26.46	Si
312 (Nodo 312)	5	-4.93	-2.33	5.45	26.46	Si
313 (Nodo 313)	5	-4.99	-2.30	5.50	26.46	Si
314 (Nodo 314)	5	-4.90	-2.26	5.40	26.46	Si

TABULATI DI INPUT - Portali da 14 a 25

Dati generali		
Nome struttura		
Fattore rigidezza assiale pilastri	1	
Numero di frequenze	45	
% Filtro masse libere	0.1	
% Coefficiente di smorzamento viscoso	5	
Spostamenti nodali con segno	Si	
Deformabilità a taglio delle aste	Si	
Spostamento ammissibile impalcati	0.0050*h	

Impalcati				
N°	Quota	Rigido	Incr.Soll.Pil	Incr.Soll.Par.
0	mm			
1	0	No		1.000
2	4820	No		1.000
3	10050	No		1.000
4	12700	No		1.000

Percentuali Spostamento masse impalcati		
Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0

Combinazioni del Sisma in X e Y e Verticale				
Comb	Pos. SismaX	Pos. SismaY	Fx	Fy
1	1	2	1	0.3
2	1	2	0.3	1
3	1	4	1	0.3
4	1	4	0.3	1
5	3	2	1	0.3
6	3	2	0.3	1
7	3	4	1	0.3
8	3	4	0.3	1
9	2	2	0.3	0.3
10	1	4	0.3	1
11	3	2	0.3	0.3
12	3	4	0.3	0.3

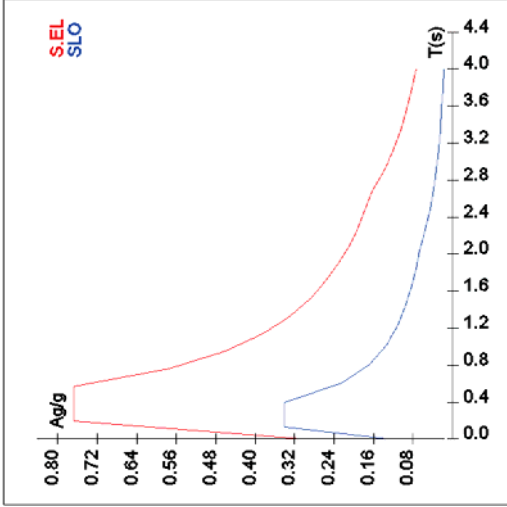
Comb. = Numero di combinazione dei sismi
Pos. SismaX = Posizione in cui viene scelto il sisma in direzione X
Pos. SismaY = Posizione in cui viene scelto il sisma in direzione Y
Fx = Fattore con cui il sisma X partecipa
Fy = Fattore con cui il sisma Y partecipa
Fz = Fattore con cui il sisma Verticale partecipa (quando richiesto)
Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx ed Fy ed Fz

Spettri di risposta

Spetro:SpettroniT(q=1) Il calcolo degli spettri e del fattore di struttura sono stati calcolati per la seguente tipologia di terreno e struttura	
Vita della struttura	
Tipo	Ponti imp. strategica (>100)>=100 anni
Vita nominale(anni)	100.0
Classe d'uso	Classe IV
Coefficiente d'uso	2.000
Periodo di riferimento(anni)	200.000

Stato limite di esercizio - SLO	PVR=81.0%
Stato limite ultimo - SLV	PVR=10.0%
Periodo di ritorno SL0(anni)	TR=120.4
Periodo di ritorno SLV(anni)	TR=1898.2
Parametri del sito	
Comune	Biancavilla - (CT)
Longitudine	14.865
Latitudine	37.646
Id reticolo del sito	47419-47197-47196-47418
Valori di riferimento del sito	
Ag/g(TR=120.4) SLO	0.1103
F0(TR=120.4) SLO	2.5726
T°C(TR=120.4) SLO	0.281
Ag/g(TR=1898.2) SLV	0.2704
F0(TR=1898.2) SLV	2.5180
T°C(TR=1898.2) SLV	0.441
Coefficiente Amplificazione Topografica	SI=1.000
Categoria terreno B	
stato limite SLV	
	S=1.13
	IB=0.19
	IC=0.57
	ID=2.68
stato limite SLO	
	S=1.20
	IB=0.13
	IC=0.40
	ID=2.04
Spettro Elastico	q=I (struttura NON dissipativa)
Smorzamento viscoso %	5.0

T	EL	EL	TSLO	SILO
0.00000	0.30491	0.00000	0.00000	0.13236
0.19040	0.76776	0.13299	0.13299	0.34050
0.57119	0.76776	0.39896	0.39896	0.34050
0.76304	0.57472	0.60424	0.22482	0.22482
0.95489	0.45925	0.80952	0.16781	0.16781
1.14675	0.38242	1.01479	0.13387	0.13387
1.33860	0.32761	1.22007	0.11134	0.11134
1.53045	0.28654	1.42535	0.09531	0.09531
1.72231	0.25462	1.63063	0.08331	0.08331
1.91416	0.22910	1.83591	0.07399	0.07399
2.10602	0.20823	2.04119	0.06655	0.06655
2.29787	0.19084	2.25883	0.05435	0.05435
2.48972	0.17614	2.47648	0.04521	0.04521
2.68158	0.16354	2.69412	0.03820	0.03820
2.90131	0.13970	2.91177	0.03270	0.03270
3.12105	0.12072	3.12942	0.02831	0.02831
3.34079	0.10537	3.34706	0.02475	0.02475
3.56053	0.09276	3.56471	0.02182	0.02182
3.78026	0.08229	3.78235	0.01938	0.01938
4.00000	0.07350	4.00000	0.01733	0.01733



Caratteristiche del terreno											
Terreno1- Cost Winkler=10.00 kg/cm²											
Falda assente											
Strato n°	Spessore cm	γ kg/mc	γSat kg/mc	φ °	Addensato	OCR	Coesione kg/cm²	Cu kg/cm²	E kg/cm²	v	
1	100	1900	1900	35	No	--	0.00	0.00	2E02	0.30	
Materiali											
Materiale: C25/30											
Peso specifico		kg/mc									
Modulo di Young E		3E05									
Modulo di Poisson ν		0.13									
Coefficiente di dilatazione termica λ		1/°C									
Materiale: Acciaio											
Peso specifico		kg/mc									
Modulo di Young E		2E06									
Modulo di Poisson ν		0.30									
Coefficiente di dilatazione termica λ		1/°C									

Nodi - Geometria e vincoli											
Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Vincoli	Impalcato
1		0	10050	1	1	0	0	0	1		2
1	10540	2370	0	1	1	0	0	0	1		0
1	8191	6232	0	0	0	0	0	0	0		1
2	7192	5824	7690	0	0	0	0	0	0		1
2	10170	3820	0	1	1	0	0	0	1		0
2	-220	870	10050	1	1	0	0	0	1		2
3	9720	5250	0	1	1	0	0	0	1		0
3	6193	5416	9000	0	0	0	0	0	0		1
3	-490	1720	10050	1	1	0	0	0	1		2
4	9190	6640	0	1	1	0	0	0	1		0
4	5832	11593	6280	0	0	0	0	0	0		1
4	-800	2560	10050	1	1	0	0	0	1		2

[illegible][illegible]

[illegible][illegible]

75	Vento X	-0	0	0	-0	-0				
75	Vento X	0	0	0	-0	-0				
76	QP Sotai	0	0	0	0	0				
76	QV Sotai	0	0	0	0	0				
76	Nave	0	0	0	0	0				
76	Nave	-0	0	0	0	0				
76	Vento X	0	0	0	0	0				
76	Vento X	-0	0	0	0	0				
80	QP Sotai	0	0	0	0	0				
80	QV Sotai	0	0	0	0	0				
80	Nave	0	0	0	0	0				
80	Nave	0	0	0	0	0				
80	Vento X	0	0	0	0	0				
80	Vento X	0	0	0	0	0				
85	QP Sotai	0	0	0	-0	-0				
85	QV Sotai	0	-0	0	-0	-0				
85	Nave	-0	0	0	-0	-0				
85	Nave	0	0	0	-0	-0				
85	Vento X	0	-0	0	-0	-0				
85	Vento X	-0	0	0	-0	-0				

Input - Aste - Tabella sezioni tipo

Tipo	Nome	Raggio
C		cm
	Fi18	l
	Fi16	l

Tiplo	Nome	Area	I _x	I _y	I _t	F _x	F _y	L _x	L _y
G		m ²	m ⁴	m ⁴	m ⁴			cm	cm
	IPE 100	0.0	1.710E-06	1.592E-07	8.826E-09	1.000	1.000	6	10
	HE 240 A	0.0	7.763E-05	2.769E-05	4.155E-07	1.000	1.000	24	23

Nome	Base	Altezza	Largez. mag.
R	cm	cm	cm
F60x100	60	100	120

Aste - Geometria e vincoli

Aste - Geometria e vincoli

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	x1	y1	z1	xf	yf	zf	Tipo	L2	L3	cm	
	1	1	28	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	211	211	cm
	1	28	12	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	271	271	
	2	2	25	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	106	5050	0	0	0	0	0	0	0	Pila	211	211	
	2	25	13	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	106	5050	0	0	0	0	0	0	0	Pila	271	271	
	3	3	27	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	109	5050	0	0	0	0	0	0	0	Pila	211	211	
	3	27	14	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	109	5050	0	0	0	0	0	0	0	Pila	271	271	
	4	4	25	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	211	211	
	4	25	15	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	271	271	
	5	5	29	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	211	211	
	5	29	16	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	271	271	
	6	6	30	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	211	211	
	6	30	17	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	271	271	
	7	7	24	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	211	211	
	7	24	18	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	271	271	
	8	8	26	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	119	5050	0	0	0	0	0	0	0	Pila	211	211	
	8	26	19	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	119	5050	0	0	0	0	0	0	0	Pila	271	271	
	9	9	31	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	211	211	
	9	31	20	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	271	271	
	10	10	32	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	125	5050	0	0	0	0	0	0	0	Pila	211	211	
	10	32	21	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	125	5050	0	0	0	0	0	0	0	Pila	271	271	
	11	11	33	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	128	5050	0	0	0	0	0	0	0	Pila	211	211	
	11	33	22	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	128	5050	0	0	0	0	0	0	0	Pila	271	271	
	12	12	2	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	128	5050	0	0	0	0	0	0	0	Pila	265	265	
	12	2	13	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	128	5050	0	0	0	0	0	0	0	Pila	265	265	
	13	13	21	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	128	5050	0	0	0	0	0	0	0	Pila	265	265	
	13	21	14	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	128	5050	0	0	0	0	0	0	0	Pila	265	265	
	14	14	9	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	265	265	
	14	9	10	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	265	265	
	15	15	11	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	265	265	
	15	11	22	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	265	265	
	16	16	7	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	265	265	
	16	7	17	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	265	265	
	17	17	6	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	265	265	
	17	6	17	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	265	265	
	18	18	5	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	265	265	
	18	5	16	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	265	265	
	19	19	4	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	265	265	
	19	4	15	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	265	265	
	20	20	3	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	109	5050	0	0	0	0	0	0	0	Pila	265	265	
	20	3	14	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	109	5050	0	0	0	0	0	0	0	Pila	265	265	
	21	21	12	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	265	265	
	21	12	11	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	265	265	
	22	22	11	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	265	265	
	22	11	22	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	265	265	
	23	23	10	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	265	265	
	23	10	39	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	265	265	
	24	24	40	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	265	265	
	24	40	11	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	265	265	
	25	25	39	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	265	265	
	25	39	40	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	265	265	
	26	26	37	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	265	265	
	26	37	41	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	103	5050	0	0	0	0	0	0	0	Pila	265	265	
	27	27	38	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	-4	0	2	Trave	123	123	
	27	38	14	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	-4	0	2	Trave	134	134	
	28	28	36	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	28	36	37	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	29	29	36	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	29	36	37	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	30	30	40	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	113	113	
	30	40	11	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	113	113	
	31	31	38	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	123	123	
	31	38	14	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	134	134	
	32	32	37	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	32	37	41	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	33	33	36	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	33	36	37	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	34	34	40	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	113	113	
	34	40	11	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	113	113	
	35	35	38	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	123	123	
	35	38	14	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	134	134	
	36	36	37	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	36	37	41	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	37	37	36	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	37	36	37	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	38	38	40	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	113	113	
	38	40	11	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	113	113	
	39	39	38	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	123	123	
	39	38	14	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	0	-4	0	-1	0	-4	0	Trave	134	134	
	40	40	37	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	40	37	41	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	41	41	36	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	41	36	37	-I- HE 240 A	Acciaio	Acciaio Pressiflessione	0	0000	2	-4	0	-1	0	-4	0	Trave	148	148	
	42	42																	

8000	1	35	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	4	0	-2	0	0	0	-1	Trave	159	159
8000	8	9	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	6	-4	-4	0	0	0	-2	Trave	170	170
8000	12	7	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	7	0	-5	0	0	0	-4	Trave	178	178
8000	17	8	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5800	0	0	-1	0	0	0	-5	Trave	182	182
8001	45	46	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5055	0	0	-4	0	0	0	-4	Trave	111	111
8001	44	45	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	108	108
8001	43	44	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	113	113
8001	42	43	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	123	123
8001	41	42	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	134	134
8001	40	41	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	148	148
8001	12	11	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	158	158
8001	11	12	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	170	170
8001	10	11	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	178	178
8001	9	10	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5550	0	0	0	0	0	0	0	Trave	182	182
8002	52	14	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5055	0	0	0	0	0	0	0	Trave	111	111
8002	51	52	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	108	108
8002	50	51	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	113	113
8002	49	50	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	123	123
8002	48	49	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	134	134
8002	15	14	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	148	148
8002	14	15	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	159	159
8002	13	14	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	170	170
8002	12	13	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5550	0	0	0	0	0	0	0	Trave	178	178
8003	28	28	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5055	0	0	-4	0	0	0	-4	Trave	182	182
8003	27	27	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	111	111
8003	26	27	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	108	108
8003	25	26	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	113	113
8003	24	25	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	123	123
8003	23	24	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	134	134
8003	22	23	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	148	148
8003	2	3	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	158	158
8003	1	2	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	170	170
8003	15	1	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5550	0	0	0	0	0	0	0	Trave	178	178
8004	64	16	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5055	0	0	0	0	0	0	0	Trave	182	182
8004	63	17	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	111	111
8004	62	18	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	108	108
8004	61	19	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	113	113
8004	60	20	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	123	123
8004	59	21	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	134	134
8004	58	22	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	148	148
8004	21	21	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	159	159
8004	19	21	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	170	170
8004	16	19	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5550	0	0	0	0	0	0	0	Trave	178	178
8004	5	17	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0058	7	0	-5	-1	0	0	1	Trave	182	182
8005	57	58	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	7	0	-4	0	0	0	-5	Trave	108	108
8005	56	57	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	6	0	-5	0	0	0	-5	Trave	113	113
8005	55	56	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	5	0	-4	0	0	0	-4	Trave	123	123
8005	54	55	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	4	0	-3	0	0	0	-4	Trave	134	134
8005	53	54	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	3	0	-2	0	0	0	-3	Trave	148	148
8005	18	53	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	2	0	-2	0	0	0	-2	Trave	158	158
8005	17	54	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	2	0	-1	0	0	0	-2	Trave	170	170
8005	16	17	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	0000	1	0	0	0	0	0	-1	Trave	178	178
8005	15	16	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5900	0	0	0	0	0	0	0	Trave	182	182
8006	70	22	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5055	0	0	-4	0	0	0	-4	Trave	111	111
8006	69	21	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	108	108
8006	68	69	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	113	113
8006	67	68	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	123	123
8006	66	67	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	134	134
8006	65	66	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	148	148
8006	24	24	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	159	159
8006	22	23	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	170	170
8006	18	22	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5550	0	0	0	0	0	0	0	Trave	178	178
8007	34	18	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5055	0	0	0	0	0	0	0	Trave	182	182
8007	33	14	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	111	111
8007	32	33	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	108	108
8007	31	34	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	113	113
8007	30	31	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	123	123
8007	29	30	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	134	134
8007	6	29	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	148	148
8007	5	6	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	158	158
8007	4	5	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	170	170
8007	19	19	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5550	0	0	0	0	0	0	0	Trave	178	178
8008	75	76	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5055	0	0	0	0	0	0	0	Trave	182	182
8008	74	75	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	108	108
8008	73	74	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	113	113
8008	72	73	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	123	123
8008	71	72	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	134	134
8008	70	71	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	148	148
8008	26	27	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	158	158
8008	25	26	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	170	170
8008	20	25	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5550	0	0	0	0	0	0	0	Trave	178	178
8009	82	20	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	182	182
8009	81	82	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	108	108
8009	80	81	I-1	HE 240 A	Aciano	Aciano Pressilessione	0	5050	0	0	-4	0	0	0	-4	Trave	111	111

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	OZi	Xf	QXf	OYf	OZf
HE 240 A	32	21	Vento X	UnitG	0	255	0	0	271	255	0	0
HE 240 A	32	21	Vento Y	UnitG	0	-128	0	0	271	-128	0	0
Piastro 11												
HE 240 A	11	33	Peso Proprio	UnitG	0	0	0	60	211	0	0	60
HE 240 A	11	33	Vento X	UnitG	0	255	0	0	211	255	0	0
HE 240 A	11	33	Vento Y	UnitG	0	-128	0	0	211	-128	0	0
HE 240 A	33	22	Peso Proprio	UnitG	0	0	0	60	271	0	0	60
HE 240 A	33	22	Vento X	UnitG	0	255	0	0	271	255	0	0
HE 240 A	33	22	Vento Y	UnitG	0	-128	0	0	271	-128	0	0
Piastro 12												
HE 240 A	2	13	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	2	13	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	2	13	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Piastro 13												
HE 240 A	10	21	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	10	21	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	10	21	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Piastro 14												
HE 240 A	9	20	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	9	20	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	9	20	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Piastro 15												
HE 240 A	8	19	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	8	19	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	8	19	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Piastro 16												
HE 240 A	7	18	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	7	18	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	7	18	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Piastro 17												
HE 240 A	6	17	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	6	17	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	6	17	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Piastro 18												
HE 240 A	5	16	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	5	16	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	5	16	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Piastro 19												
HE 240 A	4	15	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	4	15	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	4	15	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Piastro 20												
HE 240 A	3	14	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	3	14	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	3	14	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Piastro 21												
HE 240 A	1	12	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	1	12	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	1	12	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Piastro 22												
HE 240 A	11	22	Peso Proprio	UnitG	0	0	0	60	265	0	0	60
HE 240 A	11	22	Vento X	UnitG	0	128	0	0	265	128	0	0
HE 240 A	11	22	Vento Y	UnitG	0	-255	0	0	265	-255	0	0
Trave 8000												
HE 240 A	7	8	Peso Proprio	UnitG	0	0	0	60	170	0	0	60
HE 240 A	7	8	QP Solai	PolG	0	0	0	2	18	0	0	58
HE 240 A	7	8	QP Solai	PolG	18	0	0	58	178	0	0	54
HE 240 A	7	8	QV Solai	PolG	0	0	0	1	18	0	0	19
HE 240 A	7	8	QV Solai	PolG	18	0	0	19	178	0	0	17
HE 240 A	7	8	Neve	PolG	0	0	0	1	18	0	0	36
HE 240 A	7	8	Vento X	PolG	18	0	0	36	178	0	0	34
HE 240 A	7	8	Vento X	PolG	0	0	0	2	18	0	0	56
HE 240 A	8	9	Peso Proprio	UnitG	0	0	0	56	178	0	0	52
HE 240 A	8	9	QP Solai	PolG	0	0	0	60	164	0	0	60
HE 240 A	8	9	QP Solai	PolG	0	0	0	2	16	0	0	55

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	OZi	Xf	QXf	OYf	OZf
HE 240 A	8	9	QV Solai	PolG	0	0	0	0	1	16	0	0
HE 240 A	8	9	Neve	PolG	16	0	0	0	18	170	0	0
HE 240 A	8	9	Vento X	PolG	0	0	0	0	1	16	0	0
HE 240 A	8	9	Vento X	PolG	0	0	0	0	2	16	0	0
HE 240 A	9	35	Peso Proprio	UnitG	0	0	0	60	155	0	0	50
HE 240 A	9	35	QP Solai	PolG	0	0	0	2	14	0	0	53
HE 240 A	9	35	QP Solai	PolG	14	0	0	53	159	0	0	49
HE 240 A	9	35	QV Solai	PolG	0	0	0	1	14	0	0	17
HE 240 A	9	35	Neve	PolG	14	0	0	17	159	0	0	16
HE 240 A	9	35	Vento X	PolG	14	0	0	33	159	0	0	31
HE 240 A	12	7	Peso Proprio	UnitG	0	0	0	60	175	0	0	60
HE 240 A	12	7	QP Solai	PolG	0	0	0	2	19	0	0	60
HE 240 A	12	7	QV Solai	PolG	19	0	0	60	182	0	0	56
HE 240 A	12	7	Neve	PolG	0	0	0	1	19	0	0	19
HE 240 A	12	7	Neve	PolG	0	0	0	1	19	0	0	37
HE 240 A	12	7	Vento X	PolG	0	0	0	37	182	0	0	35
HE 240 A	35	36	Peso Proprio	UnitG	19	0	0	58	182	0	0	58
HE 240 A	35	36	QP Solai	PolG	0	0	0	60	146	0	0	60
HE 240 A	35	36	QP Solai	PolG	0	0	0	2	13	0	0	51
HE 240 A	35	36	Vento X	PolG	13	0	0	51	148	0	0	47
HE 240 A	35	36	QV Solai	PolG	0	0	0	1	13	0	0	16
HE 240 A	35	36	Neve	PolG	13	0	0	16	148	0	0	15
HE 240 A	36	37	Peso Proprio	UnitG	0	0	0	2	11	0	0	48
HE 240 A	36	37	QP Solai	PolG	0	0	0	48	134	0	0	45
HE 240 A	36	37	QP Solai	PolG	11	0	0	48	134	0	0	16
HE 240 A	36	37	QV Solai	PolG	0	0	0	1	11	0	0	14
HE 240 A	36	37	Neve	PolG	0	0	0	16	134	0	0	14
HE 240 A	36	37	Vento X	PolG	0	0	0	30	134	0	0	30
HE 240 A	36	37	Vento X	PolG	0	0	0	2	11	0	0	47
HE 240 A	37	38	Peso Proprio	UnitG	0	0	0	60	119	0	0	43
HE 240 A	37	38	QP Solai	PolG	0	0	0	2	10	0	0	60
HE 240 A	37	38	QP Solai	PolG	10	0	0	46	123	0	0	42
HE 240 A	37	38	QV Solai	PolG	0	0	0	1	10	0	0	15
HE 240 A	37	38	Neve	PolG	10	0	0	15	123	0	0	14
HE 240 A	37	38	Neve	PolG	0	0	0	1	10	0	0	29
HE 240 A	37	38	Vento X	PolG	10	0	0	29	123	0	0	26
HE 240 A	37	38	Vento X	PolG	0	0	0	2	10	0	0	44
HE 240 A	38	39	Peso Proprio	UnitG	0	0	0	60	108	0	0	60
HE 240 A	38	39	QP Solai	PolG	0	0	0	2	8	0	0	44
HE 240 A	38	39	QP Solai	PolG	8	0	0	44	113	0	0	40
HE 240 A	38	39	QV Solai	PolG	0	0	0	1	8	0	0	14
HE 240 A	38	39	Neve	PolG	8	0	0	14	113	0	0	13
HE 240 A	38	39	Neve	PolG	0	0	0	1	8	0	0	27
HE 240 A	38	39	Vento X	PolG	8	0	0	27	113	0	0	25
HE 240 A	39	40	Peso Proprio	UnitG	8	0	0	42	113	0	0	42
HE 240 A	39	40	QP Solai	PolG	0	0	0	60	101	0	0	38
HE 240 A	39	40	QP Solai	PolG	0	0	0	2	8	0	0	60
HE 240 A	39	40	QV Solai	PolG	8	0	0	41	108	0	0	37
HE 240 A	39	40	QV Solai	PolG	0	0	0	1	8	0	0	13
HE 240 A	39	40	Neve	PolG	8	0	0	13	108	0	0	12

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	39	40	Vento X	PolG	8	0	0	26	108	0	0	23
HE 240 A	40	12	Peso Proprio	UnifG	8	0	0	40	108	0	0	36
HE 240 A	40	12	Qp Solai	PolG	0	0	0	60	100	0	0	60
HE 240 A	40	12			7	0	0	39	111	0	0	35
HE 240 A	40	12	QV Solai	PolG	7	0	0	1	7	0	0	13
HE 240 A	40	12	Neve	PolG	7	0	0	13	111	0	0	11
HE 240 A	40	12			7	0	0	1	7	0	0	24
HE 240 A	40	12	Vento X	PolG	7	0	0	24	111	0	0	22
HE 240 A	40	12			7	0	0	2	7	0	0	38
HE 240 A	40	12			7	0	0	38	111	0	0	34
Trave 8001												
HE 240 A	10	11	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	10	11	Qp Solai	PolG	31	0	0	116	161	0	0	116
HE 240 A	10	11	QV Solai	PolG	161	0	0	112	178	0	0	58
HE 240 A	10	11			31	0	0	37	161	0	0	36
HE 240 A	10	11	Neve	PolG	161	0	0	35	161	0	0	36
HE 240 A	10	11	Neve	PolG	161	0	0	3	31	0	0	37
HE 240 A	10	11	Vento X	PolG	0	0	0	54	161	0	0	55
HE 240 A	10	11	Vento X	PolG	161	0	0	55	178	0	0	4
HE 240 A	10	11			31	0	0	57	178	0	0	52
HE 240 A	11	12	Peso Proprio	UnifG	0	0	0	60	170	0	0	60
HE 240 A	11	12	Qp Solai	PolG	28	0	0	111	154	0	0	108
HE 240 A	11	12	QV Solai	PolG	154	0	0	33	154	0	0	34
HE 240 A	11	12	Neve	PolG	28	0	0	36	154	0	0	36
HE 240 A	11	12	Neve	PolG	154	0	0	34	170	0	0	18
HE 240 A	11	12	Vento X	PolG	0	0	0	3	28	0	0	36
HE 240 A	11	12	Vento X	PolG	28	0	0	4	28	0	0	55
HE 240 A	11	12	Vento X	PolG	28	0	0	55	170	0	0	50
HE 240 A	12	41	Peso Proprio	UnifG	0	0	0	60	158	0	0	60
HE 240 A	12	41	Qp Solai	PolG	25	0	0	106	145	0	0	103
HE 240 A	12	41	QV Solai	PolG	145	0	0	103	158	0	0	54
HE 240 A	12	41			25	0	0	18	25	0	0	34
HE 240 A	12	41	Neve	PolG	0	0	0	3	25	0	0	34
HE 240 A	12	41	Vento X	PolG	145	0	0	49	145	0	0	51
HE 240 A	12	41	Vento X	PolG	145	0	0	51	158	0	0	4
HE 240 A	12	41			25	0	0	53	158	0	0	47
HE 240 A	13	10	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	13	10	Qp Solai	PolG	33	0	0	120	163	0	0	117
HE 240 A	13	10	QV Solai	PolG	163	0	0	20	33	0	0	39
HE 240 A	13	10			33	0	0	39	163	0	0	19
HE 240 A	13	10	Neve	PolG	163	0	0	36	163	0	0	37

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	13	10	Neve	PolG	163	0	0	37	182	0	0	3
HE 240 A	13	10	Vento X	PolG	33	0	0	39	182	0	0	35
HE 240 A	13	10	Vento X	PolG	33	0	0	60	182	0	0	54
HE 240 A	13	10	Vento X	PolG	163	0	0	56	163	0	0	58
HE 240 A	41	42	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	41	42	Qp Solai	PolG	23	0	0	53	23	0	0	98
HE 240 A	41	42	QV Solai	PolG	136	0	0	98	148	0	0	51
HE 240 A	41	42			23	0	0	33	136	0	0	31
HE 240 A	41	42	Neve	PolG	136	0	0	31	148	0	0	3
HE 240 A	41	42	Vento X	PolG	23	0	0	33	148	0	0	29
HE 240 A	41	42	Vento X	PolG	23	0	0	51	148	0	0	45
HE 240 A	41	42	Vento X	PolG	136	0	0	47	136	0	0	49
HE 240 A	42	43	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	42	43	Qp Solai	PolG	20	0	0	51	20	0	0	97
HE 240 A	42	43	QV Solai	PolG	124	0	0	93	124	0	0	49
HE 240 A	42	43			20	0	0	16	20	0	0	31
HE 240 A	42	43	Neve	PolG	124	0	0	31	124	0	0	30
HE 240 A	42	43	Vento X	PolG	124	0	0	45	124	0	0	46
HE 240 A	42	43	Vento X	PolG	124	0	0	4	20	0	0	48
HE 240 A	43	44	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	43	44	Qp Solai	PolG	17	0	0	92	113	0	0	89
HE 240 A	43	44	QV Solai	PolG	113	0	0	89	123	0	0	46
HE 240 A	43	44			17	0	0	16	17	0	0	30
HE 240 A	43	44	Vento X	PolG	113	0	0	29	123	0	0	3
HE 240 A	43	44	Vento X	PolG	17	0	0	4	17	0	0	46
HE 240 A	43	44	Vento X	PolG	17	0	0	42	113	0	0	41
HE 240 A	43	44	Vento X	PolG	113	0	0	44	123	0	0	4
HE 240 A	44	45	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	44	45	Qp Solai	PolG	15	0	0	88	105	0	0	84
HE 240 A	44	45	QV Solai	PolG	105	0	0	15	15	0	0	28
HE 240 A	44	45			15	0	0	28	105	0	0	27
HE 240 A	44	45	Neve	PolG	105	0	0	26	105	0	0	27
HE 240 A	44	45	Neve	PolG	105	0	0	27	113	0	0	3
HE 240 A	44	45	Vento X	PolG	15	0	0	28	113	0	0	25
HE 240 A	44	45	Vento X	PolG	105	0	0	40	105	0	0	42
HE 240 A	44	45	Vento X	PolG	105	0	0	4	15	0	0	44

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	45	46	Peso Proprio QP Solai	UnifG	15	0	0	44	113	0	0	38
	45	46		PolG	0	0	0	60	108	0	0	60
					13	0	0	44	13	0	0	83
					101	0	0	83	101	0	0	79
HE 240 A	45	46	QV Solai	PolG	0	0	0	79	108	0	0	42
					13	0	0	14	13	0	0	27
					101	0	0	25	108	0	0	13
HE 240 A	45	46	Neve	PolG	0	0	0	25	101	0	0	26
					101	0	0	26	108	0	0	3
HE 240 A	45	46	Neve	PolG	0	0	0	3	13	0	0	27
					13	0	0	27	108	0	0	23
HE 240 A	45	46	Vento X	PolG	0	0	0	38	101	0	0	40
					101	0	0	40	108	0	0	4
HE 240 A	45	46	Vento X	PolG	0	0	0	4	13	0	0	42
					13	0	0	42	108	0	0	36
HE 240 A	46	13	Peso Proprio QP Solai	UnifG	0	0	0	60	111	0	0	60
HE 240 A	46	13		PolG	0	0	0	41	13	0	0	78
				13	0	0	78	104	0	0	74	
					104	0	0	74	111	0	0	39
HE 240 A	46	13	QV Solai	PolG	0	0	0	13	13	0	0	25
					13	0	0	25	104	0	0	24
					104	0	0	24	111	0	0	13
HE 240 A	46	13	Neve	PolG	0	0	0	23	104	0	0	24
					104	0	0	24	111	0	0	3
HE 240 A	46	13	Neve	PolG	0	0	0	3	13	0	0	25
					13	0	0	25	111	0	0	22
HE 240 A	46	13	Vento X	PolG	0	0	0	36	104	0	0	38
					104	0	0	38	111	0	0	4
HE 240 A	46	13	Vento X	PolG	0	0	0	4	13	0	0	39
					13	0	0	39	111	0	0	34
Trave 8002												
HE 240 A	13	14	Peso Proprio QP Solai	UnifG	0	0	0	60	178	0	0	60
HE 240 A	13	14		PolG	0	0	0	62	45	0	0	118
					45	0	0	118	148	0	0	115
HE 240 A	13	14	QV Solai	PolG	0	0	0	115	178	0	0	61
					45	0	0	20	45	0	0	38
					148	0	0	37	148	0	0	37
HE 240 A	13	14	Neve	PolG	0	0	0	35	148	0	0	37
					148	0	0	37	178	0	0	4
HE 240 A	13	14	Neve	PolG	0	0	0	4	45	0	0	38
					45	0	0	38	148	0	0	37
HE 240 A	13	14	Vento X	PolG	0	0	0	54	148	0	0	57
					148	0	0	57	178	0	0	6
HE 240 A	13	14	Vento X	PolG	0	0	0	6	45	0	0	58
					45	0	0	58	178	0	0	52
HE 240 A	14	13	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	14	15		UnifG	0	0	0	60	170	0	0	60
HE 240 A	14	13	QP Solai	PolG	0	0	0	65	48	0	0	122
					48	0	0	122	150	0	0	119
HE 240 A	14	15	QP Solai	PolG	0	0	0	119	182	0	0	63
					150	0	0	119	182	0	0	63
HE 240 A	14	15	QV Solai	PolG	0	0	0	60	41	0	0	113
					41	0	0	113	142	0	0	110
HE 240 A	14	13	QV Solai	PolG	0	0	0	110	170	0	0	58
					48	0	0	21	48	0	0	39
HE 240 A	14	15	QV Solai	PolG	0	0	0	39	150	0	0	38
					150	0	0	38	182	0	0	20
HE 240 A	14	15	QV Solai	PolG	0	0	0	19	41	0	0	36
					41	0	0	36	142	0	0	35
HE 240 A	14	13	Neve	PolG	0	0	0	35	170	0	0	19
					150	0	0	38	150	0	0	38
HE 240 A	14	13	Neve	PolG	0	0	0	36	182	0	0	4
					48	0	0	4	48	0	0	39
HE 240 A	14	15	Neve	PolG	0	0	0	33	142	0	0	35

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	14	15	Neve	PolG	142	0	0	35	170	0	0	4
					0	0	0	4	41	0	0	36
HE 240 A	14	15	Vento X	PolG	41	0	0	36	170	0	0	32
					0	0	0	6	41	0	0	56
HE 240 A	14	13	Vento X	PolG	41	0	0	56	170	0	0	50
					0	0	0	6	48	0	0	61
HE 240 A	14	15	Vento X	PolG	48	0	0	61	182	0	0	54
					0	0	0	51	142	0	0	55
HE 240 A	14	13	Vento X	PolG	142	0	0	55	170	0	0	6
					0	0	0	56	150	0	0	59
HE 240 A	15	47	Peso Proprio QP Solai	UnifG	150	0	0	59	182	0	0	6
					0	0	0	60	159	0	0	60
HE 240 A	15	47	QV Solai	PolG	36	0	0	58	36	0	0	108
					134	0	0	105	134	0	0	105
HE 240 A	15	47	QV Solai	PolG	36	0	0	19	36	0	0	35
					134	0	0	35	134	0	0	34
HE 240 A	15	47	Neve	PolG	36	0	0	4	36	0	0	35
					0	0	0	35	159	0	0	31
HE 240 A	15	47	Neve	PolG	36	0	0	32	134	0	0	34
					134	0	0	34	159	0	0	4
HE 240 A	15	47	Vento X	PolG	36	0	0	6	36	0	0	54
					0	0	0	54	159	0	0	47
HE 240 A	15	47	Vento X	PolG	36	0	0	49	134	0	0	53
					134	0	0	53	159	0	0	6
HE 240 A	47	48	Peso Proprio QP Solai	UnifG	32	0	0	60	148	0	0	60
HE 240 A	47	48		PolG	32	0	0	55	32	0	0	104
					126	0	0	104	126	0	0	101
HE 240 A	47	48	QV Solai	PolG	32	0	0	18	32	0	0	33
					126	0	0	33	126	0	0	32
HE 240 A	47	48	Neve	PolG	126	0	0	30	126	0	0	33
					126	0	0	33	148	0	0	4
HE 240 A	47	48	Neve	PolG	32	0	0	4	32	0	0	34
					126	0	0	47	126	0	0	29
HE 240 A	47	48	Vento X	PolG	126	0	0	50	148	0	0	50
					0	0	0	6	32	0	0	6
HE 240 A	47	48	Vento X	PolG	32	0	0	52	148	0	0	45
					126	0	0	60	134	0	0	60
HE 240 A	48	49	Peso Proprio QP Solai	UnifG	28	0	0	53	28	0	0	99
HE 240 A	48	49		PolG	28	0	0	99	116	0	0	96
					116	0	0	96	134	0	0	51
HE 240 A	48	49	QV Solai	PolG	28	0	0	17	28	0	0	32
					116	0	0	32	116	0	0	31
HE 240 A	48	49	Neve	PolG	28	0	0	4	28	0	0	32
					0	0	0	32	134	0	0	28
HE 240 A	48	49	Neve	PolG	28	0	0	29	116	0	0	31
					116	0	0	31	134	0	0	4
HE 240 A	48	49	Vento X	PolG	28	0	0	6	28	0	0	50
					0	0	0	50	134	0	0	43
HE 240 A	48	49	Vento X	PolG	116	0	0	44	116	0	0	48
					28	0	0	48	134	0	0	6
HE 240 A	48	49	Peso Proprio QP Solai	UnifG	116	0	0	60	123	0	0	60
HE 240 A	49	50		PolG	116	0	0	51	24	0	0	94
					24	0	0	94	106	0	0	91
HE 240 A	49	50	QV Solai	PolG	106	0	0	91	123	0	0	49
					24	0	0	16	24	0	0	30
HE 240 A	49	50	Neve	PolG	106	0	0	30	106	0	0	29
					106	0	0	29	123	0	0	16
HE 240 A	49	50	Neve	PolG	106	0	0	27	106	0	0	30
					106	0	0	30	123	0	0	4
HE 240 A	49	50	Neve	PolG	106	0	0	4	24	0	0	31

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	49	50	Vento X	PolG	24	0	0	31	123	0	0	26
HE 240 A	49	50	Vento X	PolG	0	0	0	6	24	0	0	48
HE 240 A	49	50	Vento X	PolG	24	0	0	48	123	0	0	41
HE 240 A	50	51	Peso Proprio	UnitG	106	0	0	42	106	0	0	46
HE 240 A	50	51	QV Solai	PolG	0	0	0	46	123	0	0	6
HE 240 A	50	51	QV Solai	PolG	0	0	0	60	113	0	0	60
HE 240 A	50	51	QV Solai	PolG	0	0	0	48	21	0	0	90
HE 240 A	50	51	QV Solai	PolG	21	0	0	90	99	0	0	86
HE 240 A	50	51	QV Solai	PolG	99	0	0	86	113	0	0	47
HE 240 A	50	51	QV Solai	PolG	0	0	0	15	21	0	0	29
HE 240 A	50	51	QV Solai	PolG	21	0	0	29	99	0	0	28
HE 240 A	50	51	QV Solai	PolG	99	0	0	28	113	0	0	15
HE 240 A	50	51	QV Solai	PolG	0	0	0	26	99	0	0	28
HE 240 A	50	51	QV Solai	PolG	99	0	0	28	113	0	0	4
HE 240 A	50	51	QV Solai	PolG	0	0	0	4	21	0	0	29
HE 240 A	50	51	QV Solai	PolG	21	0	0	29	113	0	0	25
HE 240 A	50	51	QV Solai	PolG	0	0	0	6	21	0	0	46
HE 240 A	50	51	QV Solai	PolG	21	0	0	46	113	0	0	38
HE 240 A	50	51	QV Solai	PolG	0	0	0	40	99	0	0	44
HE 240 A	51	52	Peso Proprio	UnitG	99	0	0	44	113	0	0	6
HE 240 A	51	52	QV Solai	PolG	0	0	0	60	108	0	0	60
HE 240 A	51	52	QV Solai	PolG	0	0	0	46	19	0	0	85
HE 240 A	51	52	QV Solai	PolG	19	0	0	85	95	0	0	82
HE 240 A	51	52	QV Solai	PolG	95	0	0	82	108	0	0	44
HE 240 A	51	52	QV Solai	PolG	0	0	0	15	19	0	0	27
HE 240 A	51	52	QV Solai	PolG	19	0	0	27	95	0	0	26
HE 240 A	51	52	QV Solai	PolG	95	0	0	26	108	0	0	14
HE 240 A	51	52	QV Solai	PolG	0	0	0	24	95	0	0	27
HE 240 A	51	52	QV Solai	PolG	95	0	0	27	108	0	0	4
HE 240 A	51	52	QV Solai	PolG	0	0	0	4	19	0	0	28
HE 240 A	51	52	QV Solai	PolG	19	0	0	28	108	0	0	23
HE 240 A	51	52	QV Solai	PolG	0	0	0	38	95	0	0	41
HE 240 A	51	52	QV Solai	PolG	95	0	0	41	108	0	0	6
HE 240 A	51	52	QV Solai	PolG	0	0	0	6	19	0	0	43
HE 240 A	52	14	Peso Proprio	UnitG	19	0	0	43	108	0	0	36
HE 240 A	52	14	QV Solai	PolG	0	0	0	60	111	0	0	60
HE 240 A	52	14	QV Solai	PolG	0	0	0	44	18	0	0	80
HE 240 A	52	14	QV Solai	PolG	18	0	0	80	98	0	0	77
HE 240 A	52	14	QV Solai	PolG	98	0	0	77	111	0	0	42
HE 240 A	52	14	QV Solai	PolG	0	0	0	14	18	0	0	26
HE 240 A	52	14	QV Solai	PolG	18	0	0	26	98	0	0	25
HE 240 A	52	14	QV Solai	PolG	98	0	0	25	111	0	0	13
HE 240 A	52	14	QV Solai	PolG	0	0	0	23	98	0	0	25
HE 240 A	52	14	QV Solai	PolG	98	0	0	25	111	0	0	4
HE 240 A	52	14	QV Solai	PolG	0	0	0	4	18	0	0	27
HE 240 A	52	14	QV Solai	PolG	18	0	0	27	111	0	0	22
HE 240 A	52	14	QV Solai	PolG	0	0	0	35	98	0	0	39
HE 240 A	52	14	QV Solai	PolG	98	0	0	39	111	0	0	6
HE 240 A	52	14	QV Solai	PolG	0	0	0	6	18	0	0	41
HE 240 A	52	14	QV Solai	PolG	18	0	0	41	111	0	0	34
Trave 8003												
HE 240 A	1	2	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	1	2	QV Solai	PolG	0	0	0	64	52	0	0	122
HE 240 A	1	2	QV Solai	PolG	52	0	0	122	134	0	0	121
HE 240 A	1	2	QV Solai	PolG	134	0	0	121	178	0	0	67
HE 240 A	1	2	QV Solai	PolG	0	0	0	21	52	0	0	39
HE 240 A	1	2	QV Solai	PolG	52	0	0	39	134	0	0	39
HE 240 A	1	2	QV Solai	PolG	134	0	0	39	178	0	0	22
HE 240 A	1	2	QV Solai	PolG	0	0	0	34	134	0	0	37
HE 240 A	1	2	QV Solai	PolG	134	0	0	37	178	0	0	6
HE 240 A	1	2	QV Solai	PolG	0	0	0	6	52	0	0	40
HE 240 A	1	2	QV Solai	PolG	52	0	0	40	178	0	0	36
HE 240 A	1	2	QV Solai	PolG	0	0	0	53	134	0	0	58
HE 240 A	1	2	QV Solai	PolG	134	0	0	58	178	0	0	9
HE 240 A	1	2	QV Solai	PolG	0	0	0	9	52	0	0	62
HE 240 A	1	2	QV Solai	PolG	52	0	0	62	178	0	0	56

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	2	3	Peso Proprio QP Solai	UnitG	0	0	0	60	170	0	0	60
	2	3		PolG	0	0	0	62	50	0	0	120
					50	0	0	120	130	0	0	119
HE 240 A			QV Solai	PolG	130	0	0	119	170	0	0	67
	2	3			0	0	0	20	50	0	0	38
					50	0	0	38	130	0	0	38
HE 240 A	2	3	Neve	PolG	130	0	0	38	170	0	0	22
					0	0	0	6	50	0	0	40
					50	0	0	40	170	0	0	36
HE 240 A	2	3	Neve	PolG	0	0	0	33	130	0	0	36
					130	0	0	36	170	0	0	6
					0	0	0	51	130	0	0	56
HE 240 A	2	3	Vento X	PolG	130	0	0	56	170	0	0	9
					0	0	0	9	50	0	0	62
					0	0	0	62	170	0	0	56
HE 240 A	3	23	Peso Proprio QP Solai	UnitG	0	0	0	60	158	0	0	60
	3	23		PolG	0	0	0	60	47	0	0	117
				47	0	0	117	123	0	0	116	
HE 240 A	3	23	QV Solai	PolG	123	0	0	116	158	0	0	67
					0	0	0	19	47	0	0	38
					47	0	0	38	123	0	0	37
HE 240 A	3	23	Neve	PolG	123	0	0	37	158	0	0	22
					0	0	0	31	123	0	0	35
					123	0	0	35	158	0	0	6
HE 240 A	3	23	Vento X	PolG	0	0	0	6	47	0	0	40
					47	0	0	40	158	0	0	36
					0	0	0	49	123	0	0	54
HE 240 A	3	23	Vento X	PolG	123	0	0	54	158	0	0	9
					0	0	9	47	0	0	62	
					47	0	0	62	158	0	0	56
HE 240 A	15	1	Peso Proprio QP Solai	UnitG	0	0	0	60	182	0	0	60
	15	1		PolG	0	0	0	67	53	0	0	124
					53	0	0	124	135	0	0	123
HE 240 A	15	1	QV Solai	PolG	135	0	0	123	182	0	0	67
					0	0	0	21	53	0	0	40
					53	0	0	40	135	0	0	39
HE 240 A	15	1	Neve	PolG	135	0	0	39	182	0	0	22
					0	0	0	6	53	0	0	40
					53	0	0	40	182	0	0	36
HE 240 A	15	1	Neve	PolG	0	0	0	36	135	0	0	39
					135	0	0	39	182	0	0	6
					0	0	0	9	53	0	0	62
HE 240 A	15	1	Vento X	PolG	53	0	0	62	182	0	0	56
					0	0	0	55	135	0	0	60
					135	0	0	60	182	0	0	9
HE 240 A	23	24	Peso Proprio QP Solai	UnitG	0	0	0	60	148	0	0	60
	23	24		PolG	0	0	0	57	44	0	0	115
				44	0	0	115	117	0	0	114	
HE 240 A	23	24	QV Solai	PolG	117	0	0	114	148	0	0	67
					0	0	0	18	44	0	0	37
					44	0	0	37	117	0	0	36
HE 240 A	23	24	Neve	PolG	117	0	0	36	148	0	0	22
					0	0	0	6	44	0	0	40
					44	0	0	40	148	0	0	36
HE 240 A	23	24	Neve	PolG	0	0	0	30	117	0	0	33
					117	0	0	33	148	0	0	6
					0	0	0	46	117	0	0	52
HE 240 A	23	24	Vento X	PolG	117	0	0	52	148	0	0	9
					0	0	0	9	44	0	0	62
					44	0	0	62	148	0	0	56
HE 240 A	24	25	Peso Proprio QP Solai	UnitG	0	0	0	60	134	0	0	60
	24	25		PolG	0	0	0	55	40	0	0	113
				40	0	0	113	108	0	0	112	
HE 240 A	24	25	QV Solai	PolG	108	0	0	112	134	0	0	67
					0	0	0	18	40	0	0	36
					40	0	0	36	108	0	0	36

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	17	18	Vento X	PolG	0	0	0	9	53	0	0	58
HE 240 A	18	53	Peso Proprio	UnifG	53	0	0	58	170	0	0	50
HE 240 A	18	53	QP Solai	PolG	0	0	0	60	156	0	0	60
					47	0	0	67	47	0	0	119
								119	111	0	0	118
HE 240 A	18	53	QV Solai	PolG	111	0	0	118	158	0	0	59
					0	0	0	22	47	0	0	38
					47	0	0	38	111	0	0	38
HE 240 A	18	53	Neve	PolG	111	0	0	38	158	0	0	19
					0	0	0	6	47	0	0	36
HE 240 A	18	53	Neve	PolG	47	0	0	36	158	0	0	31
					0	0	0	36	111	0	0	40
HE 240 A	18	53	Neve	PolG	111	0	0	40	158	0	0	6
HE 240 A	18	53	Vento X	PolG	0	0	0	9	47	0	0	56
					47	0	0	56	158	0	0	48
HE 240 A	18	53	Vento X	PolG	111	0	0	62	158	0	0	62
					0	0	0	6	158	0	0	9
HE 240 A	53	54	Peso Proprio	UnifG	0	0	0	60	145	0	0	60
HE 240 A	53	54	QP Solai	PolG	0	0	0	67	42	0	0	116
					42	0	0	116	103	0	0	115
					103	0	0	115	148	0	0	56
HE 240 A	53	54	QV Solai	PolG	0	0	0	22	42	0	0	37
					42	0	0	37	103	0	0	37
					103	0	0	37	148	0	0	18
HE 240 A	53	54	Neve	PolG	0	0	0	6	42	0	0	35
					42	0	0	35	148	0	0	29
HE 240 A	53	54	Neve	PolG	0	0	0	36	103	0	0	40
					103	0	0	40	148	0	0	6
HE 240 A	53	54	Vento X	PolG	0	0	0	56	103	0	0	62
					103	0	0	62	148	0	0	9
HE 240 A	53	54	Vento X	PolG	0	0	0	9	42	0	0	53
					42	0	0	53	148	0	0	46
HE 240 A	54	55	Peso Proprio	UnifG	0	0	0	60	130	0	0	60
HE 240 A	54	55	QP Solai	PolG	0	0	0	67	37	0	0	114
					37	0	0	114	94	0	0	113
					94	0	0	113	134	0	0	54
HE 240 A	54	55	QV Solai	PolG	0	0	0	22	37	0	0	37
					37	0	0	37	94	0	0	36
					94	0	0	36	134	0	0	17
HE 240 A	54	55	Neve	PolG	0	0	0	36	94	0	0	40
					94	0	0	40	134	0	0	6
HE 240 A	54	55	Neve	PolG	0	0	0	6	37	0	0	33
					37	0	0	33	134	0	0	28
HE 240 A	54	55	Vento X	PolG	0	0	0	9	37	0	0	51
					37	0	0	51	134	0	0	43
HE 240 A	54	55	Vento X	PolG	0	0	0	56	94	0	0	62
					94	0	0	62	134	0	0	9
HE 240 A	55	56	Peso Proprio	UnifG	0	0	0	60	118	0	0	60
HE 240 A	55	56	QP Solai	PolG	0	0	0	67	32	0	0	112
					32	0	0	112	86	0	0	111
					86	0	0	111	123	0	0	52
HE 240 A	55	56	QV Solai	PolG	0	0	0	22	32	0	0	36
					32	0	0	36	86	0	0	35
					86	0	0	35	123	0	0	17
HE 240 A	55	56	Neve	PolG	0	0	0	36	86	0	0	40
					86	0	0	40	123	0	0	6
HE 240 A	55	56	Neve	PolG	0	0	0	6	32	0	0	32
					32	0	0	32	123	0	0	27
HE 240 A	55	56	Vento X	PolG	0	0	0	9	32	0	0	49
					32	0	0	49	123	0	0	41
HE 240 A	55	56	Vento X	PolG	0	0	0	56	86	0	0	62
					86	0	0	62	123	0	0	9
HE 240 A	56	57	Peso Proprio	UnifG	0	0	0	60	107	0	0	60
HE 240 A	56	57	QP Solai	PolG	0	0	0	67	28	0	0	109
					28	0	0	109	79	0	0	108

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	56	57	QV Solai	PolG	0	0	0	22	28	0	0	35
					28	0	0	35	79	0	0	35
HE 240 A	56	57	Neve	PolG	0	0	0	35	113	0	0	16
					79	0	0	36	79	0	0	40
HE 240 A	56	57	Neve	PolG	0	0	0	6	28	0	0	30
					28	0	0	30	113	0	0	25
HE 240 A	56	57	Vento X	PolG	0	0	0	56	79	0	0	62
					79	0	0	62	113	0	0	9
HE 240 A	56	57	Vento X	PolG	0	0	0	9	28	0	0	47
					28	0	0	47	113	0	0	39
HE 240 A	57	58	Peso Proprio	UnifG	0	0	0	60	101	0	0	60
HE 240 A	57	58	QP Solai	PolG	0	0	0	67	25	0	0	107
					25	0	0	107	76	0	0	106
					76	0	0	106	108	0	0	47
HE 240 A	57	58	QV Solai	PolG	0	0	0	22	25	0	0	34
					25	0	0	34	76	0	0	34
					76	0	0	34	108	0	0	15
HE 240 A	57	58	Neve	PolG	0	0	0	6	25	0	0	29
					25	0	0	29	108	0	0	24
HE 240 A	57	58	Neve	PolG	0	0	0	36	76	0	0	40
					76	0	0	40	108	0	0	6
HE 240 A	57	58	Vento X	PolG	0	0	0	9	25	0	0	45
					25	0	0	45	108	0	0	36
HE 240 A	57	58	Vento X	PolG	0	0	0	56	76	0	0	62
					76	0	0	62	108	0	0	9
HE 240 A	58	17	Peso Proprio	UnifG	0	0	0	60	114	0	0	60
HE 240 A	58	17	QP Solai	PolG	0	0	0	67	25	0	0	105
					25	0	0	105	78	0	0	104
					78	0	0	104	111	0	0	45
HE 240 A	58	17	QV Solai	PolG	0	0	0	22	25	0	0	34
					25	0	0	34	78	0	0	33
					78	0	0	33	111	0	0	14
HE 240 A	58	17	Neve	PolG	0	0	0	6	25	0	0	28
					25	0	0	28	111	0	0	22
HE 240 A	58	17	Neve	PolG	0	0	0	36	78	0	0	40
					78	0	0	40	111	0	0	6
HE 240 A	58	17	Vento X	PolG	0	0	0	9	25	0	0	43
					25	0	0	43	111	0	0	34
HE 240 A	58	17	Vento X	PolG	0	0	0	56	78	0	0	62
					78	0	0	62	111	0	0	9
Trave 8006												
HE 240 A	18	22	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	18	22	QP Solai	PolG	0	0	0	63	40	0	0	122
					40	0	0	122	122	0	0	123
					122	0	0	123	182	0	0	68
HE 240 A	18	22	QV Solai	PolG	0	0	0	20	40	0	0	39
					40	0	0	39	122	0	0	39
					122	0	0	39	182	0	0	22
HE 240 A	18	22	Neve	PolG	0	0	0	3	40	0	0	39
					40	0	0	39	182	0	0	35
HE 240 A	18	22	Neve	PolG	0	0	0	36	122	0	0	40
					122	0	0	40	182	0	0	7
HE 240 A	18	22	Vento X	PolG	0	0	0	55	122	0	0	61
					122	0	0	61	182	0	0	11
HE 240 A	18	22	Vento X	PolG	0	0	0	5	40	0	0	60
					40	0	0	60	182	0	0	54
HE 240 A	22	23	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	22	23	QP Solai	PolG	0	0	0	61	37	0	0	117
					37	0	0	117	122	0	0	118
					122	0	0	118	178	0	0	66
HE 240 A	22	23	QV Solai	PolG	0	0	0	19	37	0	0	38
					37	0	0	38	122	0	0	38
					122	0	0	38	178	0	0	21
HE 240 A	22	23	Neve	PolG	0	0	0	3	37	0	0	37
					37	0	0	37	178	0	0	34

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	22	23		PolG	0	0	0	34	122	0	0	38
HE 240 A	22	23	Neve	PolG	122	0	0	38	178	0	0	7
HE 240 A	22	23	Vento X	PolG	0	0	0	5	37	0	0	58
HE 240 A	22	23	Vento X	PolG	37	0	0	58	178	0	0	52
HE 240 A	22	23	Vento X	PolG	0	0	0	53	122	0	0	59
HE 240 A	23	24	Peso Proprio	UnitG	122	0	0	59	178	0	0	11
HE 240 A	23	24	QP Solai	PolG	0	0	0	60	170	0	0	60
HE 240 A	23	24		PolG	34	0	0	58	34	0	0	113
HE 240 A				PolG	34	0	0	113	119	0	0	113
HE 240 A	23	24	QV Solai	PolG	119	0	0	113	170	0	0	63
HE 240 A	23	24		PolG	0	0	0	19	34	0	0	36
HE 240 A					34	0	0	36	119	0	0	36
HE 240 A	23	24	Neve	PolG	119	0	0	36	170	0	0	20
HE 240 A	23	24	Neve	PolG	0	0	0	3	34	0	0	36
HE 240 A	23	24	Neve	PolG	34	0	0	36	170	0	0	32
HE 240 A	23	24	Vento X	PolG	119	0	0	37	170	0	0	7
HE 240 A	23	24	Vento X	PolG	0	0	0	51	119	0	0	57
HE 240 A	23	24	Vento X	PolG	119	0	0	57	170	0	0	11
HE 240 A	23	24	Vento X	PolG	0	0	0	5	34	0	0	56
HE 240 A	24	65	Peso Proprio	UnitG	34	0	0	56	170	0	0	50
HE 240 A	24	65	QP Solai	PolG	0	0	0	60	159	0	0	60
HE 240 A				PolG	0	0	0	56	30	0	0	108
HE 240 A				PolG	30	0	0	108	113	0	0	109
HE 240 A	24	65	QV Solai	PolG	113	0	0	109	159	0	0	61
HE 240 A				PolG	0	0	0	18	30	0	0	35
HE 240 A	24	65	Vento X	PolG	30	0	0	35	113	0	0	35
HE 240 A	24	65		PolG	113	0	0	5	30	0	0	54
HE 240 A	24	65	Neve	PolG	30	0	0	54	159	0	0	47
HE 240 A	24	65	Vento X	PolG	0	0	0	49	113	0	0	55
HE 240 A	65	66	Peso Proprio	UnitG	113	0	0	55	159	0	0	11
HE 240 A	65	66	QP Solai	PolG	0	0	0	60	148	0	0	60
HE 240 A				PolG	27	0	0	54	27	0	0	103
HE 240 A	65	66	QV Solai	PolG	107	0	0	104	148	0	0	59
HE 240 A				PolG	27	0	0	33	107	0	0	33
HE 240 A	65	66	Neve	PolG	107	0	0	33	148	0	0	19
HE 240 A	65	66	Neve	PolG	0	0	0	30	107	0	0	34
HE 240 A	65	66	Neve	PolG	107	0	0	34	148	0	0	7
HE 240 A	66	67	Peso Proprio	UnitG	27	0	0	3	27	0	0	33
HE 240 A	66	67	QP Solai	PolG	27	0	0	33	148	0	0	29
HE 240 A	65	66	Vento X	PolG	0	0	0	52	23	0	0	99
HE 240 A	65	66	Vento X	PolG	107	0	0	53	148	0	0	11
HE 240 A	65	66	Vento X	PolG	0	0	0	5	27	0	0	51
HE 240 A	66	67	Peso Proprio	UnitG	27	0	0	51	148	0	0	45
HE 240 A	66	67	QP Solai	PolG	23	0	0	52	23	0	0	99
HE 240 A				PolG	99	0	0	99	99	0	0	100
HE 240 A	66	67	QV Solai	PolG	23	0	0	100	134	0	0	56
HE 240 A				PolG	23	0	0	17	23	0	0	32
HE 240 A	66	67	Neve	PolG	99	0	0	32	134	0	0	18
HE 240 A	66	67	Neve	PolG	0	0	0	3	23	0	0	32
HE 240 A	66	67	Neve	PolG	23	0	0	32	134	0	0	28
HE 240 A	66	67	Vento X	PolG	99	0	0	29	99	0	0	33
HE 240 A	66	67	Vento X	PolG	0	0	0	44	99	0	0	51
HE 240 A	66	67	Vento X	PolG	99	0	0	51	134	0	0	11
HE 240 A	66	67	Vento X	PolG	0	0	0	5	23	0	0	49

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	67	68	Peso Proprio	UnitG	0	0	0	60	123	0	0	60
HE 240 A	67	68	QP Solai	PolG	20	0	0	49	20	0	0	94
HE 240 A	67	68	QV Solai	PolG	92	0	0	95	123	0	0	54
HE 240 A	67	68		PolG	20	0	0	16	20	0	0	30
HE 240 A	67	68	Neve	PolG	92	0	0	30	123	0	0	30
HE 240 A	67	68	Neve	PolG	92	0	0	27	92	0	0	32
HE 240 A	67	68	Neve	PolG	92	0	0	32	123	0	0	7
HE 240 A	67	68	Vento X	PolG	20	0	0	3	20	0	0	30
HE 240 A	67	68	Vento X	PolG	20	0	0	42	92	0	0	26
HE 240 A	67	68	Vento X	PolG	92	0	0	49	123	0	0	49
HE 240 A	67	68	Vento X	PolG	0	0	0	5	20	0	0	47
HE 240 A	68	69	Peso Proprio	UnitG	20	0	0	47	123	0	0	41
HE 240 A	68	69	QP Solai	PolG	0	0	0	60	113	0	0	60
HE 240 A	68	69		PolG	17	0	0	47	17	0	0	89
HE 240 A	68	69	QV Solai	PolG	86	0	0	90	113	0	0	51
HE 240 A	68	69	QV Solai	PolG	86	0	0	29	86	0	0	29
HE 240 A	68	69	Neve	PolG	86	0	0	29	113	0	0	16
HE 240 A	68	69	Neve	PolG	0	0	0	26	86	0	0	30
HE 240 A	68	69	Neve	PolG	86	0	0	30	113	0	0	7
HE 240 A	69	70	Peso Proprio	UnitG	17	0	0	3	17	0	0	29
HE 240 A	69	70	QP Solai	PolG	0	0	0	29	113	0	0	25
HE 240 A	69	70	Vento X	PolG	86	0	0	40	86	0	0	47
HE 240 A	69	70	Vento X	PolG	86	0	0	47	113	0	0	11
HE 240 A	69	70	Vento X	PolG	17	0	0	45	113	0	0	45
HE 240 A	69	70	Peso Proprio	UnitG	0	0	0	60	108	0	0	60
HE 240 A	69	70	QP Solai	PolG	16	0	0	45	16	0	0	85
HE 240 A	69	70	QV Solai	PolG	84	0	0	85	84	0	0	86
HE 240 A	69	70	QV Solai	PolG	84	0	0	86	108	0	0	49
HE 240 A	69	70	Neve	PolG	16	0	0	27	84	0	0	27
HE 240 A	69	70	Neve	PolG	84	0	0	27	108	0	0	16
HE 240 A	69	70	Neve	PolG	84	0	0	24	84	0	0	29
HE 240 A	69	70	Neve	PolG	0	0	0	29	108	0	0	7
HE 240 A	69	70	Vento X	PolG	16	0	0	3	16	0	0	28
HE 240 A	69	70	Vento X	PolG	16	0	0	28	108	0	0	23
HE 240 A	69	70	Vento X	PolG	84	0	0	38	84	0	0	45
HE 240 A	69	70	Vento X	PolG	84	0	0	45	108	0	0	11
HE 240 A	70	22	Peso Proprio	UnitG	16	0	0	5	16	0	0	43
HE 240 A	70	22	QP Solai	PolG	0	0	0	43	108	0	0	36
HE 240 A	70	22		PolG	0	0	0	60	111	0	0	60
HE 240 A	70	22		PolG	0	0	0	42	15	0	0	80
HE 240 A	70	22	Neve	PolG	15	0	0	80	87	0	0	81
HE 240 A	70	22	QV Solai	PolG	87	0	0	81	111	0	0	47
HE 240 A	70	22	QV Solai	PolG	0	0	0	14	15	0	0	26
HE 240 A	70	22	Neve	PolG	15	0	0	26	87	0	0	26
HE 240 A	70	22	Neve	PolG	87	0	0	26	111	0	0	15
HE 240 A	70	22	Vento X	PolG	15	0	0	3	15	0	0	26
HE 240 A	70	22	Vento X	PolG	0	0	0	26	111	0	0	22
HE 240 A	70	22	Vento X	PolG	87	0	0	27	111	0	0	7
HE 240 A	70	22	Vento X	PolG	0	0	0	5	15	0	0	40
HE 240 A	70	22	Vento X	PolG	15	0	0	40	111	0	0	34
HE 240 A	70	22	Vento X	PolG	0	0	0	35	87	0	0	42
HE 240 A	70	22	Vento X	PolG	87	0	0	42	111	0	0	11
Trave 8007												
HE 240 A	4	5	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	4	5	QP Solai	PolG	0	0	0	63	51	0	0	119
HE 240 A	4	5		PolG	51	0	0	119	141	0	0	116
HE 240 A	4	5	QV Solai	PolG	141	0	0	116	178	0	0	62
HE 240 A	4	5		PolG	0	0	0	20	51	0	0	38

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					51	0	0	38	141	0	0	37
					141	0	0	37	178	0	0	20
HE 240 A	4	5	Neve	PolG	0	0	0	34	141	0	0	37
HE 240 A	4	5	Neve	PolG	0	0	0	37	178	0	0	5
HE 240 A	4	5			0	0	0	5	51	0	0	38
HE 240 A	4	5	Vento X	PolG	51	0	0	38	178	0	0	34
HE 240 A	4	5			0	0	0	53	141	0	0	58
HE 240 A	4	5	Vento X	PolG	141	0	0	58	178	0	0	8
HE 240 A	4	5	Vento X	PolG	0	0	0	8	51	0	0	59
HE 240 A	5	6	Peso Proprio	UnifG	51	0	0	59	178	0	0	52
HE 240 A	5	6	QP Solai	PolG	0	0	0	60	170	0	0	60
					46	0	0	61	46	0	0	114
HE 240 A	5	6	QV Solai	PolG	137	0	0	114	137	0	0	111
					137	0	0	111	170	0	0	60
HE 240 A	5	6			46	0	0	37	137	0	0	37
					137	0	0	36	170	0	0	36
HE 240 A	5	6	Neve	PolG	0	0	0	5	46	0	0	37
HE 240 A	5	6	Neve	PolG	46	0	0	37	170	0	0	32
HE 240 A	5	6	Neve	PolG	0	0	0	33	137	0	0	36
HE 240 A	5	6	Vento X	PolG	137	0	0	36	170	0	0	5
HE 240 A	5	6			46	0	0	8	46	0	0	57
HE 240 A	5	6	Vento X	PolG	46	0	0	57	170	0	0	50
HE 240 A	5	6	Vento X	PolG	0	0	0	51	137	0	0	55
HE 240 A	6	29	Peso Proprio	UnifG	137	0	0	55	170	0	0	8
HE 240 A	6	29	QP Solai	PolG	0	0	0	60	158	0	0	60
					41	0	0	59	41	0	0	109
HE 240 A	6	29	Neve	PolG	129	0	0	109	129	0	0	107
HE 240 A	6	29	Neve	PolG	0	0	0	107	158	0	0	57
HE 240 A	6	29	Neve	PolG	41	0	0	19	41	0	0	35
HE 240 A	6	29	Vento X	PolG	41	0	0	35	129	0	0	34
					129	0	0	34	158	0	0	18
HE 240 A	6	29			0	0	0	32	129	0	0	34
HE 240 A	6	29	Neve	PolG	129	0	0	34	158	0	0	5
HE 240 A	6	29	Neve	PolG	41	0	0	5	41	0	0	35
HE 240 A	6	29	Vento X	PolG	0	0	0	49	129	0	0	53
HE 240 A	6	29	Vento X	PolG	129	0	0	53	158	0	0	8
HE 240 A	19	4	Peso Proprio	UnifG	41	0	0	55	158	0	0	48
HE 240 A	19	4	QP Solai	PolG	0	0	0	66	54	0	0	123
					54	0	0	123	143	0	0	121
HE 240 A	19	4	QV Solai	PolG	143	0	0	121	182	0	0	64
					0	0	0	21	54	0	0	39
HE 240 A	19	4	Neve	PolG	54	0	0	39	143	0	0	39
HE 240 A	19	4	Neve	PolG	143	0	0	36	143	0	0	39
HE 240 A	19	4	Neve	PolG	0	0	0	5	54	0	0	5
HE 240 A	19	4	Vento X	PolG	54	0	0	40	182	0	0	35
HE 240 A	19	4	Vento X	PolG	0	0	0	56	143	0	0	60
HE 240 A	19	4	Vento X	PolG	143	0	0	60	182	0	0	8
HE 240 A	19	4	Vento X	PolG	0	0	0	8	54	0	0	61
HE 240 A	29	30	Peso Proprio	UnifG	54	0	0	61	182	0	0	54
HE 240 A	29	30	QP Solai	PolG	0	0	0	60	148	0	0	60
					37	0	0	105	37	0	0	105
HE 240 A	29	30	QV Solai	PolG	122	0	0	102	148	0	0	55
					0	0	0	18	37	0	0	34
HE 240 A	29	30	Neve	PolG	122	0	0	33	148	0	0	18
HE 240 A	29	30	Neve	PolG	37	0	0	5	37	0	0	34
HE 240 A	29	30	Neve	PolG	0	0	0	30	122	0	0	33
					122	0	0	33	148	0	0	5

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	29	30	Vento X	PolG	37	0	0	8	37	0	0	53
HE 240 A	29	30	Vento X	PolG	0	0	0	53	148	0	0	45
HE 240 A	30	31	Peso Proprio	UnifG	122	0	0	51	148	0	0	8
HE 240 A	30	31	QP Solai	PolG	0	0	0	54	32	0	0	100
					32	0	0	100	112	0	0	97
HE 240 A	30	31	QV Solai	PolG	112	0	0	97	134	0	0	53
					32	0	0	32	112	0	0	31
HE 240 A	30	31	Neve	PolG	112	0	0	31	134	0	0	17
HE 240 A	30	31	Neve	PolG	112	0	0	32	134	0	0	5
HE 240 A	30	31	Vento X	PolG	32	0	0	33	134	0	0	33
HE 240 A	30	31	Vento X	PolG	0	0	0	44	112	0	0	49
HE 240 A	30	31	Vento X	PolG	112	0	0	49	134	0	0	8
HE 240 A	31	32	Peso Proprio	UnifG	32	0	0	8	32	0	0	51
HE 240 A	31	32	QP Solai	PolG	0	0	0	51	134	0	0	43
HE 240 A	31	32			104	0	0	30	123	0	0	16
HE 240 A	31	32	Neve	PolG	104	0	0	27	104	0	0	30
HE 240 A	31	32	Neve	PolG	0	0	0	5	28	0	0	31
HE 240 A	31	32	Vento X	PolG	28	0	0	42	104	0	0	47
HE 240 A	31	32	Vento X	PolG	104	0	0	47	123	0	0	8
HE 240 A	31	32	Vento X	PolG	0	0	0	8	28	0	0	48
HE 240 A	32	33	Peso Proprio	UnifG	28	0	0	48	123	0	0	41
HE 240 A	32	33	QP Solai	PolG	0	0	0	49	24	0	0	91
					24	0	0	91	97	0	0	88
HE 240 A	32	33	QV Solai	PolG	97	0	0	88	113	0	0	48
					24	0	0	29	97	0	0	28
HE 240 A	32	33	Neve	PolG	97	0	0	28	113	0	0	15
HE 240 A	32	33	Neve	PolG	97	0	0	26	97	0	0	29
HE 240 A	32	33	Neve	PolG	0	0	0	29	113	0	0	5
HE 240 A	32	33	Vento X	PolG	24	0	0	5	24	0	0	30
HE 240 A	32	33	Vento X	PolG	0	0	0	40	97	0	0	44
HE 240 A	32	33	Vento X	PolG	97	0	0	44	113	0	0	8
HE 240 A	33	34	Peso Proprio	UnifG	24	0	0	46	113	0	0	46
HE 240 A	33	34	QP Solai	PolG	0	0	0	60	108	0	0	60
HE 240 A	33	34	QP Solai	PolG	0	0	0	47	22	0	0	86
HE 240 A	33	34	QV Solai	PolG	22	0	0	86	93	0	0	83
					93	0	0	83	108	0	0	45
HE 240 A	33	34	QV Solai	PolG	0	0	0	15	22	0	0	28
					22	0	0	28	93	0	0	27
HE 240 A	33	34	Neve	PolG	93	0	0	27	108	0	0	15
HE 240 A	33	34	Neve	PolG	22	0	0	28	108	0	0	23
HE 240 A	33	34	Vento X	PolG	93	0	0	27	108	0	0	5
HE 240 A	33	34	Vento X	PolG	93	0	0	38	93	0	0	42
HE 240 A	33	34	Vento X	PolG	0	0	0	42	108	0	0	8
HE 240 A	34	18	Peso Proprio	UnifG	22	0	0	44	108	0	0	36
HE 240 A	34	18	QP Solai	PolG	0	0	0	60	111	0	0	60
					122	0	0	45	21	0	0	81

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					21	0	0	81	97	0	0	78
HE 240 A	34	18	QV Solai	PolG	97	0	0	78	111	0	0	43
					21	0	0	14	21	0	0	26
					97	0	0	26	97	0	0	25
HE 240 A	34	18	Neve	PolG	0	0	5	21	111	0	0	14
					21	0	0	27	111	0	0	22
HE 240 A	34	18	Neve	PolG	0	0	23	97	0	0	0	26
					97	0	0	26	111	0	5	
HE 240 A	34	18	Vento X	PolG	0	0	8	21	0	0	42	0
					21	0	0	42	111	0	0	34
HE 240 A	34	18	Vento X	PolG	0	0	35	97	0	0	40	
					97	0	0	40	111	0	0	8
Trave 8008												
HE 240 A	20	25	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	20	25	QV Solai	PolG	68	0	0	68	68	0	0	125
					129	0	0	125	129	0	0	124
HE 240 A	20	25	QV Solai	PolG	0	0	0	124	182	0	0	67
					68	0	0	22	68	0	0	40
					129	0	0	40	129	0	0	40
HE 240 A	20	25	Neve	PolG	0	0	0	40	182	0	0	22
					68	0	0	6	68	0	0	40
HE 240 A	20	25	Neve	PolG	0	0	0	40	182	0	0	35
					129	0	0	39	182	0	0	39
HE 240 A	25	26	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	25	26	QV Solai	PolG	0	0	0	66	64	0	0	121
					64	0	0	121	129	0	0	119
HE 240 A	25	26	QV Solai	PolG	0	0	0	119	178	0	0	65
					64	0	0	21	64	0	0	39
HE 240 A	25	26	Neve	PolG	0	0	0	39	129	0	0	38
					129	0	0	38	178	0	0	21
HE 240 A	25	26	Neve	PolG	0	0	0	6	64	0	0	39
					64	0	0	39	178	0	0	34
HE 240 A	25	26	Neve	PolG	0	0	0	34	129	0	0	38
HE 240 A	25	26	Vento X	PolG	0	0	0	53	129	0	0	59
HE 240 A	25	26	Vento X	PolG	0	0	0	59	178	0	0	10
HE 240 A	25	26	Vento X	PolG	0	0	0	10	64	0	0	60
					64	0	0	60	178	0	0	52
HE 240 A	26	27	Peso Proprio	UnifG	0	0	0	60	170	0	0	60
HE 240 A	26	27	QV Solai	PolG	0	0	0	63	59	0	0	116
					59	0	0	116	125	0	0	114
HE 240 A	26	27	QV Solai	PolG	0	0	0	114	170	0	0	62
					125	0	0	20	59	0	0	37
HE 240 A	26	27	QV Solai	PolG	0	0	0	37	125	0	0	37
					125	0	0	37	170	0	0	20
HE 240 A	26	27	Neve	PolG	0	0	0	33	125	0	0	37
					125	0	0	37	170	0	0	6
HE 240 A	26	27	Neve	PolG	0	0	0	6	59	0	0	38
HE 240 A	26	27	Vento X	PolG	0	0	0	38	170	0	0	32
					59	0	0	10	59	0	0	58
HE 240 A	26	27	Vento X	PolG	0	0	0	58	170	0	0	50
HE 240 A	26	27	Vento X	PolG	0	0	0	51	125	0	0	56
					125	0	0	56	170	0	0	10
HE 240 A	27	71	Peso Proprio	UnifG	0	0	0	60	158	0	0	60
HE 240 A	27	71	QV Solai	PolG	0	0	0	61	52	0	0	111
					52	0	0	111	118	0	0	109
HE 240 A	27	71	QV Solai	PolG	0	0	0	109	158	0	0	60
					52	0	0	20	52	0	0	36
HE 240 A	27	71	QV Solai	PolG	0	0	0	36	118	0	0	35
					118	0	0	35	158	0	0	19

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	27	71	Neve	PolG	0	0	0	6	52	0	0	36
HE 240 A	27	71	Neve	PolG	52	0	0	36	158	0	0	31
					118	0	0	35	158	0	0	6
HE 240 A	27	71	Vento X	PolG	0	0	0	10	52	0	0	56
					52	0	0	56	158	0	0	48
HE 240 A	27	71	Vento X	PolG	0	0	0	49	118	0	0	54
					118	0	0	54	158	0	0	10
HE 240 A	71	72	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	71	72	QV Solai	PolG	0	0	0	59	47	0	0	107
					47	0	0	107	112	0	0	105
HE 240 A	71	72	QV Solai	PolG	112	0	0	105	148	0	0	58
					47	0	0	19	47	0	0	34
HE 240 A	71	72	Neve	PolG	112	0	0	34	112	0	0	18
					47	0	0	6	47	0	0	35
HE 240 A	71	72	Neve	PolG	0	0	0	35	148	0	0	29
					112	0	0	30	112	0	0	34
HE 240 A	71	72	Vento X	PolG	0	0	0	46	112	0	0	6
					112	0	0	52	148	0	0	10
HE 240 A	71	72	Vento X	PolG	0	0	0	10	47	0	0	54
					47	0	0	54	148	0	0	46
HE 240 A	72	73	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	72	73	QV Solai	PolG	0	0	0	56	40	0	0	102
					40	0	0	102	104	0	0	100
HE 240 A	72	73	QV Solai	PolG	104	0	0	100	134	0	0	55
					0	0	0	18	40	0	0	33
HE 240 A	72	73	Vento X	PolG	40	0	0	33	104	0	0	32
					104	0	0	32	134	0	0	18
HE 240 A	72	73	Neve	PolG	0	0	0	29	104	0	0	32
					104	0	0	32	134	0	0	6
HE 240 A	72	73	Neve	PolG	0	0	0	6	40	0	0	34
					40	0	0	34	134	0	0	28
HE 240 A	72	73	Vento X	PolG	0	0	0	10	40	0	0	52
					40	0	0	52	134	0	0	43
HE 240 A	72	73	Vento X	PolG	0	0	0	44	104	0	0	50
					104	0	0	50	134	0	0	10
HE 240 A	73	74	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	73	74	QV Solai	PolG	0	0	0	54	35	0	0	98
					35	0	0	98	96	0	0	95
HE 240 A	73	74	QV Solai	PolG	96	0	0	95	123	0	0	53
					0	0	0	17	35	0	0	31
					35	0	0	31	96	0	0	31
HE 240 A	73	74	Neve	PolG	96	0	0	27	96	0	0	17
					96	0	0	31	123	0	0	31
HE 240 A	73	74	Neve	PolG	0	0	0	6	35	0	0	6
					35	0	0	32	123	0	0	26
HE 240 A	73	74	Vento X	PolG	0	0	0	42	96	0	0	48
					96	0	0	48	123	0	0	10
HE 240 A	73	74	Vento X	PolG	0	0	0	10	35	0	0	50
					35	0	0	50	123	0	0	41
HE 240 A	74	75	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	74	75	QV Solai	PolG	0	0	0	52	30	0	0	93
					30	0	0	93	90	0	0	90
HE 240 A	74	75	QV Solai	PolG	90	0	0	90	113	0	0	50
					30	0	0	17	30	0	0	30
HE 240 A	74	75	Neve	PolG	90	0	0	29	113	0	0	16
					90	0	0	26	90	0	0	30
HE 240 A	74	75	Neve	PolG	0	0	0	30	113	0	0	6
					30	0	0	6	30	0	0	31
HE 240 A	74	75	Vento X	PolG	0	0	0	31	113	0	0	25
					90	0	0	40	90	0	0	46
HE 240 A	74	75	Vento X	PolG	0	0	0	46	113	0	0	10

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	74	75	Vento X	PolG	30	0	0	10	30	0	0	48
HE 240 A	75	76	Peso Proprio	UnifG	30	0	0	48	113	0	0	39
HE 240 A	75	76	QP Solai	PolG	0	0	0	49	27	0	0	88
HE 240 A	75	76			27	0	0	88	87	0	0	86
HE 240 A	75	76			87	0	0	86	108	0	0	48
HE 240 A	75	76	QV Solai	PolG	0	0	0	16	27	0	0	28
HE 240 A	75	76			27	0	0	28	87	0	0	27
HE 240 A	75	76	Neve	PolG	87	0	0	27	108	0	0	15
HE 240 A	75	76			0	0	0	24	87	0	0	28
HE 240 A	75	76	Neve	PolG	87	0	0	28	108	0	0	6
HE 240 A	75	76			0	0	0	6	27	0	0	29
HE 240 A	75	76	Vento X	PolG	27	0	0	29	108	0	0	24
HE 240 A	75	76			0	0	0	37	87	0	0	44
HE 240 A	75	76	Vento X	PolG	87	0	0	44	108	0	0	10
HE 240 A	75	76			27	0	0	10	27	0	0	46
HE 240 A	76	19	Peso Proprio	UnifG	0	0	0	46	108	0	0	36
HE 240 A	76	19	QP Solai	PolG	0	0	0	60	111	0	0	60
HE 240 A	76	19			26	0	0	47	26	0	0	84
HE 240 A	76	19			91	0	0	84	91	0	0	81
HE 240 A	76	19			91	0	0	81	111	0	0	46
HE 240 A	76	19	QV Solai	PolG	0	0	0	15	26	0	0	27
HE 240 A	76	19			26	0	0	27	91	0	0	26
HE 240 A	76	19	Neve	PolG	91	0	0	26	111	0	0	15
HE 240 A	76	19			91	0	0	23	91	0	0	27
HE 240 A	76	19	Neve	PolG	91	0	0	27	111	0	0	6
HE 240 A	76	19			0	0	0	6	26	0	0	28
HE 240 A	76	19	Vento X	PolG	26	0	0	28	111	0	0	22
HE 240 A	76	19			91	0	0	35	91	0	0	42
HE 240 A	76	19	Vento X	PolG	91	0	0	42	111	0	0	10
HE 240 A	76	19			0	0	0	10	26	0	0	43
HE 240 A	76	19	Vento X	PolG	26	0	0	43	111	0	0	34
Trave 8009												
HE 240 A	21	28	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	21	28	QP Solai	PolG	0	0	0	70	85	0	0	128
HE 240 A	21	28			85	0	0	128	115	0	0	127
HE 240 A	21	28	QV Solai	PolG	115	0	0	127	182	0	0	70
HE 240 A	21	28			0	0	0	23	85	0	0	41
HE 240 A	21	28			85	0	0	41	115	0	0	41
HE 240 A	21	28	Neve	PolG	115	0	0	41	182	0	0	22
HE 240 A	21	28			0	0	0	8	85	0	0	41
HE 240 A	21	28	Neve	PolG	85	0	0	41	182	0	0	36
HE 240 A	21	28			115	0	0	36	115	0	0	40
HE 240 A	21	28	Vento X	PolG	0	0	0	40	182	0	0	8
HE 240 A	21	28			115	0	0	12	85	0	0	63
HE 240 A	21	28	Vento X	PolG	85	0	0	63	182	0	0	55
HE 240 A	21	28			0	0	0	55	115	0	0	62
HE 240 A	21	28	Vento X	PolG	115	0	0	62	182	0	0	12
HE 240 A	28	29	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	28	29	QP Solai	PolG	0	0	0	68	80	0	0	123
HE 240 A	28	29			80	0	0	123	115	0	0	122
HE 240 A	28	29			115	0	0	122	178	0	0	68
HE 240 A	28	29	QV Solai	PolG	0	0	0	22	80	0	0	39
HE 240 A	28	29			80	0	0	39	115	0	0	39
HE 240 A	28	29	Neve	PolG	115	0	0	39	178	0	0	22
HE 240 A	28	29			0	0	0	34	115	0	0	38
HE 240 A	28	29	Neve	PolG	115	0	0	38	178	0	0	8
HE 240 A	28	29			0	0	0	8	80	0	0	39
HE 240 A	28	29	Vento X	PolG	80	0	0	39	178	0	0	34
HE 240 A	28	29			0	0	0	53	115	0	0	60
HE 240 A	28	29	Vento X	PolG	115	0	0	60	178	0	0	12
HE 240 A	28	29			0	0	0	12	80	0	0	61
HE 240 A	29	30	Peso Proprio	UnifG	80	0	0	61	178	0	0	53
HE 240 A	29	30	QP Solai	PolG	0	0	0	60	170	0	0	60
HE 240 A	29	30			73	0	0	66	73	0	0	118

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	29	30	QV Solai	PolG	113	0	0	117	170	0	0	65
HE 240 A	29	30			73	0	0	21	73	0	0	38
HE 240 A	29	30	Neve	PolG	113	0	0	38	170	0	0	21
HE 240 A	29	30			73	0	0	8	73	0	0	38
HE 240 A	29	30	Neve	PolG	73	0	0	38	170	0	0	33
HE 240 A	29	30			113	0	0	33	113	0	0	37
HE 240 A	29	30	Vento X	PolG	113	0	0	12	73	0	0	8
HE 240 A	29	30			73	0	0	59	170	0	0	50
HE 240 A	29	30	Vento X	PolG	73	0	0	51	113	0	0	57
HE 240 A	30	77	Peso Proprio	UnifG	113	0	0	57	170	0	0	12
HE 240 A	30	77	QP Solai	PolG	0	0	0	60	158	0	0	60
HE 240 A	30	77			66	0	0	64	66	0	0	114
HE 240 A	30	77	Neve	PolG	66	0	0	114	108	0	0	112
HE 240 A	30	77			108	0	0	112	158	0	0	63
HE 240 A	30	77	QV Solai	PolG	108	0	0	20	66	0	0	36
HE 240 A	30	77			66	0	0	36	108	0	0	36
HE 240 A	30	77	Neve	PolG	108	0	0	36	158	0	0	20
HE 240 A	30	77			66	0	0	8	66	0	0	37
HE 240 A	30	77	Neve	PolG	66	0	0	37	158	0	0	31
HE 240 A	30	77			108	0	0	31	108	0	0	36
HE 240 A	30	77	Vento X	PolG	108	0	0	36	158	0	0	8
HE 240 A	30	77			66	0	0	13	66	0	0	57
HE 240 A	30	77	Vento X	PolG	66	0	0	57	158	0	0	48
HE 240 A	30	77			108	0	0	49	108	0	0	55
HE 240 A	30	77	Vento X	PolG	108	0	0	55	158	0	0	12
HE 240 A	77	78	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	77	78	QP Solai	PolG	0	0	0	61	58	0	0	109
HE 240 A	77	78			58	0	0	109	103	0	0	108
HE 240 A	77	78			103	0	0	108	148	0	0	60
HE 240 A	77	78	QV Solai	PolG	0	0	0	20	58	0	0	35
HE 240 A	77	78			58	0	0	35	103	0	0	35
HE 240 A	77	78	Neve	PolG	103	0	0	35	148	0	0	19
HE 240 A	77	78			103	0	0	30	103	0	0	34
HE 240 A	77	78	Neve	PolG	103	0	0	34	148	0	0	8
HE 240 A	77	78			58	0	0	8	58	0	0	35
HE 240 A	77	78	Vento X	PolG	58	0	0	35	148	0	0	30
HE 240 A	77	78			103	0	0	46	103	0	0	53
HE 240 A	77	78	Vento X	PolG	103	0	0	53	148	0	0	12
HE 240 A	77	78			58	0	0	13	58	0	0	55
HE 240 A	77	78	Vento X	PolG	58	0	0	55	148	0	0	46
HE 240 A	78	79	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	78	79	QP Solai	PolG	0	0	0	59	51	0	0	105
HE 240 A	78	79			51	0	0	105	96	0	0	103
HE 240 A	78	79	Neve	PolG	96	0	0	103	134	0	0	58
HE 240 A	78	79			96	0	0	19	51	0	0	34
HE 240 A	78	79	QV Solai	PolG	51	0	0	34	96	0	0	33
HE 240 A	78	79			96	0	0	33	134	0	0	8
HE 240 A	78	79	Vento X	PolG	96	0	0	44	96	0	0	51
HE 240 A	78	79	Neve	PolG	96	0	0	51	134	0	0	12
HE 240 A	78	79			51	0	0	13	51	0	0	53
HE 240 A	78	79	Vento X	PolG	51	0	0	53	134	0	0	43
HE 240 A	79	80	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	79	80	QP Solai	PolG	0	0	0	57	44	0	0	100
HE 240 A	79	80			44	0	0	100	89	0	0	98
HE 240 A	79	80	Neve	PolG	89	0	0	98	123	0	0	55
HE 240 A	79	80			44	0	0	18	44	0	0	32
HE 240 A	79	80	QV Solai	PolG	44	0	0	32	89	0	0	31
HE 240 A	79	80			89	0	0	31	123	0	0	18
HE 240 A	79	80	Neve	PolG	0	0	0	27	89	0	0	32
HE 240 A	79	80			89	0	0	52	123	0	0	8

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	79	80	Neve	PolG	44	0	0	8	44	0	0	33
HE 240 A	79	80	Vento X	PolG	0	0	0	33	123	0	0	27
HE 240 A					89	0	0	42	89	0	0	49
HE 240 A	79	80	Vento X	PolG	0	0	0	49	123	0	0	12
HE 240 A					44	0	0	51	123	0	0	51
HE 240 A	80	81	Peso Proprio	UnifG	0	0	0	60	113	0	0	41
HE 240 A	80	81	QP Solai	PolG	0	0	0	54	39	0	0	95
HE 240 A					39	0	0	95	84	0	0	93
HE 240 A					84	0	0	93	113	0	0	53
HE 240 A	80	81	QV Solai	PolG	0	0	0	17	39	0	0	31
HE 240 A					39	0	0	31	84	0	0	30
HE 240 A					84	0	0	30	113	0	0	17
HE 240 A	80	81	Neve	PolG	0	0	0	8	39	0	0	31
HE 240 A					39	0	0	31	113	0	0	25
HE 240 A	80	81	Neve	PolG	0	0	0	26	84	0	0	30
HE 240 A	80	81	Vento X	PolG	84	0	0	30	113	0	0	8
HE 240 A					0	0	0	40	84	0	0	47
HE 240 A	80	81	Vento X	PolG	84	0	0	47	113	0	0	12
HE 240 A					0	0	0	13	39	0	0	49
HE 240 A	81	82	Peso Proprio	UnifG	39	0	0	49	113	0	0	39
HE 240 A	81	82	QP Solai	PolG	0	0	0	60	108	0	0	60
HE 240 A					0	0	0	52	35	0	0	91
HE 240 A					35	0	0	91	82	0	0	89
HE 240 A					82	0	0	89	108	0	0	51
HE 240 A	81	82	QV Solai	PolG	0	0	0	17	35	0	0	29
HE 240 A					35	0	0	29	82	0	0	28
HE 240 A					82	0	0	28	108	0	0	16
HE 240 A	81	82	Neve	PolG	0	0	0	24	82	0	0	29
HE 240 A					82	0	0	29	108	0	0	8
HE 240 A	81	82	Neve	PolG	0	0	0	8	35	0	0	30
HE 240 A					35	0	0	30	108	0	0	24
HE 240 A	81	82	Vento X	PolG	0	0	0	38	82	0	0	45
HE 240 A					82	0	0	45	108	0	0	12
HE 240 A	81	82	Vento X	PolG	0	0	0	13	35	0	0	46
HE 240 A	82	20	Peso Proprio	UnifG	35	0	0	46	108	0	0	36
HE 240 A	82	20	QP Solai	PolG	0	0	0	50	34	0	0	86
HE 240 A					34	0	0	86	86	0	0	84
HE 240 A					86	0	0	84	111	0	0	48
HE 240 A	82	20	QV Solai	PolG	0	0	0	16	34	0	0	28
HE 240 A					34	0	0	28	86	0	0	27
HE 240 A					86	0	0	27	111	0	0	15
HE 240 A	82	20	Neve	PolG	0	0	0	8	34	0	0	29
HE 240 A					34	0	0	29	111	0	0	22
HE 240 A	82	20	Neve	PolG	0	0	0	23	86	0	0	28
HE 240 A					86	0	0	28	111	0	0	8
HE 240 A	82	20	Vento X	PolG	0	0	0	13	34	0	0	44
HE 240 A					34	0	0	44	111	0	0	34
HE 240 A	82	20	Vento X	PolG	0	0	0	35	86	0	0	43
HE 240 A					86	0	0	43	111	0	0	12
Trave 8010												
HE 240 A	22	31	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	22	31	QP Solai	PolG	0	0	0	57	98	0	0	64
HE 240 A					98	0	0	64	182	0	0	15
HE 240 A	22	31	QV Solai	PolG	0	0	0	18	98	0	0	21
HE 240 A					98	0	0	21	182	0	0	5
HE 240 A	22	31	Neve	PolG	0	0	0	36	98	0	0	40
HE 240 A					98	0	0	40	182	0	0	10
HE 240 A	22	31	Vento X	PolG	0	0	0	55	98	0	0	62
HE 240 A	31	32	Peso Proprio	UnifG	98	0	0	62	182	0	0	15
HE 240 A	31	32	QP Solai	PolG	0	0	0	60	178	0	0	60
HE 240 A					99	0	0	55	99	0	0	62
HE 240 A	31	32	QV Solai	PolG	0	0	0	62	178	0	0	15
HE 240 A					99	0	0	18	99	0	0	20

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	31	32		PolG	99	0	0	0	34	99	0	0
HE 240 A					0	0	0	39	178	0	0	10
HE 240 A	31	32	Vento X	PolG	0	0	0	53	99	0	0	60
HE 240 A					99	0	0	60	178	0	0	15
HE 240 A	32	33	Peso Proprio	UnifG	0	0	0	60	170	0	0	60
HE 240 A	32	33	QP Solai	PolG	0	0	0	53	98	0	0	60
HE 240 A					98	0	0	60	170	0	0	15
HE 240 A	32	33	QV Solai	PolG	0	0	0	17	98	0	0	19
HE 240 A					98	0	0	19	170	0	0	5
HE 240 A	32	33	Neve	PolG	0	0	0	33	98	0	0	37
HE 240 A					98	0	0	37	170	0	0	10
HE 240 A	32	33	Vento X	PolG	0	0	0	51	98	0	0	58
HE 240 A					98	0	0	58	170	0	0	15
HE 240 A	33	83	Peso Proprio	UnifG	0	0	0	60	159	0	0	60
HE 240 A	33	83	QP Solai	PolG	0	0	0	50	95	0	0	58
HE 240 A					95	0	0	58	159	0	0	15
HE 240 A	33	83	QV Solai	PolG	0	0	0	16	95	0	0	19
HE 240 A					95	0	0	19	159	0	0	5
HE 240 A	33	83	Neve	PolG	0	0	0	31	95	0	0	36
HE 240 A					95	0	0	36	159	0	0	10
HE 240 A	33	83	Vento X	PolG	0	0	0	48	95	0	0	56
HE 240 A					95	0	0	56	159	0	0	15
HE 240 A	83	84	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	83	84	QP Solai	PolG	0	0	0	48	91	0	0	56
HE 240 A					91	0	0	56	148	0	0	15
HE 240 A	83	84	QV Solai	PolG	0	0	0	15	91	0	0	18
HE 240 A					91	0	0	18	148	0	0	5
HE 240 A	83	84	Neve	PolG	0	0	0	30	91	0	0	35
HE 240 A					91	0	0	35	148	0	0	10
HE 240 A	83	84	Vento X	PolG	0	0	0	46	91	0	0	54
HE 240 A					91	0	0	54	148	0	0	15
HE 240 A	84	85	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	84	85	QP Solai	PolG	0	0	0	46	85	0	0	54
HE 240 A					85	0	0	54	134	0	0	15
HE 240 A	84	85	QV Solai	PolG	0	0	0	15	85	0	0	17
HE 240 A					85	0	0	17	134	0	0	5
HE 240 A	84	85	Neve	PolG	0	0	0	28	85	0	0	34
HE 240 A					85	0	0	34	134	0	0	10
HE 240 A	84	85	Vento X	PolG	0	0	0	44	85	0	0	52
HE 240 A					85	0	0	52	134	0	0	15
HE 240 A	85	86	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	85	86	QP Solai	PolG	0	0	0	43	80	0	0	52
HE 240 A					80	0	0	52	123	0	0	15
HE 240 A	85	86	QV Solai	PolG	0	0	0	14	80	0	0	17
HE 240 A					80	0	0	17	123	0	0	5
HE 240 A	85	86	Neve	PolG	0	0	0	27	80	0	0	32
HE 240 A					80	0	0	32	123	0	0	10
HE 240 A	85	86	Vento X	PolG	0	0	0	42	80	0	0	50
HE 240 A					80	0	0	50	123	0	0	15
HE 240 A	86	87	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	86	87	QP Solai	PolG	0	0	0	41	76	0	0	50
HE 240 A					76	0	0	50	113	0	0	15
HE 240 A	86	87	QV Solai	PolG	0	0	0	13	76	0	0	16
HE 240 A					76	0	0	16	113	0	0	5
HE 240 A	86	87	Neve	PolG	0	0	0	26	76	0	0	31
HE 240 A					76	0	0	31	113	0	0	10
HE 240 A	86	87	Vento X	PolG	0	0	0	40	76	0	0	48
HE 240 A					76	0	0	48	113	0	0	15
HE 240 A	87	88	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
HE 240 A	87	88	QP Solai	PolG	0	0	0	39	75	0	0	48
HE 240 A					75	0	0	48	108	0	0	15
HE 240 A	87	88	QV Solai	PolG	0	0	0	12	75	0	0	15
HE 240 A					75	0	0	15	108	0	0	5
HE 240 A	87	88	Neve	PolG	0	0	0	24	75	0	0	30
HE 240 A					75	0	0	30	108	0	0	10
HE 240 A	87	88	Vento X	PolG	0	0	0	37	75	0	0	46

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	88	21	Peso Proprio	UnifG	75	0	0	46	108	0	0	15
HE 240 A	88	21	QP Solai	PolG	0	0	0	60	111	0	0	60
HE 240 A	88	21	QV Solai	PolG	79	0	0	46	111	0	0	15
HE 240 A	88	21	Neve	PolG	79	0	0	15	111	0	0	5
HE 240 A	88	21	Vento X	PolG	79	0	0	23	79	0	0	28
HE 240 A	88	21		PolG	79	0	0	35	79	0	0	44
Trave 8013												
IPE 100	23	29	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	24	26	Peso Proprio	UnifG	0	0	0	8	161	0	0	8
IPE 100	25	27	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	26	31	Peso Proprio	UnifG	0	0	0	8	137	0	0	8
IPE 100	27	23	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	28	25	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	29	30	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	30	24	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	31	32	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	32	33	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
Trave 8014												
IPE 100	12	13	Peso Proprio	UnifG	0	0	0	8	162	0	0	8
IPE 100	12	13	QP Solai	PolG	0	0	0	71	139	0	0	71
IPE 100	12	13	QV Solai	PolG	139	0	0	23	139	0	0	23
IPE 100	12	13	Neve	PolG	139	0	0	23	150	0	0	2
IPE 100	12	13	Vento X	PolG	0	0	0	44	139	0	0	44
IPE 100	13	14	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	13	14	QP Solai	PolG	0	0	0	71	133	0	0	71
IPE 100	13	14	QV Solai	PolG	133	0	0	23	133	0	0	23
IPE 100	13	14	Neve	PolG	133	0	0	23	150	0	0	4
IPE 100	13	14	Vento X	PolG	0	0	0	44	133	0	0	44
IPE 100	14	15	Peso Proprio	UnifG	0	0	0	68	133	0	0	68
IPE 100	14	15	QP Solai	PolG	0	0	0	8	137	0	0	8
IPE 100	14	15	QV Solai	PolG	126	0	0	71	126	0	0	71
IPE 100	14	15	Neve	PolG	0	0	0	23	126	0	0	19
IPE 100	14	15	Vento X	PolG	126	0	0	23	149	0	0	23
IPE 100	14	15		PolG	0	0	0	44	126	0	0	44
IPE 100	14	15	Vento X	PolG	126	0	0	68	126	0	0	68
IPE 100	15	16	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	15	16	QP Solai	PolG	0	0	0	71	126	0	0	71
IPE 100	15	16	QV Solai	PolG	126	0	0	23	126	0	0	23
IPE 100	15	16	Neve	PolG	0	0	0	44	126	0	0	44
IPE 100	15	16	Vento X	PolG	126	0	0	44	126	0	0	44
IPE 100	16	17	Peso Proprio	UnifG	0	0	0	8	162	0	0	8
IPE 100	16	17	QP Solai	PolG	0	0	0	71	126	0	0	71
IPE 100	16	17	QV Solai	PolG	126	0	0	23	126	0	0	23
IPE 100	16	17	Neve	PolG	0	0	0	23	149	0	0	7
IPE 100	16	17	Vento X	PolG	126	0	0	44	126	0	0	44
IPE 100	16	17		PolG	0	0	0	68	126	0	0	68

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	17	18	Peso Proprio	UnifG	126	0	0	68	149	0	0	21
IPE 100	17	18	QP Solai	PolG	0	0	0	71	120	0	0	71
IPE 100	17	18	QV Solai	PolG	120	0	0	23	120	0	0	23
IPE 100	17	18	Neve	PolG	120	0	0	44	120	0	0	44
IPE 100	17	18	Vento X	PolG	120	0	0	68	120	0	0	68
IPE 100	18	19	Peso Proprio	UnifG	120	0	0	8	149	0	0	8
IPE 100	18	19	QP Solai	PolG	129	0	0	71	149	0	0	71
IPE 100	18	19	QV Solai	PolG	129	0	0	23	129	0	0	23
IPE 100	18	19	Neve	PolG	129	0	0	44	129	0	0	44
IPE 100	18	19	Vento X	PolG	129	0	0	68	129	0	0	68
IPE 100	19	20	Peso Proprio	UnifG	129	0	0	8	149	0	0	8
IPE 100	19	20	QP Solai	PolG	123	0	0	71	123	0	0	71
IPE 100	19	20	QV Solai	PolG	123	0	0	23	123	0	0	23
IPE 100	19	20	Neve	PolG	117	0	0	44	117	0	0	44
IPE 100	20	21	Peso Proprio	UnifG	117	0	0	68	117	0	0	68
IPE 100	20	21	QP Solai	PolG	117	0	0	71	117	0	0	71
IPE 100	20	21	QV Solai	PolG	117	0	0	23	117	0	0	23
IPE 100	20	21	Neve	PolG	117	0	0	44	117	0	0	44
IPE 100	20	21	Vento X	PolG	117	0	0	68	117	0	0	68
IPE 100	21	22	Peso Proprio	UnifG	117	0	0	8	150	0	0	8
IPE 100	21	22	QP Solai	PolG	111	0	0	71	150	0	0	71
IPE 100	21	22	QV Solai	PolG	111	0	0	23	111	0	0	23
IPE 100	21	22	Neve	PolG	111	0	0	44	111	0	0	44
IPE 100	21	22	Vento X	PolG	111	0	0	68	111	0	0	68
Trave 8015												
IPE 100	1	19	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	1	19	QP Solai	PolG	23	0	0	90	23	0	0	140
IPE 100	1	19	QV Solai	PolG	126	0	0	140	150	0	0	91
IPE 100	1	19	Neve	PolG	23	0	0	29	23	0	0	45
IPE 100	1	19	Vento X	PolG	126	0	0	45	126	0	0	45
IPE 100	1	19		PolG	0	0	0	43	126	0	0	43
IPE 100	1	19	Neve	PolG	126	0	0	43	150	0	0	13
IPE 100	1	19	Vento X	PolG	23	0	0	67	126	0	0	67
IPE 100	1	19	Vento X	PolG	126	0	0	67	150	0	0	20
IPE 100	4	25	Peso Proprio	UnifG	23	0	0	68	150	0	0	68
IPE 100	4	25	QP Solai	PolG	0	0	0	8	143	0	0	8
IPE 100					20	0	0	90	20	0	0	140
IPE 100					117	0	0	140	143	0	0	91

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	OZi	Xf	QXf	QYf	OZf
IPE 100	4	25	QV Solai	PolG	0	0	0	29	20	0	0	45
					20	0	0	45	117	0	0	45
IPE 100	4	25	Neve	PolG	0	0	0	43	117	0	0	29
					117	0	0	43	143	0	0	43
IPE 100	4	25	Neve	PolG	0	0	0	13	20	0	0	44
					20	0	0	44	143	0	0	44
IPE 100	4	25	Vento X	PolG	0	0	0	67	117	0	0	67
					117	0	0	67	143	0	0	19
IPE 100	4	25	Vento X	PolG	0	0	0	20	20	0	0	68
					20	0	0	68	143	0	0	68
IPE 100	7	10	Peso Proprio	UnifG	0	0	0	8	144	0	0	8
IPE 100	7	10	QP Solai	PolG	0	0	0	76	5	0	0	140
					5	0	0	140	133	0	0	140
IPE 100	7	10	QV Solai	PolG	0	0	0	24	5	0	0	45
					5	0	0	45	133	0	0	45
IPE 100	7	10	Neve	PolG	0	0	0	45	144	0	0	25
					133	0	0	4	5	0	0	44
IPE 100	7	10	Neve	PolG	0	0	0	44	144	0	0	44
					5	0	0	43	133	0	0	43
IPE 100	7	10	Vento X	PolG	0	0	0	43	144	0	0	4
					133	0	0	67	133	0	0	67
IPE 100	7	10	Vento X	PolG	0	0	0	67	144	0	0	7
					133	0	0	7	5	0	0	68
IPE 100	10	13	Peso Proprio	UnifG	0	0	0	8	144	0	0	8
IPE 100	10	13	QP Solai	PolG	0	0	0	82	11	0	0	140
					11	0	0	140	127	0	0	140
IPE 100	10	13	QV Solai	PolG	0	0	0	140	144	0	0	83
					127	0	0	26	11	0	0	45
IPE 100	10	13			11	0	0	45	127	0	0	45
					127	0	0	45	144	0	0	27
IPE 100	10	13	Neve	PolG	0	0	0	43	127	0	0	43
					127	0	0	43	144	0	0	8
IPE 100	10	13	Neve	PolG	0	0	0	8	11	0	0	44
					11	0	0	44	144	0	0	44
IPE 100	10	13	Vento X	PolG	0	0	0	12	11	0	0	68
					11	0	0	68	144	0	0	68
IPE 100	10	13	Vento X	PolG	0	0	0	67	127	0	0	67
					127	0	0	67	144	0	0	12
IPE 100	13	1	Peso Proprio	UnifG	0	0	0	8	143	0	0	8
IPE 100	13	1	QP Solai	PolG	0	0	0	87	17	0	0	140
					17	0	0	140	120	0	0	140
IPE 100	13	1	QV Solai	PolG	0	0	0	28	17	0	0	45
					17	0	0	45	120	0	0	45
IPE 100	13	1	Neve	PolG	0	0	0	45	143	0	0	28
					120	0	0	43	120	0	0	43
IPE 100	13	1	Neve	PolG	0	0	0	43	143	0	0	11
					120	0	0	11	17	0	0	44
IPE 100	13	1	Neve	PolG	0	0	0	44	143	0	0	44
					17	0	0	44	143	0	0	68
IPE 100	13	1	Vento X	PolG	0	0	0	17	17	0	0	68
					17	0	0	68	143	0	0	68
IPE 100	13	1	Vento X	PolG	0	0	0	67	120	0	0	67
					120	0	0	67	143	0	0	17
IPE 100	16	22	Peso Proprio	UnifG	0	0	0	8	144	0	0	8
IPE 100	16	22	QP Solai	PolG	0	0	0	92	24	0	0	140
					24	0	0	140	114	0	0	140
IPE 100	16	22	QV Solai	PolG	0	0	0	140	144	0	0	93
					0	0	0	30	24	0	0	45
IPE 100	16	22	Neve	PolG	0	0	0	45	114	0	0	45
					114	0	0	45	144	0	0	30
IPE 100	16	22	Neve	PolG	0	0	0	43	114	0	0	43
					114	0	0	43	144	0	0	14
IPE 100	16	22	Neve	PolG	0	0	0	14	24	0	0	44

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	OZi	Xf	QXf	QYf	OZf
IPE 100	16	22	Vento X	PolG	0	0	0	22	144	0	0	44
					24	0	0	22	144	0	0	68
IPE 100	16	22	Vento X	PolG	0	0	0	68	144	0	0	68
					114	0	0	67	114	0	0	21
IPE 100	19	16	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	19	16	QP Solai	PolG	0	0	0	91	23	0	0	140
					23	0	0	140	126	0	0	140
IPE 100	19	16	QV Solai	PolG	0	0	0	140	149	0	0	92
					126	0	0	29	23	0	0	45
IPE 100	19	16			23	0	0	45	126	0	0	45
IPE 100	19	16	Neve	PolG	0	0	0	45	149	0	0	29
					126	0	0	43	126	0	0	43
IPE 100	19	16	Neve	PolG	0	0	0	43	149	0	0	13
					23	0	0	13	23	0	0	44
IPE 100	19	16	Vento X	PolG	0	0	0	44	149	0	0	44
					126	0	0	67	126	0	0	67
IPE 100	19	16	Vento X	PolG	0	0	0	67	149	0	0	20
					23	0	0	21	23	0	0	68
IPE 100	22	4	Peso Proprio	UnifG	0	0	0	68	149	0	0	68
IPE 100	22	4	QP Solai	PolG	0	0	0	8	143	0	0	8
					14	0	0	84	14	0	0	140
IPE 100	22	4			14	0	0	140	123	0	0	140
IPE 100	22	4	QV Solai	PolG	0	0	0	140	143	0	0	85
					123	0	0	27	14	0	0	45
IPE 100	22	4			14	0	0	45	123	0	0	45
IPE 100	22	4	Neve	PolG	0	0	0	45	143	0	0	27
					123	0	0	9	14	0	0	44
IPE 100	22	4	Neve	PolG	0	0	0	44	143	0	0	44
					14	0	0	43	123	0	0	43
IPE 100	22	4	Vento X	PolG	0	0	0	43	143	0	0	9
					123	0	0	67	123	0	0	67
IPE 100	22	4	Vento X	PolG	0	0	0	67	143	0	0	14
					123	0	0	14	14	0	0	68
IPE 100	25	28	Peso Proprio	UnifG	0	0	0	8	143	0	0	8
IPE 100	25	28	QP Solai	PolG	0	0	0	95	27	0	0	140
					27	0	0	140	111	0	0	140
IPE 100	25	28	QV Solai	PolG	0	0	0	140	144	0	0	96
					111	0	0	30	27	0	0	45
IPE 100	25	28			27	0	0	45	111	0	0	45
					111	0	0	45	144	0	0	31
IPE 100	25	28	Neve	PolG	0	0	0	43	111	0	0	43
					111	0	0	43	144	0	0	16
IPE 100	25	28	Neve	PolG	0	0	0	16	27	0	0	44
					27	0	0	44	144	0	0	44
IPE 100	25	28	Vento X	PolG	0	0	0	25	27	0	0	68
					27	0	0	68	144	0	0	68
IPE 100	25	28	Vento X	PolG	0	0	0	67	111	0	0	67
					111	0	0	67	144	0	0	24
IPE 100	28	31	Peso Proprio	UnifG	0	0	0	8	144	0	0	8
IPE 100	28	31	QP Solai	PolG	0	0	0	102	33	0	0	140
					33	0	0	140	105	0	0	140
IPE 100	28	31	QV Solai	PolG	0	0	0	140	144	0	0	102
					105	0	0	33	33	0	0	45
IPE 100	28	31	QV Solai	PolG	0	0	0	45	105	0	0	45
					33	0	0	45	144	0	0	33
IPE 100	28	31	Neve	PolG	0	0	0	43	105	0	0	43
					105	0	0	43	144	0	0	19
IPE 100	28	31	Neve	PolG	0	0	0	20	33	0	0	44
					33	0	0	44	144	0	0	44
IPE 100	28	31	Vento X	PolG	0	0	0	31	33	0	0	68
					33	0	0	68	144	0	0	68
IPE 100	28	31	Vento X	PolG	0	0	0	67	105	0	0	67
					105	0	0	67	144	0	0	30
Trave 8016					105	0	0	67	144	0	0	30

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	2	20	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	2	20	QV Solai	PolG	0	0	0	87	23	0	0	135
					23	0	0	135	126	0	0	135
					126	0	0	135	150	0	0	89
IPE 100	2	20	QV Solai	PolG	0	0	0	28	23	0	0	43
					23	0	0	43	126	0	0	43
					126	0	0	43	150	0	0	28
IPE 100	2	20	Neve	PolG	0	0	0	41	126	0	0	41
					126	0	0	41	150	0	0	12
IPE 100	2	20	Neve	PolG	0	0	0	13	23	0	0	43
					23	0	0	43	150	0	0	43
IPE 100	2	20	Vento X	PolG	0	0	0	64	126	0	0	64
					126	0	0	64	150	0	0	19
IPE 100	2	20	Vento X	PolG	0	0	0	64	150	0	0	19
					23	0	0	20	23	0	0	67
IPE 100	5	26	Peso Proprio	UnifG	0	0	0	8	137	0	0	8
IPE 100	5	26	QV Solai	PolG	0	0	0	85	20	0	0	135
					20	0	0	135	111	0	0	135
					111	0	0	135	137	0	0	87
IPE 100	5	26	QV Solai	PolG	0	0	0	27	20	0	0	43
					20	0	0	43	111	0	0	43
					111	0	0	43	137	0	0	28
IPE 100	5	26	Neve	PolG	0	0	0	41	111	0	0	41
					111	0	0	41	137	0	0	11
IPE 100	5	26	Neve	PolG	0	0	0	12	20	0	0	43
					20	0	0	43	137	0	0	43
IPE 100	5	26	Vento X	PolG	0	0	0	64	111	0	0	64
					111	0	0	64	137	0	0	17
IPE 100	5	26	Vento X	PolG	0	0	0	18	20	0	0	67
					20	0	0	67	137	0	0	67
IPE 100	8	11	Peso Proprio	UnifG	0	0	0	8	138	0	0	8
IPE 100	8	11	QV Solai	PolG	0	0	0	73	5	0	0	135
					5	0	0	135	127	0	0	135
IPE 100	8	11	QV Solai	PolG	0	0	0	135	138	0	0	76
					5	0	0	23	5	0	0	43
					127	0	0	43	127	0	0	43
IPE 100	8	11	Neve	PolG	0	0	0	4	5	0	0	43
					5	0	0	43	138	0	0	43
IPE 100	8	11	Neve	PolG	0	0	0	41	127	0	0	41
					127	0	0	41	138	0	0	4
IPE 100	8	11	Vento X	PolG	0	0	0	6	5	0	0	67
					5	0	0	67	138	0	0	67
IPE 100	8	11	Vento X	PolG	0	0	0	64	127	0	0	64
					127	0	0	64	138	0	0	6
IPE 100	11	14	Peso Proprio	UnifG	0	0	0	8	138	0	0	8
IPE 100	11	14	QV Solai	PolG	0	0	0	78	11	0	0	135
					11	0	0	135	121	0	0	135
					121	0	0	135	138	0	0	80
IPE 100	11	14	QV Solai	PolG	0	0	0	25	11	0	0	43
					11	0	0	43	121	0	0	43
					121	0	0	43	138	0	0	26
IPE 100	11	14	Neve	PolG	0	0	0	41	121	0	0	41
					121	0	0	41	138	0	0	7
IPE 100	11	14	Neve	PolG	0	0	0	7	11	0	0	43
					11	0	0	43	138	0	0	43
IPE 100	11	14	Vento X	PolG	0	0	0	64	121	0	0	64
					121	0	0	64	138	0	0	11
IPE 100	11	14	Vento X	PolG	0	0	0	11	11	0	0	67
					11	0	0	67	138	0	0	67
IPE 100	14	2	Peso Proprio	UnifG	0	0	0	8	137	0	0	8
IPE 100	14	2	QV Solai	PolG	0	0	0	83	17	0	0	135
					17	0	0	135	114	0	0	135
					114	0	0	135	137	0	0	85
IPE 100	14	2	QV Solai	PolG	0	0	0	27	17	0	0	43
					17	0	0	43	114	0	0	43

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	14	2	Neve	PolG	114	0	0	43	137	0	0	27
					114	0	0	41	114	0	0	41
IPE 100	14	2	Neve	PolG	0	0	0	10	17	0	0	43
					17	0	0	43	137	0	0	43
IPE 100	14	2	Vento X	PolG	0	0	0	64	114	0	0	64
					114	0	0	64	137	0	0	15
IPE 100	14	2	Vento X	PolG	0	0	0	16	17	0	0	67
					17	0	0	67	137	0	0	67
IPE 100	17	23	Peso Proprio	UnifG	0	0	0	8	138	0	0	8
IPE 100	17	23	QV Solai	PolG	0	0	0	88	24	0	0	135
					24	0	0	135	108	0	0	135
IPE 100	17	23	QV Solai	PolG	0	0	0	28	24	0	0	43
					24	0	0	43	108	0	0	43
IPE 100	17	23	Neve	PolG	0	0	0	13	24	0	0	29
					24	0	0	43	138	0	0	43
IPE 100	17	23	Neve	PolG	0	0	0	41	108	0	0	41
					108	0	0	41	138	0	0	13
IPE 100	17	23	Vento X	PolG	0	0	0	64	108	0	0	64
					108	0	0	64	138	0	0	20
IPE 100	17	23	Vento X	PolG	0	0	0	21	24	0	0	67
					24	0	0	67	138	0	0	67
IPE 100	20	17	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	20	17	QV Solai	PolG	0	0	0	87	23	0	0	135
					23	0	0	135	126	0	0	135
IPE 100	20	17	Neve	PolG	0	0	0	41	126	0	0	41
					126	0	0	41	149	0	0	12
IPE 100	20	17	Neve	PolG	0	0	0	13	23	0	0	43
					23	0	0	43	149	0	0	43
IPE 100	20	17	Vento X	PolG	0	0	0	64	126	0	0	64
					126	0	0	64	149	0	0	19
IPE 100	20	17	Vento X	PolG	0	0	0	20	23	0	0	67
					23	0	0	67	149	0	0	67
IPE 100	23	5	Peso Proprio	UnifG	0	0	0	8	137	0	0	8
IPE 100	23	5	QV Solai	PolG	0	0	0	80	14	0	0	135
					14	0	0	135	117	0	0	135
					117	0	0	135	137	0	0	83
IPE 100	23	5	QV Solai	PolG	0	0	0	26	14	0	0	43
					14	0	0	43	117	0	0	43
IPE 100	23	5	Neve	PolG	0	0	0	41	117	0	0	41
					117	0	0	41	137	0	0	8
IPE 100	23	5	Neve	PolG	0	0	0	9	14	0	0	43
					14	0	0	43	137	0	0	43
IPE 100	23	5	Vento X	PolG	0	0	0	14	14	0	0	67
					14	0	0	67	137	0	0	67
IPE 100	23	5	Vento X	PolG	0	0	0	64	117	0	0	64
					117	0	0	64	137	0	0	13
IPE 100	26	29	Peso Proprio	UnifG	0	0	0	8	138	0	0	8
IPE 100	26	29	QV Solai	PolG	0	0	0	90	27	0	0	135
					27	0	0	135	105	0	0	135
					105	0	0	135	138	0	0	92
IPE 100	26	29	QV Solai	PolG	0	0	0	29	27	0	0	43
					27	0	0	43	105	0	0	43
					105	0	0	43	138	0	0	30
IPE 100	26	29	Neve	PolG	0	0	0	41	105	0	0	41
					105	0	0	41	138	0	0	14
IPE 100	26	29	Neve	PolG	0	0	0	15	27	0	0	43
					27	0	0	43	138	0	0	43
IPE 100	26	29	Vento X	PolG	0	0	0	64	105	0	0	64

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	26	29	Vento X	PolG	105	0	0	64	138	0	0	22
IPE 100	29	32	Peso Proprio	UnifG	27	0	0	67	138	0	0	67
IPE 100	29	32	QV Solai	PolG	0	0	0	8	138	0	0	8
IPE 100	33	0			33	0	0	135	98	0	0	135
IPE 100	29	32	QV Solai	PolG	98	0	0	135	138	0	0	98
IPE 100	33	0			33	0	0	43	98	0	0	43
IPE 100	29	32	Neve	PolG	0	0	0	19	33	0	0	43
IPE 100	29	32	Neve	PolG	0	0	0	41	98	0	0	41
IPE 100	29	32	Vento X	PolG	98	0	0	64	98	0	0	64
IPE 100	29	32	Vento X	PolG	98	0	0	64	138	0	0	28
IPE 100	29	32	Vento X	PolG	0	0	0	29	33	0	0	67
IPE 100	33	0			33	0	0	67	138	0	0	67
Trave 8017												
IPE 100	3	21	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	3	21	QV Solai	PolG	0	0	0	81	23	0	0	128
IPE 100	126	0			126	0	0	128	126	0	0	128
IPE 100	3	21	QV Solai	PolG	0	0	0	26	23	0	0	41
IPE 100	23	0			23	0	0	41	126	0	0	41
IPE 100	126	0			126	0	0	41	150	0	0	27
IPE 100	3	21	Neve	PolG	0	0	0	38	126	0	0	38
IPE 100	126	0			126	0	0	38	150	0	0	11
IPE 100	3	21	Neve	PolG	0	0	0	12	23	0	0	41
IPE 100	23	0			23	0	0	41	150	0	0	41
IPE 100	3	21	Vento X	PolG	0	0	0	59	126	0	0	59
IPE 100	126	0			126	0	0	59	150	0	0	18
IPE 100	3	21	Vento X	PolG	0	0	0	19	23	0	0	64
IPE 100	23	0			23	0	0	64	150	0	0	64
IPE 100	6	27	Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	6	27	QV Solai	PolG	0	0	0	79	20	0	0	128
IPE 100	20	0			20	0	0	128	105	0	0	128
IPE 100	6	27	QV Solai	PolG	0	0	0	25	20	0	0	41
IPE 100	20	0			20	0	0	41	105	0	0	41
IPE 100	105	0			105	0	0	41	131	0	0	26
IPE 100	6	27	Neve	PolG	0	0	0	38	105	0	0	38
IPE 100	105	0			105	0	0	38	131	0	0	10
IPE 100	6	27	Neve	PolG	0	0	0	11	20	0	0	41
IPE 100	20	0			20	0	0	41	131	0	0	41
IPE 100	6	27	Vento X	PolG	0	0	0	59	105	0	0	59
IPE 100	105	0			105	0	0	59	131	0	0	16
IPE 100	6	27	Vento X	PolG	0	0	0	17	20	0	0	64
IPE 100	20	0			20	0	0	64	131	0	0	64
IPE 100	9	12	Peso Proprio	UnifG	0	0	0	8	132	0	0	8
IPE 100	9	12	QV Solai	PolG	0	0	0	68	5	0	0	128
IPE 100	5	0			5	0	0	128	121	0	0	128
IPE 100	121	0			121	0	0	128	132	0	0	72
IPE 100	0	0			0	0	0	22	5	0	0	41
IPE 100	5	0			5	0	0	41	121	0	0	41
IPE 100	121	0			121	0	0	41	132	0	0	23
IPE 100	0	0			0	0	0	38	121	0	0	38
IPE 100	121	0			121	0	0	38	132	0	0	4
IPE 100	9	12	Neve	PolG	0	0	0	4	5	0	0	41
IPE 100	5	0			5	0	0	41	132	0	0	41
IPE 100	9	12	Vento X	PolG	0	0	0	6	5	0	0	64
IPE 100	5	0			5	0	0	64	132	0	0	64
IPE 100	9	12	Vento X	PolG	0	0	0	59	121	0	0	59
IPE 100	121	0			121	0	0	59	132	0	0	5
IPE 100	12	15	Peso Proprio	UnifG	0	0	0	8	132	0	0	8
IPE 100	12	15	QV Solai	PolG	0	0	0	72	11	0	0	128

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	12	15	QV Solai	PolG	115	0	0	128	115	0	0	128
IPE 100	115	0			115	0	0	128	132	0	0	76
IPE 100	11	0			11	0	0	41	132	0	0	41
IPE 100	115	0			115	0	0	41	132	0	0	24
IPE 100	12	15	Neve	PolG	0	0	0	38	115	0	0	38
IPE 100	115	0			115	0	0	38	132	0	0	6
IPE 100	12	15	Neve	PolG	0	0	0	7	11	0	0	41
IPE 100	11	0			11	0	0	41	132	0	0	41
IPE 100	12	15	Vento X	PolG	0	0	0	10	11	0	0	64
IPE 100	11	0			11	0	0	64	132	0	0	64
IPE 100	12	15	Vento X	PolG	0	0	0	59	115	0	0	59
IPE 100	115	0			115	0	0	59	132	0	0	10
IPE 100	15	3	Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	15	3	QV Solai	PolG	0	0	0	77	17	0	0	128
IPE 100	17	0			17	0	0	128	108	0	0	128
IPE 100	108	0			108	0	0	128	131	0	0	80
IPE 100	15	3	QV Solai	PolG	0	0	0	25	17	0	0	41
IPE 100	17	0			17	0	0	41	108	0	0	41
IPE 100	108	0			108	0	0	41	131	0	0	26
IPE 100	15	3	Neve	PolG	0	0	0	38	108	0	0	38
IPE 100	108	0			108	0	0	38	131	0	0	9
IPE 100	15	3	Neve	PolG	0	0	0	10	17	0	0	41
IPE 100	17	0			17	0	0	41	131	0	0	41
IPE 100	15	3	Vento X	PolG	0	0	0	15	17	0	0	64
IPE 100	17	0			17	0	0	64	131	0	0	64
IPE 100	15	3	Vento X	PolG	0	0	0	59	108	0	0	59
IPE 100	108	0			108	0	0	59	131	0	0	14
IPE 100	18	24	Peso Proprio	UnifG	0	0	0	8	132	0	0	8
IPE 100	18	24	QV Solai	PolG	0	0	0	82	24	0	0	128
IPE 100	24	0			24	0	0	128	102	0	0	128
IPE 100	102	0			102	0	0	26	24	0	0	85
IPE 100	18	24	QV Solai	PolG	0	0	0	26	24	0	0	41
IPE 100	24	0			24	0	0	41	102	0	0	41
IPE 100	102	0			102	0	0	12	24	0	0	41
IPE 100	18	24	Neve	PolG	0	0	0	38	102	0	0	38
IPE 100	102	0			102	0	0	38	132	0	0	11
IPE 100	18	24	Vento X	PolG	0	0	0	59	102	0	0	59
IPE 100	102	0			102	0	0	59	132	0	0	18
IPE 100	18	24	Vento X	PolG	0	0	0	19	24	0	0	64
IPE 100	24	0			24	0	0	64	132	0	0	64
IPE 100	21	18	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	21	18	QV Solai	PolG	0	0	0	82	23	0	0	128
IPE 100	23	0			23	0	0	128	126	0	0	128
IPE 100	126	0			126	0	0	128	149	0	0	85
IPE 100	21	18	QV Solai	PolG	0	0	0	26	23	0	0	41
IPE 100	23	0			23	0	0	41	126	0	0	41
IPE 100	126	0			126	0	0	41	149	0	0	41
IPE 100	21	18	Neve	PolG	0	0	0	38	126	0	0	38
IPE 100	21	18	Vento X	PolG	0	0	0	59	126	0	0	59
IPE 100	21	18	Vento X	PolG	0	0	0	19	23	0	0	18
IPE 100	21	18	Vento X	PolG	0	0	0	19	23	0	0	64
IPE 100	24	6	Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	24	6	QV Solai	PolG	0	0	0	75	14	0	0	128
IPE 100	14	0			14	0	0	128	131	0	0	78
IPE 100	24	6	QV Solai	PolG	0	0	0	24	14	0	0	41
IPE 100	14	0			14	0	0	41	111	0	0	41
IPE 100	111	0			111	0	0	41	131	0	0	25
IPE 100	24	6	Neve	PolG	0	0	0	8	14	0	0	41

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	24	6	Neve	PolG	14	0	0	41	131	0	0	41
IPE 100					0	0	0	38	111	0	0	38
IPE 100	24	6	Vento X	PolG	111	0	0	38	131	0	0	7
IPE 100					0	0	0	12	14	0	0	64
IPE 100					14	0	0	64	131	0	0	64
IPE 100	24	6	Vento X	PolG	0	0	0	59	111	0	0	59
IPE 100					111	0	0	59	131	0	0	11
IPE 100	27	30	Peso Proprio	UnifG	0	0	0	8	132	0	0	8
IPE 100	27	30	QP Solai	PolG	0	0	0	84	27	0	0	128
IPE 100					27	0	0	128	99	0	0	128
IPE 100					99	0	0	128	132	0	0	87
IPE 100	27	30	QV Solai	PolG	0	0	0	27	27	0	0	41
IPE 100					27	0	0	41	99	0	0	41
IPE 100	27	30	Neve	PolG	99	0	0	41	132	0	0	28
IPE 100					99	0	0	38	99	0	0	38
IPE 100	27	30	Neve	PolG	0	0	0	38	132	0	0	13
IPE 100					99	0	0	14	27	0	0	41
IPE 100	27	30	Vento X	PolG	27	0	0	41	132	0	0	41
IPE 100					99	0	0	59	99	0	0	59
IPE 100					99	0	0	59	132	0	0	20
IPE 100	27	30	Vento X	PolG	0	0	0	21	27	0	0	64
IPE 100					27	0	0	64	132	0	0	64
IPE 100	30	33	Peso Proprio	UnifG	0	0	0	8	132	0	0	8
IPE 100	30	33	QP Solai	PolG	0	0	0	90	33	0	0	128
IPE 100					33	0	0	128	92	0	0	128
IPE 100					92	0	0	128	132	0	0	92
IPE 100	30	33	QV Solai	PolG	0	0	0	29	33	0	0	41
IPE 100					33	0	0	41	92	0	0	41
IPE 100	30	33	Neve	PolG	0	0	0	41	132	0	0	29
IPE 100					92	0	0	38	92	0	0	38
IPE 100	30	33	Neve	PolG	0	0	0	38	132	0	0	16
IPE 100					92	0	0	17	33	0	0	41
IPE 100	30	33	Vento X	PolG	33	0	0	41	132	0	0	41
IPE 100					33	0	0	27	33	0	0	64
IPE 100	30	33	Vento X	PolG	0	0	0	64	132	0	0	64
IPE 100					33	0	0	59	92	0	0	59
IPE 100					92	0	0	59	132	0	0	25
Trave 8018												
IPE 100	23	59	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	23	59	QP Solai	PolG	0	0	0	76	23	0	0	119
IPE 100					23	0	0	119	126	0	0	119
IPE 100					126	0	0	119	150	0	0	79
IPE 100	23	59	QV Solai	PolG	0	0	0	24	23	0	0	38
IPE 100					23	0	0	38	126	0	0	38
IPE 100	23	59	Neve	PolG	126	0	0	38	150	0	0	25
IPE 100					0	0	0	11	23	0	0	38
IPE 100	23	59	Neve	PolG	23	0	0	38	150	0	0	38
IPE 100					126	0	0	36	126	0	0	36
IPE 100	23	59	Vento X	PolG	0	0	0	18	23	0	0	59
IPE 100					23	0	0	59	150	0	0	59
IPE 100	23	59	Vento X	PolG	0	0	0	55	126	0	0	55
IPE 100					126	0	0	55	150	0	0	17
IPE 100	29	71	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	29	71	QP Solai	PolG	0	0	0	73	20	0	0	119
IPE 100					20	0	0	119	99	0	0	119
IPE 100					99	0	0	119	125	0	0	76
IPE 100	29	71	QV Solai	PolG	0	0	0	23	20	0	0	38
IPE 100					20	0	0	38	99	0	0	38
IPE 100	29	71	Neve	PolG	99	0	0	38	125	0	0	24
IPE 100					0	0	0	10	20	0	0	38
IPE 100	29	71	Neve	PolG	20	0	0	38	125	0	0	38
IPE 100					99	0	0	36	99	0	0	36
IPE 100	29	71	Vento X	PolG	0	0	0	15	20	0	0	9
IPE 100					20	0	0	59	125	0	0	59

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	29	71	Vento X	PolG	0	0	0	55	99	0	0	55
IPE 100					99	0	0	55	125	0	0	14
IPE 100	35	41	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	35	41	QP Solai	PolG	0	0	0	63	5	0	0	119
IPE 100					5	0	0	119	115	0	0	119
IPE 100					115	0	0	119	126	0	0	67
IPE 100	35	41	QV Solai	PolG	0	0	0	20	5	0	0	38
IPE 100					5	0	0	38	115	0	0	38
IPE 100	35	41	Neve	PolG	115	0	0	38	126	0	0	21
IPE 100					0	0	0	3	5	0	0	38
IPE 100	35	41	Neve	PolG	5	0	0	38	126	0	0	38
IPE 100					5	0	0	36	115	0	0	36
IPE 100	35	41	Vento X	PolG	115	0	0	36	126	0	0	3
IPE 100					0	0	0	5	5	0	0	59
IPE 100	35	41	Vento X	PolG	5	0	0	59	126	0	0	59
IPE 100					5	0	0	55	115	0	0	55
IPE 100	41	47	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	41	47	QP Solai	PolG	0	0	0	67	11	0	0	119
IPE 100					11	0	0	119	108	0	0	119
IPE 100					108	0	0	119	126	0	0	71
IPE 100	41	47	QV Solai	PolG	0	0	0	22	11	0	0	38
IPE 100					11	0	0	38	108	0	0	38
IPE 100	41	47	Neve	PolG	108	0	0	38	126	0	0	23
IPE 100					0	0	0	6	11	0	0	38
IPE 100	41	47	Neve	PolG	11	0	0	38	126	0	0	38
IPE 100					108	0	0	36	108	0	0	36
IPE 100	41	47	Vento X	PolG	108	0	0	36	126	0	0	5
IPE 100					0	0	0	9	11	0	0	59
IPE 100	41	47	Vento X	PolG	11	0	0	59	126	0	0	59
IPE 100					11	0	0	55	108	0	0	55
IPE 100	41	47	Vento X	PolG	108	0	0	55	126	0	0	8
IPE 100					0	0	0	8	125	0	0	8
IPE 100	47	23	Peso Proprio	UnifG	0	0	0	71	17	0	0	119
IPE 100	47	23	QP Solai	PolG	0	0	0	119	102	0	0	119
IPE 100					17	0	0	119	125	0	0	74
IPE 100	47	23	QV Solai	PolG	102	0	0	23	17	0	0	38
IPE 100					17	0	0	38	102	0	0	38
IPE 100					102	0	0	38	125	0	0	24
IPE 100	47	23	Neve	PolG	0	0	0	36	102	0	0	36
IPE 100					102	0	0	36	125	0	0	8
IPE 100	47	23	Neve	PolG	0	0	0	8	17	0	0	38
IPE 100					17	0	0	38	125	0	0	38
IPE 100	47	23	Vento X	PolG	0	0	0	13	17	0	0	59
IPE 100					17	0	0	59	125	0	0	59
IPE 100	47	23	Vento X	PolG	0	0	0	55	102	0	0	55
IPE 100					102	0	0	55	125	0	0	12
IPE 100	53	65	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	53	65	QP Solai	PolG	0	0	0	75	24	0	0	119
IPE 100					24	0	0	119	96	0	0	119
IPE 100					96	0	0	119	126	0	0	78
IPE 100	53	65	QV Solai	PolG	0	0	0	24	24	0	0	38
IPE 100					24	0	0	38	96	0	0	38
IPE 100					96	0	0	38	126	0	0	25
IPE 100	53	65	Neve	PolG	0	0	0	36	96	0	0	36
IPE 100					96	0	0	36	126	0	0	10
IPE 100	53	65	Neve	PolG	0	0	0	11	24	0	0	38
IPE 100					24	0	0	38	126	0	0	38
IPE 100	53	65	Vento X	PolG	0	0	0	17	24	0	0	59
IPE 100					24	0	0	59	126	0	0	59
IPE 100	53	65	Vento X	PolG	0	0	0	55	96	0	0	55
IPE 100					96	0	0	55	126	0	0	16
IPE 100	59	53	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	59	53	QP Solai	PolG	0	0	0	76	23	0	0	119
IPE 100					23	0	0	119	126	0	0	119

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	59	53	QV Solai	PolG	0	0	0	24	23	0	0	38
					23	0	0	38	126	0	0	38
IPE 100			Neve	PolG	126	0	0	38	149	0	0	36
	59	53			0	0	0	36	126	0	0	36
IPE 100			Neve	PolG	126	0	0	36	149	0	0	11
	59	53			0	0	0	12	23	0	0	38
IPE 100			Vento X	PolG	23	0	0	38	149	0	0	38
	59	53			0	0	0	55	126	0	0	55
IPE 100			Vento X	PolG	126	0	0	55	149	0	0	17
	59	53			0	0	0	18	23	0	0	59
IPE 100			Peso Proprio	UnifG	23	0	0	59	149	0	0	59
	65	29	QP Solai	PolG	0	0	0	8	125	0	0	8
IPE 100					0	0	0	69	14	0	0	119
	65	29			14	0	0	119	105	0	0	119
IPE 100			QV Solai	PolG	105	0	0	119	125	0	0	72
	65	29			0	0	0	22	14	0	0	38
IPE 100			Neve	PolG	14	0	0	38	105	0	0	38
	65	29			105	0	0	38	125	0	0	23
IPE 100			Neve	PolG	0	0	0	36	105	0	0	36
	65	29			105	0	0	36	125	0	0	7
IPE 100			Neve	PolG	0	0	0	7	14	0	0	38
	65	29			14	0	0	38	125	0	0	38
IPE 100			Vento X	PolG	0	0	0	55	105	0	0	55
	65	29			105	0	0	55	125	0	0	10
IPE 100			Vento X	PolG	0	0	0	11	14	0	0	59
	65	29			14	0	0	59	125	0	0	59
IPE 100			Peso Proprio	UnifG	0	0	0	8	126	0	0	8
	71	77	QP Solai	PolG	0	0	0	77	27	0	0	119
IPE 100			Neve	PolG	93	0	0	38	126	0	0	26
	71	77			0	0	0	36	93	0	0	36
IPE 100			Neve	PolG	93	0	0	12	27	0	0	38
	71	77			27	0	0	38	126	0	0	38
IPE 100			Vento X	PolG	0	0	0	19	27	0	0	59
	71	77			27	0	0	59	126	0	0	59
IPE 100			Vento X	PolG	0	0	0	55	93	0	0	55
	71	77			93	0	0	55	126	0	0	17
IPE 100			Peso Proprio	UnifG	0	0	0	8	126	0	0	8
	77	83	QP Solai	PolG	0	0	0	83	33	0	0	119
IPE 100					33	0	0	119	86	0	0	119
	77	83			86	0	0	119	126	0	0	85
IPE 100			QV Solai	PolG	0	0	0	26	33	0	0	38
	77	83			33	0	0	38	86	0	0	38
IPE 100			Neve	PolG	86	0	0	38	126	0	0	27
	77	83			0	0	0	15	33	0	0	38
IPE 100			Neve	PolG	33	0	0	38	126	0	0	38
	77	83			0	0	0	36	86	0	0	36
IPE 100			Vento X	PolG	86	0	0	36	126	0	0	14
	77	83			0	0	0	24	33	0	0	59
IPE 100			Vento X	PolG	33	0	0	59	126	0	0	59
	77	83			0	0	0	55	86	0	0	55
IPE 100					86	0	0	55	126	0	0	22
Trave 8019												
IPE 100	24	60	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
	24	60	QP Solai	PolG	0	0	0	70	23	0	0	110
IPE 100					23	0	0	110	126	0	0	110
IPE 100			QV Solai	PolG	126	0	0	110	150	0	0	73
	24	60			0	0	0	22	23	0	0	35
IPE 100			Neve	PolG	23	0	0	35	126	0	0	35
	24	60			126	0	0	35	150	0	0	24
IPE 100			Vento X	PolG	0	0	0	33	126	0	0	33

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	24	60	Neve	PolG	0	0	0	11	23	0	0	36
	24	60			23	0	0	36	150	0	0	36
IPE 100			Vento X	PolG	0	0	0	17	23	0	0	55
	24	60			23	0	0	55	150	0	0	55
IPE 100			Vento X	PolG	0	0	0	50	126	0	0	50
	24	60			126	0	0	50	150	0	0	15
IPE 100			Peso Proprio	UnifG	0	0	0	8	119	0	0	8
	30	72	QP Solai	PolG	0	0	0	66	20	0	0	110
IPE 100					20	0	0	110	93	0	0	110
IPE 100			QV Solai	PolG	93	0	0	110	119	0	0	70
	30	72			0	0	0	21	20	0	0	35
IPE 100					20	0	0	35	93	0	0	35
	30	72	Neve	PolG	93	0	0	35	119	0	0	22
IPE 100			Neve	PolG	0	0	0	33	93	0	0	33
IPE 100					93	0	0	33	119	0	0	8
IPE 100			Vento X	PolG	0	0	0	9	20	0	0	36
	30	72			20	0	0	36	119	0	0	36
IPE 100			Vento X	PolG	0	0	0	13	20	0	0	55
	30	72			20	0	0	55	119	0	0	55
IPE 100			Vento X	PolG	0	0	0	50	93	0	0	50
	30	72			0	0	0	50	119	0	0	12
IPE 100			Peso Proprio	UnifG	93	0	0	50	119	0	0	8
	36	42	QP Solai	PolG	0	0	0	8	119	0	0	8
IPE 100					0	0	0	57	5	0	0	110
IPE 100			QV Solai	PolG	5	0	0	110	109	0	0	110
	36	42			109	0	0	110	120	0	0	62
IPE 100					0	0	0	18	5	0	0	35
IPE 100			QV Solai	PolG	5	0	0	35	109	0	0	35
	36	42			109	0	0	35	120	0	0	20
IPE 100			Vento X	PolG	0	0	0	50	109	0	0	50
	36	42			109	0	0	50	120	0	0	4
IPE 100			Vento X	PolG	0	0	0	5	5	0	0	55
	36	42			0	0	0	55	120	0	0	55
IPE 100			Peso Proprio	UnifG	5	0	0	8	120	0	0	8
	42	48	QP Solai	PolG	0	0	0	61	11	0	0	110
IPE 100					0	0	0	110	102	0	0	110
IPE 100			QV Solai	PolG	102	0	0	110	120	0	0	65
	42	48			11	0	0	20	11	0	0	35
IPE 100					11	0	0	35	102	0	0	35
IPE 100			Neve	PolG	102	0	0	35	120	0	0	21
	42	48			0	0	0	33	102	0	0	33
IPE 100			Neve	PolG	0	0	0	33	120	0	0	5
	42	48			102	0	0	5	11	0	0	36
IPE 100			Vento X	PolG	11	0	0	36	120	0	0	36
	42	48			102	0	0	50	102	0	0	50
IPE 100			Vento X	PolG	102	0	0	50	120	0	0	7
	42	48			0	0	0	8	11	0	0	55
IPE 100			Peso Proprio	UnifG	11	0	0	55	120	0	0	55
	48	24	QP Solai	PolG	0	0	0	8	119	0	0	8
IPE 100					0	0	0	64	17	0	0	110
	48	24			17	0	0	110	96	0	0	110
IPE 100			QV Solai	PolG	96	0	0	110	119	0	0	68
	48	24			17	0	0	21	17	0	0	35
IPE 100					17	0	0	35	96	0	0	35
IPE 100			Neve	PolG	96	0	0	35	119	0	0	22
	48	24			0	0	0	7	17	0	0	36
IPE 100			Neve	PolG	17	0	0	36	119	0	0	36
	48	24			0	0	0	33	96	0	0	33
IPE 100			Vento X	PolG	96	0	0	33	119	0	0	7
	48	24			17	0	0	12	17	0	0	55
IPE 100			Vento X	PolG	17	0	0	55	119	0	0	55
	48	24			0	0	0	50	96	0	0	50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	54	66	Peso Proprio	UnifG	0	0	0	8	120	0	0	8
IPE 100	54	66	QP Solai	PolG	0	0	0	68	24	0	0	110
					24	0	0	110	90	0	0	110
					90	0	0	110	120	0	0	110
IPE 100	54	66	QV Solai	PolG	0	0	0	22	24	0	0	35
					24	0	0	35	90	0	0	35
					90	0	0	10	24	0	0	23
IPE 100	54	66	Neve	PolG	0	0	0	10	24	0	0	36
					24	0	0	36	120	0	0	36
IPE 100	54	66	Neve	PolG	0	0	0	33	90	0	0	33
					90	0	0	33	120	0	0	9
IPE 100	54	66	Vento X	PolG	0	0	0	15	24	0	0	55
					24	0	0	55	120	0	0	55
IPE 100	54	66	Vento X	PolG	0	0	0	50	90	0	0	50
					90	0	0	50	120	0	0	14
IPE 100	60	54	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	60	54	QP Solai	PolG	0	0	0	70	23	0	0	110
					23	0	0	110	126	0	0	110
					126	0	0	110	149	0	0	73
IPE 100	60	54	QV Solai	PolG	0	0	0	22	23	0	0	35
					23	0	0	35	126	0	0	35
					126	0	0	35	149	0	0	24
IPE 100	60	54	Neve	PolG	0	0	0	11	23	0	0	36
					23	0	0	36	149	0	0	36
IPE 100	60	54	Neve	PolG	0	0	0	33	126	0	0	33
					126	0	0	33	149	0	0	10
IPE 100	60	54	Vento X	PolG	0	0	0	17	23	0	0	55
					23	0	0	55	149	0	0	55
IPE 100	60	54	Vento X	PolG	0	0	0	50	126	0	0	50
					126	0	0	50	149	0	0	15
IPE 100	66	30	Peso Proprio	UnifG	0	0	0	8	119	0	0	8
IPE 100	66	30	QP Solai	PolG	0	0	0	62	14	0	0	110
					14	0	0	110	99	0	0	110
IPE 100	66	30	QV Solai	PolG	0	0	0	20	14	0	0	35
					99	0	0	35	99	0	0	35
					99	0	0	35	119	0	0	21
IPE 100	66	30	Neve	PolG	0	0	0	6	14	0	0	36
					14	0	0	36	119	0	0	36
IPE 100	66	30	Neve	PolG	0	0	0	33	99	0	0	33
					99	0	0	33	119	0	0	6
IPE 100	66	30	Vento X	PolG	0	0	0	50	99	0	0	50
					99	0	0	50	119	0	0	9
IPE 100	66	30	Vento X	PolG	0	0	0	10	14	0	0	55
					14	0	0	55	119	0	0	55
IPE 100	72	78	Peso Proprio	UnifG	0	0	0	8	120	0	0	8
IPE 100	72	78	QP Solai	PolG	0	0	0	70	27	0	0	110
					27	0	0	110	87	0	0	110
IPE 100	72	78	QV Solai	PolG	0	0	0	110	120	0	0	73
					87	0	0	110	27	0	0	35
IPE 100	72	78	Neve	PolG	0	0	0	33	87	0	0	33
					87	0	0	33	120	0	0	10
IPE 100	72	78	Neve	PolG	0	0	0	11	27	0	0	36
					27	0	0	36	120	0	0	36
IPE 100	72	78	Vento X	PolG	0	0	0	50	87	0	0	50
					87	0	0	50	120	0	0	15
IPE 100	72	78	Vento X	PolG	0	0	0	17	27	0	0	55
					27	0	0	55	120	0	0	55
IPE 100	78	84	Peso Proprio	UnifG	0	0	0	8	120	0	0	8
IPE 100	78	84	QP Solai	PolG	0	0	0	75	33	0	0	110
					33	0	0	110	80	0	0	110
					80	0	0	110	120	0	0	77
IPE 100	78	84	QV Solai	PolG	0	0	0	24	33	0	0	35
					33	0	0	35	80	0	0	35

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	78	84	Neve	PolG	0	0	0	35	120	0	0	25
					33	0	0	36	120	0	0	36
IPE 100	78	84	Neve	PolG	0	0	0	33	80	0	0	33
					80	0	0	33	120	0	0	12
IPE 100	78	84	Vento X	PolG	0	0	0	21	33	0	0	55
					33	0	0	55	120	0	0	55
IPE 100	78	84	Vento X	PolG	0	0	0	50	80	0	0	50
					80	0	0	50	120	0	0	19
Trave 80/20												
IPE 100	25	61	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	25	61	QP Solai	PolG	0	0	0	64	23	0	0	100
					23	0	0	100	126	0	0	100
					126	0	0	100	150	0	0	67
IPE 100	25	61	QV Solai	PolG	0	0	0	20	23	0	0	32
					23	0	0	32	126	0	0	32
					126	0	0	32	150	0	0	21
IPE 100	25	61	Neve	PolG	0	0	0	30	126	0	0	30
					126	0	0	30	150	0	0	9
IPE 100	25	61	Neve	PolG	0	0	0	10	23	0	0	33
					23	0	0	33	150	0	0	33
IPE 100	25	61	Vento X	PolG	0	0	0	46	126	0	0	46
					126	0	0	46	150	0	0	14
IPE 100	25	61	Vento X	PolG	0	0	0	15	23	0	0	50
					23	0	0	50	150	0	0	50
IPE 100	31	73	Peso Proprio	UnifG	0	0	0	8	113	0	0	8
IPE 100	31	73	QP Solai	PolG	0	0	0	60	20	0	0	100
					20	0	0	100	87	0	0	100
					87	0	0	100	113	0	0	63
IPE 100	31	73	QV Solai	PolG	0	0	0	19	20	0	0	32
					20	0	0	32	87	0	0	32
					87	0	0	32	113	0	0	20
IPE 100	31	73	Neve	PolG	0	0	0	30	87	0	0	30
					87	0	0	30	113	0	0	7
IPE 100	31	73	Neve	PolG	0	0	0	7	20	0	0	33
					20	0	0	33	113	0	0	33
IPE 100	31	73	Vento X	PolG	0	0	0	12	20	0	0	50
					20	0	0	50	113	0	0	50
IPE 100	31	73	Vento X	PolG	0	0	0	46	87	0	0	46
					87	0	0	46	113	0	0	10
IPE 100	37	43	Peso Proprio	UnifG	0	0	0	8	114	0	0	8
IPE 100	37	43	QP Solai	PolG	0	0	0	52	5	0	0	100
					5	0	0	100	103	0	0	100
					103	0	0	100	114	0	0	56
IPE 100	37	43	QV Solai	PolG	0	0	0	17	5	0	0	32
					5	0	0	32	103	0	0	32
					103	0	0	32	114	0	0	18
IPE 100	37	43	Neve	PolG	0	0	0	30	103	0	0	30
					103	0	0	30	114	0	0	2
IPE 100	37	43	Neve	PolG	0	0	0	3	5	0	0	33
					5	0	0	33	114	0	0	33
IPE 100	37	43	Vento X	PolG	0	0	0	4	5	0	0	50
					5	0	0	50	114	0	0	50
IPE 100	37	43	Vento X	PolG	0	0	0	46	103	0	0	46
					103	0	0	46	114	0	0	4
IPE 100	43	49	Peso Proprio	UnifG	0	0	0	8	113	0	0	8
IPE 100	43	49	QP Solai	PolG	0	0	0	55	11	0	0	100
					11	0	0	100	96	0	0	100
					96	0	0	100	113	0	0	59
IPE 100	43	49	QV Solai	PolG	0	0	0	18	11	0	0	32
					11	0	0	32	96	0	0	32
					96	0	0	32	113	0	0	19
IPE 100	43	49	Neve	PolG	0	0	0	30	96	0	0	30
					96	0	0	30	113	0	0	4
IPE 100	43	49	Neve	PolG	0	0	0	5	11	0	0	33
					11	0	0	33	113	0	0	33

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	43	49	Vento X	PolG	96	0	0	46	96	0	0	46
IPE 100	43	49	Vento X	PolG	0	0	0	46	113	0	0	6
IPE 100	49	25	Peso Proprio	UnifG	11	0	0	50	113	0	0	50
IPE 100	49	25	QP Solai	PolG	0	0	0	8	113	0	0	8
					17	0	0	58	17	0	0	100
IPE 100	49	25	QV Solai	PolG	90	0	0	100	113	0	0	62
					17	0	0	32	90	0	0	32
IPE 100	49	25	Neve	PolG	90	0	0	30	90	0	0	30
IPE 100	49	25	Neve	PolG	90	0	0	30	113	0	0	6
IPE 100	55	67	Peso Proprio	UnifG	17	0	0	33	113	0	0	33
IPE 100	55	67	QP Solai	PolG	0	0	0	10	17	0	0	50
					17	0	0	50	113	0	0	50
IPE 100	49	25	Vento X	PolG	0	0	0	46	90	0	0	46
IPE 100	55	67	Peso Proprio	UnifG	24	0	0	62	24	0	0	100
IPE 100	55	67	QP Solai	PolG	84	0	0	100	84	0	0	65
					24	0	0	20	24	0	0	32
IPE 100	55	67	Neve	PolG	84	0	0	30	84	0	0	30
IPE 100	55	67	Neve	PolG	84	0	0	30	114	0	0	8
IPE 100	55	67	Neve	PolG	24	0	0	33	114	0	0	33
IPE 100	55	67	Vento X	PolG	84	0	0	46	84	0	0	46
IPE 100	55	67	Vento X	PolG	0	0	0	13	24	0	0	50
IPE 100	61	55	Peso Proprio	UnifG	23	0	0	64	23	0	0	100
IPE 100	61	55	QP Solai	PolG	126	0	0	100	126	0	0	67
					23	0	0	30	126	0	0	30
IPE 100	61	55	QV Solai	PolG	0	0	0	20	23	0	0	32
					23	0	0	32	126	0	0	32
IPE 100	61	55	Neve	PolG	126	0	0	30	126	0	0	21
IPE 100	61	55	Neve	PolG	126	0	0	30	149	0	0	9
IPE 100	61	55	Neve	PolG	0	0	0	10	23	0	0	33
IPE 100	61	55	Vento X	PolG	23	0	0	33	149	0	0	33
IPE 100	61	55	Vento X	PolG	0	0	0	15	23	0	0	50
IPE 100	61	55	Vento X	PolG	23	0	0	50	149	0	0	50
					93	0	0	100	113	0	0	60
IPE 100	67	31	QV Solai	PolG	0	0	0	18	14	0	0	32
					14	0	0	32	93	0	0	32
IPE 100	67	31	Neve	PolG	93	0	0	32	113	0	0	19
IPE 100	67	31	Neve	PolG	0	0	0	5	14	0	0	33
IPE 100	67	31	Neve	PolG	14	0	0	33	113	0	0	33
IPE 100	67	31	Vento X	PolG	93	0	0	30	113	0	0	5
IPE 100	67	31	Vento X	PolG	0	0	0	46	93	0	0	46
IPE 100	67	31	Vento X	PolG	93	0	0	46	113	0	0	7
					14	0	0	8	14	0	0	50
IPE 100	73	79	Peso Proprio	UnifG	0	0	0	50	113	0	0	50
IPE 100	73	79	QP Solai	PolG	0	0	0	8	114	0	0	8

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	73	79	QV Solai	PolG	81	0	0	100	114	0	0	100
					27	0	0	20	27	0	0	32
IPE 100	73	79	Neve	PolG	81	0	0	30	81	0	0	30
IPE 100	73	79	Neve	PolG	81	0	0	30	114	0	0	8
IPE 100	73	79	Neve	PolG	0	0	0	9	27	0	0	33
IPE 100	73	79	Vento X	PolG	27	0	0	33	114	0	0	33
IPE 100	73	79	Vento X	PolG	81	0	0	46	81	0	0	46
IPE 100	73	79	Vento X	PolG	0	0	0	15	27	0	0	50
IPE 100	79	85	Peso Proprio	UnifG	27	0	0	50	114	0	0	50
IPE 100	79	85	QP Solai	PolG	0	0	0	8	113	0	0	8
					33	0	0	100	74	0	0	100
IPE 100	79	85	QV Solai	PolG	74	0	0	100	114	0	0	70
					33	0	0	32	74	0	0	32
IPE 100	79	85	Neve	PolG	74	0	0	32	114	0	0	22
IPE 100	79	85	Neve	PolG	0	0	0	30	74	0	0	30
IPE 100	79	85	Neve	PolG	74	0	0	30	114	0	0	11
IPE 100	79	85	Vento X	PolG	33	0	0	33	114	0	0	33
IPE 100	79	85	Vento X	PolG	0	0	0	18	33	0	0	50
IPE 100	79	85	Vento X	PolG	33	0	0	50	114	0	0	50
IPE 100	79	85	Vento X	PolG	0	0	0	46	74	0	0	46
					74	0	0	46	114	0	0	16
Trave 8021												
IPE 100	26	62	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	26	62	QP Solai	PolG	0	0	0	59	23	0	0	92
					23	0	0	92	126	0	0	92
IPE 100	26	62	QV Solai	PolG	126	0	0	92	149	0	0	61
					23	0	0	19	23	0	0	29
IPE 100	26	62	Neve	PolG	126	0	0	29	149	0	0	20
IPE 100	26	62	Neve	PolG	126	0	0	27	126	0	0	27
IPE 100	26	62	Neve	PolG	0	0	0	9	23	0	0	8
IPE 100	26	62	Vento X	PolG	23	0	0	30	149	0	0	30
IPE 100	26	62	Vento X	PolG	0	0	0	14	23	0	0	46
IPE 100	26	62	Vento X	PolG	23	0	0	46	149	0	0	46
IPE 100	32	74	Peso Proprio	UnifG	126	0	0	42	126	0	0	42
IPE 100	32	74	QP Solai	PolG	0	0	0	42	149	0	0	13
IPE 100	32	74	Neve	PolG	0	0	0	54	20	0	0	8
IPE 100	32	74	Neve	PolG	20	0	0	92	81	0	0	92
IPE 100	32	74	QV Solai	PolG	81	0	0	92	107	0	0	57
IPE 100	32	74	QV Solai	PolG	0	0	0	17	20	0	0	29
IPE 100	32	74	Vento X	PolG	20	0	0	29	81	0	0	29
IPE 100	32	74	Vento X	PolG	81	0	0	29	107	0	0	18
IPE 100	32	74	Neve	PolG	0	0	0	27	81	0	0	27
IPE 100	32	74	Neve	PolG	81	0	0	27	107	0	0	6
IPE 100	32	74	Neve	PolG	0	0	0	6	20	0	0	30
IPE 100	32	74	Vento X	PolG	20	0	0	30	107	0	0	30
IPE 100	32	74	Vento X	PolG	0	0	0	10	20	0	0	46
IPE 100	32	74	Vento X	PolG	20	0	0	46	107	0	0	46
IPE 100	38	44	Peso Proprio	UnifG	81	0	0	42	81	0	0	42
IPE 100	38	44	QP Solai	PolG	0	0	0	42	107	0	0	9
IPE 100	38	44	Neve	PolG	0	0	0	8	108	0	0	8
IPE 100	38	44	Neve	PolG	0	0	0	48	5	0	0	92
IPE 100	38	44	QV Solai	PolG	5	0	0	92	97	0	0	92
IPE 100	38	44	QV Solai	PolG	97	0	0	92	108	0	0	51
					5	0	0	15	5	0	0	29
IPE 100	73	79	QP Solai	PolG	97	0	0	29	97	0	0	29
					97	0	0	29	108	0	0	16

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	OZi	Xf	QXf	QYf	OZf
IPE 100	38	44	Neve	PolG	0	0	0	27	97	0	0	27
IPE 100	38	44	Neve	PolG	97	0	0	27	108	0	0	2
IPE 100	38	44	Vento X	PolG	5	0	0	30	108	0	0	30
IPE 100	38	44	Vento X	PolG	0	0	0	3	5	0	0	46
IPE 100	38	44	Vento X	PolG	5	0	0	46	108	0	0	46
IPE 100	38	44	Vento X	PolG	0	0	0	42	97	0	0	42
IPE 100	44	50	Peso Proprio	UnifG	97	0	0	42	108	0	0	3
IPE 100	44	50	QV Solai	PolG	0	0	0	8	107	0	0	8
IPE 100	44	50		PolG	11	0	0	50	11	0	0	92
IPE 100	44	50		PolG	11	0	0	92	90	0	0	92
IPE 100	44	50	QV Solai	PolG	90	0	0	92	107	0	0	54
IPE 100	44	50	QV Solai	PolG	0	0	0	16	11	0	0	29
IPE 100	44	50	Neve	PolG	11	0	0	29	90	0	0	29
IPE 100	44	50	Neve	PolG	90	0	0	29	107	0	0	17
IPE 100	44	50	Neve	PolG	90	0	0	27	90	0	0	27
IPE 100	44	50	Neve	PolG	0	0	0	4	11	0	0	4
IPE 100	44	50	Vento X	PolG	11	0	0	30	107	0	0	30
IPE 100	44	50	Vento X	PolG	0	0	0	6	11	0	0	46
IPE 100	44	50	Vento X	PolG	11	0	0	46	107	0	0	46
IPE 100	44	50	Vento X	PolG	0	0	0	42	90	0	0	42
IPE 100	50	26	QV Solai	PolG	84	0	0	92	107	0	0	56
IPE 100	50	26	QV Solai	PolG	0	0	0	17	17	0	0	29
IPE 100	50	26	QV Solai	PolG	17	0	0	29	84	0	0	29
IPE 100	50	26	Neve	PolG	84	0	0	29	107	0	0	18
IPE 100	50	26	Neve	PolG	0	0	0	53	17	0	0	92
IPE 100	50	26	Neve	PolG	17	0	0	92	84	0	0	92
IPE 100	50	26	Neve	PolG	84	0	0	42	84	0	0	5
IPE 100	50	26	Neve	PolG	0	0	0	6	17	0	0	30
IPE 100	50	26	Vento X	PolG	17	0	0	30	107	0	0	30
IPE 100	50	26	Vento X	PolG	0	0	0	9	17	0	0	46
IPE 100	50	26	Vento X	PolG	17	0	0	46	107	0	0	46
IPE 100	50	26	Vento X	PolG	0	0	0	42	84	0	0	42
IPE 100	56	68	Peso Proprio	UnifG	84	0	0	42	107	0	0	8
IPE 100	56	68	QV Solai	PolG	0	0	0	8	108	0	0	8
IPE 100	56	68	QV Solai	PolG	24	0	0	56	24	0	0	92
IPE 100	56	68	QV Solai	PolG	24	0	0	92	78	0	0	92
IPE 100	56	68	QV Solai	PolG	78	0	0	92	108	0	0	59
IPE 100	56	68	QV Solai	PolG	0	0	0	18	24	0	0	29
IPE 100	56	68	QV Solai	PolG	24	0	0	29	78	0	0	29
IPE 100	56	68	Neve	PolG	78	0	0	29	108	0	0	19
IPE 100	56	68	Neve	PolG	0	0	0	7	24	0	0	30
IPE 100	56	68	Neve	PolG	24	0	0	30	108	0	0	30
IPE 100	56	68	Neve	PolG	78	0	0	27	78	0	0	27
IPE 100	56	68	Vento X	PolG	0	0	0	27	108	0	0	7
IPE 100	56	68	Vento X	PolG	0	0	0	42	78	0	0	42
IPE 100	56	68	Vento X	PolG	78	0	0	42	108	0	0	11
IPE 100	56	68	Vento X	PolG	0	0	0	12	24	0	0	46
IPE 100	62	56	Peso Proprio	UnifG	24	0	0	46	108	0	0	46
IPE 100	62	56	QV Solai	PolG	0	0	0	8	149	0	0	8
IPE 100	62	56	QV Solai	PolG	23	0	0	58	23	0	0	92
IPE 100	62	56	QV Solai	PolG	126	0	0	92	126	0	0	92
IPE 100	62	56	QV Solai	PolG	126	0	0	92	149	0	0	61
IPE 100	62	56	QV Solai	PolG	23	0	0	19	23	0	0	29
IPE 100	62	56	QV Solai	PolG	23	0	0	29	126	0	0	29
IPE 100	62	56	Neve	PolG	126	0	0	29	149	0	0	20
IPE 100	62	56	Neve	PolG	0	0	0	27	126	0	0	27
IPE 100	62	56	Neve	PolG	126	0	0	27	149	0	0	8
IPE 100	62	56	Neve	PolG	0	0	0	9	23	0	0	30
IPE 100	62	56	Vento X	PolG	23	0	0	30	149	0	0	30
IPE 100	62	56	Vento X	PolG	0	0	0	14	23	0	0	46
IPE 100	62	56	Vento X	PolG	23	0	0	46	149	0	0	46

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	OZi	Xf	QXf	QYf	OZf
IPE 100	62	56	Vento X	PolG	126	0	0	42	126	0	0	42
IPE 100	68	32	Peso Proprio	UnifG	0	0	0	8	107	0	0	8
IPE 100	68	32	QV Solai	PolG	0	0	0	52	14	0	0	92
IPE 100	68	32	QV Solai	PolG	14	0	0	92	87	0	0	92
IPE 100	68	32	QV Solai	PolG	87	0	0	92	107	0	0	55
IPE 100	68	32	QV Solai	PolG	0	0	0	17	14	0	0	29
IPE 100	68	32	Neve	PolG	14	0	0	29	87	0	0	29
IPE 100	68	32	Neve	PolG	0	0	0	27	87	0	0	27
IPE 100	68	32	Neve	PolG	87	0	0	27	107	0	0	4
IPE 100	68	32	Neve	PolG	0	0	0	5	14	0	0	30
IPE 100	68	32	Vento X	PolG	14	0	0	30	107	0	0	30
IPE 100	68	32	Vento X	PolG	0	0	0	42	87	0	0	42
IPE 100	68	32	Vento X	PolG	87	0	0	42	107	0	0	6
IPE 100	68	32	Vento X	PolG	14	0	0	7	14	0	0	46
IPE 100	74	80	Peso Proprio	UnifG	0	0	0	8	108	0	0	8
IPE 100	74	80	QV Solai	PolG	0	0	0	57	27	0	0	92
IPE 100	74	80	QV Solai	PolG	27	0	0	92	75	0	0	92
IPE 100	74	80	QV Solai	PolG	75	0	0	92	108	0	0	60
IPE 100	74	80	QV Solai	PolG	0	0	0	18	27	0	0	29
IPE 100	74	80	QV Solai	PolG	27	0	0	29	75	0	0	29
IPE 100	74	80	Neve	PolG	75	0	0	29	108	0	0	19
IPE 100	74	80	Neve	PolG	0	0	0	8	27	0	0	30
IPE 100	74	80	Neve	PolG	27	0	0	30	108	0	0	30
IPE 100	74	80	Neve	PolG	0	0	0	27	75	0	0	27
IPE 100	74	80	Vento X	PolG	75	0	0	27	108	0	0	7
IPE 100	74	80	Vento X	PolG	0	0	0	42	75	0	0	42
IPE 100	74	80	Vento X	PolG	75	0	0	42	108	0	0	11
IPE 100	74	80	Vento X	PolG	0	0	0	13	27	0	0	46
IPE 100	80	86	Peso Proprio	UnifG	27	0	0	46	108	0	0	46
IPE 100	80	86	QV Solai	PolG	0	0	0	8	107	0	0	8
IPE 100	80	86	QV Solai	PolG	0	0	0	61	33	0	0	92
IPE 100	80	86	QV Solai	PolG	33	0	0	92	68	0	0	92
IPE 100	80	86	QV Solai	PolG	68	0	0	92	107	0	0	63
IPE 100	80	86	QV Solai	PolG	0	0	0	19	33	0	0	29
IPE 100	80	86	QV Solai	PolG	33	0	0	29	68	0	0	29
IPE 100	80	86	Neve	PolG	68	0	0	29	107	0	0	20
IPE 100	80	86	Neve	PolG	0	0	0	27	68	0	0	27
IPE 100	80	86	Neve	PolG	68	0	0	27	107	0	0	9
IPE 100	80	86	Neve	PolG	0	0	0	10	33	0	0	30
IPE 100	80	86	Vento X	PolG	33	0	0	30	107	0	0	30
IPE 100	80	86	Vento X	PolG	0	0	0	42	68	0	0	42
IPE 100	80	86	Vento X	PolG	68	0	0	42	107	0	0	14
IPE 100	80	86	Vento X	PolG	0	0	0	16	33	0	0	46
IPE 100	80	86	Vento X	PolG	33	0	0	46	107	0	0	46
Trave 8022												
IPE 100	27	63	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	27	63	QV Solai	PolG	0	0	0	55	23	0	0	86
IPE 100	27	63	QV Solai	PolG	23	0	0	86	126	0	0	86
IPE 100	27	63	QV Solai	PolG	126	0	0	86	149	0	0	57
IPE 100	27	63	QV Solai	PolG	0	0	0	18	23	0	0	28
IPE 100	27	63	QV Solai	PolG	23	0	0	28	126	0	0	28
IPE 100	27	63	QV Solai	PolG	126	0	0	28	149	0	0	18
IPE 100	27	63	QV Solai	PolG	0	0	0	8	23	0	0	27
IPE 100	27	63	QV Solai	PolG	23	0	0	27	149	0	0	27
IPE 100	27	63	QV Solai	PolG	126	0	0	26	126	0	0	26
IPE 100	27	63	QV Solai	PolG	126	0	0	26	149	0	0	8
IPE 100	27	63	Vento X	PolG	0	0	0	41	126	0	0	41
IPE 100	27	63	Vento X	PolG	126	0	0	41	149	0	0	12
IPE 100	27	63	Vento X	PolG	0	0	0	13	23	0	0	42
IPE 100	33	75	Peso Proprio	UnifG	23	0	0	42	149	0	0	42
IPE 100	33	75	QV Solai	PolG	0	0	0	8	101	0	0	8
IPE 100	33	75	QV Solai	PolG	20	0	0	51	20	0	0	86
IPE 100	33	75	QV Solai	PolG	20	0	0	86	75	0	0	86

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	33	75	QV Solai	PolG	75	0	0	86	101	0	0	53
					20	0	0	16	20	0	0	28
IPE 100					75	0	0	28	75	0	0	28
IPE 100	33	75	Neve	PolG	0	0	0	26	75	0	0	26
					75	0	0	26	101	0	0	5
IPE 100	33	75	Neve	PolG	0	0	0	6	20	0	0	27
IPE 100	33	75	Vento X	PolG	0	0	0	41	75	0	0	41
IPE 100	33	75	Vento X	PolG	0	0	0	9	20	0	0	42
IPE 100	39	45	Peso Proprio	UnifG	0	0	0	8	102	0	0	8
IPE 100	39	45	QV Solai	PolG	5	0	0	43	5	0	0	86
					91	0	0	86	91	0	0	86
IPE 100	39	45	QV Solai	PolG	0	0	0	15	5	0	0	28
					5	0	0	28	91	0	0	28
IPE 100	39	45	Neve	PolG	0	0	0	28	102	0	0	15
IPE 100	39	45	Neve	PolG	0	0	0	26	91	0	0	26
IPE 100	39	45	Neve	PolG	0	0	0	26	102	0	0	2
IPE 100	39	45	Vento X	PolG	0	0	0	27	102	0	0	27
IPE 100	45	51	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	45	51	QV Solai	PolG	0	0	0	48	11	0	0	86
					11	0	0	86	84	0	0	86
IPE 100	45	51	QV Solai	PolG	84	0	0	86	101	0	0	49
					91	0	0	41	102	0	0	3
IPE 100	45	51	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	45	51	QV Solai	PolG	0	0	0	26	84	0	0	16
IPE 100	45	51	Neve	PolG	84	0	0	26	84	0	0	26
IPE 100	45	51	Neve	PolG	0	0	0	3	11	0	0	3
IPE 100	45	51	Vento X	PolG	0	0	0	27	101	0	0	27
IPE 100	45	51	Vento X	PolG	0	0	0	5	11	0	0	42
IPE 100	45	51	Vento X	PolG	0	0	0	41	84	0	0	41
IPE 100	51	27	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	51	27	QV Solai	PolG	0	0	0	50	17	0	0	86
					17	0	0	86	78	0	0	86
IPE 100	51	27	QV Solai	PolG	0	0	0	86	101	0	0	51
					17	0	0	28	78	0	0	28
IPE 100	51	27	Neve	PolG	0	0	0	28	101	0	0	16
IPE 100	51	27	Neve	PolG	0	0	0	5	17	0	0	27
IPE 100	51	27	Neve	PolG	0	0	0	27	101	0	0	27
IPE 100	51	27	Vento X	PolG	78	0	0	26	78	0	0	26
IPE 100	51	27	Vento X	PolG	0	0	0	7	17	0	0	42
IPE 100	51	27	Vento X	PolG	0	0	0	42	101	0	0	42
IPE 100	57	69	Peso Proprio	UnifG	0	0	0	41	78	0	0	40
IPE 100	57	69	QV Solai	PolG	0	0	0	8	102	0	0	8
					24	0	0	86	72	0	0	86
IPE 100	57	69	QV Solai	PolG	0	0	0	17	24	0	0	28
					24	0	0	28	72	0	0	28
IPE 100	57	69	Neve	PolG	72	0	0	26	72	0	0	26
					72	0	0	26	102	0	0	6

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	57	69		PolG	24	0	0	7	24	0	0	27
IPE 100	57	69	Vento X	PolG	0	0	0	41	72	0	0	41
IPE 100	57	69	Vento X	PolG	72	0	0	10	102	0	0	10
IPE 100	57	69	Vento X	PolG	0	0	0	10	24	0	0	42
IPE 100	63	57	Peso Proprio	UnifG	24	0	0	42	102	0	0	42
IPE 100	63	57	QV Solai	PolG	0	0	0	55	23	0	0	86
IPE 100	63	57	QV Solai	PolG	126	0	0	86	149	0	0	57
IPE 100	63	57	QV Solai	PolG	0	0	0	18	23	0	0	28
IPE 100	63	57	Neve	PolG	126	0	0	28	149	0	0	18
IPE 100	63	57	Neve	PolG	126	0	0	26	126	0	0	26
IPE 100	63	57	Neve	PolG	0	0	0	8	23	0	0	8
IPE 100	63	57	Vento X	PolG	23	0	0	27	149	0	0	27
IPE 100	63	57	Vento X	PolG	0	0	0	41	126	0	0	41
IPE 100	63	57	Vento X	PolG	126	0	0	13	23	0	0	42
IPE 100	69	33	Peso Proprio	UnifG	23	0	0	42	149	0	0	42
IPE 100	69	33	QV Solai	PolG	0	0	0	8	101	0	0	8
IPE 100	69	33	QV Solai	PolG	0	0	0	49	14	0	0	86
IPE 100	69	33	QV Solai	PolG	14	0	0	86	101	0	0	86
IPE 100	69	33	QV Solai	PolG	81	0	0	16	14	0	0	28
IPE 100	69	33	QV Solai	PolG	0	0	0	28	81	0	0	28
IPE 100	69	33	QV Solai	PolG	81	0	0	28	101	0	0	16
IPE 100	69	33	QV Solai	PolG	0	0	0	26	81	0	0	26
IPE 100	69	33	QV Solai	PolG	81	0	0	26	101	0	0	4
IPE 100	69	33	QV Solai	PolG	0	0	0	4	14	0	0	27
IPE 100	69	33	QV Solai	PolG	14	0	0	27	101	0	0	27
IPE 100	69	33	QV Solai	PolG	0	0	0	6	14	0	0	42
IPE 100	69	33	QV Solai	PolG	14	0	0	42	101	0	0	42
IPE 100	75	81	Peso Proprio	UnifG	81	0	0	41	101	0	0	6
IPE 100	75	81	QV Solai	PolG	0	0	0	8	102	0	0	8
IPE 100	75	81	QV Solai	PolG	27	0	0	54	27	0	0	86
IPE 100	75	81	QV Solai	PolG	69	0	0	86	102	0	0	55
IPE 100	75	81	QV Solai	PolG	27	0	0	17	27	0	0	28
IPE 100	75	81	QV Solai	PolG	69	0	0	28	69	0	0	18
IPE 100	75	81	QV Solai	PolG	0	0	0	28	102	0	0	18
IPE 100	75	81	QV Solai	PolG	0	0	0	7	27	0	0	27
IPE 100	75	81	QV Solai	PolG	27	0	0	27	102	0	0	26
IPE 100	75	81	QV Solai	PolG	69	0	0	26	102	0	0	7
IPE 100	75	81	QV Solai	PolG	0	0	0	11	27	0	0	42
IPE 100	75	81	QV Solai	PolG	27	0	0	42	102	0	0	42
IPE 100	75	81	QV Solai	PolG	69	0	0	41	69	0	0	41
IPE 100	81	87	Peso Proprio	UnifG	69	0	0	41	102	0	0	10
IPE 100	81	87	QV Solai	PolG	0	0	0	8	101	0	0	8
IPE 100	81	87	QV Solai	PolG	33	0	0	57	33	0	0	86
IPE 100	81	87	QV Solai	PolG	62	0	0	86	62	0	0	86
IPE 100	81	87	QV Solai	PolG	33	0	0	18	33	0	0	28
IPE 100	81	87	QV Solai	PolG	62	0	0	28	62	0	0	28
IPE 100	81	87	QV Solai	PolG	0	0	0	28	101	0	0	18
IPE 100	81	87	QV Solai	PolG	33	0	0	9	33	0	0	27
IPE 100	81	87	QV Solai	PolG	62	0	0	26	62	0	0	26
IPE 100	81	87	QV Solai	PolG	62	0	0	26	101	0	0	8
IPE 100	81	87	QV Solai	PolG	62	0	0	41	62	0	0	41
IPE 100	81	87	QV Solai	PolG	33	0	0	14	33	0	0	42

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Trave 8023												
IPE 100	28	64	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	28	64	QP Solai	PolG	0	0	0	56	23	0	0	85
					23	0	0	85	126	0	0	85
IPE 100					126	0	0	85	149	0	0	55
IPE 100	28	64	QV Solai	PolG	0	0	0	18	23	0	0	27
					23	0	0	27	126	0	0	27
IPE 100					126	0	0	27	149	0	0	18
IPE 100	28	64	Neve	PolG	0	0	0	8	23	0	0	26
IPE 100					23	0	0	26	149	0	0	26
IPE 100	28	64	Neve	PolG	0	0	0	27	126	0	0	27
IPE 100					126	0	0	27	149	0	0	8
IPE 100	28	64	Vento X	PolG	0	0	0	41	126	0	0	42
IPE 100					126	0	0	42	149	0	0	13
IPE 100	28	64	Vento X	PolG	0	0	0	12	23	0	0	41
IPE 100					23	0	0	41	149	0	0	41
IPE 100	34	76	Peso Proprio	UnitG	0	0	0	8	95	0	0	8
IPE 100	34	76	QP Solai	PolG	0	0	0	51	20	0	0	85
					20	0	0	85	69	0	0	85
IPE 100					69	0	0	85	95	0	0	50
IPE 100	34	76	QV Solai	PolG	0	0	0	16	20	0	0	27
					20	0	0	27	69	0	0	27
IPE 100					69	0	0	27	95	0	0	5
IPE 100	34	76	Vento X	PolG	0	0	0	8	20	0	0	41
IPE 100					20	0	0	41	95	0	0	41
IPE 100	34	76	Neve	PolG	0	0	0	5	20	0	0	26
IPE 100					20	0	0	26	95	0	0	26
IPE 100	34	76	Neve	PolG	0	0	0	27	69	0	0	27
IPE 100					69	0	0	27	95	0	0	8
IPE 100	34	76	Vento X	PolG	0	0	0	8	20	0	0	41
IPE 100					20	0	0	41	95	0	0	41
IPE 100	34	76	Vento X	PolG	0	0	0	41	69	0	0	41
IPE 100					69	0	0	41	95	0	0	8
IPE 100	40	46	Peso Proprio	UnitG	0	0	0	8	96	0	0	8
IPE 100	40	46	QP Solai	PolG	0	0	0	46	5	0	0	85
					5	0	0	85	85	0	0	85
IPE 100					85	0	0	85	96	0	0	45
IPE 100	40	46	QV Solai	PolG	0	0	0	15	5	0	0	27
					5	0	0	27	85	0	0	27
IPE 100					85	0	0	27	96	0	0	14
IPE 100	40	46	Neve	PolG	0	0	0	27	85	0	0	27
IPE 100					85	0	0	27	96	0	0	2
IPE 100	40	46	Neve	PolG	0	0	0	2	5	0	0	26
IPE 100					5	0	0	26	96	0	0	26
IPE 100	40	46	Vento X	PolG	0	0	0	3	5	0	0	41
IPE 100					5	0	0	41	96	0	0	41
IPE 100	40	46	Vento X	PolG	0	0	0	41	85	0	0	41
IPE 100					85	0	0	41	96	0	0	3
IPE 100	46	52	Peso Proprio	UnitG	0	0	0	8	95	0	0	8
IPE 100	46	52	QP Solai	PolG	0	0	0	48	11	0	0	85
					11	0	0	85	78	0	0	85
IPE 100					78	0	0	85	95	0	0	47
IPE 100	46	52	QV Solai	PolG	0	0	0	15	11	0	0	27
					11	0	0	27	78	0	0	27
IPE 100					78	0	0	27	95	0	0	15
IPE 100	46	52	Neve	PolG	0	0	0	27	78	0	0	27
IPE 100					78	0	0	27	95	0	0	3
IPE 100	46	52	Neve	PolG	0	0	0	3	11	0	0	26
IPE 100					11	0	0	26	95	0	0	26
IPE 100	46	52	Vento X	PolG	0	0	0	5	11	0	0	41
IPE 100					11	0	0	41	95	0	0	41
IPE 100	46	52	Vento X	PolG	0	0	0	41	78	0	0	41
IPE 100					78	0	0	41	95	0	0	5
IPE 100	52	28	Peso Proprio	UnitG	0	0	0	8	95	0	0	8
IPE 100	52	28	QP Solai	PolG	0	0	0	50	17	0	0	85
					17	0	0	85	72	0	0	85
IPE 100					72	0	0	85	95	0	0	49

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					17	0	0	27	72	0	0	27
IPE 100	52	28	Neve	PolG	0	0	0	4	17	0	0	26
IPE 100					17	0	0	26	95	0	0	26
IPE 100	52	28	Neve	PolG	0	0	0	27	72	0	0	27
IPE 100					72	0	0	27	95	0	0	4
IPE 100	52	28	Vento X	PolG	0	0	0	7	17	0	0	41
IPE 100					17	0	0	41	95	0	0	41
IPE 100	52	28	Vento X	PolG	0	0	0	41	72	0	0	41
IPE 100					72	0	0	41	95	0	0	7
IPE 100	58	70	Peso Proprio	UnitG	0	0	0	8	96	0	0	8
IPE 100	58	70	QP Solai	PolG	0	0	0	53	24	0	0	85
					24	0	0	85	66	0	0	85
IPE 100					66	0	0	85	96	0	0	52
IPE 100	58	70	QV Solai	PolG	0	0	0	17	24	0	0	27
					24	0	0	27	66	0	0	17
IPE 100					66	0	0	27	96	0	0	27
IPE 100	58	70	Neve	PolG	0	0	0	6	24	0	0	26
IPE 100					24	0	0	26	96	0	0	26
IPE 100	58	70	Neve	PolG	0	0	0	27	66	0	0	27
IPE 100					66	0	0	27	96	0	0	6
IPE 100	58	70	Vento X	PolG	0	0	0	9	24	0	0	41
IPE 100					24	0	0	41	96	0	0	41
IPE 100	58	70	Vento X	PolG	0	0	0	41	66	0	0	42
IPE 100					66	0	0	42	96	0	0	9
IPE 100	64	58	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	64	58	QP Solai	PolG	0	0	0	56	23	0	0	85
					23	0	0	85	126	0	0	85
IPE 100					126	0	0	85	149	0	0	55
IPE 100	64	58	QV Solai	PolG	0	0	0	18	23	0	0	27
					23	0	0	27	126	0	0	27
IPE 100					126	0	0	27	149	0	0	18
IPE 100	64	58	Neve	PolG	0	0	0	8	23	0	0	26
IPE 100					23	0	0	26	149	0	0	26
IPE 100	64	58	Neve	PolG	0	0	0	27	126	0	0	27
IPE 100					126	0	0	27	149	0	0	8
IPE 100	64	58	Vento X	PolG	0	0	0	12	23	0	0	41
IPE 100					23	0	0	41	149	0	0	41
IPE 100	64	58	Vento X	PolG	0	0	0	41	126	0	0	41
IPE 100					126	0	0	41	149	0	0	12
IPE 100	70	34	Peso Proprio	UnitG	0	0	0	8	95	0	0	8
IPE 100	70	34	QP Solai	PolG	0	0	0	49	14	0	0	85
					14	0	0	85	75	0	0	85
IPE 100					75	0	0	85	95	0	0	48
IPE 100	70	34	QV Solai	PolG	0	0	0	16	14	0	0	27
					14	0	0	27	75	0	0	27
IPE 100					75	0	0	27	95	0	0	15
IPE 100	70	34	Neve	PolG	0	0	0	27	75	0	0	27
IPE 100					75	0	0	27	95	0	0	4
IPE 100	70	34	Neve	PolG	0	0	0	4	14	0	0	26
IPE 100					14	0	0	26	95	0	0	26
IPE 100	70	34	Vento X	PolG	0	0	0	5	14	0	0	41
IPE 100					14	0	0	41	95	0	0	41
IPE 100	70	34	Vento X	PolG	0	0	0	41	75	0	0	41
IPE 100					75	0	0	41	95	0	0	6
IPE 100	76	82	Peso Proprio	UnitG	0	0	0	8	96	0	0	8
IPE 100	76	82	QP Solai	PolG	0	0	0	53	27	0	0	85
					27	0	0	85	63	0	0	85
IPE 100					63	0	0	85	96	0	0	52
IPE 100	76	82	QV Solai	PolG	0	0	0	17	27	0	0	27
					27	0	0	27	63	0	0	27
IPE 100					63	0	0	27	96	0	0	17
IPE 100	76	82	Neve	PolG	0	0	0	27	63	0	0	27
IPE 100					63	0	0	27	96	0	0	6
IPE 100	76	82	Neve	PolG	0	0	0	6	27	0	0	26

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	76	82	Vento X	PolG	0	0	0	41	63	0	0	41
IPE 100	76	82	Vento X	PolG	63	0	0	41	96	0	0	10
IPE 100	82	88	Peso Proprio	UnifG	27	0	0	10	41	96	0	41
IPE 100	82	88	QV Solai	PolG	0	0	0	8	95	0	0	8
					33	0	0	56	33	0	0	85
					56	0	0	85	56	0	0	85
IPE 100	82	88	QV Solai	PolG	0	0	0	18	33	0	0	27
					33	0	0	27	56	0	0	27
IPE 100	82	88	Neve	PolG	56	0	0	27	95	0	0	18
IPE 100	82	88	Neve	PolG	33	0	0	26	95	0	0	26
IPE 100	82	88	Neve	PolG	0	0	0	27	56	0	0	27
IPE 100	82	88	Vento X	PolG	56	0	0	27	95	0	0	8
IPE 100	82	88	Vento X	PolG	0	0	0	13	33	0	0	41
IPE 100	82	88	Vento X	PolG	33	0	0	41	95	0	0	41
					56	0	0	41	56	0	0	41
Trave 8024												
IPE 100	12	13	Peso Proprio	UnifG	0	0	0	8	66	0	0	8
IPE 100	12	13	QV Solai	PolG	0	0	0	3	5	0	0	43
IPE 100	12	13	QV Solai	PolG	5	0	0	43	90	0	0	43
IPE 100	12	13	Neve	PolG	5	0	0	1	5	0	0	14
IPE 100	12	13	Neve	PolG	0	0	0	2	5	0	0	27
IPE 100	12	13	Vento X	PolG	5	0	0	27	90	0	0	27
IPE 100	12	13	Vento X	PolG	0	0	0	3	5	0	0	41
IPE 100	13	14	Peso Proprio	UnifG	0	0	0	41	90	0	0	41
IPE 100	13	14	QV Solai	PolG	0	0	0	8	101	0	0	8
IPE 100	13	14	QV Solai	PolG	11	0	0	5	11	0	0	43
IPE 100	13	14	QV Solai	PolG	0	0	0	43	89	0	0	43
IPE 100	13	14	QV Solai	PolG	0	0	0	2	11	0	0	14
IPE 100	13	14	Neve	PolG	11	0	0	14	89	0	0	14
IPE 100	13	14	Neve	PolG	0	0	0	3	11	0	0	27
IPE 100	13	14	Vento X	PolG	11	0	0	27	89	0	0	41
IPE 100	14	15	Peso Proprio	UnifG	0	0	0	8	90	0	0	8
IPE 100	14	15	QV Solai	PolG	0	0	0	7	17	0	0	43
IPE 100	14	15	QV Solai	PolG	17	0	0	43	90	0	0	43
IPE 100	14	15	QV Solai	PolG	0	0	0	2	17	0	0	14
IPE 100	14	15	Neve	PolG	17	0	0	14	90	0	0	14
IPE 100	14	15	Neve	PolG	0	0	0	4	17	0	0	27
IPE 100	14	15	Vento X	PolG	17	0	0	27	90	0	0	27
IPE 100	15	16	Peso Proprio	UnifG	0	0	0	6	17	0	0	41
IPE 100	15	16	QV Solai	PolG	17	0	0	41	90	0	0	41
IPE 100	15	16	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	15	16	QV Solai	PolG	0	0	0	13	23	0	0	43
IPE 100	15	16	QV Solai	PolG	23	0	0	43	149	0	0	43
IPE 100	15	16	QV Solai	PolG	0	0	0	4	23	0	0	14
IPE 100	15	16	QV Solai	PolG	23	0	0	14	149	0	0	27
IPE 100	15	16	Neve	PolG	23	0	0	8	23	0	0	27
IPE 100	15	16	Neve	PolG	0	0	0	27	149	0	0	27
IPE 100	15	16	Vento X	PolG	23	0	0	13	23	0	0	41
IPE 100	16	17	Peso Proprio	UnifG	23	0	0	41	149	0	0	41
IPE 100	16	17	QV Solai	PolG	0	0	0	8	149	0	0	8
IPE 100	16	17	QV Solai	PolG	0	0	0	13	23	0	0	43
IPE 100	16	17	QV Solai	PolG	23	0	0	43	149	0	0	43
IPE 100	16	17	Neve	PolG	23	0	0	14	149	0	0	14
IPE 100	16	17	Neve	PolG	0	0	0	8	23	0	0	27
IPE 100	16	17	Vento X	PolG	23	0	0	12	23	0	0	42
IPE 100	17	22	Peso Proprio	UnifG	23	0	0	42	149	0	0	41

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	17	22	QV Solai	PolG	24	0	0	9	24	0	0	43
IPE 100	17	22	QV Solai	PolG	0	0	0	3	24	0	0	43
IPE 100	17	22	Neve	PolG	24	0	0	14	90	0	0	14
IPE 100	17	22	Vento X	PolG	24	0	0	27	90	0	0	27
IPE 100	17	22	Vento X	PolG	0	0	0	9	24	0	0	41
IPE 100	18	19	Peso Proprio	UnifG	24	0	0	41	90	0	0	41
IPE 100	18	19	QV Solai	PolG	0	0	0	8	89	0	0	8
IPE 100	18	19	QV Solai	PolG	20	0	0	43	89	0	0	43
IPE 100	18	19	QV Solai	PolG	20	0	0	3	20	0	0	14
IPE 100	18	19	Neve	PolG	20	0	0	5	20	0	0	27
IPE 100	18	19	Vento X	PolG	20	0	0	27	89	0	0	27
IPE 100	18	19	Vento X	PolG	0	0	0	8	20	0	0	41
IPE 100	19	20	Peso Proprio	UnifG	0	0	0	8	102	0	0	8
IPE 100	19	20	QV Solai	PolG	27	0	0	10	27	0	0	43
IPE 100	19	20	QV Solai	PolG	0	0	0	3	27	0	0	14
IPE 100	19	20	Neve	PolG	27	0	0	6	27	0	0	27
IPE 100	19	20	Vento X	PolG	27	0	0	27	90	0	0	27
IPE 100	20	21	Peso Proprio	UnifG	27	0	0	41	90	0	0	41
IPE 100	20	21	QV Solai	PolG	0	0	0	8	77	0	0	8
IPE 100	20	21	QV Solai	PolG	0	0	0	13	33	0	0	43
IPE 100	20	21	QV Solai	PolG	33	0	0	43	89	0	0	43
IPE 100	20	21	QV Solai	PolG	0	0	0	4	33	0	0	14
IPE 100	20	21	Neve	PolG	33	0	0	14	89	0	0	14
IPE 100	20	21	Neve	PolG	0	0	0	8	33	0	0	27
IPE 100	20	21	Vento X	PolG	33	0	0	27	89	0	0	27
IPE 100	22	18	Peso Proprio	UnifG	33	0	0	12	33	0	0	41
IPE 100	22	18	QV Solai	PolG	0	0	0	41	89	0	0	41
IPE 100	22	18	QV Solai	PolG	0	0	0	5	14	0	0	43
IPE 100	22	18	QV Solai	PolG	14	0	0	43	89	0	0	43
IPE 100	22	18	QV Solai	PolG	0	0	0	2	14	0	0	14
IPE 100	22	18	Neve	PolG	14	0	0	3	14	0	0	27
IPE 100	22	18	Vento X	PolG	14	0	0	27	89	0	0	27
IPE 100	22	18	Vento X	PolG	0	0	0	5	14	0	0	42
IPE 100	22	18	Vento X	PolG	14	0	0	42	89	0	0	41
Fondazione 9005												
F60x100	1	2	Peso Proprio	UnifG	0	0	0	1500	162	0	0	1500
F60x100	2	3	Peso Proprio	UnifG	0	0	0	1500	150	0	0	1500
F60x100	3	4	Peso Proprio	UnifG	0	0	0	1500	149	0	0	1500
F60x100	4	5	Peso Proprio	UnifG	0	0	0	1500	150	0	0	1500
F60x100	5	6	Peso Proprio	UnifG	0	0	0	1500	149	0	0	1500
F60x100	6	7	Peso Proprio	UnifG	0	0	0	1500	150	0	0	1500
F60x100	7	8	Peso Proprio	UnifG	0	0	0	1500	149	0	0	1500
F60x100	8	9	Peso Proprio	UnifG	0	0	0	1500	149	0	0	1500
F60x100	9	10	Peso Proprio	UnifG	0	0	0	1500	149	0	0	1500
F60x100	10	11	Peso Proprio	UnifG	0	0	0	1500	150	0	0	1500
Fondazione 9006												
F60x100	1	2	Peso Proprio	UnifG	0	0	0	1500	102	0	0	1500
F60x100	2	3	Peso Proprio	UnifG	0	0	0	1500	89	0	0	1500
F60x100	3	4	Peso Proprio	UnifG	0	0	0	1500	90	0	0	1500
F60x100	4	5	Peso Proprio	UnifG	0	0	0	1500	149	0	0	1500
F60x100	5	6	Peso Proprio	UnifG	0	0	0	1500	149	0	0	1500
F60x100	6	11	Peso Proprio	UnifG	0	0	0	1500	90	0	0	1500
F60x100	7	8	Peso Proprio	UnifG	0	0	0	1500	89	0	0	1500
F60x100	8	9	Peso Proprio	UnifG	0	0	0	1500	90	0	0	1500
F60x100	9	10	Peso Proprio	UnifG	0	0	0	1500	101	0	0	1500
F60x100	11	7	Peso Proprio	UnifG	0	0	0	1500	89	0	0	1500

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Generica 7001												
Fi18	1	25	Peso Proprio	UnifG	0	0	0	2	259	0	0	2
Generica 7002												
Fi18	25	12	Peso Proprio	UnifG	0	0	0	2	310	0	0	2
Generica 7003												
Fi16	12	11	Peso Proprio	UnifG	0	0	0	2	385	0	0	2
Generica 7004												
Fi16	11	35	Peso Proprio	UnifG	0	0	0	2	353	0	0	2
Generica 7005												
Fi16	35	43	Peso Proprio	UnifG	0	0	0	2	306	0	0	2
Generica 7006												
Fi16	43	39	Peso Proprio	UnifG	0	0	0	2	258	0	0	2
Generica 7007												
Fi16	39	13	Peso Proprio	UnifG	0	0	0	2	237	0	0	2
Generica 7008												
Fi16	13	1	Peso Proprio	UnifG	0	0	0	2	280	0	0	2
Generica 7009												
Fi16	2	12	Peso Proprio	UnifG	0	0	0	2	280	0	0	2
Generica 7010												
Fi16	12	45	Peso Proprio	UnifG	0	0	0	2	237	0	0	2
Generica 7011												
Fi16	45	37	Peso Proprio	UnifG	0	0	0	2	258	0	0	2
Generica 7012												
Fi16	37	41	Peso Proprio	UnifG	0	0	0	2	306	0	0	2
Generica 7013												
Fi16	41	8	Peso Proprio	UnifG	0	0	0	2	354	0	0	2
Generica 7014												
Fi16	8	13	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7015												
Fi18	13	28	Peso Proprio	UnifG	0	0	0	2	310	0	0	2
Generica 7016												
Fi18	28	2	Peso Proprio	UnifG	0	0	0	2	259	0	0	2
Generica 7017												
Fi18	10	33	Peso Proprio	UnifG	0	0	0	2	259	0	0	2
Generica 7018												
Fi18	33	21	Peso Proprio	UnifG	0	0	0	2	310	0	0	2
Generica 7019												
Fi16	21	32	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7020												
Fi16	32	77	Peso Proprio	UnifG	0	0	0	2	353	0	0	2
Generica 7021												
Fi16	77	85	Peso Proprio	UnifG	0	0	0	2	305	0	0	2
Generica 7022												
Fi16	85	81	Peso Proprio	UnifG	0	0	0	2	257	0	0	2
Generica 7023												
Fi16	81	21	Peso Proprio	UnifG	0	0	0	2	238	0	0	2
Generica 7024												
Fi16	21	9	Peso Proprio	UnifG	0	0	0	2	280	0	0	2
Generica 7025												
Fi16	10	20	Peso Proprio	UnifG	0	0	0	2	270	0	0	2
Generica 7026												
Fi16	20	87	Peso Proprio	UnifG	0	0	0	2	235	0	0	2
Generica 7027												
Fi16	87	79	Peso Proprio	UnifG	0	0	0	2	258	0	0	2
Generica 7028												
Fi16	79	83	Peso Proprio	UnifG	0	0	0	2	305	0	0	2
Generica 7029												
Fi16	83	29	Peso Proprio	UnifG	0	0	0	2	354	0	0	2
Generica 7030												
Fi16	29	22	Peso Proprio	UnifG	0	0	0	2	386	0	0	2
Generica 7031												
Fi18	22	32	Peso Proprio	UnifG	0	0	0	2	305	0	0	2
Generica 7032												
Fi18	32	11	Peso Proprio	UnifG	0	0	0	2	259	0	0	2
Generica 7033												
Fi18	7	30	Peso Proprio	UnifG	0	0	0	2	255	0	0	2

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Generica 7034												
Fi18	30	18	Peso Proprio	UnifG	0	0	0	2	310	0	0	2
Generica 7035												
Fi16	18	17	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7036												
Fi16	17	65	Peso Proprio	UnifG	0	0	0	2	353	0	0	2
Generica 7037												
Fi16	65	55	Peso Proprio	UnifG	0	0	0	2	306	0	0	2
Generica 7038												
Fi16	55	69	Peso Proprio	UnifG	0	0	0	2	259	0	0	2
Generica 7039												
Fi16	69	17	Peso Proprio	UnifG	0	0	0	2	237	0	0	2
Generica 7040												
Fi16	17	11	Peso Proprio	UnifG	0	0	0	2	275	0	0	2
Generica 7041												
Fi16	22	57	Peso Proprio	UnifG	0	0	0	2	238	0	0	2
Generica 7042												
Fi16	57	67	Peso Proprio	UnifG	0	0	0	2	258	0	0	2
Generica 7043												
Fi16	67	53	Peso Proprio	UnifG	0	0	0	2	306	0	0	2
Generica 7044												
Fi16	53	23	Peso Proprio	UnifG	0	0	0	2	354	0	0	2
Generica 7045												
Fi16	23	17	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7046												
Fi18	17	24	Peso Proprio	UnifG	0	0	0	2	310	0	0	2
Generica 7047												
Fi18	24	6	Peso Proprio	UnifG	0	0	0	2	259	0	0	2
Generica 7048												
Fi16	13	14	Peso Proprio	UnifG	0	0	0	2	386	0	0	2
Generica 7049												
Fi16	14	15	Peso Proprio	UnifG	0	0	0	2	386	0	0	2
Generica 7050												
Fi16	15	20	Peso Proprio	UnifG	0	0	0	2	389	0	0	2
Generica 7051												
Fi16	20	17	Peso Proprio	UnifG	0	0	0	2	388	0	0	2
Generica 7052												
Fi16	18	5	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7053												
Fi16	5	20	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7054												
Fi16	20	29	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7055												
Fi16	21	26	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7056												
Fi16	26	19	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7057												
Fi16	19	23	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7058												
Fi16	17	16	Peso Proprio	UnifG	0	0	0	2	389	0	0	2
Generica 7059												
Fi16	16	2	Peso Proprio	UnifG	0	0	0	2	390	0	0	2
Generica 7060												
Fi16	2	14	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7061												
Fi16	14	11	Peso Proprio	UnifG	0	0	0	2	387	0	0	2
Generica 7062												
Fi16	13	51	Peso Proprio	UnifG	0	0	0	2	236	0	0	2
Generica 7063												
Fi16	51	15	Peso Proprio	UnifG	0	0	0	2	236	0	0	2
Generica 7064												
Fi16	15	63	Peso Proprio	UnifG	0	0	0	2	263	0	0	2
Generica 7065												
Fi16	63	17	Peso Proprio	UnifG	0	0	0	2	261	0	0	2
Generica 7066												
Fi16	22	33	Peso Proprio	UnifG	0	0	0	2	237	0	0	2

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Generica 7067												
Fil6	33	19	Peso Proprio	UnifG	0	0	0	2	237	0	0	2
Generica 7068												
Fil6	19	81	Peso Proprio	UnifG	0	0	0	2	237	0	0	2
Generica 7069												
Fil6	45	14	Peso Proprio	UnifG	0	0	0	2	237	0	0	2
Generica 7070												
Fil6	14	27	Peso Proprio	UnifG	0	0	0	2	237	0	0	2
Generica 7071												
Fil6	27	16	Peso Proprio	UnifG	0	0	0	2	263	0	0	2
Generica 7072												
Fil6	16	57	Peso Proprio	UnifG	0	0	0	2	263	0	0	2
Generica 7073												
Fil6	69	18	Peso Proprio	UnifG	0	0	0	2	236	0	0	2
Generica 7074												
Fil6	18	75	Peso Proprio	UnifG	0	0	0	2	237	0	0	2
Generica 7075												
Fil6	75	20	Peso Proprio	UnifG	0	0	0	2	237	0	0	2
Generica 7076												
Fil6	22	6	Peso Proprio	UnifG	0	0	0	2	280	0	0	2

Dati solai

Solatio n°	Nodi		Tipo
0	13-10-7-12		Vetro strutturale
0	14-13-10-13		Vetro strutturale
0	15-1-13-14		Vetro strutturale
0	16-19-1-15		Vetro strutturale
0	17-16-19-16		Vetro strutturale
0	18-22-16-17		Vetro strutturale
0	19-4-22-18		Vetro strutturale
0	20-25-4-19		Vetro strutturale
0	21-28-25-20		Vetro strutturale
0	22-31-28-21		Vetro strutturale
0	1-23-14-13		Vetro strutturale
0	2-3-15-14		Vetro strutturale
0	3-23-47-15		Vetro strutturale
0	23-24-48-47		Vetro strutturale
0	24-25-49-48		Vetro strutturale
0	25-26-50-49		Vetro strutturale
0	26-27-51-50		Vetro strutturale
0	27-28-52-51		Vetro strutturale
0	28-15-14-52		Vetro strutturale
0	4-5-23-22		Vetro strutturale
0	5-6-24-23		Vetro strutturale
0	6-29-65-24		Vetro strutturale
0	29-30-66-65		Vetro strutturale
0	30-31-67-66		Vetro strutturale
0	31-32-68-67		Vetro strutturale
0	32-33-69-68		Vetro strutturale
0	33-34-70-69		Vetro strutturale
0	34-18-22-70		Vetro strutturale
0	10-11-8-7		Vetro strutturale
0	11-12-9-8		Vetro strutturale
0	12-41-35-9		Vetro strutturale
0	41-42-36-35		Vetro strutturale
0	42-43-37-36		Vetro strutturale
0	43-44-38-37		Vetro strutturale
0	44-45-39-38		Vetro strutturale
0	45-46-40-39		Vetro strutturale
0	46-13-12-40		Vetro strutturale
0	13-14-11-10		Vetro strutturale
0	14-15-12-11		Vetro strutturale
0	15-47-41-12		Vetro strutturale
0	47-48-42-41		Vetro strutturale
0	48-49-43-42		Vetro strutturale

0	49-50-44-43	Vetro strutturale
0	50-51-45-44	Vetro strutturale
0	51-52-46-45	Vetro strutturale
0	52-14-13-46	Vetro strutturale
0	16-17-20-19	Vetro strutturale
0	17-18-21-20	Vetro strutturale
0	18-53-59-21	Vetro strutturale
0	53-54-60-59	Vetro strutturale
0	54-55-61-60	Vetro strutturale
0	55-56-62-61	Vetro strutturale
0	56-57-63-62	Vetro strutturale
0	57-58-64-63	Vetro strutturale
0	58-17-16-64	Vetro strutturale
0	19-20-2-1	Vetro strutturale
0	20-21-3-2	Vetro strutturale
0	21-59-23-3	Vetro strutturale
0	59-60-24-23	Vetro strutturale
0	60-61-25-24	Vetro strutturale
0	61-62-26-25	Vetro strutturale
0	62-63-27-26	Vetro strutturale
0	63-64-28-27	Vetro strutturale
0	64-16-15-28	Vetro strutturale
0	22-23-17-16	Vetro strutturale
0	23-24-18-17	Vetro strutturale
0	24-65-53-18	Vetro strutturale
0	65-66-54-53	Vetro strutturale
0	66-67-55-54	Vetro strutturale
0	67-68-56-55	Vetro strutturale
0	68-69-57-56	Vetro strutturale
0	69-70-58-57	Vetro strutturale
0	70-22-17-58	Vetro strutturale
0	25-26-5-4	Vetro strutturale
0	26-27-6-5	Vetro strutturale
0	27-71-29-6	Vetro strutturale
0	71-72-30-29	Vetro strutturale
0	72-73-31-30	Vetro strutturale
0	73-74-32-31	Vetro strutturale
0	74-75-33-32	Vetro strutturale
0	75-76-34-33	Vetro strutturale
0	76-19-18-34	Vetro strutturale
0	28-29-26-25	Vetro strutturale
0	29-30-27-26	Vetro strutturale
0	30-77-71-27	Vetro strutturale
0	77-78-72-71	Vetro strutturale
0	78-79-73-72	Vetro strutturale
0	79-80-74-73	Vetro strutturale
0	80-81-75-74	Vetro strutturale
0	81-82-76-75	Vetro strutturale
0	82-20-19-76	Vetro strutturale
0	31-32-29-28	Vetro strutturale
0	32-33-30-29	Vetro strutturale
0	33-83-77-30	Vetro strutturale
0	83-84-78-77	Vetro strutturale
0	84-85-79-78	Vetro strutturale
0	85-86-80-79	Vetro strutturale
0	86-87-81-80	Vetro strutturale
0	87-88-82-81	Vetro strutturale
0	88-21-20-82	Vetro strutturale

TABULATI DI VERIFICA

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Forze sismiche e masse
- Taglienti di piano
- Spostamenti Relativi dei nodi (SLD)
- Fattori di partecipazione e masse modali
- Massime tensioni sul terreno aste
- Massime reazioni vincolari
- Massime sollecitazioni travi
- Massime sollecitazioni pilastri
- Massime sollecitazioni aste generiche

Risultati Analisi Dinamica - Baricentri masse e masse	
Scenario di calcolo : Set_NT_SLV_A2_STR/GEO	

Combinazione masse 1

Piano	Rigido	Massa		X	Y	Z
			kg	cm	cm	cm
0	No	24990		788	919	15
1	No	37364		404	704	947
2	No	0		0	0	0
3	No	2234		-186	473	1270

Combinazione masse 2

Piano	Rigido	Massa		X	Y	Z
			kg	cm	cm	cm
0	No	24990		792	927	15
1	No	37364		425	749	947
2	No	0		0	0	0
3	No	2234		-184	478	1270

Combinazione masse 3

Piano	Rigido	Massa		X	Y	Z
			kg	cm	cm	cm
0	No	24990		788	936	15
1	No	37364		404	794	947
2	No	0		0	0	0
3	No	2234		-186	484	1270

Combinazione masse 4

Piano	Rigido	Massa		X	Y	Z
			kg	cm	cm	cm
0	No	24990		784	927	15
1	No	37364		383	749	947
2	No	0		0	0	0
3	No	2234		-188	478	1270

Taglienti di piano

Scenario di calcolo : Set_NT_SLV_A2_STR/GEO	
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I taglienti sono dati per combinazioni di calcolo C-S-Pm con C=Combinazione(1,2,...) S=Sisma(1,II) Pm=posizione masse(1,2,...) Azioni complessive, riferite al sistema WCS,con origine in (0,0,0),i momenti sono comprensivi dei momenti di trasporto

$\Theta = F_z \cdot d_r / (F_h \cdot H)$

con:

- F_z**=forza verticale,
- d_r**=spost medio del piano rispetto al piano inferiore,
- F_h**=tagliante,
- H**=altezza del piano

Combinazione 12-I-1 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-15492	-218	27851	-23076	-22167	-7245	7756	9364	2110	--
1	26780	0	-35990	-9021	22675	-8486	2569	6905	10043	0.001661
2	0	0	0	0	0	0	0	0	0	0.000000
3	12148	-212	-12219	10663	5095	-1944	-1944	4870	12700	0.003437

Piano	FxPil/Isol.	FyPil/Isol.	FzPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg
0	-12773	-5099	0	0	0	0	0	-15492	-218
1	12773	5099	0	0	0	0	0	26780	0
2	0	0	0	0	0	0	0	0	0
3	10978	1978	0	0	0	0	0	12148	-212

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX		%Par. FX		%Shell. FX	
	0	100.00	0.00	0.00		
	1	100.00	0.00	0.00		
	2	--	--	--		
	3	100.00	0.00	0.00		

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY		%Par. FY		%Shell. FY	
	0	100.00	0.00	0.00		
	1	100.00	0.00	0.00		
	2	--	--	--		
	3	100.00	0.00	0.00		

Combinazione 12-I-2 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-16407	-363	28493	-22498	-21332	-5001	7756	9364	2110	--
1	26904	-80	-36848	-10947	15139	-17044	2569	6905	10043	0.001660
2	0	0	0	0	0	0	0	0	0	0.000000
3	11351	-257	-12289	6755	4796	-7559	-1944	4870	12700	0.003645

Piano	FxPil/Isol.	FyPil/Isol.	FzPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg
0	-13559	-5505	0	0	0	0	0	-16407	-363
1	13559	5505	0	0	0	0	0	26904	-80
2	0	0	0	0	0	0	0	0	0
3	10189	1909	0	0	0	0	0	11351	-257

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX		%Par. FX		%Shell. FX	
	0	100.00	0.00	0.00		
	1	100.00	0.00	0.00		
	2	--	--	--		
	3	100.00	0.00	0.00		

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY		%Par. FY		%Shell. FY	
	0	100.00	0.00	0.00		
	1	100.00	0.00	0.00		
	2	--	--	--		
	3	100.00	0.00	0.00		

Combinazione 12-I-3 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-16459	-98	28122	-32826	-26030	-1544	7756	9364	2110	--
1	26744	1	-36408	-4537	16482	-30893	2569	6905	10043	0.001659
2	0	0	0	0	0	0	0	0	0	0.000000
3	11132	164	-12326	4839	4012	-14565	-1944	4870	12700	0.003694

Piano	FxPII/Isol.	FyPII/Isol.	FzPII/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg
0	-13472	-5523		0	0	0	0	-16459	-98
1	13472	5523		0	0	0	0	26744	1
2	0	0	0	0	0	0	0	0	0
3	10001	2258		0	0	0	0	11132	164

Percentuali assorbite in direzione X

Piano	%PII/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%PII/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 12-I-4 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-15606	39	27115	-28665	-24570	-4250	7756	9364	2110	--
1	26933	186	-35187	-6930	19673	-21503	2569	6905	10043	0.001643
2	0	0	0	0	0	0	0	0	0	0.000000
3	12089	267	-12044	6818	3250	-9804	-1944	4870	12700	0.003415

Piano	FxPII/Isol.	FyPII/Isol.	FzPII/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg
0	-12745	-5130		0	0	0	0	-15606	39
1	12745	5130		0	0	0	0	26933	186
2	0	0	0	0	0	0	0	0	0
3	10939	2405		0	0	0	0	12089	267

Percentuali assorbite in direzione X

Piano	%PII/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%PII/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 13-I-1 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-3743	-17529	29134	65552	24509	3753	7756	9364	2110	--
1	-416	26300	-36055	-14094	38058	53985	2569	6905	10043	0.001680
2	0	0	0	0	0	0	0	0	0	0.000000
3	-3996	9425	-10798	-14632	3073	27059	-1944	4870	12700	0.002690

Piano	FxPII/Isol.	FyPII/Isol.	FzPII/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg
0	-8822	-5762		0	0	0	0	-3743	-17529
1	8822	5762		0	0	0	0	-416	26300
2	0	0	0	0	0	0	0	0	0
3	-1863	4757		0	0	0	0	-3996	9425

Percentuali assorbite in direzione X

Piano	%PII/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%PII/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 13-I-2 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-4304	-17862	31085	56205	20225	2163	7756	9364	2110	--
1	-104	26522	-38108	-6743	47975	53831	2569	6905	10043	0.001742
2	0	0	0	0	0	0	0	0	0	0.000000
3	-3910	9662	-10923	-14988	3491	22743	-1944	4870	12700	0.002677

Piano	FxPII/Isol.	FyPII/Isol.	FzPII/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg
0	-9422	-5997		0	0	0	0	-4304	-17862
1	9422	5997		0	0	0	0	-104	26522
2	0	0	0	0	0	0	0	0	0
3	-1781	4996		0	0	0	0	-3910	9662

Percentuali assorbite in direzione X

Piano	%PII/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%PII/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 13-I-3 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-4284	-17742	30192	57904	21112	4512	7756	9364	2110	--
1	-192	26614	-37085	-9202	41970	47135	2569	6905	10043	0.001672
2	0	0	0	0	0	0	0	0	0	0.000000
3	-4090	9765	-10783	-16273	2923	19817	-19444	4870	12700	0.002630

Piano	FxPil/Isol.	FyPil/Isol.	FzPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg
0	-9339	-6011	0	0	0	0	0	-4284	-17742
1	9339	6011	0	0	0	0	0	-192	26614
2	0	0	0	0	0	0	0	0	0
3	-1953	5080	0	0	0	0	0	-4090	9765

Percentuali assorbite in direzione X

Piano	%aPil/Isol. FX	%aPar. FX	%Shell. FX
1	100.00	0.00	0.00
2	100.00	0.00	0.00
3	--	--	--
	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%aPil/Isol. FY	%aPar. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 13-I-4 (SISMAY SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-3938	-17445	28670	22226	4890	7756	9364	2110	--	
1	-149	26470	-35454	-10968	37664	48155	2569	6905	10043	0.001628
2	0	0	0	0	0	0	0	0	0	0.000000
3	-3618	9895	-10636	-15835	2362	22031	-1944	4870	12700	0.002616

Piano	FxPil/Isol.	FyPil/Isol.	FzPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg
0	-8949	-5815	0	0	0	0	0	-3938	-17445
1	8949	5815	0	0	0	0	0	-149	26470
2	0	0	0	0	0	0	0	0	0
3	-1479	5207	0	0	0	0	0	-3618	9895

Percentuali assorbite in direzione X

Piano	%aPil/Isol. FX	%aPar. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%aPil/Isol. FY	%aPar. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Verifica Degli Spostamenti Relativi

Scenario di calcolo : **Set NT SLV A2 STR/GEO**

Attenzione calcolo agli SLU. Gli spostamenti dovuti al sisma sono stati calcolati in via approssimata moltiplicando gli spostamenti derivanti dagli spettri al limite ultimo per il coefficiente e=Sd(T0)/Su(T0),dove T0 è il periodo fondamentale nella direzione considerata, Sd(T0) e Su(T0) il valore dello spettro in T0 rispettivamente di danno e ultimo

Combinazione	Spettro	
SISMAY SLV	SpettroNTI(q=1)	e=0.417
SISMAY SLV	SpettroNTI(q=1)	e=0.417

Interp.	Comb.	ηXv mm	ηXh mm	ηYv mm	ηYh mm	Nodo1	Nodo2	η mm	ηAmm mm	Cs
0-1	(12+13)-III-3	4.83	6.76	2.05	0.35	1	12	11.59	24.10	2.08
0-1	(12+13)-I-4	4.65	6.36	2.01	2.17	2	13	11.02	24.10	2.19
0-1	(12+13)-I-4	4.81	6.37	2.09	2.20	3	14	11.19	24.10	2.15
0-1	(12+13)-I-4	5.03	6.29	2.20	2.20	4	15	11.32	24.10	2.13
0-1	(12+13)-V-4	5.20	6.23	2.33	2.12	5	16	11.43	24.10	2.11
0-1	(12+13)-V-4	5.02	6.44	2.32	2.24	6	17	11.46	24.10	2.10
0-1	(12+13)-V-4	4.82	6.37	2.29	2.24	7	18	11.19	24.10	2.15
0-1	(12+13)-V-4	4.66	6.35	2.26	2.26	8	19	11.01	24.10	2.19
0-1	(12+13)-VII-4	4.62	6.27	2.28	2.24	9	20	10.89	24.10	2.21
0-1	(12+13)-VII-4	4.52	5.99	2.25	2.12	10	21	10.51	24.10	2.29
0-1	(12+13)-VII-4	4.66	6.08	2.37	2.20	11	22	10.73	24.10	2.25
2-3	(12+13)-I-4	0.41	4.38	0.28	1.54	1	12	4.79	13.25	2.77
2-3	(12+13)-I-4	0.50	4.46	0.30	1.56	2	13	4.96	13.25	2.67
2-3	(12+13)-I-4	0.58	4.49	0.32	1.56	3	14	5.07	13.25	2.61
2-3	(12+13)-I-4	0.65	4.47	0.33	1.54	4	15	5.12	13.25	2.59
2-3	(12+13)-I-4	0.70	4.39	0.33	1.49	5	16	5.09	13.25	2.61
2-3	(12+13)-VII-4	0.72	4.32	0.32	1.62	6	17	5.04	13.25	2.63
2-3	(12+13)-VII-4	0.63	4.37	0.26	1.62	7	18	5.00	13.25	2.65
2-3	(12+13)-VII-4	0.60	4.36	0.23	1.62	8	19	4.96	13.25	2.67
2-3	(12+13)-VII-4	0.54	4.36	0.19	1.63	9	20	4.90	13.25	2.70
2-3	(12+13)-V-3	0.48	4.63	0.14	0.31	10	21	5.11	13.25	2.59
2-3	(12+13)-VII-4	0.65	4.34	0.28	1.62	11	22	5.00	13.25	2.65
Minimo										
0-1	(12+13)-III-3	4.83	6.76	2.05	0.35	1	12	11.59	24.10	2.08

Periodi di vibrazione e Masse modali

Scenario di calcolo : **Set NT SLV A2 STR/GEO**

Posizione masse 1

Numero di Frequenze calcolate =45, filtrate=19

N	T(s)	Coef. Partecipazione	Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	
1(1)	0.2975	17.053	57.630	2852	32570	78.77
2(2)	0.2967	-58.272	16.932	33299	2812	80.53
3(3)	0.2404	4.977	6.306	243	390	0.59
4(4)	0.1783	1.365	-4.472	18	196	0.04
5(5)	0.1780	0.651	4.305	4	182	0.01
6(6)	0.1709	2.675	0.075	70	0	0.17
7(8)	0.1520	2.935	-7.086	84	492	0.20
8(12)	0.1308	-3.026	3.195	90	100	0.22
9(13)	0.1250	2.865	-8.511	80	710	0.19
10(14)	0.1194	5.921	-12.213	344	1463	0.83
11(15)	0.1103	1.590	-2.252	25	50	0.06
12(16)	0.1046	-2.284	-1.653	51	27	0.12
13(17)	0.1014	-0.660	5.629	4	311	0.01
14(18)	0.0920	-0.825	3.294	7	106	0.02
15(19)	0.0897	6.979	-0.479	478	2	1.16
16(20)	0.0862	16.165	7.074	2563	491	6.20
17(21)	0.0843	2.863	1.086	80	12	0.19
18(22)	0.0772	-1.401	-4.752	19	221	0.05
19(41)	0.0400	2.070	-4.688	42	215	0.10
Somma delle Masse Modali [kgm*g]			40354		40350	
Masse strutturali libere [kgm*g]			41350		41350	

Posizione masse		4	
N	T(s)	Coeff. Partecipazione	Percentuali
Percentuale			
		97.59	97.58
		97.59	97.59

Posizione masse		2	
Numero di Frequenze calcolate =45, filtrate=22			
N	T(s)	Coeff. Partecipazione	Percentuali
		Dir=0°	Dir=90°
		kgm°g	kgm°g
1(1)	0.2919	54.529	7381
2(2)	0.2892	27.312	-53.904
3(3)	0.2319	0.125	3.809
4(4)	0.1818	-0.273	2.146
5(5)	0.1725	2.944	0.036
6(6)	0.1655	-4.823	-2.736
7(7)	0.1526	-2.359	7.330
8(8)	0.1453	2.280	-3.410
9(9)	0.1368	-2.987	2.954
10(12)	0.1208	-5.187	13.154
11(13)	0.1195	-2.367	4.344
12(14)	0.1155	4.154	-7.680
13(16)	0.0988	2.680	-3.247
14(18)	0.0898	-6.594	-4.194
15(19)	0.0860	-2.482	0.131
16(20)	0.0844	8.208	2.286
17(21)	0.0824	-12.729	-6.150
18(24)	0.0737	-0.344	3.124
19(26)	0.0648	2.504	1.899
20(33)	0.0491	1.630	-3.716
21(37)	0.0445	0.852	-2.138
22(38)	0.0441	-1.117	2.301
Somma delle Masse Modali [kgm°g]		40384	40385
Masse strutturali libere [kgm°g]		41350	41350
Percentuale		97.66	97.67

Posizione masse		3	
Numero di Frequenze calcolate =45, filtrate=20			
N	T(s)	Coeff. Partecipazione	Percentuali
		Dir=0°	Dir=90°
		kgm°g	kgm°g
1(1)	0.2925	58.268	17.330
2(2)	0.2893	16.809	-58.084
3(3)	0.2306	6.203	-0.932
4(6)	0.1669	-4.873	-2.860
5(7)	0.1528	-3.636	7.473
6(8)	0.1436	-2.427	2.217
7(9)	0.1374	2.504	-0.812
8(10)	0.1372	2.084	-3.100
9(12)	0.1233	-3.169	8.592
10(13)	0.1180	6.037	-12.885
11(15)	0.1098	-0.935	9
12(16)	0.0997	1.282	-3.177
13(18)	0.0909	7.203	1.075
14(19)	0.0855	-4.160	-3.297
15(20)	0.0837	11.311	6.496
16(21)	0.0822	8.655	4.290
17(24)	0.0732	-2.607	1.569
18(26)	0.0648	2.765	1.378
19(33)	0.0490	1.451	-3.787
20(37)	0.0443	-1.212	2.911
Somma delle Masse Modali [kgm°g]		40294	40318
Masse strutturali libere [kgm°g]		41350	41350
Percentuale		97.45	97.50

Posizione masse 4

Numero di Frequenze calcolate =45, filtrate=21

		Coeff. Partecipazione		Masse Modali		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
		kgm°g	kgm°g	kgm°g	kgm°g	kgm°g	kgm°g
N	T(s)						
1(1)	0.2973	-29.851	52.261	8739	26785	21.13	64.77
2(2)	0.2959	-53.043	-30.153	27592	8916	66.73	21.56
3(3)	0.2404	-3.414	2.062	42	114	0.10	0.28
4(4)	0.1796	-0.411	4.675	2	214	0.00	0.52
5(5)	0.1776	-2.508	2.788	62	76	0.15	0.18
6(7)	0.1585	-0.640	3.260	4	104	0.01	0.25
7(8)	0.1517	3.634	-6.471	130	411	0.31	0.99
8(10)	0.1420	0.833	-2.500	7	61	0.02	0.15
9(11)	0.1315	3.155	3.172	99	98	0.24	0.24
10(12)	0.1290	-0.711	4.226	5	175	0.01	0.42
11(13)	0.1278	0.764	-2.332	6	53	0.01	0.13
12(14)	0.1200	6.209	-13.936	378	1905	0.91	4.61
13(15)	0.1105	-1.914	4.381	36	188	0.09	0.46
14(17)	0.1017	3.746	0.573	138	3	0.33	0.01
15(18)	0.0927	1.029	-5.494	10	296	0.03	0.72
16(19)	0.0914	4.946	-0.103	240	0	0.58	0.00
17(20)	0.0859	16.613	7.967	2707	622	6.55	1.51
18(21)	0.0839	2.702	0.933	72	9	0.17	0.02
19(22)	0.0776	-1.316	3.539	17	123	0.04	0.30
20(41)	0.0397	1.728	-3.502	29	120	0.07	0.29
21(42)	0.0392	-1.653	3.850	27	145	0.06	0.35
Somma delle Masse Modali [kgm°g]				40338	40419		
Masse strutturali libere [kgm°g]				41350	41350		
Percentuale				97.55	97.75		

Risultati Analisi Dinamica - Massime tensioni sul terreno aste

Scenario di calcolo : Set NT_S1_V_A2 STR/GEO											
Asta	N.in.	N.fin.	0/5	1/5	2/5	3/5	4/5	5/5			
			kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq			
9005	1	2	1.40(12-1-2)	1.42(2)	1.45(2)	1.48(2)	1.52(2)	1.56(2)			
9005	10	11	1.49(2)	1.43(2)	1.39(2)	1.35(13-1-3)	1.40(13-1-3)	1.45(13-1-3)			
9005	9	10	1.57(2)	1.54(2)	1.52(2)	1.51(2)	1.50(2)	1.49(2)			
9005	8	9	1.58(2)	1.56(2)	1.55(2)	1.55(2)	1.56(2)	1.57(2)			
9005	7	8	1.56(2)	1.55(2)	1.55(2)	1.55(2)	1.56(2)	1.57(2)			
9005	6	7	1.52(2)	1.51(2)	1.52(2)	1.52(2)	1.54(2)	1.56(2)			
9005	5	6	1.51(2)	1.50(2)	1.49(2)	1.49(2)	1.50(2)	1.52(2)			
9005	4	5	1.54(2)	1.53(2)	1.51(2)	1.50(2)	1.50(2)	1.51(2)			
9005	3	4	1.59(2)	1.57(2)	1.56(2)	1.55(2)	1.54(2)	1.54(2)			
9005	2	3	1.56(2)	1.56(2)	1.56(2)	1.57(2)	1.58(2)	1.59(2)			
9006	1	2	2.02(12-11-1)	1.96(12-11-1)	1.90(12-11-1)	1.85(12-11-1)	1.80(12-11-1)	1.75(12-11-1)			
9006	9	10	1.98(12-11-4)	2.07(12-11-4)	2.17(12-11-4)	2.27(12-11-4)	2.37(12-11-4)	2.47(12-11-4)			
9006	8	9	1.74(12-11-4)	1.79(12-11-4)	1.84(12-11-4)	1.89(12-11-4)	1.94(12-11-4)	1.99(12-11-4)			
9006	7	8	1.59(12-11-4)	1.62(12-11-4)	1.65(12-11-4)	1.68(12-11-4)	1.71(12-11-4)	1.74(12-11-4)			
9006	11	7	1.56(12-11-4)	1.57(12-11-4)	1.58(12-11-4)	1.58(12-11-4)	1.59(12-11-4)	1.60(12-11-4)			
9006	6	11	1.57(12-11-4)	1.57(12-11-4)	1.57(12-11-4)	1.57(12-11-4)	1.56(12-11-4)	1.56(12-11-4)			
9006	5	6	1.64(12-11-1)	1.63(12-11-4)	1.61(12-11-4)	1.58(12-11-4)	1.57(12-11-4)	1.57(12-11-4)			
9006	4	5	1.61(12-11-1)	1.62(12-11-1)	1.63(12-11-1)	1.64(12-11-1)	1.64(12-11-1)	1.64(12-11-1)			
9006	3	4	1.65(12-11-1)	1.64(12-11-1)	1.63(12-11-1)	1.63(12-11-1)	1.62(12-11-1)	1.62(12-11-1)			
9006	2	3	1.75(12-11-1)	1.73(12-11-1)	1.71(12-11-1)	1.69(12-11-1)	1.67(12-11-1)	1.64(12-11-1)			

Risultati Analisi Dinamica - Reazioni massime - Nodi

Scenario di calcolo : Set NT_S1_V_A2 STR/GEO									
Nodo	Rx	Ry	Rz	Mx	My	Mz			
	kg	kg	kg	kg°m	kg°m	kg°m			
1	-1812(7)	-2422(13-1-2)	0	0	0	0			
1	2373(6)	2024(13-11-1)	0	0	0	0			
2	-1804(7)	-2534(13-1-2)	0	0	0	-23(13-1-2)			
2	2448(6)	2077(13-11-1)	0	0	0	0			

3	2620(6)	1139(13-II-1)	0	0	0	0	0	0	0
3	-187(7)	-751(13-I-2)	0	0	0	0	0	0	0
4	2809(6)	1262(13-I-1)	0	0	0	0	0	0	0
4	-1940(7)	-804(13-I-2)	0	0	0	0	0	0	0
5	2988(6)	1257(13-II-4)	0	0	0	0	0	0	0
5	-1999(7)	-798(13-I-2)	0	0	0	0	0	0	0
6	-2108(7)	-2480(13-I-2)	0	0	0	0	0	0	-2(13-II-3)
6	2961(6)	1904(13-I-4)	0	0	0	0	0	0	0
7	-1979(7)	-2639(13-I-2)	0	0	0	0	0	0	-1(13-I-2)
7	2515(6)	1145(13-II-4)	0	0	0	0	0	0	0
8	-2174(7)	-885(13-I-3)	0	0	0	0	0	0	0
8	2337(6)	1150(6)	0	0	0	0	0	0	0
9	-1760(7)	-862(13-I-3)	0	0	0	0	0	0	0
9	2806(12-II-3)	1438(13-I-3)	0	0	0	0	0	0	0
10	2727(12-II-3)	1286(13-II-3)	0	0	0	0	0	0	0
10	-2174(7)	-1832(13-I-2)	0	0	0	0	0	0	-1(7)
11	2737(6)	2131(13-II-4)	0	0	0	0	0	0	0
11	-2065(7)	-2124(13-I-3)	0	0	0	0	0	0	3(13-I-4)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Travi

Scenario di calcolo - Set NT SLV A2 STR/GEO									
Asta	N.in	N.fin	N	Ty	Tz	Mt	My	Mz	
				kg	kg	kg*m	kg*m	kg*m	kg*m
8000	7	-4178(6)	192(13-I-2)	-1187(3)	-3(13-I-2)	2632(12-I-1)	175(13-I-2)		
8	8	-3839(6)	192(13-I-2)	-1006(13-II-1)	-3(13-I-2)	-1882(12-II-1)	222(13-II-1)		
8000	8	-2622(13-I-4)	280(13-II-1)	-872(3)	-1(13-II-1)	-1895(12-II-1)	207(13-II-1)		
9	-2480(13-I-4)	280(13-II-1)	-733(12-I-1)	-733(12-I-1)	-2192(13-II-1)	207(13-II-4)			
8000	9	-2398(13-I-4)	-80(12-II-3)	-925(12-I-1)	-4(12-I-3)	-2202(13-II-1)	-278(13-II-4)		
35	-2273(13-I-4)	-80(12-II-3)	-810(12-I-1)	-4(12-I-3)	-2652(13-II-1)	-187(13-II-4)			
8000	12	-4850(6)	-125(13-I-2)	-1504(3)	6(13-I-3)	3877(3)	-47(13-I-4)		
7	-4485(6)	-125(13-I-2)	-125(13-I-2)	-125(13-I-2)	6(13-I-3)	2665(12-I-1)	176(13-I-2)		
8000	35	-2404(13-I-4)	-68(13-I-2)	-737(12-I-1)	-3(12-I-3)	-2638(13-II-1)	-203(13-II-4)		
36	-2297(13-I-4)	-68(13-I-2)	733(12-II-1)	733(12-II-1)	-3(12-I-3)	-2222(13-II-4)	-285(13-II-3)		
8000	36	-2162(13-I-4)	-165(13-II-3)	793(13-II-1)	11(13-II-4)	-2221(13-II-4)	-312(13-II-3)		
37	2170(13-II-4)	904(13-II-1)	904(13-II-1)	904(13-II-1)	11(13-II-4)	-2495(12-I-1)	-94(13-II-4)		
8000	37	-1075(12-I-1)	-28(13-I-4)	1391(13-II-1)	14(13-II-4)	-2490(12-I-1)	-101(13-II-3)		
38	-1016(12-I-1)	-28(13-I-4)	1498(13-II-1)	14(13-II-4)	-2287(12-I-1)	84(13-I-2)			
8000	38	-1168(12-II-1)	260(13-I-2)	1462(13-II-1)	18(13-II-3)	-2279(12-I-1)	90(13-I-2)		
39	-1134(12-II-1)	260(13-I-2)	1565(13-II-1)	18(13-II-3)	2404(13-II-1)	-192(13-I-3)			
8000	39	-2292(13-II-1)	-254(13-I-2)	1156(6)	20(13-I-4)	2544(13-I-2)	-220(13-I-3)		
40	-2286(13-I-1)	-254(13-I-2)	1358(6)	20(13-I-4)	3235(13-II-1)	42(13-I-2)			
8000	40	-2437(13-II-1)	48(13-II-3)	1032(3)	-17(13-II-4)	3294(13-II-1)	60(13-I-2)		
12	-2465(13-II-1)	48(13-II-3)	1214(3)	-7(13-II-4)	3628(6)	73(13-I-4)			
8001	10	-5396(6)	288(13-I-2)	-148(3)	2(13-I-1)	2340(12-I-1)	260(13-I-3)		
11	-4803(6)	288(13-I-2)	-1037(3)	2(13-I-1)	-2345(12-II-1)	332(13-II-1)			
8001	11	-5292(6)	460(13-II-1)	-823(3)	5(13-I-1)	-2345(12-II-1)	339(13-II-1)		
12	-4757(6)	460(13-II-1)	-457(12-I-2)	5(13-I-1)	-2418(12-II-1)	-456(13-II-4)			
8001	12	-4314(6)	-114(13-II-1)	-787(12-I-1)	1(13-I-3)	-2420(12-II-1)	-476(13-II-4)		
41	-3857(6)	-114(13-II-1)	-615(12-I-1)	1(13-I-3)	-2307(3)	-303(13-II-4)			
8001	13	-6503(6)	-127(13-II-1)	-2225(3)	-2(13-I-2)	4806(3)	341(13-I-1)		
10	-5292(6)	-127(13-II-1)	916(12-II-1)	8(13-II-4)	-2733(12-I-1)	-287(13-II-4)			
8001	41	-4290(6)	138(13-II-2)	-824(12-I-1)	-3(13-II-2)	-2304(3)	255(13-I-3)		
42	-3905(6)	138(13-II-2)	948(12-II-1)	948(12-II-1)	-3(13-II-2)	-1928(3)	-522(13-II-4)		
8001	42	-3678(6)	-265(13-II-3)	907(12-II-1)	7(13-II-4)	-1932(3)	-586(13-II-4)		
43	-3383(6)	-265(13-II-3)	1069(12-II-1)	7(13-II-4)	-2231(12-I-1)	-230(13-II-4)			
8001	43	-2536(6)	-149(13-II-4)	916(12-II-1)	8(13-II-4)	-2743(12-I-1)	-287(13-II-4)		
44	-2330(6)	-149(13-II-4)	1074(12-II-1)	8(13-II-4)	-2233(12-I-1)	-109(13-II-2)			
8001	44	-2565(12-II-1)	-219(13-II-2)	850(6)	12(13-II-2)	-2743(12-I-1)	-154(13-II-3)		
45	-2516(12-II-1)	-219(13-II-2)	1218(6)	12(13-II-2)	3086(12-II-1)	-98(13-II-3)			
8001	45	-1855(12-II-1)	-71(13-I-3)	1386(13-II-4)	14(13-I-3)	3086(12-II-1)	-90(13-I-3)		
46	-1848(12-II-1)	-71(13-I-3)	1535(13-II-4)	14(13-I-3)	2914(12-II-1)	45(13-II-4)			
8001	46	-1864(12-II-1)	78(13-II-4)	1651(13-II-4)	-18(13-II-4)	2914(12-II-1)	24(13-I-2)		
13	-1896(12-I-1)	78(13-II-4)	1795(13-II-4)	-18(13-II-4)	-3835(6)	-71(13-II-3)			
8002	13	-5678(6)	257(13-I-2)	-1524(3)	-2(13-I-3)	2365(12-I-1)	223(13-I-3)		
14	-5094(6)	257(13-I-2)	-1087(3)	-2(13-I-3)	-2358(12-II-1)	337(13-II-1)			
8002	14	-5094(6)	450(13-II-1)	-940(3)	-3(13-II-1)	-2338(12-II-1)	344(13-II-1)		

	15	-4532(6)	450(13-I-1)	-535(12-I-2)	-3(13-I-1)	-2475(12-II-1)	-439(13-I-4)
8002	14	-6823(6)	-153(13-I-3)	-2256(3)	-6(13-I-2)	5059(3)	136(13-II-1)
	13	-6201(6)	-153(13-I-3)	-1806(3)	-6(13-I-2)	2365(12-I-1)	218(13-I-3)
8002	15	-4698(6)	-83(13-I-3)	-862(12-I-1)	2(6)	-2474(12-II-1)	-460(13-II-4)
	47	-3645(6)	-83(13-I-3)	-691(12-I-1)	2(6)	-2576(3)	-445(13-I-4)
8002	47	-3291(6)	84(13-I-2)	-850(12-I-1)	-4(13-I-2)	-2570(3)	-480(13-II-4)
	48	-2908(6)	84(13-I-2)	949(12-I-1)	-4(13-I-2)	-2254(3)	-580(13-I-4)
8002	48	-2688(6)	-234(13-I-3)	912(12-II-1)	4(13-I-2)	-2257(3)	-656(13-I-4)
	49	-2395(6)	-234(13-I-3)	1074(12-II-1)	4(13-I-2)	-2323(12-I-1)	-342(13-I-4)
8002	49	-2429(12-I-1)	-213(13-I-4)	879(12-II-1)	-6(13-I-4)	-2322(12-I-1)	-421(13-I-4)
	50	-2344(12-I-1)	-213(13-I-4)	1184(6)	-6(13-I-4)	-2627(12-I-1)	-162(13-II-2)
8002	50	-2615(12-I-1)	-317(13-I-2)	1061(6)	-11(13-I-2)	-2627(12-I-1)	-235(13-II-2)
	51	-2567(12-I-1)	-317(13-I-2)	1430(6)	-11(13-I-2)	2934(12-II-1)	125(13-I-4)
8002	51	-1639(12-I-1)	-48(13-I-2)	1025(3)	14(13-I-3)	2934(12-II-1)	-82(13-I-2)
	52	-1632(12-I-1)	-48(13-I-2)	1372(3)	14(13-I-3)	2987(12-II-1)	71(13-II-4)
8002	52	-1819(6)	40(13-I-2)	1307(12-I-1)	-18(13-I-4)	2987(12-II-1)	23(13-I-2)
	14	-1895(6)	40(13-I-2)	1539(3)	-18(13-I-4)	4118(6)	38(13-I-2)
8003	1	-6140(6)	297(13-I-2)	-1616(3)	2(13-I-3)	2439(12-I-2)	251(13-I-3)
	2	-5548(6)	297(13-I-2)	-1174(3)	2(13-I-3)	-2333(12-II-1)	383(13-II-1)
8003	2	-5583(6)	443(13-II-1)	-1013(3)	-5(13-II-1)	-2335(12-II-1)	394(13-II-1)
	3	-5041(6)	443(13-II-1)	-577(3)	-5(13-II-1)	-2522(12-II-1)	-381(13-II-4)
8003	3	-4581(6)	-99(13-I-2)	-864(12-I-1)	2(13-I-3)	-2522(12-II-1)	-398(13-I-4)
	23	-4107(6)	-99(13-I-2)	-688(12-I-1)	2(13-I-3)	-2771(3)	-416(13-I-4)
8003	15	-7297(6)	-96(13-I-3)	-2334(6)	-3(13-I-3)	5365(3)	79(13-I-2)
	1	-6676(6)	-96(13-I-3)	-1885(3)	-3(13-I-3)	2439(12-I-2)	246(13-I-2)
8003	23	-3740(6)	46(13-I-2)	-833(12-I-1)	-1(13-I-3)	-2775(3)	-500(13-I-4)
	24	-3333(6)	46(13-I-2)	947(12-II-1)	-1(13-I-3)	-2438(3)	-500(13-I-4)
8003	24	-3086(6)	-202(13-I-3)	924(12-II-1)	4(13-I-1)	-2438(3)	-567(13-I-4)
	25	-2769(6)	-202(13-I-3)	1097(12-II-1)	4(13-I-1)	-2321(12-I-1)	-299(13-I-4)
8003	25	-2665(6)	-152(13-II-4)	904(12-II-1)	-4(13-I-4)	-2318(12-I-1)	-375(13-I-4)
	26	-2438(6)	-152(13-II-4)	1269(6)	-4(13-I-4)	-2610(12-I-1)	-191(13-II-3)
8003	26	-2725(12-I-1)	-440(13-I-3)	1140(6)	15(13-I-1)	-2610(12-I-1)	-264(13-I-3)
	27	-2672(12-I-1)	-440(13-I-3)	1555(6)	15(13-I-1)	2932(12-II-1)	233(13-I-3)
8003	27	-1814(6)	-174(13-I-3)	1132(3)	16(13-I-3)	2922(12-II-1)	223(13-II-3)
	28	-1795(6)	-174(13-I-3)	1531(3)	16(13-I-3)	3050(12-II-1)	49(13-II-4)
8003	28	-2203(6)	-59(13-I-3)	1346(12-I-1)	-17(13-I-4)	3050(12-II-1)	23(13-I-2)
	15	-2292(6)	-59(13-I-3)	1735(3)	-17(13-I-4)	4478(6)	55(13-I-2)
8004	16	-7634(6)	-81(13-I-3)	-2395(6)	-3(13-I-3)	5577(3)	-115(13-I-1)
	19	-7012(6)	-81(13-I-3)	-1945(3)	-3(13-I-3)	2503(12-I-2)	238(13-I-3)
8004	19	-6467(6)	304(13-I-2)	-1668(3)	-2(13-I-3)	2503(12-I-2)	242(13-I-3)
	20	-5866(6)	304(13-I-2)	-1219(3)	-2(13-I-3)	-2242(12-II-1)	391(13-II-1)
8004	20	-6164(6)	476(13-I-1)	-1070(3)	-3(13-I-1)	-2242(12-II-1)	399(13-II-1)
	21	-5607(6)	476(13-I-1)	-621(3)	-3(13-I-1)	-2476(12-II-1)	-435(13-I-4)
8004	21	-5124(6)	-53(13-I-2)	-848(12-I-1)	0	-2476(12-II-1)	-456(13-I-4)
	59	-4631(6)	-53(13-I-2)	-666(12-I-1)	0	-2879(3)	-413(13-I-4)
8004	59	-4234(6)	-82(13-I-2)	-814(12-I-1)	-5(13-I-3)	-2879(3)	-448(13-I-4)
	60	-3804(6)	-82(13-I-2)	913(12-II-1)	-5(13-I-3)	-2571(3)	-546(13-I-4)
8004	60	-3526(6)	-248(13-I-3)	891(12-II-1)	3(13-I-1)	-2574(3)	-618(13-I-4)
	61	-3185(6)	-248(13-I-3)	1073(12-II-1)	3(13-I-1)	-2326(12-I-2)	-286(13-I-4)
8004	61	-3061(6)	-129(13-II-4)	892(12-II-1)	4(13-I-4)	-2326(12-I-2)	-358(13-I-4)
	62	-2815(6)	-129(13-II-4)	1327(6)	4(13-I-4)	-2538(12-I-1)	-202(13-I-3)
8004	62	-2879(6)	-342(13-I-3)	1189(6)	19(13-I-4)	-2538(12-I-1)	-268(13-I-3)
	63	-2735(6)	-342(13-I-3)	1649(6)	19(13-I-4)	2853(12-I-1)	-120(13-I-4)
8004	63	-2194(6)	-128(13-I-3)	1188(3)	20(13-I-3)	2857(12-II-1)	-145(13-I-4)
	64	-2173(6)	-128(13-I-3)	1639(6)	20(13-I-3)	3063(12-II-1)	26(13-I-2)
8004	64	-2611(6)	311(13-I-2)	1423(3)	-16(13-II-4)	3063(12-II-1)	32(13-I-3)
	16	-2713(6)	311(13-I-2)	1871(3)	-16(13-II-4)	4741(6)	-41(13-I-2)
8005	16	-5687(6)	242(13-I-2)	-1645(3)	-1(13-I-4)	2564(12-I-3)	166(13-I-3)
	17	-5106(6)	242(13-I-2)	-1208(3)	-1(13-I-4)	-2257(12-I-3)	-340(13-I-3)
8005	17	-5165(6)	377(13-II-1)	-1042(3)	-7(13-I-1)	-2263(12-I-3)	-345(13-I-1)
	18	-4635(6)	377(13-II-1)	-681(12-I-2)	-7(13-I-1)	-2429(6)	-317(13-II-4)
8005	17	-6838(6)	-112(13-II-1)	-2374(3)	0	5464(3)	208(13-I-2)
	16	-6226(6)	-112(13-II-1)	-1929(3)	0	2567(12-I-3)	166(13-I-3)
8005	18	-4166(6)	-61(13-I-2)	-904(12-I-4)	-1(13-I-2)	-2432(6)	-334(13-I-4)
	53	-3706(6)	-61(13-I-2)	732(12-I-4)	-1(13-I-2)	-2860(3)	-330(13-I-4)
8005	53	-3641(6)	-61(13-I-2)	-773(12-I-4)	-1(13-I-2)	-2859(3)	-353(13-I-4)
	54	-3249(6)	-41(13-I-2)	820(12-I-3)	1(13-I-2)	-2528(3)	-383(13-I-4)

8005	54	-3067(12-II-1)	-164(13-II-3)	794(12-II-3)	7(13-II-4)	-2502(3)	-43(13-II-4)
8005	55	-2945(12-II-1)	-164(13-II-3)	960(12-II-3)	7(13-II-4)	-2488(12-I-3)	-217(13-II-4)
8005	56	-2620(6)	-139(13-II-4)	1216(13-II-4)	8(13-II-4)	-2510(12-I-3)	268(13-I-4)
8005	56	-2406(6)	-139(13-II-4)	1379(13-II-4)	8(13-II-4)	-2379(12-I-3)	107(13-II-2)
8005	57	-2486(6)	197(13-I-3)	1155(6)	14(13-II-1)	-2347(12-I-3)	146(13-I-2)
8005	57	-2365(6)	197(13-I-3)	1548(6)	14(13-II-1)	-2555(13-II-4)	-67(13-I-4)
8005	57	-2377(13-II-1)	30(13-II-3)	1201(13-I-3)	-1(13-I-3)	2527(13-II-4)	48(13-II-4)
8005	58	-2370(13-II-4)	30(13-II-3)	1527(6)	-1(13-I-3)	2830(12-II-4)	-32(13-II-4)
8005	58	-2360(13-II-4)	65(13-II-4)	1676(13-I-3)	-18(13-II-4)	2845(6)	-15(13-I-2)
8006	17	-2385(13-II-4)	65(13-II-4)	1924(6)	-18(13-II-4)	4802(6)	-70(13-II-4)
8006	18	-7198(6)	-95(13-I-3)	-2252(3)	1(13-II-2)	5137(3)	-66(13-II-1)
8006	22	-6582(6)	-95(13-I-3)	-1807(3)	1(13-II-2)	2336(12-I-3)	216(13-I-3)
8006	22	-6067(6)	303(13-I-2)	-1528(3)	-1(13-I-1)	2336(12-I-3)	219(13-I-2)
8006	23	-5487(6)	303(13-I-2)	-1095(3)	-1(13-I-1)	-2096(12-II-3)	-387(13-I-1)
8006	23	-5109(6)	-427(13-I-1)	-980(3)	-4(13-II-1)	-2096(12-II-3)	-395(13-I-1)
8006	24	-4586(6)	-427(13-I-1)	-565(13-I-3)	-4(13-II-1)	-2460(12-II-4)	352(13-I-4)
8006	24	-4143(6)	49(13-II-2)	-697(12-I-4)	-1(13-II-2)	-2460(12-II-4)	367(13-I-4)
8006	65	-3692(6)	49(13-II-2)	-527(12-I-4)	-1(13-II-2)	-2639(3)	314(13-I-4)
8006	65	-3325(13-II-4)	-89(13-I-2)	-773(12-I-4)	2(13-I-2)	-2639(3)	338(13-I-4)
8006	66	-3170(13-II-4)	-89(13-I-2)	852(12-II-4)	2(13-I-2)	-2365(3)	459(13-I-4)
8006	66	-3256(13-II-4)	210(13-I-3)	933(12-II-4)	6(13-II-4)	-2362(3)	518(13-I-4)
8006	67	-3136(13-II-1)	210(13-I-3)	1095(12-II-4)	6(13-II-4)	-2080(12-I-3)	236(13-I-4)
8006	67	-2101(13-II-1)	116(13-I-4)	1129(12-II-1)	6(13-II-4)	-2080(12-I-3)	295(13-I-4)
8006	68	-2016(12-II-1)	116(13-I-4)	1287(12-II-1)	6(13-II-4)	-2605(12-I-4)	155(13-I-1)
8006	68	-2309(12-II-1)	315(13-I-4)	1133(6)	15(13-II-1)	-2605(12-I-4)	214(13-I-1)
8006	69	-2261(12-II-1)	315(13-I-4)	1502(6)	15(13-II-1)	-2605(12-I-4)	-144(13-I-4)
8006	69	-2110(12-II-1)	111(13-I-3)	1161(3)	-15(13-I-3)	3180(12-II-4)	137(13-II-4)
8007	5	-5119(6)	283(13-I-2)	-1075(3)	2(13-I-3)	-2167(12-II-3)	-382(13-I-1)
8007	5	-4999(6)	-456(13-I-1)	-953(3)	3(13-I-4)	-2167(12-II-3)	-389(13-I-1)
8007	6	-4474(6)	-456(13-I-1)	-531(3)	3(13-I-4)	-2381(12-II-4)	414(13-I-4)
8007	6	-4032(6)	68(13-II-2)	-750(12-I-3)	0	-2381(12-II-4)	403(13-I-4)
8007	19	-6837(6)	113(13-II-3)	-2239(6)	3(13-II-3)	504(13-I)	-32(13-I-1)
8007	4	-6218(6)	113(13-II-3)	-179(3)	3(13-II-3)	2300(12-I-3)	-211(13-I-1)
8007	29	-3232(6)	-98(13-I-2)	-744(12-I-3)	-3(13-II-3)	-2596(3)	437(13-I-4)
8007	30	-2851(6)	-98(13-I-2)	847(12-I-3)	-3(13-II-3)	-2278(3)	568(13-I-4)
8007	30	-2627(6)	235(13-I-4)	856(12-II-4)	-4(13-I-1)	-2271(3)	643(13-I-4)
8007	31	-2334(6)	235(13-I-4)	1018(12-II-4)	-4(13-I-1)	-2111(12-I-3)	328(13-I-4)
8007	31	-2262(6)	196(13-I-4)	892(12-II-4)	-5(13-I-4)	-2110(12-I-3)	405(13-I-4)
8007	32	-2080(12-II-3)	196(13-I-4)	1190(6)	-5(13-I-4)	-2397(12-I-3)	167(13-I-1)
8007	32	-2358(12-II-3)	318(13-I-4)	1075(6)	-12(13-I-1)	-2397(12-I-3)	240(13-I-4)
8007	33	-2310(12-II-3)	51(13-II-2)	1444(6)	-12(13-I-1)	2752(12-II-3)	-121(13-I-4)
8007	33	-1558(12-II-3)	51(13-II-2)	1048(3)	-13(13-II-3)	2752(12-II-3)	79(13-II-2)
8007	34	-1551(12-II-3)	51(13-II-2)	1396(3)	-13(13-II-3)	3000(12-II-4)	-72(13-I-4)
8007	34	-1828(6)	-29(13-II-2)	1224(3)	17(13-I-4)	3000(12-II-4)	-26(13-I-4)
8007	18	-1904(6)	-29(13-II-2)	1558(3)	17(13-I-4)	4169(6)	12(12-I-3)
8008	20	-6673(6)	76(12-I-2)	-2215(3)	3(12-I-2)	4964(3)	-104(13-I-1)
8008	25	-6063(6)	76(12-I-2)	-1776(3)	3(12-I-2)	2200(12-I-3)	-198(13-I-1)
8008	25	-5552(6)	-259(13-I-2)	-149(3)	1(12-I-2)	2200(12-I-3)	-202(12-I-2)
8008	26	-4978(6)	-259(13-I-2)	-1062(3)	1(12-I-2)	-2074(12-II-3)	-363(13-I-1)
8008	26	-5031(6)	-443(13-I-1)	-922(3)	3(13-I-1)	-2074(12-II-3)	-370(13-I-1)
8008	27	-4511(6)	-443(13-I-1)	-505(3)	3(13-I-1)	-2247(12-II-4)	409(13-I-4)
8008	27	-4080(6)	68(12-II-1)	-712(12-I-3)	-1(13-I-4)	-2247(12-II-4)	427(13-I-4)
8008	71	-3632(6)	68(12-II-1)	-544(12-I-3)	-1(13-I-4)	-2521(3)	364(13-I-4)
8008	71	-3273(6)	-165(13-I-2)	-684(12-I-3)	5(13-I-3)	-2514(3)	394(13-I-4)
8008	72	-2894(6)	-165(13-I-2)	785(12-I-3)	5(13-I-3)	-2203(3)	622(13-I-4)
8008	72	-2677(6)	308(13-I-4)	784(12-I-3)	-5(13-I-2)	-2206(3)	698(13-I-4)
8008	73	-2385(6)	308(13-I-4)	946(12-II-3)	-5(13-I-2)	-1974(12-I-3)	283(13-I-4)
8008	73	-2307(6)	159(13-I-4)	831(12-II-4)	-5(13-I-4)	-1974(12-I-3)	358(13-I-4)
8008	74	-2102(6)	159(13-I-4)	1166(6)	-5(13-I-4)	-2213(12-I-3)	164(13-I-4)
8008	74	-2191(6)	289(13-I-4)	1037(6)	13(13-II-1)	-2213(12-I-3)	232(13-I-4)
8008	75	-2075(6)	289(13-I-4)	1406(6)	13(13-II-1)	2592(12-I-3)	97(13-II-4)
8008	75	-1471(6)	56(13-II-2)	979(3)	-14(13-II-4)	2592(12-I-3)	66(13-II-2)

8008	76	-1455(6)	56(13-II-2)	1329(6)	-14(13-I-4)	2896(12-II-4)	-60(13-I-4)
8008	76	-1801(6)	-43(13-II-1)	1154(3)	16(13-I-4)	2896(12-II-4)	-27(13-II-2)
8009	19	-1877(6)	-43(13-II-1)	1490(3)	16(13-I-4)	4001(6)	-35(13-I-1)
8009	21	-6421(6)	126(12-II-1)	-2134(3)	2(12-I-3)	4696(3)	-46(13-II-1)
8009	28	-5822(6)	126(12-II-2)	-1702(3)	2(12-I-3)	1968(12-I-3)	-262(12-I-2)
8009	28	-5308(6)	-268(13-II-2)	-1422(3)	-2(13-I-4)	1968(12-I-3)	-267(12-I-2)
8009	29	-4742(6)	-268(13-II-2)	-998(3)	-2(13-I-4)	-1875(12-II-3)	-335(13-I-1)
8009	29	-5519(6)	-387(13-I-1)	-808(3)	5(13-I-1)	-1875(12-II-3)	-342(13-I-1)
8009	30	-5005(6)	-387(13-I-1)	-451(12-I-3)	5(13-I-1)	-2008(6)	336(13-I-4)
8009	30	-4583(6)	88(13-II-2)	-642(12-I-3)	-2(13-II-2)	-2008(6)	350(13-I-4)
8009	77	-4139(6)	88(13-II-2)	-474(12-I-3)	-2(13-II-2)	-2218(3)	326(13-I-4)
8009	77	-4184(6)	-102(13-I-3)	-552(12-I-3)	2(13-I-2)	-2218(3)	351(13-I-4)
8009	78	-3808(6)	-102(13-I-3)	647(12-II-3)	2(13-I-2)	-2218(3)	489(13-I-4)
8009	78	-3590(6)	262(13-I-2)	587(13-II-4)	-7(13-I-4)	-1924(3)	550(13-I-4)
8009	79	-3299(6)	262(13-I-2)	748(13-II-4)	-7(13-I-4)	-1690(13-I-3)	209(13-I-4)
8009	79	-2235(13-I-4)	114(13-I-4)	750(13-II-4)	-7(13-I-4)	-1690(13-I-3)	241(13-I-4)
8009	80	-2151(13-I-4)	114(13-I-4)	945(6)	-7(13-I-4)	-2006(13-I-4)	111(13-I-4)
8009	80	-2280(13-I-4)	241(13-I-4)	842(6)	13(13-I-4)	-2006(13-I-4)	155(13-I-1)
8009	81	-2232(13-I-4)	241(13-I-4)	1212(6)	13(13-I-4)	2110(13-I-4)	122(13-II-4)
8009	81	-1538(13-II-4)	98(13-II-3)	1482(13-I-4)	-12(13-II-4)	2094(13-II-4)	119(13-II-4)
8009	82	-1531(13-I-4)	98(13-II-3)	1632(13-I-4)	-12(13-II-4)	2760(12-II-3)	-37(13-I-4)
8009	82	-1399(6)	-32(13-II-2)	1906(13-I-4)	15(13-I-4)	2762(12-II-3)	-22(13-II-2)
8009	20	-1476(6)	-32(13-II-2)	2053(13-I-4)	15(13-I-4)	3958(6)	-19(13-II-3)
8010	22	-4171(6)	164(12-I-2)	-1577(3)	-3(12-I-1)	4074(13-I-3)	-33(13-II-1)
8010	31	-3816(6)	164(12-I-2)	-1320(3)	-3(12-I-1)	2301(13-I-3)	-303(12-I-2)
8010	31	-3551(6)	-261(13-II-2)	-1198(3)	4(13-I-4)	2301(13-I-3)	-306(12-I-2)
8010	32	-3214(6)	-261(13-II-2)	-945(3)	4(13-I-4)	-1623(12-II-3)	313(13-II-1)
8010	32	-2254(12-I-1)	-314(13-I-1)	-993(13-I-1)	9(13-I-4)	-1623(12-II-3)	318(13-II-1)
8010	33	-2111(12-I-1)	-314(13-I-1)	-875(13-I-3)	9(13-I-4)	-2279(12-II-4)	254(12-II-1)
8010	33	-1961(12-I-1)	89(12-II-1)	-786(13-I-3)	4(13-I-2)	-2279(12-II-4)	263(12-II-1)
8010	83	-1837(12-I-1)	89(12-II-1)	-670(13-I-3)	4(13-I-2)	-2270(3)	206(13-I-1)
8010	83	-2530(13-I-4)	-67(13-I-3)	-636(12-I-4)	3(12-I-1)	-2270(3)	217(13-I-1)
8010	84	-2423(13-I-4)	-67(13-I-3)	649(12-II-4)	3(12-I-1)	-2524(13-I-3)	308(13-I-2)
8010	84	-2441(13-I-4)	198(13-I-2)	894(12-II-4)	-13(13-I-4)	-2524(13-I-3)	335(13-I-2)
8010	85	-2422(13-I-4)	198(13-I-2)	1007(12-II-4)	-11(13-I-4)	-2223(13-I-3)	70(13-I-3)
8010	85	-1063(12-II-4)	52(13-I-4)	1155(12-II-4)	-11(13-I-4)	-2223(13-I-3)	103(13-I-3)
8010	86	-1003(12-II-4)	52(13-I-4)	1266(12-II-4)	-11(13-I-4)	-2125(12-I-3)	-45(13-II-2)
8010	87	-1256(12-I-4)	-128(13-II-2)	1284(6)	14(13-I-4)	2822(12-II-3)	96(13-II-4)
8010	87	-2093(12-I-3)	94(13-II-3)	957(3)	-10(13-II-3)	2822(12-II-3)	104(13-II-4)
8010	88	-2088(12-II-3)	94(13-II-3)	1175(3)	-10(13-II-3)	3288(12-II-3)	-32(13-II-2)
8010	88	-2218(12-I-3)	-60(13-I-4)	974(3)	16(13-I-4)	3288(12-II-3)	39(13-I-4)
8013	23	967(3)	-2(13-I-2)	-8(3)	0	0	-1(13-I-2)
8013	29	967(3)	-2(13-I-2)	8(1)	0	0	3(13-I-2)
8013	24	1280(6)	-8(13-I-3)	-8(6)	0	0	-8(13-I-3)
8013	26	1280(6)	-8(13-I-3)	8(4)	0	0	4(13-I-3)
8013	25	988(6)	-1(12-I-1)	-8(4)	0	0	-2(12-I-1)
8013	27	988(6)	-1(12-I-1)	8(1)	0	0	-1(13-I-1)
8013	26	1105(3)	-4(6)	-7(6)	0	0	-4(6)
8013	31	1105(3)	-4(6)	7(4)	0	0	2(6)
8013	27	986(6)	-1(13-I-1)	-8(6)	0	0	-1(13-I-1)
8013	23	986(6)	-1(13-I-1)	8(1)	0	0	0
8013	28	737(6)	-3(13-I-1)	-8(4)	0	0	-2(13-I-1)
8013	25	737(6)	-3(13-I-1)	8(6)	0	0	-2(13-I-1)
8013	29	971(3)	-7(13-I-1)	-8(1)	0	0	2(13-I-1)
8013	30	971(3)	-7(13-I-1)	8(3)	0	0	3(13-II-1)
8013	30	1261(3)	-4(13-I-1)	-8(6)	0	0	-8(13-II-3)
8013	24	1261(3)	-4(13-I-1)	8(1)	0	0	7(13-I-1)
8013	31	881(2)	-6(13-I-2)	-8(6)	0	0	2(13-II-2)
8013	32	881(2)	-6(13-I-2)	8(7)	0	0	6(13-I-2)
8013	32	582(3)	6(12-II-3)	-8(6)	0	0	-3(13-I-4)
8013	33	582(3)	6(12-II-3)	8(4)	0	0	0
8014	12	1832(13-I-1)	-17(13-I-1)	-192(6)	0	0	-10(13-I-2)
8014	13	1826(13-I-1)	-17(13-I-1)	180(6)	0	0	12(12-II-3)
8014	13	3638(13-I-2)	-28(13-I-2)	-177(6)	0	0	-16(13-I-2)
8014	14	3639(13-I-2)	-28(13-I-2)	162(6)	0	0	26(13-I-2)

8014	14	2381(13-12)	-45(13-12)	-161(6)	0	0	-34(13-12)
	15	2385(13-12)	-45(13-12)	145(6)	0	0	28(13-12)
8014	15	2082(6)	-21(13-13)	-177(6)	0	0	-16(13-13)
	16	2082(6)	-21(13-13)	160(6)	0	0	15(13-13)
8014	16	2370(13-11)	12(13-13)	-191(6)	0	0	10(13-13)
	17	2366(13-11)	12(13-13)	173(6)	0	0	-9(13-13)
8014	17	2102(6)	22(13-11)	-162(6)	0	0	15(13-11)
	18	2116(6)	22(13-11)	144(6)	0	0	-16(13-11)
8014	18	2021(6)	21(13-13)	-177(6)	0	0	15(13-13)
	19	2021(6)	21(13-13)	161(6)	0	0	-16(13-13)
8014	19	1666(12-13)	18(13-13)	-176(6)	0	0	14(13-13)
	20	1666(12-13)	18(13-13)	158(6)	0	0	-12(13-13)
8014	20	2769(13-11)	22(12-13)	-176(6)	0	0	16(12-13)
	21	2769(13-11)	22(12-13)	156(6)	0	0	-16(12-13)
8014	21	1677(13-11)	24(13-11)	-176(6)	0	0	18(13-11)
	22	1677(13-11)	24(13-11)	157(6)	0	0	-18(13-11)
8015	1	2681(2-1)	-6(13-12)	-326(6)	0	0	-4(13-12)
	19	2681(2-1)	-6(13-12)	326(6)	0	0	5(13-12)
8015	4	345(12-1)	-6(13-14)	-312(6)	0	0	-4(13-14)
	25	345(12-1)	-6(13-14)	309(6)	0	0	-5(13-14)
8015	7	131(13-13)	-17(13-13)	-325(6)	0	0	-22(13-13)
	10	127(13-13)	-17(13-13)	320(6)	0	0	5(12-13)
8015	10	260(13-11)	-12(13-11)	-320(6)	0	0	-9(13-11)
	13	260(13-11)	-12(13-11)	315(6)	0	0	8(13-11)
8015	13	254(13-11)	-4(13-13)	-313(6)	0	0	-3(13-13)
	1	254(13-11)	-4(13-13)	310(6)	0	0	4(13-13)
8015	16	441(13-11)	-8(12-11)	-312(6)	0	0	-6(12-11)
	22	440(13-11)	-8(12-11)	309(6)	0	0	5(12-11)
8015	19	315(12-1)	8(13-13)	-325(6)	0	0	5(12-1)
	16	316(12-1)	8(13-13)	325(6)	0	0	-8(13-13)
8015	22	382(12-1)	12(13-13)	-317(6)	0	0	10(13-13)
	4	382(12-1)	12(13-13)	312(6)	0	0	-7(13-13)
8015	25	320(12-1)	13(12-12)	-310(6)	0	0	8(12-12)
	28	320(12-1)	13(12-12)	307(6)	0	0	-1(12-12)
8015	28	233(12-12)	5(13-12)	-310(6)	0	0	-5(12-12)
	31	233(12-12)	5(13-12)	308(6)	0	0	-5(13-12)
8016	2	-91(6)	-13(13-11)	-314(6)	0	0	1(13-11)
	20	-91(6)	-13(13-11)	315(6)	0	0	-1(13-11)
8016	5	889(13-14)	-18(13-14)	-289(6)	0	0	-13(13-14)
	26	889(13-14)	-18(13-14)	286(6)	0	0	12(13-14)
8016	8	703(13-11)	27(13-11)	-301(6)	0	0	-14(13-11)
	11	703(13-11)	27(13-11)	296(6)	0	0	13(13-11)
8016	11	-1195(13-11)	-15(13-11)	-296(6)	0	0	-15(13-11)
	14	-1195(13-11)	-15(13-11)	292(6)	0	0	6(13-11)
8016	14	-944(13-11)	-17(13-11)	-290(6)	0	0	-13(13-11)
	2	-945(13-11)	-17(13-11)	286(6)	0	0	10(13-11)
8016	17	-1027(6)	-33(13-14)	-288(6)	0	0	-23(13-14)
	23	-1027(6)	-33(13-14)	285(6)	0	0	23(13-14)
8016	20	-1045(6)	12(12-11)	-314(6)	0	0	-11(13-11)
	17	-1045(6)	12(12-11)	315(6)	0	0	12(12-11)
8016	23	-941(6)	13(13-14)	-293(6)	0	0	12(13-14)
	5	-941(6)	13(13-14)	289(6)	0	0	-8(13-14)
8016	26	-1238(13-14)	15(12-11)	-286(6)	0	0	8(13-14)
	29	-1238(13-14)	15(12-11)	284(6)	0	0	-14(12-11)
8016	29	825(13-14)	-20(13-14)	-286(6)	0	0	-19(13-14)
	32	825(13-14)	-20(13-14)	284(6)	0	0	9(13-14)
8017	3	-557(6)	15(13-14)	-298(6)	0	0	13(13-14)
	21	-557(6)	15(13-14)	299(6)	0	0	-10(13-14)
8017	6	-482(6)	-18(13-14)	-260(6)	0	0	-11(13-14)
	27	-482(6)	-18(13-14)	258(6)	0	0	13(13-14)
8017	9	-145(6)	21(6)	-272(6)	0	0	19(13-11)
	12	-146(6)	21(6)	268(6)	0	0	-17(13-13)
8017	12	-334(6)	44(13-14)	-267(6)	0	0	-35(13-14)
	15	-330(6)	44(13-14)	263(6)	0	0	-24(13-11)
8017	15	-462(6)	16(13-14)	-261(6)	0	0	8(13-14)
	3	-465(6)	16(13-14)	259(6)	0	0	-13(13-14)
8017	18	-616(6)	-26(13-13)	-259(6)	0	0	-16(13-13)

8017	24	-616(6)	-26(13-13)	257(6)	0	0	18(13-13)
	21	-610(6)	40(13-14)	-297(6)	0	0	23(13-14)
8017	18	-610(6)	40(13-14)	298(6)	0	0	-36(13-14)
	24	-573(6)	46(13-14)	-264(6)	0	0	36(13-14)
8017	6	-573(6)	46(13-14)	261(6)	0	0	-25(13-14)
	27	-345(6)	-38(13-14)	-258(6)	0	0	-22(13-14)
8017	30	-345(6)	-38(13-14)	256(6)	0	0	29(13-14)
	30	-175(6)	-17(6)	-256(6)	0	0	-16(13-13)
8017	33	-175(6)	-17(6)	255(6)	0	0	14(12-11)
	23	-574(6)	29(13-14)	-278(6)	0	0	24(13-14)
8018	59	-571(6)	29(13-14)	279(6)	0	0	-18(13-14)
	29	-62(6)	-21(13-14)	-231(6)	0	0	-13(13-14)
8018	71	-620(6)	-21(13-14)	229(6)	0	0	13(13-14)
	35	-601(13-14)	17(6)	-243(6)	0	0	17(13-14)
8018	41	-602(13-14)	17(6)	238(6)	0	0	-14(13-11)
	41	-833(13-14)	56(13-14)	-238(6)	0	0	42(13-14)
8018	47	-832(13-14)	56(13-14)	234(6)	0	0	-29(13-14)
	47	-600(3)	32(13-14)	-232(6)	0	0	16(13-14)
8018	23	-604(3)	32(13-14)	230(6)	0	0	-24(13-14)
	53	-574(3)	-22(13-14)	-230(6)	0	0	-12(13-14)
8018	65	-574(3)	-22(13-14)	228(6)	0	0	15(13-14)
	59	-928(13-11)	50(13-14)	-278(6)	0	0	31(13-14)
8018	53	-928(13-11)	50(13-14)	279(6)	0	0	-44(13-14)
	65	-585(3)	65(13-14)	-235(6)	0	0	47(13-14)
8018	29	-585(3)	65(13-14)	232(6)	0	0	-35(13-14)
	71	-997(13-11)	-52(13-14)	-229(6)	0	0	-27(13-14)
8018	77	-997(13-11)	-52(13-14)	227(6)	0	0	39(13-14)
	83	-627(13-11)	-13(3)	-227(6)	0	0	-10(13-14)
8019	83	-627(13-11)	-13(3)	226(6)	0	0	17(13-11)
	24	-263(12-12)	56(13-14)	-257(6)	0	0	42(13-14)
8019	60	-265(3)	56(13-14)	258(6)	0	0	-41(13-14)
	30	-343(13-12)	-71(13-14)	-202(6)	0	0	-44(13-14)
8019	72	-344(13-12)	-71(13-14)	200(6)	0	0	44(13-14)
	36	-78(12-11)	46(13-13)	-213(6)	0	0	36(13-13)
8019	42	-80(12-11)	46(13-13)	209(6)	0	0	-19(13-12)
	48	-285(12-13)	75(13-14)	-203(6)	0	0	43(13-14)
8019	24	-284(12-13)	75(13-14)	201(6)	0	0	-46(13-14)
	54	-364(13-13)	-25(13-12)	-201(6)	0	0	-16(13-12)
8019	66	-363(13-13)	-25(13-12)	200(6)	0	0	14(13-12)
	60	-281(12-13)	74(13-14)	-256(6)	0	0	52(13-14)
8019	54	-280(12-13)	74(13-14)	257(6)	0	0	-59(13-14)
	66	-368(13-12)	-103(13-14)	-206(6)	0	0	-65(13-14)
8019	30	-369(13-12)	-103(13-14)	204(6)	0	0	58(13-14)
	72	-168(13-13)	-100(13-14)	-200(6)	0	0	-56(13-14)
8019	78	-167(13-13)	-100(13-14)	199(6)	0	0	63(13-14)
	84	-91(13-13)	-47(13-12)	-198(6)	0	0	-20(13-12)
8020	84	-91(13-13)	-47(13-12)	197(6)	0	0	36(13-12)
	25	-349(13-11)	54(13-14)	-234(6)	0	0	40(13-14)
8020	61	-350(13-11)	54(13-14)	236(6)	0	0	-41(13-14)
	31	-337(12-14)	-71(13-14)	-174(6)	0	0	40(13-14)
8020	73	-338(12-14)	-71(13-14)	173(6)	0	0	-41(13-14)
	37	-434(12-11)	35(13-13)	-185(6)	0	0	25(13-13)
8020	43	-434(12-11)	35(13-13)	181(6)	0	0	-15(13-12)
	43	-454(12-14)	91(13-14)	-180(6)	0	0	54(13-14)
8020	49	-453(12-14)	91(13-14)	177(6)	0	0	-49(13-14)
	49	-336(12-11)	79(13-14)	-176(6)	0	0	44(13-14)
8020	25	-336(12-11)	79(13-14)	174(6)	0	0	-45(13-14)
	55	-342(12-14)	-30(13-12)	-174(6)	0	0	17(13-12)
8020	67	-342(12-14)	-30(13-12)	173(6)	0	0	-17(13-12)
	61	-743(13-12)	61(13-14)	-234(6)	0	0	-45(13-14)
8020	55	-743(13-12)	61(13-14)	235(6)	0	0	-47(13-14)
	67	-456(12-14)	-94(13-14)	-178(6)	0	0	-55(13-14)
8020	31	-455(12-14)	-94(13-14)	176(6)	0	0	51(13-14)
	73	-428(13-13)	-86(13-14)	-172(6)	0	0	-46(13-14)
8020	79	-428(13-13)	-86(13-14)	171(6)	0	0	51(13-14)

		21	-3170(13-12)	-475(13-11)	2725(12-13)	0	3422(6)	24(13-14)
14		9	-2231(12-13)	-463(7)	2832(12-13)	0	-3886(12-11-3)	123(13-14)
		20	-2071(12-13)	-438(13-14)	2832(12-13)	0	3983(6)	91(12-11)
15		8	-2249(6)	515(13-14)	2591(6)	0	-3729(12-11-3)	1354(13-14)
		19	-2041(6)	515(13-14)	2519(12-11-3)	0	3999(6)	-17(6)
16		7	-2314(6)	544(13-13)	2738(6)	0	-3904(12-11-3)	1419(13-13)
		18	-2107(6)	544(13-13)	2570(12-11-3)	0	4169(6)	-32(6)
17		6	-2920(13-11)	-599(13-11-3)	3091(6)	0	-4203(12-11-4)	1537(13-13)
		17	-2761(13-11)	-599(13-11-3)	2842(12-11-4)	0	4590(6)	52(13-11-3)
18		5	-2870(6)	-608(13-11-3)	3166(6)	0	-4067(12-11-3)	-1586(13-11-3)
		16	-2663(6)	-608(13-11-3)	2696(6)	0	474(16)	27(13-14)
19		4	-2613(6)	-602(13-11-3)	2978(6)	0	-4073(12-11-1)	-1581(13-11-3)
		15	-2406(6)	-602(13-11-3)	2622(12-11-4)	0	4477(6)	16(6)
20		3	-2296(6)	-597(13-11-3)	2733(6)	0	-4017(12-11-1)	-1570(13-11-3)
		14	-2089(6)	-597(13-11-3)	2553(12-11-1)	0	4117(6)	13(13-14)
21		1	-3686(13-11-2)	-585(13-11-4)	2431(13-11-1)	0	-3415(12-11-1)	-1531(13-11-4)
		12	-3526(13-11-2)	-585(13-11-4)	2431(13-11-1)	0	3826(6)	-29(12-11-1)
22		11	-3224(13-12)	-580(13-11-3)	2900(6)	0	-4033(12-11-3)	-1475(13-11-3)
		22	-3065(13-12)	-580(13-11-3)	2578(12-11-3)	0	4381(6)	62(13-11-4)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Aste generiche

Scenario di calcolo : Set NF_SLV_A2_STR/GEO									
Asta	N.in.	N	Ty	Tz	Mt	My	Mz		
	N fin.	kg	kg	kg	kg*m	kg*m	kg*m		
7001	1	3337(13-1-2)	0	-2(1)	0	0	0		
	25	3342(13-1-2)	0	2(1)	0	0	0		
7002	25	-4869(13-1-2)	0	-2(1)	0	0	0		
	12	-4864(13-1-2)	0	2(1)	0	0	0		
7003	12	-1531(13-1-4)	0	-3(1)	0	0	0		
	11	-1527(13-1-4)	0	3(1)	0	0	0		
7004	11	1565(13-1-1)	0	-3(1)	0	0	0		
	35	1569(13-1-1)	0	3(1)	0	0	0		
7005	35	913(13-1-4)	0	-3(1)	0	0	0		
	43	916(13-1-4)	0	3(1)	0	0	0		
7006	43	-2068(13-1-4)	0	-2(1)	0	0	0		
	39	-2066(13-1-4)	0	2(1)	0	0	0		
7007	39	-791(13-1-4)	0	-2(1)	0	0	0		
	13	-792(13-1-4)	0	2(1)	0	0	0		
7008	13	-2958(13-1-4)	0	0	0	0	0		
	1	-2962(13-1-4)	0	0	0	0	0		
7009	2	2869(13-1-4)	0	0	0	0	0		
	12	2873(13-1-4)	0	0	0	0	0		
7010	12	-995(12-1-1)	0	-2(1)	0	0	0		
	45	-994(12-1-1)	0	2(1)	0	0	0		
7011	45	2044(13-1-4)	0	-2(1)	0	0	0		
	37	2043(13-1-4)	0	2(1)	0	0	0		
7012	37	-694(13-1-4)	0	-3(1)	0	0	0		
	41	-697(13-1-4)	0	3(1)	0	0	0		
7013	41	-1510(13-1-1)	0	-3(1)	0	0	0		
	8	-1514(13-1-1)	0	3(1)	0	0	0		
7014	8	1461(13-1-4)	0	-3(1)	0	0	0		
	13	1457(13-1-4)	0	3(1)	0	0	0		
7015	13	5042(13-1-2)	0	-2(1)	0	0	0		
	28	5037(13-1-2)	0	2(1)	0	0	0		
7016	28	-3427(13-1-2)	0	-2(1)	0	0	0		
	2	-3431(13-1-2)	0	2(1)	0	0	0		
7017	10	-2822(13-1-2)	0	-2(1)	0	0	0		
	33	-2817(13-1-2)	0	2(1)	0	0	0		
7018	33	3961(13-1-2)	0	-2(1)	0	0	0		
	21	3966(13-1-2)	0	2(1)	0	0	0		
7019	21	1308(12-1-1)	0	-3(1)	0	0	0		
	32	1313(12-1-1)	0	3(1)	0	0	0		
7020	32	-1702(13-1-1)	0	-3(1)	0	0	0		
	77	-1698(13-1-1)	0	3(1)	0	0	0		
7021	77	-793(12-1-1)	0	-3(1)	0	0	0		
	85	-790(12-1-1)	0	3(1)	0	0	0		

7022	85	2035(13-1-4)	0	-2(1)	0	0	0
	81	2036(13-1-4)	0	2(1)	0	0	0
7023	81	-775(13-1-4)	0	-2(1)	0	0	0
	21	-775(13-1-4)	0	2(1)	0	0	0
7024	21	-2337(13-1-1)	0	0	0	0	0
	9	-2341(13-1-1)	0	0	0	0	0
7025	10	-2478(13-1-1)	0	0	0	0	0
	20	-2474(13-1-1)	0	0	0	0	0
7026	20	-722(12-1-1)	0	-2(1)	0	0	0
	87	-722(12-1-1)	0	2(1)	0	0	0
7027	87	-1610(13-1-1)	0	-2(1)	0	0	0
	79	-1612(13-1-1)	0	2(1)	0	0	0
7028	79	905(12-1-1)	0	-3(1)	0	0	0
	83	903(12-1-1)	0	3(1)	0	0	0
7029	83	1746(13-1-1)	0	-3(1)	0	0	0
	29	1742(13-1-1)	0	3(1)	0	0	0
7030	29	-1407(12-1-1)	0	-3(1)	0	0	0
	22	-1412(12-1-1)	0	3(1)	0	0	0
7031	22	-3977(13-1-2)	0	-2(1)	0	0	0
	32	-3982(13-1-2)	0	2(1)	0	0	0
7032	32	2786(13-1-1)	0	-2(1)	0	0	0
	11	2781(13-1-1)	0	2(1)	0	0	0
7033	7	-3303(13-1-2)	0	-2(1)	0	0	0
	30	-3299(13-1-2)	0	2(1)	0	0	0
7034	30	-5037(13-1-2)	0	-2(1)	0	0	0
	18	-5031(13-1-2)	0	2(1)	0	0	0
7035	18	-1723(13-1-4)	0	-3(1)	0	0	0
	17	-1719(13-1-4)	0	3(1)	0	0	0
7036	17	1974(13-1-1)	0	-3(1)	0	0	0
	65	1977(13-1-1)	0	3(1)	0	0	0
7037	65	-445(13-1-4)	0	-3(1)	0	0	0
	55	-442(13-1-4)	0	3(1)	0	0	0
7038	55	2256(13-1-4)	0	-2(1)	0	0	0
	69	2258(13-1-4)	0	2(1)	0	0	0
7039	69	-548(13-1-2)	0	-2(1)	0	0	0
	17	-549(13-1-2)	0	2(1)	0	0	0
7040	17	2850(13-1-3)	0	0	0	0	0
	11	-2854(13-1-3)	0	0	0	0	0
7041	22	-848(12-1-3)	0	-2(1)	0	0	0
	57	-847(12-1-3)	0	2(1)	0	0	0
7042	57	-2321(13-1-4)	0	-2(1)	0	0	0
	67	-2323(13-1-4)	0	2(1)	0	0	0
7043	67	447(13-1-4)	0	-3(1)	0	0	0
	53	444(13-1-4)	0	3(1)	0	0	0
7044	53	-2021(13-1-1)	0	-3(1)	0	0	0
	23	-2025(13-1-1)	0	3(1)	0	0	0
7045	23	-1535(13-1-4)	0	-3(1)	0	0	0
	17	-1540(13-1-4)	0	3(1)	0	0	0
7046	17	-5152(13-1-2)	0	-2(1)	0	0	0
	24	-5158(13-1-2)	0	2(1)	0	0	0
7047	24	-3293(13-1-2)	0	-2(1)	0	0	0
	6	-3297(13-1-2)	0	2(1)	0	0	0
7048	13	-2043(13-1-1)	0	-3(1)	0	0	0
	14	-2039(13-1-1)	0	3(1)	0	0	0
7049	14	2124(13-1-1)	0	-3(1)	0	0	0
	15	2119(13-1-1)	0	3(1)	0	0	0
7050	15	-2235(13-1-1)	0	-3(1)	0	0	0
	20	-2231(13-1-1)	0	3(1)	0	0	0
7051	20	-2376(13-1-1)	0	-3(1)	0	0	0
	17	-2380(13-1-1)	0	3(1)	0	0	0
7052	18	2303(13-1-1)	0	-3(1)	0	0	0
	5	2307(13-1-1)	0	3(1)	0	0	0
7053	5	-2336(13-1-1)	0	-3(1)	0	0	0
	20	-2340(13-1-1)	0	3(1)	0	0	0
7054	20	1947(13-1-1)	0	-3(1)	0	0	0
	29	1952(13-1-1)	0	3(1)	0	0	0
7055	21	-2175(13-1-1)	0	-3(1)	0	0	0

Sez. R:	$B_y=60.0\text{ cm}$	$B_z=100.0\text{ cm}$	$L=149.9\text{ cm}$	$L_n=149.9\text{ cm}$	Terreno: Terreno I
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Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	M ₁	M ₂	ΔM ₁	ΔM ₂	ΔM ₃	Af ₁	Af ₂	Af ₃	Mr ⁺	C ⁻	C ⁺	CS
ILN	6936	3912	--	--	--	12.06	12.06	12.06	42365	(12+13)-VII-2	(12+13)-VII-3	6.11
15.0	6764	3269	172	643	12.06	12.06	12.06	42365	42365	(12+13)-VII-2	(12+13)-VII-3	6.11
CAMP	6564	2673	392	1239	12.06	12.06	12.06	42365	42365	(12+13)-VII-2	(12+13)-VII-3	6.11
134.9	6091	2163	525	876	12.06	12.06	12.06	42365	42365	(12+13)-VI-1	(12+13)-VI-4	6.40
661.1	3039	--	--	--	--	12.06	12.06	12.06	42365	(12+13)-VI-1	(12+13)-VI-4	6.40

Verifica a taglio: $\cot(\theta) = 2.500$

$$\text{Comb} = (12+13)\text{-VI-2}$$

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
Sin	12006	--	125983	81507	81507	0	42365	149.6	9.65	6.79
Des							42365			

Trave di Fond.: 9005 [7, 8] Pilastrate [7, 8]

Sez. R: $B_y=60.0\text{ cm}$ $B_z=100.0\text{ cm}$ $L=149.4\text{ cm}$ $L_n=149.4\text{ cm}$ **Terreno: Terrenol**

Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	M- cm	M- kg*m	M+ kg*m	ΔM- kg*m	ΔM+ kg*m	AfS cmq	AfI cmq	Mr- kg*m	Mr+ kg*m	C- (12+13)VII-2	C+ (12+13)VII-3	CS (12+13)VII-3
ILN	11.896	63.29	--	--	--	12.06	12.06	42365	42365	(12+13)VII-2	(12+13)VII-3	3.56
ILN	14.9	11427	5396	469	933	12.06	12.06	42365	42365	(12+13)VII-2	(12+13)VII-3	3.56
CAMP	10900	4509	996	1821	12.06	12.06	12.06	42365	42365	(12+13)VII-2	(12+13)VII-3	3.56
FLN	134.4	7877	1149	1154	877	12.06	12.06	42365	42365	(12+13)V-1	(12+13)V-4	4.95
FLN	6802	7402	1333	1333	12.06	12.06	12.06	42365	42365	(12+13)V-1	(12+13)V-4	5.16

Verifica a taglio: $\cot(\theta) = 2.500$

$$\text{Comb} = (12+13)\text{-II-3}$$

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Statfe	CS
	kg	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	6972	--	125983	87692	87692	0	42365	149.9	10.39	12.6
Des							42365			

Trave di Fond.: 9005 | 5, 6 | Pilastrate | 5, 6 |

Sez. R: $B_y=60.0$ cm $B_z=100.0$ cm $L=149.3$ cm $L_n=149.3$ cm

Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	M-	M+	ΔM^-	ΔM^+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg ⁺ m	kg ⁺ m	kg ⁺ m	kg ⁺ m	cmq	cmq	kg ⁺ m	kg ⁺ m			
LN	5581	2081	2448	1187	12.06	12.06	42365	42365	(12+13)-V1-	(12+13)-V1+	5.28
14.9	6455	2436	2458	1358	12.06	12.06	42365	42365	(12+13)-V1-	(12+13)-V1+	4.80
CAMP	11805	6596	1304	1763	12.06	12.06	42365	42365	(12+13)-V1-	(12+13)-V1+	3.23
134.4	12468	7443	641	916	12.06	12.06	42365	42365	(12+13)-V1-	(12+13)-V1+	3.23
LN	13109	8359	--	--	12.06	12.06	42365	42365	(12+13)-V1-	(12+13)-V1+	3.23

X	X_0	d_0	X_0/d_0
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	cm	cm
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[illegible]

Verifica a taglio: $\cot(\theta) = 2.500$

$$\text{Comb} = (12+13)\text{-II-2}$$

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	7248	--	125983	88185	88185	0	42365	149.3	10.44	12.2
Des							42365			

Trave di Fond.: 9005 [6, 7] Pilastrate [6, 7]

Sez. R: By=60.0 cm Bz=100.0 cm L=149.6 cm Ln=149.6 cm

Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	m	M	ΔM	ΔM^+	Afs	Afi	Mr ⁺	C ⁻	C ⁺	CS
LN	12143	7400	--	--	12.06	12.06	42365	(12+13)-V1-	(12+13)-V1+	3.49
15.0	11255	6087	889	1393	12.06	12.06	42365	(12+13)-V1-	(12+13)-V1+	3.49
CAMP	10342	4603	1801	2717	12.06	12.06	42365	(12+13)-V1-	(12+13)-V1+	3.49
134.6	10225	4344	768	1133	12.06	12.06	42365	(12+13)-V1-	(12+13)-V1-	3.85
FLN	10954	5478	--	--	12.06	12.06	42365	(12+13)-V1-2	(12+13)-V1-2	3.85

X	X^-	d^-	$X^-/$
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cm	cm
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ILN	19.4	95.9	0.202	193	95.9	0.201	42365	(12+13)-VI-1	(12+13)-VI-4	Parz.	Parz.
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Trave di Fond.: 9005 [8, 9 | Pilastrate [8, 9]

Sez. R: $B_y = 60.0\text{ cm}$ $B_z = 100.0\text{ cm}$ $L = 149.2\text{ cm}$ $L_n = 149.2\text{ cm}$ **Terreno: Terrenol**

Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	M- cm	M+ kg m ³	ΔM- kg m ³	ΔM+ kg m ³	ΔF ₁ cmq	ΔF ₂ cmq	Mr- kg m ³	Mr+ kg m ³	C- (12+13)-V1-	C+ (12+13)-V1+	CS
ILN	6697	1082	2038	1479	12.06	12.06	42365	42365	(12+13)-V1-	(12+13)-V1+	4.85
14.9	7463	1551	1859	1609	12.06	12.06	42365	42365	(12+13)-V1-	(12+13)-V1+	4.54
CAMP	2128	7114	1250	2456	12.06	12.06	42365	42365	(12+13)-H-2	(12+13)-H-2	3.17
134.3	12784	8320	594	1250	12.06	12.06	42365	42365	(12+13)-H-3	(12+13)-H-3	3.17
ILN	13377	9571	--	--	12.06	12.06	42365	42365	(12+13)-H-2	(12+13)-H-2	3.17

X	X^*	d^*	X/X^*
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cm	cm
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CAMP	194	95.9	0.202	19.3	95.9	0.202	42.365	(12+13)-II-3	(12+13)-II-2	Parz.
134.3	194	95.9	0.202	19.3	95.9	0.202	42.365	(12+13)-II-3	(12+13)-II-2	Parz.
FLN	194	95.9	0.202	19.3	95.9	0.202	42.365	(12+13)-III-3	(12+13)-III-2	Parz.
ILN	193	95.9	0.201	19.2	95.9	0.201	42.365	(12+13)-VI-1	(12+13)-VI-4	Parz.
14.9	193	95.9	0.202	19.2	95.9	0.202	42.365	(12+13)-VI-1	(12+13)-VI-4	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

$$\text{Comb} = (12+13)\text{-VI-2}$$

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Statfe	CS
	kg	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	8629	--	125983	81732	81732	0	42365	149.2	9.68	9.47
Des							42365			

Trave di Fond. : 9005	9, 10	Pilastrate	9, 10
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Sez. R: B_y= 60.0 cm B_z=100.0 cm L=149.5 cm Ln=149.5 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	cmq	kg*m	kg*m			
ILN	12245	8278	2715	2682	12.06	12.06	42365	42365	(12+13)>VI-3	(12+13)>VI-2	2.83
ILN	13249	9170	2521	2789	12.06	12.06	42365	42365	(12+13)>VI-3	(12+13)>VI-2	2.69
CAMP	18317	16316	715	2188	12.06	12.06	42365	42365	(12+13)>VI-3	(12+13)>VI-2	2.23
134.5	18722	17409	310	1094	12.06	12.06	42365	42365	(12+13)>VI-3	(12+13)>VI-2	2.23
FLN	19032	18504	--	--	12.06	12.06	42365	42365	(12+13)>VI-3	(12+13)>VI-2	2.23

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.4	95.9	0.201	19.4	95.9	0.202	42365	42365	(12+13)>VI-3	(12+13)>VI-2	Parz.	Parz.
ILN	14.9	19.4	95.9	0.202	19.4	95.9	0.202	42365	(12+13)>VI-3	(12+13)>VI-2	Parz.	Parz.
CAMP	19.5	95.9	0.203	19.5	95.9	0.203	42365	42365	(12+13)>VI-3	(12+13)>VI-2	Parz.	Parz.
134.5	19.5	95.9	0.203	19.5	95.9	0.203	42365	42365	(12+13)>VI-3	(12+13)>VI-2	Parz.	Parz.
FLN	19.5	95.9	0.203	19.5	95.9	0.203	42365	42365	(12+13)>VI-3	(12+13)>VI-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)>V-2

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin	8216	--	125983	81551	81551	0	42365	149.5	9.66	9.93
Des							42365			

Trave di Fond.: 9005 [10 , 11] Pilastrate [10 , 11]

Sez. R: B_y= 60.0 cm B_z=100.0 cm L=150.0 cm Ln=150.0 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	cmq	kg*m	kg*m			
ILN	18017	17283	--	--	12.06	12.06	42365	42365	(12+13)>VI-3	(12+13)>VI-2	2.35
ILN	16872	15884	1145	1398	12.06	12.06	42365	42365	(12+13)>VI-3	(12+13)>VI-2	2.35
CAMP	15620	14468	2998	2814	12.06	12.06	42365	42365	(12+13)>VI-3	(12+13)>VI-2	2.35
135.0	3234	3093	5930	5106	12.06	12.06	42365	42365	(12+13)>VI-3	(12+13)>VI-2	4.62
FLN	847	1107	6401	5406	12.06	12.06	42365	42365	(12+13)>VI-3	(12+13)>VI-2	5.85

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.5	95.9	0.203	19.4	95.9	0.203	42365	42365	(12+13)>VI-3	(12+13)>VI-2	Parz.	Parz.
ILN	15.0	19.5	95.9	0.203	19.4	95.9	0.203	42365	(12+13)>VI-3	(12+13)>VI-2	Parz.	Parz.
CAMP	19.5	95.9	0.203	19.4	95.9	0.203	42365	42365	(12+13)>VI-3	(12+13)>VI-2	Parz.	Parz.
135.0	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)>VI-3	(12+13)>VI-2	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>VI-3	(12+13)>VI-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)>VI-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin	16517	--	125983	87991	87991	0	42365	150.0	10.42	5.33
Des							42365			

Trave di Fond.: 9006 [1 , 2] Pilastrate [21 , 12]

Sez. R: B_y= 60.0 cm B_z=100.0 cm L=89.7 cm Ln=101.7 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	cmq	kg*m	kg*m			
ILN	770	990	2460	2002	12.06	12.06	42365	42365	(12+13)>II-2	(12+13)>II-3	13.1
ILN	10.2	1447	1498	2221	1915	12.06	42365	42365	(12+13)>II-2	(12+13)>II-3	11.6
CAMP	4631	4496	494	724	12.06	12.06	42365	42365	(12+13)>II-2	(12+13)>II-3	8.12
91.6	4897	4863	228	357	12.06	12.06	42365	42365	(12+13)>II-2	(12+13)>II-3	8.12
FLN	5125	5220	--	--	12.06	12.06	42365	42365	(12+13)>II-2	(12+13)>II-3	8.12

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				

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X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
ILN	19.2	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)>II-2	(12+13)>II-3	Parz.	Parz.
Parz.	10.2	19.3	95.9	0.201	19.2	95.9	0.201	42365	(12+13)>II-2	(12+13)>II-3	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>II-2	(12+13)>II-3	Parz.	Parz.
91.6	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>II-2	(12+13)>II-3	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>II-2	(12+13)>II-3	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)>IV-2

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin	6972	--	125983	91208	91208	0	42365	101.7	10.80	13.1
Des							42365			

Trave di Fond.: 9006 [2 , 3] Pilastrate [12 , 20]

Sez. R: B_y= 60.0 cm B_z=100.0 cm L=89.2 cm Ln=89.2 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	cmq	kg*m	kg*m			
ILN	6695	6772	--	--	12.06	12.06	42365	42365	(12+13)>II-2	(12+13)>II-3	6.26
ILN	8.9	6543	6581	152	191	12.06	42365	42365	(12+13)>II-2	(12+13)>II-3	6.26
CAMP	5931	5973	764	799	12.06	12.06	42365	42365	(12+13)>II-2	(12+13)>II-3	6.26
80.3	4465	4888	1426	1052	12.06	12.06	42365	42365	(12+13)>II-2	(12+13)>II-3	7.13
FLN	4115	4666	1521	1062	12.06	12.06	42365	42365	(12+13)>II-2	(12+13)>II-3	7.40

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>II-2	(12+13)>II-3	Parz.	Parz.
ILN	8.9	19.3	95.9	0.201	19.3	95.9	0.201	42365	(12+13)>II-2	(12+13)>II-3	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>II-2	(12+13)>II-3	Parz.	Parz.
80.3	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>II-2	(12+13)>II-3	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>II-2	(12+13)>II-3	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)>VIII-4

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin	4767	--	125983	78848	78848	0	42365	89.2	9.34	16.5
Des							42365			

Trave di Fond.: 9006 [3 , 4] Pilastrate [20 , 19]

Sez. R: B_y= 60.0 cm B_z=100.0 cm L=89.5 cm Ln=89.5 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	cmq	kg*m	kg*m			
ILN	5986	6505	--	82	12.06	12.06	42365	42365	(12+13)>I-2	(12+13)>I-3	6.43
9.0	6045	6528	--	67	12.06	12.06	42365	42365	(12+13)>I-2	(12+13)>I-3	6.42
CAMP	6104	6579	--	26	12.06	12.06	42365	42365	(12+13)>I-2	(12+13)>I-3	6.41
80.6	5834	6605	266	--	12.06	12.06	42365	42365	(12+13)>I-2	(12+13)>I-3	6.41
FLN	5728	6603	351	--	12.06	12.06	42365	42365	(12+13)>I-2	(12+13)>I-3	6.42

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>I-2	(12+13)>I-3	Parz.	Parz.
ILN	9.0	19.3	95.9	0.201	19.3	95.9	0.201	42365	(12+13)>I-2	(12+13)>I-3	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>I-2	(12+13)>I-3	Parz.	Parz.
80.6	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>I-2	(12+13)>I-3	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>I-2	(12+13)>I-3	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)>VIII-4

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin	4692	--	125983	78420	78420	0	42365	89.5	9.29	16.7
Des							42365			

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Sez	Des	Td	VRdns	VRcd	VRsd	VRd	Trl	Mr	Dx	Stafie	CS
								42365			

Trave di Fond. : 9006 [8 , 9] Pilastrate [15 , 14]

Sez. R: By= 60,0 cm Bz= 100,0 cm L= 89,6 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alf	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3904	6657	1410	--	12,06	12,06	42365	42365	(12+13)÷IV-3	(12+13)÷IV-4
9,0	4256	6561	1362	96	12,06	12,06	42365	42365	(12+13)÷VIII-3	(12+13)÷IV-4
CAMP	6010	6440	253	228	12,06	12,06	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2
80,6	6150	6556	113	112	12,06	12,06	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2
FLN	6263	6668	--	--	12,06	12,06	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato-
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19,3	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷IV-3	(12+13)÷IV-4	Parz.	Parz.
9,0	19,3	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷VIII-3	(12+13)÷IV-4	Parz.	Parz.
CAMP	19,3	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2	Parz.	Parz.
80,6	19,3	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2	Parz.	Parz.
FLN	19,3	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)÷I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Trl	Mr	Dx	Stafie	CS
		kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6345	--	125983	78359	78359	0	42365	89,6	9,28	12,3
Des							42365			

Trave di Fond. : 9006 [9 , 10] Pilastrate [14 , 13]

Sez. R: By= 60,0 cm Bz= 100,0 cm L= 89,2 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alf	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4890	5302	--	--	12,06	12,06	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2
10,1	4668	4904	222	398	12,06	12,06	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2
CAMP	3764	3661	1126	1642	12,06	12,06	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2
91,1	1340	1399	2139	1944	12,06	12,06	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2
FLN	700	915	2357	1989	12,06	12,06	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato-
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19,3	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2	Parz.	Parz.
10,1	19,3	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2	Parz.	Parz.
CAMP	19,3	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2	Parz.	Parz.
91,1	19,2	95,9	0,201	19,2	95,9	0,201	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2	Parz.	Parz.
FLN	19,2	95,9	0,201	19,2	95,9	0,201	42365	42365	(12+13)÷VIII-3	(12+13)÷VIII-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)÷II-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Trl	Mr	Dx	Stafie	CS
		kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6621	--	125983	7882,5	7882,5	0	42365	101,2	9,34	11,9
Des							42365			

Verifica Stabilità aste Metalliche

Scenario di calcolo : **Set NT_SIV_A2_STR/GEO**

Asta : **1 [1 , 28]**

Sez. G: HE 240 A L=211,0 cm Ln1=211,0 cm Ln2=211,0 cm Crit.: Acciaio_Pressflessione γM=1,05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq.**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	γY	γZ	kyy	kzy	kzz
	kg	kg	kg	kg	kg							
-8317	4701	-305	211298	20492	9673	21	35	0,985	0,895	--	0,664	0,464
											0,398	0,774

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Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	8317	3120	198247	19516	9213	9213	(12+13)÷III-2	4,60
1	Z	8317	1872	236	180054	19516	9213	(12+13)÷III-2	5,96

Asta : **1 [28 , 12]**

Sez. G: HE 240 A L=271,0 cm Ln1=271,0 cm Ln2=271,0 cm Crit.: Acciaio_Pressflessione γM=1,05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq.**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	γY	γZ	kyy	kzy	kzz
	kg	kg	kg	kg	kg							
-8074	-4078	-198	211298	20492	9673	27	45	0,960	0,832	--	0,621	0,392
											0,373	0,653

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg	kg	kg	kg	kg		
1	Y	8074	2533	78	193231	19516	9213	(12+13)÷VIII-2	5,56
1	Z	8074	1520	129	167375	19516	9213	(12+13)÷VIII-2	7,14

Asta : **2 [2 , 25]**

Sez. G: HE 240 A L=211,0 cm Ln1=211,0 cm Ln2=211,0 cm Crit.: Acciaio_Pressflessione γM=1,05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq.**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	γY	γZ	kyy	kzy	kzz
	kg	kg	kg	kg	kg							
-13100	2486	1042	211298	20492	9673	21	35	0,985	0,895	--	0,656	0,419
											0,394	0,698

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg	kg	kg	kg	kg		
1	Y	13100	1631	437	198247	19516	9213	(12+13)÷II-1	5,07
1	Z	13100	978	728	180054	19516	9213	(12+13)÷II-1	4,95

Asta : **2 [25 , 13]**

Sez. G: HE 240 A L=271,0 cm Ln1=271,0 cm Ln2=271,0 cm Crit.: Acciaio_Pressflessione γM=1,05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq.**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	γY	γZ	kyy	kzy	kzz
	kg	kg	kg	kg	kg							
-7624	-4839	-151	211298	20492	9673	27	45	0,960	0,832	--	0,615	0,607
											0,369	1,011

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg	kg	kg	kg	kg		
1	Y	7624	2977	91	193231	19516	9213	3	4,95
1	Z	7624	1786	152	167375	19516	9213	3	6,51

Asta : **3 [3 , 27]**

Sez. G: HE 240 A L=211,0 cm Ln1=211,0 cm Ln2=211,0 cm Crit.: Acciaio_Pressflessione γM=1,05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq.**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	γY	γZ	kyy	kzy	kzz
	kg	kg	kg	kg	kg							
-2536	3594	-547	211298	20492	9673	21	35	0,985	0,895	--	0,690	0,423
											0,414	0,705

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg	kg	kg	kg	kg		
1	Y	2536	2480	231	198247	19516	9213	(12+13)÷III-2	6,06
1	Z	2536	1488	386	180054	19516	9213	(12+13)÷III-2	7,56

Asta : **3 [27 , 14]**

Sez. G: HE 240 A L=271,0 cm Ln1=271,0 cm Ln2=271,0 cm Crit.: Acciaio_Pressflessione γM=1,05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq.**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	γY	γZ	kyy	kzy	kzz
	kg	kg	kg	kg	kg							
-7148	-5079	-125	211298	20492	9673	27	45	0,960	0,832	--	0,610	0,598
											0,366	0,996

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg	kg	kg	kg	kg		
1	Y	7148	3099	75	193231	19516	9213	3	4,90

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Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Z	7148		1859	125	167375	19516	9213	3	6.60

Asta : 4 [4 , 23]

Sez. G: HE 240 A L=211.0 cm Ln1=211.0 cm Ln2=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2681	3584	-662	211298	20492	9673	21	35	0.985	0.895	--	0.685	0.418	0.411	0.697

Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Y	2681	2457	277	198247	19516	9213	(12+13)÷III-2	5.90	
1	Z	2681	1474	461	180054	19516	9213	(12+13)÷III-2	7.12	

Asta : 4 [23 , 15]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-7768	-5365	-115	211298	20492	9673	27	45	0.960	0.832	--	0.608	0.592	0.365	0.987

Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Y	7768	3264	68	193231	19516	9213	3	4.65	
1	Z	7768	1959	113	167375	19516	9213	3	6.29	

Asta : 5 [5 , 29]

Sez. G: HE 240 A L=211.0 cm Ln1=211.0 cm Ln2=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-3162	3750	-701	211298	20492	9673	21	35	0.985	0.895	--	0.672	0.425	0.403	0.708

Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Y	3162	2520	298	198247	19516	9213	(12+13)÷VII-2	5.64	
1	Z	3162	1512	496	180054	19516	9213	(12+13)÷VII-2	6.72	

Asta : 5 [29 , 16]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-7988	-5580	-110	211298	20492	9673	27	45	0.960	0.832	--	0.606	0.593	0.364	0.988

Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Y	7988	3383	65	193231	19516	9213	3	4.51	
1	Z	7988	2030	108	167375	19516	9213	3	6.12	

Asta : 6 [6 , 30]

Sez. G: HE 240 A L=211.0 cm Ln1=211.0 cm Ln2=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-11180	3882	-708	211298	20492	9673	21	35	0.985	0.895	--	0.670	0.428	0.402	0.714

Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Y	11180	2600	303	198247	19516	9213	(12+13)÷VII-2	4.49	
1	Z	11180	1560	505	180054	19516	9213	(12+13)÷VII-2	5.08	

Asta : 6 [30 , 17]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-6697	-5489	-114	211298	20492	9673	27	45	0.960	0.832	--	0.608	0.590	0.365	0.983

Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Y	6697	3337	67	193231	19516	9213	3	4.70	
1	Z	6697	2002	112	167375	19516	9213	3	6.46	

Asta : 7 [7 , 24]

Sez. G: HE 240 A L=211.0 cm Ln1=211.0 cm Ln2=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-13147	3344	903	211298	20492	9673	21	35	0.985	0.895	--	0.673	0.404	0.404	0.673

Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Y	13147	2252	365	198247	19516	9213	(12+13)÷V1-1	4.52	
1	Z	13147	1351	608	180054	19516	9213	(12+13)÷V1-1	4.80	

Asta : 7 [24 , 18]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-8011	-5137	-104	211298	20492	9673	27	45	0.960	0.832	--	0.608	0.591	0.365	0.985

Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Y	8011	3121	62	193231	19516	9213	3	4.81	
1	Z	8011	1872	103	167375	19516	9213	3	6.45	

Asta : 8 [8 , 26]

Sez. G: HE 240 A L=211.0 cm Ln1=211.0 cm Ln2=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2471	3977	-372	211298	20492	9673	21	35	0.985	0.895	--	0.695	0.376	0.417	0.627

Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Y	2471	2763	140	198247	19516	9213	(12+13)÷V-1	5.91	
1	Z	2471	1658	233	180054	19516	9213	(12+13)÷V-1	8.07	

Asta : 8 [26 , 19]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-7268	-5038	-72	211298	20492	9673	27	45	0.960	0.832	--	0.609	0.559	0.366	0.932

Cls	Dir	N	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
1	Y	7268	3071	40	193231	19516	9213	3	5.02	
1	Z	7268	1842	67	167375	19516	9213	3	6.89	

Asta : 9 [9 , 31]

Sez. G: HE 240 A L=211.0 cm Ln1=211.0 cm Ln2=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2526	3852	-482	211298	20492	9673	21	35	0.985	0.895	--	0.692	0.369	0.415	0.616

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	2526	2666	178	198247	19516	9213	(12+13)-V-1	5.93
1	Z	2526	1599	297	180054	19516	9213	(12+13)-V-1	7.80

Asta : 9 [31 , 20]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
-7162	-4974	-84	211298	20492	9673	27	45	0.960	0.832	--	0.610	0.560	0.366
													0.933

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	7162	3036	47	193231	19516	9213	3	5.06
1	Z	7162	1821	78	167375	19516	9213	3	6.92

Asta : 10 [10 , 32]

Sez. G: HE 240 A L=211.0 cm Ln1=211.0 cm Ln2=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
-12564	2588	-1047	211298	20492	9673	21	35	0.985	0.895	--	0.676	0.390	0.406
													0.650

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	12564	1750	408	198247	19516	9213	(12+13)-V-2	5.07
1	Z	12564	1050	681	180054	19516	9213	(12+13)-V-2	5.06

Asta : 10 [32 , 21]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
-6606	-4698	80	211298	20492	9673	27	45	0.960	0.832	--	0.613	0.479	0.368
													0.798

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	6606	2881	38	193231	19516	9213	3	5.38
1	Z	6606	1729	64	167375	19516	9213	3	7.41

Asta : 11 [11 , 33]

Sez. G: HE 240 A L=211.0 cm Ln1=211.0 cm Ln2=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
-13940	3636	745	211298	20492	9673	21	35	0.985	0.895	--	0.619	0.436	0.372
													0.726

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	13940	2252	324	198247	19516	9213	(12+13)-IV-3	4.53
1	Z	13940	1351	540	180054	19516	9213	(12+13)-IV-3	4.87

Asta : 11 [33 , 22]

Sez. G: HE 240 A L=271.0 cm Ln1=271.0 cm Ln2=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
-7919	-4156	207	211298	20492	9673	27	45	0.960	0.832	--	0.572	0.335	0.343
													0.558

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	7919	2378	69	193231	19516	9213	(12+13)-IV-3	5.87

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Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Z	7919	1427	116	167375	19516	9213	(12+13)+IV-3	7.52

Asta : 12 [2 , 13]

Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
-2767	2516	1381	211298	20492	9673	26	44	0.963	0.838	--	0.445	0.358	0.267
													0.596

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	2767	1121	494	193741	19516	9213	(12+13)+II-1	7.98
1	Z	2767	672	824	168682	19516	9213	(12+13)+II-1	7.13

Asta : 13 [10 , 21]

Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
-3767	2410	1506	211298	20492	9673	26	44	0.963	0.838	--	0.488	0.360	0.293
													0.600

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	3767	1176	542	193741	19516	9213	(12+13)+IV-3	7.22
1	Z	3767	705	904	168682	19516	9213	(12+13)+IV-3	6.39

Asta : 14 [9 , 20]

Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
-2594	2799	-1202	211298	20492	9673	26	44	0.963	0.838	--	0.454	0.380	0.272
													0.633

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	2594	1271	457	193741	19516	9213	(12+13)+V-2	7.81
1	Z	2594	762	761	168682	19516	9213	(12+13)+V-2	7.30

Asta : 15 [8 , 19]

Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
-1465	1765	1609	211298	20492	9673	26	44	0.963	0.838	--	0.609	0.359	0.366
													0.598

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	1465	1076	577	193741	19516	9213	(12+13)+II-3	7.98
1	Z	1465	645	962	168682	19516	9213	(12+13)+II-3	6.84

Asta : 16 [7 , 18]

Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
-1210	1485	1669	211298	20492	9673	26	44	0.963	0.838	--	0.593	0.357	0.356
													0.595

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	1210	881	596	193741	19516	9213	(12+13)+IV-3	8.62
1	Z	1210	529	993	168682	19516	9213	(12+13)+IV-3	7.04

Asta : 17 [6 , 17]

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Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kyz	kzy	kzz
kg	kg*	kg*	kg	kg*	kg*									
-3306	1316	-1718	211298	20492	9673	26	44	0.963	0.838	--	0.40	0.355	0.240	0.592

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
1	Y	3306	527	610	193741	19516	9213	(12+13)+VIII-2	9.07
1	Z	3306	316	1016	168682	19516	9213	(12+13)+VIII-2	6.84

Asta : 18 [5 , 16]

Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz	
kg	kg*	kg*	kg	kg*	kg*									
-1204	2127	-1775	211298	20492	9673	26	44	0.963	0.838	--	0.400	0.357	0.240	0.595

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
1	Y	1204	851	634	193741	19516	9213	(12+13)+IV-2	8.42
1	Z	1204	511	1057	168682	19516	9213	(12+13)+IV-2	6.75

Asta : 19 [4 , 15]

Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kyz	kzz	
kg	kg*	kg*	kg	kg*	kg*									
-1373	2185	-1755	211298	20492	9673	26	44	0.963	0.838	--	0.400	0.359	0.240	0.599

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
1	Y	1373	875	631	193741	19516	9213	(12+13)+IV-2	8.31
1	Z	1373	525	1051	168682	19516	9213	(12+13)+IV-2	6.71

Asta : 20 [3 , 14]

Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kyz	kzz	
kg	kg*	kg*	kg	kg*	kg*									
-1349	2172	-1722	211298	20492	9673	26	44	0.963	0.838	--	0.425	0.359	0.255	0.598

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
1	Y	1349	923	618	193741	19516	9213	(12+13)+IV-2	8.24
1	Z	1349	554	1031	168682	19516	9213	(12+13)+IV-2	6.75

Asta : 21 [1 , 12]

Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kyz	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-3941	3020	-1642	211298	20492	9673	26	44	0.963	0.838	--	0.401	0.360	0.241	0.599

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
1	Y	3941	1210	590	193741	19516	9213	(12+13)+VIII-2	6.83
1	Z	3941	726	984	168682	19516	9213	(12+13)+VIII-2	5.97

Asta : 22 [11 , 22]

Sez. G: HE 240 A L=265.0 cm Ln1=265.0 cm Ln2=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kyz	kzz	
-3430	897	1684	211298	20492	9673	26	44	0.963	0.838	--	0.552	0.359	0.331	0.598

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
1	Y	3430	495	604	193741	19516	9213	(12+13)+II-3	9.20
1	Z	3430	297	1007	168682	19516	9213	(12+13)+II-3	6.90

Asta : 8000 [12 , 7]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kyz	kzz	
	kg*	kg*m	kg	kg*m	kg*									
-3131	3854	81	211298	20492	9673	17	29	0.950	0.929	--	0.889	0.435	0.533	0.724

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
1	Y	3131	3426	35	191097	19516	9213	(12+13)+III-2	5.11
1	Z	3131	2056	59	186976	19516	9213	(12+13)+III-2	7.78

Asta : 8000 [7 , 8]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2391	2563	155	211298	20492	9673	17	28	0.953	0.933	--	0.892	0.528	0.535	0.879

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
1	Y	2391	2285	82	191685	19516	9213	(12+13)+I-1	7.22
1	Z	2391	1371	136	187783	19516	9213	(12+13)+I-1	10.2

Asta : 8000 [8 , 9]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λ_Y	λ_Z	χ_Y	χ_Z	χ_{LT}	kyy	kyz	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-665	-2142	-112	211298	20492	9673	16	27	0.956	0.938	--	1.000	0.591	0.600	0.985

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
1	Y	665	2143	66	192449	19516	9213	(12+13)+III-4	8.30
1	Z	665	1286	110	188835	19516	9213	(12+13)+III-4	12.3

Asta : 8000 [9 , 35]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyy	kyz	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1293	-2273	-165	211298	20492	9673	15	26	0.962	0.947	--	0.890	0.495	0.534	0.824

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
1	Y	1293	2024	82	193665	19516	9213	3	8.39
1	Z	1293	1214	136	190519	19516	9213	3	11.9

Asta : 8000 [35 , 36]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyy	kyz	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-314	-2284	-103	211298	20492	9673	15	24	0.968	0.955	--	1.000	0.564	0.600	0.940

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	314	2283	58	194807	19516	9213	3	8.01
1	Z	314	1370	97	192110	19516	9213	3	12.1

Asia : 8000 [36 , 37]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione γ M=1.05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq; Verificato									
N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ
kg	kg*m	kg*m	kg	kg*m	kg*m	13	22	0.977	0.967
-128	-2085	-96	211298	20492	9673	13	22	0.977	0.967
								--	--
								0.877	0.399
								0.526	0.665

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	128	1829	38	196582	19516	9213	6	10.1
1	Z	128	1097	64	194601	19516	9213	6	15.7

Asia : 8000 [37 , 38]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione γ M=1.05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq; Verificato									
N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ
kg	kg*m	kg*m	kg	kg*m	kg*m	12	20	0.986	0.980
-1206	1924	33	211298	20492	9673	12	20	0.986	0.980
								--	--
								0.786	0.500
								0.472	0.834

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1206	1513	16	198412	19516	9213	(12+13)-III-4	11.7
1	Z	1206	908	27	197192	19516	9213	(12+13)-III-4	18.0

Asia : 8000 [38 , 39]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione γ M=1.05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq; Verificato									
N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ
kg	kg*m	kg*m	kg	kg*m	kg*m	11	18	0.994	0.991
-1362	2802	36	211298	20492	9673	11	18	0.994	0.991
								--	--
								0.880	0.240
								0.528	0.400

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1362	2467	9	199935	19516	9213	(12+13)-III-4	7.45
1	Z	1362	1480	14	199366	19516	9213	(12+13)-III-4	11.9

Asia : 8000 [39 , 40]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione γ M=1.05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq; Verificato									
N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ
kg	kg*m	kg*m	kg	kg*m	kg*m	10	17	0.998	0.998
-2437	3642	181	211298	20492	9673	10	17	0.998	0.998
								--	--
								0.930	0.331
								0.558	0.552

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2437	3388	60	200891	19516	9213	(12+13)-IV-4	5.20
1	Z	2437	2033	100	200739	19516	9213	(12+13)-IV-4	7.86

Asia : 8000 [40 , 12]

Sez. G: HE 240 A L=110.7 cm Ln1=110.7 cm Ln2=110.7 cm Crit.: Acciaio_Pressflessione γ M=1.05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq; Verificato									
N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ
kg	kg*m	kg*m	kg	kg*m	kg*m	10	17	0.999	0.998
-2600	3698	-56	211298	20492	9673	10	17	0.999	0.998
								--	--
								0.985	0.527
								0.591	0.879

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2600	3644	30	201023	19516	9213	(12+13)-IV-4	4.93
1	Z	2600	2186	50	200929	19516	9213	(12+13)-IV-4	7.67

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Asia : 8000 [13 , 10]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione γ M=1.05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq; Verificato									
N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.945	0.923
-6298	4806	137	211298	20492	9673	18	30	0.945	0.923
								--	--
								0.701	0.585
								0.421	0.975

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6298	3371	80	190238	19516	9213	3	4.66
1	Z	6298	2022	133	185803	19516	9213	3	6.58

Asia : 8000 [10 , 11]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γ M=1.05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq; Verificato									
N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.948	0.927
-1082	2453	193	211298	20492	9673	18	30	0.948	0.927
								--	--
								0.903	0.455
								0.542	0.758

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1082	2215	88	190743	19516	9213	(12+13)-I-I	7.77
1	Z	1082	1329	146	186492	19516	9213	(12+13)-I-I	11.1

Asia : 8000 [11 , 12]

Sez. G: HE 240 A L=169,8 cm Ln1=169,8 cm Ln2=169,8 cm Crit.: Acciaio_Pressflessione γ M=1,05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq:Verificato									
N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ
kg	kg*m	kg*m	kg	kg*m	kg*m				
-3244	-2573	-80	211298	20492	9673	17	28	0,953	0,934
								--	--
								1,002	0,519
								0,601	0,865

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3244	2578	42	191738	19516	9213	(12+13)-II-4	6.51
1	Z	3244	1547	70	187856	19516	9213	(12+13)-II-4	9.61

Asia : 8000 [12 , 41]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione γ M=1.05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq;Verificato									
N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ
kg	kg*m	kg*m	kg	kg*m	kg*m				
-4314	-2324	-166	211298	20492	9673	16	26	0.960	0.943
								--	--
								1.002	0.448
								0.601	0.747

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4314	2328	74	193187	19516	9213	6	6.68
1	Z	4314	1397	124	189856	19516	9213	6	9.28

Asia : 8000 [41 , 42]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione γ M=1.05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq; Verificato									
N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ
kg	kg*m	kg*m	kg	kg*m	kg*m				
-4111	-2304	-119	211298	20492	9673	15	25	0.967	0.953
								--	--
								0.937	0.497
								0.562	0.828

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg	kg	kg*m	kg*m		
1	Y	4111	2158	59	194567	19516	9213	3	7.24
1	Z	4111	1295	98	191775	19516	9213	3	10.2

Asia : 8000 [42 , 43]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione γ M=1.05 fyk/γM=2619									
kg/cmq ft=4300 kg/cmq; Verificato									

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-771	-2169	-471	211298	20492	9673	13	22	0.976	0.965	—	0.848	0.453	0.509	0.755

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	771	1839	213	196339	19516	9213	(12+13)>III-2					8.24
1	Z	771	1104	355	194259	19516	9213	(12+13)>III-2					10.1

Asia : 8001 [43, 44]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2640	2311	193	211298	20492	9673	12	20	0.983	0.976	--	0.766	0.451	0.459	0.752

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2640	1769	87	197915	19516	9213	(12+13)>III-3					8.82
1	Z	2640	1062	145	196487	19516	9213	(12+13)>III-3					12.0

Asia : 8001 [44, 45]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2781	3170	104	211298	20492	9673	11	19	0.990	0.985	--	0.892	0.240	0.535	0.399

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2781	2826	25	199179	19516	9213	(12+13)>I-3					6.19
1	Z	2781	1696	41	198286	19516	9213	(12+13)>I-3					9.49

Asia : 8001 [45, 46]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1611	3198	-20	211298	20492	9673	11	18	0.993	0.990	--	0.976	0.316	0.586	0.527

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1611	3122	6	199875	19516	9213	(12+13)>III-4					5.93
1	Z	1611	1873	10	199281	19516	9213	(12+13)>III-4					9.50

Asia : 8001 [46, 13]

Sez. G: HE 240 A L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-1648	3835	9	211298	20492	9673	11	18	0.992	0.988	--	0.844	0.404	0.506	0.674

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1648	3237	4	199552	19516	9213			6			5.73
1	Z	1648	1942	6	198789	19516	9213			6			9.22

Asia : 8002 [14, 13]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-6537	5059	89	211298	20492	9673	18	30	0.945	0.923	--	0.712	0.590	0.427	0.983

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	6537	3601	52	190236	19516	9213			3			4.45
1	Z	6537	2160	87	185801	19516	9213			3			6.44

Asia : 8002 [13, 14]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-1678	2527	126	211298	20492	9673	18	30	0.948	0.927	--	0.915	0.512	0.549	0.853

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1678	2313	64	190741	19516	9213	(12+13)>I-1					7.45
1	Z	1678	1388	107	186489	19516	9213	(12+13)>I-1					10.9

Asia : 8002 [14, 15]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-2298	-2681	-63	211298	20492	9673	17	28	0.953	0.933	--	1.002	0.462	0.601	0.770

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2298	2685	29	191736	19516	9213	(12+13)>III-4					6.55
1	Z	2298	1611	48	187853	19516	9213	(12+13)>III-4					10.00

Asia : 8002 [15, 47]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-4098	-2560	-83	211298	20492	9673	16	26	0.960	0.943	--	1.002	0.427	0.601	0.712

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	4098	2566	36	193185	19516	9213			6			6.39
1	Z	4098	1540	59	189853	19516	9213			6			9.35

Asia : 8002 [47, 48]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-3097	-2570	-81	211298	20492	9673	15	25	0.967	0.953	--	0.952	0.454	0.571	0.756

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	3097	2447	37	194565	19516	9213			3			6.88
1	Z	3097	1468	61	191772	19516	9213			3			10.2

Asia : 8002 [48, 49]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2505	-2257	-91	211298	20492	9673	13	22	0.976	0.965	--	0.856	0.428	0.514	0.713

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2505	1933	39	196336	19516	9213			3			8.62
1	Z	2505	1160	65	194255	19516	9213			3			12.6

Asia : 8002 [49 , 50]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2514	2337	40	211298	20492	9673	12	20	0.983	0.976	--	0.786	0.435	0.472
													0.725

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2514	1837	17	197912	19516	9213	(12+13)-I+4	9.20
1	Z	2514	1102	29	196483	19516	9213	(12+13)-I+4	13.8

Asia : 8002 [50 , 51]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2732	3215	17	211298	20492	9673	11	19	0.990	0.985	--	0.891	0.240	0.535
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2732	2865	4	199176	19516	9213	(12+13)-I+4	6.21
1	Z	2732	1719	7	198282	19516	9213	(12+13)-I+4	9.75

Asia : 8002 [51 , 52]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1755	3311	-11	211298	20492	9673	11	18	0.993	0.990	--	0.988	0.377	0.593
													0.629

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1755	3271	4	199872	19516	9213	(12+13)-III+4	5.65
1	Z	1755	1963	7	199276	19516	9213	(12+13)-III+4	9.08

Asia : 8002 [52 , 14]

Sez. G: HE 240 A L=110.7 cm Ln1=110.7 cm Ln2=110.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1895	4118	9	211298	20492	9673	11	18	0.992	0.988	--	0.855	0.533	0.513
													0.888

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1895	3523	5	199529	19516	9213	6	5.25
1	Z	1895	2114	8	198785	19516	9213	6	8.42

Asia : 8003 [15 , 1]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-7001	5365	70	211298	20492	9673	18	30	0.945	0.923	--	0.718	0.439	0.431
													0.732

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7001	3854	31	190245	19516	9213	3	4.21
1	Z	7001	2312	51	185813	19516	9213	3	6.18

Asia : 8003 [1 , 2]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2582	-2594	-52	211298	20492	9673	18	30	0.948	0.927	--	0.601	0.360	0.361
													0.601

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2582	1559	19	190750	19516	9213	(12+13)-II+4	10.5
1	Z	2582	936	31	186502	19516	9213	(12+13)-II+4	15.3

Asia : 8003 [2 , 3]

Sez. G: HE 240 A L=169.7 cm Ln1=169.7 cm Ln2=169.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2559	-2768	-59	211298	20492	9673	17	28	0.953	0.934	--	1.002	0.368	0.601
													0.613

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2559	2773	22	191746	19516	9213	(12+13)-II+4	6.34
1	Z	2559	1664	36	187867	19516	9213	(12+13)-II+4	9.73

Asia : 8003 [3 , 23]

Sez. G: HE 240 A L=158.4 cm Ln1=158.4 cm Ln2=158.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4581	-2760	-49	211298	20492	9673	16	26	0.960	0.944	--	0.945	0.432	0.567
													0.720

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4581	2608	21	193195	19516	9213	6	6.27
1	Z	4581	1565	35	189868	19516	9213	6	9.25

Asia : 8003 [23 , 24]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3538	-2775	-31	211298	20492	9673	15	25	0.967	0.953	--	0.953	0.502	0.572
													0.837

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3538	2645	16	194576	19516	9213	3	6.43
1	Z	3538	1587	26	191788	19516	9213	3	9.75

Asia : 8003 [24 , 25]

Sez. G: HE 240 A L=134.3 cm Ln1=134.3 cm Ln2=134.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2897	-2438	-36	211298	20492	9673	13	22	0.976	0.965	--	0.861	0.472	0.517
													0.787

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2897	2099	17	196349	19516	9213	3	8.05
1	Z	2897	1260	28	194273	19516	9213	3	12.1

Asia : 8003 [25 , 26]

Sez. G: HE 240 A L=122.5 cm Ln1=122.5 cm Ln2=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2668	2348	44	211298	20492	9673	12	20	0.984	0.976	--	0.777	0.470	0.466
													0.784

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2668	1825	20	197927	19516	9213	(12+13)-1-4	9.16
1	Z	2668	1095	34	196503	19516	9213	(12+13)-1-4	13.6

Asta : 8003 [26 , 27]

Sez. G: HE 240 A L=113.1 cm Ln1=113.1 cm Ln2=113.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-2901	3271	-28	211298	20492	9673	11	19	0.990	0.985	--	0.887	0.239	0.532
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	2901	2903	7	199192	19516	9213	(12+13)-1-4	6.10
1	Z	2901	1742	11	198304	19516	9213	(12+13)-1-4	9.52

Asta : 8003 [27 , 28]

Sez. G: HE 240 A L=108.0 cm Ln1=108.0 cm Ln2=108.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-1966	3401	-27	211298	20492	9673	11	18	0.993	0.990	--	0.984	0.381	0.590
													0.636

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	1966	3346	10	199888	19516	9213	(12+13)-III-4	5.48
1	Z	1966	2008	17	199300	19516	9213	(12+13)-III-4	8.73

Asta : 8003 [28 , 15]

Sez. G: HE 240 A L=110.5 cm Ln1=110.5 cm Ln2=110.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-2292	4478	7	211298	20492	9673	11	18	0.992	0.988	--	0.851	0.531	0.510
													0.884

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	2292	3810	4	199545	19516	9213	6	4.83
1	Z	2292	2286	6	198808	19516	9213	6	7.73

Asta : 8004 [16 , 19]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-7330	5577	64	211298	20492	9673	18	30	0.945	0.923	--	0.721	0.379	0.433
													0.632

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	7330	4024	24	190236	19516	9213	3	4.04
1	Z	7330	2414	41	185800	19516	9213	3	5.97

Asta : 8004 [19 , 20]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-2658	-2512	-65	211298	20492	9673	18	30	0.948	0.927	--	0.601	0.360	0.361
													0.601

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	2658	1510	24	190740	19516	9213	(12+13)-1-4	10.7
1	Z	2658	906	39	186488	19516	9213	(12+13)-1-4	15.4

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Asta : 8004 [20 , 21]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-2644	-2706	119	211298	20492	9673	17	28	0.953	0.933	--	0.973	0.333	0.584
													0.556

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	2644	2633	40	191735	19516	9213	(12+13)-1-4	6.53
1	Z	2644	1580	66	187852	19516	9213	(12+13)-1-4	9.78

Asta : 8004 [21 , 59]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-5124	-2869	-26	211298	20492	9673	16	26	0.960	0.943	--	0.940	0.430	0.564
													0.716

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	5124	2698	11	193184	19516	9213	6	6.03
1	Z	5124	1619	19	189852	19516	9213	6	8.93

Asta : 8004 [59 , 60]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-4021	-2879	-15	211298	20492	9673	15	25	0.967	0.953	--	1.002	0.586	0.601
													0.977

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	4021	2884	9	194564	19516	9213	3	5.90
1	Z	4021	1731	14	191770	19516	9213	3	8.99

Asta : 8004 [60 , 61]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-3328	-2574	-16	211298	20492	9673	13	22	0.976	0.965	--	0.866	0.420	0.520
													0.701

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	3328	2229	7	196335	19516	9213	3	7.58
1	Z	3328	1338	11	194254	19516	9213	3	11.5

Asta : 8004 [61 , 62]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-2681	2258	-76	211298	20492	9673	12	20	0.983	0.976	--	0.769	0.482	0.461
													0.803

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	2681	1736	37	197911	19516	9213	(12+13)-1-4	9.39
1	Z	2681	1042	61	196481	19516	9213	(12+13)-1-4	13.6

Asta : 8004 [62 , 63]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 \text{ fyk} \cdot \gamma M=2619$

kg/cm² ft=4300 kg/cm² **Verificato**

420

	N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg*m	kg	kg*m	kg*m								
-2925	3220	51	211298	20492	9673		11	19	0.990	0.985	--	0.881	0.260	0.529
														0.433
	Clis	Dir	N	Mvseq	NRd	MvRd	MzRd							SF
			kg	kg*m		kg*m	kg*m							
	1	Y	2925	2837	13	199175	9213	19516					(12+13)-III-4	6.19
	1	Z	2925	1702	22	198280	9213	19516					(12+13)-III-4	9.58

Asia : 8004 [63 , 64]

Sez. G: HE 240 A L=108.2 cm Ln1=108.2 cm Ln2=108.2 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

Clis	Dir	N	kg	Myeq	Mzseq	NRd	MyRd	MzRd	SF
1	Y	2184	3338	13	199871	19516	9213	(12+13)-III-4	5.45
2	Y	2184	2003	21	199274	19516	9213	(12+13)-III-4	8.63

Asia : 8004 [64 , 16]

Sez. G: HE 240 A L=110.7 cm Ln1=110.7 cm Ln2=110.7 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

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Asia : 8005 [17 , 16]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

Clis	Dir	N	Myeq		NRd		MyRd		MzRd		Comb.	SF		
			kg	kg*	kg	kg*	kg	kg*	χY	χZ		χLT	kyy	kyz
1	Y	6512	3921	24	190242	19516	3	4.21						
1	Z	6512	2353	40	185809	19516	3	6.25						

Asia : 8005 [16 , 17]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

Clis	Dir	N	Mvseq kg kg*m	NRd kg kg*m	Mzseq kg kg*m	MvRk kg kg*m	MzRk kg kg*m	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz	SF
1	Y	2042	2392	64	190852	19516	9213						(12+13)→V-1			7.13
1	Z	2042	1435	107	186642	19516	9213						(12+13)→V-1			10.4

Asia : 8005 [17 , 18]

Sez. G: HE 240 A L=169.7 cm Ln1=169.7 cm Ln2=169.7 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

Clis	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg	kg*m	17	28	0.954	0.935	--	1.001	0.422	0.601
-2088	-2526	-108	211298	20492	9673									0.703

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg		
1	Y	2088	2528	45	191955	19516	9213	(12+13)→VII-4	6.88
1	Z	2088	1517	76	188154	19516	9213	(12+13)→VII-4	10.3

Asia : 8005 [18 , 53]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg	kg*m	kg	kg*m		
-4166	-2840	-8	211298	20492	9673	16	26	0.962	0.946
		kg	kg*m	kg	kg*m	kg	kg*m	--	0.945
		kg	kg*m	kg	kg*m	kg	kg*m	0.567	0.832
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg		
1	Y	4166	2683	4	193514	19516	9213	6	6.27
1	Z	4166	1610	7	190310	19516	9213	6	9.51

Asia : 8005 [53 , 54]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg		
-3418	-2859	-10	211298	20492	9673	14	24	0.969	0.956
		kg	kg*m	kg	kg*m	kg	kg*m	--	0.955
		kg	kg*m	kg	kg*m	kg	kg*m	0.573	0.476
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg		
1	Y	3418	2731	3	195008	19516	9213	3	6.34
1	Z	3418	1638	5	192390	19516	9213	3	9.78

Asia : 8005 [54 , 55]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	2785	2166	3	196897	9213	9213	3	7.97
1	Z	2785	1299	4	195046	9213	9213	3	12.3

Asia : 8005 [57 , 58]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2620	3157	44	211298	20492	9673	10	17	0.998	0.997	--	0.967	0.496	0.580
													0.827

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2620	3053	22	200795	19516	9213	(12+13)-VIII-4	5.82
1	Z	2620	1832	36	200601	19516	9213	(12+13)-VIII-4	9.02

Asia : 8005 [58 , 17]

Sez. G: HE 240 A L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2219	4802	5	211298	20492	9673	11	19	0.989	0.985	--	0.837	0.306	0.502
													0.510

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2219	4021	2	199118	19516	9213	6	4.60
1	Z	2219	2413	3	198199	19516	9213	6	7.40

Asia : 8006 [18 , 22]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6954	5137	13	211298	20492	9673	18	30	0.945	0.923	--	0.717	0.241	0.430
													0.402

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6954	3684	3	190234	19516	9213	3	4.43
1	Z	6954	2210	5	185797	19516	9213	3	6.61

Asia : 8006 [22 , 23]

Sez. G: HE 240 A L=177.7 cm Ln1=177.7 cm Ln2=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1639	2607	-99	211298	20492	9673	18	30	0.948	0.927	--	0.879	0.252	0.527
													0.419

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1639	2291	25	190738	19516	9213	(12+13)-V-1	7.77
1	Z	1639	1375	42	186485	19516	9213	(12+13)-V-1	11.9

Asia : 8006 [23 , 24]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2487	-2510	138	211298	20492	9673	17	28	0.953	0.933	--	0.960	0.327	0.576
													0.545

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2487	2410	45	191733	19516	9213	(12+13)-I-4	7.07
1	Z	2487	1446	75	187849	19516	9213	(12+13)-I-4	10.5

Asia : 8006 [24 , 65]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4143	-2633	41	211298	20492	9673	16	26	0.960	0.943	--	0.942	0.439	0.565
													0.732

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4143	2481	18	193181	19516	9213	6	6.64
1	Z	4143	1489	30	189848	19516	9213	6	9.87

Asia : 8006 [65 , 66]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3052	-2639	23	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.498	0.601
													0.830

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3052	2643	11	194561	19516	9213	3	6.56
1	Z	3052	1586	19	191767	19516	9213	3	10.1

Asia : 8006 [66 , 67]

Sez. G: HE 240 A L=134.5 cm Ln1=134.5 cm Ln2=134.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2464	-2362	26	211298	20492	9673	13	22	0.976	0.965	--	0.870	0.450	0.522
													0.750

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2464	2054	12	196332	19516	9213	3	8.40
1	Z	2464	1233	20	194250	19516	9213	3	12.8

Asia : 8006 [67 , 68]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2090	2145	46	211298	20492	9673	12	20	0.983	0.976	--	0.765	0.531	0.459
													0.885

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2090	1642	24	197908	19516	9213	(12+13)-V-4	10.3
1	Z	2090	985	40	196476	19516	9213	(12+13)-V-4	15.3

Asia : 8006 [68 , 69]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2215	3224	167	211298	20492	9673	11	19	0.990	0.985	--	0.832	0.240	0.499
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2215	2683	40	199171	19516	9213	(12+13)-III-3	6.54
1	Z	2215	1610	67	198275	19516	9213	(12+13)-III-3	9.91

Asia : 8006 [69 , 70]

Sez. G: HE 240 A L=108.2 cm Ln1=108.2 cm Ln2=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2337	3222	-115	211298	20492	9673	11	18	0.993	0.990	--	0.971	0.421	0.583
													0.702

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2337	3129	49	199867	19516	9213	(12+13)-I-3	5.64
1	Z	2337	1877	81	199269	19516	9213	(12+13)-I-3	8.57

Asia : 8006 [70 , 22]

Sez. G: HE 240 A L=110.7 cm Ln1=110.7 cm Ln2=110.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-1911	4382	7	211298	20492	9673	11	18	0.991	0.988	--	0.851	0.305	0.510
													0.508

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1911	3727	2	199524	19516	9213	6	4.98
1	Z	1911	2236	3	198778	19516	9213	6	8.03

Asia : 8007 [19 , 4]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-6517	4638	-25	211298	20492	9673	18	30	0.945	0.923	--	0.603	0.361	0.362
													0.602

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6517	2797	9	190240	19516	9213	3	5.60
1	Z	6517	1678	15	185806	19516	9213	3	8.15

Asia : 8007 [4 , 5]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-1726	2554	-127	211298	20492	9673	18	30	0.948	0.927	--	0.891	0.278	0.535
													0.463

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1726	2276	35	190745	19516	9213	(12+13)-VII-1	7.72
1	Z	1726	1365	59	186494	19516	9213	(12+13)-VII-1	11.7

Asia : 8007 [5 , 6]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-2317	-2457	112	211298	20492	9673	17	28	0.953	0.934	--	1.001	0.240	0.601
													0.400

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2317	2459	27	191740	19516	9213	(12+13)-VII-4	7.09
1	Z	2317	1475	45	187859	19516	9213	(12+13)-VII-4	10.8

Asia : 8007 [6 , 29]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-4032	-2588	86	211298	20492	9673	16	26	0.960	0.943	--	0.948	0.452	0.569
													0.753

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4052	2454	39	193189	19516	9213	6	6.63
1	Z	4032	1472	65	189859	19516	9213	6	9.65

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Asia : 8007 [29 , 30]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-3050	-2596	38	211298	20492	9673	15	25	0.967	0.953	--	0.952	0.554	0.571
													0.924

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3050	2472	21	194569	19516	9213	3	6.91
1	Z	3050	1483	35	191778	19516	9213	3	10.4

Asia : 8007 [30 , 31]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-2	-1875	545	211298	20492	9673	13	22	0.976	0.965	--	0.928	0.480	0.557
													0.800

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2	1740	262	196342	19516	9213	(12+13)-VI-1	8.50
1	Z	2	1044	436	194263	19516	9213	(12+13)-VI-1	9.91

Asia : 8007 [31 , 32]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-2354	2194	62	211298	20492	9673	12	20	0.984	0.976	--	0.779	0.499	0.468
													0.832

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2354	1710	31	197918	19516	9213	(12+13)-VII-4	9.72
1	Z	2354	1026	52	196491	19516	9213	(12+13)-VII-4	14.3

Asia : 8007 [32 , 33]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-2569	3059	52	211298	20492	9673	11	19	0.990	0.985	--	0.887	0.240	0.532
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2569	2714	12	199183	19516	9213	(12+13)-VII-4	6.52
1	Z	2569	1628	21	198291	19516	9213	(12+13)-VII-4	10.1

Asia : 8007 [33 , 34]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m			kg					
-1680	3199	-19	211298	20492	9673	11	18	0.993	0.990	--	0.983	0.507	0.590
													0.846

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	1680	3144	10	199879	19516	9213	(12+13)-VII-4	5.86
1	Z	1680	1886	16	199286	19516	9213	(12+13)-VII-4	9.36

Asia : 8007 [34 , 18]

Sez. G: HE 240 A L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619
kg/cm² ft=4300 kg/cm²**Verificato**

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N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1904	4169	-5	211298	20492	9673	11	18	0.992	0.988	--	0.854	0.240	0.513
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1904	3562	1	199535	19516	9213	6	5.20
1	Z	1904	2137	2	198794	19516	9213	6	8.38

Asia : 8008 I 20..25 I

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6409	4964	-69	211298	20492	9673	18	30	0.945	0.923	--	0.711	0.366	0.427
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6409	3531	25	190238	19516	9213	3	4.60
1	Z	6409	2119	42	185803	19516	9213	3	6.77

Asia : 8008 I 25..26 I

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1765	2484	-155	211298	20492	9673	18	30	0.948	0.927	--	0.888	0.367	0.533
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	1765	2205	57	190743	19516	9213	(12+13)÷VII-4	7.79
1	Z	1765	1323	95	186492	19516	9213	(12+13)÷VII-1	11.4

Asia : 8008 I 26..27 I

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2240	-2401	107	211298	20492	9673	17	28	0.953	0.934	--	1.001	0.303	0.600
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	2240	2403	33	191738	19516	9213	(12+13)÷VII-4	7.23
1	Z	2240	1442	54	187856	19516	9213	(12+13)÷VII-4	10.9

Asia : 8008 I 27..71 I

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4080	-2510	142	211298	20492	9673	16	26	0.960	0.943	--	1.002	0.467	0.601
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	4080	2516	67	193187	19516	9213	6	6.36
1	Z	4080	1510	111	189856	19516	9213	6	9.02

Asia : 8008 I 71..72 I

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3102	-2514	92	211298	20492	9673	15	25	0.967	0.953	--	0.952	0.528	0.571
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	3102	2293	49	194567	19516	9213	3	6.95
1	Z	3102	1436	81	191775	19516	9213	3	10.1

Asia : 8008 I 72..73 I

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2517	-2206	103	211298	20492	9673	13	22	0.976	0.965	--	0.856	0.424	0.514
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	2517	1888	44	196339	19516	9213	3	8.75
1	Z	2517	1133	73	194259	19516	9213	3	12.7

Asia : 8008 I 73..74 I

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2233	2108	65	211298	20492	9673	12	20	0.983	0.976	--	0.779	0.496	0.468
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	2233	1642	32	197915	19516	9213	(12+13)÷VII-4	10.1
1	Z	2233	985	53	196487	19516	9213	(12+13)÷VII-4	14.8

Asia : 8008 I 74..75 I

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2441	2960	53	211298	20492	9673	11	19	0.990	0.985	--	0.885	0.268	0.531
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	2441	2620	14	199180	19516	9213	(12+13)÷VII-4	6.75
1	Z	2441	1572	24	198287	19516	9213	(12+13)÷VII-4	10.5

Asia : 8008 I 75..76 I

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1622	3133	-14	211298	20492	9673	11	18	0.993	0.990	--	0.978	0.465	0.587
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	1622	5064	6	199876	19516	9213	(12+13)÷VII-4	6.03
1	Z	1622	1838	11	199282	19516	9213	(12+13)÷VII-4	9.66

Asia : 8008 I 76..19 I

Sez. G: HE 240 A L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1877	4001	-6	211298	20492	9673	11	18	0.992	0.988	--	0.855	0.501	0.513
<i>Verificato</i>													

Cls	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	1877	3422	3	199552	19516	9213	6	5.40
1	Z	1877	2053	5	198790	19516	9213	6	8.68

Asta : 8009 [21 , 28]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg*m	kg*m	kg*m								
-6078	4312	-101	211298	20492	9673	18	30	0.945	0.923	--	0.603	0.361	0.362
0.602													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6078	2600	36	190239	19516	9213	3	5.91
1	Z	6078	1560	61	185804	19516	9213	3	8.39

Asta : 8009 [28 , 29]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1546	2285	-222	211298	20492	9673	18	30	0.948	0.927	--	0.871	0.378	0.523
0.630													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1546	1991	84	190743	19516	9213	(12+13)÷VII-1	8.39
1	Z	1546	1194	140	186493	19516	9213	(12+13)÷VII-1	11.8

Asta : 8009 [29 , 30]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3327	-2163	139	211298	20492	9673	17	28	0.953	0.934	--	1.002	0.364	0.601
0.607													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3327	2167	51	191738	19516	9213	(12+13)÷VII-4	7.47
1	Z	3327	1300	85	187857	19516	9213	(12+13)÷VII-4	10.7

Asta : 8009 [30 , 77]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4583	-2217	196	211298	20492	9673	16	26	0.960	0.943	--	1.002	0.477	0.601
0.794													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4583	2222	93	193188	19516	9213	6	6.77
1	Z	4583	1333	156	189857	19516	9213	6	9.14

Asta : 8009 [77 , 78]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4000	-2218	110	211298	20492	9673	15	25	0.967	0.953	--	1.002	0.581	0.601
0.968													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4000	2222	64	194568	19516	9213	3	7.07
1	Z	4000	1333	107	191776	19516	9213	3	9.93

Asta : 8009 [78 , 79]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3063	-4156	-34	211298	20492	9673	18	30	0.945	0.923	--	0.850	0.240	0.510
0.401													

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1278	-1977	484	211298	20492	9673	13	22	0.976	0.965	--	0.875	0.448	0.525
0.747													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1278	1731	217	196340	19516	9213	(12+13)÷VIII-1	8.42
1	Z	1278	1039	361	194260	19516	9213	(12+13)÷VIII-1	10.1

Asta : 8009 [79 , 80]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2365	1861	-187	211298	20492	9673	12	20	0.984	0.976	--	0.759	0.474	0.456
0.790													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2365	1414	88	197916	19516	9213	(12+13)÷VIII-4	10.6
1	Z	2365	848	147	196488	19516	9213	(12+13)÷VIII-4	14.0

Asta : 8009 [80 , 81]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2467	2626	-122	211298	20492	9673	11	19	0.990	0.985	--	0.884	0.240	0.530
0.399													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2467	2321	29	199180	19516	9213	(12+13)÷VIII-4	7.44
1	Z	2467	1393	49	198287	19516	9213	(12+13)÷VIII-4	11.2

Asta : 8009 [81 , 82]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1144	3007	18	211298	20492	9673	11	18	0.993	0.990	--	0.928	0.240	0.557
0.400													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1144	2790	4	199876	19516	9213	(12+13)÷VII-4	6.71
1	Z	1144	1674	7	199282	19516	9213	(12+13)÷VII-4	10.8

Asta : 8009 [82 , 83]

Sez. G: HE 240 A L=110.6 cm Ln1=110.6 cm Ln2=110.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1476	3958	-6	211298	20492	9673	11	18	0.992	0.988	--	0.830	0.503	0.498
0.839													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1476	3285	3	199533	19516	9213	6	5.68
1	Z	1476	1971	5	198791	19516	9213	6	9.17

Asta : 8010 [22 , 31]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3063	-4156	-34	211298	20492	9673	18	30	0.945	0.923	--	0.850	0.240	0.510
0.401													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3063	3533	8	190237	19516	9213	(12+13)+VIII-1	5.05
1	Z	3063	2120	14	185801	19516	9213	(12+13)+VIII-1	7.90

Asta : 8010 [31 , 32]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.948	0.927	--	0.765	0.390	0.459
-2694	2576	-277	211298	20492	9673	18	30	0.948	0.927	--	0.765	0.390	0.459

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2694	1971	108	190741	19516	9213	(12+13)+VIII-1	7.88
1	Z	2694	1183	180	186489	19516	9213	(12+13)+VIII-1	10.6

Asta : 8010 [32 , 33]

Sez. G: HE 240 A L=169.8 cm Ln1=169.8 cm Ln2=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	17	28	0.953	0.933	--	0.731	0.394	0.439
-1556	-1727	197	211298	20492	9673	17	28	0.953	0.933	--	0.731	0.394	0.439

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1556	1263	77	191736	19516	9213	6	12.3
1	Z	1556	758	129	187853	19516	9213	6	16.4

Asta : 8010 [33 , 83]

Sez. G: HE 240 A L=158.5 cm Ln1=158.5 cm Ln2=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	16	26	0.960	0.943	--	0.908	0.461	0.545
-1035	-2243	205	211298	20492	9673	16	26	0.960	0.943	--	0.908	0.461	0.545

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1035	2038	95	193185	19516	9213	6	8.33
1	Z	1035	1223	158	189853	19516	9213	6	11.7

Asta : 8010 [83 , 84]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m	15	25	0.967	0.953	--	1.000	0.597	0.600
-280	-2274	95	211298	20492	9673	15	25	0.967	0.953	--	1.000	0.597	0.600

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	280	2274	57	194565	19516	9213	3	8.06
1	Z	280	1365	95	191772	19516	9213	3	12.2

Asta : 8010 [84 , 85]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m	13	22	0.976	0.965	--	0.860	0.390	0.516
-75	-2036	102	211298	20492	9673	13	22	0.976	0.965	--	0.860	0.390	0.516

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	75	1752	40	196337	19516	9213	6	10.6
1	Z	75	1051	66	194256	19516	9213	6	16.3

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Asta : 8010 [85 , 86]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	12	20	0.983	0.976	--	0.727	0.305	0.508
-1203	1777	13	211298	20492	9673	12	20	0.983	0.976	--	0.727	0.305	0.508

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1203	1292	4	197913	19516	9213	(12+13)+VII-4	13.8
1	Z	1203	775	7	196483	19516	9213	(12+13)+VII-4	21.5

Asta : 8010 [86 , 87]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	19	0.990	0.985	--	0.861	0.388	0.517
-1414	2724	-16	211298	20492	9673	11	19	0.990	0.985	--	0.861	0.388	0.517

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1414	2346	6	199177	19516	9213	(12+13)+VII-4	7.81
1	Z	1414	1408	10	198282	19516	9213	(12+13)+VII-4	12.4

Asta : 8010 [87 , 88]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
	kg	kg*m	kg*m	kg	kg*m	kg*m								
-2347	3463	-74	211298	20492	9673		11	18	0.993	0.990	--	0.939	0.322	0.563
	Cls	Dir	N	Mveq	Mzeq	NRd			MyRd	MzRd				SF
			kg	kg*m	kg*m	kg			kg*m	kg*m				
1	Y		2347	3250	24		199872	19516	19516	9213		(12+13)+V-3		5.53
1	Z		2347	1950	40		199277	19516	19516	9213		(12+13)+V-3		8.62

Asta : 8010 [88 , 211]

Sez. G: HE 240 A L=110.7 cm Ln1=110.7 cm Ln2=110.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg	kg*m	11	18	0.992	0.988	--	0.993	0.482	0.596
-2505	3488	27	211298	20492	9673	11	18	0.992	0.988	--	0.993	0.482	0.596

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2505	3464	13	199529	19516	9213	(12+13)+V-3	5.22
1	Z	2505	2079	22	198785	19516	9213	(12+13)+V-3	8.23

Verifica Resistenza aste Metalliche

Scenario di calcolo : **Set_NT_SlV_A2_STR/GEO**

Asta : 1 [1 , 28]

Sez. G: HE 240 A L=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq ;**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m			
0	1	-14689	-323	-1519	1	3135	-876	--	--	(12+13)+IV-2

X	cls	Nr	Vvr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	201236	87022	38035	19516	9213	462	25.0	3.04	>100	3.04

Asta : 1 [28 , 12]

432

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
271	1	-4690	-132	-1889	1	-4373	47	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
271	1	201236	87001	38026	19516	9213	462	20.1	3.96	>100	3.96

Asta : 2 [2 , 25]

Sez. G: HE 240 A L=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-13100	385	-1033	-1	2486	1042	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87060	38052	19516	9213	462	36.8	3.27	>100	3.27

Asta : 2 [25 , 13]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
271	1	-7411	-59	-2029	0	-4839	-124	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
271	1	201236	87078	38060	19516	9213	462	18.8	3.35	>100	3.35

Asta : 3 [3 , 27]

Sez. G: HE 240 A L=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3204	458	-1094	0	2798	1109	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87092	38066	19516	9213	462	34.8	3.58	>100	3.58

Asta : 3 [27 , 14]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
271	1	-6936	-92	-2132	0	-5079	-69	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
271	1	201236	87075	38059	19516	9213	462	17.8	3.31	>100	3.31

Asta : 4 [4 , 23]

Sez. G: HE 240 A L=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3236	435	-1164	-0	3031	1071	--	--	(12+13)-II-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87083	38062	19516	9213	462	32.7	3.48	>100	3.48

433

Asta : 4 [23 , 15]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
271	1	-7555	-114	-2239	0	-5365	-39	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
271	1	201236	87088	38064	19516	9213	462	17.0	3.16	>100	3.16

Asta : 5 [5 , 29]

Sez. G: HE 240 A L=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2512	411	-1223	0	3162	1042	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87079	38060	19516	9213	462	31.1	3.48	>100	3.48

Asta : 5 [29 , 16]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
271	1	-7775	-123	-2328	0	-5580	-22	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
271	1	201236	87070	38056	19516	9213	462	16.3	3.06	>100	3.06

Asta : 6 [6 , 30]

Sez. G: HE 240 A L=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-11180	-248	-1524	1	3882	-708	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87006	38028	19516	9213	462	24.9	3.02	>100	3.02

Asta : 6 [30 , 17]

Sez. G: HE 240 A L=271.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
271	1	-6484	-117	-2285	-1	-5489	-34	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
271	1	201236	87059	38051	19516	9213	462	16.6	3.15	>100	3.15

Asta : 7 [7 , 24]

Sez. G: HE 240 A L=211.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-13147	361	-1310	1	3344	903	--	--	(12+13)-VI-1

434

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86986	38020	19516	9213	462	29.0	2.99	>100	2.99

Asta : 7 [24 , 18]

Sez. G: HE 240 A L=2711.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
271	1	-7798	-121	-2155	0	-5137	-30	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
271	1	201236	87069	38056	19516	9213	462	17.7	3.28	>100	3.28

Asta : 8 [8 , 26]

Sez. G: HE 240 A L=2111.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2291	-413	-1205	0	3222	-987	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87060	38052	19516	9213	462	31.6	3.53	>100	3.53

Asta : 8 [26 , 19]

Sez. G: HE 240 A L=2711.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
271	1	-7056	-166	-2099	-1	-5038	50	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
271	1	201236	87059	38052	19516	9213	462	18.1	3.35	>100	3.35

Asta : 9 [9 , 31]

Sez. G: HE 240 A L=2111.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2512	-429	-1153	0	3030	-1040	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87082	38062	19516	9213	462	33.0	3.56	>100	3.56

Asta : 9 [31 , 20]

Sez. G: HE 240 A L=2711.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
271	1	-6950	-144	-2064	-0	-4974	0	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
271	1	201236	87087	38064	19516	9213	462	18.4	3.45	>100	3.45

Asta : 10 [10 , 32]

Sez. G: HE 240 A L=2111.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-12564	-446	-1003	-0	2588	-1047	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87070	38056	19516	9213	462	37.9	3.24	>100	3.24

Asta : 10 [32 , 21]

Sez. G: HE 240 A L=2711.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
271	1	-6393	-158	-1940	-1	-4698	25	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
271	1	201236	87026	38037	19516	9213	462	19.6	3.63	>100	3.63

Asta : 11 [11 , 33]

Sez. G: HE 240 A L=2111.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-13940	252	-1647	-4	3636	745	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86807	37941	19516	9213	462	23.0	2.97	>100	2.97

Asta : 11 [33 , 22]

Sez. G: HE 240 A L=2711.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
271	1	-7755	87	-1625	3	-4156	-28	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
271	1	201236	86889	37977	19516	9213	462	23.4	3.93	>100	3.93

Asta : 12 [2 , 13]

Sez. G: HE 240 A L=2651.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	811	-533	2673	-0	-3345	-1401	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87073	38057	19516	9213	462	14.2	3.05	>100	3.05

Asta : 13 [10 , 21]

Sez. G: HE 240 A L=2651.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3115	484	2836	1	-4079	1278	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87050	38047	19516	9213	462	13.4	2.75	>100	2.75

Asta : 14 [9 , 20]

Sez. G: HE 240 A L=2651.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

Asta : 20 [3 , 14]

Sez. G: HE 240 A L=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1009	-534	2263	-0	-3112	-1407	--	--	(12+13)-II-4
X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	201236	87085	38063	19516	9213	462	16.8	3.15	>100 3.15

Asta : 21 [1 , 12]

Sez. G: HE 240 A L=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3423	-537	2772	-0	-3727	-1411	--	--	(12+13)-II-4
X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	201236	87086	38063	19516	9213	462	13.7	2.77	>100 2.77

Asta : 22 [11 , 22]

Sez. G: HE 240 A L=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2376	427	2308	1	-3614	1130	--	--	(12+13)-V-3
X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	201236	87054	38049	19516	9213	462	16.5	3.13	>100 3.13

Asta : 7001 [1 , 25]

Sez. G: Fi18 L=258.7 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
259	1	3553	--	--	--	--	--	--	--	(12+13)-VI-3
X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
259	1	6665	--	--	--	--	--	>100	1.88	>100 1.88

Asta : 7002 [25 , 12]

Sez. G: Fi18 L=309.6 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-5202	--	--	--	--	--	--	--	(12+13)-VI-3
X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	6665	--	--	--	--	--	>100	1.28	>100 1.28

Asta : 7003 [12 , 11]

Sez. G: Fi16 L=386.9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1581	--	--	--	--	--	--	--	(12+13)-IV-2
X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	5266	--	--	--	--	--	>100	3.33	>100 3.33

Asta : 7004 [11 , 35]

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	609	413	2758	-0	-3633	1205	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	201236	87072	38057	19516	9213	462	13.8	3.13	>100 3.13

Asta : 15 [8 , 19]

Sez. G: HE 240 A L=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-868	478	2353	-0	-5344	1255	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	201236	87072	38057	19516	9213	462	16.2	3.21	>100 3.21

Asta : 16 [7 , 18]

Sez. G: HE 240 A L=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-721	472	2388	1	-3521	1223	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	201236	87057	38050	19516	9213	462	15.9	3.16	>100 3.16

Asta : 17 [6 , 17]

Sez. G: HE 240 A L=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2466	-525	1986	-1	-3104	-1345	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	201236	87054	38049	19516	9213	462	19.2	3.15	>100 3.15

Asta : 18 [5 , 16]

Sez. G: HE 240 A L=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-912	-534	2392	0	-3434	-1389	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	201236	87070	38056	19516	9213	462	15.9	3.02	>100 3.02

Asta : 19 [4 , 15]

Sez. G: HE 240 A L=265.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1067	-534	2395	0	-3379	-1401	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	201236	87070	38056	19516	9213	462	15.9	3.03	>100 3.03

Sez. G: Fil16 L=353,5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	2.90
353	1	1819	--	--	--	--	--	--	--	--	Comb.

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	>100	2.90	>100
353	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7005 [35 , 43]

Sez. G: Fil16 L=306,2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
306	1	975	--	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	>100	5.40	>100
306	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7006 [43 , 39]

Sez. G: Fil16 L=258,3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
0	1	-2181	--	--	--	--	--	--	--	--	(12+13)>VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	2.41
0	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7007 [39 , 13]

Sez. G: Fil16 L=236,9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
237	1	-838	--	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	6.28
237	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7008 [13 , 1]

Sez. G: Fil6 L=279,8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
280	1	-3190	--	--	--	--	--	--	--	--	(12+13)>IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	1.65
280	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7009 [2 , 12]

Sez. G: Fil16 L=237,1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
280	1	3092	--	--	--	--	--	--	--	--	(12+13)>IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	1.70
280	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7010 [12 , 45]

Sez. G: Fil6 L=237,1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
0	1	-1063	--	--	--	--	--	--	--	--	(12+13)>I-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	4.96
0	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7011 [45 , 37]

Sez. G: Fil16 L=258,2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
0	1	2351	--	--	--	--	--	--	--	--	(12+13)>IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	2.24
0	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7012 [37 , 41]

Sez. G: Fil6 L=306,1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
306	1	-788	--	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	6.68
306	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7013 [41 , 8]

Sez. G: Fil16 L=353,6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
354	1	-1774	--	--	--	--	--	--	--	--	(12+13)>VIII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	2.97
354	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7014 [8 , 13]

Sez. G: Fil16 L=389,8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
0	1	1529	--	--	--	--	--	--	--	--	(12+13)>IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	3.44
0	1	5266	--	--	--	--	--	--	--	--	Comb.

Asia : 7015 [13 , 28]

Sez. G: Fil18 L=309,6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
0	1	5432	--	--	--	--	--	--	--	--	(12+13)>VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	1.23
0	1	6665	--	--	--	--	--	--	--	--	Comb.

Asia : 7016 [28 , 2]

Sez. G: Fil18 L=258,7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ϕ f=4300 kg/cm ϕ : Verificato											
X	cls	N	TY	Nr	Vyr	Vzr	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	--	Comb.
259	1	-3634	--	--	--	--	--	--	--	--	(12+13)>VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF M _t	SF
cm		kg	kg	kg	kg	kg	kg*m	kg*m	kg*m	>100	1.83
259	1	6665	--	--	--	--	--	--	--	--	Comb.

Asia : 7017 [10 , 33]

Sez. G: Fil8 L=258.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	-3418	--	--	--	--	--	--	--
(12+13)+V1-2									

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	6665	--	--	--	--	--	>100	1.95	>100	1.95

Asia : 7018 [31 , 21]

Sez. G: Fil8 L=309.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
310	1	4876	---	---	---	---	---	---	---	(12+13)+V1-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
310	1	6665	--	--	--	--	--	>100	1.37	>100	1.37

Asia : 7019 [21 , 32]

Sez. G: Fil6 L=387.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
387	1	1581	--	--	--	--	--	--	--	(12+13)+V1-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
387	1	5266	--	--	--	--	--	>100	3.33	>100	3.33

Asia : 7020 [32 , 77]

Sez. G: Fil6 L=353.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1769	--	--	--	--	--	--	--	(12+13)+V1-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.98	>100	2.98

Asia : 7021 [77 , 85]

Sez. G: Fil6 L=306.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-887	--	--	--	--	--	--	--	--	(12+13)+V1-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	5.94	>100	5.94

Asia : 7022 [85 , 81]

Sez. G: Fil6 L=257.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
257	1	2290	--	--	--	--	--	--	--	(12+13)+V1-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
257	1	5266	--	--	--	--	--	>100	2.30	>100	2.30

Asia : 7023 [81 , 21]

Sez. G: Fil6 L=237.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato									
---	--	--	--	--	--	--	--	--	--

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*	kg*	kg*				
238	1	-899	--	--	--	--	--	--	--	--	(12+13)+V11-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
238	1	5266	--	--	--	--	--	>100	5.85	>100	5.85

Asia : 7024 [21 , 9]

Sez. G: Fil6 L=279.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
280	1	-2845	--	--	--	--	--	--	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
280	1	5266	--	--	--	--	--	>100	1.85	>100	1.85

Asia : 7025 [10 , 20]

Sez. G: Fil6 L=279.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3002	--	--	--	--	--	--	--	(12+13)+V1-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	1.75	>100	1.75

Asia : 7026 [20 , 87]

Sez. G: Fil6 L=235.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-815	--	--	--	--	--	--	--	(12+13)+V1-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	6.46	>100	6.46

Asia : 7027 [87 , 79]

Sez. G: Fil6 L=258.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
258	1	-1923	--	--	--	--	--	--	--	--	(12+13)+V1-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
258	1	5266	--	--	--	--	--	>100	2.74	>100	2.74

Asia : 7028 [79 , 83]

Sez. G: Fil6 L=305.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	1042	--	--	--	--	--	--	--	--	(12+13)+V1-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	5.06	>100	5.06

Asia : 7029 [83 , 29]

Sez. G: Fil6 L=354.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	1840	--	--	--	--	--	--	--	--	(12+13)+V1-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.86	>100	2.86
0	1	5266	--	--	--	--	--				

Asia : 7030 [29 , 22]

Sez. G: F116 L=386,5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
386	1	-1702	--	--	--	--	--	--	--	(12+13)-III-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.09	>100	3.09
386	1	5266	--	--	--	--	--				

Asia : 7031 [22 , 32]

Sez. G: F118 L=309,7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
305	1	-4880	--	--	--	--	--	--	--	(12+13)-VI-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.37	>100	1.37
305	1	6665	--	--	--	--	--				

Asia : 7032 [32 , 11]

Sez. G: F118 L=258,9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	3397	--	--	--	--	--	--	--	(12+13)-VI-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.96	>100	1.96
0	1	6665	--	--	--	--	--				

Asia : 7033 [7 , 30]

Sez. G: F118 L=309,5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-3760	--	--	--	--	--	--	--	(12+13)-VI-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.77	>100	1.77
0	1	6665	--	--	--	--	--				

Asia : 7034 [30 , 18]

Sez. G: F118 L=309,5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-5692	--	--	--	--	--	--	--	(12+13)-VI-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.17	>100	1.17
0	1	6665	--	--	--	--	--				

Asia : 7035 [18 , 17]

Sez. G: F116 L=387,0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1954	--	--	--	--	--	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.69	>100	2.69
0	1	5266	--	--	--	--	--				

Asia : 7036 [17 , 65]

Sez. G: F116 L=353,4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
353	1	2204	--	--	--	--	--	--	--	(12+13)-V-III-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.39	>100	2.39
353	1	5266	--	--	--	--	--				

Asia : 7037 [65 , 55]

Sez. G: F116 L=306,1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-533	--	--	--	--	--	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	9.89	>100	9.89
0	1	5266	--	--	--	--	--				

Asia : 7038 [55 , 69]

Sez. G: F116 L=238,6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
259	1	2657	--	--	--	--	--	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.98	>100	1.98
259	1	5266	--	--	--	--	--				

Asia : 7039 [69 , 17]

Sez. G: F116 L=236,5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
237	1	-585	--	--	--	--	--	--	--	(12+13)-VI-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	9.00	>100	9.00
237	1	5266	--	--	--	--	--				

Asia : 7040 [17 , 11]

Sez. G: F116 L=279,9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
275	1	-3267	--	--	--	--	--	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.61	>100	1.61
275	1	5266	--	--	--	--	--				

Asia : 7041 [22 , 57]

Sez. G: F116 L=237,6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-920	--	--	--	--	--	--	--	(12+13)-V-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	5.73	>100	5.73
0	1	5266	--	--	--	--	--				

Asia : 7042 [57 , 67]

Sez. G: F116 L=258,0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm η f=4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
258	1	-2622	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
258	1	5266	--	--	--	--	--	>100	2.01	>100	2.01

Asia : 7043 [67, 53]

Sez. G: Fil16 L=306.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	548	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	9.60	>100	9.60

Asia : 7044 [53, 23]

Sez. G: Fil16 L=353.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
354	1	-2224	--	--	--	--	--	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
354	1	5266	--	--	--	--	--	>100	2.37	>100	2.37

Asia : 7045 [23, 17]

Sez. G: Fil16 L=386.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
387	1	-1764	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
387	1	5266	--	--	--	--	--	>100	2.98	>100	2.98

Asia : 7046 [17, 24]

Sez. G: Fil18 L=309.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
310	1	-5856	--	--	--	--	--	--	--	(12+13)+VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
310	1	6665	--	--	--	--	--	>100	1.14	>100	1.14

Asia : 7047 [24, 6]

Sez. G: Fil18 L=258.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
259	1	-3749	--	--	--	--	--	--	--	(12+13)+VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
259	1	6665	--	--	--	--	--	>100	1.78	>100	1.78

Asia : 7048 [13, 14]

Sez. G: Fil16 L=386.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2314	--	--	--	--	--	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.28	>100	2.28

Asia : 7049 [14, 15]

Sez. G: Fil16 L=386.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	2379	--	--	--	--	--	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.21	>100	2.21

Asia : 7050 [15, 20]

Sez. G: Fil16 L=388.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2491	--	--	--	--	--	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.11	>100	2.11

Asia : 7051 [20, 17]

Sez. G: Fil16 L=388.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
388	1	-2601	--	--	--	--	--	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
388	1	5266	--	--	--	--	--	>100	2.02	>100	2.02

Asia : 7052 [18, 5]

Sez. G: Fil16 L=386.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
387	1	2534	--	--	--	--	--	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
387	1	5266	--	--	--	--	--	>100	2.08	>100	2.08

Asia : 7053 [5, 20]

Sez. G: Fil16 L=386.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
387	1	-2525	--	--	--	--	--	--	--	(12+13)+V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
387	1	5266	--	--	--	--	--	>100	2.09	>100	2.09

Asia : 7054 [20, 29]

Sez. G: Fil16 L=386.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
387	1	2135	--	--	--	--	--	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
387	1	5266	--	--	--	--	--	>100	2.47	>100	2.47

Asia : 7055 [21 , 26]

Sez. G: Fil16 L=386,9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-2336	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.25	>100	2.25

Asia : 7056 [26 , 19]

Sez. G: Fil16 L=386,6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	2268	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.32	>100	2.32

Asia : 7057 [19 , 23]

Sez. G: Fil16 L=386,7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-2609	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.02	>100	2.02

Asia : 7058 [17 , 16]

Sez. G: Fil16 L=389,2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
389	1	-2680	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
389	1	5266	--	--	--	--	--	>100	1.96	>100	1.96

Asia : 7059 [16 , 2]

Sez. G: Fil16 L=389,5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
390	1	2347	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
390	1	5266	--	--	--	--	--	>100	2.24	>100	2.24

Asia : 7060 [2 , 14]

Sez. G: Fil16 L=386,7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
387	1	-2350	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
387	1	5266	--	--	--	--	--	>100	2.24	>100	2.24

Asia : 7061 [14 , 11]

Sez. G: Fil16 L=386,9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
387	1	2041	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
387	1	5266	--	--	--	--	--	>100	2.58	>100	2.58

Asia : 7062 [13 , 51]

Sez. G: Fil16 L=236,6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1928	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.73	>100	2.73

Asia : 7063 [51 , 15]

Sez. G: Fil16 L=236,3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
236	1	-1843	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
236	1	5266	--	--	--	--	--	>100	2.86	>100	2.86

Asia : 7064 [15 , 63]

Sez. G: Fil16 L=262,9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-2489	--	--	--	--	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.12	>100	2.12

Asia : 7065 [63 , 17]

Sez. G: Fil16 L=262,8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
261	1	-2526	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
261	1	5266	--	--	--	--	--	>100	2.08	>100	2.08

Asia : 7066 [22 , 33]

Sez. G: Fil16 L=237,4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-2092	--	--	--	--	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.52	>100	2.52

Asia : 7067 [33 , 19]

Sez. G: Fil16 L=236,8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
237	1	-2083	--	--	--	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.53	>100	2.53
237	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7068 [19 , 81]

Sez. G: F116 L=237.2 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-1611	--	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.27	>100	3.27
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7069 [45 , 14]

Sez. G: F116 L=237.0 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
237	1	-1435	--	--	--	--	--	--	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.67	>100	3.67
237	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7070 [14 , 27]

Sez. G: F116 L=237.2 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-2183	--	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.41	>100	2.41
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7071 [27 , 16]

Sez. G: F116 L=263.6 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
263	1	-2435	--	--	--	--	--	--	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.16	>100	2.16
263	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7072 [16 , 57]

Sez. G: F116 L=263.3 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-2495	--	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.11	>100	2.11
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7073 [69 , 18]

Sez. G: F116 L=263.6 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
236	1	-2130	--	--	--	--	--	--	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.47	>100	2.47
236	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7074 [18 , 75]

Sez. G: F116 L=236.6 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-2013	--	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.62	>100	2.62
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7075 [75 , 20]

Sez. G: F116 L=239.6 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
237	1	-1866	--	--	--	--	--	--	--	--	(12+13)+VII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.82	>100	2.82
237	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7076 [22 , 6]

Sez. G: F116 L=239.9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
280	1	-3260	--	--	--	--	--	--	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.62	>100	1.62
280	1	5266	--	--	--	--	--	--	--	--	--

Asia : 8000 [12 , 7]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-4625	-62	-1504	3	3877	-9	--	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	25.2	4.49	>100	4.49
0	1	201236	86859	37964	19516	9213	462	462	4.49	>100	4.49

Asia : 8000 [7 , 8]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-2712	-77	-870	-2	2721	86	--	--	--	(12+13)+III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	43.7	6.16	>100	6.16
0	1	201236	86947	38003	19516	9213	462	462	6.16	>100	6.16

Asia : 8000 [8 , 9]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
164	1	1118	244	-594	-11	-2398	-258	--	--	--	(12+13)+IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	63.5	6.39	42.5	6.39
164	1	201236	86275	37709	19516	9213	462	462	6.39	42.5	6.39

Asia : 8000 [9 , 35]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
155	1	1366	-44	-438	-3	-2708	-209	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
155	1	201236	86908	37985	19516	9213	462	86.8	5.94	>100	5.94

Asta : 8000 [35 , 36]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
146	1	2561	68	130	0	-2531	-321	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
146	1	201236	87076	38059	19516	9213	462	>100	5.64	>100	5.64

Asta : 8000 [36 , 37]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	2537	-184	594	13	-2531	-352	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86136	37648	19516	9213	462	63.4	5.54	36.5	5.54

Asta : 8000 [37 , 38]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	549	-21	419	11	-2602	-91	--	--	(12+13)+III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86268	37706	19516	9213	462	89.9	6.85	42.2	6.85

Asta : 8000 [38 , 39]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
108	1	-1103	-206	1520	15	2871	159	--	--	(12+13)+IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	201236	85968	37574	19516	9213	462	24.7	5.89	31.0	5.89

Asta : 8000 [39 , 40]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
101	1	-2432	197	695	-17	3642	-21	--	--	(12+13)+IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	201236	85782	37493	19516	9213	462	54.0	4.97	26.7	4.97

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Asta : 8000 [40 , 12]

Sez. G: HE 240 A L=110.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2572	37	-213	-15	3698	-40	--	--	(12+13)+IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	85986	37583	19516	9213	462	>100	4.84	31.6	4.84

Asta : 8001 [13 , 10]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6298	5	-2225	-0	4806	137	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87062	38053	19516	9213	462	17.1	3.42	>100	3.42

Asta : 8001 [10 , 11]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1082	54	-387	-1	2453	193	--	--	(12+13)+I-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87037	38042	19516	9213	462	98.3	6.58	>100	6.58

Asta : 8001 [11 , 12]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
85	1	-3138	19	-1	1	-2571	-80	--	--	(12+13)+III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
85	1	201236	87047	38046	19516	9213	462	>100	6.41	>100	6.41

Asta : 8001 [12 , 41]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3171	-69	500	0	-2558	-83	--	--	(12+13)+III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87074	38058	19516	9213	462	76.1	6.42	>100	6.42

Asta : 8001 [41 , 42]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4111	35	54	-1	-2504	-68	--	--	3

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X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87005	38028	19516	9213	462	>100	6.86	>100	6.86

Asia : 8001 [42 , 43]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
134	1	-650	-215	-520	6	-2169	-182	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
134	1	201236	86673	37883	19516	9213	462	72.9	7.45	82.3	7.45

Asia : 8001 [43 , 44]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
123	1	1073	-117	-399	6	-2827	-85	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
123	1	201236	86622	37860	19516	9213	462	94.9	6.27	73.4	6.27

Asia : 8001 [44 , 45]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
113	1	-2733	155	822	-10	3170	-72	--	--	(12+13)-I-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	201236	86329	37732	19516	9213	462	45.9	5.44	45.5	5.44

Asia : 8001 [45 , 46]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2078	-59	-518	9	3170	-71	--	--	(12+13)-I-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86436	37779	19516	9213	462	73.0	5.54	52.9	5.54

Asia : 8001 [46 , 13]

Sez. G: HE 240 A L=110.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
111	1	-526	65	1470	-15	3863	-60	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
111	1	201236	85920	37554	19516	9213	462	25.5	4.83	29.8	4.83

Asia : 8002 [14 , 13]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-6537	-3	-2256	-1	5059	84	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86999	38025	19516	9213	462	16.9	3.32	>100	3.32

Asia : 8002 [13 , 14]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-2103	-8	-695	0	-2575	-25	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	87085	38063	19516	9213	462	54.7	6.89	>100	6.89

Asia : 8002 [14 , 15]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
85	1	-2193	-3	-44	0	-2663	-63	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
85	1	201236	87070	38056	19516	9213	462	>100	6.49	>100	6.49

Asia : 8002 [15 , 47]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1818	-46	163	1	-1997	-414	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87009	38030	19516	9213	462	>100	6.40	>100	6.40

Asia : 8002 [47 , 48]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
15	1	-3068	33	47	-0	-2566	-37	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
15	1	201236	87094	38067	19516	9213	462	>100	6.64	>100	6.64

Asia : 8002 [48 , 49]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-654	-266	168	4	-1298	-742	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86793	37935	19516	9213	462	>100	6.66	>100	6.66

Asia : 8002 [49 , 50]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

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: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
123	1	1105	-38	-258	1	-2837	-25	--	--	(12+13)+I-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
123	1	201236	86993	38022	19516	9213	462	>100	6.51	>100	6.51

Asia : 8002 [50 , 51]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
113	1	-2684	22	882	-2	3215	-9	--	--	(12+13)+I-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	201236	86923	37992	19516	9213	462	43.1	5.59	>100	5.59

Asia : 8002 [51 , 52]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
108	1	-1748	-13	157	1	3311	-1	--	--	(12+13)+III-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
108	1	201236	86985	38019	19516	9213	462	>100	5.60	>100	5.60

Asia : 8002 [52 , 14]

Sez. G: HE 240 A L=110.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	-1895	-2	1518	-1	4118	9	--	--	6

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	201236	87010	38030	19516	9213	462	25.0	4.52	>100	4.52

Asia : 8003 [15 , 1]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-7001	-26	-2333	-1	5365	23	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87050	38047	19516	9213	462	16.3	3.20	>100	3.20

Asia : 8003 [1 , 2]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-2366	6	-769	0	-2594	0	--	--	(12+13)+III-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	87073	38058	19516	9213	462	49.5	6.91	>100	6.91

Asia : 8003 [2 , 3]

Sez. G: HE 240 A L=169.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
170	1	-2228	-38	10	1	-2741	70	--	--	(12+13)+I-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	201236	87050	38048	19516	9213	462	>100	6.29	>100	6.29

Asia : 8003 [3 , 23]

Sez. G: HE 240 A L=158.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
143	1	-4146	-22	-62	1	-2753	-18	--	--	6

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
143	1	201236	87052	38049	19516	9213	462	>100	6.11	>100	6.11

Asia : 8003 [23 , 24]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3740	8	66	-0	-2764	-15	--	--	6

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87089	38064	19516	9213	462	>100	6.18	>100	6.18

Asia : 8003 [24 , 25]

Sez. G: HE 240 A L=134.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2897	-14	430	-0	-2438	-36	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87092	38066	19516	9213	462	88.6	6.98	>100	6.98

Asia : 8003 [25 , 26]

Sez. G: HE 240 A L=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
123	1	1027	-28	-251	1	-2884	-28	--	--	(12+13)+I-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
123	1	201236	87028	38038	19516	9213	462	>100	6.41	>100	6.41

Asia : 8003 [26 , 27]

Sez. G: HE 240 A L=113.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
113	1	-2847	48	938	-2	3273	-27	--	--	(12+13)+III-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
113	1	201236	86923	37992	19516	9213	462	40.5	5.41	>100	5.41

Asia : 8003 [27 , 28]

Sez. G: HE 240 A L=108.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
108	1	-1959	-24	213	3	3401	-2	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	201236	86903	37983	19516	9213	462	>100	5.43	>100	5.43

Asia : 8003 [28 , 15]

Sez. G: HE 240 A L=110.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
111	1	-2292	-2	1723	-0	4478	7	--	--	6

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
111	1	201236	87076	38059	19516	9213	462	22.1	4.14	>100	4.14

Asia : 8004 [16 , 19]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-7330	-33	-2394	-0	5577	5	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87065	38054	19516	9213	462	15.9	3.10	>100	3.10

Asia : 8004 [19 , 20]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
18	1	-1864	-37	-520	0	2531	122	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
18	1	201236	87085	38063	19516	9213	462	73.2	6.57	>100	6.57

Asia : 8004 [20 , 21]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
170	1	-2316	411	-150	-2	-2252	-368	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	86910	37986	19516	9213	462	>100	5.99	>100	5.99

Asia : 8004 [21 , 59]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
159	1	-4409	-13	-100	0	-2879	-13	--	--	3

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X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
159	1	201236	87084	38063	19516	9213	462	>100	5.85	>100	5.85

Asia : 8004 [59 , 60]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4021	-1	-16	-0	-2879	-15	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87094	38067	19516	9213	462	>100	5.91	>100	5.91

Asia : 8004 [60 , 61]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3328	-9	422	0	-2574	-16	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87083	38062	19516	9213	462	90.1	6.66	>100	6.66

Asia : 8004 [61 , 62]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
123	1	794	-35	-222	1	-2841	-39	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
123	1	201236	87057	38050	19516	9213	462	>100	6.50	>100	6.50

Asia : 8004 [62 , 63]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
113	1	-2867	64	971	-3	3220	-21	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	201236	86854	37962	19516	9213	462	39.1	5.51	>100	5.51

Asia : 8004 [63 , 64]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
108	1	-2175	-21	226	4	3413	-17	--	--	(12+13)-III-4

X	cls	Nr	Vyr	Vzr	Mrv	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	201236	86819	37946	19516	9213	462	>100	5.33	>100	5.33

Asia : 8004 [64 , 16]

Sez. G: HE 240 A L=110.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

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X	cls	Nr	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
111	1	-2713	2	1864	0	4741	1	--	--	6
X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
111	1	201236	87085	38063	19516	9213	462	20.4	3.90	>100

Asia : 8005 [17 , 16]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6512	-7	-2374	-0	5464	32	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	87096	38068	19516	9213	462	16.0	3.17	>100

Asia : 8005 [16 , 17]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2042	-24	-514	-0	2737	111	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	87082	38061	19516	9213	462	74.0	6.16	>100

Asia : 8005 [17 , 18]

Sez. G: HE 240 A L=169.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
168	1	-1156	325	-280	-6	-2314	-295	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
168	1	201236	86669	37881	19516	9213	462	>100	6.40	81.6

Asia : 8005 [18 , 53]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
156	1	-3439	1	-94	-0	-2860	-11	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
156	1	201236	87078	38060	19516	9213	462	>100	6.07	>100

Asia : 8005 [53 , 54]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3418	-10	19	0	-2859	-10	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	87069	38056	19516	9213	462	>100	6.08	>100

Asia : 8005 [54 , 55]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
39	1	1360	-123	-278	5	-2162	-278	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
39	1	201236	86719	37903	19516	9213	462	>100	6.77	92.2

Asia : 8005 [55 , 56]

Sez. G: HE 240 A L=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
118	1	818	-18	-98	1	-2840	-21	--	--	(12+13)-VII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
118	1	201236	87007	38029	19516	9213	462	>100	6.59	>100

Asia : 8005 [56 , 57]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
107	1	-2621	-166	1215	12	3180	58	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
107	1	201236	86189	37671	19516	9213	462	31.0	5.49	38.6

Asia : 8005 [57 , 58]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2620	25	-361	-10	3157	44	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86332	37733	19516	9213	462	>100	5.57	45.7

Asia : 8005 [58 , 17]

Sez. G: HE 240 A L=110.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
114	1	-2219	-6	1924	1	4802	5	--	--	6

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
114	1	201236	87043	38044	19516	9213	462	19.8	3.88	>100

Asia : 8006 [18 , 22]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6954	-12	-2252	0	5137	-9	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mtr
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	87081	38061	19516	9213	462	16.9	3.35	>100

Asia : 8006 [22 , 23]

Sez. G: HE 240 A L=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*		
0	1	-1657	-59	-530	1	2589	-47	--	(12+13)-VII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87049	38047	19516	9213	462	71.7	6.85	>100	6.85

Asia : 8006 [23 , 24]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			
170	1	-1843	-313	-237	3	-2294	308	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
170	1	201236	86853	37961	19516	9213	462	>100	6.25	>100	6.25

Asia : 8006 [24 , 65]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			
0	1	-1633	52	78	0	-2294	321	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87092	38066	19516	9213	462	>100	6.23	>100	6.23

Asia : 8006 [65 , 66]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			
0	1	-3201	-6	32	0	-2633	15	--	6

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87094	38067	19516	9213	462	>100	6.56	>100	6.56

Asia : 8006 [66 , 67]

Sez. G: HE 240 A L=134.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			
0	1	1352	237	224	-6	-1706	581	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86621	37860	19516	9213	462	>100	6.36	73.3	6.36

Asia : 8006 [67 , 68]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			
123	1	824	-9	-230	1	-2730	-27	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
123	1	201236	87027	38037	19516	9213	462	>100	6.81	>100	6.81

Asia : 8006 [68 , 69]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			
113	1	-2160	255	1234	-12	3233	-122	--	(12+13)-I-3

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
113	1	201236	86220	37685	19516	9213	462	30.6	5.27	39.9	5.27

Asia : 8006 [69 , 70]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			
0	1	-2337	-87	-243	13	3222	-115	--	(12+13)-I-3

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86106	37635	19516	9213	462	>100	5.28	35.3	5.28

Asia : 8006 [70 , 22]

Sez. G: HE 240 A L=110.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			
111	1	-1911	-7	1651	2	4382	7	--	6

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
111	1	201236	86977	38016	19516	9213	462	23.0	4.26	>100	4.26

Asia : 8007 [19 , 4]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			
0	1	-6562	3	-2237	0	5041	-19	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87077	38059	19516	9213	462	17.0	3.41	>100	3.41

Asia : 8007 [4 , 5]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			
0	1	-1726	-72	-491	0	2554	-100	--	(12+13)-VII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mtr	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87064	38054	19516	9213	462	77.6	6.65	>100	6.65

Asia : 8007 [5 , 6]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
170	1	-1755	-345	-158	2	-2041	401	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	86932	37996	19516	9213	462	>100	6.38	>100	6.38

Asta : 8007 [6 , 29]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1774	56	142	-1	-2041	421	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87040	38043	19516	9213	462	>100	6.29	>100	6.29

Asta : 8007 [29 , 30]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3232	-4	62	-0	-2588	35	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87081	38061	19516	9213	462	>100	6.56	>100	6.56

Asta : 8007 [30 , 31]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-624	264	56	-4	-1317	720	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86770	37925	19516	9213	462	>100	6.72	>100	6.72

Asta : 8007 [31 , 32]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
123	1	960	-17	-216	0	-2692	-32	--	--	(12+13)-VII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
123	1	201236	87087	38063	19516	9213	462	>100	6.84	>100	6.84

Asta : 8007 [32 , 33]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
113	1	-2520	72	869	-2	3059	-30	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	201236	86954	38006	19516	9213	462	43.8	5.80	>100	5.80

Asta : 8007 [33 , 34]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
108	1	-1673	-12	173	3	3199	-12	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	201236	86865	37967	19516	9213	462	>100	5.76	>100	5.76

Asta : 8007 [34 , 18]

Sez. G: HE 240 A L=110.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
111	1	-1904	-7	1345	2	4169	3	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
111	1	201236	86925	37993	19516	9213	462	24.6	4.48	>100	4.48

Asta : 8008 [20 , 25]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6409	37	-2215	1	4964	-1	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87039	38043	19516	9213	462	17.2	3.49	>100	3.49

Asta : 8008 [25 , 26]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1765	-84	-439	1	2484	-155	--	--	(12+13)-VII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87032	38040	19516	9213	462	86.6	6.54	>100	6.54

Asta : 8008 [26 , 27]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
170	1	-4511	-88	-465	-0	-2199	136	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	87097	38068	19516	9213	462	81.8	6.67	>100	6.67

Asta : 8008 [27 , 71]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
95	1	-3808	50	-151	-1	-2471	95	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
95	1	201236	87001	38026	19516	9213	462	>100	6.42	>100	6.42

Asia : 8008 [71 , 72]

Sez. G: HE 240 A L=147,9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
148	1	-1797	-175	-83	5	-1376	694	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
148	1	201236	86706	37897	19516	9213	462	>100	6.46	89.2	6.46

Asia : 8008 [72 , 73]

Sez. G: HE 240 A L=134,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-138	348	-82	-6	-1365	794	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86664	37879	19516	9213	462	>100	6.38	80.5	6.38

Asia : 8008 [73 , 74]

Sez. G: HE 240 A L=122,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	653	141	-134	-5	-2022	311	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86743	37913	19516	9213	462	>100	7.11	98.6	7.11

Asia : 8008 [74 , 75]

Sez. G: HE 240 A L=113,2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
113	1	-2392	64	820	-2	2960	-20	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
113	1	201236	86977	38016	19516	9213	462	46.3	6.03	>100	6.03

Asia : 8008 [75 , 76]

Sez. G: HE 240 A L=108,1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
108	1	-1615	-3	199	4	3133	-14	--	--	(12+13)-VII-4

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
108	1	201236	86778	37929	19516	9213	462	>100	5.88	>100	5.88

Asia : 8008 [76 , 79]

Sez. G: HE 240 A L=110,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
111	1	-1877	-2	1482	3	4001	-4	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				

465

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
111	1	201236	86868	37968	19516	9213	462	25.6	4.66	>100	4.66

Asia : 8009 [21 , 28]

Sez. G: HE 240 A L=181,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-6124	36	-2134	1	4696	-35	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87058	38051	19516	9213	462	17.8	3.64	>100	3.64

Asia : 8009 [28 , 29]

Sez. G: HE 240 A L=177,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-1546	-117	-777	1	2285	-222	--	--	(12+13)-VII-1

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87031	38039	19516	9213	462	48.9	6.72	>100	6.72

Asia : 8009 [29 , 30]

Sez. G: HE 240 A L=169,8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
170	1	-5005	-108	-357	-0	-2008	187	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
170	1	201236	87096	38068	19516	9213	462	>100	6.75	>100	6.75

Asia : 8009 [30 , 77]

Sez. G: HE 240 A L=158,5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
63	1	-4415	64	-170	-1	-2169	156	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
63	1	201236	87033	38040	19516	9213	462	>100	6.67	>100	6.67

Asia : 8009 [77 , 78]

Sez. G: HE 240 A L=147,9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-4184	-5	34	1	-2200	104	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87046	38046	19516	9213	462	>100	6.91	>100	6.91

Asia : 8009 [78 , 79]

Sez. G: HE 240 A L=134,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-2131	293	-328	-8	-1195	621	--	--	(12+13)-IV-3

466

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86529	37820	19516	9213	462	>100	7.18	61.5	7.18

Asia.: 8009 [79 , 80]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
123	1	944	102	-307	-7	-2435	96	--	--	(12+13)+VII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
123	1	201236	86600	37851	19516	9213	462	>100	7.15	70.2	7.15

Asia.: 8009 [80 , 81]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
113	1	-2418	-200	776	12	2626	105	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	201236	86218	37684	19516	9213	462	48.6	6.33	39.8	6.33

Asia.: 8009 [81 , 82]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
108	1	-1137	-3	631	4	3007	18	--	--	(12+13)+VII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
108	1	201236	86796	37937	19516	9213	462	60.1	6.19	>100	6.19

Asia.: 8009 [82 , 20]

Sez. G: HE 240 A L=110.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
111	1	-1476	-2	1694	4	3958	-4	--	--	6

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
111	1	201236	86807	37941	19516	9213	462	22.4	4.75	>100	4.75

Asia.: 8010 [22 , 31]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3063	16	-935	1	4156	18	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86991	38022	19516	9213	462	40.7	4.35	>100	4.35

Asia.: 8010 [31 , 32]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2175	-150	-420	0	2243	-271	--	--	(12+13)+VII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87070	38056	19516	9213	462	90.6	6.45	>100	6.45

Asia.: 8010 [32 , 33]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
170	1	1387	-257	-577	7	-2220	304	--	--	(12+13)+III-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	201236	86560	37834	19516	9213	462	65.6	6.51	65.1	6.51

Asia.: 8010 [33 , 83]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
159	1	1506	71	-615	3	-2520	228	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
159	1	201236	86894	37979	19516	9213	462	61.7	6.20	>100	6.20

Asia.: 8010 [83 , 84]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
148	1	2593	-58	-68	1	-2638	326	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
148	1	201236	87019	38034	19516	9213	462	>100	5.45	>100	5.45

Asia.: 8010 [84 , 85]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2620	207	488	-15	-2638	355	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	85970	37575	19516	9213	462	77.0	5.36	31.1	5.36

Asia.: 8010 [85 , 86]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	554	46	650	-10	-2434	92	--	--	(12+13)+III-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86360	37746	19516	9213	462	58.1	7.27	47.5	7.27

Asia.: 8010 [86 , 87]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
113	1	-1076	86	1406	-72	2929	-9	-7	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
113	1	201236	86442	37782	19516	9213	462	26.9	6.13	53.4

Asta : 8010 [87 , 88]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
108	1	-2342	-62	515	10	3463	12	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
108	1	201236	86350	37742	19516	9213	462	73.2	5.25	46.8

Asta : 8010 [88 , 21]

Sez. G: HE 240 A L=110.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
111	1	-2505	-40	89	13	3488	27	--	--	--	(12+13)-V-3

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
111	1	201236	86141	37650	19516	9213	462	>100	5.15	36.6

Asta : 8013 [28 , 25]

Sez. G: IPE 100 L=149.6 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
150	1	584	3	6	-0	0	-3	--	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
150	1	27037	9477	7685	1033	240	27	>100	30.2	>100

Asta : 8013 [25 , 27]

Sez. G: IPE 100 L=149.9 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
60	1	1057	0	-1	-0	-2	-2	--	--	--	(12+13)-VIII-2

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
60	1	27037	9480	7688	1033	240	27	>100	21.1	>100

Asta : 8013 [27 , 23]

Sez. G: IPE 100 L=148.8 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
45	1	986	-1	-3	0	-2	-0	--	--	--	6

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
45	1	27037	9479	7688	1033	240	27	>100	25.1	>100

Asta : 8013 [23 , 29]

Sez. G: IPE 100 L=149.9 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
75	1	967	-0	0	0	-3	0	--	--	--	3

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
75	1	27037	9480	7688	1033	240	27	>100	25.7	>100

Asta : 8013 [29 , 30]

Sez. G: IPE 100 L=149.3 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
149	1	852	7	6	-0	0	-8	--	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
149	1	27037	9480	7688	1033	240	27	>100	15.7	>100

Asta : 8013 [30 , 24]

Sez. G: IPE 100 L=149.6 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
45	1	1237	-1	-3	-0	-2	-3	--	--	--	6

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
45	1	27037	9479	7687	1033	240	27	>100	16.7	>100

Asta : 8013 [24 , 26]

Sez. G: IPE 100 L=149.4 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
0	1	697	7	-7	0	0	8	--	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	27037	9481	7689	1033	240	27	>100	16.8	>100

Asta : 8013 [26 , 31]

Sez. G: IPE 100 L=149.2 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
0	1	1069	-4	-7	-0	0	-4	--	--	--	6

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	27037	9480	7689	1033	240	27	>100	17.2	>100

Asta : 8013 [31 , 32]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
150	1	852	-7	6	0	0	7	--	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mtr	Mtrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*			
150	1	27037	9480	7688	1033	240	27	>100	16.0	>100

Asta : 8013 [32 , 33]

Sez. G: IPE 100 L=150.0 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
150	1	512	6	6	0	0	-11	--	--	--	(12+13)-VI-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
150	1	27037	9478	7686	1033	240	27	>100	15.2	>100	15.2

Asia : 8014 [12 , 13]

Sez. G: IPE 100 L=149,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	2002	-20	-64	-0	0	-20	--	--	(12+13)>VL-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9475	7684	1033	240	27	>100	6.39	>100	6.39

Asia : 8014 [13 , 14]

Sez. G: IPE 100 L=149,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	3935	-30	54	-0	0	28	--	--	(12+13)>VL-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9478	7687	1033	240	27	>100	3.78	>100	3.78

Asia : 8014 [14 , 15]

Sez. G: IPE 100 L=148,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	2467	-49	-54	-0	0	-37	--	--	(12+13)>VL-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9479	7688	1033	240	27	>100	4.05	>100	4.05

Asia : 8014 [15 , 16]

Sez. G: IPE 100 L=149,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	2082	-9	37	0	-63	2	--	--	6	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9481	7689	1033	240	27	>100	6.84	>100	6.84

Asia : 8014 [16 , 17]

Sez. G: IPE 100 L=149,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
81	1	2043	1	1	-0	-75	0	--	--	3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
81	1	27037	9481	7689	1033	240	27	>100	6.72	>100	6.72

Asia : 8014 [17 , 18]

Sez. G: IPE 100 L=149,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
83	1	2111	6	34	0	-53	-1	--	--	6	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
83	1	27037	9481	7689	1033	240	27	>100	7.50	>100	7.50

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Asia : 8014 [18 , 19]

Sez. G: IPE 100 L=149,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	2021	1	1	-0	-66	-0	--	--	6	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	27037	9481	7689	1033	240	27	>100	7.18	>100	7.18

Asia : 8014 [19 , 20]

Sez. G: IPE 100 L=149,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	1800	21	-58	-0	0	17	--	--	(12+13)>VIII-2	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9479	7687	1033	240	27	>100	7.32	>100	7.32

Asia : 8014 [20 , 21]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	3197	24	52	-0	0	-18	--	--	(12+13)>VI-2	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9479	7688	1033	240	27	>100	5.16	>100	5.16

Asia : 8014 [21 , 22]

Sez. G: IPE 100 L=150,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	1926	25	-59	0	0	19	--	--	(12+13)>VI-2	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9475	7684	1033	240	27	>100	6.71	>100	6.71

Asia : 8015 [7 , 10]

Sez. G: IPE 100 L=143,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	114	-8	-66	-0	-114	-7	--	--	6	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9475	7684	1033	240	27	>100	6.97	>100	6.97

Asia : 8015 [10 , 13]

Sez. G: IPE 100 L=143,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
72	1	147	-5	0	-0	-118	-1	--	--	6	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
72	1	27037	9480	7688	1033	240	27	>100	8.00	>100	8.00

Asia : 8015 [13 , 1]

Sez. G: IPE 100 L=142,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
71	1	158	-2	0	-0	-116	0	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
71	1	27037	9479	7688	1033	240	27	>100	8.38	>100	8.38

Asta : 8015 [16 , 19]

Sez. G: IPE 100 L=149,8 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	189	-4	-0	-0	-128	1	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	27037	9480	7688	1033	240	27	>100	7.53	>100	7.53

Asta : 8015 [19 , 16]

Sez. G: IPE 100 L=149,3 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	238	0	-0	0	-127	1	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	27037	9480	7689	1033	240	27	>100	7.40	>100	7.40

Asta : 8015 [16 , 22]

Sez. G: IPE 100 L=143,6 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
72	1	261	0	1	0	-117	-0	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
72	1	27037	9479	7687	1033	240	27	>100	8.12	>100	8.12

Asta : 8015 [22 , 4]

Sez. G: IPE 100 L=143,4 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
72	1	289	1	0	0	-117	-0	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
72	1	27037	9481	7689	1033	240	27	>100	7.93	>100	7.93

Asta : 8015 [4 , 25]

Sez. G: IPE 100 L=143,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
72	1	284	-0	1	0	-116	-0	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
72	1	27037	9480	7689	1033	240	27	>100	8.04	>100	8.04

Asta : 8015 [25 , 28]

Sez. G: IPE 100 L=143,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
72	1	222	3	1	0	-116	-0	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
72	1	27037	9479	7687	1033	240	27	>100	8.14	>100	8.14

Asta : 8015 [28 , 31]

Sez. G: IPE 100 L=143,9 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
72	1	142	2	1	0	-116	-1	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
72	1	27037	9477	7685	1033	240	27	>100	8.18	>100	8.18

Asta : 8016 [8 , 11]

Sez. G: IPE 100 L=137,7 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
138	1	-713	31	96	-0	0	-27	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
138	1	27037	9464	7675	1033	240	27	80.3	7.11	>100	7.11

Asta : 8016 [11 , 14]

Sez. G: IPE 100 L=137,8 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
55	1	-143	-8	-61	-0	-101	-4	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
55	1	27037	9478	7687	1033	240	27	>100	8.49	>100	8.49

Asta : 8016 [14 , 2]

Sez. G: IPE 100 L=136,9 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
68	1	-615	-3	0	-0	-103	1	--		6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
68	1	27037	9479	7687	1033	240	27	>100	7.84	>100	7.84

Asta : 8016 [2 , 20]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-918	-5	-0	-0	-123	-1	--		6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	27037	9479	7688	1033	240	27	>100	6.43	>100	6.43

Asta : 8016 [20 , 17]

Sez. G: IPE 100 L=149,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
75	1	-1045	1	-0	0	-123	0	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
75	1	27037	9480	7688	1033	240	27	>100	6.31	>100	6.31

Asia : 8016 [17 , 23]

Sez. G: IPE 100 L=137,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
69	1	-1027	-1	1	0	-104	0	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
69	1	27037	9479	7687	1033	240	27	>100	7.22	>100	7.22

Asia : 8016 [23 , 5]

Sez. G: IPE 100 L=137,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
69	1	-941	2	0	0	-104	-0	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
69	1	27037	9480	7688	1033	240	27	>100	7.36	>100	7.36

Asia : 8016 [5 , 26]

Sez. G: IPE 100 L=137,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
69	1	-685	-0	0	0	-103	-1	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
69	1	27037	9480	7688	1033	240	27	>100	7.84	>100	7.84

Asia : 8016 [26 , 29]

Sez. G: IPE 100 L=137,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
69	1	-323	2	1	0	-103	-1	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
69	1	27037	9478	7687	1033	240	27	>100	8.61	>100	8.61

Asia : 8016 [29 , 32]

Sez. G: IPE 100 L=137,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-858	-23	-92	0	0	-22	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9465	7676	1033	240	27	83.2	8.07	>100	8.07

Asia : 8017 [9 , 12]

Sez. G: IPE 100 L=131,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
39	1	-145	21	-111	0	-76	0	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
39	1	27037	9478	7687	1033	240	27	69.4	9.65	>100	9.65

Asia : 8017 [12 , 15]

Sez. G: IPE 100 L=131,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

475

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-89	-47	-86	-0	0	-39	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9477	7686	1033	240	27	88.9	6.04	>100	6.04

Asia : 8017 [15 , 3]

Sez. G: IPE 100 L=131,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
65	1	-464	6	0	-0	-89	1	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
65	1	27037	9479	7687	1033	240	27	>100	9.30	>100	9.30

Asia : 8017 [3 , 21]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	-557	0	-0	-0	-117	-0	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	27037	9480	7688	1033	240	27	>100	7.38	>100	7.38

Asia : 8017 [21 , 18]

Sez. G: IPE 100 L=149,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	-170	48	96	-0	0	-44	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9479	7688	1033	240	27	79.7	5.28	>100	5.28

Asia : 8017 [18 , 24]

Sez. G: IPE 100 L=131,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
66	1	-616	-3	0	0	-90	1	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
66	1	27037	9480	7688	1033	240	27	>100	8.95	>100	8.95

Asia : 8017 [24 , 6]

Sez. G: IPE 100 L=131,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-133	55	-86	-0	0	43	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	89.9	5.42	>100	5.42

Asia : 8017 [6 , 27]

Sez. G: IPE 100 L=131,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
66	1	-482	-5	0	0	-89	-1	--	--	6	

476

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
66	1	27037	9480	7688	1033	240	27	>100	9.36	>100	9.36

Asia : 8017 [27 , 30]

Sez. G: IPE 100 L=131,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	-97	-48	83	-0	0	37	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9478	7687	1033	240	27	92.7	6.41	>100	6.41

Asia : 8017 [30 , 33]

Sez. G: IPE 100 L=131,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
79	1	-175	-17	56	-0	-85	4	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
79	1	27037	9479	7688	1033	240	27	>100	9.47	>100	9.47

Asia : 8018 [35 , 41]

Sez. G: IPE 100 L=125,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
38	1	-668	12	-32	-0	-21	15	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
38	1	27037	9481	7689	1033	240	27	>100	9.33	>100	9.33

Asia : 8018 [41 , 47]

Sez. G: IPE 100 L=125,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-920	63	-77	0	0	47	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9476	7685	1033	240	27	99.6	4.38	>100	4.38

Asia : 8018 [47 , 23]

Sez. G: IPE 100 L=125,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	-447	36	75	0	0	-27	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	27037	9478	7687	1033	240	27	>100	7.66	>100	7.66

Asia : 8018 [23 , 59]

Sez. G: IPE 100 L=149,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-438	-31	-90	0	0	-27	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9480	7688	1033	240	27	85.3	7.72	>100	7.72

Asia : 8018 [59 , 53]

Sez. G: IPE 100 L=149,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	-963	-58	90	0	0	50	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9480	7688	1033	240	27	85.0	4.09	>100	4.09

Asia : 8018 [53 , 65]

Sez. G: IPE 100 L=125,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
63	1	-569	-3	0	0	-76	0	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
63	1	27037	9481	7689	1033	240	27	>100	10.3	>100	10.3

Asia : 8018 [65 , 29]

Sez. G: IPE 100 L=125,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-484	76	-76	-0	0	55	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9479	7687	1033	240	27	>100	4.06	>100	4.06

Asia : 8018 [29 , 71]

Sez. G: IPE 100 L=125,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
63	1	-621	-3	0	0	-76	-1	--	--	6	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
63	1	27037	9481	7689	1033	240	27	>100	9.95	>100	9.95

Asia : 8018 [71 , 77]

Sez. G: IPE 100 L=125,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	-1079	-62	74	-0	0	46	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	27037	9476	7685	1033	240	27	>100	4.29	>100	4.29

Asia : 8018 [77 , 83]

Sez. G: IPE 100 L=125,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
101	1	-689	-11	47	-0	-15	16	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
101	1	27037	9478	7686	1033	240	27	>100	9.46	>100	9.46

Asia : 8019 [36 , 42]

Sez. G: IPE 100 L=119,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-42	53	-69	-0	0	41	--	--	(12+13)+V1-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9473	7683	1033	240	27	>100	5.78	>100	5.78

Astia : 8019 [42, 48]

Sez. G: IPE 100 L=119,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-147	114	-68	0	0	74	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9473	7683	1033	240	27	83.0	3.20	>100	3.20

Astia : 8019 [48, 24]

Sez. G: IPE 100 L=119,1 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
119	1	-164	84	66	0	0	-52	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9477	7686	1033	240	27	>100	4.51	>100	4.51

Astia : 8019 [24, 60]

Sez. G: IPE 100 L=149,6 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-48	63	-84	-0	0	48	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7688	1033	240	27	91.9	4.94	>100	4.94

Astia : 8019 [60, 54]

Sez. G: IPE 100 L=149,1 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
149	1	-190	-86	84	-0	0	68	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9477	7685	1033	240	27	91.7	3.44	>100	3.44

Astia : 8019 [54, 66]

Sez. G: IPE 100 L=119,8 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-321	-27	-66	0	0	-18	--	--	(12+13)-V1-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9473	7682	1033	240	27	>100	11.8	>100	11.8

Astia : 8019 [66, 30]

Sez. G: IPE 100 L=119,4 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-332	-119	-67	-0	0	-75	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9474	7683	1033	240	27	79.8	3.06	>100	3.06

Astia : 8019 [30, 72]

Sez. G: IPE 100 L=119,2 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
119	1	-311	-81	65	-0	0	50	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9476	7685	1033	240	27	>100	4.57	>100	4.57

Astia : 8019 [72, 78]

Sez. G: IPE 100 L=119,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
120	1	-132	-115	65	-0	0	73	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
120	1	27037	9474	7683	1033	240	27	82.6	3.24	>100	3.24

Astia : 8019 [78, 84]

Sez. G: IPE 100 L=119,6 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
120	1	-74	-51	64	0	0	39	--	--	(12+13)-V1-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
120	1	27037	9472	7682	1033	240	27	>100	5.99	>100	5.99

Astia : 8020 [37, 43]

Sez. G: IPE 100 L=113,7 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-361	41	-60	-0	0	29	--	--	(12+13)+I1-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9463	7674	1033	240	27	>100	7.36	>100	7.36

Astia : 8020 [43, 49]

Sez. G: IPE 100 L=113,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-440	102	-59	0	0	60	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9474	7684	1033	240	27	93.3	3.74	>100	3.74

Astia : 8020 [49, 25]

Sez. G: IPE 100 L=113,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
113	1	-166	89	57	0	0	-51	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27037	9479	7687	1033	240	27	>100	4.60	>100	4.60

Asia : 8020 [25 , 61]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	183	61	77	-0	0	-46	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9480	7688	1033	240	27	99.8	5.05	>100	5.05

Asia : 8020 [61 , 55]

Sez. G: IPE 100 L=149,1 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	-748	-72	77	-0	0	55	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9475	7684	1033	240	27	>100	3.91	>100	3.91

Asia : 8020 [55 , 67]

Sez. G: IPE 100 L=113,8 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-201	-33	-57	0	0	-19	--	--	(12+13)+VI-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9466	7677	1033	240	27	>100	11.5	>100	11.5

Asia : 8020 [67 , 31]

Sez. G: IPE 100 L=113,4 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	336	-108	-58	-0	0	-64	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9473	7682	1033	240	27	87.4	3.59	>100	3.59

Asia : 8020 [31 , 73]

Sez. G: IPE 100 L=113,2 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27	-82	57	0	0	47	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27037	9479	7688	1033	240	27	>100	5.08	>100	5.08

Asia : 8020 [73 , 79]

Sez. G: IPE 100 L=113,6 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
114	1	-369	-98	56	-0	0	58	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
114	1	27037	9475	7684	1033	240	27	96.8	3.90	>100	3.90

Asia : 8020 [79 , 85]

Sez. G: IPE 100 L=113,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
113	1	-365	-30	56	0	0	20	--	--	(12+13)+II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27037	9462	7674	1033	240	27	>100	10.2	>100	10.2

Asia : 8021 [38 , 44]

Sez. G: IPE 100 L=107,7 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-161	28	-53	-0	0	17	--	--	(12+13)+VI-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9462	7674	1033	240	27	>100	13.0	>100	13.0

Asia : 8021 [44 , 50]

Sez. G: IPE 100 L=107,4 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-58	82	-51	0	0	45	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7687	1033	240	27	>100	5.32	>100	5.32

Asia : 8021 [50 , 26]

Sez. G: IPE 100 L=107,3 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	15	90	50	-0	0	-50	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9480	7688	1033	240	27	>100	4.81	>100	4.81

Asia : 8021 [26 , 62]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	-125	57	71	0	0	-43	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9480	7688	1033	240	27	>100	5.47	>100	5.47

Asia : 8021 [62 , 56]

Sez. G: IPE 100 L=149,0 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	178	-56	-71	-0	0	-42	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9477	7685	1033	240	27	>100	5.44	>100	5.44

Asia : 8021 [56 , 68]

Sez. G: IPE 100 L=107,8 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	80	-43	49	0	0	24	--	--	(12+13)+VI-3	

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
108	1	27037	9466	7677	1033	240	27	>100	9.76	>100	9.76

Asia : 8021 [68 , 32]

Sez. G: IPE 100 L=107.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
0	1	124	-95	-51	-0	0	-52		--	--	(12+13)>IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9476	7685	1033	240	27	>100	4.51	>100	4.51

Asia : 8021 [32 , 74]

Sez. G: IPE 100 L=107.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
107	1	90	-82	49	0	0	44		--	--	(12+13)>IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	27037	9479	7688	1033	240	27	>100	5.34	>100	5.34

Asia : 8021 [74 , 80]

Sez. G: IPE 100 L=107.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
108	1	59	-81	49	-0	0	44		--	--	(12+13)>VIII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
108	1	27037	9481	7689	1033	240	27	>100	5.34	>100	5.34

Asia : 8021 [80 , 86]

Sez. G: IPE 100 L=107.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
107	1	35	-24	48	0	0	14		--	--	(12+13)>VI-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	27037	9462	7674	1033	240	27	>100	16.9	>100	16.9

Asia : 8022 [39 , 45]

Sez. G: IPE 100 L=101.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
0	1	-1683	23	-47	0	0	12		--	--	(12+13)>IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9469	7679	1033	240	27	>100	8.75	>100	8.75

Asia : 8022 [45 , 51]

Sez. G: IPE 100 L=101.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
0	1	2826	50	-46	-0	0	25		--	--	(12+13)>IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9473	7682	1033	240	27	>100	4.74	>100	4.74

Asia : 8022 [51 , 27]

Sez. G: IPE 100 L=101.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
0	1	1955	54	-45	-0	0	27		--	--	(12+13)>IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9476	7685	1033	240	27	>100	5.35	>100	5.35

Asia : 8022 [27 , 63]

Sez. G: IPE 100 L=149.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
0	1	678	23	-67	0	0	18		--	--	(12+13)>IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9480	7688	1033	240	27	>100	10.1	>100	10.1

Asia : 8022 [63 , 57]

Sez. G: IPE 100 L=149.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
149	1	1369	-24	67	-0	0	18		--	--	(12+13)>IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
149	1	27037	9480	7688	1033	240	27	>100	7.88	>100	7.88

Asia : 8022 [57 , 69]

Sez. G: IPE 100 L=101.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
31	1	1363	-6	-19	0	-10	-1		--	--	(12+13)>II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
31	1	27037	9474	7684	1033	240	27	>100	15.2	>100	15.2

Asia : 8022 [69 , 33]

Sez. G: IPE 100 L=101.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
101	1	512	-56	44	0	0	29		--	--	(12+13)>IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
101	1	27037	9476	7685	1033	240	27	>100	7.20	>100	7.20

Asia : 8022 [33 , 75]

Sez. G: IPE 100 L=101.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
0	1	1457	-53	-44	0	0	-27		--	--	(12+13)>IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9475	7684	1033	240	27	>100	6.01	>100	6.01

Asia : 8022 [75 , 81]

Sez. G: IPE 100 L=101.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mry	Mrz	MTrd	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
102	1	2343	-46	43	0	0	24	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
102	1	27037	9473	7683	1033	240	27	>100	5.38	>100	5.38

Asia : 8022 [81 , 87]

Sez. G: IPE 100 L=101,4 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1065	-19	-43	-0	0	-10	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9469	7680	1033	240	27	>100	12.4	>100	12.4

Asia : 8023 [40 , 46]

Sez. G: IPE 100 L=95,7 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201	19	-44	-0	0	9	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9477	7685	1033	240	27	>100	21.8	>100	21.8

Asia : 8023 [46 , 52]

Sez. G: IPE 100 L=95,3 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-54	65	-42	-0	0	31	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9470	7680	1033	240	27	>100	7.58	>100	7.58

Asia : 8023 [52 , 58]

Sez. G: IPE 100 L=95,5 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-19	66	-41	-0	0	32	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9477	7686	1033	240	27	>100	7.48	>100	7.48

Asia : 8023 [28 , 64]

Sez. G: IPE 100 L=149,4 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	217	-23	-66	-0	0	-18	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9480	7689	1033	240	27	>100	12.3	>100	12.3

Asia : 8023 [64 , 58]

Sez. G: IPE 100 L=149,0 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
149	1	264	-26	66	0	0	20	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9477	7686	1033	240	27	>100	10.7	>100	10.7

Asia : 8023 [58 , 70]

Sez. G: IPE 100 L=95,9 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
38	1	100	-6	-27	-0	-30	-1	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
38	1	27037	9479	7687	1033	240	27	>100	28.0	>100	28.0

Asia : 8023 [70 , 34]

Sez. G: IPE 100 L=95,4 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
95	1	174	-71	41	0	0	34	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
95	1	27037	9472	7682	1033	240	27	>100	6.71	>100	6.71

Asia : 8023 [34 , 76]

Sez. G: IPE 100 L=95,2 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
95	1	97	-68	40	0	0	32	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
95	1	27037	9476	7685	1033	240	27	>100	7.19	>100	7.19

Asia : 8023 [76 , 82]

Sez. G: IPE 100 L=95,6 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
96	1	57	-61	39	0	0	29	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
96	1	27037	9471	7681	1033	240	27	>100	8.06	>100	8.06

Asia : 8023 [82 , 88]

Sez. G: IPE 100 L=95,3 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-11	-19	-39	0	0	-9	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9477	7686	1033	240	27	>100	26.0	>100	26.0

Asia : 8024 [12 , 13]

Sez. G: IPE 100 L=89,7 cm Crit.: Acciaio Flessione $\gamma M=1,05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} \cdot \text{Verificato}$										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	1822	183	-16	-0	0	61	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9465	7676	1033	240	27	51.6	3.10	>100	3.10

Asia : 8024 [13 , 14]

Sez. G: IPE 100 L=89,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
101	1	3141	8	26	0	0	-5	--	--	(12+13)+IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	27037	9477	7686	1033	240	27	>100	7.40	>100	7.40

Asia : 8024 [14 , 15]

Sez. G: IPE 100 L=89,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	2310	-6	-20	-0	0	-3	--	--	(12+13)+II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9480	7688	1033	240	27	>100	10.3	>100	10.3

Asia : 8024 [15 , 16]

Sez. G: IPE 100 L=149,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
75	1	789	1	-1	0	-41	-0	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	27037	9481	7689	1033	240	27	>100	14.4	>100	14.4

Asia : 8024 [16 , 17]

Sez. G: IPE 100 L=148,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
119	1	1901	6	23	-0	-9	-4	--	--	(12+13)+II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9478	7687	1033	240	27	>100	10.5	>100	10.5

Asia : 8024 [17 , 22]

Sez. G: IPE 100 L=90,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
102	1	1549	-27	26	0	0	15	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
102	1	27037	9470	7680	1033	240	27	>100	8.39	>100	8.39

Asia : 8024 [22 , 18]

Sez. G: IPE 100 L=89,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
77	1	953	19	20	-0	0	-7	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
77	1	27037	9477	7686	1033	240	27	>100	15.0	>100	15.0

Asia : 8024 [18 , 19]

Sez. G: IPE 100 L=89,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
89	1	1859	12	23	-0	0	-5	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9479	7687	1033	240	27	>100	10.9	>100	10.9

Asia : 8024 [19 , 20]

Sez. G: IPE 100 L=89,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	2750	7	-21	-0	0	4	--	--	(12+13)+II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7687	1033	240	27	>100	8.53	>100	8.53

Asia : 8024 [20 , 21]

Sez. G: IPE 100 L=89,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	1772	-108	-16	0	0	-42	--	--	(12+13)+IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9468	7678	1033	240	27	88.1	4.16	>100	4.16

Verifica spostamenti verticali delle aste in Acciaio secondo NTC 2008										
Scenario di calcolo : Set NT SLD A2 STRGEO										

Travata: 8000 (Travata 8000) [12 (Nodo 12), 12 (Nodo 12)]

L = 1369.7cm Crit.Prog: Acciaio Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	cm	Comb.	δmax	mm	L/250.00	Cs
737.1		2	9.63	54.79		5.69

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	cm	Comb.	δ2	mm	L/300.00	Cs
722.5		2	3.78	45.66		12.1

Travata: 8001 (Travata 8001) [13 (Nodo 13), 13 (Nodo 13)]

L = 1424.4cm Crit.Prog: Acciaio Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	cm	Comb.	δmax	mm	L/250.00	Cs
731.9		2	10.46	56.97		5.45

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	cm	Comb.	δ2	mm	L/300.00	Cs
687.5		2	4.34	47.48		11.0

Travata: 8002 (Travata 8002) [14 (Nodo 14), 14 (Nodo 14)]

L = 1424.6cm Crit.Prog: Acciaio Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	cm	Comb.	δmax	mm	L/250.00	Cs
731.9		2	11.34	56.98		5.02

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
702.4	2	4.80	47.49	9.89

Travata: 8003 (Travata 8003) [15 (Nodo 15), 15 (Nodo 15)]

L = 1423.6cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
746.4	2	12.11	56.94	4.70

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
716.8	2	5.21	47.45	9.11

Travata: 8004 (Travata 8004) [16 (Nodo 16), 16 (Nodo 16)]

L = 1424.6cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
746.7	2	12.66	56.99	4.50

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
717.2	2	5.48	47.49	8.67

Travata: 8005 (Travata 8005) [17 (Nodo 17), 17 (Nodo 17)]

L = 1397.1cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
740.2	2	12.38	55.88	4.52

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
711.3	2	5.31	46.57	8.78

Travata: 8006 (Travata 8006) [18 (Nodo 18), 22 (Nodo 22)]

L = 1424.9cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
746.8	2	11.70	56.99	4.87

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
717.2	2	5.00	47.50	9.50

Travata: 8007 (Travata 8007) [19 (Nodo 19), 18 (Nodo 18)]

L = 1424.2cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
731.8	2	11.37	56.97	5.01

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
702.2	2	4.85	47.47	9.80

Travata: 8008 (Travata 8008) [20 (Nodo 20), 19 (Nodo 19)]

L = 1424.4cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
731.9	2	11.10	56.97	5.13

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
702.3	2	4.70	47.48	10.1

Travata: 8009 (Travata 8009) [21 (Nodo 21), 20 (Nodo 20)]

L = 1424.3cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
746.6	2	10.28	56.97	5.54

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
702.3	2	4.26	47.48	11.1

Travata: 8010 (Travata 8010) [22 (Nodo 22), 21 (Nodo 21)]

L = 1424.5cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
761.5	2	9.73	56.98	5.86

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
731.9	2	3.82	47.48	12.4

Travata: 8013 (Travata 8013) [28 (Nodo 28), 33 (Nodo 33)]

L = 1494.7cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
1195.6	6	0.27	59.79	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300,00	Cs
cm		mm	mm	
1195.6	6	0.15	49.82	>100

Travata: 8014 (Travata 8014) [12 (Nodo 12), 22 (Nodo 22)]

L = 1495.0cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250,00	Cs
cm		mm	mm	
236.4	5	0.59	59.80	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
97.0	5	0.31	49.83	>100

Travata: 8015 (Travata 8015) [7 (Nodo 7), 31 (Nodo 31)]

L = 1447.0cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
505.3	5	1.71	57.88	33.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
505.3	5	0.88	48.23	54.6

Travata: 8016 (Travata 8016) [8 (Nodo 8), 32 (Nodo 32)]

L = 1398.5cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
486.9	5	2.71	55.94	20.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
486.9	5	1.47	46.62	31.8

Travata: 8017 (Travata 8017) [9 (Nodo 9), 33 (Nodo 33)]

L = 1350.7cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
603.6	5	3.32	54.03	16.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
484.1	5	1.84	45.02	24.4

Travata: 8018 (Travata 8018) [35 (Nodo 35), 83 (Nodo 83)]

L = 1302.3cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
585.3	5	3.43	52.09	15.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
465.9	5	1.91	43.41	22.7

Travata: 8019 (Travata 8019) [36 (Nodo 36), 84 (Nodo 84)]

L = 1254.2cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
567.2	5	3.07	50.17	16.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
567.2	5	1.73	41.81	24.1

Travata: 8020 (Travata 8020) [37 (Nodo 37), 85 (Nodo 85)]

L = 1206.4cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
549.5	5	2.47	48.26	19.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
549.5	5	1.39	40.21	28.9

Travata: 8021 (Travata 8021) [38 (Nodo 38), 86 (Nodo 86)]

L = 1158.4cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
546.4	5	1.76	46.33	26.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
546.4	5	0.98	38.61	39.4

Travata: 8022 (Travata 8022) [39 (Nodo 39), 87 (Nodo 87)]

L = 1110.2cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
528.3	5	1.09	44.41	40.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
528.3	5	0.58	37.01	63.5

Travata: 8023 (Travata 8023) [40 (Nodo 40), 88 (Nodo 88)]

L = 1062.2cm Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
510.3	2	0.47	42.49	90.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
510.3	2	0.24	35.41	>100

Travata: 8024 (Travata 8024) [12 (Nodo 12), 21 (Nodo 21)]

L = 1002.0cm bb Crit.Prog: Acciaio_Flessione δ̄ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
734.0	5	-0.30	40.08	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	1.300,00	Cs
cm		mm	mm	
734.0	5	-0.21	33.40	>100

Verifica delle travi (Stati limite esercizio)

Scenario di calcolo : Set NT_SLD_A2_STR/GEO

Trave di Fond. : 9005 | 1, 2 | Pilastrate | 1, 2 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.6 cm Ln= 161.6 cm Terreno: TerrenoI

Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma_{fal}[kg/cmq]=3600$

X	M+	M-	Act	Mq	Alsup	Alinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m		cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	589	--	12.06	12.06	-1	54	--	--	--	--	5	6	Si	66.3
16.2	373	28	12.06	12.06	-1	34	-0	3	-0	3	5	6	Si	>100
80.8	225	1043	12.06	12.06	-0	21	-2	96	-2	96	5	6	Si	37.4
145.5	1405	1216	12.06	12.06	-2	129	-2	112	-2	112	5	6	Si	27.8
161.6	1936	1099	12.06	12.06	-3	178	-2	101	-2	101	5	6	Si	20.2

Combinazione OP: $\sigma_{cal}[kg/cmq]=112$ $\sigma_{fal}[kg/cmq]=3600$

X	M+	M-	Act	Mq	Alsup	Alinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m		cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	302	--	12.06	12.06	-0	28	--	--	--	--	14	14	Si	>100
16.2	67	--	12.06	12.06	-0	6	--	--	--	--	14	14	Si	>100
80.8	--	482	12.06	12.06	--	--	--	44	-1	44	14	14	Si	81.0
145.5	--	296	12.06	12.06	--	--	--	27	-0	27	14	14	Si	>100
161.6	--	117	12.06	12.06	--	--	--	11	-0	11	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M+	M-	Act	Mq	Alsup	Alinf	pAlt	S _{max}	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Wd	Wk	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m		mm	cmq	cmq	cm	cm	kg/cmq	kg/cmq	kg/cmq	kg/cmq	mm	mm				
0.0	-296	0.1	12.06	30.16	22.4	27	0.002	0.002	12(Fr)	27	0.002	0.002	12(Fr)	27	0.002	0.002	12(Fr)	Si	>100
0.0	-302	0.1	12.06	30.16	22.4	28	0.002	0.002	14(Qp)	28	0.002	0.002	14(Qp)	28	0.002	0.002	14(Qp)	Si	>100
16.2	-47	0.1	12.06	30.16	22.4	6	0.000	0.000	14(Qp)	6	0.000	0.000	14(Qp)	6	0.000	0.000	14(Qp)	Si	>100
16.2	-45	0.1	12.06	30.16	22.4	4	0.000	0.000	12(Fr)	4	0.000	0.000	12(Fr)	4	0.000	0.000	12(Fr)	Si	>100
80.8	482	0.1	12.06	30.16	22.4	44	0.003	0.003	14(Qp)	44	0.003	0.003	14(Qp)	44	0.003	0.003	14(Qp)	Si	>100
80.8	325	0.1	12.06	30.16	22.4	30	0.002	0.002	11(Fr)	30	0.002	0.002	11(Fr)	30	0.002	0.002	11(Fr)	Si	>100
145.5	296	0.1	12.06	30.16	22.4	27	0.002	0.002	14(Qp)	27	0.002	0.002	14(Qp)	27	0.002	0.002	14(Qp)	Si	>100
145.5	-52	0.1	12.06	30.16	22.4	5	0.000	0.000	11(Fr)	5	0.000	0.000	11(Fr)	5	0.000	0.000	11(Fr)	Si	>100
161.6	117	0.1	12.06	30.16	22.4	11	0.001	0.001	9(Fr)	11	0.001	0.001	9(Fr)	11	0.001	0.001	9(Fr)	Si	>100
161.6	117	0.1	12.06	30.16	22.4	11	0.001	0.001	9(Fr)	11	0.001	0.001	9(Fr)	11	0.001	0.001	9(Fr)	Si	>100

Trave di Fond. : 9005 | 2, 3 | Pilastrate | 2, 3 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.9 cm Ln= 149.9 cm Terreno: TerrenoI

Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma_{fal}[kg/cmq]=3600$

X	M+	M-	Act	Mq	Alsup	Alinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m		cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	2341	1088	12.06	12.06	-4	216	-2	100	-2	100	5	6	Si	16.7
15.0	1687	1531	12.06	12.06	-3	156	-2	141	-2	141	5	6	Si	23.1
75.0	--	2677	12.06	12.06	--	--	--	4	-4	247	5	6	Si	14.6
134.9	--	2791	12.06	12.06	--	--	--	-4	-4	257	5	6	Si	14.0
149.9	--	2652	12.06	12.06	--	--	--	-4	-4	244	5	6	Si	14.7

Combinazione OP: $\sigma_{cal}[kg/cmq]=112$ $\sigma_{fal}[kg/cmq]=3600$

X	M+	M-	Act	Mq	Alsup	Alinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m		cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	21	12.06	12.06	--	--	--	--	-0	2	14	14	Si	>100
15.0	--	375	12.06	12.06	--	--	--	--	-1	35	14	14	Si	>100
75.0	--	1286	12.06	12.06	--	--	--	--	-2	118	14	14	Si	30.4

X	M+	M-	Act	Mq	Alsup	Alinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	Cs
134.9	--	1370	12.06	12.06	12.06	12.06	--	--	-2	126	14	14	Si	28.5
149.9	--	1258	12.06	12.06	12.06	12.06	--	--	-2	116	14	14	Si	31.0

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M+	M-	Act	Mq	Alsup	Alinf	pAlt	S _{max}	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Wd	Wk	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m		mm	cmq	cmq	cm	cm	kg/cmq	kg/cmq	kg/cmq	kg/cmq	mm	mm				
0.0	14	0.1	12.06	30.16	22.4	22.4	22.4	1	0.000	0.000	10(Fr)	1	0.000	0.000	10(Fr)	Si	>100		
0.0	21	0.1	12.06	30.16	22.4	22.4	22.4	2	0.000	0.000	14(Qp)	2	0.000	0.000	14(Qp)	Si	>100		
15.0	375	0.1	12.06	30.16	22.4	22.4	22.4	35	0.002	0.002	14(Qp)	35	0.002	0.002	14(Qp)	Si	>100		
15.0	-48	0.1	12.06	30.16	22.4	22.4	22.4	4	0.000	0.000	11(Fr)	4	0.000	0.000	11(Fr)	Si	>100		
75.0	1286	0.1	12.06	30.16	22.4	22.4	22.4	118	0.008	0.008	14(Qp)	118	0.008	0.008	14(Qp)	Si	39.6		
75.0	986	0.1	12.06	30.16	22.4	22.4	22.4	91	0.006	0.006	11(Fr)	91	0.006	0.006	11(Fr)	Si	68.9		
134.9	1370	0.1	12.06	30.16	22.4	22.4	22.4	126	0.008	0.008	14(Qp)	126	0.008	0.008	14(Qp)	Si	37.2		
134.9	1100	0.1	12.06	30.16	22.4	22.4	22.4	101	0.006	0.006	11(Fr)	101	0.006	0.006	11(Fr)	Si	61.7		
149.9	1258	0.1	12.06	30.16	22.4	22.4	22.4	116	0.007	0.007	14(Qp)	116	0.007	0.007	14(Qp)	Si	40.5		
149.9	980	0.1	12.06	30.16	22.4	22.4	22.4	90	0.006	0.006	11(Fr)	90	0.006	0.006	11(Fr)	Si	69.3		

Trave di Fond. : 9005 | 3, 4 | Pilastrate | 3, 4 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 148.8 cm Ln= 148.8 cm Terreno: TerrenoI

Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma_{fal}[kg/cmq]=3600$

X	M+	M-	Act	Mq	Alsup	Alinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m		cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	290	2701	12.06	12.06	12.06	12.06	-0	27	-4	249	5	6	Si	14.5
14.9	--	3016	12.06	12.06	--	--	--	--	-5	278	5	6	Si	13.0
74.4	--	3617	12.06	12.06	--	--	--	--	-6	333	5	6	Si	10.8
133.9	--	3222	12.06	12.06	--	--	--	--	-5	297	5	6	Si	12.1
148.8	--	2973	12.06	12.06	--	--	--	--	-5	274	5	6	Si	13.1

Combinazione OP: $\sigma_{cal}[kg/cmq]=112$ $\sigma_{fal}[kg/cmq]=3600$

X	M+	M-	Act	Mq	Alsup	Alinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m		cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	1190	12.06	12.06	12.06	12.06	--	--	-2	110	14	14	Si	32.8
14.9	--	1457	12.06	12.06	12.06	12.06	--	--	-2	134	14	14	Si	26.8
74.4	--	2007	12.06	12.06	12.06	12.06	--	--	-3	185	14	14	Si	19.5
133.9	--	1758	12.06	12.06	12.06	12.06	--	--	-3	162	14	14	Si	22.2
148.8	--	1575	12.06	12.06	12.06	12.06	--	--	-2	145	14	14	Si	24.8

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	defined	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	848	0.1	12.06	30.16	22.4	78	0.005	0.005	11(Fr)	Si	80.1
0.0	1190	0.1	12.06	30.16	22.4	110	0.007	0.007	14(Qp)	Si	42.8
14.9	1457	0.1	12.06	30.16	22.4	134	0.009	0.009	14(Qp)	Si	35.0
14.9	1509	0.1	12.06	30.16	22.4	107	0.007	0.007	11(Fr)	Si	58.6
74.4	2007	0.1	12.06	30.16	22.4	185	0.012	0.012	14(Qp)	Si	25.4
74.4	1823	0.1	12.06	30.16	22.4	168	0.011	0.011	11(Fr)	Si	37.3
133.9	1758	0.1	12.06	30.16	22.4	162	0.010	0.010	14(Qp)	Si	29.0
133.9	1592	0.1	12.06	30.16	22.4	147	0.009	0.009	11(Fr)	Si	42.7
148.8	1575	0.1	12.06	30.16	22.4	145	0.009	0.009	14(Qp)	Si	32.3
148.8	1398	0.1	12.06	30.16	22.4	129	0.008	0.008	11(Fr)	Si	48.6

X	M+	M-	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Cb+	Cb-	Ver.	CS
149.9	--	3086		12.06	12.06	--	--	-5	284	5	1	Si	12.7

Combinazione OP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1629	0.1	12.06	30.16	22.4	117	0.007	0.007	11(Fr)	Si	53.5		
0.0	1512	0.1	12.06	30.16	22.4	139	0.009	0.009	14(Qp)	Si	33.7		
15.0	1748	0.1	12.06	30.16	22.4	161	0.010	0.010	14(Qp)	Si	29.1		
15.0	1551	0.1	12.06	30.16	22.4	143	0.009	0.009	11(Fr)	Si	43.8		
74.9	2220	0.1	12.06	30.16	22.4	205	0.013	0.013	14(Qp)	Si	22.9		
74.9	2147	0.1	12.06	30.16	22.4	198	0.013	0.013	11(Fr)	Si	31.6		
134.9	1964	0.1	12.06	30.16	22.4	181	0.012	0.012	14(Qp)	Si	25.9		
134.9	1919	0.1	12.06	30.16	22.4	177	0.011	0.011	11(Fr)	Si	35.4		
149.9	1788	0.1	12.06	30.16	22.4	165	0.011	0.011	14(Qp)	Si	28.5		
149.9	1735	0.1	12.06	30.16	22.4	160	0.010	0.010	11(Fr)	Si	39.1		

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cm	kg/cmq	kg/cmq	kg/cmq	mm	mm			
0.0	1269	0.1	12.06	30.16	22.4	117	0.007	0.007	11(Fr)	Si	53.5		
0.0	1512	0.1	12.06	30.16	22.4	139	0.009	0.009	14(Qp)	Si	33.7		
15.0	1748	0.1	12.06	30.16	22.4	161	0.010	0.010	14(Qp)	Si	29.1		
15.0	1551	0.1	12.06	30.16	22.4	143	0.009	0.009	11(Fr)	Si	43.8		
74.9	2220	0.1	12.06	30.16	22.4	205	0.013	0.013	14(Qp)	Si	22.9		
74.9	2147	0.1	12.06	30.16	22.4	198	0.013	0.013	11(Fr)	Si	31.6		
134.9	1964	0.1	12.06	30.16	22.4	181	0.012	0.012	14(Qp)	Si	25.9		
134.9	1919	0.1	12.06	30.16	22.4	177	0.011	0.011	11(Fr)	Si	35.4		
149.9	1788	0.1	12.06	30.16	22.4	165	0.011	0.011	14(Qp)	Si	28.5		
149.9	1735	0.1	12.06	30.16	22.4	160	0.010	0.010	11(Fr)	Si	39.1		

Trave di Fond.: 9005 [5. 6] Pilastrate [5. 6]

Sez. R: By= 60.0 cm Bz= 100.0 cm L=149.3 cm Ln= 149.3 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	3159	12.06	12.06	--	--	-5	291	5	6	Si	12.4	
14.9	--	3478	12.06	12.06	--	--	-5	321	5	1	Si	11.2	
74.7	--	4271	12.06	12.06	--	--	-7	394	8	1	Si	9.15	
134.4	--	4047	12.06	12.06	--	--	-6	373	8	1	Si	9.65	
149.3	--	3837	12.06	12.06	--	--	-6	354	7	2	Si	10.2	

Combinazione OP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	1750	12.06	12.06	--	--	-3	161	14	14	Si	22.3	
14.9	--	2010	12.06	12.06	--	--	-3	185	14	14	Si	19.4	
74.7	--	2613	12.06	12.06	--	--	-4	241	14	14	Si	14.9	
134.4	--	2512	12.06	12.06	--	--	-4	232	14	14	Si	15.5	
149.3	--	2375	12.06	12.06	--	--	-4	219	14	14	Si	16.4	

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cm	kg/cmq	kg/cmq	kg/cmq	mm	mm			
0.0	1629	0.1	12.06	30.16	22.4	150	0.010	0.010	11(Fr)	Si	41.7		
0.0	1750	0.1	12.06	30.16	22.4	161	0.010	0.010	14(Qp)	Si	29.1		
14.9	2010	0.1	12.06	30.16	22.4	185	0.012	0.012	14(Qp)	Si	25.3		
14.9	1940	0.1	12.06	30.16	22.4	179	0.011	0.011	11(Fr)	Si	35.0		
74.7	2613	0.1	12.06	30.16	22.4	241	0.015	0.015	14(Qp)	Si	19.5		
74.7	2613	0.1	12.06	30.16	22.4	241	0.015	0.015	9(Fr)	Si	26.0		
134.4	2512	0.1	12.06	30.16	22.4	232	0.015	0.015	14(Qp)	Si	20.3		
134.4	2512	0.1	12.06	30.16	22.4	232	0.015	0.015	9(Fr)	Si	27.0		
149.3	2375	0.1	12.06	30.16	22.4	219	0.014	0.014	14(Qp)	Si	21.4		
149.3	2375	0.1	12.06	30.16	22.4	219	0.014	0.014	9(Fr)	Si	28.6		

Trave di Fond.: 9005 [6. 7] Pilastrate [6. 7]

Sez. R: By= 60.0 cm Bz= 100.0 cm L=149.6 cm Ln= 149.6 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	3923	12.06	12.06	--	--	-6	362	8	1	Si	9.96	
15.0	--	4358	12.06	12.06	--	--	-7	402	8	1	Si	8.96	
74.8	--	5416	12.06	12.06	--	--	-8	499	5	1	Si	7.21	
134.6	--	5437	12.06	12.06	--	--	-8	501	5	6	Si	7.18	
149.6	--	5313	12.06	12.06	--	--	-8	490	5	6	Si	7.35	

Combinazione OP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	2372	12.06	12.06	--	--	-4	219	14	14	Si	16.5	
15.0	--	2624	12.06	12.06	--	--	-4	242	14	14	Si	14.9	
74.8	--	3166	12.06	12.06	--	--	-5	292	14	14	Si	12.3	
134.6	--	2941	12.06	12.06	--	--	-5	271	14	14	Si	13.3	
149.6	--	2758	12.06	12.06	--	--	-4	254	14	14	Si	14.2	

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cm	kg/cmq	kg/cmq	kg/cmq	mm	mm			
0.0	2372	0.1	12.06	30.16	22.4	219	0.014	0.014	9(Fr)	Si	28.6		
0.0	2372	0.1	12.06	30.16	22.4	219	0.014	0.014	14(Qp)	Si	21.5		
15.0	2624	0.1	12.06	30.16	22.4	242	0.015	0.015	14(Qp)	Si	19.4		
15.0	2624	0.1	12.06	30.16	22.4	242	0.015	0.015	9(Fr)	Si	25.9		
74.8	3166	0.1	12.06	30.16	22.4	292	0.018	0.018	14(Qp)	Si	16.1		
74.8	3110	0.1	12.06	30.16	22.4	287	0.018	0.018	11(Fr)	Si	21.8		
134.6	2941	0.1	12.06	30.16	22.4	271	0.017	0.017	14(Qp)	Si	17.3		
134.6	2685	0.1	12.06	30.16	22.4	247	0.016	0.016	11(Fr)	Si	25.3		
149.6	2758	0.1	12.06	30.16	22.4	254	0.016	0.016	14(Qp)	Si	18.5		
149.6	2439	0.1	12.06	30.16	22.4	225	0.014	0.014	11(Fr)	Si	27.8		

Trave di Fond.: 9005 [7. 8] Pilastrate [7. 8]

Sez. R: By= 60.0 cm Bz= 100.0 cm L=149.4 cm Ln= 149.4 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	5533	12.06	12.06	--	--	-9	510	5	6	Si	7.06	
14.9	--	5732	12.06	12.06	--	--	-9	528	5	6	Si	6.81	
74.7	--	5927	12.06	12.06	--	--	-9	546	5	1	Si	6.59	
134.4	--	5047	12.06	12.06	--	--	-8	465	5	1	Si	7.74	
149.4	--	4630	12.06	12.06	--	--	-7	427	5	1	Si	8.44	

Combinazione OP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{sup}	A _{finf}	σ _{c+}	σ _{f+}	σ _{c-}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	2783	12.06	12.06	--	--	-4	257	14	14	Si	14.0	
14.9	--	3016	12.06	12.06	--	--	-5	278	14	14	Si	13.0	
74.7	--	3425	12.06	12.06	--	--	-5	316	14	14	Si	11.4	
134.4	--	3002	12.06	12.06	--	--	-5	277	14	14	Si	13.0	
149.4	--	2764	12.06	12.06	--	--	-4	255	14	14	Si	14.1	

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	ofrmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmqd	mm	mm			
0.0	2396	0.1	12.06	30.16	22.4	221	0.014	0.014	11(Fr)	Si	28.3
0.0	2783	0.1	12.06	30.16	22.4	221	0.016	0.016	14(Qp)	Si	18.3
14.9	3016	0.1	12.06	30.16	22.4	278	0.018	0.018	14(Qp)	Si	16.9
14.9	2689	0.1	12.06	30.16	22.4	248	0.016	0.016	11(Fr)	Si	25.3
74.7	3425	0.1	12.06	30.16	22.4	316	0.020	0.020	14(Qp)	Si	14.9
74.7	3287	0.1	12.06	30.16	22.4	303	0.019	0.019	11(Fr)	Si	20.7

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
134.4	3002	0.1	12.06	30.16	22.4	277	0.018	0.018	14(Qp)	Si	17.0
134.4	2966	0.1	12.06	30.16	22.4	273	0.017	0.017	11(Fr)	Si	22.9
149.4	2764	0.1	12.06	30.16	22.4	255	0.016	0.016	14(Qp)	Si	18.4
149.4	2740	0.1	12.06	30.16	22.4	253	0.016	0.016	11(Fr)	Si	24.8

Trave di Fond. : 9005 | 9 , 10 | Pilastrate [8 , 9]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.2 cm Ln= 149.2 cm Terreno: **Terrenol**

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Alsup	Alinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	4819	12.06	12.06	--	--	-7	444	5	1	Si	8.10
14.9	--	4947	12.06	12.06	--	--	-8	456	5	1	Si	7.90
74.6	--	4812	12.06	12.06	--	--	-7	443	7	2	Si	8.12
134.3	--	4191	12.06	12.06	--	--	-6	386	7	5	Si	9.32
149.2	--	3881	12.06	12.06	--	--	-6	358	6	5	Si	10.1

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	Alsup	Alinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	2808	12.06	12.06	--	--	-4	259	14	14	Si	13.9
14.9	--	2956	12.06	12.06	--	--	-5	272	14	14	Si	13.2
74.6	--	3015	12.06	12.06	--	--	-5	278	14	14	Si	13.0
134.3	--	2232	12.06	12.06	--	--	-3	206	14	14	Si	17.5
149.2	--	1903	12.06	12.06	--	--	-3	175	14	14	Si	20.5

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	2713	0.1	12.06	30.16	22.4	250	0.016	0.016	11(Fr)	Si	25.0
0.0	2808	0.1	12.06	30.16	22.4	259	0.017	0.017	14(Qp)	Si	18.1
14.9	2956	0.1	12.06	30.16	22.4	272	0.017	0.017	14(Qp)	Si	17.2
14.9	2926	0.1	12.06	30.16	22.4	270	0.017	0.017	11(Fr)	Si	23.2
74.6	3015	0.1	12.06	30.16	22.4	278	0.018	0.018	14(Qp)	Si	16.9
74.6	3015	0.1	12.06	30.16	22.4	278	0.018	0.018	9(Fr)	Si	22.5
134.3	2232	0.1	12.06	30.16	22.4	206	0.013	0.013	14(Qp)	Si	22.8
134.3	2232	0.1	12.06	30.16	22.4	206	0.013	0.013	9(Fr)	Si	30.4
149.2	1903	0.1	12.06	30.16	22.4	175	0.011	0.011	14(Qp)	Si	26.8
149.2	1869	0.1	12.06	30.16	22.4	172	0.011	0.011	12(Fr)	Si	36.3

Trave di Fond. : 9005 | 9 , 10 | Pilastrate [9 , 10]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.5 cm Ln= 149.5 cm Terreno: **Terrenol**

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Alsup	Alinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	3625	12.06	12.06	--	--	-6	334	7	5	Si	10.8
14.9	--	4033	12.06	12.06	--	--	-6	372	6	5	Si	9.68
74.7	--	4756	12.06	12.06	--	--	-7	438	6	5	Si	8.21
134.5	825	4027	12.06	12.06	-1	76	-6	371	6	5	Si	9.70
149.5	1473	3614	12.06	12.06	-2	136	-6	333	6	5	Si	10.8

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	Alsup	Alinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	1984	12.06	12.06	--	--	-3	183	14	14	Si	19.7
14.9	--	2040	12.06	12.06	--	--	-3	188	14	14	Si	19.1
74.7	--	1745	12.06	12.06	--	--	-3	161	14	14	Si	22.4
134.5	--	656	12.06	12.06	--	--	-1	60	14	14	Si	59.5
149.5	--	264	12.06	12.06	--	--	-0	24	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

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X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	1984	0.1	12.06	30.16	22.4	183	0.012	0.012	9(Fr)	Si	34.2
0.0	1984	0.1	12.06	30.16	22.4	183	0.012	0.012	14(Qp)	Si	25.7
14.9	2040	0.1	12.06	30.16	22.4	188	0.012	0.012	14(Qp)	Si	25.0
14.9	2015	0.1	12.06	30.16	22.4	186	0.012	0.012	12(Fr)	Si	33.7
74.7	1745	0.1	12.06	30.16	22.4	161	0.010	0.010	14(Qp)	Si	29.2
74.7	1574	0.1	12.06	30.16	22.4	145	0.009	0.009	12(Fr)	Si	43.2
134.5	656	0.1	12.06	30.16	22.4	60	0.004	0.004	14(Qp)	Si	77.6
134.5	339	0.1	12.06	30.16	22.4	31	0.002	0.002	12(Fr)	Si	>100
149.5	264	0.1	12.06	30.16	22.4	24	0.002	0.002	14(Qp)	Si	>100
149.5	-89	0.1	12.06	30.16	22.4	8	0.001	0.001	12(Fr)	Si	>100

Trave di Fond. : 9005 | 10 , 11 | Pilastrate [10 , 11]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 150.0 cm Ln= 150.0 cm Terreno: **Terrenol**

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Alsup	Alinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1126	3400	12.06	12.06	-2	104	-5	313	6	5	Si	11.5
15.0	905	3495	12.06	12.06	-1	83	-5	322	6	5	Si	11.2
75.0	432	2945	12.06	12.06	-1	40	-5	271	6	5	Si	13.3
135.0	372	919	12.06	12.06	-1	34	-1	85	6	5	Si	42.5
150.0	382	181	12.06	12.06	-1	35	-0	17	6	5	Si	>100

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	Alsup	Alinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	367	12.06	12.06	--	--	-1	34	14	14	Si	>100
15.0	--	494	12.06	12.06	--	--	-1	46	14	14	Si	79.1
75.0	--	572	12.06	12.06	--	--	-1	53	14	14	Si	68.3
135.0	--	70	12.06	12.06	--	--	-0	6	14	14	Si	>100
150.0	130	--	12.06	12.06	-0	12	--	--	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	59	0.1	12.06	30.16	22.4	5	0.000	0.000	12(Fr)	Si	>100
0.0	367	0.1	12.06	30.16	22.4	34	0.002	0.002	14(Qp)	Si	>100
15.0	494	0.1	12.06	30.16	22.4	46	0.003	0.003	14(Qp)	Si	>100
15.0	200	0.1	12.06	30.16	22.4	18	0.001	0.001	12(Fr)	Si	>100
75.0	572	0.1	12.06	30.16	22.4	53	0.003	0.003	14(Qp)	Si	89.0
75.0	354	0.1	12.06	30.16	22.4	33	0.002	0.002	12(Fr)	Si	>100
135.0	70	0.1	12.06	30.16	22.4	6	0.000	0.000	14(Qp)	Si	>100
135.0	-19	0.1	12.06	30.16	22.4	2	0.000	0.000	12(Fr)	Si	>100
150.0	-130	0.1	12.06	30.16	22.4	12	0.001	0.001	14(Qp)	Si	>100
150.0	-62	0.1	12.06	30.16	22.4	6	0.000	0.000	11(Fr)	Si	>100

Trave di Fond. : 9006 | 1 , 2 | Pilastrate [21 , 12]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.7 cm Ln= 101.7 cm Terreno: **Terrenol**

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	Alsup	Alinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	227	--	12.06	12.06	-0	21	--	--	5	6	Si	>100
10.2	102	131	12.06	12.06	-0	9	-0	12	5	6	Si	>100
50.9	--	507	12.06	12.06	--	--	--	-1	47	5	Si	77.0
91.6	369	613	12.06	12.06	-1	34	-1	57	5	6	Si	63.7
101.7	535	599	12.06	12.06	-1	49	-1	55	5	6	Si	65.2

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	Alsup	Alinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				

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Trave di Fond.: 9006 [5, 6 | Pilastrate [18, 17]

Sez. R:	Bv= 60.0 cm	Bz= 100.0 cm	L= 148.9 cm	Ln= 148.9 cm	Terreno: Terrenol
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Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149$ $\sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M-	Alfup	Alfint	cc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg ² m	kg ² m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	3279	792	12.06	12.06	-5	302	-1	73	5	6	Si	11.9
14.9	3229	831	12.06	12.06	-5	298	-1	75	5	6	Si	12.1
74.5	3330	611	12.06	12.06	-5	307	-1	58	5	6	Si	11.7
134.0	3870	38	12.06	12.06	-6	357	-0	3	5	6	Si	10.1
148.9	4064	--	12.06	12.06	-6	375	--	--	5	6	Si	9.61

Combinazione OP: $\sigma_{ca}[\text{kg/cmq}] = 112 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M _*	Δfup	Δfinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg* ^m	kg* ^m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	693	12.06	12.06	12.06	-1	64	--	--	14	14	Si	56.4
14.9	655	12.06	12.06	12.06	-1	60	--	--	14	14	Si	59.7
74.5	697	12.06	12.06	12.06	-1	64	--	--	14	14	Si	56.1
1037	134.0	12.06	12.06	12.06	-2	96	--	--	14	14	Si	37.7
148.9	1166	12.06	12.06	12.06	-2	107	--	--	14	14	Si	33.5

Verifica aperture fessure: Wamm $\text{Freq}[\text{mm}] = 0.400$ Wamm $\text{Op}[\text{mm}] = 0.300$

X	M	Act	Aft	pAft	S _{max}	orfted	Wd	Wk	Ch	Ver.	Cs
cm	kg* ^m	m ^q	cm ^q	cm	cm	mm	mm	mm			
-355	0.1	12.06	30.16	22.4	33	0.002	0.002	12(Fr)	Si	>100	
-693	0.1	12.06	30.16	22.4	64	0.004	0.004	14(Qp)	Si	73.5	
-655	0.1	12.06	30.16	22.4	60	0.004	0.004	14(Qp)	Si	77.8	
-322	0.1	12.06	30.16	22.4	30	0.002	0.002	12(Fr)	Si	>100	
-677	0.1	12.06	30.16	22.4	64	0.004	0.004	14(Qp)	Si	73.1	
-390	0.1	12.06	30.16	22.4	36	0.002	0.002	12(Fr)	Si	>100	
-1037	0.1	12.06	30.16	22.4	96	0.006	0.006	14(Qp)	Si	49.1	
-767	0.1	12.06	30.16	22.4	71	0.005	0.005	12(Fr)	Si	88.5	
-1166	0.1	12.06	30.16	22.4	107	0.007	0.007	14(Qp)	Si	43.7	
-909	0.1	12.06	30.16	22.4	84	0.005	0.005	12(Fr)	Si	74.7	

Trave di Fond. : 9006 | 6, 11 | Pilastrate [17, 22]

Sez. R:	$B_V = 60,0 \text{ cm}$	$B_Z = 100,0 \text{ cm}$	$L = 90,0 \text{ cm}$	$L_n = 90,0 \text{ cm}$	Terreno: Terreno I
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Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149$ $\sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M ⁺ kg m ³	M ⁺ kg m ⁻³	M ⁺ cmq	Alinf	cc+	σf ⁺ kg cmq	cc-	σf- kg cmq	Cb+	Cb-	Ver.	CS
cm													
0.0		4216	49	12.06	12.06	-7	389	-0	4	5	6	Si	9.27
9.0	4198	77	12.06	12.06	-6	387	-0	7	5	6	Si	9.30	
45.0	4203	93	12.06	12.06	-6	387	-0	9	5	6	Si	9.29	
81.0	4322	--	12.06	12.06	-7	398	--	11	5	6	Si	9.04	
90.0	4368	--	12.06	12.06	-7	403	--	12	5	6	Si	8.94	

Combinazione OP: $\sigma_{ca}[\text{kg/cmq}] = 112 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	M ₂ ^a	M ₂ ^b	M ₂ ^c	M ₂ ^d	A ₁ up	A ₁ inf	σ ₊ ^e	σ ₋ ^f	σ ₋ ^g	Cb ⁺	Cb ⁻	Ver.	CS
cm	kg ^a m	kg ^b m	kg ^c m	kg ^d m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	11.76	0.0	12.06	12.06	-2	108	-	14	14	14	14	Si	33.2
9.0	11.61	9.0	12.06	12.06	-2	107	-	14	14	14	14	Si	33.6
45.0	11.63	45.0	12.06	12.06	-2	107	-	14	14	14	14	Si	33.6
81.0	12.63	81.0	12.06	12.06	-2	116	-	14	14	14	14	Si	30.9
90.0	13.03	90.0	12.06	12.06	-2	120	-	14	14	14	14	Si	30.0

Verifica aperture fessure: W_{amm} $F_{req}[mm]=0.400$ W_{amm} $Q_p[mm]=0.300$

X	M	Act	mq	emq	pAft	S _{max}	cm	kg/cm ³	Wd	Wk	Ch	Ver.	Cs
0.0	cm	kg*m	0.1	12.06	30.16	22.4	22.4	80	0.005	0.005	mm	mm	
0.0	-871	0.1	12.06	30.16	30.16	22.4	22.4	108	0.007	0.007	14(Qp)	Si	77.9
0.0	-1176	0.1	12.06	30.16	30.16	22.4	22.4	107	0.007	0.007	14(Qp)	Si	43.3
9.0	-1161	0.1	12.06	30.16	30.16	22.4	22.4	79	0.005	0.005	14(Qp)	Si	43.9
9.0	-854	0.1	12.06	30.16	30.16	22.4	22.4	79	0.005	0.005	14(Qp)	Si	79.5

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X	M	Act	Aft	pAft	S _{max}	σ _{fixed}	Wd	Wk	Cb	Ver	Cs
450	-1163	0.1	12.06	30.16	22.4	107	0.007	0.007	14(Qp)	Si	43.8
-853		0.1	12.06	30.16	22.4	79	0.005	0.005	12(Ft)	Si	79.7
81	-1263	0.1	12.06	30.16	22.4	116	0.007	0.007	14(Qp)	Si	40.3
-958		0.1	12.06	30.16	22.4	88	0.006	0.006	12(Ft)	Si	70.9
90	-1303	0.1	12.06	30.16	22.4	120	0.008	0.008	14(Qp)	Si	39.1
-1001		0.1	12.06	30.16	22.4	92	0.006	0.006	12(Ft)	Si	67.8

Trave di Fond. : 9006 | 11, 7 | Pilastrate | 22, 16 |

Sez. R:	$B_V=60.0\text{ cm}$	$B_Z=100.0\text{ cm}$	$L=89.4\text{ cm}$	$L_n=89.4\text{ cm}$	Terreno: Terreno I
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Criterio: CLS TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149$ $\sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M-	Afsup	Aflinf	σc+	σf+	σc-	kg/cmq	kg/cmq	Cb+	Cb-	Ver.	CS
cm	kg* ³ m	kg* ³ m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	4520	142	12.06	12.06	-7	417	-0	13		5	6	Si	8.64
8.9	4383	132	12.06	12.06	-7	404	-0	12		5	6	Si	8.91
44.7	3900	--	12.06	12.06	-6	359	--	--		5	6	Si	10.0
80.5	3527	--	12.06	12.06	-5	325	--	--		5	6	Si	11.1
89.4	3451	--	12.06	12.06	-5	318	--	--		5	6	Si	11.3

Combinazione OP: $\sigma_{ca}[\text{kg/cm}^2]=112$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

X	M ⁺ kg·m ⁻³	M ⁻ kg·m ⁻³	A _{sup} cm/q	A _{finf} cm/q	σ ₊ kg/cmq	σ ₋ kg/cmq	σ _f kg/cmq	Cb+	Cb-	Ver.	CS
cm	0.0	1306	--	12.06	-2	120	--	14	14	Si	29.9
0.0	8.9	1257	--	12.06	-2	116	--	14	14	Si	31.1
44.7	11.22	--	12.06	12.06	-2	103	--	14	14	Si	34.8
80.5	1086	--	12.06	12.06	-2	100	--	14	14	Si	36.0
89.4	1093	--	12.06	12.06	-2	101	--	14	14	Si	35.7

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	cm	M	g* ^m	Act	mq	Aft	cmq	pAft	cm	S _{max}	formed	Wd	Wk	Cb	Ver.	Cs
	0.0	-953	0.1	12.06	30.16	22.4	88				mm	mm	0.006	12(Ft)	Si	71.3
	0.0	-1306	0.1	12.06	30.16	22.4	120				kg/cmq	0.008	0.008	14(Qp)	Si	39.0
	8.9	-1257	0.1	12.06	30.16	22.4	116					0.007	0.007	14(Qp)	Si	40.5
	8.9	-918	0.1	12.06	30.16	22.4	85					0.005	0.005	12(Ft)	Si	74.0
	44.7	-1122	0.1	12.06	30.16	22.4	103					0.007	0.007	14(Qp)	Si	45.4
	44.7	-843	0.1	12.06	30.16	22.4	78					0.005	0.005	12(Ft)	Si	80.5
	80.5	-1086	0.1	12.06	30.16	22.4	100					0.006	0.006	14(Qp)	Si	46.9
	87.7	-877	0.1	12.06	30.16	22.4	81					0.005	0.005	12(Ft)	Si	77.4
	89.4	-1093	0.1	12.06	30.16	22.4	101					0.006	0.006	14(Qp)	Si	46.6
	89.4	-903	0.1	12.06	30.16	22.4	83					0.005	0.005	12(Ft)	Si	75.2

Trave di Fond.: 9006 [7, 8 | Pilastrate [16, 15]

Sez. R:	$B_V=60.0\text{ cm}$	$B_Z=100.0\text{ cm}$	$L=89.2\text{ cm}$	$L_n=89.2\text{ cm}$	<i>Terreno: Terreno I</i>
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Criterio: CLS_TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149$ $\sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M-	A _{sup}	A _{inf}	σ ₊ ⁺	σ ₋ ⁺	σ ₋ ⁻	Cb+	Cb-	Ver.	CS
cm	kg ⁺ m	kg ⁻ m	cm/kg ⁺ m	cm/kg ⁻ m	kg/cmkg	kg/cmkg	kg/cmkg				
0.0	3629	0.0	12.06	12.06	-6	335	--	5	6	Si	10.8
8.9	3411	--	12.06	12.06	-5	314	--	5	6	Si	11.5
44.6	2620	--	12.06	12.06	-4	242	--	5	6	Si	14.9
80.3	1988	--	12.06	12.06	-3	183	--	5	6	Si	19.6
89.2	1859	--	12.06	12.06	-3	171	--	5	6	Si	21.0

Combinazione OP: $\sigma_{ca}[\text{kg/cmq}] = 112 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	kg* π	M*	A π sq	A π inf	σ + kg/cmq	σ + kg/cmq	sf- kg/cmq	Cb+	Cb-	Ver.	CS
0.0	1104	--	12.06	12.06	12.06	-2	102	--	14	14	Si	35.4
8.9	1028	--	12.06	12.06	12.06	-2	95	--	14	14	Si	38.0
44.6	791	--	12.06	12.06	12.06	-1	73	--	14	14	Si	49.4
80.3	671	--	12.06	12.06	12.06	-1	62	--	14	14	Si	58.2
89.2	661	--	12.06	12.06	12.06	-1	61	--	14	14	Si	59.1

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Verifica aperture fessure: Wamm. Freq[mm]=0.400 Wamm. Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	Wd	Wk	Ch	Ver.	Cs
cm	kg·m	mq	cmq	cm	cm	mm	mm			
0.0	-861	0.1	12.06	30.16	22.4	0.005	0.005	12(Fr)	Si	78.9
0.0	-1104	0.1	12.06	30.16	22.4	0.007	0.007	14(Qp)	Si	46.1
8.9	-804	0.1	12.06	30.16	22.4	0.006	0.006	14(Qp)	Si	49.6
8.9	-804	0.1	12.06	30.16	22.4	0.005	0.005	12(Fr)	Si	84.5
44.6	-791	0.1	12.06	30.16	22.4	0.005	0.005	14(Qp)	Si	64.4
44.6	-649	0.1	12.06	30.16	22.4	0.004	0.004	12(Fr)	Si	>100
80.3	-671	0.1	12.06	30.16	22.4	0.004	0.004	14(Qp)	Si	75.9
80.3	-616	0.1	12.06	30.16	22.4	0.004	0.004	12(Fr)	Si	>100
89.2	-661	0.1	12.06	30.16	22.4	0.004	0.004	14(Qp)	Si	77.1
89.2	-628	0.1	12.06	30.16	22.4	0.004	0.004	12(Fr)	Si	>100

Trave di Fond.: 9006 | 8. 9 | Pilastrate [15. 14]

Sec. R: B_y= 60.0 cm B_z= 100.0 cm B_z= 89.6 cm L_n= 89.6 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: σca[kg/cm²]=149 σfa[kg/cm²]=3600

X	cm	kg*m	M-	M+	Afup	Afinf	σc+	σc-	σf	Cb+	Cb-	Ver.	CS
0.0	2063	--	12.06	12.06	-3	190	--	---	kg/cmq	---	---	6	Si 18.9
9.0	1799	--	12.06	12.06	-3	166	--	---	---	5	---	6	Si 21.7
44.8	894	--	12.06	12.06	-1	82	--	---	---	5	---	7	Si 43.7
80.6	773	--	12.06	12.06	-1	71	--	---	---	6	---	8	Si 50.5
89.6	864	--	12.06	12.06	-1	80	--	---	---	6	---	5	Si 45.2

Combinazione QP: σca[kg/cm²]=112 σfa[kg/cm²]=3600

X	M+	M-	Afup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cm²	kg/cm²	kg/cm²	kg/cm²				
0.0	673	--	12.06	12.06	-1	62	--	--	14	14	Si	58.1
9.0	583	--	12.06	12.06	-1	54	--	--	14	14	Si	67.0
44.8	314	--	12.06	12.06	-0	29	--	--	14	14	Si	>100
80.6	203	--	12.06	12.06	-0	19	--	--	14	14	Si	>100
89.6	202	--	12.06	12.06	-0	19	--	--	14	14	Si	>100

Verifica aperture fessure: Wamm. Freq[mm]=0.400 Wamm. Qp[mm]=0.300

X	cm	M	kg·m	Act	mq	Aft	cmq	pAft	cm	S _{rmax}	cm	defined	kg/cmq	mm	Wk	Cb	Ver.	Cs
0.0	-582	0.1	12.06	30.16	22.4	54	0.003	0.003	12(Fr)	Si	>100							
0.0	-673	0.1	12.06	30.16	22.4	62	0.004	0.004	14(Qp)	Si	75.7							
9.0	-583	0.1	12.06	30.16	22.4	54	0.003	0.003	14(Qp)	Si	87.4							
9.0	-515	0.1	12.06	30.16	22.4	47	0.003	0.003	12(Fr)	Si	>100							
44.8	-314	0.1	12.06	30.16	22.4	29	0.002	0.002	14(Qp)	Si	>100							
44.8	-314	0.1	12.06	30.16	22.4	29	0.002	0.002	9(Fr)	Si	>100							
80.6	-203	0.1	12.06	30.16	22.4	19	0.001	0.001	14(Qp)	Si	>100							
80.6	-203	0.1	12.06	30.16	22.4	19	0.001	0.001	9(Fr)	Si	>100							
89.6	-202	0.1	12.06	30.16	22.4	19	0.001	0.001	14(Qp)	Si	>100							
89.6	-185	0.1	12.06	30.16	22.4	17	0.001	0.001	11(Fr)	Si	>100							

Trave di Fond.: 9006 | 9. 10 | Pilastrate [14. 13]

Sec. R: B_y= 60.0 cm B_z= 100.0 cm B_z= 89.2 cm L_n= 101.2 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

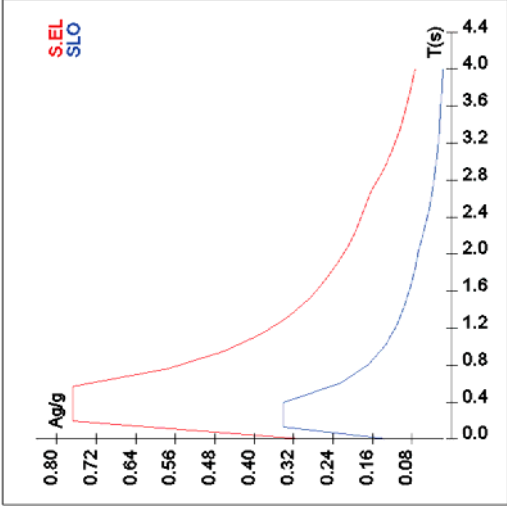
Combinazione Rara: σca[kg/cm²]=149 σfa[kg/cm²]=3600

X	M+	M-	Afup	Afinf	σc+	σc-	σf	Cb+	Ch-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	573	--	12.06	12.06	-1	53	--	6	8	Si	68.2
10.1	501	--	12.06	12.06	-1	46	--	6	8	Si	78.0
50.6	329	324	12.06	12.06	-1	30	-1	30	6	5	Si >100
91.1	336	148	12.06	12.06	-1	31	-0	14	6	5	Si >100
101.2	364	--	12.06	12.06	-1	34	--	6	5	Si	>100

Combinazione QP: σca[kg/cm²]=112 σfa[kg/cm²]=3600

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X	cm	M+	M-	Afup	Afinf	σc+	σf+	σc-	σf-	Ch+	Ch-	Ver.	CS
	0.0	206	--	12.06	12.06	-0	19	--	--	14	14	Si	>100
	10.1	118	--	12.06	12.06	-0	11	--	--	14	14	Si	>100
	50.6	--	74	12.06	12.06	--	--	-0	7	14	14	Si	>100
	91.1	30	--	12.06	12.06	-0	3	--	--	14	14	Si	>100
	101.2	107	--	12.06	12.06	-0	10	--	--	14	14	Si	>100



Caratteristiche del terreno

Terreno1- Cost. Winkler=10.00 kg/cm2										
Falda asseme										
Strato n°	Spessore cm	γ kg/mc	γSat kg/mc	φ °	Addensato	OCR	Coesione kg/cmq	Cu kg/cmq	E kg/cm2	v
1	100	1900	1900	35	No	--	0.00	0.00	2E02	0.30

[illegible]

336	Neve	-0	0	0	0	0	0
336	Vento X	-0	0	0	0	0	0
336	Vento X	0	-0	0	0	0	0
337	QP Sola	0	-0	0	0	0	0
337	QV Sola	-0	0	0	0	0	0
337	Neve	0	0	0	0	0	0
337	Neve	0	0	0	0	0	0
337	Vento X	0	-0	0	0	0	0
337	Vento X	0	0	0	0	0	0

Input - Aste - Tabella sezioni tipo		
Tipo	Nome	Raggio
	C	cm
	F16	l
	F14	l

Type	Nome	Area	lx	ly	lt	Fx	Fy	Lx	Lx
G		mq	m ⁴	m ⁴	m ⁴			cm	Lx
	IPE 100	0.0	1.710E-06	1.592E-07	8.826E-09	1.000	1.000	6	10
	HE 240 A	0.0	7.763E-05	2.769E-05	4.155E-07	1.000	1.000	24	23

Nome	Base	Altezza	Larg. mag.
R		cm	cm
F60x100		60	100
		60	120

Aste - Geometria e vincoli

Aste - Geometria e vincoli

Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	e	f.f.	xi	vi	zi	xf	yf	zf	Tipo	L2	L3	cm	
1	1	28	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	131	5050	0	0	0	0	0	0	0	Pila	204	204	
1	28	101	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	131	5050	0	0	0	0	0	0	0	Pila	204	204	
2	2	24	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	131	5050	0	0	0	0	0	0	0	Pila	204	204	
2	24	102	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	131	5050	0	0	0	0	0	0	0	Pila	204	204	
3	3	23	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	131	5050	0	0	0	0	0	0	0	Pila	204	204	
3	23	103	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	131	5050	0	0	0	0	0	0	0	Pila	204	204	
4	4	25	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	128	5050	0	0	0	0	0	0	0	Pila	204	204	
4	25	104	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	128	5050	0	0	0	0	0	0	0	Pila	204	204	
5	5	21	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	204	204	
5	21	105	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	204	204	
6	6	26	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	204	204	
6	26	106	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	204	204	
7	7	29	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	119	5050	0	0	0	0	0	0	0	Pila	204	204	
7	29	107	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	119	5050	0	0	0	0	0	0	0	Pila	204	204	
8	8	27	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	204	204	
8	27	108	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	204	204	
9	9	22	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	204	204	
9	22	109	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	204	204	
10	10	30	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	109	5050	0	0	0	0	0	0	0	Pila	204	204	
10	30	110	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	109	5050	0	0	0	0	0	0	0	Pila	204	204	
11	11	31	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	131	5050	0	0	0	0	0	0	0	Pila	140	140	
11	31	312	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	131	5050	0	0	0	0	0	0	0	Pila	140	140	
21	21	212	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	128	5050	0	0	0	0	0	0	0	Pila	140	140	
21	212	313	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	128	5050	0	0	0	0	0	0	0	Pila	140	140	
21	313	314	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	140	140	
21	314	315	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	140	140	
215	215	216	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	122	5050	0	0	0	0	0	0	0	Pila	140	140	
217	217	317	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	119	5050	0	0	0	0	0	0	0	Pila	140	140	
218	218	318	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	115	5050	0	0	0	0	0	0	0	Pila	140	140	
219	219	319	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	112	5050	0	0	0	0	0	0	0	Pila	140	140	
220	220	320	I-I	HE 240 A	Acciaio	Acciaio Pressiflessione	109	5050	0	0	0	0	0	0	0	Pila	140	140	
101	101	102	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	0	0	0	0	Trave	149	149	
102	102	103	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	0	0	0	0	Trave	149	149	
103	152	157	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	-0	0	0	0	Trave	149	149	
104	153	158	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	-0	0	0	0	Trave	149	149	
1005	154	159	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	-0	0	0	-1	-1	0	Trave	149	149	
1006	155	160	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	-1	0	0	-1	-1	0	Trave	149	149	
1007	233	235	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	-2	0	-0	0	-1	-1	Trave	149	149	
1008	234	236	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	-2	0	-0	0	0	0	Trave	149	149	
1009	339	335	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	-0	0	-1	-0	-1	0	Trave	149	149	
1010	334	336	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	0	-0	-1	0	Trave	149	149	
1011	311	312	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	-0	0	0	0	Trave	149	149	
1012	156	136	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	-0	0	-0	0	Trave	150	150	
1013	157	137	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	-0	0	-0	0	Trave	150	150	
1014	158	138	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	-0	0	-0	0	Trave	150	150	
1015	159	139	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	-0	0	-0	0	Trave	150	150	
1016	160	140	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	0	0	0	0	Trave	150	150	
1017	235	227	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	-1	0	0	0	0	Trave	150	150	
1018	236	228	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	0	0	0	-2	0	0	Trave	150	150	
1019	335	327	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	-0	0	-1	-0	-0	0	Trave	150	150	
1020	336	328	Cy-Cy	HE 100	Acciaio	Acciaio Flessione	0	8080	0	-0	0	-1	-0	-0	0	Trave	150	150	

[illegible][illegible]

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	OXf	OYf	QZf
HE 240 A	5	21	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	5	21	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	21	105	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	21	105	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	21	105	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	21	105	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastro 6												
HE 240 A	6	26	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	6	26	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	6	26	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	6	26	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	26	106	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	26	106	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	26	106	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	26	106	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastro 7												
HE 240 A	7	29	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	7	29	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	7	29	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	7	29	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	29	107	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	29	107	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	29	107	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	29	107	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastro 8												
HE 240 A	8	27	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	8	27	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	8	27	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	8	27	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	27	108	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	27	108	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	27	108	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	27	108	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastro 9												
HE 240 A	9	22	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	9	22	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	9	22	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	9	22	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	22	109	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	22	109	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	22	109	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	22	109	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastro 10												
HE 240 A	10	30	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	10	30	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	10	30	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	10	30	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	30	110	Peso Proprio	UnifG	0	0	0	60	204	0	0	60
HE 240 A	30	110	Vento X	UnifL	0	0	0	-255	204	0	0	-255
HE 240 A	30	110	Vento Y	UnifL	0	0	0	126	204	0	0	126
HE 240 A	30	110	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastro 211												
HE 240 A	211	311	Peso Proprio	UnifG	0	0	0	60	140	0	0	60
HE 240 A	211	311	Vento X	UnifL	0	0	0	-126	140	0	0	-126
HE 240 A	211	311	Vento Y	UnifL	0	0	0	225	140	0	0	225
HE 240 A	211	311	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastro 212												
HE 240 A	212	312	Peso Proprio	UnifG	0	0	0	60	140	0	0	60
HE 240 A	212	312	Vento X	UnifL	0	0	0	-126	140	0	0	-126
HE 240 A	212	312	Vento Y	UnifL	0	0	0	225	140	0	0	225
HE 240 A	212	312	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Piastro 213												
HE 240 A	213	313	Peso Proprio	UnifG	0	0	0	60	140	0	0	60
HE 240 A	213	313	Vento X	UnifL	0	0	0	-126	140	0	0	-126
HE 240 A	213	313	Vento Y	UnifL	0	0	0	225	140	0	0	225

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	OXf	OYf	QZf
HE 240 A	213	313	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Piastro 214												
HE 240 A	214	314	Peso Proprio	UnifG	0	0	0	60	140	0	0	60
HE 240 A	214	314	Vento X	UnifL	0	0	0	-126	140	0	0	-126
HE 240 A	214	314	Vento Y	UnifL	0	0	0	225	140	0	0	225
HE 240 A	214	314	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Piastro 215												
HE 240 A	215	315	Peso Proprio	UnifG	0	0	0	60	140	0	0	60
HE 240 A	215	315	Vento X	UnifL	0	0	0	-126	140	0	0	-126
HE 240 A	215	315	Vento Y	UnifL	0	0	0	225	140	0	0	225
HE 240 A	215	315	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Piastro 216												
HE 240 A	216	316	Peso Proprio	UnifG	0	0	0	60	140	0	0	60
HE 240 A	216	316	Vento X	UnifL	0	0	0	-126	140	0	0	-126
HE 240 A	216	316	Vento Y	UnifL	0	0	0	225	140	0	0	225
HE 240 A	216	316	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Piastro 217												
HE 240 A	217	317	Peso Proprio	UnifG	0	0	0	60	140	0	0	60
HE 240 A	217	317	Vento X	UnifL	0	0	0	-126	140	0	0	-126
HE 240 A	217	317	Vento Y	UnifL	0	0	0	225	140	0	0	225
HE 240 A	217	317	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Piastro 218												
HE 240 A	218	318	Peso Proprio	UnifG	0	0	0	60	140	0	0	60
HE 240 A	218	318	Vento X	UnifL	0	0	0	-126	140	0	0	-126
HE 240 A	218	318	Vento Y	UnifL	0	0	0	225	140	0	0	225
HE 240 A	218	318	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Piastro 219												
HE 240 A	219	319	Peso Proprio	UnifG	0	0	0	60	140	0	0	60
HE 240 A	219	319	Vento X	UnifL	0	0	0	-126	140	0	0	-126
HE 240 A	219	319	Vento Y	UnifL	0	0	0	225	140	0	0	225
HE 240 A	219	319	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Piastro 220												
HE 240 A	220	320	Peso Proprio	UnifG	0	0	0	60	140	0	0	60
HE 240 A	220	320	Vento X	UnifL	0	0	0	-126	140	0	0	-126
HE 240 A	220	320	Vento Y	UnifL	0	0	0	225	140	0	0	225
HE 240 A	220	320	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1001												
IPE 100	101	102	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	101	102	QP Solai	PolG	0	0	0	71	54	0	0	71
					54	0	0	71	122	0	0	91
					122	0	0	91	149	0	0	71
IPE 100	101	102	QV Solai	PolG	0	0	0	23	54	0	0	23
					54	0	0	23	122	0	0	29
					122	0	0	29	149	0	0	23
IPE 100	101	102	Neve	PolG	0	0	0	44	54	0	0	44
					54	0	0	44	122	0	0	57
					122	0	0	57	149	0	0	44
IPE 100	101	102	Vento X	PolG	0	0	0	68	54	0	0	68
					54	0	0	68	122	0	0	87
					122	0	0	87	149	0	0	68
IPE 100	101	102	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 1002												
IPE 100	151	156	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	151	156	QP Solai	PolG	0	0	0	140	27	0	0	160
					27	0	0	160	54	0	0	152
					54	0	0	152	95	0	0	152
					95	0	0	152	122	0	0	160
					122	0	0	160	149	0	0	140
IPE 100	151	156	QV Solai	PolG	0	0	0	45	27	0	0	51
					27	0	0	51	54	0	0	49
					54	0	0	49	95	0	0	49
					95	0	0	49	122	0	0	51
					122	0	0	51	149	0	0	45
IPE 100	151	156	Neve	PolG	0	0	0	43	54	0	0	43
					54	0	0	43	122	0	0	55

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	151	156	Neve	PolG	122	0	0	55	149	0	0	43
					27	0	0	44	27	0	0	57
IPE 100	151	156	Vento X	PolG	95	0	0	44	149	0	0	44
					0	0	0	68	27	0	0	87
					27	0	0	87	95	0	0	68
IPE 100	151	156	Vento X	PolG	95	0	0	68	149	0	0	68
					54	0	0	67	54	0	0	67
					86	0	0	67	122	0	0	86
IPE 100	151	156	Carichi termici	Termico	122	0	0	86	149	0	0	67
Trave 1003												
IPE 100	152	157	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	152	157	QP Solai	PolG	0	0	0	136	27	0	0	155
					27	0	0	155	54	0	0	147
					54	0	0	147	95	0	0	147
					95	0	0	147	122	0	0	154
IPE 100	152	157	QV Solai	PolG	122	0	0	154	149	0	0	136
					0	0	0	43	27	0	0	50
					27	0	0	50	54	0	0	47
					54	0	0	47	95	0	0	47
					95	0	0	47	122	0	0	49
					122	0	0	49	149	0	0	43
IPE 100	152	157	Neve	PolG	0	0	0	43	27	0	0	55
					27	0	0	55	95	0	0	43
IPE 100	152	157	Neve	PolG	95	0	0	43	149	0	0	43
					0	0	0	41	54	0	0	41
					54	0	0	41	122	0	0	53
IPE 100	152	157	Vento X	PolG	122	0	0	53	149	0	0	41
					0	0	0	67	27	0	0	86
					27	0	0	86	95	0	0	67
IPE 100	152	157	Vento X	PolG	95	0	0	67	149	0	0	67
					0	0	0	64	54	0	0	64
					54	0	0	64	122	0	0	82
IPE 100	152	157	Carichi termici	Termico	122	0	0	82	149	0	0	64
Trave 1004												
IPE 100	153	158	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	153	158	QP Solai	PolG	0	0	0	128	27	0	0	147
					27	0	0	147	54	0	0	139
					54	0	0	139	95	0	0	139
					95	0	0	139	122	0	0	146
IPE 100	153	158	QV Solai	PolG	122	0	0	146	149	0	0	128
					0	0	0	41	27	0	0	47
					27	0	0	47	54	0	0	45
					54	0	0	45	95	0	0	44
					95	0	0	44	122	0	0	47
IPE 100	153	158	Neve	PolG	122	0	0	47	149	0	0	41
					0	0	0	38	54	0	0	38
IPE 100	153	158	Vento X	PolG	54	0	0	38	122	0	0	49
					122	0	0	49	149	0	0	38
IPE 100	153	158	Neve	PolG	0	0	0	41	27	0	0	53
					27	0	0	53	95	0	0	41
IPE 100	153	158	Vento X	PolG	95	0	0	41	149	0	0	41
					0	0	0	59	54	0	0	59
					54	0	0	59	122	0	0	76
IPE 100	153	158	Vento X	PolG	122	0	0	76	149	0	0	59
					0	0	0	64	27	0	0	82
					27	0	0	82	95	0	0	64
IPE 100	153	158	Carichi termici	Termico	95	0	0	64	149	0	0	64
Trave 1005												
IPE 100	154	159	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	154	159	QP Solai	PolG	0	0	0	120	27	0	0	137
					27	0	0	137	54	0	0	130
					54	0	0	130	95	0	0	129

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	154	159	QV Solai	PolG	122	0	0	136	149	0	0	120
					0	0	0	38	27	0	0	44
					27	0	0	44	54	0	0	42
					54	0	0	42	95	0	0	41
					95	0	0	41	122	0	0	44
IPE 100	154	159	Neve	PolG	122	0	0	44	149	0	0	38
					0	0	0	36	54	0	0	36
					54	0	0	36	122	0	0	46
IPE 100	154	159	Neve	PolG	122	0	0	46	149	0	0	36
					0	0	0	38	27	0	0	49
					27	0	0	49	95	0	0	38
IPE 100	154	159	Vento X	PolG	95	0	0	38	149	0	0	38
					27	0	0	59	27	0	0	76
					27	0	0	76	95	0	0	59
IPE 100	154	159	Vento X	PolG	95	0	0	59	149	0	0	59
					0	0	0	55	54	0	0	55
					54	0	0	55	122	0	0	71
IPE 100	154	159	Carichi termici	Termico	122	0	0	55	122	0	0	71
					122	0	0	71	149	0	0	55
Trave 1006												
IPE 100	155	160	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	155	160	QP Solai	PolG	0	0	0	110	27	0	0	126
					27	0	0	126	54	0	0	120
					54	0	0	120	95	0	0	119
					95	0	0	119	122	0	0	125
IPE 100	155	160	QV Solai	PolG	122	0	0	125	149	0	0	110
					0	0	0	35	27	0	0	41
					27	0	0	41	54	0	0	38
					54	0	0	38	95	0	0	38
					95	0	0	38	122	0	0	40
IPE 100	155	160	Neve	PolG	122	0	0	33	54	0	0	33
					0	0	0	33	122	0	0	42
					54	0	0	42	149	0	0	33
IPE 100	155	160	Neve	PolG	122	0	0	36	27	0	0	46
					27	0	0	46	95	0	0	36
IPE 100	155	160	Vento X	PolG	95	0	0	36	149	0	0	36
					27	0	0	55	27	0	0	71
					27	0	0	71	95	0	0	55
IPE 100	155	160	Vento X	PolG	95	0	0	55	149	0	0	55
					0	0	0	50	54	0	0	50
					54	0	0	50	122	0	0	65
IPE 100	155	160	Carichi termici	Termico	122	0	0	65	149	0	0	50
					122	0	0	50	122	0	0	65
Trave 1007												
IPE 100	233	235	Peso Proprio	UnifG	0	0	0	8	149	0	0	8
IPE 100	233	235	QP Solai	PolG	0	0	0	100	27	0	0	115
					27	0	0	115	54	0	0	109
					54	0	0	109	95	0	0	108
					95	0	0	108	122	0	0	114
IPE 100	233	235	QV Solai	PolG	122	0	0	114	149	0	0	100
					0	0	0	32	27	0	0	37
					27	0	0	37	54	0	0	35
					54	0	0	35	95	0	0	35
					95	0	0	35	122	0	0	36
IPE 100	233	235	Neve	PolG	122	0	0	36	149	0	0	32
					0	0	0	30	54	0	0	30
					54	0	0	30	122	0	0	38
IPE 100	233	235	Neve	PolG	122	0	0	38	149	0	0	30
					0	0	0	33	27	0	0	42
					27	0	0	42	95	0	0	33
IPE 100	233	235	Vento X	PolG	95	0	0	33	149	0	0	33
					0	0	0	46	54	0	0	46
					54	0	0	46	122	0	0	59
					122	0	0	59	149	0	0	46

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	233	235	Vento X	PolG	0	0	0	50	27	0	0	65
					27	0	0	65	95	0	0	50
IPE 100	233	235	Carichi termici	Termico	95	0	0	50	149	0	0	50
Trave 1008												
IPE 100	234	236	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	234	236	QP Solai	PolG	0	0	0	92	27	0	0	106
					27	0	0	106	54	0	0	100
					54	0	0	100	95	0	0	100
					95	0	0	100	122	0	0	105
					122	0	0	105	149	0	0	92
IPE 100	234	236	QV Solai	PolG	0	0	0	29	27	0	0	34
					27	0	0	34	54	0	0	32
					54	0	0	32	95	0	0	32
					95	0	0	32	122	0	0	34
IPE 100	234	236	Neve	PolG	0	0	0	34	149	0	0	29
					27	0	0	27	54	0	0	27
					54	0	0	27	122	0	0	35
IPE 100	234	236	Neve	PolG	0	0	0	35	149	0	0	27
					122	0	0	30	27	0	0	38
					27	0	0	38	95	0	0	30
IPE 100	234	236	Vento X	PolG	0	0	0	30	149	0	0	30
					95	0	0	46	27	0	0	59
					27	0	0	59	95	0	0	46
IPE 100	234	236	Vento X	PolG	0	0	0	46	149	0	0	46
					95	0	0	42	54	0	0	42
					54	0	0	42	122	0	0	55
IPE 100	234	236	Carichi termici	Termico	122	0	0	55	149	0	0	42
Trave 1009												
IPE 100	333	335	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	333	335	QP Solai	PolG	0	0	0	86	27	0	0	99
					27	0	0	99	54	0	0	94
					54	0	0	94	95	0	0	94
					95	0	0	94	122	0	0	98
IPE 100	333	335	QV Solai	PolG	0	0	0	98	149	0	0	86
					122	0	0	28	27	0	0	32
					27	0	0	32	54	0	0	30
					54	0	0	30	95	0	0	30
					95	0	0	30	122	0	0	32
IPE 100	333	335	Neve	PolG	0	0	0	32	149	0	0	28
					122	0	0	26	54	0	0	26
					54	0	0	26	122	0	0	34
IPE 100	333	335	Neve	PolG	0	0	0	34	149	0	0	26
					27	0	0	27	27	0	0	35
					27	0	0	35	95	0	0	27
IPE 100	333	335	Vento X	PolG	0	0	0	42	27	0	0	55
					27	0	0	55	95	0	0	42
IPE 100	333	335	Vento X	PolG	0	0	0	42	149	0	0	42
					95	0	0	41	54	0	0	41
					54	0	0	41	122	0	0	52
IPE 100	333	335	Carichi termici	Termico	122	0	0	52	149	0	0	41
Trave 1010												
IPE 100	334	336	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	334	336	QP Solai	PolG	0	0	0	86	27	0	0	98
					27	0	0	98	54	0	0	93
					54	0	0	93	95	0	0	94
					95	0	0	94	122	0	0	98
IPE 100	334	336	QV Solai	PolG	0	0	0	98	149	0	0	86
					122	0	0	28	27	0	0	31
					27	0	0	31	54	0	0	30
					54	0	0	30	95	0	0	30
					95	0	0	30	122	0	0	32
IPE 100	334	336	Neve	PolG	0	0	0	32	149	0	0	28

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	334	336	Neve	PolG	0	0	0	27	54	0	0	27
					54	0	0	27	122	0	0	35
IPE 100	334	336	Neve	PolG	0	0	0	35	149	0	0	27
					122	0	0	26	27	0	0	34
					27	0	0	34	95	0	0	26
IPE 100	334	336	Vento X	PolG	0	0	0	26	149	0	0	26
					95	0	0	42	54	0	0	42
					54	0	0	42	122	0	0	54
IPE 100	334	336	Vento X	PolG	0	0	0	54	149	0	0	42
					122	0	0	41	27	0	0	52
					27	0	0	52	95	0	0	41
IPE 100	334	336	Carichi termici	Termico	95	0	0	41	149	0	0	41
Trave 1011												
IPE 100	311	312	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	311	312	QP Solai	PolG	0	0	0	44	27	0	0	56
					27	0	0	56	95	0	0	44
					95	0	0	44	149	0	0	44
IPE 100	311	312	QV Solai	PolG	0	0	0	14	27	0	0	18
					27	0	0	18	95	0	0	14
					95	0	0	14	149	0	0	14
IPE 100	311	312	Neve	PolG	0	0	0	27	27	0	0	35
					27	0	0	35	95	0	0	27
					95	0	0	27	149	0	0	27
IPE 100	311	312	Vento X	PolG	0	0	0	42	27	0	0	54
					27	0	0	54	95	0	0	42
					95	0	0	42	149	0	0	42
IPE 100	311	312	Carichi termici	Termico	95	0	0	42	149	0	0	42
Trave 1012												
IPE 100	156	136	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	156	136	QP Solai	PolG	0	0	0	140	28	0	0	161
					28	0	0	161	54	0	0	153
					54	0	0	153	96	0	0	153
					96	0	0	153	122	0	0	161
IPE 100	156	136	QV Solai	PolG	0	0	0	161	150	0	0	140
					122	0	0	45	28	0	0	52
					28	0	0	52	54	0	0	49
					54	0	0	49	96	0	0	49
					96	0	0	49	122	0	0	51
					122	0	0	51	150	0	0	45
IPE 100	156	136	Neve	PolG	0	0	0	43	54	0	0	43
					54	0	0	43	122	0	0	56
					122	0	0	56	150	0	0	43
IPE 100	156	136	Neve	PolG	0	0	0	44	28	0	0	57
					28	0	0	57	96	0	0	44
					96	0	0	44	150	0	0	44
IPE 100	156	136	Vento X	PolG	0	0	0	67	54	0	0	67
					54	0	0	67	122	0	0	86
					122	0	0	86	150	0	0	67
IPE 100	156	136	Vento X	PolG	0	0	0	88	28	0	0	88
					28	0	0	88	96	0	0	68
					96	0	0	68	150	0	0	68
IPE 100	156	136	Carichi termici	Termico	96	0	0	68	150	0	0	68
Trave 1013												
IPE 100	157	137	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	157	137	QP Solai	PolG	0	0	0	135	28	0	0	156
					28	0	0	156	54	0	0	148
					54	0	0	148	96	0	0	147
					96	0	0	147	122	0	0	155
IPE 100	157	137	QV Solai	PolG	0	0	0	155	150	0	0	135
					122	0	0	43	28	0	0	50
					28	0	0	50	54	0	0	47
					54	0	0	47	96	0	0	47
					96	0	0	47	122	0	0	50
IPE 100	157	137	Neve	PolG	0	0	0	43	28	0	0	56

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
					28	0	0	0	56	96	0	43
IPE 100	157	137	Neve	PolG	96	0	0	43	150	0	0	43
					54	0	0	41	54	0	0	41
IPE 100			Vento X	PolG	122	0	0	53	150	0	0	41
	157	137			0	0	0	67	28	0	0	86
					28	0	0	86	96	0	0	67
IPE 100	157	137	Vento X	PolG	96	0	0	67	150	0	0	67
					54	0	0	64	54	0	0	64
IPE 100					122	0	0	82	150	0	0	82
	157	137	Carichi termici	Termico	122	0	0	82	150	0	0	64
Trave 1014 ΔXY=15°C, ΔXZ=15°C												
IPE 100	158	138	Peso Proprio	UnifG	0	0	0	0	8	150	0	8
IPE 100	158	138	QV Solai	PolG	0	0	0	128	28	0	0	148
					28	0	0	148	54	0	0	140
					54	0	0	140	96	0	0	139
					96	0	0	139	122	0	0	146
IPE 100			QV Solai	PolG	122	0	0	146	150	0	0	128
	158	138			0	0	0	41	28	0	0	47
					28	0	0	47	54	0	0	45
					54	0	0	45	96	0	0	45
					96	0	0	45	122	0	0	47
IPE 100	158	138	Neve	PolG	122	0	0	47	150	0	0	41
			Neve	PolG	0	0	0	38	54	0	0	38
IPE 100			Vento X	PolG	54	0	0	38	122	0	0	50
					122	0	0	50	150	0	0	38
IPE 100	158	138	Neve	PolG	0	0	0	41	28	0	0	53
					28	0	0	53	96	0	0	41
IPE 100	158	138	Vento X	PolG	96	0	0	41	150	0	0	41
					28	0	0	64	28	0	0	82
IPE 100			Vento X	PolG	28	0	0	82	96	0	0	64
	158	138			96	0	0	64	150	0	0	64
IPE 100			Vento X	PolG	54	0	0	59	54	0	0	59
					122	0	0	59	122	0	0	77
IPE 100	158	138	Carichi termici	Termico	122	0	0	77	150	0	0	59
Trave 1015 ΔXY=15°C, ΔXZ=15°C												
IPE 100	159	139	Peso Proprio	UnifG	0	0	0	0	8	150	0	8
IPE 100	159	139	QV Solai	PolG	0	0	0	119	28	0	0	138
					28	0	0	138	54	0	0	131
					54	0	0	131	96	0	0	130
					96	0	0	130	122	0	0	136
IPE 100	159	139	QV Solai	PolG	122	0	0	136	150	0	0	119
					28	0	0	38	28	0	0	44
					54	0	0	44	54	0	0	42
					96	0	0	42	96	0	0	42
IPE 100			Neve	PolG	122	0	0	44	150	0	0	38
	159	139	Neve	PolG	0	0	0	38	28	0	0	50
IPE 100	159	139	Vento X	PolG	28	0	0	50	96	0	0	38
			Neve	PolG	96	0	0	38	150	0	0	38
	159	139			0	0	0	36	54	0	0	36
					54	0	0	36	122	0	0	46
IPE 100	159	139	Vento X	PolG	122	0	0	46	150	0	0	36
					54	0	0	55	54	0	0	55
IPE 100	159	139	Vento X	PolG	28	0	0	72	150	0	0	72
					122	0	0	72	150	0	0	55
IPE 100	159	139	Vento X	PolG	0	0	0	59	28	0	0	77
					28	0	0	77	96	0	0	59
IPE 100	159	139	Carichi termici	Termico	96	0	0	59	150	0	0	59
Trave 1016 ΔXY=15°C, ΔXZ=15°C												
IPE 100	160	140	Peso Proprio	UnifG	0	0	0	0	8	150	0	8
IPE 100	160	140	QV Solai	PolG	0	0	0	110	28	0	0	127
					28	0	0	127	54	0	0	120

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
					54	0	0	0	120	95	0	119
					95	0	0	0	119	122	0	125
IPE 100	160	140	QV Solai	PolG	122	0	0	0	125	150	0	110
					0	0	0	35	28	0	0	41
					28	0	0	41	54	0	0	39
					54	0	0	39	95	0	0	38
					95	0	0	38	122	0	0	40
IPE 100	160	140	Neve	PolG	122	0	0	40	150	0	0	35
					0	0	0	33	54	0	0	33
IPE 100					54	0	0	33	122	0	0	42
					122	0	0	42	150	0	0	33
	160	140	Neve	PolG	0	0	0	36	28	0	0	46
					28	0	0	46	95	0	0	36
IPE 100	160	140	Vento X	PolG	95	0	0	36	150	0	0	36
					0	0	0	55	28	0	0	72
					28	0	0	72	95	0	0	55
IPE 100	160	140	Vento X	PolG	95	0	0	55	150	0	0	55
					0	0	0	50	54	0	0	50
IPE 100					54	0	0	50	122	0	0	65
					122	0	0	65	150	0	0	50
Trave 1017 ΔXY=15°C, ΔXZ=15°C												
IPE 100	235	227	Peso Proprio	UnifG	0	0	0	0	8	150	0	8
IPE 100	235	227	QV Solai	PolG	0	0	0	100	28	0	0	115
					28	0	0	115	54	0	0	109
					54	0	0	109	95	0	0	109
					95	0	0	109	122	0	0	114
IPE 100	235	227	QV Solai	PolG	122	0	0	114	150	0	0	100
					0	0	0	32	28	0	0	37
					28	0	0	37	54	0	0	35
					54	0	0	35	95	0	0	35
					95	0	0	35	122	0	0	37
					122	0	0	37	150	0	0	32
IPE 100	235	227	Neve	PolG	0	0	0	30	54	0	0	30
					54	0	0	30	122	0	0	38
IPE 100	235	227	Neve	PolG	122	0	0	38	150	0	0	30
					0	0	0	33	28	0	0	42
					28	0	0	42	95	0	0	33
IPE 100	235	227	Vento X	PolG	95	0	0	46	54	0	0	46
					54	0	0	46	122	0	0	59
IPE 100	235	227	Vento X	PolG	122	0	0	59	150	0	0	46
					0	0	0	50	28	0	0	65
					28	0	0	65	95	0	0	50
IPE 100	235	227	Carichi termici	Termico	95	0	0	50	150	0	0	50
Trave 1018 ΔXY=15°C, ΔXZ=15°C												
IPE 100	236	228	Peso Proprio	UnifG	0	0	0	0	8	150	0	8
IPE 100	236	228	QV Solai	PolG	0	0	0	92	28	0	0	106
					28	0	0	106	54	0	0	100
					54	0	0	100	95	0	0	100
					95	0	0	100	122	0	0	105
IPE 100	236	228	QV Solai	PolG	122	0	0	105	150	0	0	92
					0	0	0	29	28	0	0	34
					28	0	0	34	54	0	0	32
					54	0	0	32	95	0	0	32
					95	0	0	32	122	0	0	34
IPE 100	236	228	Neve	PolG	122	0	0	34	150	0	0	29
					0	0	0	30	28	0	0	38
					28	0	0	38	95	0	0	30
IPE 100	236	228	Neve	PolG	95	0	0	30	150	0	0	30
					0	0	0	27	54	0	0	27
					54	0	0	27	122	0	0	35
IPE 100	236	228	Vento X	PolG	122	0	0	35	150	0	0	27
					0	0	0	42	54	0	0	42
					54	0	0	42	122	0	0	55

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	236	228	Vento X	PolG	0	0	0	55	150	0	0	42
					28	0	0	46	28	0	0	59
					95	0	0	59	95	0	0	46
IPE 100	236	228	Carichi termici	Termico	95	0	0	46	150	0	0	46
Trave 1019 AXY=15°C, AXZ=15°C												
IPE 100	335	327	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	335	327	QP Solai	PolG	0	0	0	86	27	0	0	99
					27	0	0	99	54	0	0	94
					54	0	0	94	95	0	0	94
					95	0	0	94	122	0	0	98
					122	0	0	98	150	0	0	86
IPE 100	335	327	QV Solai	PolG	0	0	0	28	27	0	0	32
					27	0	0	32	54	0	0	30
					54	0	0	30	95	0	0	30
					95	0	0	30	122	0	0	32
					122	0	0	32	150	0	0	28
IPE 100	335	327	Neve	PolG	0	0	0	27	27	0	0	35
					27	0	0	35	95	0	0	27
					95	0	0	27	150	0	0	27
IPE 100	335	327	Neve	PolG	0	0	0	26	54	0	0	26
					54	0	0	26	122	0	0	34
					122	0	0	34	150	0	0	26
IPE 100	335	327	Vento X	PolG	0	0	0	41	54	0	0	41
					54	0	0	41	122	0	0	52
					122	0	0	52	150	0	0	41
IPE 100	335	327	Vento X	PolG	0	0	0	42	27	0	0	55
					27	0	0	55	95	0	0	42
					95	0	0	42	150	0	0	42
IPE 100	335	327	Carichi termici	Termico	95	0	0	42	150	0	0	42
Trave 1020 AXY=15°C, AXZ=15°C												
IPE 100	336	328	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	336	328	QP Solai	PolG	0	0	0	86	27	0	0	98
					27	0	0	98	54	0	0	93
					54	0	0	93	95	0	0	94
					95	0	0	94	122	0	0	99
					122	0	0	99	150	0	0	86
IPE 100	336	328	QV Solai	PolG	0	0	0	28	27	0	0	31
					27	0	0	31	54	0	0	30
					54	0	0	30	95	0	0	30
					95	0	0	30	122	0	0	32
					122	0	0	32	150	0	0	28
IPE 100	336	328	Neve	PolG	0	0	0	26	27	0	0	34
					27	0	0	34	95	0	0	26
					95	0	0	26	150	0	0	26
IPE 100	336	328	Neve	PolG	0	0	0	27	54	0	0	27
					54	0	0	27	122	0	0	35
					122	0	0	35	150	0	0	27
IPE 100	336	328	Vento X	PolG	0	0	0	41	27	0	0	52
					27	0	0	52	95	0	0	41
					95	0	0	41	150	0	0	41
IPE 100	336	328	Vento X	PolG	0	0	0	42	54	0	0	42
					54	0	0	42	122	0	0	54
					122	0	0	54	150	0	0	42
IPE 100	336	328	Carichi termici	Termico	95	0	0	42	150	0	0	42
Trave 1021 AXY=15°C, AXZ=15°C												
IPE 100	312	313	Peso Proprio	UnifG	0	0	0	8	137	0	0	8
IPE 100	312	313	QP Solai	PolG	0	0	0	44	27	0	0	56
					27	0	0	56	95	0	0	44
					95	0	0	44	149	0	0	44
IPE 100	312	313	QV Solai	PolG	0	0	0	14	27	0	0	18
					27	0	0	18	95	0	0	14
					95	0	0	14	149	0	0	14
IPE 100	312	313	Neve	PolG	0	0	0	27	27	0	0	35
					27	0	0	35	95	0	0	27
					95	0	0	27	149	0	0	27

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	312	313	Vento X	PolG	0	0	0	42	27	0	0	54
					27	0	0	54	95	0	0	42
					95	0	0	42	149	0	0	42
IPE 100	312	313	Carichi termici	Termico	95	0	0	42	149	0	0	42
Trave 1022 AXY=15°C, AXZ=15°C												
IPE 100	102	103	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	102	103	QP Solai	PolG	0	0	0	71	54	0	0	71
					54	0	0	71	122	0	0	92
					122	0	0	92	150	0	0	71
IPE 100	102	103	QV Solai	PolG	0	0	0	23	54	0	0	23
					54	0	0	23	122	0	0	29
					122	0	0	29	150	0	0	23
IPE 100	102	103	Neve	PolG	0	0	0	44	54	0	0	44
					54	0	0	44	122	0	0	57
					122	0	0	57	150	0	0	44
IPE 100	102	103	Vento X	PolG	0	0	0	68	54	0	0	68
					54	0	0	68	122	0	0	88
					122	0	0	88	150	0	0	68
IPE 100	102	103	Carichi termici	Termico	95	0	0	42	150	0	0	42
Trave 1023 AXY=15°C, AXZ=15°C												
IPE 100	137	147	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	137	147	QP Solai	PolG	0	0	0	118	15	0	0	121
					15	0	0	121	92	0	0	123
					92	0	0	123	101	0	0	121
IPE 100	137	147	QV Solai	PolG	0	0	0	38	15	0	0	39
					15	0	0	39	92	0	0	39
					92	0	0	39	101	0	0	39
IPE 100	137	147	Neve	PolG	0	0	0	41	15	0	0	41
					15	0	0	41	101	0	0	32
IPE 100	137	147	Neve	PolG	0	0	0	32	92	0	0	43
					92	0	0	43	101	0	0	43
IPE 100	137	147	Vento X	PolG	0	0	0	64	15	0	0	64
					15	0	0	64	101	0	0	50
IPE 100	137	147	Vento X	PolG	0	0	0	50	92	0	0	67
					92	0	0	67	101	0	0	67
IPE 100	137	147	Carichi termici	Termico	95	0	0	42	150	0	0	42
Trave 1024 AXY=15°C, AXZ=15°C												
IPE 100	138	148	Peso Proprio	UnifG	0	0	0	8	107	0	0	8
IPE 100	138	148	QP Solai	PolG	0	0	0	115	21	0	0	118
					21	0	0	118	92	0	0	120
					92	0	0	120	107	0	0	118
IPE 100	138	148	QV Solai	PolG	0	0	0	37	21	0	0	38
					21	0	0	38	92	0	0	38
					92	0	0	38	107	0	0	38
IPE 100	138	148	Neve	PolG	0	0	0	33	92	0	0	41
					92	0	0	41	107	0	0	41
IPE 100	138	148	Neve	PolG	0	0	0	38	21	0	0	38
					21	0	0	38	107	0	0	32
IPE 100	138	148	Vento X	PolG	0	0	0	59	21	0	0	59
					21	0	0	59	107	0	0	50
IPE 100	138	148	Vento X	PolG	0	0	0	51	92	0	0	64
					92	0	0	64	107	0	0	64
IPE 100	138	148	Carichi termici	Termico	95	0	0	42	150	0	0	42
Trave 1025 AXY=15°C, AXZ=15°C												
IPE 100	139	149	Peso Proprio	UnifG	0	0	0	8	113	0	0	8
IPE 100	139	149	QP Solai	PolG	0	0	0	110	27	0	0	113
					27	0	0	113	92	0	0	114
					92	0	0	114	113	0	0	113
IPE 100	139	149	QV Solai	PolG	0	0	0	35	27	0	0	36
					27	0	0	36	92	0	0	37
					92	0	0	37	113	0	0	36
IPE 100	139	149	Neve	PolG	0	0	0	36	27	0	0	36
					27	0	0	36	113	0	0	32
IPE 100	139	149	Neve	PolG	0	0	0	32	92	0	0	38
					92	0	0	38	113	0	0	38
IPE 100	139	149	Vento X	PolG	0	0	0	50	92	0	0	59

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	139	149	Vento X	PolG	0	0	0	59	113	0	0	59
IPE 100	139	149		PolG	0	0	0	55	27	0	0	55
IPE 100	139	149	Carichi termici	Termico	27	0	0	55	113	0	0	49
Trave 1026 AXY=15°C, AXZ=15°C												
IPE 100	140	150	Peso Proprio	UnifG	0	0	0	8	119	0	0	8
IPE 100	140	150	QP Solai	PolG	0	0	0	104	33	0	0	106
IPE 100	140	150		PolG	33	0	0	106	92	0	0	108
IPE 100	140	150	QV Solai	PolG	92	0	0	108	119	0	0	106
IPE 100	140	150		PolG	0	0	0	33	33	0	0	34
IPE 100	140	150		PolG	33	0	0	34	92	0	0	34
IPE 100	140	150		PolG	92	0	0	34	119	0	0	34
IPE 100	140	150	Neve	PolG	0	0	0	33	33	0	0	33
IPE 100	140	150	Neve	PolG	33	0	0	33	119	0	0	30
IPE 100	140	150	Neve	PolG	0	0	0	32	92	0	0	36
IPE 100	140	150	Vento X	PolG	92	0	0	36	119	0	0	36
IPE 100	140	150		PolG	0	0	0	49	92	0	0	55
IPE 100	140	150	Vento X	PolG	92	0	0	55	119	0	0	55
IPE 100	140	150	Vento X	PolG	0	0	0	50	33	0	0	50
IPE 100	140	150		PolG	33	0	0	50	119	0	0	47
IPE 100	140	150	Carichi termici	Termico	33	0	0	50	119	0	0	47
Trave 1027 AXY=15°C, AXZ=15°C												
IPE 100	227	231	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	227	231	QP Solai	PolG	0	0	0	97	92	0	0	99
IPE 100	227	231		PolG	92	0	0	99	125	0	0	99
IPE 100	227	231	QV Solai	PolG	0	0	0	31	92	0	0	32
IPE 100	227	231		PolG	92	0	0	32	125	0	0	32
IPE 100	227	231	Neve	PolG	0	0	0	30	125	0	0	29
IPE 100	227	231	Neve	PolG	0	0	0	30	92	0	0	33
IPE 100	227	231	Neve	PolG	92	0	0	33	125	0	0	33
IPE 100	227	231	Vento X	PolG	0	0	0	47	92	0	0	50
IPE 100	227	231	Vento X	PolG	92	0	0	50	125	0	0	50
IPE 100	227	231	Vento X	PolG	0	0	0	46	125	0	0	45
IPE 100	227	231	Carichi termici	Termico	46	0	0	46	125	0	0	45
Trave 1028 AXY=15°C, AXZ=15°C												
IPE 100	228	232	Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	228	232	QP Solai	PolG	0	0	0	91	45	0	0	91
IPE 100	228	232		PolG	45	0	0	91	127	0	0	94
IPE 100	228	232	QV Solai	PolG	127	0	0	94	131	0	0	92
IPE 100	228	232	Neve	PolG	0	0	0	29	131	0	0	29
IPE 100	228	232	Neve	PolG	0	0	0	27	45	0	0	27
IPE 100	228	232	Neve	PolG	45	0	0	27	127	0	0	29
IPE 100	228	232		PolG	127	0	0	29	131	0	0	27
IPE 100	228	232	Neve	PolG	0	0	0	29	131	0	0	30
IPE 100	228	232	Vento X	PolG	0	0	0	42	45	0	0	42
IPE 100	228	232	Vento X	PolG	45	0	0	42	127	0	0	44
IPE 100	228	232		PolG	127	0	0	44	131	0	0	42
IPE 100	228	232	Vento X	PolG	0	0	0	45	131	0	0	46
IPE 100	228	232	Carichi termici	Termico	45	0	0	45	131	0	0	46
Trave 1029 AXY=15°C, AXZ=15°C												
IPE 100	327	331	Peso Proprio	UnifG	0	0	0	8	137	0	0	8
IPE 100	327	331	QP Solai	PolG	0	0	0	86	4	0	0	88
IPE 100	327	331		PolG	4	0	0	88	51	0	0	87
IPE 100	327	331	QV Solai	PolG	51	0	0	87	93	0	0	89
IPE 100	327	331	Neve	PolG	93	0	0	89	127	0	0	91
IPE 100	327	331	Neve	PolG	127	0	0	91	137	0	0	86
IPE 100	327	331	QV Solai	PolG	0	0	0	28	51	0	0	28
IPE 100	327	331		PolG	51	0	0	28	127	0	0	29
IPE 100	327	331	Neve	PolG	127	0	0	29	137	0	0	28
IPE 100	327	331	Neve	PolG	0	0	0	27	4	0	0	29
IPE 100	327	331	Neve	PolG	4	0	0	29	93	0	0	27
IPE 100	327	331	Neve	PolG	93	0	0	27	137	0	0	27
IPE 100	327	331	Neve	PolG	0	0	0	26	51	0	0	26
IPE 100	327	331	Neve	PolG	51	0	0	26	127	0	0	29
IPE 100	327	331	Vento X	PolG	127	0	0	29	137	0	0	26

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
					4	0	0	0	44	93	0	0
					93	0	0	0	42	137	0	0
IPE 100	327	331	Vento X	PolG	0	0	0	0	41	51	0	0
					51	0	0	0	41	127	0	0
					127	0	0	0	45	137	0	0
IPE 100	327	331	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1030												
IPE 100	328	332	Peso Proprio	UnifG	0	0	0	0	8	143	0	0
IPE 100	328	332	QP Solai	PolG	0	0	0	0	86	10	0	0
					10	0	0	0	90	57	0	0
					57	0	0	0	88	93	0	0
					93	0	0	0	90	127	0	0
					127	0	0	0	94	143	0	0
IPE 100	328	332	QV Solai	PolG	0	0	0	0	28	10	0	0
					10	0	0	0	29	57	0	0
					57	0	0	0	28	93	0	0
IPE 100					93	0	0	0	29	127	0	0
					127	0	0	0	30	143	0	0
IPE 100	328	332	Neve	PolG	0	0	0	0	27	57	0	0
					57	0	0	0	27	127	0	0
					127	0	0	0	32	143	0	0
IPE 100	328	332	Neve	PolG	0	0	0	0	26	10	0	0
					10	0	0	0	29	93	0	0
					93	0	0	0	26	143	0	0
IPE 100	328	332	Vento X	PolG	0	0	0	0	41	10	0	0
					10	0	0	0	45	93	0	0
					93	0	0	0	41	143	0	0
IPE 100	328	332	Vento X	PolG	0	0	0	0	42	57	0	0
					57	0	0	0	42	127	0	0
					127	0	0	0	50		0	0
IPE 100	328	332	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1031												
IPE 100	313	314	Peso Proprio	UnifG	0	0	0	0	8	161	0	0
IPE 100	313	314	QP Solai	PolG	0	0	0	0	44	16	0	0
					16	0	0	0	51	93	0	0
					93	0	0	0	44	149	0	0
IPE 100	313	314	QV Solai	PolG	0	0	0	0	14	16	0	0
					16	0	0	0	16	93	0	0
					93	0	0	0	14	149	0	0
IPE 100	313	314	Neve	PolG	0	0	0	0	27	16	0	0
					16	0	0	0	32	93	0	0
					93	0	0	0	27	149	0	0
IPE 100	313	314	Vento X	PolG	0	0	0	0	42	16	0	0
					16	0	0	0	49	93	0	0
					93	0	0	0	42	149	0	0
IPE 100	313	314	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1032												
IPE 100	103	104	Peso Proprio	UnifG	0	0	0	0	8	89	0	0
IPE 100	103	104	QP Solai	PolG	0	0	0	0	71	3	0	0
IPE 100	103	104	QV Solai	PolG	3	0	0	0	71	89	0	0
					3	0	0	0	23	3	0	0
IPE 100	103	104	Neve	PolG	0	0	0	0	23	89	0	0
					0	0	0	0	44	3	0	0
IPE 100	103	104	Vento X	PolG	3	0	0	0	44	89	0	0
					0	0	0	0	68	3	0	0
IPE 100	103	104	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1033												
IPE 100	136	146	Peso Proprio	UnifG	0	0	0	0	8	95	0	0
IPE 100	136	146	QP Solai	PolG	0	0	0	0	119	9	0	0
					9	0	0	0	121	92	0	0
IPE 100	136	146	QV Solai	PolG	92	0	0	0	123	95	0	0
					0	0	0	0	38	9	0	0
					9	0	0	0	39	92	0	0
IPE 100	136	146	Neve	PolG	92	0	0	0	39	95	0	0
					0	0	0	0	43	9	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	136	146	Neve	PolG	0	0	0	43	95	0	0	32
IPE 100	136	146	Vento X	PolG	92	0	0	31	92	0	0	44
IPE 100	136	146	Vento X	PolG	0	0	0	44	95	0	0	44
IPE 100	136	146	Vento X	PolG	9	0	0	67	95	0	0	67
IPE 100	136	146	Vento X	PolG	0	0	0	67	95	0	0	49
IPE 100	136	146	Vento X	PolG	92	0	0	48	92	0	0	68
IPE 100	136	146	Carichi termici	Termico	AXY=15°C,AXZ=15°C	92	0	0	68	95	0	68
Trave 1034												
IPE 100	148	133	Peso Proprio	UnifG	0	0	0	8	107	0	0	8
IPE 100	148	133	QP Solai	PolG	30	0	0	110	30	0	0	116
IPE 100								116	83	0	0	118
IPE 100	148	133	QV Solai	PolG	83	0	0	118	107	0	0	113
IPE 100								35	30	0	0	37
IPE 100								30	0	0	0	38
IPE 100	148	133	Neve	PolG	83	0	0	38	107	0	0	36
IPE 100								0	0	0	0	41
IPE 100	148	133	Neve	PolG	83	0	0	41	107	0	0	41
IPE 100								0	0	0	0	38
IPE 100	148	133	Vento X	PolG	30	0	0	38	107	0	0	29
IPE 100								0	0	0	0	64
IPE 100	148	133	Vento X	PolG	83	0	0	46	83	0	0	64
IPE 100								0	0	0	0	59
IPE 100	148	133	Vento X	PolG	0	0	0	59	30	0	0	59
IPE 100								30	0	0	0	45
IPE 100	148	133	Carichi termici	Termico	AXY=15°C,AXZ=15°C	30	0	0	59	107	0	45
Trave 1035												
IPE 100	149	134	Peso Proprio	UnifG	0	0	0	8	113	0	0	8
IPE 100	149	134	QP Solai	PolG	0	0	0	105	36	0	0	111
IPE 100								36	0	0	0	112
IPE 100								83	0	0	0	108
IPE 100	149	134	QV Solai	PolG	0	0	0	34	36	0	0	36
IPE 100								36	0	0	0	36
IPE 100								83	0	0	0	34
IPE 100	149	134	Neve	PolG	0	0	0	36	113	0	0	36
IPE 100								36	0	0	0	36
IPE 100	149	134	Neve	PolG	36	0	0	36	113	0	0	28
IPE 100								0	0	0	0	38
IPE 100	149	134	Vento X	PolG	83	0	0	38	113	0	0	38
IPE 100								0	0	0	0	59
IPE 100	149	134	Vento X	PolG	83	0	0	59	113	0	0	59
IPE 100								0	0	0	0	55
IPE 100	149	134	Vento X	PolG	36	0	0	55	113	0	0	44
IPE 100	149	134	Carichi termici	Termico	AXY=15°C,AXZ=15°C	36	0	0	55	113	0	44
Trave 1036												
IPE 100	150	135	Peso Proprio	UnifG	0	0	0	8	119	0	0	8
IPE 100	150	135	QP Solai	PolG	0	0	0	99	42	0	0	104
IPE 100								42	0	0	0	106
IPE 100								83	0	0	0	101
IPE 100	150	135	QV Solai	PolG	0	0	0	106	119	0	0	101
IPE 100								0	0	0	0	33
IPE 100								42	0	0	0	34
IPE 100								83	0	0	0	33
IPE 100	150	135	Neve	PolG	0	0	0	34	119	0	0	33
IPE 100								0	0	0	0	33
IPE 100	150	135	Neve	PolG	42	0	0	33	119	0	0	27
IPE 100								0	0	0	0	36
IPE 100	150	135	Vento X	PolG	83	0	0	29	83	0	0	36
IPE 100								0	0	0	0	50
IPE 100	150	135	Vento X	PolG	42	0	0	50	119	0	0	42
IPE 100								0	0	0	0	55
IPE 100	150	135	Vento X	PolG	0	0	0	44	83	0	0	55
IPE 100								83	0	0	0	55
IPE 100	150	135	Carichi termici	Termico	AXY=15°C,AXZ=15°C	83	0	0	55	119	0	55
Trave 1037												
IPE 100	231	225	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	231	225	QP Solai	PolG	48	0	0	92	48	0	0	98
IPE 100								83	0	0	0	94
IPE 100	231	225	QV Solai	PolG	0	0	0	98	125	0	0	31
IPE 100								48	0	0	0	31

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf		
IPE 100	231	225	Neve	PolG	83	0	0	31	125	0	0	30		
IPE 100	231	225	Neve	PolG	48	0	0	30	125	0	26			
IPE 100	231	225	Vento X	PolG	83	0	0	33	125	0	33			
IPE 100	231	225	Vento X	PolG	48	0	0	46	125	0	46			
IPE 100	231	225	Vento X	PolG	0	0	0	42	83	0	50			
IPE 100	231	225	Carichi termici	Termico	AXY=15°C,AXZ=15°C	83	0	0	50	125	0	50		
Trave 1038														
IPE 100	232	226	Peso Proprio	UnifG	0	0	0	8	131	0	0	8		
					QP Solai	PolG	0	0	0	86	54	0	0	90
							54	0	0	90	83	0	0	91
IPE 100	232	226	QV Solai	PolG	83	0	0	91	131	0	0	88		
IPE 100	232	226	Neve	PolG	54	0	0	28	54	0	0	29		
IPE 100	232	226	Neve	PolG	83	0	0	29	131	0	0	28		
IPE 100	232	226	Neve	PolG	54	0	0	27	131	0	0	25		
IPE 100	232	226	Vento X	PolG	83	0	0	30	131	0	0	30		
IPE 100	232	226	Vento X	PolG	0	0	0	42	54	0	0	42		
IPE 100	232	226	Vento X	PolG	54	0	0	42	131	0	0	39		
IPE 100	232	226	Vento X	PolG	0	0	0	41	83	0	0	46		
IPE 100	232	226	Carichi termici	Termico	AXY=15°C,AXZ=15°C	83	0	0	46	131	0	46		
Trave 1039														
IPE 100	331	325	Peso Proprio	UnifG	0	0	0	8	137	0	0	8		
					QP Solai	PolG	0	0	0	83	60	0	0	85
							60	0	0	85	83	0	0	86
IPE 100	331	325	QV Solai	PolG	83	0	0	86	137	0	0	85		
IPE 100	331	325	Neve	PolG	83	0	0	27	137	0	0	27		
IPE 100	331	325	Neve	PolG	83	0	0	25	83	0	0	27		
IPE 100	331	325	Vento X	PolG	0	0	0	26	137	0	0	25		
IPE 100	331	325	Vento X	PolG	0	0	0	41	60	0	0	41		
IPE 100	331	325	Vento X	PolG	60	0	0	41	137	0	0	39		
IPE 100	331	325	Vento X	PolG	0	0	0	39	83	0	0	42		
IPE 100	331	325	Carichi termici	Termico	AXY=15°C,AXZ=15°C	83	0	0	42	137	0	42		
Trave 1040														
IPE 100	332	326	Peso Proprio	UnifG	0	0	0	8	143	0	0	8		
					QP Solai	PolG	0	0	0	85	83	0	0	86
							83	0	0	86	143	0	0	86
IPE 100	332	326	QV Solai	PolG	0	0	0	27	143	0	0	28		
IPE 100	332	326	Neve	PolG	0	0	0	25	143	0	0	26		
IPE 100	332	326	Neve	PolG	0	0	0	27	143	0	0	27		
IPE 100	332	326	Vento X	PolG	0	0	0	42	143	0	0	42		
IPE 100	332	326	Vento X	PolG	0	0	0	39	83	0	0	41		
IPE 100	332	326	Carichi termici	Termico	AXY=15°C,AXZ=15°C	83	0	0	41	143	0	41		
Trave 1041														
IPE 100	314	315	Peso Proprio	UnifG	0	0	0	8	149	0	0	8		
					QP Solai	PolG	0	0	0	44	149	0	0	44
							0	0	0	14	149	0	0	14
IPE 100	314	315	QV Solai	PolG	0	0	0	27	149	0	0	27		
IPE 100	314	315	Neve	PolG	0	0	0	27	149	0	0	27		
IPE 100	314	315	Vento X	PolG	0	0	0	42	149	0	0	42		
IPE 100	314	315	Carichi termici	Termico	AXY=15°C,AXZ=15°C	83	0	0	41	143	0	41		
Trave 1042														
IPE 100	104	105	Peso Proprio	UnifG	0	0	0	8	89	0	0	8		
					QP Solai	PolG	0	0	0	71	12	0	0	71
							12	0	0	71	89	0	0	44
IPE 100	104	105	QV Solai	PolG	0	0	0	23	12	0	0	23		
IPE 100	104	105	Carichi termici	Termico	AXY=15°C,AXZ=15°C	12	0	0	23	89	0	14		

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	104	105	Neve	PolG	0	0	0	44	12	0	0	44
IPE 100	104	105	Vento X	PolG	0	0	0	44	89	0	0	27
IPE 100	104	105			12	0	0	68	89	0	0	42
Trave 1043												
IPE 100	147	132	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	147	132	QP Solai	PolG	0	0	0	113	24	0	0	120
IPE 100					24	0	0	120	83	0	0	121
IPE 100	147	132	QV Solai	PolG	83	0	0	121	101	0	0	116
IPE 100					24	0	0	36	24	0	0	38
IPE 100					24	0	0	38	83	0	0	39
IPE 100	147	132	Neve	PolG	83	0	0	39	101	0	0	37
IPE 100					83	0	0	29	83	0	0	43
IPE 100	147	132	Neve	PolG	83	0	0	43	101	0	0	43
IPE 100	147	132	Vento X	PolG	24	0	0	41	24	0	0	41
IPE 100	147	132	Vento X	PolG	0	0	0	45	83	0	0	67
IPE 100	147	132	Vento X	PolG	83	0	0	67	101	0	0	67
IPE 100	147	132			0	0	0	64	24	0	0	64
IPE 100	147	132			24	0	0	64	101	0	0	45
Trave 1044												
IPE 100	146	131	Peso Proprio	UnifG	0	0	0	8	95	0	0	8
IPE 100	146	131	QP Solai	PolG	0	0	0	115	18	0	0	120
IPE 100					18	0	0	120	83	0	0	121
IPE 100	146	131	QV Solai	PolG	83	0	0	121	95	0	0	117
IPE 100					18	0	0	37	18	0	0	39
IPE 100					18	0	0	39	83	0	0	39
IPE 100	146	131	Neve	PolG	83	0	0	39	95	0	0	37
IPE 100					83	0	0	28	83	0	0	44
IPE 100	146	131	Neve	PolG	83	0	0	44	95	0	0	44
IPE 100	146	131	Vento X	PolG	0	0	0	43	18	0	0	43
IPE 100	146	131	Vento X	PolG	18	0	0	43	95	0	0	29
IPE 100	146	131			0	0	0	67	18	0	0	67
IPE 100	146	131	Vento X	PolG	18	0	0	67	95	0	0	44
IPE 100	146	131			0	0	0	44	83	0	0	68
IPE 100	146	131			83	0	0	68	95	0	0	68
Trave 1045												
IPE 100	134	144	Peso Proprio	UnifG	0	0	0	8	113	0	0	8
IPE 100	134	144	QP Solai	PolG	0	0	0	100	45	0	0	112
IPE 100					45	0	0	112	74	0	0	112
IPE 100	134	144	QV Solai	PolG	74	0	0	112	113	0	0	103
IPE 100					45	0	0	32	45	0	0	36
IPE 100					45	0	0	36	74	0	0	36
IPE 100	134	144	Neve	PolG	74	0	0	36	113	0	0	33
IPE 100					74	0	0	36	45	0	0	36
IPE 100	134	144	Neve	PolG	45	0	0	36	113	0	0	25
IPE 100	134	144			0	0	0	26	74	0	0	38
IPE 100	134	144	Vento X	PolG	74	0	0	38	113	0	0	38
IPE 100	134	144			0	0	0	55	45	0	0	55
IPE 100	134	144	Vento X	PolG	45	0	0	55	113	0	0	39
IPE 100	134	144			45	0	0	41	74	0	0	59
IPE 100	134	144			74	0	0	59	113	0	0	59
Trave 1046												
IPE 100	135	145	Peso Proprio	UnifG	0	0	0	8	119	0	0	8
IPE 100	135	145	QP Solai	PolG	0	0	0	94	51	0	0	105
IPE 100					51	0	0	105	74	0	0	106
IPE 100	135	145	QV Solai	PolG	74	0	0	106	119	0	0	97
IPE 100					0	0	0	30	51	0	0	34
IPE 100	135	145	Neve	PolG	51	0	0	34	74	0	0	34
IPE 100	135	145			74	0	0	34	119	0	0	31
IPE 100	135	145			0	0	0	33	51	0	0	33
IPE 100					51	0	0	33	119	0	0	24

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	135	145	Neve	PolG	0	0	0	26	74	0	0	36
IPE 100	135	145	Vento X	PolG	74	0	0	36	119	0	0	36
IPE 100					51	0	0	50	51	0	0	50
IPE 100	135	145	Vento X	PolG	0	0	0	50	119	0	0	38
IPE 100	135	145			74	0	0	40	74	0	0	55
Trave 1047												
IPE 100	225	229	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	225	229	QP Solai	PolG	0	0	0	87	57	0	0	97
IPE 100					57	0	0	97	74	0	0	98
IPE 100	225	229	QV Solai	PolG	74	0	0	98	125	0	0	90
IPE 100					74	0	0	28	57	0	0	31
IPE 100					57	0	0	31	74	0	0	31
IPE 100	225	229	Neve	PolG	74	0	0	31	125	0	0	29
IPE 100	225	229	Neve	PolG	0	0	0	30	57	0	0	30
IPE 100	225	229	Neve	PolG	57	0	0	30	125	0	0	23
IPE 100	225	229	Vento X	PolG	0	0	0	25	74	0	0	33
IPE 100	225	229	Vento X	PolG	74	0	0	33	125	0	0	33
IPE 100					74	0	0	46	57	0	0	46
IPE 100	225	229	Vento X	PolG	57	0	0	46	125	0	0	36
IPE 100	225	229	Vento X	PolG	0	0	0	38	74	0	0	50
IPE 100	225	229			74	0	0	50	125	0	0	50
Trave 1048												
IPE 100	226	230	Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	226	230	QP Solai	PolG	0	0	0	82	63	0	0	90
IPE 100					63	0	0	90	74	0	0	91
IPE 100	226	230	QV Solai	PolG	74	0	0	91	131	0	0	84
IPE 100					74	0	0	26	63	0	0	29
IPE 100					63	0	0	29	74	0	0	29
IPE 100	226	230	Neve	PolG	74	0	0	29	131	0	0	27
IPE 100	226	230	Neve	PolG	0	0	0	23	74	0	0	30
IPE 100	226	230	Neve	PolG	74	0	0	30	131	0	0	30
IPE 100					63	0	0	27	63	0	0	27
IPE 100	226	230	Vento X	PolG	0	0	0	27	131	0	0	22
IPE 100	226	230			63	0	0	42	63	0	0	42
IPE 100	226	230	Vento X	PolG	63	0	0	42	131	0	0	35
IPE 100	226	230	Vento X	PolG	0	0	0	36	74	0	0	46
IPE 100	226	230			74	0	0	46	131	0	0	46
Trave 1049												
IPE 100	325	329	Peso Proprio	UnifG	0	0	0	8	137	0	0	8
IPE 100	325	329	QP Solai	PolG	0	0	0	79	69	0	0	86
IPE 100					69	0	0	86	74	0	0	86
IPE 100	325	329	QV Solai	PolG	74	0	0	86	137	0	0	80
IPE 100					74	0	0	25	69	0	0	27
IPE 100					69	0	0	27	74	0	0	28
IPE 100	325	329	Neve	PolG	74	0	0	28	137	0	0	26
IPE 100	325	329	Neve	PolG	0	0	0	23	74	0	0	27
IPE 100	325	329	Neve	PolG	74	0	0	27	137	0	0	27
IPE 100	325	329	Vento X	PolG	69	0	0	26	69	0	0	22
IPE 100	325	329	Vento X	PolG	0	0	0	41	69	0	0	40
IPE 100	325	329	Vento X	PolG	69	0	0	40	137	0	0	35
IPE 100	325	329	Vento X	PolG	0	0	0	35	74	0	0	42
IPE 100	325	329			74	0	0	42	137	0	0	42
Trave 1050												
IPE 100	326	330	Peso Proprio	UnifG	0	0	0	8	143	0	0	8
IPE 100	326	330	QP Solai	PolG	0	0	0	80	74	0	0	86
IPE 100					74	0	0	86	75	0	0	86
IPE 100	326	330	QV Solai	PolG	75	0	0	86	143	0	0	81
IPE 100					75	0	0	26	74	0	0	28
IPE 100	326	330	Neve	PolG	74	0	0	28	75	0	0	28
IPE 100					75	0	0	28	143	0	0	26

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	326	330	Neve	PolG	0	0	0	27	75	0	0	27
IPE 100	326	330	Neve	PolG	75	0	0	27	143	0	0	24
IPE 100	326	330	Vento X	PolG	0	0	0	23	74	0	0	26
IPE 100	326	330	Vento X	PolG	74	0	0	35	74	0	0	41
IPE 100	326	330	Vento X	PolG	74	0	0	41	143	0	0	41
IPE 100	326	330	Vento X	PolG	0	0	0	42	75	0	0	42
IPE 100	326	330	Carichi termici	Termico	75	0	0	42	143	0	0	38
Trave 1051												
IPE 100	315	316	Peso Proprio	UnitG	0	0	0	8	138	0	0	8
IPE 100	315	316	QP Solai	PolG	0	0	0	39	74	0	0	44
IPE 100	315	316	QV Solai	PolG	74	0	0	13	74	0	0	14
IPE 100	315	316	Neve	PolG	74	0	0	14	149	0	0	14
IPE 100	315	316	Vento X	PolG	0	0	0	24	74	0	0	27
IPE 100	315	316	Vento X	PolG	74	0	0	27	149	0	0	27
IPE 100	315	316	Vento X	PolG	0	0	0	38	74	0	0	42
IPE 100	315	316	Carichi termici	Termico	74	0	0	42	149	0	0	42
Trave 1052												
IPE 100	132	142	Peso Proprio	UnitG	0	0	0	8	101	0	0	8
IPE 100	132	142	QP Solai	PolG	0	0	0	109	33	0	0	121
IPE 100	132	142	QV Solai	PolG	33	0	0	121	75	0	0	112
IPE 100	132	142	Neve	PolG	75	0	0	121	101	0	0	39
IPE 100	132	142	Vento X	PolG	0	0	0	35	33	0	0	39
IPE 100	132	142	Vento X	PolG	33	0	0	39	75	0	0	36
IPE 100	132	142	Vento X	PolG	75	0	0	27	75	0	0	43
IPE 100	132	142	Vento X	PolG	75	0	0	43	101	0	0	41
IPE 100	132	142	Vento X	PolG	0	0	0	41	33	0	0	41
IPE 100	132	142	Vento X	PolG	33	0	0	41	101	0	0	26
IPE 100	132	142	Vento X	PolG	0	0	0	64	33	0	0	64
IPE 100	132	142	Vento X	PolG	33	0	0	64	101	0	0	41
IPE 100	132	142	Carichi termici	Termico	75	0	0	67	101	0	0	67
Trave 1053												
IPE 100	105	106	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	105	106	QP Solai	PolG	0	0	0	71	21	0	0	71
IPE 100	105	106	QV Solai	PolG	21	0	0	71	89	0	0	40
IPE 100	105	106	Neve	PolG	0	0	0	23	21	0	0	23
IPE 100	105	106	Vento X	PolG	21	0	0	23	89	0	0	13
IPE 100	105	106	Vento X	PolG	0	0	0	44	21	0	0	44
IPE 100	105	106	Vento X	PolG	21	0	0	44	89	0	0	25
IPE 100	105	106	Vento X	PolG	0	0	0	68	21	0	0	68
IPE 100	105	106	Carichi termici	Termico	21	0	0	68	89	0	0	39
Trave 1054												
IPE 100	133	143	Peso Proprio	UnitG	0	0	0	8	107	0	0	8
IPE 100	133	143	QP Solai	PolG	0	0	0	105	39	0	0	117
IPE 100	133	143	QV Solai	PolG	39	0	0	117	75	0	0	118
IPE 100	133	143	Neve	PolG	75	0	0	118	107	0	0	108
IPE 100	133	143	Vento X	PolG	0	0	0	34	39	0	0	37
IPE 100	133	143	Vento X	PolG	39	0	0	37	75	0	0	38
IPE 100	133	143	Vento X	PolG	75	0	0	38	107	0	0	35
IPE 100	133	143	Vento X	PolG	0	0	0	38	39	0	0	38
IPE 100	133	143	Vento X	PolG	39	0	0	38	107	0	0	26
IPE 100	133	143	Vento X	PolG	75	0	0	41	107	0	0	41
IPE 100	133	143	Vento X	PolG	0	0	0	59	39	0	0	59
IPE 100	133	143	Vento X	PolG	39	0	0	59	107	0	0	40
IPE 100	133	143	Vento X	PolG	75	0	0	41	75	0	0	64
IPE 100	133	143	Carichi termici	Termico	75	0	0	64	107	0	0	64
Trave 1055												

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	131	141	Peso Proprio	UnitG	0	0	0	8	95	0	0	8
IPE 100	131	141	QP Solai	PolG	0	0	0	110	27	0	0	121
IPE 100	131	141	QV Solai	PolG	27	0	0	121	75	0	0	113
IPE 100	131	141	Neve	PolG	75	0	0	35	27	0	0	39
IPE 100	131	141	Neve	PolG	27	0	0	39	75	0	0	36
IPE 100	131	141	Neve	PolG	75	0	0	26	75	0	0	44
IPE 100	131	141	Neve	PolG	75	0	0	44	95	0	0	44
IPE 100	131	141	Vento X	PolG	0	0	0	43	27	0	0	43
IPE 100	131	141	Vento X	PolG	27	0	0	40	75	0	0	26
IPE 100	131	141	Vento X	PolG	0	0	0	68	95	0	0	68
IPE 100	131	141	Vento X	PolG	75	0	0	67	27	0	0	67
IPE 100	131	141	Carichi termici	Termico	27	0	0	67	95	0	0	40
Trave 1056												
IPE 100	145	165	Peso Proprio	UnitG	0	0	0	8	119	0	0	8
IPE 100	145	165	QP Solai	PolG	0	0	0	89	59	0	0	108
IPE 100	145	165	QV Solai	PolG	59	0	0	108	66	0	0	92
IPE 100	145	165	Neve	PolG	66	0	0	108	119	0	0	35
IPE 100	145	165	Neve	PolG	59	0	0	35	66	0	0	35
IPE 100	145	165	Neve	PolG	66	0	0	35	119	0	0	30
IPE 100	145	165	Neve	PolG	0	0	0	23	66	0	0	36
IPE 100	145	165	Neve	PolG	66	0	0	36	119	0	0	36
IPE 100	145	165	Neve	PolG	0	0	0	33	59	0	0	33
IPE 100	145	165	Vento X	PolG	59	0	0	33	119	0	0	21
IPE 100	145	165	Vento X	PolG	0	0	0	35	66	0	0	55
IPE 100	145	165	Vento X	PolG	66	0	0	55	119	0	0	55
IPE 100	145	165	Vento X	PolG	0	0	0	50	59	0	0	50
IPE 100	145	165	Carichi termici	Termico	59	0	0	50	119	0	0	33
Trave 1057												
IPE 100	229	237	Peso Proprio	UnitG	0	0	0	8	126	0	0	8
IPE 100	229	237	QP Solai	PolG	0	0	0	83	66	0	0	100
IPE 100	229	237	QV Solai	PolG	66	0	0	100	126	0	0	86
IPE 100	229	237	Neve	PolG	0	0	0	27	66	0	0	32
IPE 100	229	237	Neve	PolG	66	0	0	32	126	0	0	27
IPE 100	229	237	Neve	PolG	0	0	0	22	66	0	0	33
IPE 100	229	237	Neve	PolG	66	0	0	33	126	0	0	33
IPE 100	229	237	Neve	PolG	0	0	0	30	66	0	0	30
IPE 100	229	237	Vento X	PolG	66	0	0	30	126	0	0	21
IPE 100	229	237	Vento X	PolG	0	0	0	46	66	0	0	46
IPE 100	229	237	Vento X	PolG	66	0	0	46	126	0	0	32
IPE 100	229	237	Vento X	PolG	0	0	0	34	66	0	0	50
IPE 100	229	237	Carichi termici	Termico	66	0	0	50	126	0	0	50
Trave 1058												
IPE 100	230	238	Peso Proprio	UnitG	0	0	0	8	132	0	0	8
IPE 100	230	238	QP Solai	PolG	0	0	0	78	66	0	0	92
IPE 100	230	238	QV Solai	PolG	66	0	0	92	72	0	0	92
IPE 100	230	238	Neve	PolG	72	0	0	92	132	0	0	80
IPE 100	230	238	Neve	PolG	0	0	0	25	66	0	0	29
IPE 100	230	238	Neve	PolG	66	0	0	29	72	0	0	26
IPE 100	230	238	Neve	PolG	72	0	0	29	132	0	0	27
IPE 100	230	238	Neve	PolG	0	0	0	27	72	0	0	20
IPE 100	230	238	Neve	PolG	72	0	0	21	66	0	0	30
IPE 100	230	238	Vento X	PolG	66	0	0	30	132	0	0	30
IPE 100	230	238	Vento X	PolG	0	0	0	42	72	0	0	42
IPE 100	230	238	Vento X	PolG	72	0	0	42	132	0	0	31
IPE 100	230	238	Vento X	PolG	0	0	0	32	66	0	0	46
IPE 100	230	238	Carichi termici	Termico	66	0	0	46	132	0	0	46
Trave 1059												

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	QZf
IPE 100	329	337	Peso Proprio	UnifG	0	0	0	8	138	0	0	8
IPE 100	329	337	QP Solai	PolG	0	0	0	75	66	0	0	86
					66	0	0	86	78	0	0	86
					78	0	0	86	138	0	0	76
IPE 100	329	337	QV Solai	PolG	0	0	0	24	66	0	0	28
					66	0	0	28	78	0	0	28
					78	0	0	28	138	0	0	24
IPE 100	329	337	Neve	PolG	0	0	0	20	66	0	0	27
					66	0	0	27	138	0	0	27
IPE 100	329	337	Neve	PolG	0	0	0	26	78	0	0	26
					78	0	0	26	138	0	0	20
IPE 100	329	337	Vento X	PolG	0	0	0	41	78	0	0	41
					78	0	0	41	138	0	0	31
IPE 100	329	337	Vento X	PolG	0	0	0	31	66	0	0	42
					66	0	0	42	138	0	0	42
IPE 100	329	337	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Trave 1060												
IPE 100	330	338	Peso Proprio	UnifG	0	0	0	8	144	0	0	8
IPE 100	330	338	QP Solai	PolG	0	0	0	76	66	0	0	86
					66	0	0	86	84	0	0	86
					84	0	0	86	144	0	0	77
IPE 100	330	338	QV Solai	PolG	0	0	0	24	66	0	0	28
					66	0	0	28	84	0	0	28
					84	0	0	28	144	0	0	25
IPE 100	330	338	Neve	PolG	0	0	0	27	84	0	0	27
					84	0	0	27	144	0	0	22
IPE 100	330	338	Neve	PolG	0	0	0	20	66	0	0	26
					66	0	0	26	144	0	0	26
IPE 100	330	338	Vento X	PolG	0	0	0	31	66	0	0	41
					66	0	0	41	144	0	0	41
IPE 100	330	338	Vento X	PolG	0	0	0	42	84	0	0	42
					84	0	0	42	144	0	0	33
IPE 100	330	338	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Trave 1061												
IPE 100	316	317	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	316	317	QP Solai	PolG	0	0	0	35	66	0	0	44
					66	0	0	44	150	0	0	44
IPE 100	316	317	QV Solai	PolG	0	0	0	11	66	0	0	14
					66	0	0	14	150	0	0	14
IPE 100	316	317	Neve	PolG	0	0	0	22	66	0	0	27
					66	0	0	27	150	0	0	27
IPE 100	316	317	Vento X	PolG	0	0	0	34	66	0	0	42
					66	0	0	42	150	0	0	42
IPE 100	316	317	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Trave 1062												
IPE 100	141	161	Peso Proprio	UnifG	0	0	0	8	95	0	0	8
IPE 100	141	161	QP Solai	PolG	0	0	0	105	35	0	0	124
					35	0	0	124	66	0	0	123
IPE 100	141	161	QV Solai	PolG	0	0	0	123	95	0	0	107
					66	0	0	34	35	0	0	40
					35	0	0	40	66	0	0	39
IPE 100	141	161	Neve	PolG	0	0	0	39	95	0	0	34
					35	0	0	43	35	0	0	43
IPE 100	141	161	Neve	PolG	0	0	0	43	95	0	0	23
					66	0	0	22	66	0	0	44
IPE 100	141	161	Vento X	PolG	0	0	0	67	35	0	0	67
					35	0	0	67	95	0	0	35
IPE 100	141	161	Vento X	PolG	0	0	0	35	66	0	0	68
					66	0	0	68	95	0	0	68
IPE 100	141	161	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Trave 1063												
IPE 100	143	163	Peso Proprio	UnifG	0	0	0	8	107	0	0	8
IPE 100	143	163	QP Solai	PolG	0	0	0	100	47	0	0	120
					47	0	0	120	66	0	0	120
					66	0	0	120	107	0	0	103

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	QZf
IPE 100	143	163	QV Solai	PolG	0	0	0	32	47	0	0	38
					47	0	0	38	66	0	0	39
IPE 100	143	163	Neve	PolG	0	0	0	24	66	0	0	41
					66	0	0	41	107	0	0	41
IPE 100	143	163	Neve	PolG	0	0	0	38	47	0	0	38
					47	0	0	38	107	0	0	23
IPE 100	143	163	Vento X	PolG	0	0	0	36	66	0	0	64
					66	0	0	64	107	0	0	64
IPE 100	143	163	Vento X	PolG	0	0	0	59	47	0	0	59
					47	0	0	59	107	0	0	35
IPE 100	143	163	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Trave 1064												
IPE 100	106	107	Peso Proprio	UnifG	0	0	0	8	89	0	0	8
IPE 100	106	107	QP Solai	PolG	29	0	0	71	29	0	0	71
					29	0	0	71	89	0	0	35
IPE 100	106	107	QV Solai	PolG	0	0	0	23	29	0	0	23
					29	0	0	23	89	0	0	11
IPE 100	106	107	Neve	PolG	0	0	0	44	29	0	0	44
					29	0	0	44	89	0	0	22
IPE 100	106	107	Vento X	PolG	0	0	0	68	29	0	0	68
					29	0	0	68	89	0	0	33
IPE 100	106	107	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Trave 1065												
IPE 100	144	164	Peso Proprio	UnifG	0	0	0	8	113	0	0	8
IPE 100	144	164	QP Solai	PolG	0	0	0	95	53	0	0	115
					53	0	0	115	66	0	0	115
					66	0	0	115	113	0	0	98
IPE 100	144	164	QV Solai	PolG	0	0	0	30	53	0	0	37
					53	0	0	37	66	0	0	37
					66	0	0	37	113	0	0	31
IPE 100	144	164	Neve	PolG	0	0	0	36	53	0	0	36
					53	0	0	36	113	0	0	22
IPE 100	144	164	Neve	PolG	0	0	0	23	66	0	0	38
					66	0	0	38	113	0	0	38
IPE 100	144	164	Vento X	PolG	0	0	0	55	53	0	0	55
					53	0	0	55	113	0	0	35
IPE 100	144	164	Vento X	PolG	0	0	0	36	66	0	0	59
					66	0	0	59	113	0	0	59
IPE 100	144	164	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Trave 1066												
IPE 100	142	162	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	142	162	QP Solai	PolG	0	0	0	104	41	0	0	124
					41	0	0	124	66	0	0	123
					66	0	0	123	101	0	0	106
IPE 100	142	162	QV Solai	PolG	0	0	0	33	41	0	0	40
					41	0	0	40	66	0	0	40
					66	0	0	40	101	0	0	34
IPE 100	142	162	Neve	PolG	0	0	0	23	66	0	0	43
					66	0	0	43	101	0	0	43
IPE 100	142	162	Neve	PolG	0	0	0	41	41	0	0	41
					41	0	0	41	101	0	0	23
IPE 100	142	162	Vento X	PolG	0	0	0	36	66	0	0	67
					66	0	0	67	101	0	0	67
IPE 100	142	162	Vento X	PolG	0	0	0	64	41	0	0	64
					41	0	0	64	101	0	0	36
IPE 100	142	162	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Trave 1067												
IPE 100	237	239	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	237	239	QP Solai	PolG	0	0	0	78	58	0	0	100
					58	0	0	100	73	0	0	100
					73	0	0	100	125	0	0	81
IPE 100	237	239	QV Solai	PolG	0	0	0	25	58	0	0	32
					58	0	0	32	73	0	0	32
					73	0	0	32	125	0	0	26
IPE 100	237	239	Neve	PolG	0	0	0	30	73	0	0	30

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	237	239	Neve	PolG	73	0	0	30	125	0	0	18
IPE 100	237	239	Vento X	PolG	58	0	0	19	58	0	0	33
IPE 100	237	239	Vento X	PolG	58	0	0	29	58	0	0	50
IPE 100	237	239	Vento X	PolG	58	0	0	50	125	0	0	50
IPE 100	237	239	Vento X	PolG	73	0	0	46	73	0	0	46
IPE 100	237	239	Carichi termici	Termico	AXY=15°C,AXZ=15°C			46	125	0	0	27
Trave 1068												
IPE 100	238	240	Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	238	240	QP Solai	PolG	58	0	0	73	58	0	0	92
IPE 100	238	240			58	0	0	92	79	0	0	92
IPE 100	238	240	QV Solai	PolG	79	0	0	92	131	0	0	75
IPE 100	238	240			58	0	0	23	58	0	0	29
IPE 100	238	240	QV Solai	PolG	58	0	0	29	79	0	0	29
IPE 100	238	240			79	0	0	29	131	0	0	24
IPE 100	238	240	Neve	PolG	0	0	0	27	79	0	0	27
IPE 100	238	240	Neve	PolG	79	0	0	27	131	0	0	17
IPE 100	238	240			58	0	0	18	58	0	0	30
IPE 100	238	240	Vento X	PolG	58	0	0	30	131	0	0	30
IPE 100	238	240			79	0	0	42	79	0	0	42
IPE 100	238	240	Vento X	PolG	0	0	0	42	131	0	0	26
IPE 100	238	240			58	0	0	28	58	0	0	46
IPE 100	238	240	Carichi termici	Termico	AXY=15°C,AXZ=15°C			46	131	0	0	46
Trave 1069												
IPE 100	337	339	Peso Proprio	UnifG	0	0	0	8	137	0	0	8
IPE 100	337	339	QP Solai	PolG	58	0	0	70	58	0	0	86
IPE 100	337	339			58	0	0	86	85	0	0	86
IPE 100	337	339	QV Solai	PolG	85	0	0	86	137	0	0	72
IPE 100	337	339			58	0	0	22	58	0	0	28
IPE 100	337	339			58	0	0	28	85	0	0	28
IPE 100	337	339	Neve	PolG	85	0	0	28	137	0	0	23
IPE 100	337	339	Neve	PolG	0	0	0	17	58	0	0	27
IPE 100	337	339			58	0	0	26	85	0	0	26
IPE 100	337	339	Vento X	PolG	85	0	0	26	137	0	0	17
IPE 100	337	339			0	0	0	41	85	0	0	41
IPE 100	337	339	Vento X	PolG	85	0	0	41	137	0	0	26
IPE 100	337	339			58	0	0	27	58	0	0	42
IPE 100	337	339	Carichi termici	Termico	AXY=15°C,AXZ=15°C			42	137	0	0	42
Trave 1070												
IPE 100	338	340	Peso Proprio	UnifG	0	0	0	8	143	0	0	8
IPE 100	338	340	QP Solai	PolG	58	0	0	72	58	0	0	86
IPE 100	338	340			58	0	0	86	91	0	0	86
IPE 100	338	340	QV Solai	PolG	91	0	0	86	143	0	0	72
IPE 100	338	340			58	0	0	23	58	0	0	28
IPE 100	338	340	Neve	PolG	58	0	0	28	91	0	0	28
IPE 100	338	340	Neve	PolG	91	0	0	28	143	0	0	23
IPE 100	338	340			91	0	0	27	91	0	0	27
IPE 100	338	340	Neve	PolG	0	0	0	27	143	0	0	18
IPE 100	338	340	Neve	PolG	58	0	0	17	58	0	0	26
IPE 100	338	340	Vento X	PolG	58	0	0	26	143	0	0	26
IPE 100	338	340			58	0	0	27	58	0	0	41
IPE 100	338	340	Vento X	PolG	58	0	0	41	143	0	0	41
IPE 100	338	340			91	0	0	42	91	0	0	42
IPE 100	338	340	Carichi termici	Termico	AXY=15°C,AXZ=15°C			42	143	0	0	29
Trave 1071												
IPE 100	317	318	Peso Proprio	UnifG	0	0	0	8	161	0	0	8
IPE 100	317	318	QP Solai	PolG	58	0	0	30	58	0	0	44
IPE 100	317	318	QV Solai	PolG	58	0	0	44	149	0	0	44
IPE 100	317	318			58	0	0	10	58	0	0	14
IPE 100	317	318	Neve	PolG	0	0	0	19	58	0	0	27

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	317	318	Vento X	PolG	58	0	0	27	149	0	0	27
IPE 100	317	318			58	0	0	29	58	0	0	42
IPE 100	317	318	Carichi termici	Termico	AXY=15°C,AXZ=15°C			42	149	0	0	42
Trave 1072												
IPE 100	165	170	Peso Proprio	UnifG	0	0	0	8	119	0	0	8
IPE 100	165	170	QP Solai	PolG	58	0	0	84	58	0	0	110
IPE 100	165	170			58	0	0	110	67	0	0	87
IPE 100	165	170	QV Solai	PolG	67	0	0	110	119	0	0	35
IPE 100	165	170			58	0	0	27	58	0	0	35
IPE 100	165	170			67	0	0	35	67	0	0	28
IPE 100	165	170	Neve	PolG	0	0	0	33	67	0	0	33
IPE 100	165	170	Neve	PolG	67	0	0	33	119	0	0	18
IPE 100	165	170			58	0	0	20	58	0	0	36
IPE 100	165	170	Vento X	PolG	58	0	0	36	119	0	0	36
IPE 100	165	170			58	0	0	30	58	0	0	55
IPE 100	165	170	Vento X	PolG	58	0	0	55	119	0	0	55
IPE 100	165	170			67	0	0	50	67	0	0	50
IPE 100	165	170	Carichi termici	Termico	AXY=15°C,AXZ=15°C			50	119	0	0	28
Trave 1073												
IPE 100	162	167	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	162	167	QP Solai	PolG	49	0	0	98	49	0	0	130
IPE 100	162	167			58	0	0	130	58	0	0	101
IPE 100	162	167	QV Solai	PolG	58	0	0	32	49	0	0	42
IPE 100	162	167			49	0	0	42	58	0	0	42
IPE 100	162	167	Neve	PolG	58	0	0	41	49	0	0	41
IPE 100	162	167			49	0	0	41	101	0	0	20
IPE 100	162	167	Neve	PolG	0	0	0	20	58	0	0	43
IPE 100	162	167	Vento X	PolG	58	0	0	43	101	0	0	43
IPE 100	162	167			58	0	0	31	58	0	0	67
IPE 100	162	167	Vento X	PolG	58	0	0	67	101	0	0	67
IPE 100	162	167			49	0	0	64	49	0	0	64
IPE 100	162	167	Carichi termici	Termico	AXY=15°C,AXZ=15°C			64	101	0	0	30
Trave 1074												
IPE 100	164	169	Peso Proprio	UnifG	0	0	0	8	113	0	0	8
IPE 100	164	169	QP Solai	PolG	58	0	0	90	58	0	0	119
IPE 100	164	169			61	0	0	119	113	0	0	93
IPE 100	164	169	QV Solai	PolG	0	0	0	29	58	0	0	38
IPE 100	164	169			58	0	0	38	61	0	0	38
IPE 100	164	169	Neve	PolG	61	0	0	38	113	0	0	30
IPE 100	164	169			58	0	0	20	58	0	0	38
IPE 100	164	169	Neve	PolG	58	0	0	38	113	0	0	38
IPE 100	164	169			61	0	0	36	61	0	0	36
IPE 100	164	169	Vento X	PolG	61	0	0	36	113	0	0	19
IPE 100	164	169			61	0	0	55	61	0	0	55
IPE 100	164	169	Vento X	PolG	61	0	0	55	113	0	0	30
IPE 100	164	169			58	0	0	31	58	0	0	59
IPE 100	164	169	Carichi termici	Termico	AXY=15°C,AXZ=15°C			59	113	0	0	59
Trave 1075												
IPE 100	161	166	Peso Proprio	UnifG	0	0	0	8	95	0	0	8
IPE 100	161	166	QP Solai	PolG	44	0	0	100	44	0	0	130
IPE 100	161	166			58	0	0	130	58	0	0	102
IPE 100	161	166	QV Solai	PolG	0	0	0	32	44	0	0	42
IPE 100	161	166			44	0	0	42	58	0	0	42
IPE 100	161	166	Neve	PolG	58	0	0	42	95	0	0	33
IPE 100	161	166			58	0	0	19	58	0	0	44
IPE 100	161	166	Neve	PolG	58	0	0	44	95	0	0	44

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	161	166	Vento X	PolG	0	0	0	43	95	0	0	19
IPE 100	161	166	Vento X	PolG	58	0	0	68	95	0	0	68
IPE 100	161	166			44	0	0	67	95	0	0	67
IPE 100	161	166	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1076												
IPE 100	107	108	Peso Proprio	UnifG	0	0	0	8	89	0	0	8
IPE 100	107	108	QP Solai	PolG	0	0	0	71	38	0	0	71
IPE 100	107	108			38	0	0	71	89	0	0	30
IPE 100	107	108	QV Solai	PolG	0	0	0	23	38	0	0	23
IPE 100	107	108			38	0	0	23	89	0	0	10
IPE 100	107	108	Neve	PolG	0	0	0	44	38	0	0	44
IPE 100	107	108			38	0	0	44	89	0	0	19
IPE 100	107	108	Vento X	PolG	0	0	0	68	38	0	0	68
IPE 100	107	108			38	0	0	68	89	0	0	29
IPE 100	107	108	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1077												
IPE 100	163	168	Peso Proprio	UnifG	0	0	0	8	107	0	0	8
IPE 100	163	168	QP Solai	PolG	0	0	0	94	55	0	0	127
IPE 100	163	168			55	0	0	127	58	0	0	127
IPE 100	163	168	QV Solai	PolG	0	0	0	127	107	0	0	98
IPE 100	163	168			58	0	0	30	55	0	0	41
IPE 100	163	168	Neve	PolG	0	0	0	41	58	0	0	41
IPE 100	163	168			58	0	0	41	107	0	0	31
IPE 100	163	168	Neve	PolG	0	0	0	20	58	0	0	41
IPE 100	163	168			58	0	0	41	107	0	0	41
IPE 100	163	168	Neve	PolG	0	0	0	38	55	0	0	38
IPE 100	163	168			55	0	0	38	107	0	0	19
IPE 100	163	168	Vento X	PolG	0	0	0	59	55	0	0	59
IPE 100	163	168			55	0	0	59	107	0	0	30
IPE 100	163	168	Vento X	PolG	0	0	0	31	58	0	0	64
IPE 100	163	168			58	0	0	64	107	0	0	64
IPE 100	163	168	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1078												
IPE 100	240	222	Peso Proprio	UnifG	0	0	0	8	132	0	0	8
IPE 100	240	222	QP Solai	PolG	0	0	0	70	51	0	0	92
IPE 100	240	222			51	0	0	92	87	0	0	92
IPE 100	240	222	QV Solai	PolG	0	0	0	92	132	0	0	72
IPE 100	240	222			87	0	0	22	51	0	0	29
IPE 100	240	222	Neve	PolG	0	0	0	29	87	0	0	29
IPE 100	240	222			87	0	0	29	132	0	0	23
IPE 100	240	222	Neve	PolG	0	0	0	16	51	0	0	30
IPE 100	240	222			51	0	0	30	132	0	0	30
IPE 100	240	222	Neve	PolG	0	0	0	27	87	0	0	27
IPE 100	240	222			87	0	0	27	132	0	0	15
IPE 100	240	222	Vento X	PolG	0	0	0	25	51	0	0	46
IPE 100	240	222			51	0	0	46	132	0	0	46
IPE 100	240	222	Vento X	PolG	0	0	0	42	87	0	0	42
IPE 100	240	222			87	0	0	42	132	0	0	23
IPE 100	240	222	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1079												
IPE 100	339	321	Peso Proprio	UnifG	0	0	0	8	138	0	0	8
IPE 100	339	321	QP Solai	PolG	0	0	0	67	51	0	0	86
IPE 100	339	321			51	0	0	86	93	0	0	86
IPE 100	339	321	QV Solai	PolG	0	0	0	86	138	0	0	68
IPE 100	339	321			93	0	0	21	51	0	0	28
IPE 100	339	321	Neve	PolG	0	0	0	28	93	0	0	28
IPE 100	339	321			93	0	0	28	138	0	0	22
IPE 100	339	321	Neve	PolG	0	0	0	15	51	0	0	27
IPE 100	339	321			51	0	0	27	138	0	0	27
IPE 100	339	321	Neve	PolG	0	0	0	26	93	0	0	26
IPE 100	339	321			93	0	0	26	138	0	0	15
IPE 100	339	321	Vento X	PolG	0	0	0	24	51	0	0	42
IPE 100	339	321			51	0	0	42	138	0	0	42
IPE 100	339	321	Vento X	PolG	0	0	0	41	93	0	0	41

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	339	321	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1080												
IPE 100	340	322	Peso Proprio	UnifG	0	0	0	8	144	0	0	8
IPE 100	340	322	QP Solai	PolG	0	0	0	68	51	0	0	86
IPE 100	340	322			51	0	0	86	99	0	0	86
IPE 100	340	322	QV Solai	PolG	0	0	0	22	51	0	0	28
IPE 100	340	322			51	0	0	28	99	0	0	28
IPE 100	340	322	Neve	PolG	0	0	0	28	144	0	0	22
IPE 100	340	322			99	0	0	27	144	0	0	16
IPE 100	340	322	Neve	PolG	0	0	0	15	51	0	0	26
IPE 100	340	322	Vento X	PolG	0	0	0	24	51	0	0	41
IPE 100	340	322			51	0	0	41	144	0	0	41
IPE 100	340	322	Vento X	PolG	0	0	0	42	99	0	0	42
IPE 100	340	322			99	0	0	42	144	0	0	25
IPE 100	340	322	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1081												
IPE 100	318	319	Peso Proprio	UnifG	0	0	0	8	150	0	0	8
IPE 100	318	319	QP Solai	PolG	0	0	0	27	51	0	0	44
IPE 100	318	319			51	0	0	44	150	0	0	44
IPE 100	318	319	QV Solai	PolG	0	0	0	9	51	0	0	14
IPE 100	318	319			51	0	0	14	150	0	0	14
IPE 100	318	319	Neve	PolG	0	0	0	17	51	0	0	27
IPE 100	318	319			51	0	0	27	150	0	0	27
IPE 100	318	319	Vento X	PolG	0	0	0	26	51	0	0	42
IPE 100	318	319			51	0	0	42	150	0	0	42
IPE 100	318	319	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1082												
IPE 100	170	125	Peso Proprio	UnifG	0	0	0	8	120	0	0	8
IPE 100	170	125	QP Solai	PolG	0	0	0	80	51	0	0	110
IPE 100	170	125			51	0	0	110	75	0	0	110
IPE 100	170	125	QV Solai	PolG	0	0	0	26	51	0	0	35
IPE 100	170	125			51	0	0	35	75	0	0	35
IPE 100	170	125	Neve	PolG	0	0	0	35	120	0	0	27
IPE 100	170	125			75	0	0	17	51	0	0	36
IPE 100	170	125	Neve	PolG	0	0	0	33	75	0	0	33
IPE 100	170	125			75	0	0	33	120	0	0	16
IPE 100	170	125	Vento X	PolG	0	0	0	27	51	0	0	55
IPE 100	170	125			51	0	0	55	120	0	0	55
IPE 100	170	125	Vento X	PolG	0	0	0	50	75	0	0	50
IPE 100	170	125			75	0	0	50	120	0	0	25
IPE 100	170	125	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1083												
IPE 100	169	124	Peso Proprio	UnifG	0	0	0	8	114	0	0	8
IPE 100	169	124	QP Solai	PolG	0	0	0	86	51	0	0	119
IPE 100	169	124			51	0	0	119	69	0	0	119
IPE 100	169	124	QV Solai	PolG	0	0	0	28	51	0	0	38
IPE 100	169	124			51	0	0	38	69	0	0	38
IPE 100	169	124	Neve	PolG	0	0	0	18	51	0	0	38
IPE 100	169	124			51	0	0	38	114	0	0	38
IPE 100	169	124	Neve	PolG	0	0	0	36	69	0	0	36
IPE 100	169	124	Vento X	PolG	0	0	0	55	69	0	0	55
IPE 100	169	124			69	0	0	55	114	0	0	26
IPE 100	169	124	Vento X	PolG	0	0	0	27	51	0	0	59
IPE 100	169	124			51	0	0	59	114	0	0	59
IPE 100	169	124	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 1084												
IPE 100	167	122	Peso Proprio	UnifG	0	0	0	8	102	0	0	8

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	167	122		PolG	0	0	0	95	51	0	0	135
			QP Solai		51	0	0	135	57	0	0	135
IPE 100	167	122		PolG	0	0	0	135	102	0	0	97
			QV Solai		30	51	0	30	51	0	0	43
IPE 100	167	122		PolG	51	0	0	43	57	0	0	43
			Neve		57	0	0	43	102	0	0	31
IPE 100	167	122		PolG	0	0	0	18	51	0	0	43
			Neve		51	0	0	43	102	0	0	43
IPE 100	167	122		PolG	0	0	0	41	57	0	0	41
			Neve		57	0	0	41	102	0	0	17
IPE 100	167	122		PolG	0	0	0	64	57	0	0	64
			Vento X		57	0	0	64	102	0	0	27
IPE 100	167	122		PolG	0	0	0	27	51	0	0	67
			Vento X		51	0	0	27	51	0	0	67
IPE 100	167	122		Termico	AXY=15°C, AXZ=15°C	51	0	67	102	0	0	67
			Carichi termici									
Trave 1085												
IPE 100	239	221		UnitG	0	0	0	8	126	0	0	8
			Peso Proprio		0	0	0	75	51	0	0	100
IPE 100	239	221		PolG	0	0	0	100	81	0	0	100
			QP Solai		51	0	0	100	126	0	0	77
IPE 100	239	221		PolG	81	0	0	24	51	0	0	32
			QV Solai		51	0	0	32	81	0	0	32
IPE 100	239	221		PolG	81	0	0	32	126	0	0	25
			Neve		0	0	0	17	51	0	0	33
IPE 100	239	221		PolG	51	0	0	33	126	0	0	33
			Neve		0	0	0	30	81	0	0	30
IPE 100	239	221		PolG	81	0	0	30	126	0	0	16
			Vento X		0	0	0	26	51	0	0	50
IPE 100	239	221		PolG	51	0	0	50	126	0	0	50
			Vento X		0	0	0	46	81	0	0	46
IPE 100	239	221		Termico	AXY=15°C, AXZ=15°C	81	0	46	126	0	0	24
			Carichi termici									
Trave 1086												
IPE 100	168	123		UnitG	0	0	0	8	108	0	0	8
			Peso Proprio		0	0	0	91	51	0	0	128
IPE 100	168	123		PolG	0	0	0	128	63	0	0	128
			QP Solai		51	0	0	128	108	0	0	94
IPE 100	168	123		PolG	0	0	0	29	51	0	0	41
			QV Solai		51	0	0	41	63	0	0	41
IPE 100	168	123		PolG	63	0	0	41	108	0	0	30
			Neve		0	0	0	38	63	0	0	38
IPE 100	168	123		PolG	63	0	0	38	108	0	0	17
			Neve		0	0	0	18	51	0	0	41
IPE 100	168	123		PolG	51	0	0	41	108	0	0	41
			Vento X		0	0	0	59	63	0	0	59
IPE 100	168	123		PolG	63	0	0	59	108	0	0	27
			Vento X		0	0	0	28	51	0	0	64
IPE 100	168	123		Termico	AXY=15°C, AXZ=15°C	51	0	64	108	0	0	64
			Carichi termici									
Trave 1087												
IPE 100	166	121		UnitG	0	0	0	8	96	0	0	8
			Peso Proprio		0	0	0	96	51	0	0	140
IPE 100	166	121		PolG	0	0	0	140	96	0	0	98
			QP Solai		51	0	0	31	51	0	0	45
IPE 100	166	121		PolG	0	0	0	45	96	0	0	31
			QV Solai		51	0	0	31	51	0	0	44
IPE 100	166	121		PolG	0	0	0	17	51	0	0	44
			Neve		51	0	0	44	96	0	0	44
IPE 100	166	121		PolG	0	0	0	43	51	0	0	43
			Neve		51	0	0	43	96	0	0	17
IPE 100	166	121		PolG	0	0	0	26	51	0	0	68
			Vento X		51	0	0	68	96	0	0	68
IPE 100	166	121		PolG	51	0	0	67	51	0	0	67
			Vento X		51	0	0	67	96	0	0	26
IPE 100	166	121		Termico	AXY=15°C, AXZ=15°C	51	0	67	96	0	0	26
			Carichi termici									
Trave 1088												
IPE 100	108	109		UnitG	0	0	0	8	90	0	0	8
			Peso Proprio									

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	108	109		PolG	0	0	0	71	45	0	0	71
			QP Solai		45	0	0	71	90	0	0	26
IPE 100	108	109		PolG	0	0	0	23	45	0	0	23
			QV Solai		45	0	0	23	90	0	0	8
IPE 100	108	109		PolG	0	0	0	44	45	0	0	44
			Neve		45	0	0	44	90	0	0	16
IPE 100	108	109		PolG	0	0	0	68	45	0	0	68
			Vento X		45	0	0	68	90	0	0	25
IPE 100	108	109		Termico	ΔXY=15°C, ΔXZ=15°C	45	0	68	90	0	0	25
			Carichi termici									
Trave 1089												
IPE 100	321	323		UnitG	0	0	0	8	137	0	0	8
			Peso Proprio		0	0	0	63	44	0	0	86
IPE 100	321	323		PolG	0	0	0	86	100	0	0	86
			QP Solai		44	0	0	86	137	0	0	64
IPE 100	321	323		PolG	100	0	0	20	44	0	0	28
			QV Solai		44	0	0	28	100	0	0	28
IPE 100	321	323		PolG	100	0	0	26	100	0	0	21
			Neve		0	0	0	26	137	0	0	13
IPE 100	321	323		PolG	0	0	0	13	44	0	0	27
			Neve		44	0	0	27	137	0	0	27
IPE 100	321	323		PolG	0	0	0	41	100	0	0	40
			Vento X		100	0	0	40	137	0	0	19
IPE 100	321	323		PolG	0	0	0	20	44	0	0	42
			Vento X		44	0	0	42	137	0	0	42
IPE 100	321	323		Termico	ΔXY=15°C, ΔXZ=15°C	44	0	42	137	0	0	42
			Carichi termici									
Trave 1090												
IPE 100	322	324		UnitG	0	0	0	8	143	0	0	8
			Peso Proprio		0	0	0	64	44	0	0	86
IPE 100	322	324		PolG	0	0	0	86	106	0	0	86
			QP Solai		44	0	0	86	143	0	0	64
IPE 100	322	324		PolG	106	0	0	21	44	0	0	28
			QV Solai		44	0	0	28	106	0	0	28
IPE 100	322	324		PolG	106	0	0	27	106	0	0	21
			Neve		106	0	0	27	143	0	0	14
IPE 100	322	324		PolG	0	0	0	13	44	0	0	26
			Neve		44	0	0	26	143	0	0	26
IPE 100	322	324		PolG	0	0	0	42	106	0	0	42
			Vento X		106	0	0	42	143	0	0	21
IPE 100	322	324		PolG	0	0	0	20	44	0	0	41
			Vento X		44	0	0	41	143	0	0	41
IPE 100	322	324		Termico	ΔXY=15°C, ΔXZ=15°C	44	0	41	143	0	0	41
			Carichi termici									
Trave 1091												
IPE 100	319	320		UnitG	0	0	0	8	137	0	0	8
			Peso Proprio		0	0	0	22	44	0	0	44
IPE 100	319	320		PolG	0	0	0	44	149	0	0	44
			QP Solai		44	0	0	7	44	0	0	14
IPE 100	319	320		PolG	0	0	0	14	149	0	0	14
			QV Solai		44	0	0	14	149	0	0	27
IPE 100	319	320		PolG	0	0	0	27	149	0	0	27
			Neve		44	0	0	27	149	0	0	42
IPE 100	319	320		PolG	0	0	0	21	44	0	0	42
			Vento X		44	0	0	42	149	0	0	42
IPE 100	319	320		Termico	ΔXY=15°C, ΔXZ=15°C	44	0	42	149	0	0	42
			Carichi termici									
Trave 1092												
IPE 100	222	224		UnitG	0	0	0	8	131	0	0	8
			Peso Proprio		0	0	0	66	44	0	0	92
IPE 100	222	224		PolG	0	0	0	92	94	0	0	92
			QP Solai		44	0	0	92	131	0	0	68
IPE 100	222	224		PolG	94	0	0	21	44	0	0	29
			QV Solai		44	0	0	29	94	0	0	29
IPE 100	222	224		PolG	0	0	0	13	44	0	0	30
			Neve		94	0	0	30	131	0	0	30
IPE 100	222	224		PolG	0	0	0	27	94	0	0	27
			Neve		44	0	0	27	131	0	0	13
IPE 100	222	224		PolG	94	0	0	27	131	0	0	13
			Neve		44	0	0	27	131	0	0	13

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	222	224	Vento X	PolG	0	0	0	42	94	0	0	42
IPE 100	222	224	Vento X	PolG	94	0	0	42	131	0	0	20
IPE 100	222	224	Vento X	PolG	0	0	0	21	44	0	0	46
IPE 100	222	224	Carichi termici	Termico	44	0	0	46	131	0	0	46
Trave 1093 AXY=15°C,AXZ=15°C												
IPE 100	221	223	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	221	223	QP Solai	PolG	0	0	0	70	44	0	0	100
IPE 100					44	0	0	100	88	0	0	100
IPE 100	221	223	QV Solai	PolG	88	0	0	100	125	0	0	73
IPE 100					44	0	0	32	44	0	0	32
IPE 100					44	0	0	32	88	0	0	32
IPE 100	221	223	Neve	PolG	88	0	0	32	125	0	0	24
IPE 100					44	0	0	14	44	0	0	33
IPE 100	221	223	Neve	PolG	44	0	0	33	125	0	0	33
IPE 100	221	223	Vento X	PolG	88	0	0	30	88	0	0	30
IPE 100					88	0	0	30	125	0	0	13
IPE 100	221	223	Vento X	PolG	0	0	0	46	88	0	0	46
IPE 100					88	0	0	46	125	0	0	20
IPE 100	221	223	Vento X	PolG	0	0	0	22	44	0	0	50
IPE 100					44	0	0	50	125	0	0	50
Trave 1094 AXY=15°C,AXZ=15°C												
IPE 100	123	128	Peso Proprio	UnifG	0	0	0	8	107	0	0	8
IPE 100	123	128	QP Solai	PolG	0	0	0	87	44	0	0	128
IPE 100					44	0	0	128	69	0	0	128
IPE 100	123	128	QV Solai	PolG	69	0	0	128	107	0	0	90
IPE 100					44	0	0	28	44	0	0	41
IPE 100					69	0	0	41	69	0	0	41
IPE 100	123	128	Neve	PolG	69	0	0	41	107	0	0	29
IPE 100					44	0	0	15	44	0	0	41
IPE 100	123	128	Neve	PolG	44	0	0	41	107	0	0	41
IPE 100					69	0	0	38	69	0	0	38
IPE 100	123	128	Vento X	PolG	0	0	0	38	107	0	0	15
IPE 100					69	0	0	59	69	0	0	59
IPE 100	123	128	Vento X	PolG	69	0	0	59	107	0	0	23
IPE 100					64	0	0	24	44	0	0	64
IPE 100	123	128	Carichi termici	Termico	44	0	0	64	107	0	0	64
Trave 1095 AXY=15°C,AXZ=15°C												
IPE 100	125	130	Peso Proprio	UnifG	0	0	0	8	119	0	0	8
IPE 100	125	130	QP Solai	PolG	0	0	0	76	44	0	0	110
IPE 100					44	0	0	110	82	0	0	110
IPE 100	125	130	QV Solai	PolG	82	0	0	110	119	0	0	80
IPE 100					44	0	0	24	44	0	0	35
IPE 100					44	0	0	35	82	0	0	35
IPE 100	125	130	Neve	PolG	82	0	0	35	119	0	0	26
IPE 100					0	0	0	33	82	0	0	33
IPE 100	125	130	Neve	PolG	82	0	0	33	119	0	0	14
IPE 100					44	0	0	15	44	0	0	36
IPE 100	125	130	Vento X	PolG	44	0	0	36	119	0	0	36
IPE 100					44	0	0	23	44	0	0	55
IPE 100	125	130	Vento X	PolG	44	0	0	55	119	0	0	55
IPE 100	125	130	Vento X	PolG	0	0	0	50	82	0	0	50
IPE 100	125	130	Carichi termici	Termico	82	0	0	50	119	0	0	21
Trave 1096 AXY=15°C,AXZ=15°C												
IPE 100	122	127	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	122	127	QP Solai	PolG	0	0	0	91	44	0	0	135
IPE 100					44	0	0	135	63	0	0	135
IPE 100	122	127	QV Solai	PolG	63	0	0	135	101	0	0	93
IPE 100					44	0	0	29	44	0	0	43
IPE 100					44	0	0	43	63	0	0	43
IPE 100	122	127	Neve	PolG	63	0	0	43	101	0	0	30
IPE 100					44	0	0	15	44	0	0	43
IPE 100	122	127	Carichi termici	Termico	44	0	0	43	101	0	0	43

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
IPE 100	122	127	Neve	PolG	0	0	0	41	63	0	0	41
IPE 100	122	127	Vento X	PolG	63	0	0	41	101	0	0	15
IPE 100	122	127	Vento X	PolG	44	0	0	67	101	0	0	67
IPE 100	122	127	Vento X	PolG	0	0	0	64	63	0	0	64
IPE 100	122	127	Carichi termici	Termico	63	0	0	64	101	0	0	23
Trave 1097 AXY=15°C,AXZ=15°C												
IPE 100	121	126	Peso Proprio	UnifG	0	0	0	8	95	0	0	8
IPE 100	121	126	QP Solai	PolG	0	0	0	93	44	0	0	140
IPE 100					44	0	0	140	57	0	0	140
IPE 100	121	126	QV Solai	PolG	57	0	0	140	95	0	0	94
IPE 100					44	0	0	30	44	0	0	45
IPE 100					44	0	0	45	57	0	0	45
IPE 100	121	126	Neve	PolG	57	0	0	43	57	0	0	43
IPE 100	121	126	Neve	PolG	0	0	0	15	44	0	0	44
IPE 100	121	126	Vento X	PolG	44	0	0	44	95	0	0	44
IPE 100	121	126	Vento X	PolG	0	0	0	23	44	0	0	68
IPE 100					44	0	0	68	95	0	0	68
IPE 100	121	126	Vento X	PolG	0	0	0	67	57	0	0	67
IPE 100	121	126	Carichi termici	Termico	57	0	0	67	95	0	0	23
Trave 1098 AXY=15°C,AXZ=15°C												
IPE 100	124	129	Peso Proprio	UnifG	0	0	0	8	113	0	0	8
IPE 100	124	129	QP Solai	PolG	0	0	0	82	44	0	0	119
IPE 100					44	0	0	119	75	0	0	119
IPE 100	124	129	QV Solai	PolG	75	0	0	119	113	0	0	85
IPE 100					44	0	0	26	44	0	0	38
IPE 100					44	0	0	38	75	0	0	38
IPE 100	124	129	Neve	PolG	75	0	0	36	75	0	0	36
IPE 100	124	129	Neve	PolG	0	0	0	15	44	0	0	14
IPE 100					44	0	0	38	113	0	0	38
IPE 100	124	129	Vento X	PolG	0	0	0	55	75	0	0	55
IPE 100	124	129	Vento X	PolG	75	0	0	55	113	0	0	22
IPE 100					44	0	0	23	44	0	0	59
IPE 100	124	129	Carichi termici	Termico	44	0	0	59	113	0	0	59
Trave 1099 AXY=15°C,AXZ=15°C												
IPE 100	109	110	Peso Proprio	UnifG	0	0	0	8	89	0	0	8
IPE 100	109	110	QP Solai	PolG	0	0	0	71	51	0	0	71
IPE 100	109	110	QV Solai	PolG	51	0	0	71	89	0	0	23
IPE 100					51	0	0	23	51	0	0	23
IPE 100	109	110	Neve	PolG	0	0	0	44	51	0	0	44
IPE 100	109	110	Neve	PolG	51	0	0	44	89	0	0	14
IPE 100	109	110	Vento X	PolG	0	0	0	68	51	0	0	68
IPE 100	109	110	Carichi termici	Termico	51	0	0	68	89	0	0	22
Trave 1099 AXY=15°C,AXZ=15°C												
IPE 100	101	151	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
IPE 100	101	151	QP Solai	PolG	0	0	0	37	182	0	0	48
IPE 100	101	151	QV Solai	PolG	0	0	0	12	182	0	0	15
IPE 100	101	151	Neve	PolG	0	0	0	23	182	0	0	30
IPE 100	101	151	Vento X	PolG	0	0	0	36	182	0	0	46
IPE 100	101	151	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	151	152	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
IPE 100	151	152	QP Solai	PolG	0	0	0	37	178	0	0	48
IPE 100	151	152	QV Solai	PolG	0	0	0	12	178	0	0	15
IPE 100	151	152	Neve	PolG	0	0	0	23	178	0	0	30
IPE 100	151	152	Vento X	PolG	0	0	0	36	178	0	0	46
IPE 100	151	152	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	152	153	Peso Proprio	UnifG	0	0	0	60	170	0	0	60

Sezione	Ni	Nf	Cond	Tipo c	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf			
HE 240 A	103	136	QP Solai	PolG	0	0	0	0	83	125	0	0	86		
HE 240 A	103	136		PolG	125	0	0	0	86	182	0	0	73		
HE 240 A	103	136		PolG	125	0	0	0	27	125	0	0	28		
HE 240 A	103	136		PolG	125	0	0	0	28	182	0	0	23		
HE 240 A	103	136	Neve	PolG	0	0	0	0	29	182	0	0	23		
HE 240 A	103	136	Neve	PolG	0	0	0	0	22	125	0	0	28		
HE 240 A	103	136	Vento X	PolG	125	0	0	0	28	182	0	0	22		
HE 240 A	103	136		PolG	125	0	0	0	35	125	0	0	44		
HE 240 A	103	136	Vento X	PolG	125	0	0	0	44	182	0	0	34		
HE 240 A	103	136		PolG	0	0	0	0	46	182	0	0	36		
HE 240 A	103	136	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	UnifG	0	0	0	60	178	0	0	60	
HE 240 A	103	136				Peso Proprio	PolG	0	0	0	83	131	0	0	86
HE 240 A	136	137				QP Solai	PolG	131	0	0	86	178	0	0	75
HE 240 A	136	137				QV Solai	PolG	0	0	0	27	131	0	0	28
HE 240 A	136	137				Neve	PolG	131	0	0	28	178	0	0	24
HE 240 A	136	137				Neve	PolG	0	0	0	30	178	0	0	23
HE 240 A	136	137				Neve	PolG	0	0	0	22	131	0	0	29
HE 240 A	136	137				Neve	PolG	131	0	0	29	178	0	0	23
HE 240 A	136	137				Vento X	PolG	0	0	0	35	131	0	0	45
HE 240 A	136	137				Vento X	PolG	131	0	0	45	178	0	0	36
HE 240 A	136	137				Vento X	PolG	0	0	0	46	178	0	0	36
HE 240 A	136	137				Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	UnifG	0	0	0	60	170	0
HE 240 A	137	138	Peso Proprio	PolG	0				0	0	83	134	0	0	86
HE 240 A	137	138	QP Solai	PolG	134				0	0	86	170	0	0	77
HE 240 A	137	138	QV Solai	PolG	0				0	0	27	134	0	0	28
HE 240 A	137	138	Neve	PolG	134				0	0	28	170	0	0	25
HE 240 A	137	138	Neve	PolG	0				0	0	22	134	0	0	29
HE 240 A	137	138	Neve	PolG	134				0	0	29	170	0	0	25
HE 240 A	137	138	Vento X	PolG	0				0	0	30	170	0	0	23
HE 240 A	137	138	Vento X	PolG	0				0	0	46	170	0	0	36
HE 240 A	137	138	Vento X	PolG	0				0	0	35	134	0	0	45
HE 240 A	137	138	Vento X	PolG	134				0	0	45	170	0	0	38
HE 240 A	137	138	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C				UnifG	0	0	0	60	158	0
HE 240 A	138	139				Peso Proprio	PolG	0	0	0	84	132	0	0	87
HE 240 A	138	139				QP Solai	PolG	132	0	0	87	158	0	0	79
HE 240 A	138	139				QV Solai	PolG	0	0	0	27	132	0	0	28
HE 240 A	138	139				Neve	PolG	132	0	0	28	158	0	0	25
HE 240 A	138	139				Neve	PolG	0	0	0	22	132	0	0	30
HE 240 A	138	139				Neve	PolG	132	0	0	30	158	0	0	26
HE 240 A	138	139				Neve	PolG	0	0	0	30	158	0	0	23
HE 240 A	138	139				Vento X	PolG	0	0	0	35	132	0	0	46
HE 240 A	138	139				Vento X	PolG	132	0	0	46	158	0	0	40
HE 240 A	138	139				Vento X	PolG	0	0	0	46	158	0	0	36
HE 240 A	138	139				Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	UnifG	0	0	0	60	148	0
HE 240 A	138	139	Peso Proprio	PolG	0				0	0	84	131	0	0	87
HE 240 A	139	140	QP Solai	PolG	131				0	0	87	148	0	0	82
HE 240 A	139	140	QV Solai	PolG	0				0	0	27	131	0	0	28
HE 240 A	139	140	Neve	PolG	131				0	0	28	148	0	0	26
HE 240 A	139	140	Neve	PolG	0				0	0	22	131	0	0	30
HE 240 A	139	140	Neve	PolG	131				0	0	30	148	0	0	28
HE 240 A	139	140	Vento X	PolG	0				0	0	30	148	0	0	23
HE 240 A	139	140	Vento X	PolG	0				0	0	46	148	0	0	36
HE 240 A	139	140	Vento X	PolG	0				0	0	35	131	0	0	46
HE 240 A	139	140	Vento X	PolG	131				0	0	46	148	0	0	43
HE 240 A	139	140	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C				UnifG	0	0	0	60	134	0
HE 240 A	140	227				Peso Proprio	PolG	0	0	0	84	125	0	0	87
HE 240 A	140	227				QP Solai	PolG	125	0	0	87	134	0	0	84
HE 240 A	140	227				QV Solai	PolG	0	0	0	27	125	0	0	28
HE 240 A	140	227	Neve	PolG	125	0	0	28	134	0	0	27			
HE 240 A	140	227	Neve	PolG	0	0	0	22	125	0	0	30			
HE 240 A	140	227	Neve	PolG	125	0	0	30	134	0	0	29			

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf	
HE 240 A	140	227	Neve Vento X Vento X	PolG	0	0	0	0	30	134	0	0	23
	140	227		PolG	0	0	0	0	46	134	0	0	36
	140	227		PolG	0	0	0	0	35	125	0	0	47
				Termico AXY=15°C, AXZ=15°C	125	0	0	0	47	134	0	0	45
HE 240 A	140	227	Carichi termici	Termico	AXY=15°C, AXZ=15°C								
HE 240 A	227	228	Peso Proprio	UnifG	0	0	0	0	60	123	0	0	60
HE 240 A	227	228	QP Solai	PolG	0	0	0	0	84	120	0	0	87
HE 240 A				PolG	120	0	0	0	87	123	0	0	86
HE 240 A	227	228	QV Solai	PolG	0	0	0	0	27	120	0	0	28
HE 240 A	227	228	Neve	PolG	0	0	0	0	30	113	0	0	23
HE 240 A	228	327	Neve	PolG	0	0	0	0	22	113	0	0	31
HE 240 A	228	327	Vento X	PolG	0	0	0	0	35	113	0	0	48
HE 240 A	228	327	Vento X	PolG	0	0	0	0	46	113	0	0	36
HE 240 A	228	327	Carichi termici	Termico	AXY=15°C, AXZ=15°C								
HE 240 A	228	327	Peso Proprio	UnifG	0	0	0	0	60	108	0	0	60
HE 240 A	327	328	QP Solai	PolG	0	0	0	0	84	108	0	0	87
HE 240 A	327	328	QV Solai	PolG	0	0	0	0	27	108	0	0	28
HE 240 A	327	328	Neve	PolG	0	0	0	0	22	108	0	0	31
HE 240 A	327	328	Neve	PolG	0	0	0	0	30	108	0	0	23
HE 240 A	327	328	Vento X	PolG	0	0	0	0	46	108	0	0	36
HE 240 A	327	328	Vento X	PolG	0	0	0	0	35	108	0	0	48
HE 240 A	327	328	Carichi termici	Termico	AXY=15°C, AXZ=15°C								
HE 240 A	327	328	Peso Proprio	UnifG	0	0	0	0	60	112	0	0	60
HE 240 A	328	313	QP Solai	PolG	0	0	0	0	84	112	0	0	87
HE 240 A	328	313	QV Solai	PolG	0	0	0	0	27	112	0	0	28
HE 240 A	328	313	Neve	PolG	0	0	0	0	30	112	0	0	23
HE 240 A	328	313	Neve	PolG	0	0	0	0	22	112	0	0	31
HE 240 A	328	313	Vento X	PolG	0	0	0	0	46	112	0	0	36
HE 240 A	328	313	Vento X	PolG	0	0	0	0	35	112	0	0	48
HE 240 A	328	313	Carichi termici	Termico	AXY=15°C, AXZ=15°C								
Tavola 8003													
HE 240 A	104	146	Peso Proprio	UnifG	0	0	0	0	60	182	0	0	60
HE 240 A	104	146	QP Solai	PolG	0	0	0	0	69	54	0	0	86
				PolG	54	0	0	0	86	113	0	0	88
					113	0	0	0	88	182	0	0	69
HE 240 A	104	146	QV Solai	PolG	0	0	0	0	22	54	0	0	28
				PolG	54	0	0	0	28	113	0	0	28
					113	0	0	0	28	182	0	0	22
				PolG	0	0	0	0	23	54	0	0	29
					54	0	0	0	29	182	0	0	21
HE 240 A	104	146	Neve	PolG	0	0	0	0	20	113	0	0	29
				PolG	113	0	0	0	29	182	0	0	22
HE 240 A	104	146	Neve	PolG	0	0	0	0	35	54	0	0	45
HE 240 A	104	146	Vento X	PolG	0	0	0	0	45	182	0	0	32
				PolG	54	0	0	0	31	113	0	0	45
HE 240 A	104	146	Vento X	PolG	0	0	0	0	31	113	0	0	45
					113	0	0	0	45	182	0	0	34
Tavola 8004													
HE 240 A	104	146	Carichi termici	Termico	AXY=15°C, AXZ=15°C								
HE 240 A	104	146	Peso Proprio	UnifG	0	0	0	0	60	178	0	0	60
HE 240 A	146	147	QP Solai	PolG	0	0	0	0	71	44	0	0	86
HE 240 A	146	147	Neve	PolG	44	0	0	0	86	118	0	0	88
					118	0	0	0	88	178	0	0	72
				PolG	0	0	0	0	23	44	0	0	28
HE 240 A	146	147	QV Solai	PolG	44	0	0	0	28	118	0	0	28
					118	0	0	0	28	178	0	0	23
			Neve	PolG	0	0	0	0	20	111	0	0	30
HE 240 A	146	147		PolG	0	0	0	0	20	111	0	0	30

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
HE 240 A	146	147	Neve	PolG	118	0	0	30	178	0	0	24
HE 240 A	146	147	Neve	PolG	0	0	0	24	44	0	0	30
HE 240 A	146	147	Vento X	PolG	44	0	0	30	178	0	0	21
HE 240 A	146	147	Vento X	PolG	0	0	0	31	118	0	0	46
HE 240 A	146	147	Vento X	PolG	118	0	0	46	178	0	0	36
HE 240 A	146	147	Vento X	PolG	0	0	0	37	44	0	0	46
HE 240 A	146	147	Carichi termici	Termico	44	0	0	0	46	178	0	32
HE 240 A	147	148	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C							
HE 240 A	147	148	QP Solai	PolG	0	0	0	60	170	0	0	60
HE 240 A	147	148	QP Solai	PolG	0	0	0	74	35	0	0	86
HE 240 A	147	148	QP Solai	PolG	35	0	0	86	120	0	0	88
HE 240 A	147	148	QP Solai	PolG	120	0	0	88	170	0	0	74
HE 240 A	147	148	QP Solai	PolG	0	0	0	24	35	0	0	27
HE 240 A	147	148	QP Solai	PolG	35	0	0	27	120	0	0	28
HE 240 A	147	148	QP Solai	PolG	120	0	0	28	170	0	0	24
HE 240 A	147	148	QP Solai	PolG	0	0	0	20	120	0	0	30
HE 240 A	147	148	QP Solai	PolG	120	0	0	30	170	0	0	25
HE 240 A	147	148	QP Solai	PolG	0	0	0	26	35	0	0	30
HE 240 A	147	148	QP Solai	PolG	35	0	0	30	170	0	0	21
HE 240 A	147	148	QP Solai	PolG	0	0	0	31	120	0	0	47
HE 240 A	147	148	QP Solai	PolG	120	0	0	47	170	0	0	39
HE 240 A	147	148	QP Solai	PolG	0	0	0	40	35	0	0	47
HE 240 A	147	148	QP Solai	PolG	35	0	0	47	170	0	0	32
HE 240 A	147	148	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	148	149	Peso Proprio	UnifG	0	0	0	60	159	0	0	60
HE 240 A	148	149	QP Solai	PolG	0	0	0	76	25	0	0	85
HE 240 A	148	149	QP Solai	PolG	25	0	0	85	119	0	0	88
HE 240 A	148	149	QP Solai	PolG	119	0	0	88	159	0	0	76
HE 240 A	148	149	QP Solai	PolG	0	0	0	24	25	0	0	27
HE 240 A	148	149	QP Solai	PolG	25	0	0	27	119	0	0	28
HE 240 A	148	149	QP Solai	PolG	119	0	0	28	159	0	0	24
HE 240 A	148	149	QP Solai	PolG	0	0	0	27	25	0	0	31
HE 240 A	148	149	QP Solai	PolG	25	0	0	31	159	0	0	21
HE 240 A	148	149	QP Solai	PolG	119	0	0	31	159	0	0	31
HE 240 A	148	149	QP Solai	PolG	0	0	0	31	119	0	0	48
HE 240 A	148	149	QP Solai	PolG	119	0	0	48	159	0	0	41
HE 240 A	148	149	QP Solai	PolG	0	0	0	42	25	0	0	47
HE 240 A	148	149	QP Solai	PolG	25	0	0	47	159	0	0	32
HE 240 A	148	149	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	149	150	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	149	150	QP Solai	PolG	0	0	0	79	16	0	0	85
HE 240 A	149	150	QP Solai	PolG	16	0	0	85	117	0	0	88
HE 240 A	149	150	QP Solai	PolG	117	0	0	88	148	0	0	78
HE 240 A	149	150	QP Solai	PolG	0	0	0	25	16	0	0	27
HE 240 A	149	150	QP Solai	PolG	16	0	0	27	117	0	0	28
HE 240 A	149	150	QP Solai	PolG	117	0	0	28	148	0	0	25
HE 240 A	149	150	QP Solai	PolG	0	0	0	20	117	0	0	32
HE 240 A	149	150	QP Solai	PolG	117	0	0	32	148	0	0	28
HE 240 A	149	150	QP Solai	PolG	0	0	0	29	16	0	0	31
HE 240 A	149	150	QP Solai	PolG	16	0	0	31	148	0	0	21
HE 240 A	149	150	QP Solai	PolG	0	0	0	31	117	0	0	49
HE 240 A	149	150	QP Solai	PolG	117	0	0	49	148	0	0	43
HE 240 A	149	150	QP Solai	PolG	0	0	0	44	16	0	0	48
HE 240 A	149	150	QP Solai	PolG	16	0	0	48	148	0	0	32
HE 240 A	149	150	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	150	231	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	150	231	QP Solai	PolG	0	0	0	81	9	0	0	85
HE 240 A	150	231	QP Solai	PolG	9	0	0	85	112	0	0	89
HE 240 A	150	231	QP Solai	PolG	112	0	0	89	134	0	0	81
HE 240 A	150	231	QP Solai	PolG	0	0	0	26	9	0	0	27
HE 240 A	150	231	QP Solai	PolG	9	0	0	27	112	0	0	28
HE 240 A	150	231	QP Solai	PolG	112	0	0	28	134	0	0	26
HE 240 A	150	231	QP Solai	PolG	0	0	0	30	9	0	0	32
HE 240 A	150	231	QP Solai	PolG	9	0	0	32	134	0	0	21
HE 240 A	150	231	QP Solai	PolG	0	0	0	20	112	0	0	32

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	150	231	Vento X	PolG	112	0	0	32	134	0	0	29
HE 240 A	150	231	Vento X	PolG	9	0	0	49	134	0	0	32
HE 240 A	150	231			112	0	0	50	134	0	0	45
HE 240 A	150	231	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
	HE 240 A	231	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
	HE 240 A	231	QP Solai	PolG	2	0	0	85	108	0	0	89
HE 240 A					108	0	0	89	123	0	0	83
					0	0	0	27	2	0	0	27
					2	0	0	27	108	0	0	28
HE 240 A	231	232	Neve	PolG	108	0	0	32	2	0	0	32
HE 240 A	231	232	Neve	PolG	2	0	0	32	123	0	0	21
HE 240 A	231	232	Vento X	PolG	108	0	0	33	123	0	0	33
HE 240 A	231	232	Vento X	PolG	108	0	0	31	108	0	0	51
HE 240 A	231	232	Vento X	PolG	108	0	0	51	123	0	0	47
HE 240 A	231	232			2	0	0	49	2	0	0	50
HE 240 A	231	232	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
	HE 240 A	232	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
	HE 240 A	232	QP Solai	PolG	104	0	0	89	113	0	0	85
HE 240 A					104	0	0	27	104	0	0	29
HE 240 A	232	331	QP Solai	PolG	104	0	0	29	113	0	0	27
HE 240 A	232	331	Neve	PolG	0	0	0	20	104	0	0	33
HE 240 A	232	331	Neve	PolG	104	0	0	33	113	0	0	32
HE 240 A	232	331	Vento X	PolG	0	0	0	32	113	0	0	21
HE 240 A	232	331	Vento X	PolG	104	0	0	31	104	0	0	49
HE 240 A	232	331	Vento X	PolG	0	0	0	52	113	0	0	32
HE 240 A	232	331	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
	HE 240 A	331	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
	HE 240 A	331	QP Solai	PolG	0	0	0	84	104	0	0	89
HE 240 A					104	0	0	89	108	0	0	87
HE 240 A	331	332	QP Solai	PolG	104	0	0	27	104	0	0	29
HE 240 A	331	332	Neve	PolG	104	0	0	29	108	0	0	28
HE 240 A	331	332	Neve	PolG	0	0	0	32	108	0	0	21
HE 240 A	331	332	Vento X	PolG	0	0	0	20	104	0	0	34
HE 240 A	331	332	Vento X	PolG	104	0	0	34	108	0	0	33
HE 240 A	331	332	Vento X	PolG	0	0	0	50	108	0	0	32
HE 240 A	331	332	Vento X	PolG	0	0	0	31	104	0	0	53
HE 240 A	331	332	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
	HE 240 A	331	Peso Proprio	UnifG	104	0	0	53	108	0	0	52
	HE 240 A	332	QP Solai	PolG	0	0	0	60	112	0	0	60
HE 240 A	332	314	QP Solai	PolG	0	0	0	84	112	0	0	89
HE 240 A	332	314	QP Solai	PolG	0	0	0	27	112	0	0	29
HE 240 A	332	314	Neve	PolG	0	0	0	32	112	0	0	21
HE 240 A	332	314	Neve	PolG	0	0	0	20	112	0	0	35
HE 240 A	332	314	Vento X	PolG	0	0	0	50	112	0	0	32
HE 240 A	332	314	Vento X	PolG	0	0	0	31	112	0	0	53
Trave 8004												
HE 240 A	105	131	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	105	131	QP Solai	PolG	0	0	0	65	66	0	0	89
HE 240 A					66	0	0	89	103	0	0	90
HE 240 A	105	131	QP Solai	PolG	103	0	0	90	182	0	0	66
HE 240 A					66	0	0	21	66	0	0	28
HE 240 A					66	0	0	28	103	0	0	29
HE 240 A	105	131	Neve	PolG	103	0	0	29	182	0	0	21
HE 240 A					0	0	0	23	66	0	0	30
HE 240 A	105	131	Neve	PolG	66	0	0	30	182	0	0	19
HE 240 A					0	0	0	18	103	0	0	30
HE 240 A	105	131	Neve	PolG	103	0	0	30	182	0	0	22

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
HE 240 A	105	131	Vento X	PolG	0	0	0	35	66	0	0	46
HE 240 A	105	131	Vento X	PolG	66	0	0	46	182	0	0	29
HE 240 A	105	131	Carichi termici	Termico	103	0	0	46	182	0	0	34
HE 240 A	131	132	Peso Proprio	UnitG	AXY=15°C, AXZ=15°C	0	0	60	178	0	0	60
HE 240 A	131	132	QP Solai	PolG	0	0	0	68	57	0	0	89
HE 240 A	131	132	QP Solai	PolG	57	0	0	89	107	0	0	90
HE 240 A	131	132	QP Solai	PolG	107	0	0	90	178	0	0	68
HE 240 A	131	132	QP Solai	PolG	0	0	0	22	57	0	0	28
HE 240 A	131	132	QP Solai	PolG	57	0	0	28	107	0	0	29
HE 240 A	131	132	QP Solai	PolG	107	0	0	29	178	0	0	22
HE 240 A	131	132	Neve	PolG	0	0	0	24	57	0	0	31
HE 240 A	131	132	Neve	PolG	57	0	0	31	178	0	0	19
HE 240 A	131	132	Neve	PolG	0	0	0	18	107	0	0	30
HE 240 A	131	132	Neve	PolG	107	0	0	30	178	0	0	24
HE 240 A	131	132	Vento X	PolG	0	0	0	28	107	0	0	47
HE 240 A	131	132	Vento X	PolG	107	0	0	47	178	0	0	37
HE 240 A	131	132	Vento X	PolG	0	0	0	37	57	0	0	47
HE 240 A	131	132	Vento X	PolG	57	0	0	47	178	0	0	29
HE 240 A	131	132	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	170	0	0	60
HE 240 A	132	133	Peso Proprio	UnitG	0	0	0	70	47	0	0	89
HE 240 A	132	133	QP Solai	PolG	47	0	0	89	108	0	0	90
HE 240 A	132	133	QP Solai	PolG	108	0	0	90	170	0	0	70
HE 240 A	132	133	QP Solai	PolG	0	0	0	23	47	0	0	28
HE 240 A	132	133	QP Solai	PolG	47	0	0	28	108	0	0	29
HE 240 A	132	133	QP Solai	PolG	108	0	0	29	170	0	0	23
HE 240 A	132	133	Neve	PolG	0	0	0	26	47	0	0	31
HE 240 A	132	133	Neve	PolG	47	0	0	31	170	0	0	19
HE 240 A	132	133	Neve	PolG	0	0	0	18	108	0	0	31
HE 240 A	132	133	Neve	PolG	108	0	0	31	170	0	0	25
HE 240 A	132	133	Vento X	PolG	0	0	0	28	108	0	0	48
HE 240 A	132	133	Vento X	PolG	108	0	0	48	170	0	0	39
HE 240 A	132	133	Vento X	PolG	0	0	0	40	47	0	0	48
HE 240 A	132	133	Vento X	PolG	47	0	0	48	170	0	0	29
HE 240 A	132	133	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	159	0	0	60
HE 240 A	133	134	Peso Proprio	UnitG	0	0	0	73	38	0	0	81
HE 240 A	133	134	QP Solai	PolG	38	0	0	88	107	0	0	91
HE 240 A	133	134	QP Solai	PolG	107	0	0	91	159	0	0	73
HE 240 A	133	134	QP Solai	PolG	0	0	0	23	38	0	0	28
HE 240 A	133	134	QP Solai	PolG	38	0	0	28	107	0	0	29
HE 240 A	133	134	Neve	PolG	107	0	0	29	159	0	0	23
HE 240 A	133	134	Neve	PolG	0	0	0	18	107	0	0	32
HE 240 A	133	134	Neve	PolG	107	0	0	32	159	0	0	26
HE 240 A	133	134	Neve	PolG	0	0	0	27	38	0	0	32
HE 240 A	133	134	Neve	PolG	38	0	0	32	159	0	0	19
HE 240 A	133	134	Vento X	PolG	107	0	0	49	159	0	0	49
HE 240 A	133	134	Vento X	PolG	0	0	0	49	159	0	0	41
HE 240 A	133	134	Vento X	PolG	107	0	0	42	38	0	0	49
HE 240 A	133	134	Vento X	PolG	38	0	0	49	159	0	0	29
HE 240 A	133	134	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	148	0	0	60
HE 240 A	134	135	Peso Proprio	UnitG	0	0	0	75	29	0	0	88
HE 240 A	134	135	QP Solai	PolG	29	0	0	88	105	0	0	91
HE 240 A	134	135	QP Solai	PolG	105	0	0	91	148	0	0	75
HE 240 A	134	135	QP Solai	PolG	0	0	0	24	29	0	0	28
HE 240 A	134	135	QP Solai	PolG	29	0	0	28	105	0	0	29
HE 240 A	134	135	Neve	PolG	105	0	0	29	148	0	0	24
HE 240 A	134	135	Neve	PolG	0	0	0	29	29	0	0	33
HE 240 A	134	135	Neve	PolG	29	0	0	33	148	0	0	19
HE 240 A	134	135	Neve	PolG	0	0	0	18	105	0	0	33
HE 240 A	134	135	Neve	PolG	105	0	0	33	148	0	0	28
HE 240 A	134	135	Vento X	PolG	0	0	0	44	29	0	0	50
HE 240 A	134	135	Vento X	PolG	29	0	0	50	148	0	0	29

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf	
HE 240 A	134	135	Vento X	PolG	0	0	0	0	28	105	0	0	43
HE 240 A	134	135	Vento X	PolG	105	0	0	0	51	148	0	0	51
HE 240 A	135	225	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	60	134	0	0	60
HE 240 A	135	225	Peso Proprio	UnitG	0	0	0	0	77	21	0	0	88
HE 240 A	135	225	QP Solai	PolG	21	0	0	0	88	100	0	0	91
HE 240 A	135	225	QP Solai	PolG	100	0	0	0	91	134	0	0	77
HE 240 A	135	225	QP Solai	PolG	0	0	0	0	25	21	0	0	28
HE 240 A	135	225	QP Solai	PolG	21	0	0	0	28	100	0	0	29
HE 240 A	135	225	QP Solai	PolG	100	0	0	0	29	134	0	0	25
HE 240 A	135	225	Neve	PolG	0	0	0	0	18	100	0	0	34
HE 240 A	135	225	Neve	PolG	100	0	0	0	34	134	0	0	29
HE 240 A	135	225	Neve	PolG	0	0	0	0	30	21	0	0	33
HE 240 A	135	225	Vento X	PolG	21	0	0	0	33	134	0	0	19
HE 240 A	135	225	Vento X	PolG	0	0	0	0	28	100	0	0	52
HE 240 A	135	225	Vento X	PolG	100	0	0	0	52	134	0	0	45
HE 240 A	135	225	Vento X	PolG	0	0	0	0	47	21	0	0	52
HE 240 A	135	225	Vento X	PolG	21	0	0	0	52	134	0	0	29
HE 240 A	225	225	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	60	123	0	0	60
HE 240 A	225	226	Peso Proprio	UnitG	0	0	0	0	80	14	0	0	88
HE 240 A	225	226	QP Solai	PolG	14	0	0	0	88	96	0	0	91
HE 240 A	225	226	QP Solai	PolG	96	0	0	0	91	123	0	0	79
HE 240 A	225	226	QP Solai	PolG	0	0	0	0	26	14	0	0	28
HE 240 A	225	226	QP Solai	PolG	14	0	0	0	28	96	0	0	29
HE 240 A	225	226	QP Solai	PolG	96	0	0	0	29	123	0	0	25
HE 240 A	225	226	Neve	PolG	0	0	0	0	32	14	0	0	34
HE 240 A	225	226	Neve	PolG	14	0	0	0	34	123	0	0	19
HE 240 A	225	226	Neve	PolG	0	0	0	0	18	96	0	0	34
HE 240 A	225	226	Vento X	PolG	96	0	0	0	34	123	0	0	31
HE 240 A	225	226	Vento X	PolG	0	0	0	0	49	14	0	0	53
HE 240 A	225	226	Vento X	PolG	14	0	0	0	53	123	0	0	29
HE 240 A	225	226	Vento X	PolG	0	0	0	0	28	96	0	0	53
HE 240 A	225	226	Vento X	PolG	96	0	0	0	53	123	0	0	47
HE 240 A	225	226	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	60	113	0	0	60
HE 240 A	226	325	Peso Proprio	UnitG	0	0	0	0	82	9	0	0	87
HE 240 A	226	325	QP Solai	PolG	9	0	0	0	87	93	0	0	92
HE 240 A	226	325	QP Solai	PolG	93	0	0	0	92	113	0	0	82
HE 240 A	226	325	QP Solai	PolG	0	0	0	0	26	9	0	0	28
HE 240 A	226	325	QP Solai	PolG	9	0	0	0	28	93	0	0	29
HE 240 A	226	325	QP Solai	PolG	93	0	0	0	29	113	0	0	26
HE 240 A	226	325	Neve	PolG	0	0	0	0	18	93	0	0	35
HE 240 A	226	325	Neve	PolG	93	0	0	0	35	113	0	0	32
HE 240 A	226	325	Neve	PolG	0	0	0	0	33	9	0	0	35
HE 240 A	226	325	Neve	PolG	9	0	0	0	35	113	0	0	19
HE 240 A	226	325	Vento X	PolG	0	0	0	0	51	9	0	0	54
HE 240 A	226	325	Vento X	PolG	9	0	0	0	54	113	0	0	29
HE 240 A	226	325	Vento X	PolG	0	0	0	0	28	93	0	0	54
HE 240 A	226	325	Vento X	PolG	93	0	0	0	54	113	0	0	50
HE 240 A	226	325	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	60	108	0	0	60
HE 240 A	325	326	Peso Proprio	UnitG	0	0	0	0	85	4	0	0	87
HE 240 A	325	326	QP Solai	PolG	4	0	0	0	87	92	0	0	92
HE 240 A	325	326	QP Solai	PolG	92	0	0	0	92	108	0	0	84
HE 240 A	325	326	QP Solai	PolG	0	0	0	0	27	4	0	0	28
HE 240 A	325	326	QP Solai	PolG	4	0	0	0	28	92	0	0	29
HE 240 A	325	326	QP Solai	PolG	92	0	0	0	29	108	0	0	27
HE 240 A	325	326	Neve	PolG	0	0	0	0	18	92	0	0	36
HE 240 A	325	326	Neve	PolG	92	0	0	0	36	108	0	0	34
HE 240 A	325	326	Neve	PolG	0	0	0	0	35	4	0	0	35
HE 240 A	325	326	Vento X	PolG	4	0	0	0	35	108	0	0	19
HE 240 A	325	326	Vento X	PolG	0	0	0	0	28	92	0	0	56
HE 240 A	325	326	Vento X	PolG	92	0	0	0	56	108	0	0	52
HE 240 A	325	326	Vento X	PolG	0	0	0	0	54	4	0	0	55
HE 240 A	325	326	Vento X	PolG	4	0	0	0	55	108	0	0	29

Sezione	Ni	Nf	Cond.	Tip. c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	326	326	Cartechi termici Peso Proprio	UnitG	0	0	0	60	112	0	0	60
	326	315		PolG	0	0	0	87	100	0	0	92
	326	315		QV Solai	100	0	0	92	112	0	0	86
HE 240 A	326	315	QV Solai	PolG	0	0	0	28	100	0	0	30
HE 240 A	326	315	Neve	PolG	100	0	0	36	112	0	0	28
HE 240 A	326	315	Neve	PolG	0	0	0	18	100	0	0	37
HE 240 A	326	315	Vento X	PolG	100	0	0	37	112	0	0	35
HE 240 A	326	315	Vento X	PolG	0	0	0	28	100	0	0	57
HE 240 A	326	315	Vento X	PolG	100	0	0	57	112	0	0	54
HE 240 A	326	315	Cartechi termici	Termico	0	0	0	56	112	0	0	29
Trave 8005												
HE 240 A	106	141	Peso Proprio	UnitG	0	0	0	60	182	0	0	60
HE 240 A	106	141	QV Solai	PolG	0	0	0	62	76	0	0	93
					76	0	0	93	89	0	0	94
HE 240 A	106	141	QV Solai	PolG	89	0	0	94	182	0	0	63
					0	0	0	20	76	0	0	30
HE 240 A	106	141	Neve	PolG	0	0	0	30	89	0	0	30
					76	0	0	30	182	0	0	20
HE 240 A	106	141	Neve	PolG	89	0	0	22	76	0	0	30
					0	0	0	30	182	0	0	17
HE 240 A	106	141	Vento X	PolG	76	0	0	16	89	0	0	30
					0	0	0	30	182	0	0	22
HE 240 A	106	141	Vento X	PolG	89	0	0	35	76	0	0	47
					76	0	0	47	182	0	0	26
HE 240 A	106	141	Vento X	PolG	0	0	0	25	89	0	0	46
					89	0	0	46	182	0	0	35
Trave 8006												
HE 240 A	106	141	Cartechi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	141	142	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	141	142	QV Solai	PolG	0	0	0	64	68	0	0	93
					68	0	0	93	93	0	0	94
HE 240 A	141	142	QV Solai	PolG	93	0	0	94	178	0	0	65
					0	0	0	21	68	0	0	30
HE 240 A	141	142	Neve	PolG	68	0	0	30	93	0	0	30
					93	0	0	30	178	0	0	21
HE 240 A	141	142	Neve	PolG	0	0	0	24	68	0	0	31
					68	0	0	31	178	0	0	17
HE 240 A	141	142	Neve	PolG	0	0	0	16	93	0	0	31
					93	0	0	31	178	0	0	24
HE 240 A	141	142	Vento X	PolG	0	0	0	25	93	0	0	47
					93	0	0	47	178	0	0	37
HE 240 A	141	142	Vento X	PolG	0	0	0	37	68	0	0	48
					68	0	0	48	178	0	0	26
Trave 8007												
HE 240 A	141	142	Cartechi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	142	143	Peso Proprio	UnitG	0	0	0	60	170	0	0	60
HE 240 A	142	143	QV Solai	PolG	0	0	0	67	59	0	0	93
					59	0	0	93	95	0	0	94
HE 240 A	142	143	QV Solai	PolG	95	0	0	94	170	0	0	67
					0	0	0	21	59	0	0	30
HE 240 A	142	143	Neve	PolG	59	0	0	30	95	0	0	30
					95	0	0	30	170	0	0	22
HE 240 A	142	143	Neve	PolG	0	0	0	26	59	0	0	32
					59	0	0	32	170	0	0	17
HE 240 A	142	143	Neve	PolG	0	0	0	16	95	0	0	32
					95	0	0	32	170	0	0	25
HE 240 A	142	143	Vento X	PolG	0	0	0	39	59	0	0	49
					59	0	0	49	170	0	0	26
HE 240 A	142	143	Vento X	PolG	0	0	0	25	95	0	0	49
					95	0	0	49	170	0	0	39
Trave 8008												
HE 240 A	142	143	Cartechi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	143	144	Peso Proprio	UnitG	0	0	0	60	158	0	0	60
HE 240 A	143	144	QV Solai	PolG	0	0	0	69	50	0	0	92
					50	0	0	92	94	0	0	94
					94	0	0	94	158	0	0	69

Sezione	Ni	NF	Cond	Tipo c.	Xi	QXi	QYi	QZi	Xi	QXi	QYi	QZi
HE 240 A	143	144	QV Solai	PolG	0	0	0	22	50	0	0	30
					50	0	0	30	94	0	0	30
					94	0	0	30	158	0	0	22
HE 240 A	143	144	Neve	PolG	0	0	0	16	94	0	0	33
					94	0	0	33	158	0	0	27
HE 240 A	143	144	Neve	PolG	0	0	0	27	50	0	0	33
					50	0	0	33	158	0	0	17
HE 240 A	143	144	Vento X	PolG	0	0	0	25	94	0	0	50
					94	0	0	50	158	0	0	41
HE 240 A	143	144	Vento X	PolG	0	0	0	42	50	0	0	51
					50	0	0	51	158	0	0	26
HE 240 A	143	144	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$							
HE 240 A	144	145	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	144	145	QP Solai	PolG	0	0	0	72	41	0	0	92
					41	0	0	92	93	0	0	95
HE 240 A	144	145			93	0	0	95	148	0	0	77
HE 240 A	144	145	QV Solai	PolG	0	0	0	23	41	0	0	30
					41	0	0	30	93	0	0	30
HE 240 A	144	145			93	0	0	30	148	0	0	23
HE 240 A	144	145	Neve	PolG	0	0	0	29	41	0	0	34
					41	0	0	34	148	0	0	17
HE 240 A	144	145	Neve	PolG	0	0	0	16	93	0	0	33
					93	0	0	33	148	0	0	28
HE 240 A	144	145	Vento X	PolG	0	0	0	44	41	0	0	52
					41	0	0	52	148	0	0	26
HE 240 A	144	145	Vento X	PolG	0	0	0	25	93	0	0	52
					93	0	0	52	148	0	0	43
HE 240 A	145	229	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$							
HE 240 A	145	229	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	145	229	QP Solai	PolG	0	0	0	74	33	0	0	92
					33	0	0	92	89	0	0	95
HE 240 A	145	229			89	0	0	95	134	0	0	74
HE 240 A	145	229	QV Solai	PolG	0	0	0	24	33	0	0	30
					33	0	0	30	89	0	0	30
HE 240 A	145	229			89	0	0	30	134	0	0	24
HE 240 A	145	229	Neve	PolG	0	0	0	30	33	0	0	34
					33	0	0	34	134	0	0	17
HE 240 A	145	229	Neve	PolG	0	0	0	16	89	0	0	34
					89	0	0	34	134	0	0	29
HE 240 A	145	229	Vento X	PolG	0	0	0	25	89	0	0	53
					89	0	0	53	134	0	0	46
HE 240 A	145	229	Vento X	PolG	0	0	0	46	33	0	0	53
					33	0	0	53	134	0	0	26
HE 240 A	145	229	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$							
HE 240 A	229	230	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	229	230	QP Solai	PolG	0	0	0	76	26	0	0	92
					26	0	0	92	85	0	0	95
HE 240 A	229	230			85	0	0	95	123	0	0	76
HE 240 A	229	230	QV Solai	PolG	0	0	0	25	26	0	0	29
					26	0	0	29	85	0	0	30
HE 240 A	229	230			85	0	0	30	123	0	0	24
HE 240 A	229	230	Neve	PolG	0	0	0	16	85	0	0	35
					85	0	0	35	123	0	0	31
HE 240 A	229	230	Neve	PolG	0	0	0	32	26	0	0	35
					26	0	0	35	123	0	0	17
HE 240 A	229	230	Vento X	PolG	0	0	0	25	85	0	0	55
					85	0	0	55	123	0	0	48
HE 240 A	229	230	Vento X	PolG	0	0	0	48	26	0	0	55
					26	0	0	55	123	0	0	26
HE 240 A	229	230	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$							
HE 240 A	229	230	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	230	329	QP Solai	PolG	0	0	0	79	20	0	0	92
					20	0	0	92	82	0	0	95
HE 240 A	230	329			82	0	0	95	113	0	0	78
					0	0	0	25	20	0	0	29
HE 240 A	230	329	QV Solai	PolG	20	0	0	29	82	0	0	31

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	OYf	QZf
HE 240 A	230	329	Neve	PolG	82	0	0	31	113	0	0	25
HE 240 A	230	329	Neve	PolG	82	0	0	16	82	0	0	36
HE 240 A	230	329	Neve	PolG	82	0	0	36	113	0	0	32
HE 240 A	230	329	Neve	PolG	82	0	0	33	20	0	0	36
HE 240 A	230	329	Vento X	PolG	20	0	0	36	113	0	0	17
HE 240 A	230	329	Vento X	PolG	82	0	0	25	82	0	0	56
HE 240 A	230	329	Vento X	PolG	82	0	0	56	113	0	0	50
HE 240 A	230	329	Vento X	PolG	20	0	0	51	20	0	0	56
HE 240 A	230	329	Carichi termici	Termico	20	0	0	56	113	0	0	26
HE 240 A	329	330	Peso Proprio	UnitG	AXY=15°C, AXZ=15°C	0	0	60	108	0	0	60
HE 240 A	329	330	QP Solai	PolG	0	0	0	81	15	0	0	92
HE 240 A	329	330	QP Solai	PolG	15	0	0	92	82	0	0	96
HE 240 A	329	330	QP Solai	PolG	82	0	0	96	108	0	0	81
HE 240 A	329	330	QP Solai	PolG	0	0	0	26	15	0	0	29
HE 240 A	329	330	QP Solai	PolG	15	0	0	29	82	0	0	31
HE 240 A	329	330	QP Solai	PolG	82	0	0	31	108	0	0	26
HE 240 A	329	330	QP Solai	PolG	0	0	0	35	15	0	0	37
HE 240 A	329	330	QP Solai	PolG	15	0	0	37	108	0	0	17
HE 240 A	329	330	QP Solai	PolG	0	0	0	16	82	0	0	37
HE 240 A	329	330	QP Solai	PolG	82	0	0	37	108	0	0	34
HE 240 A	329	330	QP Solai	PolG	0	0	0	53	15	0	0	57
HE 240 A	329	330	QP Solai	PolG	15	0	0	57	108	0	0	26
HE 240 A	329	330	QP Solai	PolG	0	0	0	25	82	0	0	58
HE 240 A	329	330	QP Solai	PolG	82	0	0	58	108	0	0	52
HE 240 A	330	316	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	112	0	0	60
HE 240 A	330	316	Peso Proprio	UnitG	0	0	0	84	12	0	0	92
HE 240 A	330	316	Peso Proprio	PolG	12	0	0	92	89	0	0	96
HE 240 A	330	316	Peso Proprio	PolG	89	0	0	96	112	0	0	83
HE 240 A	330	316	Peso Proprio	PolG	0	0	0	27	12	0	0	29
HE 240 A	330	316	Peso Proprio	PolG	12	0	0	29	89	0	0	31
HE 240 A	330	316	Peso Proprio	PolG	89	0	0	31	112	0	0	27
HE 240 A	330	316	Peso Proprio	PolG	0	0	0	16	89	0	0	38
HE 240 A	330	316	Peso Proprio	PolG	89	0	0	38	112	0	0	35
HE 240 A	330	316	Peso Proprio	PolG	0	0	0	36	12	0	0	38
HE 240 A	330	316	Peso Proprio	PolG	12	0	0	38	112	0	0	17
HE 240 A	330	316	Peso Proprio	PolG	0	0	0	25	89	0	0	59
HE 240 A	330	316	Peso Proprio	PolG	89	0	0	59	112	0	0	54
HE 240 A	330	316	Peso Proprio	PolG	0	0	0	56	12	0	0	59
HE 240 A	330	316	Peso Proprio	PolG	12	0	0	59	112	0	0	26
HE 240 A	330	316	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	182	0	0	60
HE 240 A	107	161	Peso Proprio	UnitG	0	0	0	58	77	0	0	95
HE 240 A	107	161	Peso Proprio	PolG	77	0	0	95	90	0	0	60
HE 240 A	107	161	Peso Proprio	PolG	90	0	0	95	182	0	0	60
HE 240 A	107	161	Peso Proprio	PolG	0	0	0	19	77	0	0	30
HE 240 A	107	161	Peso Proprio	PolG	77	0	0	30	90	0	0	30
HE 240 A	107	161	Peso Proprio	PolG	90	0	0	30	182	0	0	19
HE 240 A	107	161	Peso Proprio	PolG	0	0	0	22	90	0	0	30
HE 240 A	107	161	Peso Proprio	PolG	90	0	0	30	182	0	0	15
HE 240 A	107	161	Peso Proprio	PolG	0	0	0	14	77	0	0	30
HE 240 A	107	161	Peso Proprio	PolG	77	0	0	30	182	0	0	22
HE 240 A	107	161	Peso Proprio	PolG	90	0	0	35	90	0	0	47
HE 240 A	107	161	Peso Proprio	PolG	0	0	0	47	182	0	0	22
HE 240 A	107	161	Peso Proprio	PolG	90	0	0	22	77	0	0	46
HE 240 A	107	161	Peso Proprio	PolG	77	0	0	46	182	0	0	35
HE 240 A	107	161	Peso Proprio	UnitG	AXY=15°C, AXZ=15°C	0	0	60	178	0	0	60
HE 240 A	161	162	Peso Proprio	UnitG	0	0	0	61	80	0	0	100
HE 240 A	161	162	Peso Proprio	PolG	80	0	0	100	82	0	0	100
HE 240 A	161	162	Peso Proprio	PolG	80	0	0	100	178	0	0	62
HE 240 A	161	162	Peso Proprio	PolG	82	0	0	20	80	0	0	32
HE 240 A	161	162	Peso Proprio	PolG	80	0	0	32	82	0	0	32
HE 240 A	161	162	Peso Proprio	PolG	82	0	0	32	178	0	0	20

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	161	162	Neve	PolG	80	0	0	14	80	0	0	31
HE 240 A	161	162	Neve	PolG	80	0	0	31	178	0	0	24
HE 240 A	161	162	Neve	PolG	82	0	0	24	82	0	0	31
HE 240 A	161	162	Vento X	PolG	82	0	0	31	178	0	0	15
HE 240 A	161	162	Vento X	PolG	82	0	0	37	82	0	0	48
HE 240 A	161	162	Vento X	PolG	82	0	0	48	178	0	0	22
HE 240 A	161	162	Vento X	PolG	80	0	0	22	80	0	0	48
HE 240 A	161	162	Vento X	PolG	80	0	0	48	178	0	0	37
HE 240 A	161	162	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	162	163	Peso Proprio	UnitG	0	0	0	60	170	0	0	60
HE 240 A	162	163	QP Solai	PolG	0	0	0	63	73	0	0	100
HE 240 A	162	163	QP Solai	PolG	73	0	0	100	81	0	0	101
HE 240 A	162	163	QP Solai	PolG	81	0	0	101	170	0	0	64
HE 240 A	162	163	QP Solai	PolG	0	0	0	20	73	0	0	32
HE 240 A	162	163	QP Solai	PolG	73	0	0	32	81	0	0	32
HE 240 A	162	163	QP Solai	PolG	81	0	0	32	170	0	0	21
HE 240 A	162	163	Neve	PolG	0	0	0	14	81	0	0	32
HE 240 A	162	163	Neve	PolG	81	0	0	32	170	0	0	25
HE 240 A	162	163	Neve	PolG	0	0	0	25	73	0	0	32
HE 240 A	162	163	Neve	PolG	73	0	0	32	170	0	0	15
HE 240 A	162	163	Vento X	PolG	0	0	0	39	73	0	0	50
HE 240 A	162	163	Vento X	PolG	73	0	0	50	170	0	0	22
HE 240 A	162	163	Vento X	PolG	0	0	0	22	81	0	0	49
HE 240 A	162	163	Vento X	PolG	81	0	0	49	170	0	0	39
HE 240 A	162	163	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	163	164	Peso Proprio	UnitG	0	0	0	60	158	0	0	60
HE 240 A	163	164	Peso Proprio	PolG	0	0	0	66	63	0	0	100
HE 240 A	163	164	Peso Proprio	PolG	63	0	0	100	80	0	0	101
HE 240 A	163	164	Peso Proprio	PolG	80	0	0	101	158	0	0	66
HE 240 A	163	164	Peso Proprio	PolG	0	0	0	21	63	0	0	32
HE 240 A	163	164	Peso Proprio	PolG	63	0	0	32	80	0	0	32
HE 240 A	163	164	Peso Proprio	PolG	80	0	0	32	158	0	0	21
HE 240 A	163	164	Peso Proprio	PolG	0	0	0	14	80	0	0	33
HE 240 A	163	164	Peso Proprio	PolG	80	0	0	33	158	0	0	27
HE 240 A	163	164	Peso Proprio	PolG	0	0	0	27	63	0	0	33
HE 240 A	163	164	Peso Proprio	PolG	63	0	0	33	158	0	0	15
HE 240 A	163	164	Peso Proprio	PolG	0	0	0	22	80	0	0	51
HE 240 A	163	164	Peso Proprio	PolG	80	0	0	51	158	0	0	41
HE 240 A	163	164	Peso Proprio	PolG	0	0	0	42	63	0	0	51
HE 240 A	163	164	Peso Proprio	PolG	63	0	0	51	158	0	0	22
HE 240 A	163	164	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	164	165	Peso Proprio	UnitG	0	0	0	60	148	0	0	60
HE 240 A	164	165	Peso Proprio	PolG	0	0	0	68	54	0	0	99
HE 240 A	164	165	Peso Proprio	PolG	54	0	0	99	79	0	0	101
HE 240 A	164	165	Peso Proprio	PolG	79	0	0	101	148	0	0	69
HE 240 A	164	165	Peso Proprio	PolG	0	0	0	22	54	0	0	32
HE 240 A	164	165	Peso Proprio	PolG	54	0	0	32	79	0	0	32
HE 240 A	164	165	Peso Proprio	PolG	79	0	0	32	148	0	0	22
HE 240 A	164	165	Peso Proprio	PolG	0	0	0	14	79	0	0	34
HE 240 A	164	165	Peso Proprio	PolG	79	0	0	34	148	0	0	28
HE 240 A	164	165	Peso Proprio	PolG	0	0	0	28	54	0	0	34
HE 240 A	164	165	Peso Proprio	PolG	54	0	0	34	148	0	0	15
HE 240 A	164	165	Peso Proprio	PolG	0	0	0	44	54	0	0	53
HE 240 A	164	165	Peso Proprio	PolG	54	0	0	53	148	0	0	22
HE 240 A	164	165	Peso Proprio	PolG	0	0	0	22	79	0	0	53
HE 240 A	164	165	Peso Proprio	PolG	79	0	0	53	148	0	0	43
HE 240 A	164	165	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	165	237	Peso Proprio	UnitG	0	0	0	60	134	0	0	60
HE 240 A	165	237	Peso Proprio	PolG	0	0	0	71	44	0	0	99
HE 240 A	165	237	Peso Proprio	PolG	44	0	0	99	76	0	0	101
HE 240 A	165	237	Peso Proprio	PolG	76	0	0	101	134	0	0	71
HE 240 A	165	237	Peso Proprio	PolG	0	0	0	23	44	0	0	32
HE 240 A	165	237	Peso Proprio	PolG	44	0	0	32	76	0	0	32
HE 240 A	165	237	Peso Proprio	PolG	76	0	0	32	134	0	0	23
HE 240 A	165	237	Peso Proprio	PolG	0	0	0	30	44	0	0	35
HE 240 A	165	237	Peso Proprio	PolG	44	0	0	35	134	0	0	15

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
HE 240 A	165	237	Neve	PolG	0	0	0	14	76	0	0	35
HE 240 A	165	237	Vento X	PolG	76	0	0	35	134	0	0	30
HE 240 A	165	237	Vento X	PolG	76	0	0	22	76	0	0	54
HE 240 A	165	237	Vento X	PolG	76	0	0	46	44	0	0	54
HE 240 A	165	237	Carichi termici	Termico	44	0	0	54	134	0	0	22
HE 240 A	237	238	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	237	238	QP Solai	PolG	0	0	0	73	36	0	0	98
HE 240 A	237	238	QV Solai	PolG	36	0	0	98	73	0	0	102
HE 240 A	237	238	Neve	PolG	73	0	0	102	123	0	0	73
HE 240 A	237	238	Neve	PolG	36	0	0	32	73	0	0	33
HE 240 A	237	238	Neve	PolG	73	0	0	33	123	0	0	23
HE 240 A	237	238	Neve	PolG	73	0	0	14	73	0	0	36
HE 240 A	237	238	Vento X	PolG	36	0	0	36	123	0	0	31
HE 240 A	237	238	Vento X	PolG	36	0	0	22	73	0	0	56
HE 240 A	237	238	Vento X	PolG	73	0	0	56	123	0	0	48
HE 240 A	237	238	Vento X	PolG	36	0	0	49	36	0	0	56
HE 240 A	237	238	Carichi termici	Termico	36	0	0	56	123	0	0	22
HE 240 A	238	337	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	238	337	QP Solai	PolG	0	0	0	76	30	0	0	98
HE 240 A	238	337	QV Solai	PolG	30	0	0	98	70	0	0	102
HE 240 A	238	337	Neve	PolG	70	0	0	102	113	0	0	75
HE 240 A	238	337	Neve	PolG	30	0	0	31	70	0	0	31
HE 240 A	238	337	Neve	PolG	30	0	0	33	113	0	0	24
HE 240 A	238	337	Neve	PolG	30	0	0	33	30	0	0	37
HE 240 A	238	337	Neve	PolG	30	0	0	14	70	0	0	37
HE 240 A	238	337	Vento X	PolG	70	0	0	37	113	0	0	32
HE 240 A	238	337	Vento X	PolG	30	0	0	51	30	0	0	58
HE 240 A	238	337	Vento X	PolG	30	0	0	58	113	0	0	27
HE 240 A	238	337	Vento X	PolG	70	0	0	22	70	0	0	57
HE 240 A	238	337	Carichi termici	Termico	70	0	0	57	113	0	0	50
HE 240 A	337	338	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
HE 240 A	337	338	QP Solai	PolG	0	0	0	78	25	0	0	98
HE 240 A	337	338	QV Solai	PolG	25	0	0	98	70	0	0	102
HE 240 A	337	338	Neve	PolG	70	0	0	102	108	0	0	78
HE 240 A	337	338	Neve	PolG	25	0	0	25	25	0	0	31
HE 240 A	337	338	Neve	PolG	70	0	0	33	108	0	0	25
HE 240 A	337	338	Neve	PolG	25	0	0	34	25	0	0	38
HE 240 A	337	338	Neve	PolG	25	0	0	38	108	0	0	15
HE 240 A	337	338	Vento X	PolG	70	0	0	38	108	0	0	34
HE 240 A	337	338	Vento X	PolG	25	0	0	53	25	0	0	59
HE 240 A	337	338	Vento X	PolG	25	0	0	59	108	0	0	22
HE 240 A	337	338	Vento X	PolG	70	0	0	22	70	0	0	59
HE 240 A	337	338	Carichi termici	Termico	70	0	0	59	108	0	0	52
HE 240 A	338	317	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
HE 240 A	338	317	QP Solai	PolG	0	0	0	80	22	0	0	97
HE 240 A	338	317	QV Solai	PolG	22	0	0	97	76	0	0	102
HE 240 A	338	317	Neve	PolG	76	0	0	102	112	0	0	80
HE 240 A	338	317	Neve	PolG	22	0	0	26	22	0	0	31
HE 240 A	338	317	Neve	PolG	76	0	0	33	76	0	0	33
HE 240 A	338	317	Neve	PolG	76	0	0	33	112	0	0	26
HE 240 A	338	317	Neve	PolG	0	0	0	14	76	0	0	39
HE 240 A	338	317	Neve	PolG	76	0	0	39	112	0	0	35
HE 240 A	338	317	Neve	PolG	0	0	0	36	22	0	0	39
HE 240 A	338	317	Vento X	PolG	22	0	0	39	112	0	0	15

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
HE 240 A	338	317	Vento X	PolG	0	0	0	56	22	0	0	61
HE 240 A	338	317	Vento X	PolG	22	0	0	61	112	0	0	22
HE 240 A	338	317	Carichi termici	Termico	76	0	0	61	112	0	0	54
HE 240 A	338	317	Carichi termici	Termico	76	0	0	61	112	0	0	54
HE 240 A	108	166	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	108	166	QP Solai	PolG	0	0	0	56	67	0	0	92
HE 240 A	108	166	QV Solai	PolG	67	0	0	92	102	0	0	93
HE 240 A	108	166	Neve	PolG	102	0	0	93	182	0	0	57
HE 240 A	108	166	Neve	PolG	67	0	0	18	67	0	0	29
HE 240 A	108	166	Neve	PolG	67	0	0	29	102	0	0	30
HE 240 A	108	166	Neve	PolG	102	0	0	30	182	0	0	18
HE 240 A	108	166	Vento X	PolG	0	0	0	12	67	0	0	29
HE 240 A	108	166	Vento X	PolG	67	0	0	29	182	0	0	23
HE 240 A	108	166	Vento X	PolG	67	0	0	22	102	0	0	30
HE 240 A	108	166	Vento X	PolG	102	0	0	30	182	0	0	13
HE 240 A	108	166	Vento X	PolG	0	0	0	34	102	0	0	47
HE 240 A	108	166	Vento X	PolG	102	0	0	47	182	0	0	19
HE 240 A	108	166	Vento X	PolG	0	0	0	19	67	0	0	46
HE 240 A	108	166	Carichi termici	Termico	67	0	0	46	182	0	0	35
HE 240 A	166	167	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	166	167	QP Solai	PolG	0	0	0	58	70	0	0	96
HE 240 A	166	167	QV Solai	PolG	70	0	0	96	95	0	0	97
HE 240 A	166	167	Neve	PolG	95	0	0	97	178	0	0	59
HE 240 A	166	167	Neve	PolG	0	0	0	19	70	0	0	31
HE 240 A	166	167	Neve	PolG	70	0	0	31	95	0	0	31
HE 240 A	166	167	Neve	PolG	95	0	0	24	95	0	0	19
HE 240 A	166	167	Neve	PolG	95	0	0	31	178	0	0	13
HE 240 A	166	167	Vento X	PolG	0	0	0	31	178	0	0	31
HE 240 A	166	167	Vento X	PolG	70	0	0	37	95	0	0	48
HE 240 A	166	167	Vento X	PolG	95	0	0	48	178	0	0	19
HE 240 A	166	167	Vento X	PolG	0	0	0	19	70	0	0	47
HE 240 A	166	167	Carichi termici	Termico	70	0	0	47	178	0	0	37
HE 240 A	167	168	Peso Proprio	UnifG	0	0	0	60	170	0	0	60
HE 240 A	167	168	QP Solai	PolG	0	0	0	60	71	0	0	101
HE 240 A	167	168	QV Solai	PolG	71	0	0	101	86	0	0	102
HE 240 A	167	168	Neve	PolG	86	0	0	102	170	0	0	61
HE 240 A	167	168	Neve	PolG	0	0	0	19	71	0	0	32
HE 240 A	167	168	Neve	PolG	71	0	0	32	86	0	0	33
HE 240 A	167	168	Neve	PolG	86	0	0	33	170	0	0	20
HE 240 A	167	168	Neve	PolG	86	0	0	25	86	0	0	32
HE 240 A	167	168	Neve	PolG	86	0	0	32	170	0	0	13
HE 240 A	167	168	Vento X	PolG	0	0	0	12	71	0	0	32
HE 240 A	167	168	Vento X	PolG	71	0	0	32	170	0	0	25
HE 240 A	167	168	Vento X	PolG	0	0	0	39	86	0	0	50
HE 240 A	167	168	Vento X	PolG	86	0	0	50	170	0	0	19
HE 240 A	167	168	Vento X	PolG	0	0	0	19	71	0	0	49
HE 240 A	167	168	Carichi termici	Termico	71	0	0	49	170	0	0	39
HE 240 A	168	169	Peso Proprio	UnifG	0	0	0	60	158	0	0	60
HE 240 A	168	169	QP Solai	PolG	0	0	0	63	71	0	0	106
HE 240 A	168	169	QV Solai	PolG	71	0	0	106	76	0	0	106
HE 240 A	168	169	Neve	PolG	76	0	0	106	158	0	0	64
HE 240 A	168	169	Neve	PolG	0	0	0	20	71	0	0	34
HE 240 A	168	169	Neve	PolG	71	0	0	34	76	0	0	34
HE 240 A	168	169	Neve	PolG	76	0	0	34	158	0	0	20
HE 240 A	168	169	Neve	PolG	76	0	0	27	76	0	0	33
HE 240 A	168	169	Neve	PolG	76	0	0	33	158	0	0	13
HE 240 A	168	169	Neve	PolG	0	0	0	12	71	0	0	33
HE 240 A	168	169	Vento X	PolG	71	0	0	33	158	0	0	27
HE 240 A	168	169	Vento X	PolG	0	0	0	41	76	0	0	52

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
HE 240 A	168	169	Vento X	PolG	76	0	0	52	158	0	0	19
HE 240 A	168	169	Carichi termici	Termico	71	0	0	51	158	0	0	42
HE 240 A	169	170	Peso Proprio	UnifG	AXY=15°C, AXZ=15°C							
HE 240 A	169	170	QP Solai	PolG	0	0	0	60	148	0	0	60
HE 240 A	169	170	QV Solai	PolG	67	0	0	65	67	0	0	109
HE 240 A	169	170	QV Solai	PolG	70	0	0	109	148	0	0	66
HE 240 A	169	170	QV Solai	PolG	67	0	0	21	67	0	0	35
HE 240 A	169	170	QV Solai	PolG	67	0	0	35	148	0	0	21
HE 240 A	169	170	QV Solai	PolG	70	0	0	35	148	0	0	21
HE 240 A	169	170	QV Solai	PolG	70	0	0	28	67	0	0	35
HE 240 A	169	170	QV Solai	PolG	67	0	0	35	148	0	0	13
HE 240 A	169	170	QV Solai	PolG	67	0	0	12	70	0	0	34
HE 240 A	169	170	QV Solai	PolG	70	0	0	34	148	0	0	28
HE 240 A	169	170	QV Solai	PolG	67	0	0	44	67	0	0	53
HE 240 A	169	170	QV Solai	PolG	67	0	0	53	148	0	0	19
HE 240 A	169	170	QV Solai	PolG	70	0	0	19	70	0	0	53
HE 240 A	169	170	QV Solai	PolG	70	0	0	53	148	0	0	44
HE 240 A	169	170	QV Solai	PolG	AXY=15°C, AXZ=15°C							
HE 240 A	169	170	QV Solai	PolG	0	0	0	60	134	0	0	60
HE 240 A	169	170	QV Solai	PolG	0	0	0	68	57	0	0	109
HE 240 A	169	170	QV Solai	PolG	57	0	0	109	67	0	0	109
HE 240 A	169	170	QV Solai	PolG	67	0	0	109	134	0	0	68
HE 240 A	169	170	QV Solai	PolG	67	0	0	22	57	0	0	35
HE 240 A	169	170	QV Solai	PolG	57	0	0	35	67	0	0	35
HE 240 A	169	170	QV Solai	PolG	67	0	0	35	134	0	0	22
HE 240 A	169	170	QV Solai	PolG	67	0	0	30	57	0	0	36
HE 240 A	169	170	QV Solai	PolG	57	0	0	36	134	0	0	13
HE 240 A	169	170	QV Solai	PolG	67	0	0	12	67	0	0	35
HE 240 A	169	170	QV Solai	PolG	67	0	0	35	134	0	0	30
HE 240 A	169	170	QV Solai	PolG	67	0	0	19	67	0	0	54
HE 240 A	169	170	QV Solai	PolG	67	0	0	54	134	0	0	46
HE 240 A	169	170	QV Solai	PolG	67	0	0	46	57	0	0	55
HE 240 A	169	170	QV Solai	PolG	57	0	0	55	134	0	0	19
HE 240 A	169	170	QV Solai	PolG	AXY=15°C, AXZ=15°C							
HE 240 A	169	170	QV Solai	PolG	0	0	0	60	123	0	0	60
HE 240 A	169	170	QV Solai	PolG	0	0	0	70	49	0	0	108
HE 240 A	169	170	QV Solai	PolG	49	0	0	108	64	0	0	109
HE 240 A	169	170	QV Solai	PolG	64	0	0	109	123	0	0	70
HE 240 A	169	170	QV Solai	PolG	0	0	0	22	49	0	0	35
HE 240 A	169	170	QV Solai	PolG	49	0	0	35	64	0	0	35
HE 240 A	169	170	QV Solai	PolG	64	0	0	35	123	0	0	23
HE 240 A	169	170	QV Solai	PolG	0	0	0	31	49	0	0	37
HE 240 A	169	170	QV Solai	PolG	49	0	0	37	123	0	0	13
HE 240 A	169	170	QV Solai	PolG	0	0	0	12	64	0	0	36
HE 240 A	169	170	QV Solai	PolG	64	0	0	36	123	0	0	31
HE 240 A	169	170	QV Solai	PolG	0	0	0	48	49	0	0	57
HE 240 A	169	170	QV Solai	PolG	49	0	0	57	123	0	0	19
HE 240 A	169	170	QV Solai	PolG	0	0	0	19	64	0	0	56
HE 240 A	169	170	QV Solai	PolG	64	0	0	56	123	0	0	48
HE 240 A	169	170	QV Solai	PolG	AXY=15°C, AXZ=15°C							
HE 240 A	169	170	QV Solai	PolG	0	0	0	60	113	0	0	60
HE 240 A	169	170	QV Solai	PolG	0	0	0	72	42	0	0	108
HE 240 A	169	170	QV Solai	PolG	42	0	0	108	62	0	0	110
HE 240 A	169	170	QV Solai	PolG	62	0	0	110	113	0	0	73
HE 240 A	169	170	QV Solai	PolG	0	0	0	23	42	0	0	35
HE 240 A	169	170	QV Solai	PolG	42	0	0	35	62	0	0	35
HE 240 A	169	170	QV Solai	PolG	62	0	0	35	113	0	0	23
HE 240 A	169	170	QV Solai	PolG	0	0	0	12	62	0	0	38
HE 240 A	169	170	QV Solai	PolG	62	0	0	38	113	0	0	33
HE 240 A	169	170	QV Solai	PolG	0	0	0	33	42	0	0	38
HE 240 A	169	170	QV Solai	PolG	42	0	0	38	113	0	0	13
HE 240 A	169	170	QV Solai	PolG	0	0	0	19	62	0	0	58
HE 240 A	169	170	QV Solai	PolG	62	0	0	58	113	0	0	50
HE 240 A	169	170	QV Solai	PolG	0	0	0	51	42	0	0	59

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf										
HE 240 A	240	339	Carichi termici Peso Proprio QP Solai	Termico UnifG PolG	0	0	0	0	60	108	0	0	60									
	339	340												0	0	75	37	0	0	108		
	339	340																			0	110
HE 240 A	339	340	QV Solai	PolG	0	0	0	24	37	0	0	34										
HE 240 A	339	340											37	0	0	34	62	0	0	35		
HE 240 A	339	340																			62	0
HE 240 A	339	340	Neve	PolG	0	0	0	12	62	0	0	39										
HE 240 A	339	340											Neve	PolG	0	0	34	37	0	0		
HE 240 A	339	340																			Vento X	PolG
HE 240 A	339	340	Vento X	PolG	0	0	60	108	0	0	19											
HE 240 A	339	340										Vento X	PolG	0	0	19	62	0	0	60		
HE 240 A	339	340																			Vento X	PolG
HE 240 A	339	340	Carichi termici Peso Proprio QP Solai	Termico UnifG PolG	0	0	0	60	112	0	0											
HE 240 A	340	318										0	0	0	77	35	0	0	107			
HE 240 A	340	318																		35	0	0
HE 240 A	340	318	QV Solai	PolG	0	0	25	35	0	0	34											
HE 240 A	340	318										35	0	0	34	67	0	0	35			
HE 240 A	340	318																		67	0	0
HE 240 A	340	318	Neve	PolG	0	0	36	35	0	0	40											
HE 240 A	340	318										Neve	PolG	0	0	40	112	0	0			
HE 240 A	340	318																		Vento X	PolG	0
HE 240 A	340	318	Vento X	PolG	0	0	40	112	0	0	35											
HE 240 A	340	318										Vento X	PolG	0	0	19	67	0	0			
HE 240 A	340	318																		Vento X	PolG	0
HE 240 A	340	318	Vento X	PolG	0	0	55	35	0	0	62											
HE 240 A	340	318										Vento X	PolG	0	0	62	112	0	0			
HE 240 A	340	318																		Carichi termici	Termico	0
HE 240 A	109	121	Peso Proprio QP Solai	UnifG PolG	0	0	0	60	182	0	0											
HE 240 A	109	121										58	0	0	53	58	0	0	88			
HE 240 A	109	121	112	0	0	90	182	0	0	54												
HE 240 A	109	121									QV Solai	PolG	0	0	17	58	0	0	28			
HE 240 A	109	121	58	0	0	28	112	0	0	29												
HE 240 A	109	121																		112	0	0
HE 240 A	109	121									Neve	PolG	0	0	22	112	0	0	30			
HE 240 A	109	121	Neve	PolG	0	0	30	182	0	0												
HE 240 A	109	121																		Vento X	PolG	0
HE 240 A	109	121									Vento X	PolG	0	0	29	182	0	0	23			
HE 240 A	109	121	Vento X	PolG	0	0	16	58	0	0												
HE 240 A	109	121																		Vento X	PolG	0
HE 240 A	109	121									Vento X	PolG	0	0	34	112	0	0	46			
HE 240 A	109	121	Vento X	PolG	0	0	46	182	0	0												
HE 240 A	109	121																		Carichi termici	Termico	0
HE 240 A	121	122									Peso Proprio QP Solai	UnifG PolG	0	0	0	55	60	0	0			
HE 240 A	121	122	60	0	0	93	105	0	0	95												
HE 240 A	121	122									QV Solai	PolG	0	0	95	178	0	0	56			
HE 240 A	121	122	0	0	18	60	0	0	30													
HE 240 A	121	122								0										0	30	105
HE 240 A	121	122									Neve	PolG	0	0	30	178	0	0	18			
HE 240 A	121	122	Neve	PolG	0	0	24	105	0													
HE 240 A	121	122								Neve										PolG	0	0
HE 240 A	121	122									Vento X	PolG	0	0	11	60	0	0	30			
HE 240 A	121	122	Vento X	PolG	0	0	30	178	0													
HE 240 A	121	122								Vento X										PolG	0	0
HE 240 A	121	122									Vento X	PolG	0	0	46	178	0	0	37			
HE 240 A	121	122	Vento X	PolG	0	0	37	105	0													
HE 240 A	121	122								Vento X										PolG	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYL	QZi	Xf	QXf	OYf	QZf
HE 240 A	121	122	Carichi termici	Termico	0	0	0	0	60	170	0	60
HE 240 A	122	123	Peso Proprio	UnifG	0	0	0	0	58	61	0	98
HE 240 A	122	123	QP Solai	PolG	61	0	0	0	98	96	0	99
					96	0	0	0	99	170	0	58
HE 240 A	122	123	QV Solai	PolG	0	0	0	0	18	61	0	31
					61	0	0	0	31	96	0	32
					96	0	0	0	32	170	0	19
HE 240 A	122	123	Neve	PolG	0	0	0	0	11	61	0	31
					61	0	0	0	31	170	0	25
HE 240 A	122	123	Neve	PolG	0	0	0	0	25	96	0	32
					96	0	0	0	32	170	0	11
HE 240 A	122	123	Vento X	PolG	0	0	0	0	16	61	0	48
					61	0	0	0	48	170	0	39
HE 240 A	122	123	Vento X	PolG	0	0	0	0	39	96	0	50
					96	0	0	0	50	170	0	17
HE 240 A	122	123	Carichi termici	Termico	0	0	0	0	60	159	0	60
HE 240 A	123	124	Peso Proprio	UnifG	0	0	0	0	60	60	0	103
HE 240 A	123	124	QP Solai	PolG	60	0	0	0	103	86	0	104
					86	0	0	0	104	159	0	61
HE 240 A	123	124	QV Solai	PolG	0	0	0	0	19	60	0	33
					60	0	0	0	33	86	0	33
					86	0	0	0	33	159	0	19
HE 240 A	123	124	Neve	PolG	0	0	0	0	11	60	0	33
					60	0	0	0	33	159	0	27
HE 240 A	123	124	Neve	PolG	0	0	0	0	27	86	0	33
					86	0	0	0	33	159	0	11
HE 240 A	123	124	Vento X	PolG	0	0	0	0	16	60	0	50
					60	0	0	0	50	159	0	42
HE 240 A	123	124	Vento X	PolG	0	0	0	0	41	86	0	52
					86	0	0	0	52	159	0	17
HE 240 A	123	124	Carichi termici	Termico	0	0	0	0	60	148	0	60
HE 240 A	124	125	Peso Proprio	UnifG	0	0	0	0	62	59	0	108
HE 240 A	124	125	QP Solai	PolG	59	0	0	0	108	76	0	108
					76	0	0	0	108	148	0	63
HE 240 A	124	125	QV Solai	PolG	0	0	0	0	20	59	0	35
					59	0	0	0	35	76	0	35
					76	0	0	0	35	148	0	20
HE 240 A	124	125	Neve	PolG	0	0	0	0	28	76	0	35
					76	0	0	0	35	148	0	11
HE 240 A	124	125	Neve	PolG	0	0	0	0	11	59	0	34
					59	0	0	0	34	148	0	28
HE 240 A	124	125	Vento X	PolG	0	0	0	0	44	76	0	54
					76	0	0	0	54	148	0	17
HE 240 A	124	125	Vento X	PolG	0	0	0	0	16	59	0	52
					59	0	0	0	52	148	0	44
HE 240 A	124	125	Carichi termici	Termico	0	0	0	0	60	134	0	60
HE 240 A	125	126	Peso Proprio	UnifG	0	0	0	0	65	56	0	113
HE 240 A	125	126	QP Solai	PolG	56	0	0	0	113	66	0	113
					66	0	0	0	113	134	0	65
HE 240 A	125	126	QV Solai	PolG	0	0	0	0	21	56	0	36
					56	0	0	0	36	66	0	36
					66	0	0	0	36	134	0	21
HE 240 A	125	126	Neve	PolG	0	0	0	0	30	66	0	36
					66	0	0	0	36	134	0	11
HE 240 A	125	126	Neve	PolG	0	0	0	0	11	56	0	35
					56	0	0	0	35	134	0	30
HE 240 A	125	126	Vento X	PolG	0	0	0	0	46	66	0	55
					66	0	0	0	55	134	0	17
HE 240 A	125	126	Vento X	PolG	0	0	0	0	16	56	0	54
					56	0	0	0	54	134	0	46
HE 240 A	125	126	Carichi termici	Termico	0	0	0	0	60	123	0	60
HE 240 A	125	126	Peso Proprio	UnifG	0	0	0	0	60	123	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	OYf	QZf
HE 240 A	221	222	QP Solai	PolG	0	0	0	0	67	54	0	117
					54	0	0	0	117	57	0	117
HE 240 A	221	222	QV Solai	PolG	0	0	0	0	22	54	0	38
					54	0	0	0	38	57	0	38
HE 240 A	221	222	Neve	PolG	0	0	0	0	38	123	0	22
					57	0	0	0	31	57	0	37
HE 240 A	221	222	Neve	PolG	0	0	0	0	37	123	0	11
					54	0	0	0	11	54	0	36
HE 240 A	221	222	Vento X	PolG	0	0	0	0	16	54	0	56
					54	0	0	0	56	123	0	48
HE 240 A	221	222	Vento X	PolG	0	0	0	0	48	57	0	57
					57	0	0	0	57	123	0	17
HE 240 A	221	222	Carichi termici	Termico	0	0	0	0	60	113	0	60
HE 240 A	222	321	Peso Proprio	UnifG	0	0	0	0	70	50	0	120
HE 240 A	222	321	QP Solai	PolG	50	0	0	0	120	52	0	120
					52	0	0	0	120	113	0	70
HE 240 A	222	321	QV Solai	PolG	0	0	0	0	22	50	0	38
					50	0	0	0	38	52	0	39
HE 240 A	222	321	Neve	PolG	0	0	0	0	39	113	0	22
					52	0	0	0	33	50	0	38
HE 240 A	222	321	Neve	PolG	0	0	0	0	38	113	0	11
					52	0	0	0	38	113	0	33
HE 240 A	222	321	Vento X	PolG	0	0	0	0	51	50	0	59
					50	0	0	0	59	113	0	17
HE 240 A	222	321	Vento X	PolG	0	0	0	0	16	52	0	58
					52	0	0	0	58	113	0	50
HE 240 A	222	321	Carichi termici	Termico	0	0	0	0	60	108	0	60
HE 240 A	321	322	Peso Proprio	UnifG	0	0	0	0	72	45	0	120
HE 240 A	321	322	QP Solai	PolG	45	0	0	0	120	52	0	121
					52	0	0	0	121	108	0	72
HE 240 A	321	322	QV Solai	PolG	0	0	0	0	23	45	0	38
					45	0	0	0	38	52	0	39
HE 240 A	321	322	Neve	PolG	0	0	0	0	39	108	0	23
					52	0	0	0	11	52	0	39
HE 240 A	321	322	Neve	PolG	0	0	0	0	39	108	0	34
					52	0	0	0	34	45	0	39
HE 240 A	321	322	Vento X	PolG	0	0	0	0	39	108	0	11
					45	0	0	0	16	52	0	60
HE 240 A	321	322	Vento X	PolG	0	0	0	0	60	108	0	53
					52	0	0	0	53	45	0	61
HE 240 A	321	322	Carichi termici	Termico	0	0	0	0	61	108	0	17
HE 240 A	322	319	Peso Proprio	UnifG	0	0	0	0	75	44	0	119
HE 240 A	322	319	QP Solai	PolG	44	0	0	0	119	56	0	121
					56	0	0	0	121	112	0	74
HE 240 A	322	319	QV Solai	PolG	0	0	0	0	24	44	0	38
					44	0	0	0	38	56	0	39
HE 240 A	322	319	Neve	PolG	0	0	0	0	39	112	0	24
					56	0	0	0	40	112	0	35
HE 240 A	322	319	Neve	PolG	0	0	0	0	36	44	0	41
					44	0	0	0	41	112	0	11
HE 240 A	322	319	Vento X	PolG	0	0	0	0	16	56	0	62
					56	0	0	0	62	112	0	55
HE 240 A	322	319	Vento X	PolG	0	0	0	0	55	44	0	63
					44	0	0	0	63	112	0	17
HE 240 A	322	319	Carichi termici	Termico	0	0	0	0	60	182	0	60
HE 240 A	110	126	Peso Proprio	UnifG	0	0	0	0	60	182	0	60
HE 240 A	110	126	QP Solai	PolG	0	0	0	0	35	121	0	47

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf
HE 240 A	110	126	QV Solai	PolG	121	0	0	47	182	0	0	15
HE 240 A	110	126	Neve	PolG	121	0	0	15	182	0	0	5
HE 240 A	110	126	Vento X	PolG	121	0	0	29	182	0	0	9
HE 240 A	110	126		PolG	121	0	0	34	121	0	0	45
HE 240 A	110	126	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
	126	127	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
	126	127	QP Solai	PolG	115	0	0	49	178	0	0	15
HE 240 A	126	127	QV Solai	PolG	0	0	0	12	115	0	0	16
HE 240 A	126	127	Neve	PolG	115	0	0	24	115	0	0	30
HE 240 A	126	127	Vento X	PolG	115	0	0	30	178	0	0	9
HE 240 A	126	127		PolG	115	0	0	36	115	0	0	47
HE 240 A	126	127	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
	127	128	Peso Proprio	UnitG	0	0	0	60	170	0	0	60
	127	128	QP Solai	PolG	106	0	0	51	170	0	0	15
HE 240 A	127	128	QV Solai	PolG	0	0	0	13	106	0	0	16
HE 240 A	127	128	Neve	PolG	106	0	0	25	106	0	0	32
HE 240 A	127	128	Vento X	PolG	106	0	0	32	170	0	0	9
HE 240 A	127	128		PolG	106	0	0	39	106	0	0	49
HE 240 A	127	128	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
	128	129	Peso Proprio	UnitG	0	0	0	60	158	0	0	60
	128	129	QP Solai	PolG	96	0	0	43	96	0	0	53
HE 240 A	128	129	QV Solai	PolG	0	0	0	14	96	0	0	17
HE 240 A	128	129	Neve	PolG	96	0	0	17	158	0	0	5
HE 240 A	128	129	Vento X	PolG	96	0	0	33	158	0	0	9
HE 240 A	128	129		PolG	96	0	0	41	96	0	0	51
HE 240 A	128	129	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
	129	130	Peso Proprio	UnitG	0	0	0	60	148	0	0	60
	129	130	QP Solai	PolG	87	0	0	45	87	0	0	55
HE 240 A	129	130	QV Solai	PolG	0	0	0	55	148	0	0	15
HE 240 A	129	130	Neve	PolG	87	0	0	14	87	0	0	18
HE 240 A	129	130	Vento X	PolG	87	0	0	18	148	0	0	5
HE 240 A	129	130	Neve	PolG	87	0	0	28	87	0	0	34
HE 240 A	129	130	Vento X	PolG	87	0	0	34	148	0	0	9
HE 240 A	129	130		PolG	87	0	0	43	87	0	0	53
HE 240 A	129	130	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
	130	223	Peso Proprio	UnitG	0	0	0	60	134	0	0	60
	130	223	QP Solai	PolG	0	0	0	47	76	0	0	15
HE 240 A	130	223	QV Solai	PolG	76	0	0	57	134	0	0	15
HE 240 A	130	223	Neve	PolG	0	0	0	15	76	0	0	18
HE 240 A	130	223	Vento X	PolG	76	0	0	30	76	0	0	36
HE 240 A	130	223		PolG	76	0	0	46	76	0	0	55
HE 240 A	130	223	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
	223	224	Peso Proprio	UnitG	0	0	0	60	123	0	0	60
	223	224	QP Solai	PolG	0	0	0	59	67	0	0	59
HE 240 A	223	224	QV Solai	PolG	67	0	0	59	123	0	0	15
HE 240 A	223	224	Neve	PolG	67	0	0	16	67	0	0	19
HE 240 A	223	224	Vento X	PolG	67	0	0	19	123	0	0	5
HE 240 A	223	224	Neve	PolG	0	0	0	31	67	0	0	37
HE 240 A	223	224	Vento X	PolG	67	0	0	37	123	0	0	9
HE 240 A	223	224		PolG	0	0	0	48	67	0	0	57

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	OXf	OYf	OZf		
HE 240 A	223	224	Carichi termici Peso Proprio	Termico UnitG	67	0	0	0	60	113	0	0	60	
	224	323			AXY=15°C,AXZ=15°C	0	0	0	52	60	0	0	61	
	224	323	QV Solai	PolG	60	0	0	0	61	113	0	15		
	224	323	QV Solai	PolG	0	0	0	0	17	60	0	20		
	224	323	Neve	PolG	60	0	0	0	20	113	0	5		
	224	323	Neve	PolG	0	0	0	0	32	60	0	38		
	224	323	Vento X	PolG	60	0	0	0	38	113	0	9		
	224	323	Vento X	PolG	0	0	0	0	50	60	0	59		
	224	323	Carichi termici Peso Proprio	Termico UnitG	60	0	0	0	59	113	0	14		
	323	324	AXY=15°C,AXZ=15°C		0	0	0	60	108	0	0	60		
HE 240 A	323	324	QV Solai	PolG	0	0	0	0	55	55	0	0	63	
	323	324	QV Solai	PolG	55	0	0	0	63	108	0	0	15	
	323	324	QV Solai	PolG	0	0	0	0	18	55	0	0	20	
	323	324	Neve	PolG	55	0	0	0	20	108	0	0	5	
	323	324	Neve	PolG	0	0	0	0	34	55	0	0	39	
	323	324	Vento X	PolG	55	0	0	0	39	108	0	0	9	
	323	324	Vento X	PolG	0	0	0	0	53	55	0	0	61	
	323	324	Carichi termici Peso Proprio	Termico UnitG	55	0	0	0	61	108	0	0	14	
	324	320	AXY=15°C,AXZ=15°C		0	0	0	57	55	0	0	65		
	HE 240 A	324	320	QV Solai	PolG	55	0	0	0	65	112	0	0	15
324		320	QV Solai	PolG	0	0	0	0	18	55	0	0	21	
324		320	QV Solai	PolG	55	0	0	0	21	112	0	0	5	
324		320	Neve	PolG	0	0	0	0	35	55	0	0	41	
324		320	Neve	PolG	55	0	0	0	41	112	0	0	9	
324		320	Vento X	PolG	0	0	0	0	55	55	0	0	63	
324		320	Vento X	PolG	55	0	0	0	63	112	0	0	14	
324		320	Carichi termici	Termico UnitG	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	0	8	
324		320	AXY=15°C,AXZ=15°C		0	0	0	8	89	0	0	8		
HE 240 A		324	320	Carichi termici	Termico UnitG	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	0	8
	324	320	AXY=15°C,AXZ=15°C	0		0	0	8	89	0	0	8		
	324	320	Carichi termici	Termico UnitG	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	0	8	
	324	320	AXY=15°C,AXZ=15°C		0	0	0	8	150	0	0	8		
	324	320	Carichi termici	Termico UnitG	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	0	8	
	324	320	AXY=15°C,AXZ=15°C		0	0	0	8	89	0	0	8		
	324	320	Carichi termici	Termico UnitG	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	0	8	
	324	320	AXY=15°C,AXZ=15°C		0	0	0	8	149	0	0	8		
	324	320	Carichi termici	Termico UnitG	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	0	8	
	324	320	AXY=15°C,AXZ=15°C		0	0	0	8	89	0	0	8		
Fondazione 9007	29	27	Carichi termici	Termico UnitG	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	0	8	
	29	27	AXY=15°C,AXZ=15°C		0	0	0	8	89	0	0	8		
	1	2	Peso Proprio	UnitG	AXY=15°C,AXZ=15°C	0	0	0	1500	149	0	0	1500	
	2	3	Peso Proprio		UnitG	0	0	0	1500	150	0	0	1500	
	3	4	Peso Proprio	UnitG	AXY=15°C,AXZ=15°C	0	0	0	1500	89	0	0	1500	
	4	5	Peso Proprio		UnitG	0	0	0	1500	89	0	0	1500	
	5	6	Peso Proprio	UnitG	AXY=15°C,AXZ=15°C	0	0	0	1500	89	0	0	1500	
	6	7	Peso Proprio		UnitG	0	0	0	1500	88	0	0	1500	
	7	8	Peso Proprio	UnitG	AXY=15°C,AXZ=15°C	0	0	0	1500	89	0	0	1500	
	8	9	Peso Proprio		UnitG	0	0	0	1500	90	0	0	1500	
9	10	Peso Proprio	UnitG	AXY=15°C,AXZ=15°C	0	0	0	1500	89	0	0	1500		
10	11	Peso Proprio		UnitG	0	0	0	1500	89	0	0	1500		
Fondazione 9008	211	212	Peso Proprio	UnitG	AXY=15°C,AXZ=15°C	0	0	0	1500	149	0	0	1500	
	212	213	Peso Proprio		UnitG	0	0	0	1500	149	0	0	1500	
	213	214	Peso Proprio		UnitG	AXY=15°C,AXZ=15°C	0	0	0	1500	149	0	0	1500
	214	215	Peso Proprio			UnitG	0	0	0	1500	149	0	0	1500

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	OZi	Xf	OXf	OYf	OZf
F60x100	214	215	Peso Proprio	UnitG	0	0	0	1500	149	0	0	1500
F60x100	215	216	Peso Proprio	UnitG	0	0	0	1500	149	0	0	1500
F60x100	216	217	Peso Proprio	UnitG	0	0	0	1500	150	0	0	1500
F60x100	217	218	Peso Proprio	UnitG	0	0	0	1500	149	0	0	1500
F60x100	218	219	Peso Proprio	UnitG	0	0	0	1500	150	0	0	1500
F60x100	219	220	Peso Proprio	UnitG	0	0	0	1500	149	0	0	1500
Generica 7001												
Fi16	1	24	Peso Proprio	UnitG	0	0	0	0	2	252	0	0
Fi16	1	24	Carichi termici	Termico	AXY=15°C, AXZ=15°C							2
Generica 7002												
Fi16	24	101	Peso Proprio	UnitG	0	0	0	0	2	252	0	0
Fi16	24	101	Carichi termici	Termico	AXY=15°C, AXZ=15°C							2
Generica 7003												
Fi14	101	157	Peso Proprio	UnitG	0	0	0	0	1	389	0	0
Fi14	101	157	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7004												
Fi14	157	154	Peso Proprio	UnitG	0	0	0	0	1	360	0	0
Fi14	157	154	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7005												
Fi14	154	235	Peso Proprio	UnitG	0	0	0	0	1	319	0	0
Fi14	154	235	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7006												
Fi14	235	333	Peso Proprio	UnitG	0	0	0	0	1	278	0	0
Fi14	235	333	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7007												
Fi14	333	312	Peso Proprio	UnitG	0	0	0	0	1	264	0	0
Fi14	333	312	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7008												
Fi14	311	335	Peso Proprio	UnitG	0	0	0	0	1	264	0	0
Fi14	311	335	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7009												
Fi14	335	233	Peso Proprio	UnitG	0	0	0	0	1	279	0	0
Fi14	335	233	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7010												
Fi14	233	159	Peso Proprio	UnitG	0	0	0	0	1	319	0	0
Fi14	233	159	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7011												
Fi14	159	152	Peso Proprio	UnitG	0	0	0	0	1	361	0	0
Fi14	159	152	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7012												
Fi14	152	102	Peso Proprio	UnitG	0	0	0	0	1	389	0	0
Fi14	152	102	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7013												
Fi16	102	28	Peso Proprio	UnitG	0	0	0	0	2	252	0	0
Fi16	102	28	Carichi termici	Termico	AXY=15°C, AXZ=15°C							2
Generica 7014												
Fi16	28	2	Peso Proprio	UnitG	0	0	0	0	2	252	0	0
Fi16	28	2	Carichi termici	Termico	AXY=15°C, AXZ=15°C							2
Generica 7015												
Fi14	102	137	Peso Proprio	UnitG	0	0	0	0	1	389	0	0
Fi14	102	137	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7016												
Fi14	137	104	Peso Proprio	UnitG	0	0	0	0	1	372	0	0
Fi14	137	104	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7017												
Fi14	104	132	Peso Proprio	UnitG	0	0	0	0	1	371	0	0
Fi14	104	132	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7018												
Fi14	132	106	Peso Proprio	UnitG	0	0	0	0	1	371	0	0
Fi14	132	106	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7019												
Fi14	106	162	Peso Proprio	UnitG	0	0	0	0	1	372	0	0
Fi14	106	162	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7020												
Fi14	162	108	Peso Proprio	UnitG	0	0	0	0	1	372	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	OZi	Xf	OXf	OYf	OZf
Fi14	162	108	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
Generica 7021												
Fi14	108	122	Peso Proprio	UnitG	0	0	0	0	1	372	0	0
Fi14	108	122	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7022												
Fi14	122	110	Peso Proprio	UnitG	0	0	0	0	1	371	0	0
Fi14	122	110	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7023												
Fi16	110	22	Peso Proprio	UnitG	0	0	0	0	2	218	0	0
Fi16	110	22	Carichi termici	Termico	AXY=15°C, AXZ=15°C							2
Generica 7024												
Fi16	22	10	Peso Proprio	UnitG	0	0	0	0	2	222	0	0
Fi16	22	10	Carichi termici	Termico	AXY=15°C, AXZ=15°C							2
Generica 7025												
Fi16	9	30	Peso Proprio	UnitG	0	0	0	0	2	222	0	0
Fi16	9	30	Carichi termici	Termico	AXY=15°C, AXZ=15°C							2
Generica 7026												
Fi16	30	109	Peso Proprio	UnitG	0	0	0	0	2	218	0	0
Fi16	30	109	Carichi termici	Termico	AXY=15°C, AXZ=15°C							2
Generica 7027												
Fi14	109	127	Peso Proprio	UnitG	0	0	0	0	1	372	0	0
Fi14	109	127	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7028												
Fi14	127	124	Peso Proprio	UnitG	0	0	0	0	1	344	0	0
Fi14	127	124	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7029												
Fi14	124	223	Peso Proprio	UnitG	0	0	0	0	1	304	0	0
Fi14	124	223	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7030												
Fi14	223	321	Peso Proprio	UnitG	0	0	0	0	1	269	0	0
Fi14	223	321	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7031												
Fi14	321	320	Peso Proprio	UnitG	0	0	0	0	1	260	0	0
Fi14	321	320	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7032												
Fi14	319	323	Peso Proprio	UnitG	0	0	0	0	1	261	0	0
Fi14	319	323	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7033												
Fi14	323	221	Peso Proprio	UnitG	0	0	0	0	1	269	0	0
Fi14	323	221	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7034												
Fi14	221	129	Peso Proprio	UnitG	0	0	0	0	1	306	0	0
Fi14	221	129	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7035												
Fi14	129	122	Peso Proprio	UnitG	0	0	0	0	1	344	0	0
Fi14	129	122	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7036												
Fi14	109	167	Peso Proprio	UnitG	0	0	0	0	1	371	0	0
Fi14	109	167	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7037												
Fi14	167	107	Peso Proprio	UnitG	0	0	0	0	1	371	0	0
Fi14	167	107	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7038												
Fi14	107	142	Peso Proprio	UnitG	0	0	0	0	1	371	0	0
Fi14	107	142	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7039												
Fi14	142	105	Peso Proprio	UnitG	0	0	0	0	1	372	0	0
Fi14	142	105	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7040												
Fi14	105	147	Peso Proprio	UnitG	0	0	0	0	1	372	0	0
Fi14	105	147	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7041												
Fi14	147	103	Peso Proprio	UnitG	0	0	0	0	1	369	0	0
Fi14	147	103	Carichi termici	Termico	AXY=15°C, AXZ=15°C							1
Generica 7042												

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	OZi	Xf	OXf	OYf	OZf
Fi14	103	157	Peso Proprio	UnifG	0	0	0	0	1	387	0	0
Fi14	103	157	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7043												
Fi14	312	327	Peso Proprio	UnifG	0	0	0	0	1	264	0	0
Fi14	312	327	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7044												
Fi14	327	314	Peso Proprio	UnifG	0	0	0	0	1	260	0	0
Fi14	327	314	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7045												
Fi14	314	325	Peso Proprio	UnifG	0	0	0	0	1	261	0	0
Fi14	314	325	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7046												
Fi14	325	316	Peso Proprio	UnifG	0	0	0	0	1	260	0	0
Fi14	325	316	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7047												
Fi14	316	337	Peso Proprio	UnifG	0	0	0	0	1	260	0	0
Fi14	316	337	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7048												
Fi14	337	318	Peso Proprio	UnifG	0	0	0	0	1	260	0	0
Fi14	337	318	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7049												
Fi14	318	321	Peso Proprio	UnifG	0	0	0	0	1	261	0	0
Fi14	318	321	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7050												
Fi14	319	339	Peso Proprio	UnifG	0	0	0	0	1	261	0	0
Fi14	319	339	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7051												
Fi14	339	317	Peso Proprio	UnifG	0	0	0	0	1	260	0	0
Fi14	339	317	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7052												
Fi14	317	329	Peso Proprio	UnifG	0	0	0	0	1	261	0	0
Fi14	317	329	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7053												
Fi14	329	315	Peso Proprio	UnifG	0	0	0	0	1	261	0	0
Fi14	329	315	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7054												
Fi14	315	331	Peso Proprio	UnifG	0	0	0	0	1	260	0	0
Fi14	315	331	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7055												
Fi14	331	313	Peso Proprio	UnifG	0	0	0	0	1	261	0	0
Fi14	331	313	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7056												
Fi14	313	335	Peso Proprio	UnifG	0	0	0	0	1	264	0	0
Fi14	313	335	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7057												
Fi14	132	144	Peso Proprio	UnifG	0	0	0	0	1	346	0	0
Fi14	132	144	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7058												
Fi14	144	225	Peso Proprio	UnifG	0	0	0	0	1	305	0	0
Fi14	144	225	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7059												
Fi14	225	329	Peso Proprio	UnifG	0	0	0	0	1	269	0	0
Fi14	225	329	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7060												
Fi14	325	229	Peso Proprio	UnifG	0	0	0	0	1	268	0	0
Fi14	325	229	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7061												
Fi14	229	134	Peso Proprio	UnifG	0	0	0	0	1	306	0	0
Fi14	229	134	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7062												
Fi14	134	142	Peso Proprio	UnifG	0	0	0	0	1	345	0	0
Fi14	134	142	Carichi termici	Termico	AXY=15°C,AXZ=15°C							1
Generica 7063												
Fi16	106	21	Peso Proprio	UnifG	0	0	0	0	2	222	0	0
Fi16	106	21	Carichi termici	Termico	AXY=15°C,AXZ=15°C							2

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	OZi	Xf	OXf	OYf	OZf
Generica 7064												
Fi16	21	6	Peso Proprio	UnifG	0	0	0	0	2	222	0	0
Fi16	21	6	Carichi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7065												
Fi16	5	26	Peso Proprio	UnifG	0	0	0	0	2	222	0	0
Fi16	5	26	Carichi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7066												
Fi16	26	105	Peso Proprio	UnifG	0	0	0	0	2	222	0	0
Fi16	26	105	Carichi termici	Termico	AXY=15°C,AXZ=15°C							2

Dati solai

Solaio n°	Nodi								Tipo
1	102-156-151-101								Vetro strutturale
1	103-136-156-102								Vetro strutturale
1	104-146-136-103								Vetro strutturale
1	105-131-146-104								Vetro strutturale
1	106-141-131-105								Vetro strutturale
1	107-161-141-106								Vetro strutturale
1	108-166-161-107								Vetro strutturale
1	109-121-166-108								Vetro strutturale
1	110-126-121-109								Vetro strutturale
1	121-122-167-166								Vetro strutturale
1	122-123-168-167								Vetro strutturale
1	123-124-169-168								Vetro strutturale
1	124-125-170-169								Vetro strutturale
1	169-170-165-164								Vetro strutturale
1	168-169-164-163								Vetro strutturale
1	167-168-163-162								Vetro strutturale
1	166-167-162-161								Vetro strutturale
1	164-165-145-144								Vetro strutturale
1	126-127-122-121								Vetro strutturale
1	127-128-123-122								Vetro strutturale
1	128-129-124-123								Vetro strutturale
1	129-130-125-124								Vetro strutturale
1	163-164-144-143								Vetro strutturale
1	162-163-143-142								Vetro strutturale
1	161-162-142-141								Vetro strutturale
1	159-160-155-154								Vetro strutturale
1	158-159-154-153								Vetro strutturale
1	131-132-147-146								Vetro strutturale
1	132-133-148-147								Vetro strutturale
1	133-134-149-148								Vetro strutturale
1	134-135-150-149								Vetro strutturale
1	157-158-153-152								Vetro strutturale
1	156-157-152-151								Vetro strutturale
1	149-150-140-139								Vetro strutturale
1	148-149-139-138								Vetro strutturale
1	147-148-138-137								Vetro strutturale
1	136-137-157-156								Vetro strutturale
1	137-138-158-157								Vetro strutturale
1	138-139-159-158								Vetro strutturale
1	139-140-160-159								Vetro strutturale
1	146-147-137-136								Vetro strutturale
1	144-145-135-134								Vetro strutturale
1	143-144-134-133								Vetro strutturale
1	142-143-133-132								Vetro strutturale
1	141-142-132-131								Vetro strutturale
2	160-235-233-155								Vetro strutturale
2	165-237-229-145								Vetro strutturale
2	130-223-221-125								Vetro strutturale
2	125-221-239-170								Vetro strutturale
2	145-229-225-135								Vetro strutturale
2	135-225-231-150								Vetro strutturale
2	170-239-237-165								Vetro strutturale
2	150-231-227-140								Vetro strutturale

2	140-227-235-160	Vetro strutturale
3	225-226-232-231	Vetro strutturale
3	239-240-238-237	Vetro strutturale
3	237-238-230-229	Vetro strutturale
3	235-236-234-233	Vetro strutturale
3	223-224-222-221	Vetro strutturale
3	231-232-228-227	Vetro strutturale
3	227-228-236-235	Vetro strutturale
3	229-230-226-225	Vetro strutturale
3	221-222-240-239	Vetro strutturale
4	230-329-325-226	Vetro strutturale
4	228-327-335-236	Vetro strutturale
4	232-331-327-228	Vetro strutturale
4	238-337-329-230	Vetro strutturale
4	222-321-339-240	Vetro strutturale
4	226-325-331-232	Vetro strutturale
4	236-335-333-234	Vetro strutturale
4	224-323-321-222	Vetro strutturale
4	240-339-337-238	Vetro strutturale
5	339-340-338-337	Vetro strutturale
5	331-332-328-327	Vetro strutturale
5	329-330-326-325	Vetro strutturale
5	327-328-336-335	Vetro strutturale
5	325-326-332-331	Vetro strutturale
5	323-324-322-321	Vetro strutturale
5	335-336-334-333	Vetro strutturale
5	337-338-330-329	Vetro strutturale
5	321-322-340-339	Vetro strutturale
6	322-319-318-340	Vetro strutturale
6	336-312-311-334	Vetro strutturale
6	324-320-319-322	Vetro strutturale
6	332-314-313-328	Vetro strutturale
6	326-315-314-332	Vetro strutturale
6	330-316-315-326	Vetro strutturale
6	328-313-312-336	Vetro strutturale
6	338-317-316-330	Vetro strutturale
6	340-318-317-338	Vetro strutturale

TABULATI DI VERIFICA

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Forze sismiche e masse
- Taglianti di piano
- Spostamenti Relativi dei nodi (SLD)
- Fattori di partecipazione e masse modali
- Massime tensioni sul terreno aste
- Massime reazioni vincolari
- Massime sollecitazioni travi
- Massime sollecitazioni pilastri
- Massime sollecitazioni aste generiche

Risultati Analisi Dinamica - Baricentri masse e masse						
Scenario di calcolo : Set NT SLV A2 STR/GEO						
Combinazione masse 1						
Piano	Rigido	Massa		X	Y	Z
		kg	cm	cm	cm	cm
0	No	0	0	0	0	0
1	No	33133	136		811	880
2	No	0	0		0	0
3	No	1967	-396		524	1188

569

Combinazione masse 2

Piano	Rigido	Massa		X	Y	Z
		kg	cm	cm	cm	cm
0	No	0	0	0	0	0
1	No	33133	172		860	880
2	No	0	0		0	0
3	No	1967	-392		531	1188

Combinazione masse 3

Piano	Rigido	Massa		X	Y	Z
		kg	cm	cm	cm	cm
0	No	0	0	0	0	0
1	No	33133	136		910	880
2	No	0	0		0	0
3	No	1967	-396		538	1188

Combinazione masse 4

Piano	Rigido	Massa		X	Y	Z
		kg	cm	cm	cm	cm
0	No	0	0	0	0	0
1	No	33133	101		860	880
2	No	0	0		0	0
3	No	1967	-400		531	1188

Taglianti di piano

Scenario di calcolo : **Set NT SLV A2 STR/GEO**

I taglianti sono dati per combinazioni di calcolo C-S-Pm con C=Combinazione(1,2,...) S=Sisma(1,1I) Pm=posizione masse(1,2,...) Azioni complessive, riferite al sistema WCS,con origine in (0,0,0),I momenti sono comprensivi dei momenti di trasporto

con:

Fz=forza verticale,

dr=spost medio del piano rispetto al piano inferiore,

Fh=tagliante,

H=altezza del piano

$$\Theta = Fz \cdot dr / (Fh \cdot H)$$

Combinazione 12-I-I (SISMAX SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-12424	-1161	24215	-17255	-37090	-9513	5104	11102	0	--
1	17462	-528	-32165	-8220	35468	12812	254	8056	8477	0.001733
2	0	0	0	0	0	0	0	0	0	0.000000
3	6986	-1199	-12383	3364	17180	10906	-3971	5383	11880	0.002852

Piano	FxPl/Isol.	FyPl/Isol.	FzPar	FxShell	FyPar	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg
0	-10390	-3979	0	0	0	0	-12424	-1161
1	10390	3979	0	0	0	0	17462	-528
2	0	0	0	0	0	0	0	0
3	6986	-1199	0	0	0	0	6986	-1199

Percentuali assorbite in direzione X

Piano	0	%Pl/Isol. FX	%Par. FX	%Shell. FX
		100.00	0.00	
1	1	100.00	0.00	
2	2	--	--	
3	3	100.00	0.00	

Percentuali assorbite in direzione Y

570

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13166	-1256	24542	-15897	-39622	-9458	5104	11102	0
1	17293	-313	-34467	-5895	22581	4851	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	5725	-1360	-12525	1460	17002	6733	-3971	5383	11880

Combinazione 12-I-2 (SISMAX_SLV)

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13166	-1256	24542	-15897	-39622	-9458	5104	11102	0
1	17293	-313	-34467	-5895	22581	4851	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	5725	-1360	-12525	1460	17002	6733	-3971	5383	11880

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13166	-1256	24542	-15897	-39622	-9458	5104	11102	0
1	17293	-313	-34467	-5895	22581	4851	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	5725	-1360	-12525	1460	17002	6733	-3971	5383	11880

Percentuali assorbite in direzione X

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13166	-1256	24542	-15897	-39622	-9458	5104	11102	0
1	17293	-313	-34467	-5895	22581	4851	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	5725	-1360	-12525	1460	17002	6733	-3971	5383	11880

Percentuali assorbite in direzione Y

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13166	-1256	24542	-15897	-39622	-9458	5104	11102	0
1	17293	-313	-34467	-5895	22581	4851	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	5725	-1360	-12525	1460	17002	6733	-3971	5383	11880

Combinazione 12-I-3 (SISMAX_SLV)

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13945	-1953	25454	-15865	-40020	-3073	5104	11102	0
1	18364	-290	-37321	-4879	12815	-31380	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	4641	-2693	-15283	-8612	10328	-21718	-3971	5383	11880

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13945	-1953	25454	-15865	-40020	-3073	5104	11102	0
1	18364	-290	-37321	-4879	12815	-31380	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	4641	-2693	-15283	-8612	10328	-21718	-3971	5383	11880

Percentuali assorbite in direzione X

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13945	-1953	25454	-15865	-40020	-3073	5104	11102	0
1	18364	-290	-37321	-4879	12815	-31380	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	4641	-2693	-15283	-8612	10328	-21718	-3971	5383	11880

Percentuali assorbite in direzione Y

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13945	-1953	25454	-15865	-40020	-3073	5104	11102	0
1	18364	-290	-37321	-4879	12815	-31380	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	4641	-2693	-15283	-8612	10328	-21718	-3971	5383	11880

Combinazione 12-I-4 (SISMAX_SLV)

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13204	-1819	24395	-15705	-38622	-4226	5104	11102	0
1	18103	-846	-34523	6180	26872	-21776	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	7510	-1026	-13793	685	15188	-1022	-3971	5383	11880

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13204	-1819	24395	-15705	-38622	-4226	5104	11102	0
1	18103	-846	-34523	6180	26872	-21776	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	7510	-1026	-13793	685	15188	-1022	-3971	5383	11880

Percentuali assorbite in direzione X

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13204	-1819	24395	-15705	-38622	-4226	5104	11102	0
1	18103	-846	-34523	6180	26872	-21776	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	7510	-1026	-13793	685	15188	-1022	-3971	5383	11880

Percentuali assorbite in direzione Y

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-13204	-1819	24395	-15705	-38622	-4226	5104	11102	0
1	18103	-846	-34523	6180	26872	-21776	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	7510	-1026	-13793	685	15188	-1022	-3971	5383	11880

Combinazione 13-I-1 (SISMAX_SLV)

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-3295	-12412	25460	48878	12432	8448	5104	11102	0
1	-3409	17463	-31368	-25327	28490	35859	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	-4495	6847	-10161	-8089	8404	28059	-3971	5383	11880

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-3295	-12412	25460	48878	12432	8448	5104	11102	0
1	-3409	17463	-31368	-25327	28490	35859	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	-4495	6847	-10161	-8089	8404	28059	-3971	5383	11880

Percentuali assorbite in direzione X

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-3295	-12412	25460	48878	12432	8448	5104	11102	0
1	-3409	17463	-31368	-25327	28490	35859	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	-4495	6847	-10161	-8089	8404	28059	-3971	5383	11880

Percentuali assorbite in direzione Y

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-3295	-12412	25460	48878	12432	8448	5104	11102	0
1	-3409	17463	-31368	-25327	28490	35859	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	-4495	6847	-10161	-8089	8404	28059	-3971	5383	11880

Combinazione 13-I-2 (SISMAX_SLV)

Piano				%aPil/Isol. FY		%aPar. FY		%Shell. FY	
	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z
0	-3242	-13373	26289	53617	10762	8291	5104	11102	0
1	-4562	16649	-32973	-11560	27836	29624	254	8056	8477
2	0	0	0	0	0	0	0	0	0
3	-4495	6847	-10161	-8089	8404	28059	-3971	5383	11880

Periodi di vibrazione e Masse modali

Scenario di calcolo : Set_NT_SLV_A2_STR/GEO

Posizione masse 1

Numero di Frequenze calcolate =45, filtrate=35

Coeff. Partecipazione		Masse Modali		Percentuali	
N	T(s)	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2844	-28.693	41.663	8073	17022
2(2)	0.2103	-36.600	-29.921	13136	8780
3(3)	0.1748	-15.613	0.175	2390	0
4(4)	0.1599	-12.663	-4.869	1572	233
5(5)	0.1522	7.958	0.885	621	8
6(6)	0.1440	2.337	-3.716	54	135
7(7)	0.1402	3.252	-3.390	104	77
8(8)	0.1363	-5.146	-5.368	36	113
9(9)	0.1269	-6.279	3.786	387	141
10(10)	0.1195	2.826	-3.892	78	149
11(11)	0.1169	-7.256	4.172	516	171
12(12)	0.1140	-5.146	5.952	260	347
13(13)	0.1052	-1.293	5.933	16	345
14(15)	0.0947	6.313	-12.568	391	1549
15(16)	0.0886	6.119	-15.263	367	2285
16(17)	0.0844	-1.037	4.463	11	195
17(18)	0.0782	2.46	3.987	246	156
18(20)	0.0733	12.042	5.713	1422	320
19(21)	0.0704	3.904	2.886	149	82
20(23)	0.0670	16.620	11.084	2709	1205
21(24)	0.0618	-2.521	-0.119	62	0
22(25)	0.0613	-4.685	-1.856	215	34
23(26)	0.0565	2.859	0.473	80	2
24(27)	0.0536	-2.674	-2.170	70	46
25(28)	0.0522	2.049	0.006	41	0
26(29)	0.0505	-2.748	-1.348	74	18
27(30)	0.0463	-6.239	-4.693	382	216
28(33)	0.0430	4.591	2.678	207	70
29(34)	0.0410	2.671	0.969	70	9
30(36)	0.0395	2.501	-1.764	61	31
31(37)	0.0391	-2.265	4.069	50	162
32(40)	0.0360	-2.897	-0.382	82	1
33(42)	0.0347	2.030	4.421	2	0.030
34(44)	0.0317	-1.548	-3.249	24	104
35(45)	0.0309	-3.006	-2.387	89	56
Somma delle Masse Modali [kgm*g]		34088		34268	
Masse strutturali libere [kgm*g]		35100		35100	
Percentuale		97.12		97.63	

Posizione masse 2

Numero di Frequenze calcolate =45, filtrate=32

Coeff. Partecipazione		Masse Modali		Percentuali	
N	T(s)	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2728	-27.602	41.713	7471	17063
2(2)	0.2109	-38.187	-28.888	14301	8184
3(3)	0.1760	15.692	-3.298	2415	107
4(4)	0.1498	-7.300	-2.892	523	82
5(5)	0.1455	7.130	6.064	499	361
6(6)	0.1411	-6.833	5.044	458	250
7(7)	0.1367	10	2.758	10	75
8(8)	0.1291	-2.147	-5.156	45	261
9(9)	0.1232	4.412	-2.178	191	47
10(10)	0.1128	-5.128	6.148	258	371
11(11)	0.1122	-3.031	0.962	90	9
12(12)	0.1076	-8.568	8.066	720	638
13(13)	0.1023	1.640	-6.175	26	374

575

Coeff. Partecipazione		Masse Modali		Percentuali	
N	T(s)	Dir=0°	Dir=90°	Dir=0°	Dir=90°
14(14)	0.0955	-0.211	2.580	65	0.00
15(15)	0.0917	-7.878	17.464	2991	1.73
16(16)	0.0868	0.673	-4.996	4	0.70
17(17)	0.0821	0.456	2.632	68	0.01
18(18)	0.0799	-6.126	6.238	382	1.05
19(20)	0.0710	1.998	1.204	39	0.11
20(21)	0.0698	-15.306	-8.991	2297	793
21(22)	0.0669	2.276	1.805	51	32
22(23)	0.0650	15.677	10.177	2410	1016
23(24)	0.0605	3.051	-0.024	91	0
24(27)	0.0535	-2.430	-2.430	103	58
25(28)	0.0526	-2.898	1.390	82	19
26(30)	0.0465	3.050	1.991	91	39
27(31)	0.0459	4.355	216	186	216
28(32)	0.0434	-1.816	-1.816	295	32
29(34)	0.0422	4.432	73	193	0.21
30(40)	0.0358	-0.368	80	1	0.00
31(44)	0.0322	-1.023	-2.547	10	64
32(45)	0.0314	-1.030	-2.119	44	0.03
Somma delle Masse Modali [kgm*g]		33840		34060	
Masse strutturali libere [kgm*g]		35100		35100	
Percentuale		96.41		97.04	

Posizione masse 3

Numero di Frequenze calcolate =45, filtrate=29

Coeff. Partecipazione		Masse Modali		Percentuali	
N	T(s)	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2731	-24.966	43.453	6113	18516
2(2)	0.2081	-43.168	-23.604	18274	5464
3(3)	0.1752	-3.637	11.344	130	1262
4(4)	0.1498	-5.185	-3.322	108	264
5(5)	0.1448	8.530	6.694	714	439
6(6)	0.1414	3.483	-7.212	119	510
7(7)	0.1342	4.517	-0.839	200	7
8(8)	0.1286	-3.050	0.677	91	4
9(9)	0.1272	1.638	2.620	26	67
10(10)	0.1129	-3.646	5.126	130	258
11(11)	0.1128	-1.620	4.611	26	208
12(13)	0.0993	9.346	-15.621	857	2393
13(14)	0.0950	3.255	-4.998	104	245
14(15)	0.0932	9.648	-5.830	913	333
15(16)	0.0884	0.457	-4.779	2	224
16(18)	0.0820	-5.130	11.345	258	1262
17(21)	0.0688	-12.205	-7.559	1461	560
18(22)	0.0676	-16.654	-10.279	2720	1036
19(23)	0.0628	5.373	4.917	283	237
20(24)	0.0605	-5.256	-2.431	271	58
21(26)	0.0570	1.267	1.938	16	37
22(27)	0.0549	4.188	2.069	172	42
23(28)	0.0527	-1.105	2.357	12	54
24(30)	0.0474	2.308	1.302	52	17
25(31)	0.0451	-7.393	-3.932	536	152
26(32)	0.0436	-1.411	-3.495	20	120
27(34)	0.0420	2.850	-3.811	80	142
28(43)	0.0334	3.560	0.547	124	3
29(44)	0.0321	-2.648	-2.288	69	51
Somma delle Masse Modali [kgm*g]		33880		33968	
Masse strutturali libere [kgm*g]		35100		35100	
Percentuale		96.52		96.77	

Posizione masse 4

576

Numero di Frequenze calcolate =45, filtrate=27

N	T(s)	Coeff. Partecipazione		Masse Modali kgm²g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2845	-26.586	43.175	6932	18280	19.75	52.08
2(2)	0.2043	-42.157	-26.432	17429	6852	49.65	19.52
3(3)	0.1730	-7.648	8.469	7.648	703	1.63	2.00
4(4)	0.1563	-9.661	-7.424	9.15	540	2.61	1.54
5(5)	0.1423	3.273	-4.067	105	162	0.30	0.46
6(7)	0.1401	-2.643	4.031	68	159	0.20	0.45
7(9)	0.1335	-2.907	-0.543	83	3	0.24	0.01
8(10)	0.1184	2.895	-4.947	82	240	0.23	0.68
9(11)	0.1180	2.039	-1.120	41	12	0.12	0.04
10(12)	0.1119	-2.982	-0.551	3	87	0.01	0.25
11(13)	0.1026	-11.570	12.699	1313	1582	3.74	4.51
12(14)	0.0991	-3.725	4.785	136	225	0.39	0.64
13(15)	0.0957	1.637	-10.870	26	1159	0.07	3.30
14(18)	0.0835	7.925	616	616	1739	1.75	4.95
15(20)	0.0726	3.810	2.225	142	49	0.41	0.14
16(21)	0.0702	2.125	1.868	44	34	0.13	0.10
17(22)	0.0692	-19.071	-11.915	3567	1392	10.16	3.97
18(23)	0.0651	-6.142	-2.611	370	67	1.05	0.19
19(24)	0.0623	4.983	3.844	243	145	0.69	0.41
20(25)	0.0615	3.745	3.164	3.745	98	0.39	0.28
21(27)	0.0555	4.451	2.099	194	43	0.55	0.12
22(30)	0.0480	2.241	1.346	18	18	0.14	0.05
23(31)	0.0446	-7.996	-5.395	627	285	1.79	0.81
24(37)	0.0388	-2.601	4.112	66	166	0.19	0.47
25(42)	0.0334	-3.219	-0.372	102	1	0.29	0.00
26(44)	0.0319	-2.995	-1.391	88	19	0.25	0.05
27(45)	0.0314	-1.822	-2.006	33	39	0.09	0.11
Somma delle Masse Modali [kgm²g]				33986	34100		
Masse strutturali libere [kgm²g]				35100	35100		
Percentuale				96.83	97.15	96.83	97.15

1020	336	900(3-1-1)	-27(13-1-4)	-233(6)	0	0	22(9)
328	890(3-1-1)	233(6)	0	0	20(13-1-4)	0	22(9)
1021	312	1208(13-1-1)	-27(13-1-4)	7(9)	0	0	22(9)
313	1208(13-1-1)	109(6)	0	0	12(8)	0	22(9)
1022	102	-1730(3-11-3)	9(13-11-3)	-187(6)	0	0	11(9)
103	-1730(3-11-3)	202(6)	0	0	22(8)	0	22(8)
1023	137	519(13-1-3)	-29(8)	-201(6)	0	0	12(13-1-1)
147	519(13-1-3)	203(6)	0	0	32(8)	0	32(8)
1024	138	441(13-1-3)	-51(8)	-207(6)	0	0	-18(13-1-4)
148	441(13-1-3)	209(6)	0	0	44(8)	0	44(8)
1025	139	369(13-1-3)	-55(13-1-4)	-210(6)	0	0	-34(13-1-4)
149	369(13-1-3)	212(6)	0	0	48(8)	0	48(8)
1026	140	202(12-1-1)	-80(13-1-4)	-208(6)	0	0	-50(13-1-4)
150	202(12-1-1)	210(6)	0	0	58(8)	0	58(8)
1027	227	-247(12-1-1)	-78(13-1-4)	-205(6)	0	0	-50(13-1-4)
231	-247(12-1-1)	203(6)	0	0	58(8)	0	58(8)
1028	228	-345(13-1-4)	-58(13-1-4)	-199(6)	0	0	-37(13-1-4)
232	-345(13-1-4)	201(6)	0	0	49(8)	0	49(8)
1029	327	-477(13-1-4)	-19(8)	-201(6)	0	0	-12(13-1-4)
331	-477(13-1-4)	203(6)	0	0	30(8)	0	30(8)
1030	328	131(13-1-4)	-23(13-1-4)	-213(6)	0	0	22(9)
332	130(13-1-4)	215(6)	0	0	17(13-1-4)	0	17(13-1-4)
1031	313	554(12-1-1)	-5(13-1-1)	-131(6)	0	0	20(9)
314	554(12-1-1)	125(6)	0	0	14(8)	0	14(8)
1032	103	-863(13-1-3)	31(12-1-1)	-96(6)	0	0	15(12-1-1)
104	-863(13-1-3)	85(6)	0	0	22(9)	0	22(9)
1033	136	-483(8)	14(13-1-1)	-190(6)	0	0	12(8)
146	-486(8)	191(6)	0	0	23(8)	0	23(8)
1034	148	489(13-1-3)	-95(13-1-4)	-203(6)	0	0	38(13-1-4)
133	489(13-1-3)	205(6)	0	0	65(13-1-4)	0	65(13-1-4)
1035	149	477(13-1-1)	-100(13-1-4)	-205(6)	0	0	-47(13-1-4)
134	477(13-1-1)	207(6)	0	0	66(13-1-4)	0	66(13-1-4)
1036	150	237(13-1-3)	-111(13-1-4)	-203(6)	0	0	-60(13-1-4)
135	237(13-1-3)	205(6)	0	0	72(13-1-4)	0	72(13-1-4)
1037	231	-519(13-1-1)	-79(13-1-4)	-198(6)	0	0	-50(13-1-4)
225	-519(13-1-1)	200(6)	0	0	55(8)	0	55(8)
1038	232	-400(13-1-4)	-58(13-1-4)	-194(6)	0	0	-38(13-1-4)
226	-400(13-1-4)	196(6)	0	0	49(8)	0	49(8)
1039	331	-860(13-1-1)	-25(13-1-4)	-193(6)	0	0	-16(13-1-4)
325	-860(13-1-1)	195(6)	0	0	29(9)	0	29(9)
1040	332	-288(13-1-4)	-24(13-1-4)	-204(6)	0	0	22(9)
326	-287(13-1-4)	205(6)	0	0	17(13-1-4)	0	17(13-1-4)
1041	314	537(12-1-4)	6(13-11-1)	-113(6)	0	0	20(9)
315	537(12-1-4)	113(6)	0	0	13(8)	0	13(8)
1042	104	-358(12-1-1)	20(12-1-1)	-97(6)	0	0	9(12-1-1)
105	-359(12-1-1)	83(6)	0	0	25(9)	0	25(9)
1043	147	484(13-1-3)	66(13-11-3)	-198(6)	0	0	22(13-11-2)
132	484(13-1-3)	200(6)	0	0	-25(8)	0	-25(8)
1044	146	-556(8)	45(13-11-3)	-188(6)	0	0	15(8)
131	-550(8)	189(6)	0	0	31(13-1-3)	0	31(13-1-3)
1045	134	270(13-1-3)	-62(9)	-201(6)	0	0	29(13-1-4)
144	270(13-1-3)	204(6)	0	0	51(9)	0	51(9)
1046	135	254(13-1-3)	-69(8)	-199(6)	0	0	-69(8)
145	253(13-1-3)	201(6)	0	0	57(8)	0	57(8)
1047	225	-252(13-1-1)	-67(9)	-194(6)	0	0	-27(9)
229	-252(13-1-1)	196(6)	0	0	58(8)	0	58(8)
1048	226	-169(12-1-1)	-53(9)	-190(6)	0	0	-19(9)
230	-169(12-1-1)	191(6)	0	0	51(9)	0	51(9)
1049	325	-364(12-1-1)	-22(9)	-189(6)	0	0	3(13-1-1)
329	-364(12-1-1)	190(6)	0	0	31(9)	0	31(9)
1050	326	-114(13-1-4)	4(8)	-199(6)	0	0	19(8)
330	-114(13-1-4)	200(6)	0	0	14(9)	0	14(9)
1051	315	522(12-1-4)	22(13-1-4)	-100(6)	0	0	19(8)
316	522(12-1-4)	103(6)	0	0	-15(13-1-4)	0	-15(13-1-4)
1052	132	505(13-1-3)	71(13-1-4)	-196(6)	0	0	37(13-1-4)
142	505(13-1-3)	197(6)	0	0	40(8)	0	40(8)
1053	105	-305(13-11-3)	-93(13-11-3)	-97(6)	0	0	-40(13-11-3)

1054	106	-304(13-1-3)	-93(13-11-3)	81(6)	0	0	48(8)
133	453(13-1-3)	-58(9)	0	0	31(13-1-1)	0	31(13-1-1)
1055	143	453(13-1-3)	-58(9)	202(6)	0	0	-48(9)
131	-612(8)	-60(13-11-3)	-186(6)	0	0	0	-28(13-11-3)
1056	145	252(12-1-4)	108(13-11-4)	-196(6)	0	0	31(8)
141	252(12-1-4)	199(6)	0	0	-59(13-11-4)	0	-70(13-1-4)
1057	229	-299(13-11-4)	77(13-11-4)	-191(6)	0	0	49(13-11-4)
237	-299(13-11-4)	193(6)	0	0	51(9)	0	51(9)
1058	230	-227(13-11-4)	56(13-11-4)	-187(6)	0	0	36(13-11-4)
238	-227(13-11-4)	189(6)	0	0	46(9)	0	46(9)
1059	329	-947(13-1-4)	-24(13-1-4)	-186(6)	0	0	-18(13-1-4)
337	-947(13-1-4)	187(6)	0	0	29(8)	0	29(8)
1060	330	145(13-1-1)	24(13-11-4)	-196(6)	0	0	23(8)
338	145(13-1-1)	197(6)	0	0	-17(13-11-4)	0	-17(13-11-4)
1061	316	561(12-1-4)	61(13-11-1)	-105(6)	0	0	20(8)
317	561(12-1-4)	112(6)	0	0	13(9)	0	13(9)
1062	141	-61(18)	47(13-11-3)	-184(6)	0	0	32(13-11-3)
161	-61(18)	185(6)	0	0	17(9)	0	17(9)
1063	143	388(13-1-3)	-95(13-1-4)	-198(6)	0	0	-64(13-1-4)
163	388(13-1-3)	200(6)	0	0	38(13-1-4)	0	38(13-1-4)
1064	106	-592(13-1-3)	-26(13-1-3)	-98(6)	0	0	-11(13-1-3)
107	-592(13-1-3)	79(6)	0	0	27(9)	0	27(9)
1065	144	500(13-1-3)	-97(13-1-4)	-199(6)	0	0	62(13-11-4)
164	499(13-1-3)	201(6)	0	0	37(13-11-4)	0	37(13-11-4)
1066	142	476(13-1-3)	-66(13-1-3)	-193(6)	0	0	-46(13-1-3)
162	476(13-1-3)	196(6)	0	0	28(8)	0	28(8)
1067	237	-276(12-1-4)	72(13-11-4)	-188(6)	0	0	45(13-11-4)
239	-276(12-1-4)	191(6)	0	0	50(9)	0	50(9)
1068	238	-179(8)	56(13-11-4)	-183(6)	0	0	37(13-11-4)
240	-179(8)	186(6)	0	0	45(9)	0	45(9)
1069	337	-466(13-1-1)	18(13-11-4)	-182(6)	0	0	12(13-11-4)
339	-466(13-1-1)	184(6)	0	0	29(8)	0	29(8)
1070	338	96(12-11-4)	23(13-11-4)	-192(6)	0	0	23(8)
340	96(12-11-4)	193(6)	0	0	-16(13-11-4)	0	-16(13-11-4)
1071	317	666(13-11-4)	5(13-11-1)	-110(6)	0	0	20(8)
318	666(13-11-4)	120(6)	0	0	13(9)	0	13(9)
1072	165	221(12-1-4)	73(13-11-4)	-194(6)	0	0	43(13-11-4)
170	221(12-1-4)	197(6)	0	0	49(9)	0	49(9)
1073	162	406(13-1-3)	-34(9)	-193(6)	0	0	-13(13-1-3)
167	406(13-1-3)	195(6)	0	0	35(8)	0	35(8)
1074	164	344(13-1-1)	57(13-11-4)	-196(6)	0	0	31(13-11-4)
169	343(13-1-1)	199(6)	0	0	41(9)	0	41(9)
1075	161	-535(8)	-18(13-1-3)	-184(6)	0	0	10(8)
166	-535(8)	186(6)	0	0	25(8)	0	25(8)
1076	107	-372(13-1-1)	-38(9)	-100(6)	0	0	-16(13-1-3)
108	-372(13-1-1)	79(6)	0	0	34(9)	0	34(9)
1077	163	325(13-1-3)	-45(9)	-196(6)	0	0	19(13-11-3)
168	325(13-1-3)	199(6)	0	0	42(9)	0	42(9)
1078	240	-215(8)	51(13-11-4)	-184(6)	0	0	34(13-11-4)
222	-215(8)	186(6)	0	0	46(8)	0	46(8)
1079	339	-1694(13-1-4)	24(13-11-4)	-183(6)	0	0	15(13-11-4)
321	-1692(13-1-4)	185(6)	0	0	26(8)	0	26(8)
1080	342	144(13-11-4)	24(13-11-4)	-192(6)	0	0	24(8)
322	144(13-11-4)	193(6)	0	0	-18(13-11-4)	0	-18(13-11-4)
1081	318	1280(13-11-4)	6(13-11-1)	-101(6)	0	0	20(8)
170	1280(13-11-4)	112(6)	0	0	13(9)	0	13(9)
1082	319	188(13-1-3)	106(13-11-4)	-195(6)	0	0	58(13-11-4)
125	188(13-1-3)	198(6)	0	0	48(13-11-4)	0	48(13-11-4)
1083	169	647(13-11-1)	96(13-11-4)	-198(6)	0	0	-62(13-11-4)
124	648(13-11-1)	201(6)	0	0	23(13-11-3)	0	23(13-11-3)
1084	167	317(13-1-4)	68(13-11-3)	-194(6)	0	0	-48(13-11-3)
122	317(13-1-4)	197(6)	0	0	46(13-11-4)	0	46(13-11-4)
1085	239	-498(13-1-1)	75(13-11-4)	-189(6)	0	0	48(9)
221	-498(13-1-1)	192(6)	0	0	39(13-11-4)	0	39(13-11-4)
1086	168	247(13-1-3)	97(13-11-4)	-198(6)	0	0	-65(13-11-4)
123	247(13-1-3)	201(6)	0	0		0	

1087	166	-386(8)	52(13-II-3)	-186(6)	0	0	20(8)
	121	-386(8)	52(13-II-3)	188(6)	0	0	-33(13-I-3)
1088	108	-889(13-I-1)	-33(13-I-2)	-101(6)	0	0	-13(13-I-2)
	109	-889(13-I-1)	-33(13-I-2)	80(6)	0	0	24(9)
1089	321	-1276(13-II-4)	-24(8)	-181(6)	0	0	-41(12-I-3)
	323	-1277(13-II-4)	-24(8)	183(6)	0	0	33(8)
1090	322	152(13-II-4)	-4(13-II-3)	-190(6)	0	0	19(9)
	324	153(13-II-4)	-4(13-II-3)	192(6)	0	0	15(8)
1091	319	906(13-II-4)	-24(13-II-4)	-91(6)	0	0	-17(13-I-4)
	320	906(13-II-4)	-24(13-II-4)	102(6)	0	0	16(13-II-4)
1092	222	-144(8)	-61(8)	-183(6)	0	0	-23(8)
	224	-146(8)	-61(8)	185(6)	0	0	57(8)
1093	221	-363(13-I-1)	-71(8)	-188(6)	0	0	-28(8)
	223	-363(13-I-1)	-71(8)	191(6)	0	0	61(8)
1094	123	108(13-I-3)	-67(8)	-198(6)	0	0	-30(13-I-4)
	128	108(13-I-3)	-67(8)	201(6)	0	0	48(8)
1095	125	-118(13-I-3)	-76(8)	-194(6)	0	0	-29(8)
	130	-118(13-I-3)	-76(8)	197(6)	0	0	62(8)
1096	122	203(13-I-4)	-45(8)	-195(6)	0	0	-36(13-I-4)
	127	203(13-I-4)	-45(8)	198(6)	0	0	33(8)
1097	121	-221(13-I-2)	30(13-I-1)	-187(6)	0	0	25(13-I-3)
	126	-221(13-I-2)	30(13-I-1)	189(6)	0	0	11(9)
1098	124	434(13-II-1)	-75(8)	-197(6)	0	0	-30(13-I-4)
	129	434(13-II-1)	-75(8)	201(6)	0	0	56(8)
1099	109	578(13-II-1)	67(13-I-3)	-102(6)	0	0	30(13-I-3)
	110	578(13-II-1)	67(13-I-3)	81(6)	0	0	36(9)
8000	101	-440(6)	255(13-I-3)	-1604(3)	10(13-I-1)	3779(3)	-424(13-II-3)
	151	-408(6)	255(13-I-3)	-1377(3)	10(13-I-1)	1899(12-I-2)	-424(13-II-3)
8000	151	-3758(6)	-236(8)	-1234(3)	8(13-I-1)	1899(12-I-2)	-414(13-I-3)
	152	-3455(6)	-236(8)	-1014(8)	8(13-I-1)	-1429(8)	578(9)
8000	152	-3782(13-I-4)	-267(13-I-4)	-901(8)	5(13-I-4)	-1430(8)	597(9)
	153	-3647(13-I-4)	-267(13-I-4)	-695(8)	5(13-I-4)	-2790(8)	491(8)
8000	153	-3581(13-I-4)	192(13-I-3)	-639(12-I-1)	-7(13-I-2)	-2793(8)	513(8)
	154	-3462(13-I-4)	192(13-I-3)	-528(12-I-1)	-7(13-I-2)	-3575(8)	389(9)
8000	154	-2878(13-I-4)	152(8)	-589(12-I-1)	-4(12-II-1)	-3580(8)	418(9)
	155	-2774(13-I-4)	132(8)	559(12-II-1)	-4(12-II-1)	-3801(8)	-260(13-I-4)
8000	155	-2676(13-I-4)	-150(13-I-4)	724(13-I-1)	-14(13-I-1)	-3801(8)	-276(13-I-4)
	233	-2594(13-I-4)	-150(13-I-4)	835(13-I-1)	-14(13-I-1)	-3558(8)	83(9)
8000	233	-1659(13-II-1)	109(13-I-4)	986(13-II-1)	-12(13-I-4)	-3556(8)	116(9)
	234	-1600(13-II-1)	109(13-I-4)	1097(13-I-1)	-12(13-I-4)	-3015(9)	72(13-I-1)
8000	234	-1786(13-II-1)	-150(13-II-4)	949(13-II-4)	-7(8)	-3014(9)	-73(13-I-1)
	333	-1751(13-I-1)	-150(13-I-4)	1060(13-I-4)	-7(8)	-2193(9)	-216(13-I-4)
8000	333	-2803(13-I-1)	-170(13-I-4)	1056(3)	7(13-I-1)	-201(13-I-4)	-201(13-I-4)
	334	-2798(13-II-1)	-170(13-I-4)	1284(3)	7(13-I-1)	2088(13-II-1)	58(8)
8000	334	-2761(13-II-1)	-60(13-I-1)	1515(13-I-1)	15(13-I-4)	2088(13-II-1)	-48(13-I-1)
	311	-2793(13-II-1)	-60(13-I-1)	1626(13-I-1)	15(13-I-4)	1914(10)	23(13-I-4)
8001	102	-7747(6)	242(13-I-3)	-2364(6)	2(13-I-1)	5186(3)	43(8)
	156	-7235(6)	242(13-I-3)	-1990(3)	2(13-I-1)	2099(12-I-2)	-431(13-II-3)
8001	156	-6610(6)	-250(8)	-1652(3)	4(8)	2099(12-I-2)	-429(13-I-3)
	157	-6115(6)	-250(8)	-1282(3)	4(8)	-196(12-II-1)	613(8)
8001	157	-6451(6)	-308(13-I-4)	-1073(3)	5(13-I-1)	-1957(12-II-1)	649(8)
	158	-5991(6)	-308(13-I-4)	-710(8)	5(13-I-1)	-3244(8)	593(8)
8001	158	-5442(6)	182(13-I-3)	-821(12-I-1)	2(13-I-3)	-3246(8)	625(8)
	159	-5036(6)	182(13-I-3)	-664(12-I-1)	2(13-I-3)	-3955(8)	562(8)
8001	159	-4690(6)	156(8)	-826(12-I-1)	4(9)	-3954(8)	605(8)
	160	-4336(6)	156(8)	951(12-I-1)	4(9)	-399(18)	461(13-I-4)
8001	160	-3991(6)	267(13-I-4)	882(12-II-1)	-7(13-I-1)	-3990(8)	512(13-I-4)
	235	-3711(6)	267(13-I-4)	1039(12-II-1)	-7(13-I-1)	-3595(9)	309(9)
8001	235	-3244(6)	197(8)	772(13-I-1)	-8(13-I-1)	-3596(9)	370(9)
	236	-3127(12-II-1)	197(8)	999(6)	-8(13-I-1)	-3037(9)	137(9)
8001	236	-3292(12-II-1)	161(9)	899(3)	-6(13-I-4)	-3037(9)	196(9)
	335	-3242(12-II-1)	161(9)	1269(3)	-6(13-I-4)	2321(12-II-1)	-103(13-I-4)
8001	335	-2614(12-II-1)	-58(13-I-1)	1414(13-I-1)	10(13-I-1)	2323(12-II-1)	-59(13-I-4)
	336	-2607(13-I-1)	-58(13-I-1)	1571(13-I-1)	10(13-I-1)	1712(12-II-1)	-47(13-I-1)
8001	336	-2667(6)	-43(13-I-1)	1917(12-I-1)	14(13-I-1)	1712(12-II-1)	-32(13-I-1)
	312	-2776(6)	-43(13-I-1)	2074(12-I-1)	14(13-I-4)	2347(13-II-1)	17(13-I-1)
8002	103	-6915(6)	175(13-II-3)	-2202(3)	3(12-II-1)	4986(3)	-54(13-I-3)

	136	-6411(6)	175(13-II-3)	-1838(3)	3(12-II-1)	1938(12-I-2)	-371(13-II-3)
8002	136	-5942(6)	-235(8)	-1598(3)	-3(13-I-4)	1938(12-I-2)	-378(13-II-3)
	137	-5452(6)	-235(8)	-1231(3)	-3(13-I-4)	-1649(8)	611(8)
8002	137	-5511(6)	-262(13-I-4)	-1084(3)	2(9)	-1649(8)	626(8)
	138	-5054(6)	-262(13-I-4)	-716(3)	2(9)	-3123(8)	594(8)
8002	138	-4589(6)	-117(13-II-3)	-706(12-I-2)	2(12-II-1)	-3124(8)	625(8)
	139	-4183(6)	-117(13-II-3)	-549(12-I-2)	2(12-II-1)	-3895(8)	569(8)
8002	139	-3783(6)	126(8)	-661(12-I-1)	4(8)	-3896(8)	606(8)
	140	-3428(6)	126(8)	698(12-II-1)	4(8)	-4006(8)	549(13-I-4)
8002	140	-3122(6)	289(13-I-4)	626(12-II-1)	3(8)	-4007(8)	626(13-I-4)
	227	-2840(6)	289(13-I-4)	783(12-II-1)	3(8)	-3619(8)	305(8)
8002	227	-2668(6)	240(8)	608(6)	-5(13-I-4)	-3620(8)	370(8)
	228	-2463(6)	240(8)	988(6)	-5(13-I-4)	-3001(9)	139(13-I-4)
8002	228	-2465(6)	89(8)	944(3)	-17(13-I-4)	-2995(9)	207(13-I-4)
	327	-2404(12-II-1)	89(8)	1317(6)	-17(13-I-4)	-2084(9)	149(13-I-4)
8002	327	-2151(6)	189(13-I-4)	1081(3)	23(13-I-4)	-2084(9)	165(13-I-4)
	328	-2133(6)	189(13-I-4)	1453(3)	23(13-I-4)	1636(12-II-1)	-47(13-I-1)
8002	328	-2596(6)	40(13-I-1)	1474(12-I-1)	-13(8)	1635(12-II-1)	36(13-I-1)
	313	-2706(6)	40(13-I-1)	1631(12-I-1)	-13(8)	2357(0)	11(13-II-1)
8003	104	-6293(6)	183(13-II-3)	-2047(3)	4(13-II-3)	4710(3)	-40(12-I-1)
	146	-5799(6)	183(13-II-3)	-1690(3)	4(13-II-3)	1812(12-I-2)	-358(13-II-3)
8003	146	-5483(6)	-195(8)	-1516(3)	-2(13-I-4)	1812(12-I-2)	-363(13-II-3)
	147	-5000(6)	-195(8)	-1543(3)	-2(13-I-4)	-1580(8)	603(8)
8003	147	-4856(6)	-257(13-I-4)	-1069(3)	2(9)	-1578(8)	613(8)
	148	-4401(6)	-257(13-I-4)	-703(3)	2(9)	-3035(8)	588(13-I-4)
8003	148	-4057(6)	-112(13-II-3)	-672(3)	1(12-II-1)	-3034(8)	618(13-I-4)
	149	-3651(6)	-112(13-II-3)	-488(12-I-2)	1(12-II-1)	-3816(8)	542(8)
8003	149	-3345(6)	142(8)	937(6)	3(8)	-2980(9)	188(13-I-4)
	150	-2989(6)	111(8)	570(12-II-4)	3(8)	-3960(8)	593(13-I-4)
8003	150	-2755(6)	331(13-I-4)	512(12-II-4)	3(8)	-3959(8)	672(13-I-4)
	231	-2471(6)	331(13-I-4)	670(12-II-4)	3(8)	-3605(8)	255(8)
8003	231	-2342(6)	142(8)	552(6)	3(8)	-3604(8)	324(8)
	232	-2167(6)	200(8)	911(3)	-18(13-I-4)	-2980(9)	257(13-I-4)
8003	232	-2167(6)	200(8)	1288(6)	-18(13-I-4)	-2084(9)	131(13-I-4)
	331	-1927(6)	168(13-I-4)	1101(3)	22(13-I-4)	-2083(9)	131(13-I-4)
8003	331	-1909(6)	168(13-I-4)	1478(3)	22(13-I-4)	1508(12-I-4)	-56(13-I-1)
	332	-2384(6)	-47(13-II-1)	1346(12-I-4)	-14(8)	1508(12-II-4)	-41(13-II-1)
8004	314	-2495(6)	-47(13-II-1)	1612(3)	-14(8)	2347(10)	13(13-II-1)
	105	-5927(6)	227(13-II-3)	-1972(3)	-3(13-II-4)	4582(3)	95(13-II-4)
8004	131	-5438(6)	227(13-II-3)	-1619(3)	-3(13-II-4)	1845(12-I-3)	-328(13-II-3)
	131	-5120(6)	-179(8)	-1501(3)	2(9)	1846(12-I-3)	-329(13-II-3)
8004	132	-4640(6)	-179(8)	-142(3)	2(9)	-1564(8)	617(9)
	132	-4505(6)	-196(13-I-4)	-1073(3)	2(8)	-1566(8)	631(9)
8004	133	-4052(6)	-196(13-I-4)	-709(8)	2(8)	-3043(8)	577(8)
	133	-3693(6)	-101(13-II-3)	-684(3)	3(13-II-3)	-3044(8)	607(8)
8004	134	-3451(13-I-1)	-101(13-II-3)	-504(12-I-3)	3(13-II-3)	-3851(8)	527(8)
	134	-3261(13-I-1)	123(8)	-600(12-I-4)	3(8)	-3849(8)	570(8)
8004	135	-3114(13-I-1)	123(8)	582(12-II-4)	3(8)	-3973(8)	466(13-I-4)
	135	-3091(13-I-1)	239(13-I-4)	548(12-II-4)	8(13-II-4)	-3974(8)	524(13-I-4)
8004	225	-2973(13-I-1)	239(13-I-4)	707(12-II-4)	8(13-II-4)	-3583(8)	248(8)
	225	-2407(6)	156(8)	804(13-II-4)	-3(13-I-4)	-3582(8)	320(8)
8004	226	-2198(6)	156(8)	965(6)	-3(13-I-4)	-2876(9)	-158(13-II-4)
	226	-2231(6)	404(13-I-4)	915(3)	-7(13-I-4)	-2876(9)	195(13-I-4)
8004	325	-2107(6)	404(13-I-4)	1300(6)	-7(13-I-4)	-1937(9)	-262(13-I-4)
	325	-2323(13-I-4)	-217(13-I-4)	1149(13-I-4)	12(13-I-4)	-1939(9)	-227(13-I-4)
8004	326	-2315(13-I-4)	1405(3)	1718(13-I-4)	12(13-I-4)	1533(12-I-4)	-36(13-II-1)
	326	-2369(6)	-41(13-II-1)	1880(13-I-4)	-14(9)	1533(12-II-4)	-39(13-II-1)
8005	315	-2483(6)	-41(13-II-1)	1880(13-I-4)	-14(9)	2303(10)	27(13-I-4)
	106	-6219(6)	204(13-II-3)	-2006(3)	-4(13-I-4)	4627(3)	71(8)
8005	141	-5735(6)	204(13-II-3)	-1656(3)	-4(13-I-4)	1875(12-I-3)	346(9)
	141	-5445(6)	-1509(9)	-1475(3)	-2(13-I-4)	1876(12-I-3)	351(9)
8005	142	-4968(6)	-1509(9)	-1118(3)	-2(13-I-4)	-1500(8)	618(9)
	142	-502(6)	191(13-II-4)	-1046(3)	1(9)	-1498(8)	637(9)
8005	143	-4650(6)	191(13-II-4)	-683(3)	1(9)	-2903(8)	575(9)
	143	-4314(6)	-97(13-II-3)	-677(3)	-4(13-I-3)	-2902(8)	603(9)
8005	144	-3907(6)	-97(13-II-3)	-514(12-I-3)	-4(13-I-3)	-3692(8)	469(8)

8005	144	-3367(6)	-56(13-14)	-610(12-14)	3(9)	-3690(8)	511(8)
	145	-3316(13-14)	-56(13-14)	596(12-14)	3(9)	-3896(8)	465(13-14)
8005	145	-3328(13-14)	-240(13-14)	782(12-14)	-8(13-14)	-3898(8)	521(13-14)
	229	-3210(13-14)	-240(13-14)	742(12-14)	-8(13-14)	-3669(8)	230(9)
8005	229	-2228(6)	129(8)	779(13-14)	4(9)	-3672(8)	296(9)
	230	-201(76)	129(8)	940(13-14)	4(9)	-3157(9)	156(13-14)
8005	230	-2098(12-14)	412(13-14)	862(3)	6(13-14)	-3156(9)	198(9)
	329	-2047(12-14)	412(13-14)	1251(6)	6(13-14)	-2328(9)	-274(13-14)
8005	329	-2127(12-14)	-230(13-14)	1153(3)	-11(13-14)	-2325(9)	-24(13-14)
	330	-2120(12-14)	-230(13-14)	1544(3)	-11(13-14)	1611(12-14)	-36(13-14)
8005	330	-2204(6)	-41(13-14)	1572(12-14)	-14(9)	1610(12-14)	-40(13-14)
	316	-2320(6)	-41(13-14)	1744(8)	-14(9)	2306(10)	23(13-14)
8006	316	-5904(6)	-192(8)	-1937(3)	-4(13-14)	4452(3)	56(9)
	161	-5423(6)	-192(8)	-1589(3)	-4(13-14)	1907(12-13)	404(8)
8006	161	-5114(6)	-119(9)	-1441(3)	-3(13-14)	1907(12-13)	404(8)
	162	-4639(6)	-119(9)	-1086(3)	-3(13-14)	-1495(8)	616(9)
8006	162	-4832(6)	222(13-14)	-104(13)	1(9)	-1495(8)	632(9)
	163	-4381(6)	222(13-14)	-678(3)	1(9)	-2908(8)	-574(13-14)
8006	163	-4033(6)	-111(13-14)	-708(12-13)	1(13-14)	-2909(8)	-607(13-14)
	164	-3625(6)	-111(13-14)	-551(12-13)	1(13-14)	-3708(8)	-503(13-14)
8006	164	-3322(6)	133(9)	-622(12-14)	3(9)	-3708(8)	-571(13-14)
	165	-2961(6)	133(9)	603(12-14)	3(9)	-3892(8)	-533(13-14)
8006	165	-2724(6)	-284(13-14)	541(12-14)	3(9)	-3892(8)	-612(13-14)
	237	-2433(6)	-284(13-14)	702(12-14)	3(9)	-3594(8)	243(9)
8006	237	-2312(6)	157(8)	509(12-14)	3(13-14)	-3594(8)	-319(13-14)
	238	-2098(6)	157(8)	907(6)	3(13-14)	-3023(9)	-176(13-14)
8006	238	-2165(12-14)	146(8)	868(3)	18(13-14)	-244(13-14)	-302(9)
	337	-2113(12-14)	146(8)	1263(3)	18(13-14)	-2147(9)	-111(13-14)
8006	337	-1897(12-14)	-148(13-14)	1046(3)	-23(13-14)	-2147(9)	-127(13-14)
	338	-1889(12-14)	-148(13-14)	1445(3)	-23(13-14)	1523(12-14)	421(13-14)
8006	338	-2259(6)	-39(13-14)	1425(12-14)	-14(9)	1523(12-14)	-37(13-14)
	317	-2378(6)	-39(13-14)	1616(3)	-14(9)	2258(10)	13(13-14)
8007	317	-6045(6)	-236(8)	-1959(3)	-4(13-14)	4395(3)	72(13-14)
	166	-5567(6)	-236(8)	-1614(3)	-4(13-14)	1922(12-13)	461(8)
8007	166	-5271(6)	-94(9)	-1447(3)	3(13-14)	1923(12-13)	457(8)
	167	-4797(6)	-94(9)	-1093(3)	3(13-14)	-1620(8)	622(9)
8007	167	-4950(6)	223(13-14)	-1014(3)	-1(13-14)	-1624(8)	635(9)
	168	-4499(6)	223(13-14)	-65(13)	-1(13-14)	-2998(8)	-588(13-14)
8007	168	-4175(6)	-128(13-14)	-722(12-13)	-2(13-14)	-2996(8)	-622(13-14)
	169	-3766(6)	-128(13-14)	-564(12-13)	-2(13-14)	-3716(8)	-500(13-14)
8007	169	-3475(6)	160(9)	-636(12-13)	3(9)	-3719(8)	-500(13-14)
	170	-3111(6)	160(9)	636(12-13)	3(9)	-3834(8)	-539(13-14)
8007	170	-2888(6)	-298(13-14)	532(12-14)	3(8)	-3834(8)	-617(13-14)
	239	-2595(6)	-298(13-14)	695(12-14)	3(8)	-3482(8)	247(9)
8007	239	-2475(6)	166(9)	515(6)	3(13-14)	-3482(8)	-304(13-14)
	240	-2258(6)	152(13-14)	847(3)	16(13-14)	-2911(9)	172(13-14)
8007	240	-2286(6)	152(13-14)	1247(3)	16(13-14)	-2041(9)	-234(13-14)
	339	-2175(12-13)	152(13-14)	1005(12-13)	-22(13-14)	-2042(9)	-101(13-14)
8007	339	-1959(6)	-128(13-14)	1404(3)	-22(13-14)	1478(12-14)	43(13-14)
	340	-1940(6)	-128(13-14)	1464(12-13)	-15(9)	1478(12-14)	38(13-14)
8007	340	-2381(6)	40(13-14)	1634(12-13)	-15(9)	2206(10)	-75(13-14)
	318	-2502(6)	40(13-14)	-1864(3)	-3(13-14)	4025(3)	-79(13-14)
8008	318	-5389(6)	-264(8)	-1864(3)	-3(13-14)	1858(12-13)	516(8)
	121	-4915(6)	-264(8)	-152(13)	-3(13-14)	1858(12-13)	516(8)
8008	121	-4592(6)	94(13-14)	-1377(3)	-2(13-14)	1858(12-13)	510(8)
	122	-4212(6)	94(13-14)	-1024(3)	-2(13-14)	-1710(8)	633(9)
8008	122	-4303(6)	197(13-14)	-967(3)	-2(13-14)	-1711(8)	650(9)
	123	-3853(6)	197(13-14)	-615(8)	-2(13-14)	-3025(8)	524(9)
8008	123	-3491(6)	-116(13-14)	-731(12-13)	3(13-14)	-3027(8)	557(9)
	124	-3212(13-14)	-116(13-14)	-574(12-13)	3(13-14)	-3690(8)	465(9)
8008	124	-3364(6)	132(9)	-616(12-13)	3(8)	-3701(8)	513(9)
	125	-3006(6)	132(9)	652(12-13)	3(8)	-3712(8)	-462(13-14)
8008	125	-2756(6)	-246(13-14)	525(12-13)	7(13-14)	-3714(8)	-520(13-14)
	221	-2500(13-14)	-246(13-14)	688(12-13)	7(13-14)	-3283(9)	250(8)
8008	221	-2868(6)	-163(13-14)	615(13-14)	5(13-14)	-3292(9)	314(8)
	222	-2650(6)	-163(13-14)	937(6)	5(13-14)	-2651(9)	171(8)
8008	222	-2661(6)	184(8)	791(3)	-5(13-14)	-2651(9)	234(8)

8008	321	-2530(6)	184(8)	1196(3)	-5(13-14)	-1783(9)	113(13-14)
	321	-2131(6)	87(13-14)	1146(13-14)	10(13-14)	-1782(9)	103(13-14)
8008	322	-2112(6)	87(13-14)	1316(13-14)	10(13-14)	1352(12-13)	39(13-14)
	322	-2254(6)	61(13-14)	1544(13-14)	-16(9)	1352(12-13)	32(13-14)
8009	319	-2578(6)	61(13-14)	1717(13-14)	-16(9)	2087(13-14)	-35(13-14)
	110	-3915(6)	-277(13-14)	-1270(3)	-11(13-14)	2852(3)	103(13-14)
8009	126	-3624(6)	-277(13-14)	-1059(3)	-11(13-14)	1574(12-13)	541(8)
	126	-3460(6)	131(13-14)	-997(3)	-8(13-14)	1574(12-13)	540(8)
8009	127	-3172(6)	131(13-14)	-781(3)	-8(13-14)	-1348(8)	669(9)
	127	-3359(13-14)	138(13-14)	-753(3)	-4(13-14)	-1345(8)	689(9)
8009	128	-3226(13-14)	138(13-14)	-550(8)	-4(13-14)	-2442(8)	546(9)
	128	-3192(13-14)	-103(13-14)	-539(12-13)	6(13-14)	-2438(8)	578(9)
8009	129	-3073(13-14)	-103(13-14)	-428(12-13)	6(13-14)	-3116(8)	469(9)
	129	-2539(13-14)	131(9)	-518(12-13)	6(13-14)	-3115(8)	511(8)
8009	130	-2234(13-14)	131(9)	454(12-13)	6(13-14)	-3413(8)	331(8)
	130	-2252(13-14)	149(8)	533(13-14)	17(13-14)	-3409(8)	378(8)
8009	223	-2267(13-14)	149(8)	647(13-14)	9(13-14)	-3348(8)	178(8)
	223	-1374(12-13)	-117(13-14)	948(13-14)	9(13-14)	-3037(9)	197(8)
8009	224	-1312(12-13)	-117(13-14)	808(13-14)	-5(9)	-3034(9)	247(8)
	224	-1456(12-13)	201(13-14)	925(13-14)	-5(9)	-2404(9)	239(13-14)
8009	323	-1420(12-13)	201(13-14)	999(3)	-8(8)	-2404(9)	228(13-14)
	323	-2320(13-14)	203(13-14)	1249(3)	-8(8)	1683(13-14)	40(13-14)
8009	324	-2315(13-14)	203(13-14)	1373(12-13)	-15(9)	1683(13-14)	40(13-14)
	324	-2312(13-14)	51(13-14)	1493(12-13)	-15(9)	1714(10)	-21(13-14)
8010	320	-2346(13-14)	51(13-14)	5(1)	-5(2)	0	0
	21	-520(11)	12(13-13)	5(6)	0	0	0
8010	26	-520(11)	12(13-13)	5(6)	0	0	0
	26	-249(13-14)	18(8)	5(1)	0	0	0
8010	30	-249(13-14)	18(8)	5(1)	0	0	0
	23	-689(13-12)	10(13-13)	-5(6)	0	0	0
8010	23	-689(13-12)	10(13-13)	-5(6)	0	0	0
	25	-689(13-12)	10(13-13)	-8(8)	0	0	0
8010	24	-955(13-13)	10(8)	8(1)	0	0	0
	23	-955(13-13)	10(8)	8(1)	0	0	0
8010	25	-527(11)	17(13-13)	-5(8)	0	0	0
	21	-527(11)	17(13-13)	-5(6)	0	0	0
8010	26	-689(13-12)	9(13-13)	5(1)	0	0	0
	27	-565(13-14)	-5(13-13)	-5(9)	0	0	0
8010	22	-565(13-13)	-5(13-13)	-5(1)	0	0	0
	22	-565(13-13)	-5(13-13)	-8(1)	0	0	0
8010	28	-402(13-12)	-25(8)	8(5)	0	0	0
	24	-402(13-12)	-25(8)	-5(6)	0	0	0
8010	29	-491(11)	-5(13-13)	5(1)	0	0	0
	27	-491(11)	-5(13-13)	5(1)	0	0	0

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Pilastri

Scenario di calcolo : Set NT SLV A2 STR/GEO									
Asia	N in.		N		Ty		Tz		Mz
	N fin	N in.	N	kg	kg	kg	kg	kg	
1	1	-11714(13-13)	-492(13-13)	-1527(13-11)	5(9)	294(12-11)	-1051(13-11)	587(9)	
	28	-1591(13-13)	-492(13-13)	-1527(13-11)	5(9)	-1250(9)	-1250(9)	587(9)	
1	28	-6633(13-11)	291(9)	-1509(13-11)	-4(8)	-1194(9)	-36(12-11)	599(9)	
	101	-6510(13-11)	291(9)	-1894(6)	-4(8)	-378(13)	-36(12-11)	599(9)	
2	2	-10296(13-13)	-509(13-11)	-1937(2)	-2(8)	2964(12-12)	-1102(13-11)	584(9)	
	24	-10173(13-13)	-509(13-11)	-1862(3)	-2(8)	-1222(9)	-1222(9)	584(9)	
2	24	-6869(6)	312(9)	-1889(3)	3(8)	-1201(9)	-47(8)	596(9)	
	102	-6709(6)	312(9)	-2547(6)	3(8)	-5197(3)	-47(8)	596(9)	
3	3	-7699(6)	-535(13-11)	-1887(2)	0	2835(12-12)	-1160(13-11)	571(9)	
	23	-7539(6)	-535(13-11)	-1813(3)	0	-1261(9)	-1261(9)	571(9)	
3	23	-7526(6)	292(9)	-1806(3)	-1(13-11)	-1260(9)	-46(8)	552(9)	
	103	-7367(6)	292(9)	-2460(6)	-1(13-11)	-4990(3)	-129(13-11)	562(9)	
4	4	-7103(6)	-507(13-11)	-1778(2)	0	2662(12-12)	-129(13-11)	562(9)	
	25	-6944(6)	-507(13-11)	-1670(3)	0	-1239(9)	-1239(9)	562(9)	
4	25	-6934(6)	287(9)	-1694(3)	-1(13-11)	-1240(9)	-46(13-11)	545(9)	
	104	-6735(6)	287(9)	-2345(6)	-1(13-11)	-4710(3)	-1076(13-11)	550(9)	
5	5	-10134(13-11)	-465(13-11)	-1744(2)	0	2639(12-13)	-1076(13-11)	550(9)	
	21	-1001(13-11)	-465(13-11)	-1627(3)	0	-1263(9)	-1263(9)	550(9)	

5	21	-7118(6)	304(8)	-1617(3)	2(8)	-1299(9)	560(9)
105	-6958(6)	304(8)	-2267(6)	2(8)	-458(3)	-651(3-1-4)	0
6	-10338(13-1-3)	451(13-1-3)	-178(2)	-1(13-1-3)	2686(12-1-3)	1082(13-1-4)	0
26	-10215(13-1-3)	451(13-1-3)	-1665(3)	-1(13-1-3)	-1202(9)	543(8)	0
6	-6190(6)	273(9)	-1673(3)	1(12-1-1)	-1237(9)	545(8)	0
106	-6031(6)	273(9)	-2320(6)	1(12-1-1)	-463(8)	531(13-1-3)	0
7	-6746(6)	485(13-1-3)	-1690(2)	0	2631(12-1-3)	1125(13-1-3)	0
29	-6587(6)	485(13-1-3)	-1559(3)	0	-123(9)	552(8)	0
7	-6577(6)	277(9)	-1570(3)	2(8)	-123(9)	542(8)	0
107	-6418(6)	277(9)	-2218(6)	2(8)	-4457(3)	-25(9)	0
8	-6767(6)	491(13-1-3)	-1652(2)	0	2609(12-1-3)	1142(13-1-3)	0
27	-6608(6)	491(13-1-3)	-1506(3)	0	-1274(9)	574(8)	0
8	-6598(6)	304(8)	-1522(3)	2(8)	-1274(9)	563(8)	0
108	-6439(6)	304(8)	-2169(6)	2(8)	-4409(3)	-691(3-1-2)	0
9	-9006(13-1-3)	519(13-1-3)	-1469(7)	1(8)	2395(12-1-3)	1157(13-1-3)	0
22	-8883(13-1-3)	519(13-1-3)	-1276(3)	1(8)	-1338(9)	578(8)	0
9	-5939(6)	311(8)	-1302(3)	1(8)	-134(9)	586(8)	0
109	-5780(6)	311(8)	-1950(6)	1(8)	-4036(3)	-951(13-1-3)	0
10	-10699(13-1-3)	535(13-1-3)	-1155(7)	1(13-1-4)	2077(12-1-3)	1168(13-1-3)	0
30	-10576(13-1-3)	535(13-1-3)	-1131(13-1-3)	1(13-1-4)	-1255(9)	605(8)	0
10	-5759(13-1-3)	332(8)	-1092(13-1-4)	4(8)	-1256(9)	608(8)	0
110	-5637(13-1-3)	332(8)	-1423(10)	4(8)	-2859(3)	1001(13-1-3)	0
211	-2001(3)	-741(13-1-4)	2924(13-1-1)	0	3035(13-1-1)	-969(13-1-4)	0
311	-1892(3)	-741(13-1-4)	2924(13-1-1)	0	1914(10)	751(13-1-4)	0
212	-2457(3)	-745(13-1-4)	2685(6)	0	-2895(12-1-1)	-1005(13-1-4)	0
312	-2347(3)	-745(13-1-4)	2455(12-1-1)	0	2340(13-1-1)	441(13-1-1)	0
213	-2572(3)	-736(13-1-4)	2841(6)	-1(13-1-1)	-2536(12-1-1)	-1047(13-1-4)	0
313	-2462(3)	-736(13-1-4)	2578(6)	-1(13-1-1)	2357(10)	411(13-1-4)	0
214	-2611(3)	-768(13-1-4)	2721(6)	-1(13-1-1)	-2160(12-1-4)	-1077(13-1-4)	0
314	-2501(3)	-768(13-1-4)	2585(6)	-1(13-1-1)	2346(10)	49(6)	0
215	-2491(3)	-809(13-1-4)	2585(6)	-1(13-1-1)	2272(12-1-4)	-1095(13-1-4)	0
315	-2381(3)	-809(13-1-4)	2322(6)	-1(13-1-1)	2303(10)	431(13-1-4)	0
216	-2666(3)	847(13-1-4)	2650(6)	-1(13-1-1)	2333(12-1-4)	1128(13-1-4)	0
316	-2557(3)	847(13-1-4)	2398(12-1-4)	-1(13-1-1)	2326(10)	-601(13-1-4)	0
217	-2547(3)	793(13-1-4)	2573(6)	-1(13-1-1)	2285(12-1-3)	1110(13-1-1)	0
317	-2437(3)	793(13-1-4)	2345(12-1-4)	-1(13-1-1)	2260(10)	-21(13-1-1)	0
218	-2516(3)	744(13-1-4)	2422(6)	0	2205(10)	1079(13-1-4)	0
318	-2406(3)	744(13-1-4)	2422(6)	0	-2320(12-1-3)	1058(13-1-4)	0
219	-2195(3)	768(13-1-4)	2394(6)	0	-2169(12-1-3)	1058(13-1-4)	0
319	-2086(3)	768(13-1-4)	2134(12-1-3)	0	2097(13-1-4)	541(13-1-4)	0
220	-1937(3)	771(13-1-4)	2318(13-1-4)	0	2633(12-1-3)	1029(13-1-4)	0
320	-1827(3)	771(13-1-4)	2318(13-1-4)	0	1714(10)	64(13-1-4)	0

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Aste generiche

Scenario di calcolo : Set NT_SLV_A2_STR/GEO									
Asta	N.in	N	Ty	Tz	Mt	My	Mz		
	N.fin	kg	kg	kg	kg*m	kg*m	kg*m		
7001	1	-2511(13-11-3)	0	-2(1)	0	0	1(8)		
	24	-2508(13-11-3)	0	2(1)	0	0	1(9)		
7002	24	3658(13-11-3)	0	-2(8)	0	0	1(9)		
	101	3661(13-11-3)	0	2(1)	0	0	1(8)		
7003	101	-2107(13-11-3)	0	-2(1)	0	0	0		
	157	-2104(13-11-3)	0	2(1)	0	0	0		
7004	157	778(13-11-4)	0	-2(1)	0	0	0		
	154	781(13-11-4)	0	2(1)	0	0	0		
7005	154	-1369(13-1-4)	0	-2(1)	0	0	0		
	235	-1367(13-1-4)	0	2(1)	0	0	0		
7006	235	1680(13-1-4)	0	-2(1)	0	0	0		
	333	1681(13-1-4)	0	2(1)	0	0	0		
7007	333	476(13-1-1)	0	-2(1)	0	0	0		
	312	476(13-1-1)	0	2(1)	0	0	0		
7008	311	-649(13-1-1)	0	-2(1)	0	0	0		
	335	-649(13-1-1)	0	2(1)	0	0	0		
7009	335	-1823(13-1-4)	0	-2(1)	0	0	0		
	233	-1824(13-1-4)	0	2(1)	0	0	0		
7010	233	1260(13-1-4)	0	-2(1)	0	0	0		

7011	159	1258(13-1-4)	0	2(1)	0	0	0
	159	-624(13-1-4)	0	-2(1)	0	0	0
7012	152	-627(13-1-4)	0	2(1)	0	0	0
	152	2053(13-1-3)	0	-2(1)	0	0	0
7013	102	2050(13-1-3)	0	2(1)	0	0	0
	102	-3760(13-1-3)	0	-2(8)	0	0	1(9)
	28	-3763(13-1-3)	0	2(1)	0	0	2(8)
7014	28	2457(13-1-3)	0	-2(1)	0	0	1(9)
	2	2454(13-1-3)	0	2(1)	0	0	1(8)
7015	107	-1278(13-1-4)	0	-2(1)	0	0	0
	137	-1275(13-1-4)	0	2(1)	0	0	0
7016	137	-1275(13-1-4)	0	-2(1)	0	0	0
	104	-1201(13-1-1)	0	2(1)	0	0	0
7017	104	-1205(13-1-4)	0	-2(1)	0	0	0
	132	-1201(13-1-4)	0	2(1)	0	0	0
7018	132	-1837(13-1-4)	0	-2(1)	0	0	0
	106	-1840(13-1-4)	0	2(1)	0	0	0
7019	106	-1268(13-1-4)	0	-2(1)	0	0	0
	162	-1264(13-1-4)	0	2(1)	0	0	0
7020	162	-1008(13-1-4)	0	-2(1)	0	0	0
	108	-1011(13-1-4)	0	2(1)	0	0	0
7021	108	-1091(13-1-4)	0	-2(1)	0	0	0
	122	-1087(13-1-4)	0	2(8)	0	0	0
7022	122	-1601(13-1-3)	0	-2(8)	0	0	0
	110	-1605(13-1-3)	0	2(1)	0	0	0
7023	110	3130(13-1-3)	0	0	0	0	1(8)
	22	3127(13-1-3)	0	0	0	0	1(8)
7024	22	-2043(13-1-3)	0	0	0	0	1(9)
	10	-2046(13-1-3)	0	0	0	0	1(8)
7025	9	1926(13-1-3)	0	0	0	0	1(8)
	30	1929(13-1-3)	0	0	0	0	1(9)
7026	30	-3356(13-1-3)	0	0	0	0	1(8)
	109	-3353(13-1-3)	0	0	0	0	1(9)
7027	109	-1507(13-1-3)	0	-2(1)	0	0	0
	127	-1504(13-1-3)	0	2(1)	0	0	0
7028	127	-479(13-1-4)	0	-2(2)	0	0	0
	124	-476(13-1-4)	0	2(1)	0	0	0
7029	124	1075(13-1-4)	0	-2(1)	0	0	0
	223	1077(13-1-4)	0	2(1)	0	0	0
7030	223	-1612(13-1-4)	0	-2(1)	0	0	0
	321	-1611(13-1-4)	0	2(1)	0	0	0
7031	321	-571(6)	0	-2(1)	0	0	0
	320	-571(6)	0	2(1)	0	0	0
7032	319	425(13-1-4)	0	-2(1)	0	0	0
	323	425(13-1-4)	0	2(1)	0	0	0
7033	323	1510(13-1-4)	0	-2(1)	0	0	0
	221	1509(13-1-4)	0	2(8)	0	0	0
7034	221	-1200(13-1-4)	0	-2(1)	0	0	0
	129	-1202(13-1-4)	0	2(1)	0	0	0
7035	129	-632(13-1-4)	0	-2(1)	0	0	0
	122	-635(13-1-4)	0	2(1)	0	0	0
7036	109	-947(13-1-4)	0	-2(1)	0	0	0
	167	-943(13-1-4)	0	2(1)	0	0	0
7037	167	-1077(13-1-4)	0	-2(1)	0	0	0
	107	-1081(13-1-4)	0	2(1)	0	0	0
7038	107	-1180(13-1-4)	0	-2(1)	0	0	0
	142	-1176(13-1-4)	0	2(1)	0	0	0
7039	142	-1817(13-1-4)	0	-2(1)	0	0	0
	105	-1820(13-1-4)	0	2(1)	0	0	0
7040	105	-1241(13-1-4)	0	-2(1)	0	0	0
	147	-1238(13-1-4)	0	2(8)	0	0	0
7041	147	1102(13-1-4)	0	-2(1)	0	0	0
	103	1099(13-1-4)	0	2(1)	0	0	0
7042	103	-1384(13-1-4)	0	-2(1)	0	0	0
	157	-1381(13-1-4)	0	2(1)	0	0	0
7043	312	-1330(13-1-4)	0	-2(1)	0	0	0
	327	-1330(13-1-4)	0	2(1)	0	0	0

7044	327	-1296(13-14)	0	-2(1)	0	0	0	0	0
	314	-1297(13-14)	0	2(1)	0	0	0	0	0
7045	314	-1435(13-II-4)	0	-2(1)	0	0	0	0	0
	325	-1435(13-II-4)	0	2(8)	0	0	0	0	0
7046	325	-399(8)	0	-2(1)	0	0	0	0	0
	316	-399(8)	0	2(1)	0	0	0	0	0
7047	316	-1231(13-II-4)	0	-2(2)	0	0	0	0	0
	337	-1231(13-II-4)	0	2(1)	0	0	0	0	0
7048	337	-1265(13-I-4)	0	-2(1)	0	0	0	0	0
	318	-1265(13-I-4)	0	2(8)	0	0	0	0	0
7049	318	-1402(13-II-4)	0	-2(1)	0	0	0	0	0
	321	-1401(13-II-4)	0	2(1)	0	0	0	0	0
7050	319	-1172(13-I-4)	0	-2(1)	0	0	0	0	0
	339	-1172(13-I-4)	0	2(1)	0	0	0	0	0
7051	339	-1337(13-II-4)	0	-2(1)	0	0	0	0	0
	317	-1337(13-II-4)	0	2(1)	0	0	0	0	0
7052	317	-1416(13-I-4)	0	-2(1)	0	0	0	0	0
	329	-1416(13-I-4)	0	2(1)	0	0	0	0	0
7053	329	-413(13-I-1)	0	-2(1)	0	0	0	0	0
	315	-414(13-I-1)	0	2(1)	0	0	0	0	0
7054	315	-1173(13-I-4)	0	-2(1)	0	0	0	0	0
	331	-1173(13-I-4)	0	2(1)	0	0	0	0	0
7055	331	-1238(13-II-4)	0	-2(1)	0	0	0	0	0
	313	-1239(13-II-4)	0	2(1)	0	0	0	0	0
7056	313	-1634(13-I-4)	0	-2(1)	0	0	0	0	0
	335	-1634(13-I-4)	0	2(8)	0	0	0	0	0
7057	132	-804(13-II-4)	0	-2(1)	0	0	0	0	0
	144	-801(13-II-4)	0	2(8)	0	0	0	0	0
7058	144	1105(13-I-4)	0	-2(1)	0	0	0	0	0
	225	1107(13-I-4)	0	2(1)	0	0	0	0	0
7059	225	-1992(13-I-4)	0	-2(1)	0	0	0	0	0
	329	-1991(13-I-4)	0	2(1)	0	0	0	0	0
7060	325	2051(13-I-4)	0	-2(8)	0	0	0	0	0
	229	2050(13-I-4)	0	2(1)	0	0	0	0	0
7061	229	1063(13-II-4)	0	-2(1)	0	0	0	0	0
	134	1061(13-II-4)	0	2(8)	0	0	0	0	0
7062	134	818(13-II-4)	0	-2(1)	0	0	0	0	0
	142	815(13-II-4)	0	2(1)	0	0	0	0	0
7063	106	-3186(13-II-3)	0	0	0	0	0	0	1(9)
	21	-3189(13-II-3)	0	0	0	0	0	0	1(8)
7064	21	-1983(13-I-3)	0	0	0	0	0	0	1(9)
	6	-1986(13-I-3)	0	0	0	0	0	0	1(8)
7065	5	-1941(13-II-3)	0	0	0	0	0	0	1(8)
	26	-1938(13-II-3)	0	0	0	0	0	0	1(9)
7066	26	-3244(13-I-3)	0	0	0	0	0	0	1(8)
	105	-3241(13-I-3)	0	0	0	0	0	0	1(9)

VERIFICHE STATO LIMITE ULTIMO

Verifica delle travi

Scenario di calcolo : **Set.NT.SLV.A2.STR/CEO**

Trave di Fond. : 9007 I 1, 2 I Pilastrate I 1, 2 I													
Sez. R: By= 60.0 cm Bz=100.0 cm L=149.5 cm Ln=149.5 cm Terreno: <i>Terrenol</i>													
Criterio : <i>CLS.TraviFondazione - Verifica a flessione -Verificato</i>													
X	M-	M+	AM-	AM+	Af-	Af+	Mr-	Mr+	C-	C+			
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m					
ILN	1218	1007	5825	4068	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3			
14.9	3449	2459	5207	3955	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3			
CAMP	13433	11742	1399	2590	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3			
134.5	14199	13032	633	1301	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3			
FLN	14832	14333	--	--	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3			

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
14.9	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
CAMP	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
134.5	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
FLN	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)-II-2

Sez	Td	VRds	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin	15726	--	125983	88071	88071		0	42365	149.5	5.60
Des										

Trave di Fond. : 9007 I 2, 3 I Pilastrate I 2, 3 I

Sez. R: By= 60.0 cm Bz=100.0 cm L=150.1 cm Ln=150.1 cm Terreno: *Terrenol*

Criterio : *CLS.TraviFondazione - Verifica a flessione -Verificato*

X	M-	M+	AM-	AM+	Af-	Af+	Mr-	Mr+	C-	C+		
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m				
ILN	16114	15370	--	--	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3		
15.0	15335	14664	779	707	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3		
CAMP	14444	13980	1671	1390	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3		
135.1	5695	10126	4048	1361	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3		
FLN	4171	9739	4224	1235	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3		

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
15.0	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
CAMP	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
135.1	19.3	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
FLN	19.3	95.9	0.201	19.4	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)-VI-2

Sez	Td	VRds	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin	10856	--	125983	87686	87686		0	42365	150.1	8.08
Des										

Trave di Fond. : 9007 I 3, 4 I Pilastrate I 3, 4 I

Sez. R: By= 60.0 cm Bz=100.0 cm L=88.9 cm Ln=88.9 cm Terreno: *Terrenol*

Criterio : *CLS.TraviFondazione - Verifica a flessione -Verificato*

X	M-	M+	AM-	AM+	Af-	Af+	Mr-	Mr+	C-	C+		
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m				
ILN	5395	10723	--	--	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3		
8.9	4728	10237	667	486	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3		
CAMP	2659	8911	2735	1811	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3		
80.0	-2064	6063	4623	2792	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3		
FLN	-2587	6063	4445	2465	12.06	12.06	42365	42365	(12+13)-II-2	(12+13)-II-3		

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
8.9	19.3	95.9	0.201	19.3	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.202	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
80.0	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.
FLN	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	(12+13)-II-2	(12+13)-II-3	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)-II-2

Sez	Td	VRds	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin	10044	--	125983	79240	79240		0	42365	88.9	7.89

Sez	Des	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
								42365			

Trave di Fond. : 9007 [4 , 5] Pilastrate [4 , 5]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.4 cm Terreno: **Terreno I**

Criterio : CLS TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alis	Alfi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	8217	--	342	12.06	12.06	42365	42365	1	(12+13)>V-1	4.95
8.9	--	8159	--	671	12.06	12.06	42365	42365	1	(12+13)>V-1	4.80
CAMP	342	9605	385	882	12.06	12.06	42365	42365	(12+13)>V-3	(12+13)>V-2	4.04
80.5	533	10030	194	457	12.06	12.06	42365	42365	(12+13)>V-3	(12+13)>V-2	4.04
FLN	727	10487	--	--	12.06	12.06	42365	42365	(12+13)>V-3	(12+13)>V-2	4.04

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	19.3	95.9	0.201	42365	42365	1	(12+13)>V-1	--	Parz.
8.9	--	--	--	19.3	95.9	0.201	42365	42365	1	(12+13)>V-2	--	Parz.
CAMP	19.2	95.9	0.200	19.3	95.9	0.202	42365	42365	(12+13)>V-3	(12+13)>V-2	Parz.	Parz.
80.5	19.2	95.9	0.200	19.3	95.9	0.202	42365	42365	(12+13)>V-3	(12+13)>V-2	Parz.	Parz.
FLN	19.2	95.9	0.200	19.3	95.9	0.202	42365	42365	(12+13)>V-3	(12+13)>V-2	Parz.	Parz.

Verifica a taglio:cof(0) =2.500

Comb =(12+13)-II-2

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	8641	--	125983	78583	78583	0	42365	89.4	9.31	9.09
Des							42365			

Trave di Fond. : 9007 [5 , 6] Pilastrate [5 , 6]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.3 cm Terreno: **Terreno I**

Criterio : CLS TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alis	Alfi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	169	9863	--	--	12.06	12.06	42365	42365	(12+13)>V-3	(12+13)>V-2	4.30
8.9	-1554	7962	1723	1901	12.06	12.06	42365	42365	(12+13)>V-3	(12+13)>V-2	4.30
CAMP	-1460	7694	1629	2169	12.06	12.06	42365	42365	(12+13)>V-3	(12+13)>V-2	4.30
80.4	-416	8717	436	446	12.06	12.06	42365	42365	(12+13)>V-4	(12+13)>V-2	4.62
FLN	--	8683	--	352	12.06	12.06	42365	42365	1	(12+13)>V-1	4.69

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.2	95.9	0.200	19.3	95.9	0.202	42365	42365	(12+13)>V-3	(12+13)>V-2	Parz.	Parz.
8.9	19.2	95.9	0.200	19.3	95.9	0.202	42365	42365	(12+13)>V-3	(12+13)>V-2	Parz.	Parz.
CAMP	19.2	95.9	0.200	19.3	95.9	0.202	42365	42365	(12+13)>V-3	(12+13)>V-2	Parz.	Parz.
80.4	19.2	95.9	0.200	19.3	95.9	0.202	42365	42365	(12+13)>V-4	(12+13)>V-1	Parz.	Parz.
FLN	--	--	--	19.3	95.9	0.202	42365	42365	1	(12+13)>V-1	--	Parz.

Verifica a taglio:cof(0) =2.500

Comb =8

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	4914	--	125983	78697	78697	0	42365	89.3	9.32	16.0
Des							42365			

Trave di Fond. : 9007 [6 , 7] Pilastrate [6 , 7]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.2 cm Terreno: **Terreno I**

Criterio : CLS TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alis	Alfi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	-449	8784	493	--	12.06	12.06	42365	42365	(12+13)>V-4	(12+13)>V-1	4.82
8.8	-399	8426	631	357	12.06	12.06	42365	42365	(12+13)>V-4	(12+13)>V-1	4.82
CAMP	365	7677	855	1107	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V-1	4.82
79.3	786	7440	434	307	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V-2	5.47
FLN	1220	7747	--	--	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V-2	5.47

589

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	(12+13)>V-4	(12+13)>V-1	Parz.	Parz.
8.8	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	(12+13)>V-4	(12+13)>V-1	Parz.	Parz.
CAMP	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	(12+13)>V1-3	(12+13)>V-1	Parz.	Parz.
79.3	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
FLN	19.2	95.9	0.200	19.3	95.9	0.201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.

Verifica a taglio:cof(0) =2.500

Comb =(12+13)-II-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin	9253	--	125983	78851	78851	0	42365	88.2	9.34	8.52
Des							42365			

Trave di Fond. : 9007 [7 , 8] Pilastrate [7 , 8]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.4 cm Terreno: **Terreno I**

Criterio : CLS TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alis	Alfi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	365	7015	3230	788	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	5.43
8.9	1032	7103	3200	948	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	5.26
CAMP	5522	8644	1107	665	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	4.55
80.5	6092	9699	537	340	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	4.55
FLN	6629	9309	--	--	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	4.55

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
8.9	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.202	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
80.5	19.3	95.9	0.201	19.3	95.9	0.202	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.202	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.

Verifica a taglio:cof(0) =2.500

Comb =(12+13)-II-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin	9930	--	125983	78770	78770	0	42365	89.4	9.33	7.93
Des							42365			

Trave di Fond. : 9007 [8 , 9] Pilastrate [8 , 9]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.6 cm Terreno: **Terreno I**

Criterio : CLS TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alis	Alfi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5432	8328	3149	606	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	4.74
9.0	6163	8427	2943	671	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	4.65
CAMP	10074	9491	648	404	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	3.95
80.6	10427	9688	294	207	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	3.95
FLN	10721	9894	--	--	12.06	12.06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	3.95

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
9.0	19.3	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
CAMP	19.3	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
80.6	19.3	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
FLN	19.3	95.9	0.202	19.3	95.9	0.202	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.

Verifica a taglio:cof(0) =2.500

Comb =(12+13)-II-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg		kg	cm	cmq/m	
Sin										
Des										

590

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
Sin	8961	--	125983	78400	78400	0	42365	89.6	9.29	8.75
Des							42365			

Trave di Fond. : 9007 | 9. 10 | Piastrate [9. 10]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.0 cm Ln= 89.0 cm Terreno: Terreno I

Criterio : CLS Travifondazione - Verifica a flessione : Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	cmq	kg*m	kg*m			
ILN	9477	8903	--	--	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	4.47
8.9	8987	8083	490	821	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	4.47
CAMP	7115	5667	2327	3237	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	4.47
80.1	2454	1767	4546	3782	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.05
FLN	1261	1002	4958	3757	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.81

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.
8.9	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.
CAMP	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.
80.1	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.

Verifica a taglio: cot(0) = 2.500

Comb = (12+13)-II-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
Sin	13952	--	125983	79129	79129	0	42365	89.0	9.37	5.67
Des							42365			

Trave di Fond. : 9008 | 211. 212 | Piastrate [211. 212]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.5 cm Ln= 149.5 cm Terreno: Terreno I

Criterio : CLS Travifondazione - Verifica a flessione : Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	cmq	kg*m	kg*m			
ILN	1162	1103	--	--	12.06	12.06	42365	42365	(12+13)-IV-2	(12+13)-IV-3	36.5
14.9	1243	959	--	144	12.06	12.06	42365	42365	(12+13)-IV-2	(12+13)-IV-3	34.1
CAMP	1283	815	--	288	12.06	12.06	42365	42365	(12+13)-IV-2	(12+13)-IV-3	33.0
134.5	627	215	417	271	12.06	12.06	42365	42365	(12+13)-IV-2	(12+13)-I-1	40.6
FLN	1036	486	--	--	12.06	12.06	42365	42365	(12+13)-I-4	(12+13)-I-1	40.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-IV-2	(12+13)-IV-3	Parz.
14.9	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-IV-2	(12+13)-IV-3	Parz.
CAMP	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-IV-2	(12+13)-IV-3	Parz.
134.5	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-IV-2	(12+13)-I-1	Parz.
FLN	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-I-4	(12+13)-I-1	Parz.

Verifica a taglio: cot(0) = 2.500

Comb = (12+13)-III-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
Sin	2420	--	125983	87956	87956	0	42365	149.5	10.42	36.4
Des							42365			

Trave di Fond. : 9008 | 212. 213 | Piastrate [212. 213]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.5 cm Ln= 149.5 cm Terreno: Terreno I

Criterio : CLS Travifondazione - Verifica a flessione : Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	cmq	kg*m	kg*m			
ILN	1116	923	605	--	12.06	12.06	42365	42365	(12+13)-IV-4	(12+13)-IV-3	24.6
14.9	1605	442	176	481	12.06	12.06	42365	42365	(12+13)-IV-4	(12+13)-IV-3	23.8
CAMP	2328	1684	363	677	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	15.7
134.5	2509	2006	182	355	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	15.7

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X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
FLN	2692	2361	--	--	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	15.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-IV-4	(12+13)-IV-3	Parz.
14.9	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-IV-4	(12+13)-IV-3	Parz.
CAMP	19.2	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.
134.5	19.2	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.
FLN	19.2	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.

Verifica a taglio: cot(0) = 2.500

Comb = (12+13)-V-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
Sin	2656	--	125983	88071	88071	0	42365	149.5	10.43	33.2
Des							42365			

Trave di Fond. : 9008 | 213. 214 | Piastrate [213. 214]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.2 cm Ln= 149.2 cm Terreno: Terreno I

Criterio : CLS Travifondazione - Verifica a flessione : Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	cmq	kg*m	kg*m			
ILN	2770	2381	543	343	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	12.8
14.9	2959	2471	539	428	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	12.1
CAMP	4219	3888	310	621	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	9.35
134.2	4379	4188	150	320	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	9.35
FLN	4529	4508	--	--	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	9.35

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	19.2	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.
14.9	19.2	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.
134.2	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.

Verifica a taglio: cot(0) = 2.500

Comb = (12+13)-VII-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
Sin	2423	--	125983	81768	81768	0	42365	149.2	9.68	33.7
Des							42365			

Trave di Fond. : 9008 | 214. 215 | Piastrate [214. 215]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.4 cm Ln= 149.4 cm Terreno: Terreno I

Criterio : CLS Travifondazione - Verifica a flessione : Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	cmq	kg*m	kg*m			
ILN	4513	4444	465	232	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	8.51
14.9	4683	4505	438	289	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	8.27
CAMP	5605	5477	165	437	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	7.16
134.5	5694	5687	76	226	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	7.16
FLN	5770	5913	--	--	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	7.16

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.
14.9	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.
134.5	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.

Verifica a taglio: cot(0) = 2.500

Comb = (12+13)-VII-2

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Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg		kg* ^m	cm	cmq/m	
Sin	1859	--	125983	81612	81612	0	42365	149.4	9.67	43.9
Des							42365			

Trave di Fond. : 9008 | 215, 216 | Piastrate [215, 216]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.5 cm Ln=149.5 cm Terreno: *Terreno I*

Criterio : CLS Travifondazione - Verifica a flessione - *Verificato*

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr+	Mr-	C-	C+	Stato+
cm	kg* ^m	kg* ^m	kg* ^m	kg* ^m	cmq	cmq	kg* ^m	kg* ^m			CS
--	5748	5872	194	--	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	7.13
ILN	14.9	5823	174	51	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	7.06
CAMP	6160	6071	39	269	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	6.68
I34.5	6184	6195	15	145	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	6.68
FLN	6199	6340	--	--	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	6.68

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
ILN	14.9	19.3	95.9	0.201	19.3	95.9	0.201	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
I34.5	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.

Verifica a taglio: cot(θ) = 2.500

Comb = (12+13)-IV-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg		kg* ^m	cm	cmq/m	
Sin	2445	--	125983	81551	81551	0	42365	149.5	9.66	33.4
Des							42365			

Trave di Fond. : 9008 | 216, 217 | Piastrate [216, 217]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.7 cm Ln=149.7 cm Terreno: *Terreno I*

Criterio : CLS Travifondazione - Verifica a flessione - *Verificato*

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr+	Mr-	C-	C+	Stato+
cm	kg* ^m	kg* ^m	kg* ^m	kg* ^m	cmq	cmq	kg* ^m	kg* ^m			CS
ILN	6041	6200	--	--	12.06	12.06	42365	42365	(12+13)-V-4	(12+13)-V-1	6.83
ILN	15.0	6055	6064	--	136	12.06	42365	42365	(12+13)-V-4	(12+13)-V-1	6.83
CAMP	6055	5943	--	257	12.06	12.06	42365	42365	(12+13)-V-4	(12+13)-V-1	6.83
I34.8	5706	5572	217	62	12.06	12.06	42365	42365	(12+13)-V-4	(12+13)-V-1	7.15
FLN	5604	5579	256	21	12.06	12.06	42365	42365	(12+13)-V-4	(12+13)-V-1	7.23

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-V-4	(12+13)-V-1	Parz.	Parz.
ILN	15.0	19.3	95.9	0.201	19.3	95.9	0.201	42365	(12+13)-V-4	(12+13)-V-1	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-V-4	(12+13)-V-1	Parz.	Parz.
I34.8	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-V-4	(12+13)-V-1	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-V-4	(12+13)-V-1	Parz.	Parz.

Verifica a taglio: cot(θ) = 2.500

Comb = (12+13)-IV-3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg		kg* ^m	cm	cmq/m	
Sin	1745	--	125983	88186	88186	0	42365	149.7	10.44	50.5
Des							42365			

Trave di Fond. : 9008 | 217, 218 | Piastrate [217, 218]

Sez. R: By= 60.0 cm Bz=100.0 cm L=148.9 cm Ln=148.9 cm Terreno: *Terreno I*

Criterio : CLS Travifondazione - Verifica a flessione - *Verificato*

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr+	Mr-	C-	C+	Stato+
cm	kg* ^m	kg* ^m	kg* ^m	kg* ^m	cmq	cmq	kg* ^m	kg* ^m			CS
ILN	5478	5493	--	--	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	7.71
ILN	14.9	5374	5227	103	266	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	7.71

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X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr+	Mr-	C-	C+	Stato+
CAMP	5257	4976	221	517	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	7.71
I34.0	4138	3725	517	401	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	9.10
FLN	3943	3629	541	339	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	9.45

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
ILN	14.9	19.3	95.9	0.201	19.3	95.9	0.201	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
I34.0	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.

Verifica a taglio: cot(θ) = 2.500

Comb = (12+13)-IV-1

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg		kg* ^m	cm	cmq/m	
Sin	2111	--	125983	82055	82055	0	42365	148.9	9.72	38.9
Des							42365			

Trave di Fond. : 9008 | 218, 219 | Piastrate [218, 219]

Sez. R: By= 60.0 cm Bz=100.0 cm L=150.0 cm Ln=150.0 cm Terreno: *Terreno I*

Criterio : CLS Travifondazione - Verifica a flessione - *Verificato*

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr+	Mr-	C-	C+	Stato+
cm	kg* ^m	kg* ^m	kg* ^m	kg* ^m	cmq	cmq	kg* ^m	kg* ^m			CS
ILN	3818	3550	--	--	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	11.1
ILN	15.0	3609	3171	209	379	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	11.1
CAMP	3395	2817	423	734	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	11.1
I35.0	1261	584	1244	1096	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	16.9
FLN	1668	553	620	899	12.06	12.06	42365	42365	(12+13)-VII-4	(12+13)-VII-1	18.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
ILN	15.0	19.3	95.9	0.201	19.2	95.9	0.201	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
I35.0	19.2	95.9	0.201	19.2	95.9	0.200	42365	42365	(12+13)-VII-4	(12+13)-VII-1	Parz.	Parz.
FLN	19.2	95.9	0.201	19.2	95.9	0.200	42365	42365	(12+13)-V-1	(12+13)-V-1	Parz.	Parz.

Verifica a taglio: cot(θ) = 2.500

Comb = (12+13)-VII-1

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg		kg* ^m	cm	cmq/m	
Sin	2778	--	125983	88014	88014	0	42365	150.0	10.42	31.7
Des							42365			

Trave di Fond. : 9008 | 219, 220 | Piastrate [219, 220]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.3 cm Ln=149.3 cm Terreno: *Terreno I*

Criterio : CLS Travifondazione - Verifica a flessione - *Verificato*

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr+	Mr-	C-	C+	Stato+
cm	kg* ^m	kg* ^m	kg* ^m	kg* ^m	cmq	cmq	kg* ^m	kg* ^m			CS
ILN	1538	1004	--	--	12.06	12.06	42365	42365	(12+13)-VII-1	(12+13)-VII-1	27.5
ILN	14.9	1543	661	--	343	12.06	42365	42365	8	(12+13)-VII-1	27.5
CAMP	1352	859	187	304	12.06	12.06	42365	42365	8	(12+13)-IV-2	27.5
I34.4	1327	1014	--	149	12.06	12.06	42365	42365	(12+13)-IV-3	(12+13)-IV-2	31.9
FLN	1263	1164	--	--	12.06	12.06	42365	42365	(12+13)-IV-3	(12+13)-IV-2	33.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg* ^m	kg* ^m			Stato+
ILN	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	8	(12+13)-VII-1	Parz.
ILN	14.9	19.2	95.9	0.200	19.2	95.9	0.200	42365	8	(12+13)-VII-1	Parz.
CAMP	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	8	(12+13)-IV-2	Parz.
I34.4	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-IV-3	(12+13)-IV-2	Parz.
FLN	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-IV-3	(12+13)-IV-2	Parz.

594

Verifica a taglio cot(θ)=2,500

Comb = (12+13)·VII-1

Sez	Td	VRdhs	VRcd	VRsd	Vrd	Trl	Mr	Dx	Stafle	C/S
		kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	2722	--	125983	81649	81649	0	42365	149.3	9.67	30.0
Des							42365			

Verifica Stabilità aste Metalliche

Scenario di calcolo : Set_NT_SLV_A2_STR/GEO

Asta : I [1 , 28]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq; **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								
-13164	3102	-1146	211298	20492	9673	20	34	0.988	0.902	--	0.542	0.379	0.325
													0.632

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
I	Y	13164	1681	435	198864	19516	9213	(12+13)·IV-2	5.01
I	Z	13164	1009	724	181583	19516	9213	(12+13)·IV-2	4.93

Asta : I [28 , 101]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq; **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								
-6338	-3781	386	211298	20492	9673	20	34	0.988	0.902	--	0.683	0.353	0.410
													0.588

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
I	Y	6338	2581	136	198864	19516	9213	3	5.59
I	Z	6338	1548	227	181583	19516	9213	3	7.20

Asta : 2 [2 , 24]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq; **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								
-11562	2315	1042	211298	20492	9673	20	34	0.988	0.902	--	0.612	0.401	0.367
													0.669

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
I	Y	11562	1416	419	198864	19516	9213	(12+13)·VI-3	5.68
I	Z	11562	850	698	181583	19516	9213	(12+13)·VI-3	5.47

Asta : 2 [24 , 102]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq; **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								
-6566	-5197	383	211298	20492	9673	20	34	0.988	0.902	--	0.668	0.335	0.401
													0.558

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
I	Y	6566	3473	128	198864	19516	9213	3	4.45
I	Z	6566	2084	214	181583	19516	9213	3	6.02

Asta : 3 [3 , 23]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq; **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								
-2292	2894	717	211298	20492	9673	20	34	0.988	0.902	--	0.626	0.405	0.376
													0.675

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
I	Y	2292	1812	291	198864	19516	9213	(12+13)·II-1	7.36
I	Z	2292	1087	484	181583	19516	9213	(12+13)·II-1	8.27

Asta : 3 [23 , 103]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq; **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								
-7271	-4990	363	211298	20492	9673	20	34	0.988	0.902	--	0.668	0.338	0.401
													0.563

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
I	Y	7271	3334	123	198864	19516	9213	3	4.53
I	Z	7271	2001	204	181583	19516	9213	3	6.07

Asta : 4 [4 , 25]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq; **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								
-2552	2102	1170	211298	20492	9673	20	34	0.988	0.902	--	0.580	0.395	0.348
													0.658

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
I	Y	2552	1218	462	198864	19516	9213	(12+13)·II-3	7.97
I	Z	2552	731	770	181583	19516	9213	(12+13)·II-3	7.40

Asta : 4 [25 , 104]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq; **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								
-6695	-4710	345	211298	20492	9673	20	34	0.988	0.902	--	0.668	0.348	0.401
													0.581

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
I	Y	6695	3145	120	198864	19516	9213	3	4.81
I	Z	6695	1887	200	181583	19516	9213	3	6.44

Asta : 5 [5 , 21]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq; **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								
-11205	1010	-1252	211298	20492	9673	20	34	0.988	0.902	--	0.435	0.394	0.261
													0.656

Clis	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*	kg*	kg	kg*	kg*		
I	Y	11205	439	485	198864	19516	9213	(12+13)·VI-2	7.60
I	Z	11205	264	809	181583	19516	9213	(12+13)·VI-2	6.14

Asta : 5 [21 , 105]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq; **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*	kg*	kg	kg*	kg*								
-6874	-4581	349	211298	20492	9673	20	34	0.988	0.902	--	0.672	0.333	0.403
													0.555

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6874	3078	116	198864	19516	9213	3	4.88
1	Z	6874	1847	194	181583	19516	9213	3	6.51

Asta : 6 [6 , 26]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	20	34	0.988	0.902	--	0.474	0.402	0.284
-11564	1949	1241	211298	20492	9673	20	34	0.988	0.902	--	0.474	0.402	0.284

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	11564	924	499	198864	19516	9213	(12+13)+II-3	6.27
1	Z	11564	554	831	181583	19516	9213	(12+13)+II-3	5.49

Asta : 6 [26 , 106]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	20	34	0.988	0.902	--	0.667	0.358	0.400
-5972	-4658	523	211298	20492	9673	20	34	0.988	0.902	--	0.667	0.358	0.400

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5972	3109	116	198864	19516	9213	3	4.95
1	Z	5972	1865	193	181583	19516	9213	3	6.69

Asta : 7 [7 , 29]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	20	34	0.988	0.902	--	0.557	0.391	0.334
-3360	1836	1284	211298	20492	9673	20	34	0.988	0.902	--	0.557	0.391	0.334

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	3360	1023	502	198864	19516	9213	(12+13)+II-3	8.07
1	Z	3360	614	837	181583	19516	9213	(12+13)+II-3	7.10

Asta : 7 [29 , 107]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	20	34	0.988	0.902	--	0.671	0.357	0.403
-6346	-4457	312	211298	20492	9673	20	34	0.988	0.902	--	0.671	0.357	0.403

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	6346	2992	1111	198864	19516	9213	3	5.07
1	Z	6346	1795	186	181583	19516	9213	3	6.80

Asta : 8 [8 , 27]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	20	34	0.988	0.902	--	0.541	0.392	0.325
-3173	1720	1297	211298	20492	9673	20	34	0.988	0.902	--	0.541	0.392	0.325

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	3173	931	509	198864	19516	9213	(12+13)+II-3	8.41
1	Z	3173	559	848	181583	19516	9213	(12+13)+II-3	7.24

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Asta : 8 [27 , 108]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg	kg	kg	kg*m	kg*m	20	34	0.988	0.902	--	0.677	0.319	0.406
-6368	-4409	318	211298	20492	9673	20	34	0.988	0.902	--	0.677	0.319	0.406

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	6368	2984	101	198864	19516	9213	3	5.10
1	Z	6368	1790	169	181583	19516	9213	3	6.89

Asta : 9 [9 , 22]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg	kg	kg	kg*m	kg*m	20	34	0.988	0.902	--	0.445	0.413	0.267
-9934	1030	-1009	211298	20492	9673	20	34	0.988	0.902	--	0.445	0.413	0.267

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	9934	458	417	198864	19516	9213	(12+13)+VI-2	8.43
1	Z	9934	275	695	181583	19516	9213	(12+13)+VI-2	6.94

Asta : 9 [22 , 109]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg	kg	kg	kg*m	kg*m	20	34	0.988	0.902	--	0.691	0.342	0.415
-5696	-4036	318	211298	20492	9673	20	34	0.988	0.902	--	0.691	0.342	0.415

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	5696	2788	109	198864	19516	9213	3	5.46
1	Z	5696	1673	181	181583	19516	9213	3	7.31

Asta : 10 [10 , 30]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg	kg	kg	kg*m	kg*m	20	34	0.988	0.902	--	0.464	0.383	0.278
-11692	1991	1263	211298	20492	9673	20	34	0.988	0.902	--	0.464	0.383	0.278

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	11692	923	484	198864	19516	9213	(12+13)+IV-3	6.30
1	Z	11692	554	807	181583	19516	9213	(12+13)+IV-3	5.54

Asta : 10 [30 , 110]

Sez. G: HE 240 A L=203.5 cm Ln1=203.5 cm Ln2=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg	kg	kg	kg	kg	20	34	0.988	0.902	--	0.694	0.583	0.416
-6274	-3069	104	211298	20492	9673	20	34	0.988	0.902	--	0.694	0.583	0.416
Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF				
		kg	kg	kg	kg	kg	kg						
1	Y	6274	2128	61	198864	19516	9213	(12+13)+VIII-3	6.79				
1	Z	6274	1277	101	181583	19516	9213	(12+13)+VIII-3	9.01				

Asta : 21 [21 , 311]

Sez. G: HE 240 A L=140.0 cm Ln1=140.0 cm Ln2=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$
kg/cm² ft=4300 kg/cm²**Verificato**

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Clis	Dir	N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg	kg	kg	kg	kg
-1567	3688	-433	211298	20492	9673	14	23	0.972	0.960	--			0.750	0.340	0.450

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.	SF
kg	kg	kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1567	2767	147	195600	19516	9213	(12+13)-I-1	6.03
1	Z	1567	1660	246	193220	19516	9213	(12+13)-I-1	8.35

Asia : 212 [212 . 312]

Sez. G: HE 240 A L=140.0 cm Ln1=140.0 cm Ln2=140.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg	kg	kg	kg	kg	kg
-2566	2864	-996	211298	20492	9673	14	23	0.972	0.960	--	0.925	0.348	0.555

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.	SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg		
1	Y	2566	2649	347	195600	19516	9213	(12+13)-III-2	5.36
1	Z	2566	1589	578	193220	19516	9213	(12+13)-III-2	6.35

Asia : 213 [213 . 313]

Sez. G: HE 240 A L=140.0 cm Ln1=140.0 cm Ln2=140.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg	kg	kg	kg	kg	kg
-1903	2814	-468	211298	20492	9673	14	23	0.972	0.960	--	0.861	0.361	0.517

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.	SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg		
1	Y	1903	2423	169	195600	19516	9213	(12+13)-I-1	6.57
1	Z	1903	1454	282	193220	19516	9213	(12+13)-I-1	8.70

Asia : 214 [214 . 314]

Sez. G: HE 240 A L=140.0 cm Ln1=140.0 cm Ln2=140.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg	kg	kg	kg	kg	kg
-1644	2179	712	211298	20492	9673	14	23	0.972	0.960	--	0.897	0.370	0.538

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.	SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg		
1	Y	1644	1954	263	195600	19516	9213	(12+13)-VI-1	7.29
1	Z	1644	1172	439	193220	19516	9213	(12+13)-VI-1	8.61

Asia : 215 [215 . 315]

Sez. G: HE 240 A L=140.0 cm Ln1=140.0 cm Ln2=140.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg	kg	kg	kg	kg	kg
-2188	2481	910	211298	20492	9673	14	23	0.972	0.960	--	0.883	0.355	0.530

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.	SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg		
1	Y	2188	2192	323	195600	19516	9213	(12+13)-VIII-1	6.31
1	Z	2188	1315	538	193220	19516	9213	(12+13)-VIII-1	7.29

Asia : 216 [216 . 316]

Sez. G: HE 240 A L=140.0 cm Ln1=140.0 cm Ln2=140.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg	kg	kg	kg	kg	kg
-2008	1999	-906	211298	20492	9673	14	23	0.972	0.960	--	0.976	0.349	0.586

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.	SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg		
1	Y	2008	1951	316	195600	19516	9213	(12+13)-VII-2	6.92
1	Z	2008	1171	527	193220	19516	9213	(12+13)-VII-2	7.84

Asia : 217 [217 . 317]

Sez. G: HE 240 A L=140.0 cm Ln1=140.0 cm Ln2=140.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg	kg	kg	kg	kg	kg
-1592	2002	943	211298	20492	9673	14	23	0.972	0.960	--	0.914	0.360	0.549

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.	SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg		
1	Y	1592	1830	339	195600	19516	9213	(12+13)-VIII-1	7.21
1	Z	1592	1098	565	193220	19516	9213	(12+13)-VIII-1	7.94

Asia : 218 [218 . 318]

Sez. G: HE 240 A L=140.0 cm Ln1=140.0 cm Ln2=140.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg	kg	kg	kg	kg	kg
-1638	1995	916	211298	20492	9673	14	23	0.972	0.960	--	0.929	0.369	0.558

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.	SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg		
1	Y	1638	1854	338	195600	19516	9213	(12+13)-VIII-1	7.14
1	Z	1638	1112	563	193220	19516	9213	(12+13)-VIII-1	7.90

Asia : 219 [219 . 319]

Sez. G: HE 240 A L=140.0 cm Ln1=140.0 cm Ln2=140.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg	kg	kg	kg	kg	kg	kg	kg	kg	kg
-2204	2101	898	211298	20492	9673	14	23	0.972	0.960	--	0.987	0.355	0.592

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.	SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg		
1	Y	2204	2074	319	195600	19516	9213	(12+13)-VIII-1	6.57
1	Z	2204	1244	532	193220	19516	9213	(12+13)-VIII-1	7.52

Asia : 220 [220 . 320]

Sez. G: HE 240 A L=140.0 cm Ln1=140.0 cm Ln2=140.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg	kg	kg	kg	kg	kg	kg	kg	kg	kg
-1470	3298	-757	211298	20492	9673	14	23	0.972	0.960	--	0.743	0.343	0.446

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.	SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg		
1	Y	1470	2450	260	195600	19516	9213	(12+13)-VII-2	6.20
1	Z	1470	1470	433	193220	19516	9213	(12+13)-VII-2	7.70

Verifica Resistenza aste Metalliche

Scenario di calcolo : **Set NT SILV_A2_STR/GEO**

Asia : 1 [1 . 28]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq ·**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mz4	Comb.
cm	kg	kg	kg	kg	kg*m	kg*m	kg*m		
0	1	-13164	-530	-1690	4	3102	-1146	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86775	37927	19516	9213	462	22.4	2.87	>100	2.87

Asta : 1 [28 , 101]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
204	1	-7405	-22	-1672	-2	-3687	-10	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
204	1	201236	86948	38003	19516	9213	462	22.7	4.41	>100	4.41

Asta : 2 [2 , 24]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-11562	434	-1141	1	2315	1042	--	--	(12+13)+V1-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87042	38044	19516	9213	462	33.4	3.46	>100	3.46

Asta : 2 [24 , 102]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
204	1	-6406	210	-2356	2	-5197	-44	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
204	1	201236	86957	38007	19516	9213	462	16.1	3.30	>100	3.30

Asta : 3 [3 , 23]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2420	-483	-1198	1	2486	-1048	--	--	(12+13)+III-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87033	38040	19516	9213	462	31.8	3.95	>100	3.95

Asta : 3 [23 , 103]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
204	1	-7111	197	-2273	-0	-4990	-38	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
204	1	201236	87078	38060	19516	9213	462	16.7	3.39	>100	3.39

Asta : 4 [4 , 25]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-3375	-451	-1226	1	2392	-997	--	--	(12+13)+V1I-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87047	38046	19516	9213	462	31.0	4.04	>100	4.04

Asta : 4 [25 , 104]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
204	1	-6536	179	-2162	0	-4710	-20	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
204	1	201236	87085	38063	19516	9213	462	17.6	3.62	>100	3.62

Asta : 5 [5 , 21]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-9168	-411	-1207	-1	2395	-949	--	--	(12+13)+V-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87028	38038	19516	9213	462	31.5	3.69	>100	3.69

Asta : 5 [21 , 105]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
204	1	-6714	192	-2084	2	-4581	-42	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
204	1	201236	86983	38018	19516	9213	462	18.2	3.67	>100	3.67

Asta : 6 [6 , 26]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-11564	516	-1072	-1	1949	1241	--	--	(12+13)+II-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86996	38024	19516	9213	462	35.5	3.42	>100	3.42

Asta : 6 [26 , 106]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
204	1	-5812	161	-2140	1	-4658	-5	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
204	1	201236	87027	38037	19516	9213	462	17.8	3.73	>100	3.73

Asta : 7 [7 , 29]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3360	552	-1031	-1	1836	1284	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87058	38051	19516	9213	462	36.9	4.00	>100	4.00

Asia : 7 [29 , 107]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
204	1	-6186	157	-2037	1	-4457	-7	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
204	1	201236	86989	38021	19516	9213	462	18.7	3.85	>100	3.85

Asia : 8 [8 , 27]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3173	555	-979	-1	1720	1297	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87050	38047	19516	9213	462	38.9	4.09	>100	4.09

Asia : 8 [27 , 108]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
204	1	-6209	184	-1989	2	-4409	-57	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
204	1	201236	86972	38013	19516	9213	462	19.1	3.80	>100	3.80

Asia : 9 [9 , 22]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	6127	584	-867	-0	1513	1309	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87078	38059	19516	9213	462	43.9	4.00	>100	4.00

Asia : 9 [22 , 109]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
204	1	-5536	169	-1770	1	-4036	-27	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
204	1	201236	86999	38025	19516	9213	462	21.5	4.22	>100	4.22

Asia : 10 [10 , 30]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-11692	572	-1227	-0	1991	1263	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87078	38060	19516	9213	462	30.8	3.36	>100	3.36

Asia : 10 [30 , 110]

Sez. G: HE 240 A L=203.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
204	1	-6151	-2	-944	-1	-3069	104	--	--	(12+13)-V/III-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
204	1	201236	87056	38050	19516	9213	462	40.3	5.02	>100	5.02

Asia : 211 [211 , 311]

Sez. G: HE 240 A L=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1403	542	-1942	1	3324	717	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87054	38049	19516	9213	462	19.6	3.92	>100	3.92

Asia : 212 [212 , 312]

Sez. G: HE 240 A L=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
28	1	-2550	-739	-310	-1	2864	-789	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
28	1	201236	87031	38039	19516	9213	462	>100	4.08	>100	4.08

Asia : 213 [213 , 313]

Sez. G: HE 240 A L=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-431	677	2234	-1	-2090	985	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87015	38032	19516	9213	462	17.0	4.63	>100	4.63

Asia : 214 [214 , 314]

Sez. G: HE 240 A L=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1611	593	-549	-1	2151	862	--	--	(12+13)-V/III-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
0	1	201236	87024	38036	19516	9213	462	69.2	4.72	>100	4.72

Asta : 215 [215 , 315]

Sez. G: HE 240 A L=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2188	660	-559	-1	2481	910	--	--	(12+13)-V/III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87035	38041	19516	9213	462	68.0	4.22	>100	4.22

Asta : 216 [216 , 316]

Sez. G: HE 240 A L=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1611	-690	2208	1	-2157	-926	--	--	(12+13)-V/III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87039	38043	19516	9213	462	17.2	4.57	>100	4.57

Asta : 217 [217 , 317]

Sez. G: HE 240 A L=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1592	674	-451	-1	2002	943	--	--	(12+13)-V/III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87037	38042	19516	9213	462	84.3	4.70	>100	4.70

Asta : 218 [218 , 318]

Sez. G: HE 240 A L=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1638	630	-378	-1	1995	916	--	--	(12+13)-V/III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87041	38043	19516	9213	462	>100	4.77	>100	4.77

Asta : 219 [219 , 319]

Sez. G: HE 240 A L=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2204	651	-279	1	1836	898	--	--	(12+13)-V/III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87024	38036	19516	9213	462	>100	4.94	>100	4.94

Asta : 220 [220 , 320]

Sez. G: HE 240 A L=140.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1344	-816	-1780	-1	3161	-1074	--	--	(12+13)-V/III-2

605

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87053	38049	19516	9213	462	21.4	3.51	>100	3.51

Asta : 1001 [101 , 102]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
135	1	-431	-33	134	-0	-22	36	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
135	1	27037	9480	7688	1033	240	27	57.4	5.37	>100	5.37

Asta : 1002 [151 , 156]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
105	1	-157	-27	123	-0	-97	19	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
105	1	27037	9475	7684	1033	240	27	62.4	5.54	>100	5.54

Asta : 1003 [152 , 157]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
120	1	-45	-46	180	-0	-72	29	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
120	1	27037	9476	7685	1033	240	27	42.6	5.15	>100	5.15

Asta : 1004 [153 , 158]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
149	1	10	-57	192	-0	0	49	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9479	7688	1033	240	27	40.0	4.92	>100	4.92

Asta : 1005 [154 , 159]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
149	1	-34	-62	180	-0	0	53	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9481	7689	1033	240	27	42.8	4.51	>100	4.51

Asta : 1006 [155 , 160]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
149	1	-35	-65	166	0	0	58	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9480	7688	1033	240	27	46.3	4.08	>100	4.08

606

Asta : 1007 [233 , 235]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
149	1	-142	-59	152	0	0	57	--	--	9		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9479	7688	1033	240	27	50,6	4,11	>100	4,11

Asta : 1008 [234 , 236]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
150	1	2	-45	140	0	0	49	--	--	9		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
150	1	27037	9479	7687	1033	240	27	54,9	4,86	>100	4,86

Asta : 1009 [333 , 335]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
105	1	74	-14	77	0	-61	21	--	--	8		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
105	1	27037	9478	7687	1033	240	27	99,6	6,76	>100	6,76

Asta : 1010 [334 , 336]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
60	1	70	8	-38	0	-69	18	--	--	8		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
60	1	27037	9479	7688	1033	240	27	>100	6,98	>100	6,98

Asta : 1011 [311 , 312]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
149	1	1170	24	40	-0	0	-18	--	--	(12+13)+IV-3		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9468	7678	1033	240	27	>100	8,53	>100	8,53

Asta : 1012 [156 , 136]

Sez. G: IPE 100 L=150,1 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
75	1	-347	-3	0	0	-117	18	--	--	8		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
75	1	27037	9480	7688	1033	240	27	>100	4,96	>100	4,96

Asta : 1013 [157 , 137]

Sez. G: IPE 100 L=150,0 cm Crit.: Acciaio_Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
90	1	-304	-19	60	0	-109	18	--	--	8		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	27037	9480	7688	1033	240	27	>100	5,18	>100	5,18

Asta : 1014 [158 , 138]

Sez. G: IPE 100 L=149,9 cm Crit.: Acciaio_Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
0	1	385	-67	-111	-0	0	-60	--	--	(12+13)+IV-3		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9476	7685	1033	240	27	69,1	3,77	>100	3,77

Asta : 1015 [159 , 139]

Sez. G: IPE 100 L=149,9 cm Crit.: Acciaio_Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
0	1	852	-73	-104	-0	0	-62	--	--	(12+13)+IV-3		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9472	7681	1033	240	27	73,8	3,45	>100	3,45

Asta : 1016 [160 , 140]

Sez. G: IPE 100 L=149,8 cm Crit.: Acciaio_Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
0	1	73	-89	-96	-0	0	-73	--	--	(12+13)+IV-3		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9470	7680	1033	240	27	79,7	3,27	>100	3,27

Asta : 1017 [235 , 227]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio_Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
0	1	187	-70	-88	-0	0	-54	--	--	(12+13)+IV-3		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9473	7682	1033	240	27	87,1	4,29	>100	4,29

Asta : 1018 [236 , 228]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio_Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
135	1	-41	-40	166	-0	-28	39	--	--	8		

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
135	1	27037	9481	7689	1033	240	27	46,3	5,17	>100	5,17

Asta : 1019 [335 , 327]

Sez. G: IPE 100 L=149,6 cm Crit.: Acciaio_Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato												
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*	kg*					
0	1	-2318	-27	-77	0	0	-22	--	--	(12+13)+IV-3		

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9475	7684	1033	240	27	>100	5.64	>100	5.64

Asta : 1020 [336 , 328]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	89	7	-38	-0	-69	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9480	7689	1033	240	27	>100	6.96	>100	6.96

Asta : 1021 [312 , 313]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
41	1	249	7	-36	-0	-28	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
41	1	27037	9480	7688	1033	240	27	>100	8.87	>100	8.87

Asta : 1022 [102 , 103]

Sez. G: IPE 100 L=150,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	-751	-8	27	0	-59	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9481	7689	1033	240	27	>100	6.35	>100	6.35

Asta : 1023 [137 , 147]

Sez. G: IPE 100 L=100,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
91	1	-259	-29	134	0	-15	29	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
91	1	27037	9479	7687	1033	240	27	57.4	6.92	>100	6.92

Asta : 1024 [138 , 148]

Sez. G: IPE 100 L=107,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	47	-51	173	0	0	44	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	27037	9479	7688	1033	240	27	44.5	5.39	>100	5.39

Asta : 1025 [139 , 149]

Sez. G: IPE 100 L=113,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	39	-55	175	0	0	48	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	27037	9480	7688	1033	240	27	44.0	5.00	>100	5.00

Asta : 1026 [140 , 150]

Sez. G: IPE 100 L=119,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	89	-96	-68	-0	0	-59	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9477	7686	1033	240	27	98.7	3.98	>100	3.98

Asta : 1027 [227 , 231]

Sez. G: IPE 100 L=125,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	46	-93	-66	-0	0	-59	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9477	7686	1033	240	27	>100	4.03	>100	4.03

Asta : 1028 [228 , 232]

Sez. G: IPE 100 L=131,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	-192	-50	166	0	0	49	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9479	7687	1033	240	27	46.2	4.69	>100	4.69

Asta : 1029 [327 , 331]

Sez. G: IPE 100 L=137,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
110	1	70	-19	100	0	-37	24	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
110	1	27037	9479	7687	1033	240	27	77.0	7.17	>100	7.17

Asta : 1030 [328 , 332]

Sez. G: IPE 100 L=143,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	48	7	-36	0	-60	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9480	7688	1033	240	27	>100	7.55	>100	7.55

Asta : 1031 [313 , 314]

Sez. G: IPE 100 L=149,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
64	1	258	4	-19	-0	-41	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
64	1	27037	9480	7688	1033	240	27	>100	8.27	>100	8.27

Asta : 1032 [103 , 104]

Sez. G: IPE 100 L=88,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
89	1	-510	-11	49	-0	0	22	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	27037	9480	7688	1033	240	27	>100	9.13	>100	9.13

Asia : 1033 [136 , 146]

Sez. G: IPE 100 L=94.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
66	1	-485	-12	63	0	-31	19	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
66	1	27037	9479	7688	1033	240	27	>100	7.72	>100	7.72

Asia : 1034 [148 , 133]

Sez. G: IPE 100 L=107.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
107	1	384	-114	67	0	0	79	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	27037	9479	7687	1033	240	27	82.9	2.92	>100	2.92

Asia : 1035 [149 , 134]

Sez. G: IPE 100 L=113.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
113	1	-234	-119	67	-0	0	79	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	27037	9477	7686	1033	240	27	79.4	2.96	>100	2.96

Asia : 1036 [150 , 135]

Sez. G: IPE 100 L=119.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
119	1	153	-132	67	-0	0	86	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
119	1	27037	9474	7683	1033	240	27	71.6	2.73	>100	2.73

Asia : 1037 [231 , 225]

Sez. G: IPE 100 L=125.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
125	1	-591	-95	65	-0	0	59	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	27037	9472	7682	1033	240	27	>100	3.70	>100	3.70

Asia : 1038 [232 , 226]

Sez. G: IPE 100 L=131.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-470	-69	-64	-0	0	-46	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9474	7683	1033	240	27	>100	4.81	>100	4.81

Asia : 1039 [331 , 325]

Sez. G: IPE 100 L=137.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
96	1	-135	-18	64	0	-47	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	27037	9479	7687	1033	240	27	>100	7.20	>100	7.20

Asia : 1040 [332 , 326]

Sez. G: IPE 100 L=143.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
57	1	108	8	-34	0	-58	18	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9480	7689	1033	240	27	>100	7.48	>100	7.48

Asia : 1041 [314 , 315]

Sez. G: IPE 100 L=149.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
60	1	231	5	-19	-0	-34	17	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9480	7688	1033	240	27	>100	8.92	>100	8.92

Asia : 1042 [104 , 105]

Sez. G: IPE 100 L=89.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
89	1	-245	-19	48	-0	0	25	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	27037	9479	7688	1033	240	27	>100	8.84	>100	8.84

Asia : 1043 [147 , 132]

Sez. G: IPE 100 L=101.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
101	1	496	-75	65	0	0	54	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
101	1	27037	9475	7684	1033	240	27	>100	4.11	>100	4.11

Asia : 1044 [146 , 131]

Sez. G: IPE 100 L=95.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq ; Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
95	1	-200	-52	61	0	0	36	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	27037	9474	7683	1033	240	27	>100	6.34	>100	6.34

Asia : 1045 [134 , 144]

Sez. G: IPE 100 L=113,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm			kg	kg	kg	kg*	kg*				
113	1	42	-62	115	-0	0	51	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27037	9480	7689	1033	240	27	67.0	4.64	>100	4.64

Asia : 1046 [135 , 145]

Sez. G: IPE 100 L=119,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	-24	-69	166	-0	0	57	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9480	7688	1033	240	27	46.2	4.17	>100	4.17

Asia : 1047 [225 , 229]

Sez. G: IPE 100 L=125,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	-70	-67	162	0	0	58	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	27037	9481	7689	1033	240	27	47.5	4.10	>100	4.10

Asia : 1048 [226 , 230]

Sez. G: IPE 100 L=131,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
131	1	-159	-53	158	0	0	51	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
131	1	27037	9479	7688	1033	240	27	48.6	4.54	>100	4.54

Asia : 1049 [325 , 329]

Sez. G: IPE 100 L=137,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
110	1	-10	-22	96	0	-35	25	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
110	1	27037	9478	7686	1033	240	27	80.4	7.14	>100	7.14

Asia : 1050 [326 , 330]

Sez. G: IPE 100 L=143,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
72	1	72	4	-0	0	-60	16	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
72	1	27037	9478	7686	1033	240	27	>100	7.76	>100	7.76

Asia : 1051 [315 , 316]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
55	1	122	3	-18	0	-28	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
55	1	27037	9480	7688	1033	240	27	>100	9.76	>100	9.76

Asia : 1052 [132 , 142]

Sez. G: IPE 100 L=101,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	462	86	-63	-0	0	45	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9470	7680	1033	240	27	>100	4.86	>100	4.86

Asia : 1053 [105 , 106]

Sez. G: IPE 100 L=89,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	-119	-107	27	0	0	49	--	--	(12+13)+IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9471	7681	1033	240	27	88.2	4.75	>100	4.75

Asia : 1054 [133 , 143]

Sez. G: IPE 100 L=107,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	95	-58	167	0	0	48	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9480	7689	1033	240	27	46.0	4.94	>100	4.94

Asia : 1055 [131 , 141]

Sez. G: IPE 100 L=95,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
86	1	-615	-29	124	0	-13	28	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
86	1	27037	9480	7688	1033	240	27	61.8	6.52	>100	6.52

Asia : 1056 [145 , 165]

Sez. G: IPE 100 L=119,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	165	-129	-64	-0	0	-84	--	--	(12+13)+IV-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9475	7684	1033	240	27	73.2	2.79	>100	2.79

Asia : 1057 [229 , 237]

Sez. G: IPE 100 L=125,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-240	93	-63	0	0	58	--	--	(12+13)+IV-2	

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X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9473	7682	1033	240	27	>100	3.96	>100	3.96

Asta : 1058 [230 , 238]

Sez. G: IPE 100 L=131,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	-158	-46	107	0	0	46	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9478	7687	1033	240	27	71.9	5.02	>100	5.02

Asta : 1059 [329 , 337]

Sez. G: IPE 100 L=137,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	185	-17	64	0	-46	22	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	27037	9479	7688	1033	240	27	>100	7.11	>100	7.11

Asta : 1060 [330 , 338]

Sez. G: IPE 100 L=143,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	16	9	-34	0	-57	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9481	7689	1033	240	27	>100	7.71	>100	7.71

Asta : 1061 [316 , 317]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	118	5	-20	-40	-33	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9479	7688	1033	240	27	>100	9.27	>100	9.27

Asta : 1062 [141 , 161]

Sez. G: IPE 100 L=95,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-243	52	-60	0	0	37	--	--	(12+13)-II-2	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9477	7686	1033	240	27	>100	6.18	>100	6.18

Asta : 1063 [143 , 163]

Sez. G: IPE 100 L=107,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	264	-113	-64	0	0	-77	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9477	7686	1033	240	27	83.5	3.01	>100	3.01

Asta : 1064 [106 , 107]

Sez. G: IPE 100 L=89,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	-409	-23	46	-40	0	27	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	27037	9479	7688	1033	240	27	>100	7.83	>100	7.83

Asta : 1065 [144 , 164]

Sez. G: IPE 100 L=113,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	359	-116	-65	0	0	-75	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9480	7688	1033	240	27	81.9	3.08	>100	3.08

Asta : 1066 [142 , 162]

Sez. G: IPE 100 L=111,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	379	-75	-63	0	0	-55	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9475	7684	1033	240	27	>100	4.08	>100	4.08

Asta : 1067 [237 , 239]

Sez. G: IPE 100 L=125,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	-131	86	62	0	0	-54	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	27037	9475	7684	1033	240	27	>100	4.33	>100	4.33

Asta : 1068 [238 , 240]

Sez. G: IPE 100 L=131,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	-166	-44	105	0	0	45	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9478	7687	1033	240	27	73.0	5.15	>100	5.15

Asta : 1069 [337 , 339]

Sez. G: IPE 100 L=137,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	-72	-18	64	0	-45	21	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	27037	9479	7687	1033	240	27	>100	7.40	>100	7.40

Asta : 1070 [338 , 340]

Sez. G: IPE 100 L=143,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
57	1	26	9	-34	0	-56	18	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
57	1	27037	9481	7689	1033	240	27	>100	7.74	>100	7.74

Asta : 1071 [317 , 318]

Sez. G: IPE 100 L=148.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
64	1	247	4	-22	-0	-38	17	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
64	1	27037	9479	7688	1033	240	27	>100	8.54	>100	8.54

Asta : 1072 [165 , 170]

Sez. G: IPE 100 L=119.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
119	1	-110	87	64	0	0	-53	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9473	7683	1033	240	27	>100	4.47	>100	4.47

Asta : 1073 [162 , 167]

Sez. G: IPE 100 L=101.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
101	1	-94	-34	110	0	0	35	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	27037	9480	7688	1033	240	27	70.0	6.67	>100	6.67

Asta : 1074 [164 , 169]

Sez. G: IPE 100 L=113.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
113	1	52	-43	112	0	0	41	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27037	9479	7687	1033	240	27	68.6	5.84	>100	5.84

Asta : 1075 [161 , 166]

Sez. G: IPE 100 L=95.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
67	1	-535	-15	66	-0	-52	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
67	1	27037	9480	7688	1033	240	27	>100	7.35	>100	7.35

Asta : 1076 [107 , 108]

Sez. G: IPE 100 L=89.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
89	1	-158	-38	46	-0	0	34	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9478	7687	1033	240	27	>100	6.80	>100	6.80

Asta : 1077 [163 , 168]

Sez. G: IPE 100 L=107.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
107	1	116	-45	164	0	0	42	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9479	7687	1033	240	27	46.8	5.60	>100	5.60

Asta : 1078 [240 , 222]

Sez. G: IPE 100 L=131.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
132	1	-215	-44	154	0	0	46	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
132	1	27037	9479	7687	1033	240	27	49.9	5.05	>100	5.05

Asta : 1079 [339 , 321]

Sez. G: IPE 100 L=137.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
138	1	-2025	29	61	0	0	-22	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
138	1	27037	9480	7688	1033	240	27	>100	6.01	>100	6.01

Asta : 1080 [340 , 322]

Sez. G: IPE 100 L=143.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
58	1	22	10	-34	-0	-57	18	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
58	1	27037	9480	7688	1033	240	27	>100	7.72	>100	7.72

Asta : 1081 [318 , 319]

Sez. G: IPE 100 L=150.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
60	1	413	5	-20	-0	-33	17	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
60	1	27037	9479	7687	1033	240	27	>100	8.43	>100	8.43

Asta : 1082 [170 , 125]

Sez. G: IPE 100 L=119.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
120	1	-96	125	65	0	0	-82	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
120	1	27037	9473	7683	1033	240	27	75.6	2.90	>100	2.90

Asia : 1083 [169 , 124]

Sez. G: IPE 100 L=113,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm			kg	kg	kg*	kg*	kg*				
114	1	647	113	65	0	0	-73	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
114	1	27037	9475	7685	1033	240	27	83.6	3.06	>100	3.06

Asia : 1084 [167 , 122]

Sez. G: IPE 100 L=101,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
102	1	-287	73	64	-0	0	-54	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
102	1	27037	9478	7686	1033	240	27	>100	4.26	>100	4.26

Asia : 1085 [239 , 221]

Sez. G: IPE 100 L=107,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
126	1	534	89	63	0	0	-57	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
126	1	27037	9474	7683	1033	240	27	>100	3.88	>100	3.88

Asia : 1086 [168 , 123]

Sez. G: IPE 100 L=107,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	-70	114	65	0	0	-77	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	27037	9479	7687	1033	240	27	83.1	3.09	>100	3.09

Asia : 1087 [166 , 121]

Sez. G: IPE 100 L=95,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
96	1	70	56	61	-0	0	-36	--	--	(12+13)-II-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
96	1	27037	9476	7685	1033	240	27	>100	6.55	>100	6.55

Asia : 1088 [108 , 109]

Sez. G: IPE 100 L=89,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	-1034	-38	27	0	0	19	--	--	(12+13)-II-3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	27037	9475	7684	1033	240	27	>100	8.58	>100	8.58

Asia : 1089 [321 , 323]

Sez. G: IPE 100 L=137,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
110	1	-215	-24	97	0	-34	27	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
110	1	27037	9480	7688	1033	240	27	79.6	6.55	>100	6.55

Asia : 1090 [322 , 324]

Sez. G: IPE 100 L=143,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
72	1	40	2	-0	0	-59	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
72	1	27037	9478	7687	1033	240	27	>100	7.81	>100	7.81

Asia : 1091 [319 , 320]

Sez. G: IPE 100 L=131,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	1070	-29	-32	0	0	-20	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9467	7678	1033	240	27	>100	8.18	>100	8.18

Asia : 1092 [222 , 224]

Sez. G: IPE 100 L=131,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
131	1	-146	-61	153	-0	0	57	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
131	1	27037	9479	7688	1033	240	27	50.2	4.11	>100	4.11

Asia : 1093 [221 , 223]

Sez. G: IPE 100 L=125,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	55	-71	158	-0	0	61	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	27037	9477	7685	1033	240	27	48.7	3.92	>100	3.92

Asia : 1094 [123 , 128]

Sez. G: IPE 100 L=107,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	17	-67	166	0	0	48	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9478	7687	1033	240	27	46.3	4.99	>100	4.99

Asia : 1095 [125 , 130]

Sez. G: IPE 100 L=119,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	-29	-76	163	-0	0	62	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
119	1	27037	9476	7685	1033	240	27	47.2	3.87	>100	3.87

Asta : 1096 [122 , 127]

Sez. G: IPE 100 L=101,0 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-168	-38	-63	0	0	-42	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9463	7675	1033	240	27	>100	5.51	>100	5.51

Asta : 1097 [121 , 126]

Sez. G: IPE 100 L=95,0 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-201	36	-61	-0	0	30	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9464	7675	1033	240	27	>100	7.55	>100	7.55

Asta : 1098 [124 , 129]

Sez. G: IPE 100 L=113,1 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	105	-75	166	-0	0	56	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	27037	9479	7687	1033	240	27	46.4	4.19	>100	4.19

Asta : 1099 [109 , 110]

Sez. G: IPE 100 L=89,0 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-572	75	-34	-0	0	34	--	--	(12+13)-II-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9468	7679	1033	240	27	>100	6.21	>100	6.21

Asta : 7001 [1 , 24]

Sez. G: Fil16 L=232,5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2859	--	--	--	--	--	--	--	(12+13)-II-2	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	1.84	>100	1.84

Asta : 7002 [24 , 101]

Sez. G: Fil16 L=252,5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
252	1	4210	--	--	--	--	--	--	--	(12+13)-II-2	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
252	1	5266	--	--	--	--	--	>100	1.25	>100	1.25

Asta : 7003 [101 , 157]

Sez. G: Fil14 L=389,3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2472	--	--	--	--	--	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	4032	--	--	--	--	--	>100	1.63	>100	1.63

Asta : 7004 [157 , 154]

Sez. G: Fil14 L=360,5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
360	1	937	--	--	--	--	--	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
360	1	4032	--	--	--	--	--	>100	4.30	>100	4.30

Asta : 7005 [154 , 235]

Sez. G: Fil14 L=319,3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1631	--	--	--	--	--	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	4032	--	--	--	--	--	>100	2.47	>100	2.47

Asta : 7006 [235 , 333]

Sez. G: Fil14 L=278,2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
278	1	2007	--	--	--	--	--	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
278	1	4032	--	--	--	--	--	>100	2.01	>100	2.01

Asta : 7007 [333 , 312]

Sez. G: Fil14 L=264,3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	575	--	--	--	--	--	--	--	(12+13)-IV-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	4032	--	--	--	--	--	>100	7.02	>100	7.02

Asta : 7008 [311 , 335]

Sez. G: Fil14 L=263,8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-743	--	--	--	--	--	--	--	(12+13)-II-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	4032	--	--	--	--	--	>100	5.43	>100	5.43

Asta : 7009 [335 , 233]

Sez. G: Fil14 L=278,6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	4032	--	--	--	--	--	>100	5.43	>100	5.43

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
279	1	-2178	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
279	1	4032	--	--	--	--	--	>100	1.85	>100	1.85

Asia : 7010 [233 , 159]

Sez. G: F14 L=318.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	1488	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.71	>100	2.71

Asia : 7011 [159 , 152]

Sez. G: F14 L=360.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
361	1	-749	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
361	1	4032	--	--	--	--	--	>100	5.39	>100	5.39

Asia : 7012 [152 , 102]

Sez. G: F14 L=389.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	2423	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	1.66	>100	1.66

Asia : 7013 [102 , 28]

Sez. G: F16 L=252.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
252	1	-4319	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
252	1	5266	--	--	--	--	--	>100	1.22	>100	1.22

Asia : 7014 [28 , 2]

Sez. G: F16 L=252.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	2814	--	--	--	--	--	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	1.87	>100	1.87

Asia : 7015 [102 , 137]

Sez. G: F14 L=389.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1540	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.62	>100	2.62

Asia : 7016 [137 , 104]

Sez. G: F14 L=372.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
372	1	-1431	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
372	1	4032	--	--	--	--	--	>100	2.82	>100	2.82

Asia : 7017 [104 , 132]

Sez. G: F14 L=371.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1456	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.77	>100	2.77

Asia : 7018 [132 , 106]

Sez. G: F14 L=371.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
371	1	-2181	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
371	1	4032	--	--	--	--	--	>100	1.85	>100	1.85

Asia : 7019 [106 , 162]

Sez. G: F14 L=371.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1494	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.70	>100	2.70

Asia : 7020 [162 , 108]

Sez. G: F14 L=372.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
372	1	-1209	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
372	1	4032	--	--	--	--	--	>100	3.33	>100	3.33

Asia : 7021 [108 , 122]

Sez. G: F14 L=371.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cm}^2$ fl=4300 kg/cm γ : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1284	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	3.14	>100	3.14

Asia : 7022 [122 , 110]

Sez. G: F114 L=371.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
371	1	-1879	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
371	1	4032	--	--	--	--	--	>100	2.15	>100	2.15

Asia : 7023 [110 , 22]

Sez. G: F116 L=222.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	3578	--	--	--	--	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	1.47	>100	1.47

Asia : 7024 [22 , 10]

Sez. G: F116 L=222.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
222	1	-2313	--	--	--	--	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
222	1	5266	--	--	--	--	--	>100	2.28	>100	2.28

Asia : 7025 [9 , 30]

Sez. G: F116 L=222.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
222	1	2193	--	--	--	--	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
222	1	5266	--	--	--	--	--	>100	2.40	>100	2.40

Asia : 7026 [30 , 109]

Sez. G: F116 L=222.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	-3812	--	--	--	--	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	1.38	>100	1.38

Asia : 7027 [109 , 127]

Sez. G: F114 L=371.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	-1782	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.26	>100	2.26

Asia : 7028 [127 , 124]

Sez. G: F114 L=344.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-572	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	7.04	>100	7.04

Asia : 7029 [124 , 223]

Sez. G: F114 L=305.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
304	1	1279	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
304	1	4032	--	--	--	--	--	>100	3.15	>100	3.15

Asia : 7030 [223 , 321]

Sez. G: F114 L=269.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	-1940	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.08	>100	2.08

Asia : 7031 [321 , 320]

Sez. G: F114 L=259.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
260	1	-598	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
260	1	4032	--	--	--	--	--	>100	6.74	>100	6.74

Asia : 7032 [319 , 323]

Sez. G: F114 L=260.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
261	1	508	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
261	1	4032	--	--	--	--	--	>100	7.93	>100	7.93

Asia : 7033 [323 , 221]

Sez. G: F114 L=268.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	1823	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.21	>100	2.21

Asia : 7034 [221 , 129]

Sez. G: F114 L=305.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
306	1	-1432	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.81	>100	2.81
306	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7035 [129 , 122]

Sez. G: F114 L=345.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-2	
344	1	-761	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	5.30	>100	5.30
344	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7036 [109 , 167]

Sez. G: F114 L=371.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
0	1	-1130	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.57	>100	3.57
0	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7037 [167 , 107]

Sez. G: F114 L=371.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-2	
371	1	-1270	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.17	>100	3.17
371	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7038 [107 , 142]

Sez. G: F114 L=371.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
0	1	-1411	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.86	>100	2.86
0	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7039 [142 , 105]

Sez. G: F114 L=372.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-2	
372	1	-2173	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.86	>100	1.86
372	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7040 [105 , 147]

Sez. G: F114 L=371.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
0	1	-1488	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.71	>100	2.71
0	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7041 [147 , 103]

Sez. G: F114 L=370.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
0	1	1336	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.02	>100	3.02
0	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7042 [103 , 157]

Sez. G: F114 L=388.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
0	1	-1644	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.45	>100	2.45
0	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7043 [312 , 327]

Sez. G: F114 L=259.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-2	
0	1	-1581	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.55	>100	2.55
0	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7044 [327 , 314]

Sez. G: F114 L=259.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
260	1	-1546	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.61	>100	2.61
260	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7045 [314 , 325]

Sez. G: F114 L=260.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-2	
0	1	-1702	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.37	>100	2.37
0	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7046 [325 , 316]

Sez. G: F114 L=260.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
260	1	-414	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	9.74	>100	9.74
260	1	4032	--	--	--	--	--	--	--	--	--

Asia : 7047 [316 , 337]

Sez. G: F114 L=260.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm $\eta=4300$ kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)-IV-3	
0	1	4032	--	--	--	--	--	--	--	--	--

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-1449	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.78	>100	2.78

Asia : 7048 [337 , 318]

Sez. G: F114 L=259.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
260	1	-1506	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
260	1	4032	--	--	--	--	--	>100	2.68	>100	2.68

Asia : 7049 [318 , 321]

Sez. G: F114 L=260.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1660	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.43	>100	2.43

Asia : 7050 [319 , 339]

Sez. G: F114 L=261.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1399	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.88	>100	2.88

Asia : 7051 [339 , 317]

Sez. G: F114 L=260.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
260	1	-1578	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
260	1	4032	--	--	--	--	--	>100	2.56	>100	2.56

Asia : 7052 [317 , 329]

Sez. G: F114 L=261.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1687	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.39	>100	2.39

Asia : 7053 [329 , 315]

Sez. G: F114 L=260.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
261	1	-474	--	--	--	--	--	--	--	(12+13)-II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
261	1	4032	--	--	--	--	--	>100	8.50	>100	8.50

Asia : 7054 [315 , 331]

Sez. G: F114 L=260.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1397	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.89	>100	2.89

Asia : 7055 [331 , 313]

Sez. G: F114 L=260.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
261	1	-1473	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
261	1	4032	--	--	--	--	--	>100	2.74	>100	2.74

Asia : 7056 [313 , 335]

Sez. G: F114 L=264.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1945	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	2.07	>100	2.07

Asia : 7057 [132 , 144]

Sez. G: F114 L=345.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-967	--	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	4.17	>100	4.17

Asia : 7058 [144 , 225]

Sez. G: F114 L=305.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
305	1	1321	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
305	1	4032	--	--	--	--	--	>100	3.05	>100	3.05

Asia : 7059 [225 , 329]

Sez. G: F114 L=269.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2396	--	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	1.68	>100	1.68

Asia : 7060 [325 , 229]

Sez. G: F114 L=269.0 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	2448	--	--	--	--	--	--	(12+13)-IV-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	1.65	>100	1.65

Asia : 7061 [229 , 134]

Sez. G: F114 L=344.2 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	1282	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	3.15	>100	3.15

Asia : 7062 [134 , 142]

Sez. G: F114 L=344.8 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	984	--	--	--	--	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	4032	--	--	--	--	--	>100	4.10	>100	4.10

Asia : 7063 [106 , 21]

Sez. G: F116 L=222.2 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
222	1	-3674	--	--	--	--	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
222	1	5266	--	--	--	--	--	>100	1.43	>100	1.43

Asia : 7064 [21 , 6]

Sez. G: F116 L=222.2 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
222	1	-2278	--	--	--	--	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
222	1	5266	--	--	--	--	--	>100	2.31	>100	2.31

Asia : 7065 [5 , 26]

Sez. G: F116 L=222.2 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	-2229	--	--	--	--	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.36	>100	2.36

Asia : 7066 [26 , 105]

Sez. G: F116 L=222.2 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-3731	--	--	--	--	--	--	--	(12+13)-II-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	1.41	>100	1.41

Asia : 8000 [101 , 151]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg*m	kg*m	kg*m		
0	1	-4136	-18	-1604	4	3779	2	--	--
									3
									Comb.

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86781	37930	19516	9213	462	23.6	4.66	>100	4.66

Asia : 8000 [151 , 152]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4
cm		kg	kg	kg	kg*m	kg*m	kg*m		
178	1	-2348	-236	-1014	7	-1429	573	--	--
									8
									Comb.

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86569	37837	19516	9213	462	37.3	6.80	66.1	6.80

Asia : 8000 [152 , 153]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
170	1	-877	59	-695	5	-2790	491	---	---	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	86731	37908	19516	9213	462	54.5	4.99	95.3	4.99

Asia : 8000 [153 , 154]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
159	1	-369	81	-388	2	-3575	385	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
159	1	201236	86965	38010	19516	9213	462	97.9	4.41	>100	4.41

Asia : 8000 [154 , 155]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato									
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*		
0	1	-490	152	-250	-0	-3580	414	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87060	38052	19516	9213	462	>100	4.33	>100	4.33

Asia : 8000 [155 , 233]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-95	103	81	-1	-3801	219	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87000	38026	19516	9213	462	>100	4.57	>100	4.57

Asia : 8000 [233 , 234]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-370	53	450	-3	-3556	113	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86844	37957	19516	9213	462	84.3	5.09	>100	5.09

Asia : 8000 [234 , 333]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	138	54	643	-7	-3014	68	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86569	37837	19516	9213	462	58.8	6.15	66.1	6.15

Asia : 8000 [333 , 334]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-3176	123	-49	-5	2231	150	--	--	(12+13)+IV-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86742	37913	19516	9213	462	>100	6.83	98.3	6.83

Asia : 8000 [334 , 311]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-3121	45	-837	-12	2360	56	--	--	(12+13)+IV-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86219	37684	19516	9213	462	45.0	7.02	39.9	7.02

Asia : 8001 [102 , 156]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-7425	-6	-2360	1	5186	28	--	--	3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87053	38049	19516	9213	462	16.1	3.27	>100	3.27

Asia : 8001 [156 , 157]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	-5087	-250	-1212	4	-1751	613	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86774	37927	19516	9213	462	31.3	5.51	>100	5.51

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Asia : 8001 [157 , 158]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	-5095	33	-710	1	-3244	593	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	201236	87052	38048	19516	9213	462	53.6	3.91	>100	3.91

Asia : 8001 [158 , 159]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
159	1	-4297	40	-284	2	-3955	562	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
159	1	201236	86962	38009	19516	9213	462	>100	3.51	>100	3.51

Asia : 8001 [159 , 160]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-3758	156	-188	4	-3954	605	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86830	37951	19516	9213	462	>100	3.48	>100	3.48

Asia : 8001 [160 , 235]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-3167	97	146	3	-3990	435	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86840	37956	19516	9213	462	>100	3.74	>100	3.74

Asia : 8001 [235 , 236]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2241	197	485	2	-3577	369	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86966	38011	19516	9213	462	78.4	4.26	>100	4.26

Asia : 8001 [236 , 335]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1013	161	652	-5	-3037	196	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86701	37895	19516	9213	462	58.1	5.50	88.1	5.50

Asia : 8001 [335 , 336]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq} : \textbf{Verificato}$											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-3037	-57	-1050	10	2807	-59	--	--	(12+13)-III-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86330	37733	19516	9213	462	35.9	6.05	45.6	6.05

Asia : 8001 [336 , 312]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	361	46	2380	-16	2634	-18	--	--	(12+13)-IV-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	85896	37543	19516	9213	462	15.8	7.21	29.2	7.21

Asia : 8002 [103 , 136]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/M=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-6599	-35	-2202	1	4986	-5	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86988	38020	19516	9213	462	17.3	3.46	>100	3.46

Asia : 8002 [136 , 137]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-4195	-235	-1157	2	-1649	611	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86978	38016	19516	9213	462	32.8	5.82	>100	5.82

Asia : 8002 [137 , 138]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/M=2619 kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
170	1	-3908	19	-706	2	-3123	594	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	201236	86959	38008	19516	9213	462	53.8	4.10	>100	4.10

Asia : 8002 [138 , 139]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
158	1	-3159	36	-324	1	-3895	569	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
158	1	201236	87004	38027	19516	9213	462	>100	3.61	>100	3.61

Asia : 8002 [139 , 140]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2813	126	-237	4	-3896	606	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86813	37944	19516	9213	462	>100	3.58	>100	3.58

Asia : 8002 [140 , 227]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2238	130	126	3	-4007	480	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86904	37983	19516	9213	462	>100	3.72	>100	3.72

Asia : 8002 [227 , 228]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1839	240	496	1	-5620	370	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87024	38036	19516	9213	462	76.7	4.26	>100	4.26

Asia : 8002 [228 , 327]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-762	86	682	-0	-2995	134	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87084	38063	19516	9213	462	55.8	5.82	>100	5.82

Asia : 8002 [327 , 328]

Sez. G: HE 240 A L=108.1 cm Crit: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2400	77	-363	10	2050	70	--	--	(12+13)-I-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86323	37730	19516	9213	462	>100	8.03	45.2	8.03

Asia : 8002 [328 , 313]

Sez. G: HE 240 A L=112.3 cm Crit: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	-2330	6	867	0	2357	-1	--	--	10

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	87070	38056	19516	9213	462	43.9	7.55	>100	7.55

Asia : 8003 [104 , 146]

Sez. G: HE 240 A L=181.6 cm Crit: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-6000	-68	-2047	2	4710	-1	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86978	38016	19516	9213	462	18.6	3.69	>100	3.69

Asia : 8003 [146 , 147]

Sez. G: HE 240 A L=177,6 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm			kg	kg	kg*	kg*	kg*				
178	1	-3892	-195	-1105	2	-1580	603	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86984	38019	19516	9213	462	34.4	6.03	>100	6.03

Asia : 8003 [147 , 148]

Sez. G: HE 240 A L=169,8 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	-3399	19	-697	2	-3035	581	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	86982	38018	19516	9213	462	54.6	4.25	>100	4.25

Asia : 8003 [148 , 149]

Sez. G: HE 240 A L=158,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
159	1	-2764	43	-330	1	-3816	542	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
159	1	201236	87026	38037	19516	9213	462	>100	3.73	>100	3.73

Asia : 8003 [149 , 150]

Sez. G: HE 240 A L=147,9 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-2508	111	-262	3	-3815	578	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86861	37965	19516	9213	462	>100	3.69	>100	3.69

Asia : 8003 [150 , 231]

Sez. G: HE 240 A L=134,4 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-2005	161	99	3	-3959	471	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86874	37971	19516	9213	462	>100	3.79	>100	3.79

Asia : 8003 [231 , 232]

Sez. G: HE 240 A L=122,6 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1650	142	466	3	-3604	324	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86881	37974	19516	9213	462	81.5	4.39	>100	4.39

Asia : 8003 [232 , 331]

Sez. G: HE 240 A L=113,3 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
0	1	-706	195	667	-2	-2980	203	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86924	37992	19516	9213	462	56.9	5.61	>100	5.61

Asia : 8003 [331 , 332]

Sez. G: HE 240 A L=108,1 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-614	-52	917	-8	-2083	8	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86509	37811	19516	9213	462	41.2	9.04	59.4	9.04

Asia : 8003 [332 , 314]

Sez. G: HE 240 A L=112,4 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	-2127	4	962	0	2347	-1	--	--	10	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	87064	38053	19516	9213	462	39.6	7.64	>100	7.64

Asia : 8004 [105 , 131]

Sez. G: HE 240 A L=181,6 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-5638	-61	-1972	0	4582	49	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87087	38064	19516	9213	462	19.3	3.73	>100	3.73

Asia : 8004 [131 , 132]

Sez. G: HE 240 A L=177,6 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	-3383	-179	-1103	2	-1564	616	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86965	38010	19516	9213	462	34.4	6.10	>100	6.10

Asia : 8004 [132 , 133]

Sez. G: HE 240 A L=169,8 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	-2809	31	-709	2	-5043	577	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	86966	38011	19516	9213	462	53.6	4.30	>100	4.30

Asia : 8004 [133 , 134]

Sez. G: HE 240 A L=158,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
159	1	-2145	50	-346	2	-3851	527	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
159	1	201236	86964	38010	19516	9213	462	>100	3.77	>100	3.77

Asia : 8004 [134 , 135]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2218	123	-248	3	-3849	570	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86854	37962	19516	9213	462	>100	3.70	>100	3.70

Asia : 8004 [135 , 225]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1700	147	124	4	-3974	446	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86775	37927	19516	9213	462	>100	3.84	>100	3.84

Asia : 8004 [225 , 226]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1776	156	527	2	-3582	320	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86918	37990	19516	9213	462	72.1	4.40	>100	4.40

Asia : 8004 [226 , 325]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-855	125	702	-3	-2876	189	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86900	37982	19516	9213	462	54.1	5.81	>100	5.81

Asia : 8004 [325 , 326]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2682	180	-523	-9	2118	188	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86392	37760	19516	9213	462	72.2	7.03	49.6	7.03

Asia : 8004 [326 , 315]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	-2035	1	976	0	2303	-40	--	--	10	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	87069	38056	19516	9213	462	39.0	7.80	>100	7.80

Asia : 8005 [106 , 141]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-5919	-86	-2006	-0	4627	51	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87083	38062	19516	9213	462	19.0	3.68	>100	3.68

Asia : 8005 [141 , 142]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	-3994	-149	-1062	2	-1500	614	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86977	38016	19516	9213	462	35.8	6.12	>100	6.12

Asia : 8005 [142 , 143]

Sez. G: HE 240 A L=169.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	-3899	36	-668	1	-2903	572	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	201236	87004	38027	19516	9213	462	57.0	4.35	>100	4.35

Asia : 8005 [143 , 144]

Sez. G: HE 240 A L=158.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
158	1	-3274	83	-356	2	-5692	469	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
158	1	201236	86970	38013	19516	9213	462	>100	3.90	>100	3.90

Asia : 8005 [144 , 145]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
74	1	-2727	52	-139	3	-3856	473	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
74	1	201236	86852	37961	19516	9213	462	>100	3.81	>100	3.81

Asia : 8005 [145 , 229]

Sez. G: HE 240 A L=134.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2375	190	3	3	-3898	485	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86842	37956	19516	9213	462	>100	3.79	>100	3.79

Asia : 8005 [229 , 230]

Sez. G: HE 240 A L=122.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
0	1	-1485	129	370	4	-3672	295	--	--	--	8

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	201236	86802	37939	19516	9213	462	>100	4.40	>100	4.40

Asia : 8005 [230 , 329]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	-558	113	604	-3	-3156	198	--	--	--	9

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	201236	86873	37970	19516	9213	462	62.9	5.38	>100	5.38

Asia : 8005 [329 , 330]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	-2382	-275	-413	13	1930	-289	--	--	--	(12+13)-IV-3

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	201236	86105	37634	19516	9213	462	91.2	7.04	35.3	7.04

Asia : 8005 [330 , 316]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
112	1	-2062	-2	964	0	2306	1	--	--	--	10

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
112	1	201236	87077	38059	19516	9213	462	39.5	7.78	>100	7.78

Asia : 8006 [107 , 161]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	-5608	-116	-1937	0	4452	47	--	--	--	3

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	201236	87065	38054	19516	9213	462	19.6	3.83	>100	3.83

Asia : 8006 [161 , 162]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
178	1	-3511	-115	-1033	2	-1495	609	--	--	--	8

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
178	1	201236	86960	38008	19516	9213	462	36.8	6.24	>100	6.24

Asia : 8006 [162 , 163]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
170	1	-3372	67	-673	1	-2908	512	--	--	--	8

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
170	1	201236	86998	38025	19516	9213	462	56.5	4.52	>100	4.52

Asia : 8006 [163 , 164]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
158	1	-2720	35	-341	1	-3707	485	--	--	--	8

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
158	1	201236	87044	38045	19516	9213	462	>100	3.90	>100	3.90

Asia : 8006 [164 , 165]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	-2462	132	-291	3	-3708	515	--	--	--	8

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	201236	86883	37975	19516	9213	462	>100	3.87	>100	3.87

Asia : 8006 [165 , 237]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	-1942	95	52	3	-3892	370	--	--	--	8

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	201236	86867	37967	19516	9213	462	>100	4.01	>100	4.01

Asia : 8006 [237 , 238]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	-1587	157	422	3	-3594	299	--	--	--	8

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	201236	86870	37969	19516	9213	462	90.0	4.45	>100	4.45

Asia : 8006 [238 , 337]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	-633	145	643	-0	-3023	164	--	--	--	9

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	201236	87080	38060	19516	9213	462	59.2	5.69	>100	5.69

Asia : 8006 [337 , 338]

X	cls	N	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	-503	-4	899	-10	-2147	24	--	--	--	9

X	cls	Nr	TY	TZ	Vyr	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m				
0	1	201236	86563	37747	19516	9213	462	42.0	8.68	47.6	8.68

Asia : 8006 [338 , 317]

Sez. G: HE 240 A L=112,3 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	-2062	-4	944	0	2258	1	--	--	10

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	87083	38062	19516	9213	462	40.3	7.93	>100	7.93

Asia : 8007 [108 , 166]

Sez. G: HE 240 A L=181,6 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-5751	-156	-1959	1	4395	27	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87034	38041	19516	9213	462	19.4	3.89	>100	3.89

Asia : 8007 [166 , 167]

Sez. G: HE 240 A L=177,6 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-3686	-87	-1048	2	-1620	612	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86942	38000	19516	9213	462	36.3	5.96	>100	5.96

Asia : 8007 [167 , 168]

Sez. G: HE 240 A L=169,8 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
170	1	-3477	89	-650	1	-2998	472	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
170	1	201236	87013	38031	19516	9213	462	58.5	4.50	>100	4.50

Asia : 8007 [168 , 169]

Sez. G: HE 240 A L=158,5 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
158	1	-2856	9	-291	-0	-3716	487	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
158	1	201236	87090	38065	19516	9213	462	>100	3.88	>100	3.88

Asia : 8007 [169 , 170]

Sez. G: HE 240 A L=147,9 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2610	158	-246	3	-3719	511	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86890	37978	19516	9213	462	>100	3.86	>100	3.86

Asia : 8007 [170 , 239]

Sez. G: HE 240 A L=134,4 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-2109	61	91	3	-3834	326	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86877	37972	19516	9213	462	>100	4.13	>100	4.13

Asia : 8007 [239 , 240]

Sez. G: HE 240 A L=122,6 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1754	164	437	3	-3482	297	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86853	37961	19516	9213	462	87.0	4.56	>100	4.56

Asia : 8007 [240 , 339]

Sez. G: HE 240 A L=113,2 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-763	127	635	0	-2910	152	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87084	38062	19516	9213	462	59.9	5.90	>100	5.90

Asia : 8007 [339 , 340]

Sez. G: HE 240 A L=108,1 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-647	3	869	-10	-2042	32	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86352	37743	19516	9213	462	43.4	8.98	47.0	8.98

Asia : 8007 [340 , 318]

Sez. G: HE 240 A L=112,3 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	-2120	-4	899	0	2206	-1	--	--	10

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87081	38061	19516	9213	462	42.4	8.09	>100	8.09

Asia : 8008 [109 , 121]

Sez. G: HE 240 A L=181,6 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-5119	-195	-1864	-1	4025	14	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87059	38051	19516	9213	462	20.4	4.29	>100	4.29

Asia : 8008 [121 , 122]

Sez. G: HE 240 A L=177,6 cm Crit.: Acciaio Flessione $\gamma M=1,05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-2926	-63	-995	-0	-1710	623	--	--	8

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X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	87078	38060	19516	9213	462	38.2	5.89	>100	5.89

Asia : 8008 [122 , 123]

Sez. G: HE 240 A L=169.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	-2625	74	-615	0	-3025	514	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	201236	87089	38064	19516	9213	462	61.9	4.47	>100	4.47

Asia : 8008 [123 , 124]

Sez. G: HE 240 A L=158.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
159	1	-1958	52	-256	2	-3690	462	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
159	1	201236	86967	38011	19516	9213	462	>100	4.02	>100	4.02

Asia : 8008 [124 , 125]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2335	122	-176	3	-3701	508	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86882	37974	19516	9213	462	>100	3.90	>100	3.90

Asia : 8008 [125 , 221]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1808	98	168	5	-3714	382	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86703	37896	19516	9213	462	>100	4.15	88.6	4.15

Asia : 8008 [221 , 222]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2186	117	492	5	-3267	314	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86738	37911	19516	9213	462	77.1	4.71	97.1	4.71

Asia : 8008 [222 , 321]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1143	182	632	-3	-2651	225	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86837	37954	19516	9213	462	60.0	6.03	>100	6.03

Asia : 8008 [321 , 322]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2306	104	-733	-8	1901	88	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86526	37818	19516	9213	462	51.6	8.45	61.2	8.45

Asia : 8008 [322 , 319]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	-321	-67	1403	16	2282	37	--	--	(12+13)+VIII-3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	85884	37538	19516	9213	462	26.8	8.16	28.9	8.16

Asia : 8009 [110 , 126]

Sez. G: HE 240 A L=181.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-3654	-192	-1270	-4	2852	47	--	--	3	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86758	37920	19516	9213	462	29.9	5.90	>100	5.90

Asia : 8009 [126 , 127]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	-2516	-69	-776	0	-1548	662	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	87087	38064	19516	9213	462	49.1	6.52	>100	6.52

Asia : 8009 [127 , 128]

Sez. G: HE 240 A L=169.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	-2457	85	-550	1	-2442	539	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
170	1	201236	87005	38028	19516	9213	462	69.1	5.11	>100	5.11

Asia : 8009 [128 , 129]

Sez. G: HE 240 A L=158.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
158	1	-2123	65	-331	3	-3116	469	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
158	1	201236	86860	37964	19516	9213	462	>100	4.52	>100	4.52

Asia : 8009 [129 , 130]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	My4	Mz4	Comb.
30	1	-1481	122	-269	5	-3200	475	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	201236	86685	37888	19516	9213	462	>100	4.49	84.6	4.49

Asia : 8009 [130 , 223]

Sez. G: HE 240 A L=134.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	-1270	149	-78	5	-3409	378	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86686	37888	19516	9213	462	>100	4.50	84.9	4.50

Asia : 8009 [223 , 224]

Sez. G: HE 240 A L=122.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	-353	28	230	7	-3348	231	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86598	37850	19516	9213	462	>100	5.04	70.0	5.04

Asia : 8009 [224 , 323]

Sez. G: HE 240 A L=113.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	17	163	463	-5	-3034	238	--	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86737	37911	19516	9213	462	81.8	5.51	96.9	5.51

Asia : 8009 [323 , 324]

Sez. G: HE 240 A L=108.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	-2809	-224	488	5	1925	-252	--	--	--	(12+13)-VIII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86737	37911	19516	9213	462	77.7	7.15	97.0	7.15

Asia : 8009 [324 , 320]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	-2748	-56	-761	16	2003	29	--	--	--	(12+13)-VIII-3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	85918	37553	19516	9213	462	49.4	8.37	29.7	8.37

Asia : 8010 [28 , 24]

Sez. G: IPE 100 L=149.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
149	1	399	-25	8	0	0	25	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
149	1	27037	9477	7686	1033	240	27	>100	8.29	>100	8.29

Asia : 8010 [24 , 23]

Sez. G: IPE 100 L=150.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	664	10	-8	0	0	28	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9480	7688	1033	240	27	>100	7.12	>100	7.12

Asia : 8010 [23 , 25]

Sez. G: IPE 100 L=88.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
89	1	302	-7	5	0	0	19	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9479	7688	1033	240	27	>100	11.0	>100	11.0

Asia : 8010 [25 , 21]

Sez. G: IPE 100 L=89.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-111	13	-5	0	0	19	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9480	7688	1033	240	27	>100	12.0	>100	12.0

Asia : 8010 [21 , 26]

Sez. G: IPE 100 L=89.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
89	1	207	-6	5	0	0	23	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9480	7688	1033	240	27	>100	9.66	>100	9.66

Asia : 8010 [26 , 29]

Sez. G: IPE 100 L=89.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
89	1	296	-3	5	0	0	17	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9479	7687	1033	240	27	>100	12.5	>100	12.5

Asia : 8010 [29 , 27]

Sez. G: IPE 100 L=89.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
89	1	94	-4	5	0	0	18	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9479	7688	1033	240	27	>100	12.4	>100	12.4

Asia: 8010 [27, 22]

Sez. G: IPE 100 L=89.6 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k \gamma M=2619$ kg/cmq fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	-205	-3	5	-0	0	20	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
90	1	27037	9478	7686	1033	240	27	>100	11.1	>100	11.1

Asia: 8010 [22, 30]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k \gamma M=2619$ kg/cmq fl=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	36	18	-5	-0	0	20	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9477	7686	1033	240	27	>100	11.8	>100	11.8

Verifica spostamenti verticali delle aste in Acciaio secondo NTC 2008

Scenario di calcolo : Set_NT_SLD_A2_STR/GEO

Travata: 8000 (Travata 8000) [101 (Nodo 101) , 311 (Nodo 311)]

L = 1426.5cm

Crit.Prog: Acciaio_Flessione $\delta \epsilon = 0.0cm$ Verifica: Verificata

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
820.7	2	8.22	57.06	6.94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
849.0	2	3.42	47.55	13.9

Travata: 8001 (Travata 8001) [102 (Nodo 102) , 312 (Nodo 312)]

L = 1426.5cm

Crit.Prog: Acciaio_Flessione $\delta \epsilon = 0.0cm$ Verifica: Verificata

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
776.4	2	10.06	57.06	5.67

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
805.9	2	4.27	47.55	11.1

Travata: 8002 (Travata 8002) [103 (Nodo 103) , 313 (Nodo 313)]

L = 1425.9cm

Crit.Prog: Acciaio_Flessione $\delta \epsilon = 0.0cm$ Verifica: Verificata

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
790.9	2	9.96	57.03	5.72

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
820.5	2	4.14	47.53	11.5

Travata: 8003 (Travata 8003) [104 (Nodo 104) , 314 (Nodo 314)]

L = 1426.3cm

Crit.Prog: Acciaio_Flessione $\delta \epsilon = 0.0cm$ Verifica: Verificata

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
805.9	2	9.61	57.05	5.94

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
820.7	2	3.96	47.54	12.0

Travata: 8004 (Travata 8004) [105 (Nodo 105) , 315 (Nodo 315)]

L = 1426.5cm

Crit.Prog: Acciaio_Flessione $\delta \epsilon = 0.0cm$ Verifica: Verificata

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
806.0	2	9.49	57.06	6.02

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
820.7	2	3.89	47.55	12.2

Travata: 8005 (Travata 8005) [106 (Nodo 106) , 316 (Nodo 316)]

L = 1425.4cm

Crit.Prog: Acciaio_Flessione $\delta \epsilon = 0.0cm$ Verifica: Verificata

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
820.3	2	9.49	57.02	6.01

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/250.00	Cs
cm		mm	mm	
835.1	2	3.88	47.51	12.3

Travata: 8006 (Travata 8006) [107 (Nodo 107), 317 (Nodo 317)]

L = 1425.9cm

Crit.Prog: Acciaio_Flessione δ̵ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
820.5	2	9.25	57.04	6.17

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
835.3	2	3.74	47.53	12.7

Travata: 8007 (Travata 8007) [108 (Nodo 108), 318 (Nodo 318)]

L = 1425.9cm

Crit.Prog: Acciaio_Flessione δ̵ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
805.7	2	9.11	57.03	6.26

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
820.5	2	3.64	47.53	13.1

Travata: 8008 (Travata 8008) [109 (Nodo 109), 319 (Nodo 319)]

L = 1426.4cm

Crit.Prog: Acciaio_Flessione δ̵ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
791.1	2	8.46	57.05	6.74

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
791.1	2	3.27	47.55	14.5

Travata: 8009 (Travata 8009) [110 (Nodo 110), 320 (Nodo 320)]

L = 1425.3cm

Crit.Prog: Acciaio_Flessione δ̵ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
848.5	2	6.86	57.01	8.32

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
888.8	2	2.55	47.51	18.6

Travata: 1001 (Travata 1001) [101 (Nodo 101), 102 (Nodo 102)]

L = 149.5cm

Crit.Prog: Acciaio_Flessione δ̵ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
74.7	7	-0.30	5.98	19.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
74.7	7	-0.46	4.98	10.9

Travata: 1022 (Travata 1022) [102 (Nodo 102), 103 (Nodo 103)]

L = 150.1cm

Crit.Prog: Acciaio_Flessione δ̵ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
75.1	7	-0.30	6.01	20.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
75.1	7	-0.46	5.00	10.8

Travata: 1032 (Travata 1032) [103 (Nodo 103), 104 (Nodo 104)]

L = 88.9cm

Crit.Prog: Acciaio_Flessione δ̵ = 0.0cm Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	8max	L/250.00	Cs
cm		mm	mm	
44.4	7	-0.16	3.55	22.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
44.4	7	-0.17	2.96	17.1

Travata: 1042 (Travata 1042) [104 (Nodo 104), 105 (Nodo 105)]

L = 89.4cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.7	7	-0.16	3.58	22.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
44.7	7	-0.18	2.98	17.0

Travata: 1053 (Travata 1053) [105 (Nodo 105), 106 (Nodo 106)]

L = 89.3cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.7	7	-0.16	3.57	22.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
44.7	7	-0.17	2.98	17.0

Travata: 1064 (Travata 1064) [106 (Nodo 106), 107 (Nodo 107)]

L = 89.2cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.6	7	-0.16	3.57	22.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
44.6	7	-0.17	2.97	17.0

Travata: 1076 (Travata 1076) [107 (Nodo 107), 108 (Nodo 108)]

L = 89.4cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.7	7	-0.16	3.58	22.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
44.7	7	-0.18	2.98	17.0

Travata: 1088 (Travata 1088) [108 (Nodo 108), 109 (Nodo 109)]

L = 89.6cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.8	7	-0.16	3.58	22.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
44.8	7	-0.18	2.99	17.0

Travata: 1099 (Travata 1099) [109 (Nodo 109), 110 (Nodo 110)]

L = 89.0cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
44.5	7	-0.16	3.56	22.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
44.5	7	-0.17	2.97	17.1

Travata: 1002 (Travata 1002) [151 (Nodo 151), 156 (Nodo 156)]

L = 149.5cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.7	5	0.36	5.98	16.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
74.7	7	-0.41	4.98	12.0

Travata: 1012 (Travata 1012) [156 (Nodo 156), 136 (Nodo 136)]

L = 150.1cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
75.0	5	0.37	6.00	16.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
75.0	7	-0.42	5.00	12.0

Travata: 1033 (Travata 1033) [136 (Nodo 136), 146 (Nodo 146)]

L = 94.9cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
47.4	7	-0.15	3.80	25.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
47.4	7	-0.19	3.16	16.6

Travata: 1044 (Travata 1044) [146 (Nodo 146), 131 (Nodo 131)]

L = 95.4cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
47.7	7	-0.15	3.82	25.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
47.7	7	-0.19	3.18	16.5

Travata: 1055 (Travata 1055) [131 (Nodo 131), 141 (Nodo 141)]

L = 95.3cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
47.7		7	-0.15	3.81	25.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	L/300.00	Cs
cm			mm	mm	
47.7		7	-0.19	3.18	16.5

Travata: 1062 (Travata 1062) [141 (Nodo 141), 161 (Nodo 161)]

L = 95.2cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
47.6		7	-0.15	3.81	25.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	L/300.00	Cs
cm			mm	mm	
47.6		7	-0.19	3.17	16.5

Travata: 1075 (Travata 1075) [161 (Nodo 161), 166 (Nodo 166)]

L = 95.4cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
47.7		7	-0.15	3.82	25.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	L/300.00	Cs
cm			mm	mm	
47.7		7	-0.19	3.18	16.5

Travata: 1087 (Travata 1087) [166 (Nodo 166), 121 (Nodo 121)]

L = 95.6cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
47.8		7	-0.15	3.82	25.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	L/300.00	Cs
cm			mm	mm	
47.8		7	-0.19	3.19	16.5

Travata: 1097 (Travata 1097) [121 (Nodo 121), 126 (Nodo 126)]

L = 95.0cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
47.5		7	-0.15	3.80	25.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	L/300.00	Cs
cm			mm	mm	
47.5		7	-0.19	3.17	16.6

Travata: 1003 (Travata 1003) [152 (Nodo 152), 157 (Nodo 157)]

L = 149.5cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
74.7		5	0.34	5.98	17.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	L/300.00	Cs
cm			mm	mm	
74.7		7	-0.42	4.98	11.9

Travata: 1013 (Travata 1013) [157 (Nodo 157), 137 (Nodo 137)]

L = 150.0cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
75.0		5	0.35	6.00	17.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	L/300.00	Cs
cm			mm	mm	
75.0		7	-0.42	5.00	11.9

Travata: 1023 (Travata 1023) [137 (Nodo 137), 147 (Nodo 147)]

L = 100.9cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
50.5		7	-0.16	4.04	24.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	L/300.00	Cs
cm			mm	mm	
50.5		7	-0.21	3.36	15.7

Travata: 1043 (Travata 1043) [147 (Nodo 147), 132 (Nodo 132)]

L = 101.4cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
50.7		7	-0.17	4.06	24.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	L/300.00	Cs
cm			mm	mm	
50.7		7	-0.22	3.38	15.6

Travata: 1052 (Travata 1052) [132 (Nodo 132), 142 (Nodo 142)]

L = 101.3cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250.00	Cs
cm			mm	mm	
50.7		7	-0.17	4.05	24.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	L/300.00	Cs
cm			mm	mm	
50.7		7	-0.22	3.38	15.6

Travata: 1066 (Travata 1066) [142 (Nodo 142), 162 (Nodo 162)]

L = 101.3cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
50.6	7	-0.17	4.05	24.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
50.6	7	-0.22	3.38	15.6

Travata: 1073 (Travata 1073) [162 (Nodo 162), 167 (Nodo 167)]

L = 101.6cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
50.7	7	-0.16	4.05	24.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
50.7	7	-0.22	3.38	15.6

Travata: 1084 (Travata 1084) [167 (Nodo 167), 122 (Nodo 122)]

L = 101.6cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
50.8	7	-0.16	4.07	24.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
50.8	7	-0.22	3.39	15.6

Travata: 1096 (Travata 1096) [122 (Nodo 122), 127 (Nodo 127)]

L = 101.0cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
50.5	7	-0.16	4.04	24.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
50.5	7	-0.21	3.37	15.7

Travata: 1004 (Travata 1004) [153 (Nodo 153), 158 (Nodo 158)]

L = 149.5cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.7	5	0.30	5.98	19.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.7	7	-0.42	4.98	11.8

Travata: 1014 (Travata 1014) [158 (Nodo 158), 138 (Nodo 138)]

L = 150.0cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
75.0	5	0.31	6.00	19.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
75.0	7	-0.42	5.00	11.8

Travata: 1024 (Travata 1024) [138 (Nodo 138), 148 (Nodo 148)]

L = 107.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
53.5	7	-0.18	4.28	24.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
53.5	7	-0.24	3.57	14.9

Travata: 1034 (Travata 1034) [148 (Nodo 148), 133 (Nodo 133)]

L = 107.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
53.7	7	-0.18	4.30	24.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
53.7	7	-0.24	3.58	14.8

Travata: 1054 (Travata 1054) [133 (Nodo 133), 143 (Nodo 143)]

L = 107.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
53.7	7	-0.18	4.29	23.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
53.7	7	-0.24	3.58	14.8

Travata: 1063 (Travata 1063) [143 (Nodo 143), 163 (Nodo 163)]

L = 107.3cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
53.7	7	-0.18	4.29	23.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
53.7	7	-0.24	3.58	14.8

Travata: 1077 (Travata 1077) [163 (Nodo 163), 168 (Nodo 168)]

L = 107.3cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
53.6	7	-0.18	4.29	23.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
53.6	7	-0.24	3.58	14.8

Travata: 1086 (Travata 1086) [168 (Nodo 168), 123 (Nodo 123)]

L = 107.7cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
53.8	7	-0.18	4.31	24.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
53.8	7	-0.24	3.59	14.8

Travata: 1094 (Travata 1094) [123 (Nodo 123), 128 (Nodo 128)]

L = 107.0cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
53.5	7	-0.18	4.28	24.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
53.5	7	-0.24	3.57	14.9

Travata: 1005 (Travata 1005) [154 (Nodo 154), 159 (Nodo 159)]

L = 149.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.7	5	0.26	5.98	22.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.7	7	-0.43	4.98	11.7

Travata: 1015 (Travata 1015) [159 (Nodo 159), 139 (Nodo 139)]

L = 149.9cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.9	5	0.27	6.00	22.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.9	7	-0.43	5.00	11.6

Travata: 1025 (Travata 1025) [139 (Nodo 139), 149 (Nodo 149)]

L = 113.0cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
56.5	7	-0.19	4.52	23.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
56.5	7	-0.27	3.77	14.2

Travata: 1035 (Travata 1035) [149 (Nodo 149), 134 (Nodo 134)]

L = 113.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
56.7	7	-0.19	4.54	23.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
56.7	7	-0.27	3.78	14.1

Travata: 1045 (Travata 1045) [134 (Nodo 134), 144 (Nodo 144)]

L = 113.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
56.7	7	-0.20	4.54	23.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
56.7	7	-0.27	3.78	14.1

Travata: 1065 (Travata 1065) [144 (Nodo 144), 164 (Nodo 164)]

L = 113.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
56.7	7	-0.20	4.54	23.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
56.7	7	-0.27	3.78	14.1

Travata: 1074 (Travata 1074) [164 (Nodo 164), 169 (Nodo 169)]

L = 112.9cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
56.5	7	-0.19	4.52	23.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
56.5	7	-0.27	3.76	14.1

Travata: 1083 (Travata 1083) [169 (Nodo 169), 124 (Nodo 124)]

L = 119.1cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
59.6	7	-0.21	4.77	22.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
59.6	7	-0.30	3.97	13.5

Travata: 1007 (Travata 1007) [233 (Nodo 233) , 235 (Nodo 235)]

L = 149.5cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
74.7	7	-0.22	5.98	27.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
74.7	7	-0.44	4.98	11.3

Travata: 1017 (Travata 1017) [235 (Nodo 235) , 227 (Nodo 227)]

L = 149.8cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
74.9	7	-0.22	5.99	27.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
74.9	7	-0.44	4.99	11.3

Travata: 1027 (Travata 1027) [227 (Nodo 227) , 231 (Nodo 231)]

L = 125.0cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
62.5	7	-0.23	5.00	22.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
62.5	7	-0.32	4.17	12.9

Travata: 1037 (Travata 1037) [231 (Nodo 231) , 225 (Nodo 225)]

L = 125.4cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
62.7	7	-0.23	5.02	21.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
62.7	7	-0.33	4.18	12.8

Travata: 1047 (Travata 1047) [225 (Nodo 225) , 229 (Nodo 229)]

L = 125.4cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
62.7	7	-0.23	5.02	21.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
62.7	7	-0.33	4.18	12.8

Travata: 1057 (Travata 1057) [229 (Nodo 229) , 237 (Nodo 237)]

L = 125.5cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
62.8	7	-0.23	5.02	21.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
62.8	7	-0.33	4.18	12.8

Travata: 1067 (Travata 1067) [237 (Nodo 237) , 239 (Nodo 239)]

L = 125.1cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
62.6	7	-0.23	5.01	21.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
62.6	7	-0.33	4.17	12.8

Travata: 1085 (Travata 1085) [239 (Nodo 239) , 221 (Nodo 221)]

L = 125.8cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
62.9	7	-0.23	5.03	21.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
62.9	7	-0.33	4.19	12.8

Travata: 1093 (Travata 1093) [221 (Nodo 221) , 223 (Nodo 223)]

L = 125.2cm Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0.0cm$ Verifica: *Verificata*
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Comb.		δ_{max}	L/250.00	Cs
x	mm	mm	mm	
62.6	7	-0.23	5.01	21.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

Comb.		82	L/300.00	Cs
x	mm	mm	mm	
62.6	7	-0.33	4.17	12.8

Travata: 1008 (Travata 1008) [234 (Nodo 234), 236 (Nodo 236)]

$L = 149,5\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0,0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	7	δ_{max} mm	L/250,00 mm	Cs
cm	74.8			-0.24	5.98	24.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	δ_{max} mm	L/300,00 mm	Cs
cm	74.8	7		-0.44	4.98	11.2

Travata: 1018 (Travata 1018) [236 (Nodo 236), 228 (Nodo 228)]

$L = 149,7\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0,0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	7	δ_{max} mm	L/250,00 mm	Cs
cm	74.9			-0.24	5.99	24.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	δ_{max} mm	L/300,00 mm	Cs
cm	74.9	7		-0.45	4.99	11.2

Travata: 1028 (Travata 1028) [228 (Nodo 228), 232 (Nodo 232)]

$L = 131,0\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0,0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	7	δ_{max} mm	L/250,00 mm	Cs
cm	65.5			-0.25	5.24	21.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	δ_{max} mm	L/300,00 mm	Cs
cm	65.5	7		-0.35	4.37	12.3

Travata: 1038 (Travata 1038) [232 (Nodo 232), 226 (Nodo 226)]

$L = 131,4\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0,0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	7	δ_{max} mm	L/250,00 mm	Cs
cm	65.7			-0.25	5.26	21.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	δ_{max} mm	L/300,00 mm	Cs
cm	65.7	7		-0.36	4.38	12.2

Travata: 1048 (Travata 1048) [226 (Nodo 226), 230 (Nodo 230)]

$L = 131,4\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0,0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	7	δ_{max} mm	L/250,00 mm	Cs
cm	65.7			-0.25	5.26	20.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	δ_{max} mm	L/300,00 mm	Cs
cm	65.7	7		-0.36	4.38	12.2

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Travata: 1058 (Travata 1058) [230 (Nodo 230), 238 (Nodo 238)]

$L = 131,6\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0,0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	7	δ_{max} mm	L/250,00 mm	Cs
cm	65.8			-0.25	5.26	20.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	δ_{max} mm	L/300,00 mm	Cs
cm	65.8	7		-0.36	4.39	12.2

Travata: 1068 (Travata 1068) [238 (Nodo 238), 240 (Nodo 240)]

$L = 131,1\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0,0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	7	δ_{max} mm	L/250,00 mm	Cs
cm	65.5			-0.25	5.24	20.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	δ_{max} mm	L/300,00 mm	Cs
cm	65.5	7		-0.36	4.37	12.2

Travata: 1078 (Travata 1078) [240 (Nodo 240), 222 (Nodo 222)]

$L = 131,8\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0,0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	7	δ_{max} mm	L/250,00 mm	Cs
cm	65.9			-0.25	5.27	20.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	δ_{max} mm	L/300,00 mm	Cs
cm	65.9	7		-0.36	4.39	12.2

Travata: 1092 (Travata 1092) [222 (Nodo 222), 224 (Nodo 224)]

$L = 131,2\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0,0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	7	δ_{max} mm	L/250,00 mm	Cs
cm	65.6			-0.25	5.25	20.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	δ_{max} mm	L/300,00 mm	Cs
cm	65.6	7		-0.36	4.37	12.2

Travata: 1009 (Travata 1009) [333 (Nodo 333), 335 (Nodo 335)]

$L = 149,5\text{cm}$ Crit.Prog: Acciaio_Flessione $\delta\epsilon = 0,0\text{cm}$ Verifica: **Verificata**
Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	7	δ_{max} mm	L/250,00 mm	Cs
cm	74.7			-0.26	5.98	23.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	82	δ_{max} mm	L/300,00 mm	Cs
cm	74.7	7		-0.45	4.98	11.1

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Travata: 1019 (Travata 1019) [335 (Nodo 335), 327 (Nodo 327)]
L = 149.6cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.8	7	-0.26	5.98	23.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.8	7	-0.45	4.99	11.1

Travata: 1029 (Travata 1029) [327 (Nodo 327), 331 (Nodo 331)]
L = 137.1cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.6	7	-0.26	5.48	21.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
68.6	7	-0.39	4.57	11.8

Travata: 1039 (Travata 1039) [331 (Nodo 331), 325 (Nodo 325)]
L = 137.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.7	7	-0.27	5.50	20.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
68.7	7	-0.39	4.58	11.7

Travata: 1049 (Travata 1049) [325 (Nodo 325), 329 (Nodo 329)]
L = 137.5cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.7	7	-0.27	5.50	20.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
68.7	7	-0.39	4.58	11.7

Travata: 1059 (Travata 1059) [329 (Nodo 329), 337 (Nodo 337)]
L = 137.6cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.8	7	-0.27	5.50	20.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
68.8	7	-0.39	4.59	11.7

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Travata: 1069 (Travata 1069) [337 (Nodo 337), 339 (Nodo 339)]
L = 137.0cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.5	7	-0.27	5.48	20.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
68.5	7	-0.39	4.57	11.7

Travata: 1079 (Travata 1079) [339 (Nodo 339), 321 (Nodo 321)]
L = 137.8cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.9	7	-0.27	5.51	20.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
68.9	7	-0.39	4.59	11.7

Travata: 1089 (Travata 1089) [321 (Nodo 321), 323 (Nodo 323)]
L = 137.3cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.6	7	-0.27	5.49	20.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
68.6	7	-0.39	4.58	11.7

Travata: 1010 (Travata 1010) [334 (Nodo 334), 336 (Nodo 336)]
L = 149.5cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.7	7	-0.26	5.98	23.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.7	7	-0.45	4.98	11.1

Travata: 1020 (Travata 1020) [336 (Nodo 336), 328 (Nodo 328)]
L = 149.5cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: Verificata

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.8	7	-0.26	5.98	23.0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.8	7	-0.45	4.98	11.1

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Travata: 1030 (Travata 1030) [328 (Nodo 328) , 332 (Nodo 332)]
L = 143.1cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.6	7	-0.27	5.73	21.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
71.6	7	-0.42	4.77	11.4

Travata: 1040 (Travata 1040) [332 (Nodo 332) , 326 (Nodo 326)]
L = 143.4cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.7	7	-0.27	5.74	20.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
71.7	7	-0.42	4.78	11.3

Travata: 1050 (Travata 1050) [326 (Nodo 326) , 330 (Nodo 330)]
L = 143.5cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.7	7	-0.28	5.74	20.7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
71.7	7	-0.42	4.78	11.3

Travata: 1060 (Travata 1060) [330 (Nodo 330) , 338 (Nodo 338)]
L = 143.7cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.8	7	-0.28	5.75	20.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
71.8	7	-0.42	4.79	11.3

Travata: 1070 (Travata 1070) [338 (Nodo 338) , 340 (Nodo 340)]
L = 143.0cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.5	7	-0.28	5.72	20.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
71.5	7	-0.42	4.77	11.3

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Travata: 1080 (Travata 1080) [340 (Nodo 340) , 322 (Nodo 322)]
L = 143.9cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
72.0	7	-0.28	5.76	20.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
72.0	7	-0.43	4.80	11.3

Travata: 1090 (Travata 1090) [322 (Nodo 322) , 324 (Nodo 324)]
L = 143.3cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
71.7	7	-0.28	5.73	20.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
71.7	7	-0.42	4.78	11.3

Travata: 1011 (Travata 1011) [311 (Nodo 311) , 312 (Nodo 312)]
L = 149.5cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
74.7	7	-0.37	5.98	16.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
74.7	7	-0.48	4.98	10.5

Travata: 1021 (Travata 1021) [312 (Nodo 312) , 313 (Nodo 313)]
L = 137.5cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
68.7	7	-0.33	5.50	16.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
68.7	7	-0.41	4.58	11.3

Travata: 1031 (Travata 1031) [313 (Nodo 313) , 314 (Nodo 314)]
L = 161.2cm Crit.Prog: Acciaio_Flessione $\delta\hat{x} = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
80.6	7	-0.41	6.45	15.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
80.6	7	-0.55	5.37	9.79

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Travata: 1041 (Travata 1041) [314 (Nodo 314) , 315 (Nodo 315)]
L = 149,3cm Crit.Prog: Acciaio_Flessione $\hat{\alpha} = 0,0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250,00	Cs
cm			mm	mm	
74,7		7	-0,38	5,97	15,7

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_2	L/300,00	Cs
cm			mm	mm	
74,7		7	-0,48	4,98	10,4

Travata: 1051 (Travata 1051) [315 (Nodo 315) , 316 (Nodo 316)]
L = 137,5cm Crit.Prog: Acciaio_Flessione $\hat{\alpha} = 0,0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250,00	Cs
cm			mm	mm	
68,8		7	-0,34	5,50	16,2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_2	L/300,00	Cs
cm			mm	mm	
68,8		7	-0,41	4,58	11,2

Travata: 1061 (Travata 1061) [316 (Nodo 316) , 317 (Nodo 317)]
L = 149,7cm Crit.Prog: Acciaio_Flessione $\hat{\alpha} = 0,0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250,00	Cs
cm			mm	mm	
74,9		7	-0,39	5,99	15,5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_2	L/300,00	Cs
cm			mm	mm	
74,9		7	-0,48	4,99	10,4

Travata: 1071 (Travata 1071) [317 (Nodo 317) , 318 (Nodo 318)]
L = 160,9cm Crit.Prog: Acciaio_Flessione $\hat{\alpha} = 0,0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250,00	Cs
cm			mm	mm	
80,5		7	-0,43	6,44	15,1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_2	L/300,00	Cs
cm			mm	mm	
80,5		7	-0,55	5,36	9,75

Travata: 1081 (Travata 1081) [318 (Nodo 318) , 319 (Nodo 319)]
L = 149,9cm Crit.Prog: Acciaio_Flessione $\hat{\alpha} = 0,0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250,00	Cs
cm			mm	mm	
75,0		7	-0,39	6,00	15,5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_2	L/300,00	Cs
cm			mm	mm	
75,0		7	-0,48	5,00	10,4

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Travata: 1091 (Travata 1091) [319 (Nodo 319) , 320 (Nodo 320)]
L = 137,4cm Crit.Prog: Acciaio_Flessione $\hat{\alpha} = 0,0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250,00	Cs
cm			mm	mm	
68,7		7	-0,34	5,49	16,1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_2	L/300,00	Cs
cm			mm	mm	
68,7		7	-0,41	4,58	11,2

Travata: 8010 (Travata 8010) [28 (Nodo 28) , 30 (Nodo 30)]
L = 924,3cm Crit.Prog: Acciaio_Flessione $\hat{\alpha} = 0,0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_{max}	L/250,00	Cs
cm			mm	mm	
224,6		7	-0,68	36,97	54,0

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x		Comb.	δ_2	L/300,00	Cs
cm			mm	mm	
224,6		7	-0,53	30,81	57,8

Verifica delle travi (Stati limite esercizio)

Scenario di calcolo : Set NT_SLD_A2_STR/GEO

Trave di Fond. : 9007 [1.2] Pilastrate [1.2]

Sez. R: By= 60,0 cm Bz= 100,0 cm L= 149,5 cm Ln= 149,5 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0,0	271	--	12,06	12,06	-0	25	--	--	8	1	Si	>100
14,9	--	766	12,06	12,06	--	--	-1	71	7	2	Si	51,0
74,7	--	2988	12,06	12,06	--	--	-5	275	6	8	Si	13,1
134,5	--	3602	12,06	12,06	--	--	-6	332	6	8	Si	10,8
149,5	--	3502	12,06	12,06	--	--	-5	323	6	8	Si	11,2

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0,0	--	105	12,06	12,06	--	--	-0	10	14	14	Si	>100
14,9	--	495	12,06	12,06	--	--	-1	46	14	14	Si	78,9
74,7	--	1181	12,06	12,06	--	--	-2	109	14	14	Si	33,1
134,5	--	583	12,06	12,06	--	--	-1	54	14	14	Si	66,9
149,5	--	250	12,06	12,06	--	--	-0	23	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0,400 Wamm Qp[mm]=0,300

X	M	Act	Aft	pAft	S _{trmax}	σ_{fibred}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0,0	24	0,1	12,06	30,16	22,4	2	0,000	0,000	13(Fr)	Si	>100
0,0	105	0,1	12,06	30,16	22,4	10	0,001	0,001	14(Qp)	Si	>100
14,9	495	0,1	12,06	30,16	22,4	46	0,003	0,003	14(Qp)	Si	>100
14,9	473	0,1	12,06	30,16	22,4	44	0,003	0,003	13(Fr)	Si	>100
74,7	1181	0,1	12,06	30,16	22,4	109	0,007	0,007	14(Qp)	Si	43,1
74,7	1181	0,1	12,06	30,16	22,4	109	0,007	0,007	9(Fr)	Si	57,5
134,5	583	0,1	12,06	30,16	22,4	54	0,003	0,003	14(Qp)	Si	87,3
134,5	558	0,1	12,06	30,16	22,4	51	0,003	0,003	12(Fr)	Si	>100
149,5	250	0,1	12,06	30,16	22,4	23	0,001	0,001	14(Qp)	Si	>100

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Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.0 cm Ln= 89.0 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma f_a[kg/cmq]=3600$

X	M+	M-	Act	M+	M-	Afsup	Afinf	cmq	cmq	kg/cmq	kg/cmq	σf+	σf-	σc-	σc+	σf+	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	--	625	12.06	12.06	--	--	--	--	58	6	5	5	5	5	5	5	5	5	5	62.5
8.9	--	--	875	12.06	12.06	--	--	--	--	81	7	5	5	5	5	5	5	5	5	5	44.6
44.5	--	--	1302	12.06	12.06	--	--	--	--	120	7	5	5	5	5	5	5	5	5	5	30.0
80.1	--	--	800	12.06	12.06	--	--	--	--	74	6	8	8	8	8	8	8	8	8	8	48.8
89.0	--	--	588	12.06	12.06	--	--	--	--	54	6	8	8	8	8	8	8	8	8	8	66.4

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma f_a[kg/cmq]=3600$

X	M+	M-	Act	M+	M-	Afsup	Afinf	cmq	cmq	kg/cmq	kg/cmq	σf+	σf-	σc-	σc+	σf+	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	--	287	12.06	12.06	--	--	--	--	26	14	14	14	14	14	14	14	14	14	14	>100
8.9	--	--	452	12.06	12.06	--	--	--	--	42	14	14	14	14	14	14	14	14	14	14	86.4
44.5	--	--	735	12.06	12.06	--	--	--	--	68	14	14	14	14	14	14	14	14	14	14	53.1
80.1	--	--	344	12.06	12.06	--	--	--	--	32	14	14	14	14	14	14	14	14	14	14	>100
89.0	--	--	130	12.06	12.06	--	--	--	--	12	14	14	14	14	14	14	14	14	14	14	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	cm	cm	kg/cmq	mm	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cmq	cm	cm	mm	kg/cmq	mm	mm			
0.0	264	0.1	12.06	30.16	22.4	22.4	24	24	0.002	0.002	12(Fr)	Si	>100
0.0	287	0.1	12.06	30.16	22.4	22.4	26	26	0.002	0.002	14(Qp)	Si	>100
8.9	452	0.1	12.06	30.16	22.4	22.4	42	42	0.003	0.003	14(Qp)	Si	>100
8.9	435	0.1	12.06	30.16	22.4	22.4	40	40	0.003	0.003	13(Fr)	Si	>100
44.5	735	0.1	12.06	30.16	22.4	22.4	68	68	0.004	0.004	14(Qp)	Si	69.3
44.5	735	0.1	12.06	30.16	22.4	22.4	68	68	0.004	0.004	9(Fr)	Si	92.4
80.1	344	0.1	12.06	30.16	22.4	22.4	32	32	0.002	0.002	14(Qp)	Si	>100
80.1	344	0.1	12.06	30.16	22.4	22.4	32	32	0.002	0.002	9(Fr)	Si	>100
89.0	130	0.1	12.06	30.16	22.4	22.4	12	12	0.001	0.001	14(Qp)	Si	>100
89.0	130	0.1	12.06	30.16	22.4	22.4	12	12	0.001	0.001	9(Fr)	Si	>100

Trave di Fond.: 9008 | 211.. 212 | Pilastro [211.. 212]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.5 cm Ln= 149.5 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma f_a[kg/cmq]=3600$

X	M+	M-	Act	M+	M-	Afsup	Afinf	cmq	cmq	kg/cmq	kg/cmq	σf+	σf-	σc-	σc+	σf+	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	27	39	12.06	12.06	12.06	-0	2	4	8	8	6	6	6	6	6	6	6	6	6	6	>100
14.9	--	--	206	12.06	12.06	--	--	--	--	19	8	1	1	1	1	1	1	1	1	1	>100
74.7	--	--	687	12.06	12.06	--	--	--	--	63	6	2	2	2	2	2	2	2	2	2	56.9
134.5	--	--	734	12.06	12.06	--	--	--	--	68	6	5	5	5	5	5	5	5	5	5	53.2
149.5	--	--	679	12.06	12.06	--	--	--	--	63	6	5	5	5	5	5	5	5	5	5	57.6

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma f_a[kg/cmq]=3600$

X	M+	M-	Act	M+	M-	Afsup	Afinf	cmq	cmq	kg/cmq	kg/cmq	σf+	σf-	σc-	σc+	σf+	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	--	29	12.06	12.06	--	--	--	--	3	14	14	14	14	14	14	14	14	14	14	>100
14.9	--	--	142	12.06	12.06	--	--	--	--	13	14	14	14	14	14	14	14	14	14	14	>100
74.7	--	--	390	12.06	12.06	--	--	--	--	36	14	14	14	14	14	14	14	14	14	14	>100
134.5	--	--	334	12.06	12.06	--	--	--	--	31	14	14	14	14	14	14	14	14	14	14	>100
149.5	--	--	275	12.06	12.06	--	--	--	--	25	14	14	14	14	14	14	14	14	14	14	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	cm	cm	σf _{inf}	kg/cmq	mm	Wk	Cb	Ver.	Cs
cm	kg·m	mq	cmq	cm	cm	cm	mm							
0.0	19	0.1	12.06	30.16	22.4	22.4	2	0.000	0.000	0.000	13(Fr)	Si	>100	
0.0	29	0.1	12.06	30.16	22.4	22.4	3	0.000	0.000	0.000	14(Qp)	Si	>100	
14.9	142	0.1	12.06	30.16	22.4	22.4	13	0.001	0.001	0.001	14(Qp)	Si	>100	
14.9	136	0.1	12.06	30.16	22.4	22.4	13	0.001	0.001	0.001	13(Fr)	Si	>100	
74.7	390	0.1	12.06	30.16	22.4	22.4	36	0.002	0.002	0.002	14(Qp)	Si	>100	

X	M	Act	M+	M-	Afsup	Afinf	pAft	S _{max}	cmq	cmq	kg/cmq	kg/cmq	σf+	σf-	σc-	σc-	σf+	σf-	Wk	Cb	Ver.	Cs
74.7	390	0.1	12.06	12.06	30.16	12.06	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	>100
134.5	334	0.1	12.06	12.06	30.16	12.06	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	>100
134.5	321	0.1	12.06	12.06	30.16	12.06	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	>100
149.5	275	0.1	12.06	12.06	30.16	12.06	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	>100
149.5	256	0.1	12.06	12.06	30.16	12.06	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	22.4	>100

Trave di Fond.: 9008 | 212.. 213 | Pilastro [212.. 213]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.5 cm Ln= 149.5 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma f_a[kg/cmq]=3600$

X	M+	M-	Act	M+	M-	Afsup	Afinf	cmq	cmq	kg/cmq	kg/cmq	σf+	σf-	σc-	σc-	σf+	σf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	kg*m	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	--	660	12.06	12.06	--	--	--	--	61	6	5	5	5	5	5	5	5	5	5	59.2
14.9	--	--	839	12.06	12.06	--	--	--	--	77	6	5	5	5	5	5	5	5	5	5	46.5
74.7	--	--	1285	12.06	12.06	--	--	--	--	118	6	5	5	5	5	5	5	5	5	5	30.4
134.5	--	--	1295	12.06	12.06	--	--	--	--	119	6	5	5	5	5	5	5	5	5	5	30.2
149.5	--	--	1239	12.06	12.06	--	--	--	--	114	6	8	8	8	8	8	8	8	8	8	31.5

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma f_a[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σv+ kg/cmq	σf+ kg/cmq	σv- kg/cmq	σf- kg/cmq	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	--	--	--	--				
0.0	--	--	305	12.06	--	--	-0	28	14	14	Si	>100
14.9	--	--	366	12.06	--	--	-1	34	14	14	Si	>100
74.7	--	--	439	12.06	--	--	-1	40	14	14	Si	89.0
134.5	--	--	252	12.06	--	--	-0	23	14	14	Si	>100
149.5	--	--	165	12.06	--	--	-0	15	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	cm	kg·m	Act	mq	Aft	pAft	S _{max}	cm	kg/cmq	Wd	Wk	Ch	Ver.	Cs
	0.0	121	0.1	12.06	30.16	22.4	22.4	11	0.001	mm	0.001	12(Fr)	Si	>100
	0.0	195	0.1	12.06	30.16	22.4	22.4	18	0.001	mm	0.001	14(Qp)	Si	>100
	14.9	244	0.1	12.06	30.16	22.4	22.4	22	0.001	mm	0.001	14(Qp)	Si	>100
	14.9	163	0.1	12.06	30.16	22.4	22.4	27	0.001	mm	0.001	12(Fr)	Si	>100
	74.6	289	0.1	12.06	30.16	22.4	22.4	15	0.002	mm	0.002	14(Qp)	Si	>100
	74.6	181	0.1	12.06	30.16	22.4	22.4	17	0.001	mm	0.001	12(Fr)	Si	>100
	134.2	95	0.1	12.06	30.16	22.4	22.4	9	0.001	mm	0.001	14(Qp)	Si	>100
	134.2	-40	0.1	12.06	30.16	22.4	22.4	4	0.000	mm	0.000	12(Fr)	Si	>100
	149.2	10	0.1	12.06	30.16	22.4	22.4	1	0.000	mm	0.000	14(Qp)	Si	>100
	149.2	7	0.1	12.06	30.16	22.4	22.4	1	0.000	mm	0.000	10(Fr)	Si	>100

Trave di Fond. : 9008 | 214, 215 | Pilastrate [214, 215]

Sez. R:	$B_V = 60.0 \text{ cm}$	$B_Z = 100.0 \text{ cm}$	$L = 149.4 \text{ cm}$	$L_n = 149.4 \text{ cm}$	Terreno: Terreno I
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Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma \text{ca}[\text{k}\sigma/\text{cmq}] = 149 \text{ } \sigma \text{fa}[\text{k}\sigma/\text{cmq}] = 3600$

	Composizione chimica, Oca	kg/ene	M-	M+	A _{finf}	A _{sup}	A _{finf}	A _{sup}
X								

λ	m ^a	kg ^a m	nm ^b	cmq	nmq	cmq	gm ^c	kg/cmq	kg/cmq	Cm ^d	Cm ^e	Vol.	C ^f
0.0	--	--	1761	12.06	12.06	--	--	--	162	6	8	Si	22.2
14.9	--	--	1926	12.06	12.06	--	--	--	-3	178	6	Si	20.3
74.7	--	--	2310	12.06	12.06	--	--	--	-4	213	6	Si	16.9
134.5	7	2260	12.06	12.06	12.06	-0	1	-3	208	6	8	Si	17.3
149.4	104	2178	12.06	12.06	12.06	-0	10	-3	201	6	8	Si	17.9

Combinazione QP: $\sigma_{ca}[\text{kg/cmq}] = 112 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M _*	A _{sup}	A _{inf}	σ ₊	σ ₋	σ _f	Cb+	Ch-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	34	12.06	12.06	--	-0	3	14	14	Si	>100
14.9	--	89	12.06	12.06	--	--	8	14	14	Si	>100
74.7	--	161	12.06	12.06	--	-0	15	14	14	Si	>100
134.5	--	3	12.06	12.06	--	--	0	14	14	Si	>100
149.4	72	--	12.06	12.06	-0	--	--	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	orfned	Wd	Wk	Ch	Ver.	Cs
cm	kg*	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	34	0.1	12.06	30.16	22.4	3	0.000	0.000	10(Fr)	Si	>100
0.0	34	0.1	12.06	30.16	22.4	3	0.000	0.000	14(Qp)	Si	>100
14.9	89	0.1	12.06	30.16	22.4	8	0.001	0.001	14(Qp)	Si	>100
14.9	-55	0.1	12.06	30.16	22.4	5	0.000	0.000	12(Fr)	Si	>100
74.7	161	0.1	12.06	30.16	22.4	15	0.001	0.001	14(Qp)	Si	>100
74.7	-2	0.1	12.06	30.16	22.4	0	0.000	0.000	12(Fr)	Si	>100
134.5	3	0.1	12.06	30.16	22.4	0	0.000	0.000	14(Qp)	Si	>100
134.5	1	0.1	12.06	30.16	22.4	0	0.000	0.000	10(Fr)	Si	>100
149.4	-72	0.1	12.06	30.16	22.4	7	0.000	0.000	14(Qp)	Si	>100
149.4	-72	0.1	12.06	30.16	22.4	7	0.000	0.000	9(Fr)	Si	>100

Trave di Fond. : 9008 | 215, 216 | Pilastrate [215, 216]

Sez. R:	$B_V = 60.0 \text{ cm}$	$B_Z = 100.0 \text{ cm}$	$L = 149.5 \text{ cm}$	$L_n = 149.5 \text{ cm}$	Terreno: Terreno I
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Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma \alpha [k\sigma/\text{cm}] = 149 \sigma f [k\sigma/\text{cm}] = 3600$

X	M+	M-	Afsup	Afinf	σ^+

λ	cm	kg ⁻¹ m ⁻¹	kg ⁻¹ m ²	cm ² /mol	dm ³ /mol	g/cm ³	g/mol	C _D ^a	val.	C _S
0.0	0.0	113	2141	12.06	12.06	-0	10	-3	6	8 Si 18.2
14.9	33	2270	12.06	12.06	12.06	-0	3	-4	209	6 Si 17.2
74.7	--	2512	12.06	12.06	12.06	--	--	-4	232	6 Si 15.5
134.5	64	2319	12.06	12.06	12.06	-0	6	-4	214	6 Si 16.8
149.5	153	2202	12.06	12.06	12.06	-0	14	-3	203	6 Si 17.7

Combinazione OP: $\sigma_{ca}[\text{kg/cmq}] = 112 \sigma_{fa}[\text{kg/cmq}] = 3600$

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X	M+	M-	Afup	Afin	$\sigma_{\text{c+}}$	$\sigma_{\text{c-}}$	$\sigma_{\text{c+}}$	$\sigma_{\text{c-}}$	kg/cmq	kg/cmq	Cb+	Cb-	Ver.	CS
0.0	62	--	12.06	12.06	--	6	--	--	--	--	14	14	Si	>100
14.9	--	1	12.06	12.06	--	--	--	--	--	0	14	14	Si	>100
74.7	--	111	12.06	12.06	--	--	--	--	10	14	14	14	Si	>100
134.5	6	--	12.06	12.06	--	1	--	--	--	14	14	14	Si	>100
149.5	71	--	12.06	12.06	--	7	--	--	--	14	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Afi	pAfi	S _{max}	orined	Wd	Wk	Cb	Ver.	Cs
cm	kg ³ m	mq	cmq	cm	cm		mm	mm			
0.0	-62	0.1	12.06	30.16	22.4	6	0.000	0.000	9(Fr)	Si	>100
0.0	-62	0.1	12.06	30.16	22.4	6	0.000	0.000	14(Qp)	Si	>100
14.9	1	0.1	12.06	30.16	22.4	0	0.000	0.000	14(Qp)	Si	>100
14.9	-1	0.1	12.06	30.16	22.4	0	0.000	10(Fr)	Si	>100	
74.7	111	0.1	12.06	30.16	22.4	10	0.001	0.001	14(Qp)	Si	>100
74.7	-78	0.1	12.06	30.16	22.4	7	0.000	0.000	12(Fr)	Si	>100
134.5	-6	0.1	12.06	30.16	22.4	1	0.000	0.000	14(Qp)	Si	>100
134.5	-6	0.1	12.06	30.16	22.4	1	0.000	0.000	9(Fr)	Si	>100
149.5	-71	0.1	12.06	30.16	22.4	7	0.000	0.000	14(Qp)	Si	>100
149.5	-71	0.1	12.06	30.16	22.4	7	0.000	0.000	9(Fr)	Si	>100

Travedi Fond.: 9008 | 216, 217 | Pilastrate | 216, 217 |

Sez. R: Bv=60.0 cm B7=100.0 cm L=149.7 cm Ln=149.7 cm

Criterio : C/S TraviFondazione

Combinazione B ara: $\sigma_{ca}[\text{kg}/\text{cm}^2]=149$ $\sigma_{fa}[\text{kg}/\text{cm}^2]=3600$

X	M+	M-	M-	Atsup	Atinf	ec+	ec-	sf+	sf-	Cb+	Cb-	Ver.	CS
cm	kg ³ m	kg ³ m	kg ³ m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	195	195	195	12.06	12.06	-0	18	-3	198	6	8	Si	18.2
0.0	2147	2147	2147	12.06	12.06	-0	18	-3	198	6	8	Si	18.2
15.0	88	88	88	2271	12.06	12.06	-0	8	209	6	8	Si	17.2
74.9	--	2491	2491	12.06	12.06	--	8	-4	230	6	8	Si	15.7
134.8	--	2269	2269	12.06	12.06	--	8	--	209	6	8	Si	17.2
149.7	--	2142	2142	12.06	12.06	--	8	-3	197	6	8	Si	18.2

Combinazione OP: $\sigma_{ca}[\text{kg/cmq}] = 112$ $\sigma_{fa}[\text{kg/cmq}] = 3600$

X	cm	M _z kg*m	ME kg*m	A _{sup} cmq	A _{inf} cmq	σ _c kg/cmq	σ _f kg/cmq	σ _c kg/cmq	Cb+	Cb-	Ver.	CS
0.0	0.0	79	--	12.06	12.06	-0	7	--	14	14	Si	>100
15.0	6	--	--	12.06	12.06	-0	1	--	14	14	Si	>100
74.9	74.9	--	144	12.06	12.06	--	--	-0	13	14	Si	>100
134.8	134.8	--	67	12.06	12.06	--	--	-0	6	14	Si	>100
149.7	149.7	--	12	12.06	12.06	--	--	-0	1	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Op[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	formed	Wd	Wk	Cb	Ver.	Cs
cm	kg·m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-79	0.1	12.06	30.16	22.4	7	0.000	0.000	9(Fr)	Si	>100
-79	0	0.1	12.06	30.16	22.4	7	0.000	0.000	14(Qp)	Si	>100
15.0	-6	0.1	12.06	30.16	22.4	1	0.000	0.000	14(Qp)	Si	>100
15.0	-6	0.1	12.06	30.16	22.4	1	0.000	0.000	9(Fr)	Si	>100
74.9	144	0.1	12.06	30.16	22.4	13	0.001	0.001	14(Qp)	Si	>100
74.9	-38	0.1	12.06	30.16	22.4	3	0.000	0.000	12(Fr)	Si	>100
134.8	67	0.1	12.06	30.16	22.4	6	0.000	0.000	14(Qp)	Si	>100
134.8	67	0.1	12.06	30.16	22.4	6	0.000	0.000	9(Fr)	Si	>100
149.7	12	0.1	12.06	30.16	22.4	1	0.000	0.000	14(Qp)	Si	>100
149.7	9	0.1	12.06	30.16	22.4	1	0.000	0.000	10(Fr)	Si	>100

Travedi Fond.: 9008 | 217, 218 | Pilastrate | 217, 218 |

Sez. R:	Bv=60.0 cm	B7=100.0 cm	L=148.9 cm	In=148.9 cm
<p>Sez. R: Bv=60.0 cm B7=100.0 cm L=148.9 cm In=148.9 cm</p>				

Criterio: CIS TraviFondazione

Combinazione Rara: $\sigma_{ca} [k\alpha/\text{cm}] = 149$ $\sigma_{fa} [k\alpha/\text{cm}] = 3600$

[illegible]

X	M+	M-	M- kg*m	M- kg*m	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
0.0	46	2075	12.06	12.06	-0	4	-3	191	-3	191	6	8	Si	18.8
14.9	--	2171	12.06	12.06	--	--	-3	200	--	200	6	8	Si	18.0
74.5	--	2272	12.06	12.06	--	--	-4	209	--	209	6	8	Si	17.2
134.0	--	1934	12.06	12.06	--	--	-3	178	--	178	6	8	Si	20.2
148.9	--	1781	12.06	12.06	--	--	-3	164	--	164	6	8	Si	21.9

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M- kg*m	M- kg*m	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	mm	mm	Ver.	CS
0.0	8	--	12.06	12.06	-0	1	--	--	--	--	14	14	Si	>100
14.9	--	74	12.06	12.06	--	--	-0	7	--	7	14	14	Si	>100
74.5	--	255	12.06	12.06	--	--	-0	24	--	24	14	14	Si	>100
134.0	--	206	12.06	12.06	--	--	-0	19	--	19	14	14	Si	>100
148.9	--	157	12.06	12.06	--	--	-0	14	--	14	14	14	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M- kg*m	M- kg*m	Act	Aft	pAft	S _{max}	σf _{med}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	cm	kg/cmq	mm	mm	mm	Ver.	Cs
0.0	-8	0.1	12.06	30.16	22.4	1	0.000	0.000	0.000	0.000	9(Fr)	Si	>100
0.0	-8	0.1	12.06	30.16	22.4	1	0.000	0.000	0.000	0.000	14(Qp)	Si	>100
14.9	74	0.1	12.06	30.16	22.4	7	0.000	0.000	0.000	0.000	14(Qp)	Si	>100
14.9	74	0.1	12.06	30.16	22.4	7	0.000	0.000	0.000	0.000	9(Fr)	Si	>100
74.5	255	0.1	12.06	30.16	22.4	24	0.002	0.002	0.002	0.002	14(Qp)	Si	>100
74.5	115	0.1	12.06	30.16	22.4	11	0.001	0.001	0.001	0.001	12(Fr)	Si	>100
134.0	206	0.1	12.06	30.16	22.4	19	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
134.0	92	0.1	12.06	30.16	22.4	8	0.001	0.001	0.001	0.001	12(Fr)	Si	>100
148.9	157	0.1	12.06	30.16	22.4	14	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
148.9	49	0.1	12.06	30.16	22.4	5	0.000	0.000	0.000	0.000	12(Fr)	Si	>100

Trave di Fond. : 9008 | 218 , 219 | Pilastro [218 , 219]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 150.0 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	M- kg*m	M- kg*m	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	mm	mm	Ver.	CS
0.0	--	1699	12.06	12.06	--	--	-3	157	--	157	6	8	Si	23.0
15.0	--	1766	12.06	12.06	--	--	-3	163	--	163	6	8	Si	22.1
75.0	--	1758	12.06	12.06	--	--	-3	162	--	162	6	8	Si	22.2
135.0	--	1324	12.06	12.06	--	--	-2	122	--	122	6	8	Si	29.5
150.0	--	1150	12.06	12.06	--	--	-2	106	--	106	6	8	Si	34.0

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M- kg*m	M- kg*m	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	mm	mm	Ver.	CS
0.0	--	134	12.06	12.06	--	--	-0	12	--	12	14	14	Si	>100
15.0	--	219	12.06	12.06	--	--	-0	20	--	20	14	14	Si	>100
75.0	--	406	12.06	12.06	--	--	-1	37	--	37	14	14	Si	96.1
135.0	--	339	12.06	12.06	--	--	-1	31	--	31	14	14	Si	>100
150.0	--	281	12.06	12.06	--	--	-0	26	--	26	14	14	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M- kg*m	M- kg*m	Act	Aft	pAft	S _{max}	σf _{med}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	cm	kg/cmq	mm	mm	mm	Ver.	Cs
0.0	21	0.1	12.06	30.16	22.4	2	0.000	0.000	0.000	0.000	12(Fr)	Si	>100
0.0	134	0.1	12.06	30.16	22.4	12	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
15.0	219	0.1	12.06	30.16	22.4	20	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
15.0	115	0.1	12.06	30.16	22.4	11	0.001	0.001	0.001	0.001	12(Fr)	Si	>100
75.0	406	0.1	12.06	30.16	22.4	37	0.002	0.002	0.002	0.002	14(Qp)	Si	>100
75.0	336	0.1	12.06	30.16	22.4	31	0.002	0.002	0.002	0.002	12(Fr)	Si	>100
135.0	339	0.1	12.06	30.16	22.4	31	0.002	0.002	0.002	0.002	14(Qp)	Si	>100
135.0	300	0.1	12.06	30.16	22.4	28	0.002	0.002	0.002	0.002	12(Fr)	Si	>100
150.0	281	0.1	12.06	30.16	22.4	26	0.002	0.002	0.002	0.002	14(Qp)	Si	>100
150.0	248	0.1	12.06	30.16	22.4	23	0.001	0.001	0.001	0.001	12(Fr)	Si	>100

Trave di Fond. : 9008 | 219 , 220 | Pilastro [219 , 220]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.3 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M+	M-	M- kg*m	M- kg*m	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	mm	mm	Ver.	CS
0.0	--	1059	12.06	12.06	--	--	-2	98	--	98	6	8	Si	36.9
14.9	--	1070	12.06	12.06	--	--	-2	99	--	99	6	8	Si	36.5
74.7	--	868	12.06	12.06	--	--	-1	80	--	80	6	8	Si	45.0
134.4	--	316	12.06	12.06	--	--	-0	29	--	29	5	7	Si	>100
149.3	--	153	12.06	12.06	--	--	-0	14	--	14	5	7	Si	>100

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	M+	M-	M- kg*m	M- kg*m	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	mm	mm	Ver.	CS
0.0	--	251	12.06	12.06	--	--	-0	23	--	23	14	14	Si	>100
14.9	--	313	12.06	12.06	--	--	-0	29	--	29	14	14	Si	>100
74.7	--	383	12.06	12.06	--	--	-1	35	--	35	14	14	Si	>100
134.4	--	156	12.06	12.06	--	--	-0	14	--	14	14	14	Si	>100
149.3	--	50	12.06	12.06	--	--	-0	5	--	5	14	14	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M- kg*m	M- kg*m	Act	Aft	pAft	S _{max}	σf _{med}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	cm	kg/cmq	mm	mm	mm	Ver.	Cs
0.0	213	0.1	12.06	30.16	22.4	20	0.001	0.001	0.001	0.001	12(Fr)	Si	>100
0.0	251	0.1	12.06	30.16	22.4	23	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
14.9	313	0.1	12.06	30.16	22.4	29	0.002	0.002	0.002	0.002	14(Qp)	Si	>100
14.9	283	0.1	12.06	30.16	22.4	26	0.002	0.002	0.002	0.002	12(Fr)	Si	>100
74.7	383	0.1	12.06	30.16	22.4	35	0.002	0.002	0.002	0.002	14(Qp)	Si	>100
74.7	380	0.1	12.06	30.16	22.4	35	0.002	0.002	0.002	0.002	12(Fr)	Si	>100
134.4	156	0.1	12.06	30.16	22.4	14	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
134.4	156	0.1	12.06	30.16	22.4	14	0.001	0.001	0.001	0.001	9(Fr)	Si	>100
149.3	50	0.1	12.06	30.16	22.4	5	0.000	0.000	0.000	0.000	14(Qp)	Si	>100
149.3	46	0.1	12.06	30.16	22.4	4	0.000	0.000	0.000	0.000	11(Fr)	Si	>100

VERIFICHE STATO LIMITE DI ESERCIZIO

Verifica spostamenti laterali delle colonne in acciaio secondo NTC 2008									
Scenario di calcolo : Set_NT_SLD_A2_STR/GEO									

Verifica spostamenti orizzontali relativi di piano (§4.2.4.2.2 - NTC 2008)

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup. mm	SpostY sup. mm	SpostX inf. mm	SpostY inf. mm	δ mm	h/500.00 mm	Verifica
2-3	311 (Nodo 311)	211 (Nodo 211)								
2-3	312 (Nodo 312)	212 (Nodo 212)	7	0.94	-0.19	0.00	0.00	0.95	4.67	Si
2-3	313 (Nodo 313)	213 (Nodo 213)	7	0.89	-0.22	0.00	0.00	0.92	4.67	Si
2-3	314 (Nodo 314)	214 (Nodo 214)	7	0.84	-0.25	0.00	0.00	0.88	4.67	Si
2-3	315 (Nodo 315)	215 (Nodo 215)	7	0.80	-0.29	0.00	0.00	0.85	4.67	Si
2-3	316 (Nodo 316)	216 (Nodo 216)	7	0.74	-0.32	0.00	0.00	0.81	4.67	Si
2-3	317 (Nodo 317)	217 (Nodo 217)	7	0.80	-0.29	0.00	0.00	0.85	4.67	Si
2-3	318 (Nodo 318)	218 (Nodo 218)	7	0.72	-0.34	0.00	0.00	0.80	4.67	Si
2-3	319 (Nodo 319)	219 (Nodo 219)	7	0.61	-0.39	0.00	0.00	0.72	4.67	Si
2-3	320 (Nodo 320)	220 (Nodo 220)	8	0.06	-0.67	0.00	0.00	0.67	4.67	Si
2-3			7	0.65	-0.36	0.00	0.00	0.75	4.67	Si

Verifica spostamenti orizzontali in sommità (§4.2.4.2.2 - NTC 2008)

Nodo	Comb.	SpostX mm	SpostY mm	Δ mm	H/500.00 mm	Verifica
311 (Nodo 311)						
312 (Nodo 312)	7	0.94	-0.19	0.95	23.76	Si
313 (Nodo 313)	7	0.89	-0.22	0.92	23.76	Si
314 (Nodo 314)	7	0.84	-0.25	0.88	23.76	Si
315 (Nodo 315)	7	0.80	-0.29	0.85	23.76	Si
316 (Nodo 316)	7	0.74	-0.32	0.81	23.76	Si
317 (Nodo 317)	7	0.80	-0.29	0.85	23.76	Si
318 (Nodo 318)	7	0.72	-0.34	0.80	23.76	Si
319 (Nodo 319)	7	0.61	-0.39	0.72	23.76	Si
320 (Nodo 320)	8	0.06	-0.67	0.67	23.76	Si
	7	0.65	-0.36	0.75	23.76	Si

TABULATI DI INPUT - Portale da 35 a 65

Dati generali	
Nome struttura	
Temperatura di riferimento [°C]	0
Fattore rigidezza assiale pilastri	1
Numero di frequenze	155
% Filtro masse libere	0.1
% Coefficiente di smorzamento viscoso	5
Spostamenti nodali con segno	Si
Deformabilità a taglio delle aste	Si
Impalcati deformabili per carichi termici	No
Spostamento ammissibile impalcati	0.0050*h

Impalcati			
N°	Quota	Rigido	Incr.Soll.PI
0	mm		
1	0	No	1.000
2	4070	No	1.000
3	11280	No	1.000
4	11880	No	1.000

Percentuali Spostamento masse impalcati

Posizione	% Spostamento direzione X		% Spostamento direzione Y	
	1	0	1	-5
2	5	0	5	0
3	0	0	0	5
4	-5	-5	-5	0

Combinazioni del Sisma in X e Y e Verticale

Comb	Pos. SismaX		Pos. SismaY		Fz	
	1	2	1	2	Fx	Fy
1	1	2	1	2	1	0.3
2	1	2	1	2	0.3	1
3	1	4	1	4	0.3	0.3
4	1	4	1	4	0.3	0.3
5	3	2	3	2	0.3	1
6	3	2	3	2	0.3	0.3
7	3	4	3	4	0.3	1
8	3	4	3	4	0.3	0.3
9	1	2	1	2	0.3	1
10	1	4	1	4	0.3	0.3
11	3	2	3	2	0.3	1
12	3	4	3	4	0.3	0.3

Comb = Numero di combinazione dei sismi

Pos. SismaX = Posizione in cui viene scelto il sisma in direzione X

Pos. SismaY = Posizione in cui viene scelto il sisma in direzione Y

Fx = Fattore con cui il sisma X partecipa

Fy = Fattore con cui il sisma Y partecipa

Fz = Fattore con cui il sisma Verticale partecipa (quando richiesto)

Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx ed Fy ed Fz

Spettri di risposta

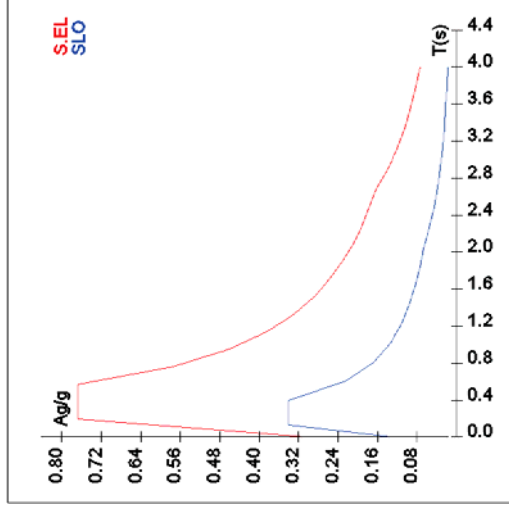
Spettro :SpettroNT(q=1)

Il calcolo degli spettri e del fattore di struttura sono stati calcolati per la seguente tipologia di terreno e struttura

Vita della struttura	684
----------------------	-----

Tipo	Ponti imp. strategica (>100) >=100 anni
Via nominale(anni)	100.0
Classe d'uso	Classe IV
Coefficiente d'uso	2.000
Periodo di riferimento(anni)	200.000
Stato limite di esercizio - SLO	PVR=81.0%
Stato limite ultimo - SLV	PVR=10.0%
Periodo di ritorno SLO(anni)	TR=120.4
Periodo di ritorno SLV(anni)	TR=1898.2
Parametri del sito	
Comune	Biancavilla - (CI)
Longitudine	14.865
Latitudine	37.646
Id reticolo del sito	47419471974719647418
Valori di riferimento del sito	
Ag(TR=120.4) SLO	0.1103
Fq(TR=120.4) SLO	2.5726
T°C(TR=120.4) SLO	0.281
Ag/TR=1898.2) SLV	0.2704
Fq(TR=1898.2) SLV	2.5180
T°C(TR=1898.2) SLV	0.441
Coefficiente Amplificazione Topografica	Sf=1.000
Categoria terreno B	
stato limite SLV	
	S=1.13
	TB=0.19
	TC=0.57
	TD=2.68
stato limite SLO	
	S=1.20
	TB=0.13
	TC=0.40
	TD=2.04
Spettro Elastico Smorzamento viscoso %	q=1 (struttura NON dissipativa) 5.0

T	EL	TSLO	SLO
0.00000	0.00000	0.00000	0.13236
0.19040	0.76776	0.13299	0.34050
0.57119	0.76776	0.39896	0.34050
0.76304	0.60424	0.57472	0.22482
0.95489	0.45925	0.80952	0.16781
1.14675	0.38242	1.01479	0.13387
1.33860	0.32761	1.22007	0.11134
1.53045	0.28654	1.42555	0.09531
1.72231	0.25462	1.63063	0.08331
1.91416	0.22910	1.83591	0.07399
2.10602	0.20823	2.04119	0.06655
2.29787	0.19084	2.25883	0.05435
2.48972	0.17614	2.47648	0.04521
2.68158	0.16354	2.69412	0.03820
2.90131	0.13970	2.91177	0.03270
3.12105	0.12072	3.12942	0.02831
3.34079	0.10537	3.34706	0.02475
3.56053	0.09276	3.56471	0.02182
3.78026	0.08229	3.78235	0.01938
4.00000	0.07350	4.00000	0.01733



Caratteristiche del terreno

Terreno1- Cost.Winkler=10.00 kg/cmc

Strato n°	Spessore cm	γ kg/mc	γ_{Sat} kg/mc	ϕ °	rati di asse			Cu	E	v
					Addensato	OCR	Coesione			
1	100	1900	1900	35	No	--	0,00	kg/cmq	2E02	0,30

Materiali

Materiale: C25/30		
Peso specifico	kg/mc	2500
Modulo di Young E	kg/cmq	3E05
Modulo di Poisson ν		0.13
Coefficiente di dilatazione termica λ_t	1/°C	1e-005
<hr/>		
Materiale: Acciaio		
Peso specifico	kg/mc	7850
Modulo di Young E	kg/cmq	2E+6
Modulo di Poisson ν		0.30
Coefficiente di dilatazione termica λ_t	1/°C	1.2e-005

Nodi - Geometria e vincoli

Nodi - Geometria e vincoli												
Nodo	X	Y	Z	Coordinate [mm]			Vincoli					Impalcato
				Tx	Ty	Tz	Rx	Ry	Rz			
0	6540	7366	8350	0	0	0	0	0	0			
0	12174	22468	9410	0	0	0	0	0	0		1	
0	11450	23270	10420	0	0	0	0	0	0		1	
0	10813	15599	5530	0	0	0	0	0	0		1	
0	9866	16118	6940	0	0	0	0	0	0		1	
0	8919	16637	8350	0	0	0	0	0	0		1	
0	7972	17156	9410	0	0	0	0	0	0		1	
0	7025	17675	10420	0	0	0	0	0	0		1	
0	11817	17212	5530	0	0	0	0	0	0		1	
0	10934	17834	6940	0	0	0	0	0	0		1	
0	10051	18456	8350	0	0	0	0	0	0		1	
0	9168	19078	9410	0	0	0	0	0	0		1	

0	8285	19700	10420	0	0	0	0	0	0
0	15829	21266	5530	0	0	0	0	0	0
0	15198	22142	6940	0	0	0	0	0	0
0	14567	23018	8350	0	0	0	0	0	0
0	13936	23894	9410	0	0	0	0	0	0
0	13305	24770	10420	0	0	0	0	0	0
0	13002	18706	5530	0	0	0	0	0	0
0	12194	19422	6940	0	0	0	0	0	0
0	11386	20138	8350	0	0	0	0	0	0
0	10578	20854	9410	0	0	0	0	0	0
0	9770	21570	10420	0	0	0	0	0	0
0	16619	21800	5530	0	0	0	0	0	0
0	16038	22710	6940	0	0	0	0	0	0
0	15457	23620	8350	0	0	0	0	0	0
0	4505	4990	10420	0	0	0	0	0	0
0	14876	24530	9410	0	0	0	0	0	0
0	14295	25440	10420	0	0	0	0	0	0
0	11294	16421	5530	0	0	0	0	0	0
0	10378	16992	6940	0	0	0	0	0	0
0	9462	17563	8350	0	0	0	0	0	0
0	8546	18134	9410	0	0	0	0	0	0
0	7630	18705	10420	0	0	0	0	0	0
0	13653	19409	5530	0	0	0	0	0	0
0	12886	20168	6940	0	0	0	0	0	0
0	12119	20927	8350	0	0	0	0	0	0
0	11352	21686	9410	0	0	0	0	0	0
0	10585	22445	10420	0	0	0	0	0	0
0	15071	20681	5530	0	0	0	0	0	0
0	14392	21522	6940	0	0	0	0	0	0
0	13713	22363	8350	0	0	0	0	0	0
0	13034	23204	9410	0	0	0	0	0	0
0	12355	24045	10420	0	0	0	0	0	0
0	17440	22291	5530	0	0	0	0	0	0
0	16910	23232	6940	0	0	0	0	0	0
0	16380	24173	8350	0	0	0	0	0	0
0	15850	25114	9410	0	0	0	0	0	0
0	15320	26055	10420	0	0	0	0	0	0
0	8797	5462	5530	0	0	0	0	0	0
0	7724	5344	6940	0	0	0	0	0	0
0	6651	5226	8350	0	0	0	0	0	0
0	98	5939	12190	0	0	0	0	0	0
0	1176	5998	12140	0	0	0	0	0	0
0	4410	6175	10420	0	0	0	0	0	0
0	5488	6234	9410	0	0	0	0	0	0
0	6566	6293	8350	0	0	0	0	0	0
0	7644	6352	6940	0	0	0	0	0	0
0	8722	6411	5530	0	0	0	0	0	0
0	684	1687	12190	0	0	0	0	0	0
0	1738	1924	12140	0	0	0	0	0	0
0	4900	2635	10420	0	0	0	0	0	0
0	5954	2872	9410	0	0	0	0	0	0
0	7008	3109	8350	0	0	0	0	0	0
0	8062	3346	6940	0	0	0	0	0	0
0	9116	3583	5530	0	0	0	0	0	0
0	5195	1475	10420	0	0	0	0	0	0

[illegible]

[illegible][illegible]

191	6590	14050	9410	0	0	0	0	0	0	0
192	5570	14405	10420	0	0	0	0	0	0	0
193	9991	13872	10420	0	0	0	0	0	0	0
194	5530	14284	6940	0	0	0	0	0	0	0
195	7993	14696	8350	0	0	0	0	0	0	0
196	6994	15108	9410	0	0	0	0	0	0	0
197	5995	15520	10420	0	0	0	0	0	0	0
198	14346	20062	5530	0	0	0	0	0	0	0
199	13622	20864	6940	0	0	0	0	0	0	0
200	12898	21666	8350	0	0	0	0	0	0	0
327	0	0	11880	0	0	0	0	0	0	0
328	-370	1450	11880	0	0	0	0	0	0	0
329	-460	2920	11880	0	0	0	0	0	0	0
330	-860	4400	11880	0	0	0	0	0	0	0
331	-980	5880	11880	0	0	0	0	0	0	0
332	-1020	7380	11880	0	0	0	0	0	0	0
333	-980	8860	11880	0	0	0	0	0	0	0
334	-850	10380	11880	0	0	0	0	0	0	0
335	-640	11840	11880	0	0	0	0	0	0	0
336	-350	13310	11880	0	0	0	0	0	0	0
337	20	14760	11880	0	0	0	0	0	0	0
338	470	16180	11880	0	0	0	0	0	0	0
339	1000	17580	11880	0	0	0	0	0	0	0
340	1610	18940	11880	0	0	0	0	0	0	0
341	2290	20270	11880	0	0	0	0	0	0	0
342	3050	21560	11880	0	0	0	0	0	0	0
343	3870	22810	11880	0	0	0	0	0	0	0
344	4770	24010	11880	0	0	0	0	0	0	0
345	5730	25150	11880	0	0	0	0	0	0	0
346	6750	26240	11880	0	0	0	0	0	0	0
347	7830	27280	11880	0	0	0	0	0	0	0
348	8960	28250	11880	0	0	0	0	0	0	0
349	10150	29150	11880	0	0	0	0	0	0	0
350	11390	29990	11880	0	0	0	0	0	0	0
351	12670	30760	11880	0	0	0	0	0	0	0
352	13990	31460	11880	0	0	0	0	0	0	0
353	2096	14164	12140	0	0	0	0	0	0	0
354	1058	14462	12190	0	0	0	0	0	0	0
355	3558	18008	12190	0	0	0	0	0	0	0
356	2584	18474	12190	0	0	0	0	0	0	0
357	1488	11478	12140	0	0	0	0	0	0	0
358	424	11659	12190	0	0	0	0	0	0	0
359	1176	8738	12140	0	0	0	0	0	0	0
360	98	8799	12190	0	0	0	0	0	0	0
361	6464	22670	12140	0	0	0	0	0	0	0
362	5617	23340	12190	0	0	0	0	0	0	0
363	1756	12830	12140	0	0	0	0	0	0	0
364	703	13070	12190	0	0	0	0	0	0	0
365	1296	10134	12140	0	0	0	0	0	0	0
366	223	10257	12190	0	0	0	0	0	0	0
367	2510	15470	12140	0	0	0	0	0	0	0
368	1490	15825	12190	0	0	0	0	0	0	0
369	2998	16756	12140	0	0	0	0	0	0	0
370	1999	17168	12190	0	0	0	0	0	0	0
371	9278	25676	12140	0	0	0	0	0	0	0
372	8554	26478	12190	0	0	0	0	0	0	0
373	4184	19232	12140	0	0	0	0	0	0	0
374	3237	19751	12190	0	0	0	0	0	0	0
375	5636	21566	12140	0	0	0	0	0	0	0
376	4753	22188	12190	0	0	0	0	0	0	0
377	11412	27398	12140	0	0	0	0	0	0	0
378	10781	28274	12190	0	0	0	0	0	0	0
379	7346	23718	12140	0	0	0	0	0	0	0
380	6538	24434	12190	0	0	0	0	0	0	0
381	12552	28170	12140	0	0	0	0	0	0	0
382	11971	29080	12190	0	0	0	0	0	0	0
383	4482	20418	12140	0	0	0	0	0	0	0

384	3966	20989	12190	0	0	0	0	0	0	0
385	8284	24722	12140	0	0	0	0	0	0	1
386	7517	25481	12190	0	0	0	0	0	0	0
387	10318	26568	12140	0	0	0	0	0	0	1
388	9639	27409	12190	0	0	0	0	0	0	0
389	13730	28878	12140	0	0	0	0	0	0	0
390	13200	29819	12190	0	0	0	0	0	0	1
391	1286	4636	12140	0	0	0	0	0	0	1
392	213	4518	12190	0	0	0	0	0	0	1
393	14944	29522	12140	0	0	0	0	0	0	1
394	14467	30491	12190	0	0	0	0	0	0	1
395	1140	7376	12140	0	0	0	0	0	0	1
396	60	7378	12190	0	0	0	0	0	0	1
397	1472	3276	12140	0	0	0	0	0	0	1
398	406	5098	12190	0	0	0	0	0	0	1
399	2078	590	12140	0	0	0	0	0	0	1
400	1039	295	12190	0	0	0	0	0	0	1

Nodi - Carichi

Nodi - Carichi													
N°	C. Car.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz
				kg			kg*mm			mm			mmrad
													°C
101	QP Solai	0	0	0	0	0	0						
101	QV Solai	0	0	3	0	0	0						
101	Nerve	0	0	5	0	0	0						
101	Vento X	0	0	8	0	0	0						
327	QP Solai	0	0	4	0	0	0						
327	QV Solai	0	0	1	0	0	0						
327	Nerve	0	0	2	0	0	0						
327	Vento X	0	0	3	0	0	0						
338	QP Solai	0	0	5	0	0	-0						
338	QV Solai	0	0	2	0	0	-0						
338	Nerve	0	0	3	0	0	-0						
338	Vento X	0	0	5	0	0	-0						

Input - Aste - Tabella sezioni tipo

Input - Aste - Tabella sezioni tipo		
Tipo	Nome	Raggio
C		cm
		l
	F120	
	F16	l

Typo	Nome	Area	lx	ly	lt	Fx	Fy	Lx	Lx
G		mq	m ⁴	m ⁴	m ⁴			cm	cm
	IPE 100	0.0	1.710E-06	1.592E-07	8.826E-09	1.000	1.000	6	10
	HE 240 A	0.0	7.763E-05	2.769E-05	4.155E-07	1.000	1.000	24	23

Tiplo	Nome	Base	Altezza	Long. mag.
R		cm	cm	cm
	F60x100	60	100	120

Aste - Geometria e vincoli

[illegible]

8019	386	346	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8585	0	0	0	0	0	Trave	112	112
8020	198	198	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8580	0	-0	0	0	0	Trave	182	182
8020	198	199	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	178	178
8020	198	200	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	178	178
8020	200	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	151	151
8020	0	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	148	148
8020	0	45	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	134	134
8020	45	46	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	123	123
8020	46	371	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	113	113
8020	371	372	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	108	108
8020	372	373	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	108	108
8020	373	374	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8580	0	-0	0	0	0	Trave	182	182
8020	374	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8580	0	-0	0	0	0	Trave	182	182
8020	12	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8580	0	-0	0	0	0	Trave	178	178
8020	0	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	151	151
8020	0	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	148	148
8020	0	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	134	134
8020	0	51	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	123	123
8020	51	32	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	113	113
8020	32	377	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	108	108
8020	377	378	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	108	108
8020	378	349	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8580	0	0	0	0	0	Trave	112	112
8020	349	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8580	0	-0	0	0	0	Trave	182	182
8020	124	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8580	0	-0	0	0	0	Trave	178	178
8020	0	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	178	178
8020	0	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	151	151
8020	0	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	148	148
8020	0	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	134	134
8020	0	55	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	123	123
8020	55	56	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	113	113
8020	56	381	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	108	108
8020	381	382	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	108	108
8020	382	350	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8085	0	0	0	0	-0	Trave	112	112
8020	350	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8085	0	0	0	0	-0	Trave	182	182
8020	125	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8580	0	0	0	0	0	Trave	178	178
8020	0	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	148	148
8020	0	0	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	134	134
8020	0	67	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	123	123
8020	67	68	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	113	113
8020	68	393	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	108	108
8020	393	394	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8080	0	0	0	0	0	Trave	112	112
8020	394	352	L1	HE 240 A	Acciao	Acciao Pressifessione	0	8585	0	0	0	-0	Trave	90	90	
8028	101	102	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8685	0	0	0	0	Trave	90	90	
8028	102	103	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	90	90	
8028	103	104	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	104	105	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	105	106	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	106	107	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	107	108	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	108	109	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	109	110	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	90	90	
8028	110	111	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	90	90	
8028	111	112	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	112	113	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	113	114	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	90	90	
8028	114	115	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	90	90	
8028	115	116	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	116	117	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	117	118	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	90	90	
8028	118	119	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	90	90	
8028	119	120	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	120	121	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	121	122	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	90	90	
8028	122	123	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	90	90	
8028	123	124	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	
8028	124	125	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	90	90	
8028	125	126	Cv-Cy	IPE 100	Acciao	Acciao Fessione	0	8585	0	0	0	0	Trave	89	89	

[illegible]

[illegible]

7106	337	365	Cy-Cy	Fil16	Acciaio	Acciaio	Tirante	0	8580	0	-40	0	0	0	0	Gen.	481	48
Aste - Carichi																		
Descrizione carichi aste																		
UnifG																		
UnifL																		
Variable lineare globale																		
Variable lineare locale																		
Polig																		
Termico																		
Forcente																		
Precomp.																		
Pol.																		
Poligonale locale																		
Sezione		Ni	Nf	Cond.		Tipo c.		Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf			
								cm	car. dist. kg/m	coppie torc. kg*m/m		cm	car. dist. kg/m	coppie torc. kg*m/m				
Pilastro 1																		
HE 240 A		1	54	Peso Proprio		UnifG		0	0	0	60	240	0	0	60	240	0	0
HE 240 A		1	54	Vento X		UnifL		0	0	0	-225	240	0	0	-225	240	0	0
HE 240 A		1	54	Vento Y		UnifL		0	0	0	113	240	0	0	113	240	0	0
HE 240 A		1	54	Carichi termici		Termico		AXY=15°C,AXZ=15°C										
HE 240 A		54	101	Peso Proprio		UnifG		0	0	0	60	167	0	0	60	167	0	0
HE 240 A		54	101	Vento X		UnifL		0	0	0	-225	167	0	0	-225	167	0	0
HE 240 A		54	101	Vento Y		UnifL		0	0	0	113	167	0	0	113	167	0	0
HE 240 A		54	101	Carichi termici		Termico		AXY=15°C,AXZ=15°C										
Pilastro 2																		
HE 240 A		2	53	Peso Proprio		UnifG		0	0	0	60	240	0	0	60	240	0	0
HE 240 A		2	53	Vento X		UnifL		0	0	0	-225	240	0	0	-225	240	0	0
HE 240 A		2	53	Vento Y		UnifL		0	0	0	113	240	0	0	113	240	0	0
HE 240 A		2	53	Carichi termici		Termico		AXY=15°C,AXZ=15°C										
HE 240 A		53	102	Peso Proprio		UnifG		0	0	0	60	167	0	0	60	167	0	0
HE 240 A		53	102	Vento X		UnifL		0	0	0	-225	167	0	0	-225	167	0	0
HE 240 A		53	102	Vento Y		UnifL		0	0	0	113	167	0	0	113	167	0	0
HE 240 A		53	102	Carichi termici		Termico		AXY=15°C,AXZ=15°C										
Pilastro 3																		
HE 240 A		3	55	Peso Proprio		UnifG		0	0	0	60	240	0	0	60	240	0	0
HE 240 A		3	55	Vento X		UnifL		0	0	0	-225	240	0	0	-225	240	0	0
HE 240 A		3	55	Vento Y		UnifL		0	0	0	113	240	0	0	113	240	0	0
HE 240 A		3	55	Carichi termici		Termico		AXY=15°C,AXZ=15°C										
HE 240 A		55	103	Peso Proprio		UnifG		0	0	0	60	167	0	0	60	167	0	0
HE 240 A		55	103	Vento X		UnifL		0	0	0	-225	167	0	0	-225	167	0	0
HE 240 A		55	103	Vento Y		UnifL		0	0	0	113	167	0	0	113	167	0	0
HE 240 A		55	103	Carichi termici		Termico		AXY=15°C,AXZ=15°C										
Pilastro 4																		
HE 240 A		4	56	Peso Proprio		UnifG		0	0	0	60	240	0	0	60	240	0	0
HE 240 A		4	56	Vento X		UnifL		0	0	0	-225	240	0	0	-225	240	0	0
HE 240 A		4	56	Vento Y		UnifL		0	0	0	113	240	0	0	113	240	0	0
HE 240 A		4	56	Carichi termici		Termico		AXY=15°C,AXZ=15°C										
HE 240 A		56	104	Peso Proprio		UnifG		0	0	0	60	167	0	0	60	167	0	0
HE 240 A		56	104	Vento X		UnifL		0	0	0	-225	167	0	0	-225	167	0	0
HE 240 A		56	104	Vento Y		UnifL		0	0	0	113	167	0	0	113	167	0	0
HE 240 A		56	104	Carichi termici		Termico		AXY=15°C,AXZ=15°C										
Pilastro 5																		
HE 240 A		5	71	Peso Proprio		UnifG		0	0	0	60	240	0	0	60	240	0	0
HE 240 A		5	71	Vento X		UnifL		0	0	0	-225	240	0	0	-225	240	0	0
HE 240 A		5	71	Vento Y		UnifL		0	0	0	113	240	0	0	113	240	0	0
HE 240 A		5	71	Carichi termici		Termico		AXY=15°C,AXZ=15°C										
HE 240 A		71	105	Peso Proprio		UnifG		0	0	0	60	167	0	0	60	167	0	0
HE 240 A		71	105	Vento X		UnifL		0	0	0	-225	167	0	0	-225	167	0	0
HE 240 A		71	105	Vento Y		UnifL		0	0	0	113	167	0	0	113	167	0	0
HE 240 A		71	105	Carichi termici		Termico		AXY=15°C,AXZ=15°C										
Pilastro 6																		
HE 240 A		6	74	Peso Proprio		UnifG		0	0	0	60	240	0	0	60	240	0	0
HE 240 A		6	74	Vento X		UnifL		0	0	0	-225	240	0	0	-225	240	0	0
HE 240 A		6	74	Vento Y		UnifL		0	0	0	113	240	0	0	113	240	0	0

[illegible]

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYL	QZi	Xf	QXf	QYf	QZf
HE 240 A	6	74	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
HE 240 A	74	106	Peso Proprio	UnifG	0	0	0	-225	240	0	0	-225
HE 240 A	74	106	Vento X	UnifL	0	0	0	113	167	0	0	113
HE 240 A	74	106	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	74	106	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
Pilastro 7												
HE 240 A	7	76	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	7	76	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	7	76	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	7	76	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
HE 240 A	76	107	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	76	107	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	76	107	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	76	107	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
Pilastro 8												
HE 240 A	8	75	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	8	75	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	8	75	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	8	75	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
HE 240 A	75	108	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	75	108	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	75	108	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	75	108	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
Pilastro 9												
HE 240 A	9	72	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	9	72	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	9	72	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	9	72	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
HE 240 A	72	109	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	72	109	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	72	109	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	72	109	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
Pilastro 10												
HE 240 A	10	70	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	10	70	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	10	70	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	10	70	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
HE 240 A	70	110	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	70	110	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	70	110	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	70	110	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
Pilastro 11												
HE 240 A	11	69	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	11	69	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	11	69	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	11	69	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
HE 240 A	69	111	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	69	111	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	69	111	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	69	111	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
Pilastro 12												
HE 240 A	12	77	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	12	77	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	12	77	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	12	77	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
HE 240 A	77	112	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	77	112	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	77	112	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	77	112	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
Pilastro 13												
HE 240 A	13	78	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	13	78	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	13	78	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	13	78	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	167	0	0
HE 240 A	78	113	Peso Proprio	UnifG	0	0	0	60	167	0	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	78	113	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	78	113	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	78	113	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Pilastro 14												
HE 240 A	14	73	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	14	73	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	14	73	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	14	73	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	73	114	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	73	114	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	73	114	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	73	114	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Pilastro 15												
HE 240 A	15	61	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	15	61	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	15	61	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	15	61	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	61	115	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	61	115	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	61	115	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	61	115	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Pilastro 16												
HE 240 A	16	62	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	16	62	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	16	62	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	16	62	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	62	116	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	62	116	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	62	116	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	62	116	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Pilastro 17												
HE 240 A	17	63	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	17	63	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	17	63	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	17	63	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	63	117	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	63	117	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	63	117	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	63	117	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Pilastro 18												
HE 240 A	18	64	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	18	64	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	18	64	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	18	64	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	64	118	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	64	118	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	64	118	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	64	118	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Pilastro 19												
HE 240 A	19	60	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	19	60	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	19	60	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	19	60	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	60	119	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	60	119	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	60	119	Vento Y	UnifL	0	0	0	113	167	0	0	113
HE 240 A	60	119	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Pilastro 20												
HE 240 A	20	57	Peso Proprio	UnifG	0	0	0	60	240	0	0	60
HE 240 A	20	57	Vento X	UnifL	0	0	0	-225	240	0	0	-225
HE 240 A	20	57	Vento Y	UnifL	0	0	0	113	240	0	0	113
HE 240 A	20	57	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	57	120	Peso Proprio	UnifG	0	0	0	60	167	0	0	60
HE 240 A	57	120	Vento X	UnifL	0	0	0	-225	167	0	0	-225
HE 240 A	57	120	Vento Y	UnifL	0	0	0	113	167	0	0	113

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Piastrino 52												
HE 240 A	26	352	Peso Proprio	UnifG	0	0	0	60	60	0	0	60
HE 240 A	26	352	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 8000												
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	0	73	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	QP Solai	PolG	0	0	0	12	39	0	0	51
HE 240 A					39	0	0	51	151	0	0	44
HE 240 A	0	0	QP Solai	PolG	0	0	0	12	40	0	0	53
HE 240 A					40	0	0	53	148	0	0	46
HE 240 A	0	0	QP Solai	PolG	0	0	0	12	40	0	0	47
HE 240 A					40	0	0	47	178	0	0	39
HE 240 A	0	0	QP Solai	PolG	0	0	0	12	43	0	0	49
HE 240 A					43	0	0	49	178	0	0	41
HE 240 A	0	73	QP Solai	PolG	0	0	0	12	38	0	0	55
HE 240 A					38	0	0	55	134	0	0	48
HE 240 A	0	73	QV Solai	PolG	0	0	0	4	38	0	0	18
HE 240 A					38	0	0	18	134	0	0	15
HE 240 A	0	0	QV Solai	PolG	0	0	0	4	40	0	0	15
HE 240 A					40	0	0	15	178	0	0	13
HE 240 A	0	0	QV Solai	PolG	0	0	0	4	39	0	0	16
HE 240 A					39	0	0	16	151	0	0	14
HE 240 A	0	0	QV Solai	PolG	0	0	0	4	43	0	0	16
HE 240 A					43	0	0	16	178	0	0	13
HE 240 A	0	0	QV Solai	PolG	0	0	0	4	40	0	0	17
HE 240 A					40	0	0	17	148	0	0	15
HE 240 A	0	0	Neve	PolG	0	0	0	7	40	0	0	29
HE 240 A					40	0	0	29	178	0	0	24
HE 240 A	0	0	Neve	PolG	0	0	0	7	40	0	0	33
HE 240 A					40	0	0	33	148	0	0	29
HE 240 A	0	73	Neve	PolG	0	0	0	7	38	0	0	34
HE 240 A					38	0	0	34	134	0	0	30
HE 240 A	0	0	Neve	PolG	0	0	0	7	39	0	0	32
HE 240 A					39	0	0	32	151	0	0	27
HE 240 A	0	0	Neve	PolG	0	0	0	7	43	0	0	30
HE 240 A					43	0	0	30	178	0	0	26
HE 240 A	0	0	Vento X	PolG	0	0	0	11	39	0	0	49
HE 240 A					39	0	0	49	151	0	0	42
HE 240 A	0	73	Vento X	PolG	0	0	0	11	38	0	0	53
HE 240 A					38	0	0	53	134	0	0	46
HE 240 A	0	0	Vento X	PolG	0	0	0	11	43	0	0	47
HE 240 A					43	0	0	47	178	0	0	40
HE 240 A	0	0	Vento X	PolG	0	0	0	11	40	0	0	51
HE 240 A					40	0	0	51	148	0	0	44
HE 240 A	0	0	Vento X	PolG	0	0	0	11	40	0	0	45
HE 240 A					40	0	0	45	178	0	0	38
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	73	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	73	74	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	73	74	QP Solai	PolG	0	0	0	12	37	0	0	57
HE 240 A					37	0	0	57	123	0	0	51
HE 240 A	73	74	QV Solai	PolG	0	0	0	4	37	0	0	18
HE 240 A					37	0	0	18	123	0	0	16
HE 240 A	73	74	Neve	PolG	0	0	0	7	37	0	0	36
HE 240 A					37	0	0	36	123	0	0	31
HE 240 A	73	74	Vento X	PolG	0	0	0	11	37	0	0	55
HE 240 A					37	0	0	55	123	0	0	49
HE 240 A	73	74	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	74	399	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	74	399	QP Solai	PolG	0	0	0	12	35	0	0	59

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	74	399	QV Solai	PolG	35	0	0	59	113	0	0	53
HE 240 A					0	0	0	4	35	0	0	19
HE 240 A	74	399	Neve	PolG	35	0	0	19	113	0	0	17
HE 240 A					0	0	0	7	35	0	0	37
HE 240 A	74	399	Vento X	PolG	35	0	0	37	113	0	0	33
HE 240 A					0	0	0	11	35	0	0	57
HE 240 A	74	399	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	74	399	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	101	0	QP Solai	PolG	0	0	0	12	38	0	0	44
HE 240 A	101	0			38	0	0	44	182	0	0	37
HE 240 A	101	0	QV Solai	PolG	0	0	0	4	38	0	0	14
HE 240 A					38	0	0	14	182	0	0	12
HE 240 A	101	0	Neve	PolG	0	0	0	7	38	0	0	28
HE 240 A					38	0	0	28	182	0	0	23
HE 240 A	101	0	Vento X	PolG	0	0	0	11	38	0	0	43
HE 240 A					38	0	0	43	182	0	0	35
HE 240 A	101	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	399	400	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
HE 240 A	399	400	QP Solai	PolG	0	0	0	12	35	0	0	62
HE 240 A					35	0	0	62	108	0	0	55
HE 240 A	399	400	QV Solai	PolG	0	0	0	4	35	0	0	20
HE 240 A					35	0	0	20	108	0	0	18
HE 240 A	399	400	Neve	PolG	0	0	0	7	35	0	0	38
HE 240 A					35	0	0	38	108	0	0	34
HE 240 A	399	400	Vento X	PolG	0	0	0	11	35	0	0	59
HE 240 A					35	0	0	59	108	0	0	53
HE 240 A	399	400	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	400	327	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
HE 240 A	400	327	QP Solai	PolG	0	0	0	12	38	0	0	64
HE 240 A					38	0	0	64	112	0	0	58
HE 240 A	400	327	QV Solai	PolG	0	0	0	4	38	0	0	20
HE 240 A					38	0	0	20	112	0	0	18
HE 240 A	400	327	Neve	PolG	0	0	0	7	38	0	0	40
HE 240 A					38	0	0	40	112	0	0	36
HE 240 A	400	327	Vento X	PolG	0	0	0	11	38	0	0	61
HE 240 A					38	0	0	61	112	0	0	55
HE 240 A	400	327	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
Trave 8001												
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	75	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	328	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
HE 240 A	0	328	QP Solai	PolG	0	0	0	66	30	0	0	123
HE 240 A					30	0	0	123	73	0	0	125
HE 240 A	0	75	QP Solai	PolG	0	0	0	57	29	0	0	104
HE 240 A					29	0	0	104	95	0	0	106
HE 240 A	0	0	QP Solai	PolG	0	0	0	54	31	0	0	99
HE 240 A					31	0	0	99	107	0	0	102
HE 240 A	0	0	QP Solai	PolG	0	0	0	52	30	0	0	94
HE 240 A					30	0	0	94	111	0	0	97
HE 240 A	0	0	QP Solai	PolG	0	0	0	97	151	0	0	53
HE 240 A					33	0	0	50	33	0	0	90
HE 240 A	0	0	QP Solai	PolG	0	0	0	90	133	0	0	92
HE 240 A					133	0	0	92	178	0	0	51
HE 240 A	0	0	QP Solai	PolG	0	0	0	47	31	0	0	85
HE 240 A					31	0	0	85	136	0	0	88
HE 240 A	0	0	QP Solai	PolG	0	0	0	88	178	0	0	49
HE 240 A					27	0	0	118	72	0	0	120

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	QV Solai	PolG	72	0	0	120	108	0	0	65
					0	0	0	15	31	0	0	27
					31	0	0	27	136	0	0	28
HE 240 A	0	0	QV Solai	PolG	136	0	0	28	178	0	0	16
					0	0	0	16	33	0	0	29
					33	0	0	29	133	0	0	30
					133	0	0	30	178	0	0	16
HE 240 A	0	0	QV Solai	PolG	30	0	0	17	30	0	0	30
					30	0	0	30	111	0	0	31
					111	0	0	31	151	0	0	17
HE 240 A	0	328	QV Solai	PolG	0	0	0	21	30	0	0	39
					30	0	0	39	73	0	0	40
					73	0	0	40	112	0	0	22
HE 240 A	0	0	QV Solai	PolG	31	0	0	17	31	0	0	32
					31	0	0	32	107	0	0	33
					107	0	0	33	148	0	0	18
HE 240 A	0	0	QV Solai	PolG	0	0	0	20	27	0	0	38
					27	0	0	38	72	0	0	39
					72	0	0	39	108	0	0	21
HE 240 A	0	75	QV Solai	PolG	0	0	0	18	29	0	0	33
					29	0	0	33	95	0	0	34
					95	0	0	34	134	0	0	19
HE 240 A	0	0	Neve	PolG	0	0	0	28	107	0	0	33
					107	0	0	33	148	0	0	6
HE 240 A	0	0	Neve	PolG	0	0	0	26	111	0	0	32
					111	0	0	32	151	0	0	6
HE 240 A	0	0	Neve	PolG	0	0	0	25	133	0	0	31
					133	0	0	31	178	0	0	6
HE 240 A	0	0	Neve	PolG	0	0	0	24	136	0	0	29
					136	0	0	29	178	0	0	6
HE 240 A	0	328	Neve	PolG	0	0	0	6	30	0	0	39
					30	0	0	39	112	0	0	36
HE 240 A	0	0	Neve	PolG	0	0	0	6	27	0	0	38
					27	0	0	38	108	0	0	34
HE 240 A	0	75	Neve	PolG	0	0	0	6	29	0	0	34
					29	0	0	34	134	0	0	30
HE 240 A	0	0	Neve	PolG	0	0	0	6	31	0	0	32
					31	0	0	32	148	0	0	29
HE 240 A	0	0	Neve	PolG	0	0	0	6	30	0	0	31
					30	0	0	31	151	0	0	27
HE 240 A	0	0	Neve	PolG	0	0	0	6	33	0	0	29
					33	0	0	29	178	0	0	26
HE 240 A	0	328	Neve	PolG	0	0	0	35	73	0	0	40
					73	0	0	40	112	0	0	6
HE 240 A	0	75	Neve	PolG	0	0	0	29	95	0	0	35
					95	0	0	35	134	0	0	6
HE 240 A	0	0	Neve	PolG	0	0	0	6	31	0	0	28
					31	0	0	28	178	0	0	24
HE 240 A	0	0	Neve	PolG	0	0	0	34	72	0	0	39
					72	0	0	39	108	0	0	6
HE 240 A	0	0	Vento X	PolG	0	0	0	52	72	0	0	60
					72	0	0	60	108	0	0	9
HE 240 A	0	328	Vento X	PolG	0	0	0	55	73	0	0	62
					73	0	0	62	112	0	0	9
HE 240 A	0	75	Vento X	PolG	0	0	0	46	95	0	0	54
					95	0	0	54	134	0	0	9
HE 240 A	0	0	Vento X	PolG	0	0	0	43	107	0	0	51
					107	0	0	51	148	0	0	9
HE 240 A	0	0	Vento X	PolG	0	0	0	9	31	0	0	43
					31	0	0	43	178	0	0	38
HE 240 A	0	0	Vento X	PolG	0	0	0	9	33	0	0	46
					33	0	0	46	178	0	0	40
HE 240 A	0	0	Vento X	PolG	0	0	0	9	30	0	0	48
					30	0	0	48	151	0	0	42
HE 240 A	0	0	Vento X	PolG	0	0	0	9	31	0	0	50
					31	0	0	50	148	0	0	44

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	75	Vento X	PolG	0	0	0	9	29	0	0	52
					29	0	0	52	134	0	0	47
HE 240 A	0	0	Vento X	PolG	0	0	0	41	111	0	0	49
					111	0	0	49	151	0	0	9
HE 240 A	0	0	Vento X	PolG	0	0	0	39	133	0	0	47
					133	0	0	47	178	0	0	9
HE 240 A	0	0	Vento X	PolG	0	0	0	9	27	0	0	58
					27	0	0	58	108	0	0	53
HE 240 A	0	328	Vento X	PolG	0	0	0	9	30	0	0	61
					30	0	0	61	112	0	0	56
HE 240 A	0	0	Vento X	PolG	0	0	0	36	136	0	0	45
					136	0	0	45	178	0	0	9
HE 240 A	0	0	Carichi termici	Termico	0	0	0	60	123	0	0	60
					0	0	0	59	28	0	0	109
HE 240 A	0	0	Carichi termici	Termico	0	0	0	109	85	0	0	111
					85	0	0	111	123	0	0	60
HE 240 A	0	328	Carichi termici	Termico	0	0	0	19	28	0	0	35
					28	0	0	35	85	0	0	36
HE 240 A	0	0	Carichi termici	Termico	0	0	0	31	85	0	0	36
					85	0	0	36	123	0	0	6
HE 240 A	0	75	Carichi termici	Termico	0	0	0	9	28	0	0	54
					28	0	0	54	123	0	0	49
HE 240 A	75	76	Peso Proprio	UnifG	0	0	0	85	0	0	0	9
					0	0	0	56	123	0	0	56
HE 240 A	75	76	QV Solai	PolG	0	0	0	48	85	0	0	56
					85	0	0	56	123	0	0	9
HE 240 A	75	76	QV Solai	PolG	0	0	0	60	113	0	0	60
					0	0	0	61	27	0	0	113
HE 240 A	76	0	Peso Proprio	UnifG	0	0	0	113	77	0	0	116
					0	0	0	116	113	0	0	63
HE 240 A	76	0	QV Solai	PolG	0	0	0	20	27	0	0	36
					27	0	0	36	77	0	0	37
HE 240 A	76	0	Neve	PolG	0	0	0	6	27	0	0	20
					27	0	0	36	113	0	0	33
HE 240 A	76	0	Neve	PolG	0	0	0	32	77	0	0	37
					77	0	0	37	113	0	0	6
HE 240 A	76	0	Vento X	PolG	0	0	0	50	77	0	0	58
					77	0	0	58	113	0	0	9
HE 240 A	76	0	Vento X	PolG	0	0	0	9	27	0	0	56
					27	0	0	56	113	0	0	51
HE 240 A	76	0	Carichi termici	Termico	0	0	0	60	182	0	0	60
					0	0	0	45	29	0	0	80
HE 240 A	102	0	Peso Proprio	UnifG	0	0	0	80	141	0	0	83
					29	0	0	83	182	0	0	46
HE 240 A	102	0	QV Solai	PolG	0	0	0	14	29	0	0	26
					29	0	0	26	141	0	0	27
HE 240 A	102	0	Neve	PolG	0	0	0	6	29	0	0	27
					29	0	0	27	182	0	0	23
HE 240 A	102	0	Neve	PolG	0	0	0	22	141	0	0	28
					141	0	0	28	182	0	0	6
HE 240 A	102	0	Vento X	PolG	0	0	0	9	29	0	0	41
					29	0	0	41	182	0	0	35
HE 240 A	102	0	Vento X	PolG	0	0	0	34	141	0	0	43

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYL	QZi	Xf	QXf	QYf	QZf
HE 240 A	102	0	Carichi termici	Termico	141	0	0	43	182	0	0	9
Trave 8002												
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	148	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	0	71	Peso Proprio	UnitG	0	0	0	60	134	0	0	60
HE 240 A	0	0	QP Solai	PolG	23	0	0	45	23	0	0	82
					23	0	0	82	145	0	0	85
HE 240 A	0	0	QP Solai	PolG	145	0	0	85	178	0	0	46
					21	0	0	49	21	0	0	92
					21	0	0	92	120	0	0	95
HE 240 A	0	0	QP Solai	PolG	120	0	0	95	151	0	0	51
					22	0	0	52	22	0	0	96
					22	0	0	96	116	0	0	99
HE 240 A	0	0	QP Solai	PolG	116	0	0	99	148	0	0	53
					24	0	0	47	24	0	0	87
					143	0	0	87	143	0	0	90
HE 240 A	0	71	QP Solai	PolG	143	0	0	90	178	0	0	48
					21	0	0	54	21	0	0	101
					104	0	0	101	104	0	0	104
HE 240 A	0	0	QV Solai	PolG	104	0	0	104	134	0	0	56
					24	0	0	15	24	0	0	28
					143	0	0	28	143	0	0	29
HE 240 A	0	71	QV Solai	PolG	143	0	0	29	178	0	0	16
					21	0	0	17	21	0	0	32
					21	0	0	32	104	0	0	33
HE 240 A	0	0	QV Solai	PolG	104	0	0	33	134	0	0	18
					23	0	0	14	23	0	0	26
HE 240 A	0	0	QV Solai	PolG	23	0	0	26	145	0	0	27
					145	0	0	27	178	0	0	15
HE 240 A	0	0	QV Solai	PolG	0	0	0	16	21	0	0	29
					21	0	0	29	120	0	0	30
HE 240 A	0	0	QV Solai	PolG	120	0	0	30	151	0	0	16
					22	0	0	17	22	0	0	31
					116	0	0	31	116	0	0	32
HE 240 A	0	0	Neve	PolG	0	0	0	32	148	0	0	17
					22	0	0	4	22	0	0	31
HE 240 A	0	0	Neve	PolG	0	0	0	31	148	0	0	29
					120	0	0	26	120	0	0	31
HE 240 A	0	71	Neve	PolG	0	0	0	4	21	0	0	33
HE 240 A	0	0	Neve	PolG	21	0	0	33	134	0	0	30
					23	0	0	4	23	0	0	27
HE 240 A	0	0	Neve	PolG	0	0	0	27	178	0	0	24
					21	0	0	4	21	0	0	30
HE 240 A	0	0	Neve	PolG	0	0	0	30	151	0	0	27
					116	0	0	28	116	0	0	32
HE 240 A	0	71	Neve	PolG	0	0	0	32	148	0	0	4
					104	0	0	29	104	0	0	34
HE 240 A	0	0	Neve	PolG	0	0	0	34	134	0	0	4
					24	0	0	28	178	0	0	26
HE 240 A	0	0	Neve	PolG	0	0	0	28	178	0	0	28
					145	0	0	28	178	0	0	4
HE 240 A	0	0	Neve	PolG	0	0	0	25	143	0	0	30
					143	0	0	30	178	0	0	4
HE 240 A	0	0	Vento X	PolG	0	0	0	39	143	0	0	46
HE 240 A	0	71	Vento X	PolG	143	0	0	46	178	0	0	7
					104	0	0	45	104	0	0	52
HE 240 A	0	0	Vento X	PolG	0	0	0	52	134	0	0	7
					21	0	0	7	21	0	0	46
HE 240 A	0	0	Vento X	PolG	0	0	0	46	151	0	0	42
					116	0	0	43	116	0	0	50
HE 240 A	0	0	Vento X	PolG	0	0	0	50	148	0	0	7

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Vento X	PolG	23	0	0	7	23	0	0	41
HE 240 A	0	0	Vento X	PolG	24	0	0	7	24	0	0	38
HE 240 A	0	71	Vento X	PolG	21	0	0	7	21	0	0	50
HE 240 A	0	0	Vento X	PolG	21	0	0	50	134	0	0	47
HE 240 A	0	0	Vento X	PolG	120	0	0	41	120	0	0	48
HE 240 A	0	0	Vento X	PolG	22	0	0	48	151	0	0	7
HE 240 A	0	0	Vento X	PolG	22	0	0	7	22	0	0	48
HE 240 A	0	0	Vento X	PolG	145	0	0	36	145	0	0	44
HE 240 A	0	0	Carichi termici	Termico	145	0	0	44	178	0	0	7
HE 240 A	0	0	Carichi termici	Termico	145	0	0	44	178	0	0	7
HE 240 A	0	0	Carichi termici	Termico	145	0	0	44	178	0	0	7
HE 240 A	0	0	Carichi termici	Termico	145	0	0	44	178	0	0	7
HE 240 A	0	71	Carichi termici	Termico	145	0	0	44	178	0	0	7
HE 240 A	71	72	Peso Proprio	UnitG	0	0	0	60	123	0	0	60
HE 240 A	71	72	QP Solai	PolG	0	0	0	106	93	0	0	106
					20	0	0	106	93	0	0	109
HE 240 A	71	72	QV Solai	PolG	93	0	0	109	123	0	0	58
					20	0	0	18	20	0	0	34
					93	0	0	34	93	0	0	35
HE 240 A	71	72	Neve	PolG	0	0	0	35	123	0	0	19
					93	0	0	31	93	0	0	35
HE 240 A	71	72	Neve	PolG	0	0	0	35	123	0	0	4
					20	0	0	4	20	0	0	34
HE 240 A	71	72	Vento X	PolG	20	0	0	34	123	0	0	32
					20	0	0	7	20	0	0	53
HE 240 A	71	72	Vento X	PolG	20	0	0	53	123	0	0	49
					93	0	0	48	93	0	0	55
HE 240 A	71	72	Vento X	PolG	93	0	0	55	123	0	0	7
HE 240 A	71	72	Carichi termici	Termico	145	0	0	60	113	0	0	60
HE 240 A	72	397	Peso Proprio	UnitG	0	0	0	59	19	0	0	111
HE 240 A	72	397	QP Solai	PolG	19	0	0	111	85	0	0	113
					85	0	0	113	113	0	0	60
HE 240 A	72	397	QV Solai	PolG	19	0	0	19	19	0	0	35
					85	0	0	35	85	0	0	36
HE 240 A	72	397	Neve	PolG	0	0	0	36	113	0	0	19
					19	0	0	4	19	0	0	35
HE 240 A	72	397	Neve	PolG	0	0	0	35	113	0	0	33
					85	0	0	32	85	0	0	37
HE 240 A	72	397	Vento X	PolG	0	0	0	50	85	0	0	4
					85	0	0	57	113	0	0	7
HE 240 A	72	397	Vento X	PolG	0	0	0	7	19	0	0	55
					19	0	0	55	113	0	0	51
HE 240 A	72	397	Carichi termici	Termico	145	0	0	60	182	0	0	60
HE 240 A	103	0	Peso Proprio	UnitG	0	0	0	42	22	0	0	77
HE 240 A	103	0	QP Solai	PolG	22	0	0	77	151	0	0	81
					151	0	0	81	182	0	0	44
HE 240 A	103	0	QV Solai	PolG	22	0	0	25	151	0	0	26
					151	0	0	26	182	0	0	14
HE 240 A	103	0	Neve	PolG	0	0	0	22	151	0	0	27
HE 240 A	103	0	Neve	PolG	151	0	0	27	182	0	0	4
HE 240 A	103	0	Vento X	PolG	22	0	0	25	182	0	0	23
					151	0	0	34	151	0	0	42
HE 240 A	103	0	Vento X	PolG	0	0	0	42	182	0	0	7
					22	0	0	39	182	0	0	35
HE 240 A	103	0	Carichi termici	Termico	145	0	0	60	182	0	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	397	398	Peso Proprio	UnifG	0	0	0	0	60	108	0	0
HE 240 A	397	398	QP Solai	PolG	0	0	0	61	19	0	0	115
					19	0	0	115	80	0	0	118
					80	0	0	118	108	0	0	63
HE 240 A	397	398	QV Solai	PolG	0	0	0	20	19	0	0	37
					19	0	0	37	80	0	0	38
					80	0	0	38	108	0	0	20
HE 240 A	397	398	Neve	PolG	0	0	0	4	19	0	0	37
					19	0	0	37	108	0	0	34
HE 240 A	397	398	Neve	PolG	0	0	0	34	80	0	0	38
					80	0	0	38	108	0	0	4
HE 240 A	397	398	Vento X	PolG	0	0	0	52	80	0	0	59
					80	0	0	59	108	0	0	7
HE 240 A	397	398	Vento X	PolG	0	0	0	7	19	0	0	57
					19	0	0	57	108	0	0	53
HE 240 A	397	398	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	398	329	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
HE 240 A	398	329	QP Solai	PolG	0	0	0	64	20	0	0	120
					20	0	0	120	82	0	0	123
					82	0	0	123	112	0	0	65
HE 240 A	398	329	QV Solai	PolG	0	0	0	20	20	0	0	38
					20	0	0	38	82	0	0	39
					82	0	0	39	112	0	0	21
HE 240 A	398	329	Neve	PolG	0	0	0	4	20	0	0	38
					20	0	0	38	112	0	0	36
HE 240 A	398	329	Neve	PolG	0	0	0	35	82	0	0	40
					82	0	0	40	112	0	0	4
HE 240 A	398	329	Vento X	PolG	0	0	0	55	82	0	0	61
					82	0	0	61	112	0	0	7
HE 240 A	398	329	Vento X	PolG	0	0	0	7	20	0	0	59
					20	0	0	59	112	0	0	56
HE 240 A	398	329	Carichi termici	Termico	AXY=15°C,AXZ=15°C							

Trave 8003

HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	0	65	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	0	0	QP Solai	PolG	0	0	0	44	13	0	0	84
					13	0	0	84	152	0	0	88
					152	0	0	88	178	0	0	46
HE 240 A	0	0	QP Solai	PolG	0	0	0	42	12	0	0	79
					12	0	0	79	154	0	0	83
					154	0	0	83	178	0	0	44
HE 240 A	0	65	QP Solai	PolG	0	0	0	51	12	0	0	98
					12	0	0	98	113	0	0	102
					113	0	0	102	134	0	0	53
HE 240 A	0	0	QP Solai	PolG	0	0	0	47	12	0	0	89
					12	0	0	89	129	0	0	92
					129	0	0	92	151	0	0	48
HE 240 A	0	0	QP Solai	PolG	0	0	0	49	12	0	0	93
					12	0	0	93	125	0	0	97
					125	0	0	97	148	0	0	51
HE 240 A	0	0	QV Solai	PolG	0	0	0	15	12	0	0	28
					12	0	0	28	129	0	0	30
					129	0	0	30	151	0	0	16
HE 240 A	0	0	QV Solai	PolG	0	0	0	14	13	0	0	27
					13	0	0	27	152	0	0	28
					152	0	0	28	178	0	0	15
HE 240 A	0	0	QV Solai	PolG	0	0	0	16	12	0	0	30
					12	0	0	30	125	0	0	31
					125	0	0	31	148	0	0	16
HE 240 A	0	0	QV Solai	PolG	0	0	0	13	12	0	0	25
					12	0	0	25	154	0	0	27
					154	0	0	27	178	0	0	14
HE 240 A	0	65	QV Solai	PolG	0	0	0	16	12	0	0	31

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					12	0	0	0	113	0	0	33
					113	0	0	33	134	0	0	17
HE 240 A	0	0	Neve	PolG	0	0	0	3	12	0	0	26
					12	0	0	26	178	0	0	24
HE 240 A	0	0	Neve	PolG	0	0	0	3	12	0	0	29
					12	0	0	29	151	0	0	27
HE 240 A	0	65	Neve	PolG	0	0	0	29	113	0	0	33
					113	0	0	33	134	0	0	3
HE 240 A	0	65	Neve	PolG	0	0	0	3	12	0	0	31
					12	0	0	31	134	0	0	30
HE 240 A	0	0	Neve	PolG	0	0	0	3	13	0	0	27
					13	0	0	27	178	0	0	26
HE 240 A	0	0	Neve	PolG	0	0	0	3	12	0	0	30
					12	0	0	30	148	0	0	29
HE 240 A	0	0	Neve	PolG	0	0	0	25	152	0	0	28
					152	0	0	28	178	0	0	3
HE 240 A	0	0	Neve	PolG	0	0	0	28	125	0	0	31
					125	0	0	31	148	0	0	3
HE 240 A	0	0	Neve	PolG	0	0	0	23	154	0	0	27
					154	0	0	27	178	0	0	3
HE 240 A	0	0	Neve	PolG	0	0	0	26	129	0	0	30
					129	0	0	30	151	0	0	3
HE 240 A	0	0	Vento X	PolG	0	0	0	36	154	0	0	42
					154	0	0	42	178	0	0	4
HE 240 A	0	0	Vento X	PolG	0	0	0	38	152	0	0	44
					152	0	0	44	178	0	0	4
HE 240 A	0	0	Vento X	PolG	0	0	0	40	129	0	0	46
					129	0	0	46	151	0	0	4
HE 240 A	0	0	Vento X	PolG	0	0	0	4	13	0	0	42
					13	0	0	42	178	0	0	40
HE 240 A	0	0	Vento X	PolG	0	0	0	4	12	0	0	46
					12	0	0	46	148	0	0	44
HE 240 A	0	0	Vento X	PolG	0	0	0	43	125	0	0	48
					125	0	0	48	148	0	0	4
HE 240 A	0	0	Vento X	PolG	0	0	0	4	12	0	0	44
					12	0	0	44	151	0	0	42
HE 240 A	0	65	Vento X	PolG	0	0	0	45	113	0	0	51
					113	0	0	51	134	0	0	4
HE 240 A	0	65	Vento X	PolG	0	0	0	4	12	0	0	49
					12	0	0	49	134	0	0	47
HE 240 A	0	0	Vento X	PolG	0	0	0	4	12	0	0	40
					12	0	0	40	178	0	0	38
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	65	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	65	66	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	65	66	QP Solai	PolG	0	0	0	54	11	0	0	103
					11	0	0	103	102	0	0	106
					102	0	0	106	123	0	0	55
HE 240 A	65	66	QV Solai	PolG	0	0	0	17	11	0	0	33
					11	0	0	33	102	0	0	34
HE 240 A	65	66	Neve	PolG	0	0	0	31	102	0	0	18
					102	0	0	34	123	0	0	34
HE 240 A	65	66	Neve	PolG	0	0	0	34	123	0	0	3
					11	0	0	3	11	0	0	33
HE 240 A	65	66	Vento X	PolG	0	0	0	4	11	0	0	51
					11	0	0	51	123	0	0	49
HE 240 A	65	66	Vento X	PolG	0	0	0	47	102	0	0	53
					102	0	0	53	123	0	0	4
HE 240 A	65	66	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	66	391	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	66	391	QP Solai	PolG	0	0	0	56	11	0	0	107
					11	0	0	107	94	0	0	111

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	66	391	QV Solai	PolG	94	0	0	0	111	113	0	58
HE 240 A					0	0	0	0	18	11	0	34
HE 240 A					11	0	0	0	34	94	0	36
HE 240 A	66	391	Neve	PolG	94	0	0	0	32	94	0	36
HE 240 A					94	0	0	0	36	113	0	3
HE 240 A	66	391	Neve	PolG	0	0	0	0	3	11	0	34
HE 240 A					11	0	0	0	34	113	0	33
HE 240 A	66	391	Vento X	PolG	0	0	0	4	11	0	0	53
HE 240 A					11	0	0	0	53	113	0	51
HE 240 A	66	391	Vento X	PolG	0	0	0	0	50	94	0	55
HE 240 A					94	0	0	0	55	113	0	4
HE 240 A	66	391	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	104	0	Peso Proprio	UnifG	0	0	0	0	60	182	0	60
HE 240 A	104	0	QP Solai	PolG	0	0	0	0	40	12	0	75
HE 240 A					12	0	0	0	75	158	0	78
HE 240 A					158	0	0	0	78	182	0	42
HE 240 A	104	0	QV Solai	PolG	0	0	0	0	13	12	0	24
HE 240 A					12	0	0	0	24	158	0	25
HE 240 A					158	0	0	0	25	182	0	13
HE 240 A	104	0	Neve	PolG	0	0	0	0	22	158	0	26
HE 240 A					158	0	0	0	26	182	0	3
HE 240 A	104	0	Neve	PolG	0	0	0	0	3	12	0	24
HE 240 A					12	0	0	0	24	182	0	23
HE 240 A	104	0	Vento X	PolG	0	0	0	4	12	0	0	38
HE 240 A					12	0	0	0	38	182	0	36
HE 240 A	104	0	Vento X	PolG	0	0	0	0	34	158	0	40
HE 240 A					158	0	0	0	40	182	0	4
HE 240 A	104	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	391	392	Peso Proprio	UnifG	0	0	0	0	60	108	0	60
HE 240 A	391	392	QP Solai	PolG	0	0	0	0	59	11	0	112
HE 240 A					11	0	0	0	112	89	0	115
HE 240 A					89	0	0	0	115	108	0	60
HE 240 A	391	392	QV Solai	PolG	0	0	0	0	19	11	0	36
HE 240 A					11	0	0	0	36	89	0	37
HE 240 A					89	0	0	0	37	108	0	19
HE 240 A	391	392	Neve	PolG	0	0	0	0	34	89	0	37
HE 240 A					89	0	0	0	37	108	0	3
HE 240 A	391	392	Neve	PolG	0	0	0	0	3	11	0	36
HE 240 A					11	0	0	0	36	108	0	34
HE 240 A	391	392	Vento X	PolG	0	0	0	0	52	89	0	57
HE 240 A					89	0	0	0	57	108	0	4
HE 240 A	391	392	Vento X	PolG	0	0	0	4	11	0	0	55
HE 240 A					11	0	0	0	55	108	0	53
HE 240 A	391	392	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	392	330	Peso Proprio	UnifG	0	0	0	0	60	112	0	60
HE 240 A	392	330	QP Solai	PolG	0	0	0	0	61	12	0	117
HE 240 A					12	0	0	0	117	91	0	120
HE 240 A					91	0	0	0	120	112	0	62
HE 240 A	392	330	QV Solai	PolG	0	0	0	0	20	12	0	37
HE 240 A					12	0	0	0	37	91	0	38
HE 240 A					91	0	0	0	38	112	0	20
HE 240 A	392	330	Neve	PolG	0	0	0	0	35	91	0	39
HE 240 A					91	0	0	0	39	112	0	3
HE 240 A	392	330	Neve	PolG	0	0	0	0	3	12	0	37
HE 240 A					12	0	0	0	37	112	0	36
HE 240 A	392	330	Vento X	PolG	0	0	0	0	54	91	0	60
HE 240 A					91	0	0	0	60	112	0	4
HE 240 A	392	330	Vento X	PolG	0	0	0	0	4	12	0	57
HE 240 A					12	0	0	0	57	112	0	55
HE 240 A	392	330	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A					0	0	0	0	60	134	0	60
HE 240 A	0	77	Peso Proprio	UnifG	0	0	0	0	60	148	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	0	60	108	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	0	60	108	0	60
HE 240 A	0	331	Peso Proprio	UnifG	0	0	0	0	60	112	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	0	60	178	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	0	60	151	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	0	60	178	0	60
HE 240 A	0	77	QP Solai	PolG	4	0	0	0	96	122	0	100
HE 240 A					122	0	0	0	100	134	0	51
HE 240 A	0	0	QP Solai	PolG	0	0	0	0	44	4	0	86
HE 240 A					4	0	0	0	86	139	0	90
HE 240 A	0	0	QP Solai	PolG	139	0	0	0	90	151	0	46
HE 240 A					0	0	0	0	47	4	0	91
HE 240 A					4	0	0	0	91	135	0	95
HE 240 A					135	0	0	0	95	148	0	49
HE 240 A	0	0	QP Solai	PolG	0	0	0	0	40	4	0	77
HE 240 A					4	0	0	0	77	164	0	81
HE 240 A	0	331	QP Solai	PolG	164	0	0	0	81	178	0	42
HE 240 A					0	0	0	0	58	4	0	114
HE 240 A					4	0	0	0	114	100	0	118
HE 240 A	0	0	QP Solai	PolG	100	0	0	0	118	112	0	61
HE 240 A					0	0	0	0	42	4	0	81
HE 240 A					4	0	0	0	81	164	0	86
HE 240 A					164	0	0	0	86	178	0	44
HE 240 A	0	0	QP Solai	PolG	0	0	0	0	56	4	0	110
HE 240 A					4	0	0	0	110	97	0	114
HE 240 A	0	0	QV Solai	PolG	97	0	0	0	114	108	0	58
HE 240 A					0	0	0	0	15	4	0	29
HE 240 A					4	0	0	0	29	135	0	30
HE 240 A					135	0	0	0	30	148	0	16
HE 240 A	0	0	QV Solai	PolG	0	0	0	0	13	4	0	25
HE 240 A					4	0	0	0	25	164	0	26
HE 240 A	0	0	QV Solai	PolG	164	0	0	0	26	178	0	13
HE 240 A					0	0	0	0	14	4	0	28
HE 240 A					4	0	0	0	28	139	0	29
HE 240 A					139	0	0	0	29	151	0	15
HE 240 A	0	0	QV Solai	PolG	0	0	0	0	13	4	0	26
HE 240 A					4	0	0	0	26	164	0	27
HE 240 A	0	77	QV Solai	PolG	164	0	0	0	27	178	0	14
HE 240 A					4	0	0	0	16	4	0	31
HE 240 A					122	0	0	0	31	122	0	32
HE 240 A	0	331	QV Solai	PolG	0	0	0	0	32	134	0	16
HE 240 A					0	0	0	0	19	4	0	37
HE 240 A					4	0	0	0	37	100	0	38
HE 240 A					100	0	0	0	38	112	0	19
HE 240 A	0	0	QV Solai	PolG	0	0	0	0	18	4	0	35
HE 240 A					4	0	0	0	35	97	0	36
HE 240 A	0	0	Neve	PolG	97	0	0	0	36	108	0	19
HE 240 A					0	0	0	0	1	4	0	27
HE 240 A	0	0	Neve	PolG	4	0	0	0	27	151	0	27
HE 240 A					4	0	0	0	1	4	0	26
HE 240 A	0	0	Neve	PolG	4	0	0	0	26	178	0	26
HE 240 A					0	0	0	0	1	4	0	24
HE 240 A					4	0	0	0	24	178	0	25
HE 240 A	0	77	Neve	PolG	0	0	0	0	29	122	0	32
HE 240 A					122	0	0	0	32	134	0	1
HE 240 A	0	331	Neve	PolG	0	0	0	0	35	100	0	37
HE 240 A					100	0	0	0	37	112	0	1
HE 240 A	0	0	Neve	PolG	0	0	0	0	1	4	0	29
HE 240 A					4	0	0	0	29	148	0	29
HE 240 A	0	77	Neve	PolG	4	0	0	0	1	4	0	30
HE 240 A					4	0	0	0	30	134	0	30
HE 240 A	0	0	Neve	PolG	0	0	0	0	1	4	0	35
HE 240 A					4	0	0	0	35	108	0	35
HE 240 A	0	0	Neve	PolG	0	0	0	0	26	139	0	29
HE 240 A					139	0	0	0	29	151	0	1
HE 240 A	0	0	Neve	PolG	0	0	0	0	25	164	0	27
HE 240 A					164	0	0	0	27	178	0	1
HE 240 A	0	331	Neve	PolG	0	0	0	0	1	4	0	36

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Neve	PolG	4	0	0	36	112	0	0	36
HE 240 A	0	0	Neve	PolG	0	0	0	33	97	0	0	36
HE 240 A	0	0	Neve	PolG	97	0	0	36	108	0	0	1
HE 240 A	0	0	Neve	PolG	0	0	0	23	164	0	0	26
HE 240 A	0	0	Neve	PolG	164	0	0	26	178	0	0	1
HE 240 A	0	0	Neve	PolG	0	0	0	28	135	0	0	30
HE 240 A	0	0	Vento X	PolG	135	0	0	30	148	0	0	1
HE 240 A	0	0	Vento X	PolG	4	0	0	54	108	0	0	54
HE 240 A	0	331	Vento X	PolG	4	0	0	2	4	0	0	56
HE 240 A	0	77	Vento X	PolG	4	0	0	56	112	0	0	56
HE 240 A	0	0	Vento X	PolG	122	0	0	45	122	0	0	49
HE 240 A	0	0	Vento X	PolG	4	0	0	2	4	0	0	45
HE 240 A	0	0	Vento X	PolG	4	0	0	45	148	0	0	45
HE 240 A	0	0	Vento X	PolG	164	0	0	36	164	0	0	40
HE 240 A	0	0	Vento X	PolG	0	0	0	40	178	0	0	2
HE 240 A	0	0	Vento X	PolG	0	0	0	43	135	0	0	47
HE 240 A	0	0	Vento X	PolG	135	0	0	47	148	0	0	2
HE 240 A	0	0	Vento X	PolG	0	0	0	40	139	0	0	44
HE 240 A	0	0	Vento X	PolG	139	0	0	44	151	0	0	2
HE 240 A	0	0	Vento X	PolG	0	0	0	38	164	0	0	42
HE 240 A	0	331	Vento X	PolG	164	0	0	42	178	0	0	2
HE 240 A	0	77	Vento X	PolG	100	0	0	58	112	0	0	2
HE 240 A	0	77	Vento X	PolG	0	0	0	2	4	0	0	47
HE 240 A	0	0	Vento X	PolG	4	0	0	47	134	0	0	47
HE 240 A	0	0	Vento X	PolG	0	0	0	2	4	0	0	42
HE 240 A	0	0	Vento X	PolG	4	0	0	42	151	0	0	42
HE 240 A	0	0	Vento X	PolG	0	0	0	2	4	0	0	38
HE 240 A	0	0	Vento X	PolG	4	0	0	38	178	0	0	38
HE 240 A	0	0	Vento X	PolG	0	0	0	2	4	0	0	40
HE 240 A	0	0	Vento X	PolG	4	0	0	40	178	0	0	40
HE 240 A	0	77	Vento X	PolG	97	0	0	51	97	0	0	55
HE 240 A	0	77	Carichi termici	Termico	AXY=15°C, AXZ=15°C	97	0	55	108	0	0	2
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	0	0	0	0
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	0	0	0	0
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	0	0	0	0
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	0	0	0	0
HE 240 A	0	331	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	0	0	0	0
HE 240 A	0	77	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	0	0	0	0
HE 240 A	77	78	Peso Proprio	UnitG	0	0	0	60	123	0	0	60
HE 240 A	77	78	QV Solai	PolG	4	0	0	51	4	0	0	100
HE 240 A	77	78	QV Solai	PolG	4	0	0	100	111	0	0	104
HE 240 A	77	78	QV Solai	PolG	111	0	0	104	123	0	0	54
HE 240 A	77	78	QV Solai	PolG	0	0	0	16	4	0	0	32
HE 240 A	77	78	QV Solai	PolG	4	0	0	32	111	0	0	33
HE 240 A	77	78	QV Solai	PolG	111	0	0	33	123	0	0	17
HE 240 A	77	78	QV Solai	PolG	0	0	0	1	4	0	0	32
HE 240 A	77	78	QV Solai	PolG	4	0	0	32	123	0	0	32
HE 240 A	77	78	QV Solai	PolG	0	0	0	30	111	0	0	33
HE 240 A	77	78	QV Solai	PolG	111	0	0	33	123	0	0	1
HE 240 A	77	78	QV Solai	PolG	0	0	0	47	111	0	0	51
HE 240 A	77	78	QV Solai	PolG	111	0	0	51	123	0	0	2
HE 240 A	77	78	QV Solai	PolG	0	0	0	2	4	0	0	49
HE 240 A	77	78	QV Solai	PolG	4	0	0	49	123	0	0	49
HE 240 A	77	78	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	0	0	0	0	0
HE 240 A	78	0	Peso Proprio	UnitG	0	0	0	60	113	0	0	60
HE 240 A	78	0	QV Solai	PolG	0	0	0	53	4	0	0	105
HE 240 A	78	0	QV Solai	PolG	4	0	0	105	102	0	0	109
HE 240 A	78	0	QV Solai	PolG	102	0	0	109	113	0	0	56
HE 240 A	78	0	QV Solai	PolG	0	0	0	17	4	0	0	34
HE 240 A	78	0	QV Solai	PolG	4	0	0	34	102	0	0	35
HE 240 A	78	0	QV Solai	PolG	102	0	0	35	113	0	0	18

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	78	0	Neve	PolG	4	0	0	1	4	0	0	33
HE 240 A	78	0	Neve	PolG	0	0	0	33	113	0	0	33
HE 240 A	78	0	Neve	PolG	102	0	0	34	113	0	0	1
HE 240 A	78	0	Vento X	PolG	0	0	0	49	102	0	0	53
HE 240 A	78	0	Vento X	PolG	102	0	0	53	113	0	0	2
HE 240 A	78	0	Vento X	PolG	0	0	0	2	4	0	0	52
HE 240 A	78	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	4	0	52	113	0	0	52
HE 240 A	105	0	Peso Proprio	UnitG	0	0	0	60	182	0	0	60
HE 240 A	105	0	QV Solai	PolG	3	0	0	72	169	0	0	76
HE 240 A	105	0	QV Solai	PolG	169	0	0	76	182	0	0	39
HE 240 A	105	0	QV Solai	PolG	0	0	0	12	3	0	0	23
HE 240 A	105	0	QV Solai	PolG	3	0	0	23	169	0	0	24
HE 240 A	105	0	QV Solai	PolG	169	0	0	24	182	0	0	13
HE 240 A	105	0	QV Solai	PolG	0	0	0	22	169	0	0	24
HE 240 A	105	0	QV Solai	PolG	169	0	0	24	182	0	0	1
HE 240 A	105	0	QV Solai	PolG	3	0	0	1	3	0	0	23
HE 240 A	105	0	QV Solai	PolG	3	0	0	23	182	0	0	23
HE 240 A	105	0	QV Solai	PolG	3	0	0	2	3	0	0	36
HE 240 A	105	0	QV Solai	PolG	3	0	0	36	182	0	0	36
HE 240 A	105	0	QV Solai	PolG	0	0	0	34	169	0	0	38
HE 240 A	105	0	QV Solai	PolG	169	0	0	38	182	0	0	2
HE 240 A	105	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	169	0	0	0	0	0	0
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	148	0	0	60
HE 240 A	0	69	Peso Proprio	UnitG	0	0	0	60	134	0	0	60
HE 240 A	0	69	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	0	69	QV Solai	PolG	130	0	0	93	130	0	0	98
HE 240 A	0	0	QV Solai	PolG	174	0	0	98	134	0	0	0
HE 240 A	0	0	QV Solai	PolG	0	0	0	74	174	0	0	79
HE 240 A	0	0	QV Solai	PolG	174	0	0	79	178	0	0	0
HE 240 A	0	0	QV Solai	PolG	144	0	0	88	144	0	0	93
HE 240 A	0	0	QV Solai	PolG	0	0	0	84	147	0	0	88
HE 240 A	0	0	QV Solai	PolG	147	0	0	88	151	0	0	0
HE 240 A	0	0	QV Solai	PolG	0	0	0	79	173	0	0	83
HE 240 A	0	0	QV Solai	PolG	173	0	0	83	178	0	0	0
HE 240 A	0	0	QV Solai	PolG	0	0	0	25	173	0	0	27
HE 240 A	0	69	QV Solai	PolG	173	0	0	27	178	0	0	0
HE 240 A	0	69	QV Solai	PolG	130	0	0	30	130	0	0	31
HE 240 A	0	0	QV Solai	PolG	0	0	0	28	144	0	0	30
HE 240 A	0	0	QV Solai	PolG	144	0	0	30	148	0	0	0
HE 240 A	0	0	QV Solai	PolG	0	0	0	27	147	0	0	28
HE 240 A	0	0	QV Solai	PolG	147	0	0	28	151	0	0	0
HE 240 A	0	0	QV Solai	PolG	174	0	0	25	178	0	0	0
HE 240 A	0	69	QV Solai	PolG	174	0	0	29	130	0	0	30
HE 240 A	0	0	QV Solai	PolG	130	0	0	30	134	0	0	0
HE 240 A	0	0	QV Solai	PolG	0	0	0	27	144	0	0	29
HE 240 A	0	0	QV Solai	PolG	144	0	0	29	148	0	0	0
HE 240 A	0	0	QV Solai	PolG	0	0	0	23	174	0	0	24
HE 240 A	0	0	QV Solai	PolG	174	0	0	24	178	0	0	0
HE 240 A	0	0	QV Solai	PolG	0	0	0	26	147	0	0	27
HE 240 A	0	69	QV Solai	PolG	147	0	0	27	151	0	0	0
HE 240 A	0	69	QV Solai	PolG	130	0	0	30	134	0	0	30
HE 240 A	0	0	QV Solai	PolG	0	0	0	26	147	0	0	28
HE 240 A	0	0	QV Solai	PolG	147	0	0	28	151	0	0	0
HE 240 A	0	0	QV Solai	PolG	144	0	0	28	144	0	0	29
HE 240 A	0	0	QV Solai	PolG	144	0	0	25	173	0	0	26

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Neve	PolG	173	0	0	26	178	0	0	0
HE 240 A	0	0	Neve	PolG	174	0	0	23	174	0	0	25
HE 240 A	0	0	Neve	PolG	174	0	0	25	178	0	0	0
HE 240 A	0	0	Neve	PolG	173	0	0	24	173	0	0	26
HE 240 A	0	0	Vento X	PolG	173	0	0	26	178	0	0	0
HE 240 A	0	0	Vento X	PolG	174	0	0	36	174	0	0	38
HE 240 A	0	0	Vento X	PolG	174	0	0	38	178	0	0	0
HE 240 A	0	0	Vento X	PolG	147	0	0	43	151	0	0	43
HE 240 A	0	69	Vento X	PolG	147	0	0	45	130	0	0	47
HE 240 A	0	69	Vento X	PolG	130	0	0	47	134	0	0	0
HE 240 A	0	69	Vento X	PolG	130	0	0	45	130	0	0	47
HE 240 A	0	0	Vento X	PolG	130	0	0	47	134	0	0	0
HE 240 A	0	0	Vento X	PolG	174	0	0	38	178	0	0	38
HE 240 A	0	0	Vento X	PolG	174	0	0	38	178	0	0	0
HE 240 A	0	0	Vento X	PolG	144	0	0	43	144	0	0	45
HE 240 A	0	0	Vento X	PolG	144	0	0	45	148	0	0	0
HE 240 A	0	0	Vento X	PolG	144	0	0	42	144	0	0	44
HE 240 A	0	0	Vento X	PolG	144	0	0	44	148	0	0	0
HE 240 A	0	0	Vento X	PolG	173	0	0	40	178	0	0	40
HE 240 A	0	0	Vento X	PolG	173	0	0	38	173	0	0	40
HE 240 A	0	0	Vento X	PolG	173	0	0	40	178	0	0	0
HE 240 A	0	0	Vento X	PolG	173	0	0	40	147	0	0	42
HE 240 A	0	0	Vento X	PolG	147	0	0	42	151	0	0	0
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	123	0	0	60
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	98	119	0	0	102
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	102	123	0	0	0
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	31	119	0	0	33
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	33	123	0	0	0
HE 240 A	69	70	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	69	70	QP Solai	PolG	119	0	0	98	119	0	0	102
HE 240 A	69	70	QP Solai	PolG	119	0	0	31	119	0	0	33
HE 240 A	69	70	Neve	PolG	119	0	0	30	119	0	0	32
HE 240 A	69	70	Neve	PolG	119	0	0	32	123	0	0	0
HE 240 A	69	70	Neve	PolG	119	0	0	31	119	0	0	32
HE 240 A	69	70	Vento X	PolG	119	0	0	32	123	0	0	0
HE 240 A	69	70	Vento X	PolG	119	0	0	47	119	0	0	49
HE 240 A	69	70	Vento X	PolG	119	0	0	49	123	0	0	0
HE 240 A	69	70	Vento X	PolG	119	0	0	47	119	0	0	49
HE 240 A	69	70	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	49	123	0	0	0
HE 240 A	70	395	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	70	395	QP Solai	PolG	109	0	0	102	109	0	0	107
HE 240 A	70	395	QP Solai	PolG	109	0	0	107	113	0	0	0
HE 240 A	70	395	QP Solai	PolG	109	0	0	33	109	0	0	34
HE 240 A	70	395	QP Solai	PolG	109	0	0	34	113	0	0	0
HE 240 A	70	395	Neve	PolG	109	0	0	32	109	0	0	33
HE 240 A	70	395	Neve	PolG	109	0	0	33	113	0	0	0
HE 240 A	70	395	Neve	PolG	109	0	0	32	109	0	0	33
HE 240 A	70	395	Vento X	PolG	109	0	0	49	109	0	0	51
HE 240 A	70	395	Vento X	PolG	109	0	0	51	113	0	0	0
HE 240 A	70	395	Vento X	PolG	109	0	0	49	109	0	0	52
HE 240 A	70	395	Vento X	PolG	109	0	0	52	113	0	0	0
HE 240 A	70	395	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	182	0	0	60
HE 240 A	106	0	Peso Proprio	UnifG	0	0	0	70	178	0	0	74
HE 240 A	106	0	QP Solai	PolG	178	0	0	74	182	0	0	0
HE 240 A	106	0	QP Solai	PolG	178	0	0	22	178	0	0	24
HE 240 A	106	0	QP Solai	PolG	178	0	0	24	182	0	0	0
HE 240 A	106	0	Neve	PolG	178	0	0	22	178	0	0	23
HE 240 A	106	0	Neve	PolG	178	0	0	23	182	0	0	0
HE 240 A	106	0	Neve	PolG	178	0	0	22	178	0	0	23

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	106	0	Vento X	PolG	178	0	0	23	182	0	0	0
HE 240 A	106	0	Vento X	PolG	178	0	0	33	178	0	0	36
HE 240 A	106	0	Vento X	PolG	178	0	0	33	178	0	0	36
HE 240 A	106	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	108	0	0	60
HE 240 A	395	396	Peso Proprio	UnifG	0	0	0	107	104	0	0	112
HE 240 A	395	396	QP Solai	PolG	104	0	0	112	108	0	0	0
HE 240 A	395	396	QP Solai	PolG	104	0	0	34	104	0	0	36
HE 240 A	395	396	Neve	PolG	104	0	0	36	108	0	0	0
HE 240 A	395	396	Neve	PolG	104	0	0	33	104	0	0	34
HE 240 A	395	396	Neve	PolG	104	0	0	34	108	0	0	0
HE 240 A	395	396	Vento X	PolG	104	0	0	35	108	0	0	35
HE 240 A	395	396	Vento X	PolG	104	0	0	52	104	0	0	54
HE 240 A	395	396	Vento X	PolG	104	0	0	54	108	0	0	0
HE 240 A	395	396	Vento X	PolG	104	0	0	51	104	0	0	53
HE 240 A	395	396	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	53	108	0	0	0
HE 240 A	396	332	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
HE 240 A	396	332	QP Solai	PolG	108	0	0	116	112	0	0	116
HE 240 A	396	332	QP Solai	PolG	108	0	0	36	108	0	0	37
HE 240 A	396	332	QP Solai	PolG	108	0	0	37	112	0	0	0
HE 240 A	396	332	Neve	PolG	108	0	0	35	108	0	0	36
HE 240 A	396	332	Neve	PolG	108	0	0	36	112	0	0	0
HE 240 A	396	332	Neve	PolG	108	0	0	35	108	0	0	36
HE 240 A	396	332	Vento X	PolG	108	0	0	36	112	0	0	0
HE 240 A	396	332	Vento X	PolG	108	0	0	54	108	0	0	56
HE 240 A	396	332	Vento X	PolG	108	0	0	56	112	0	0	0
HE 240 A	396	332	Vento X	PolG	108	0	0	53	108	0	0	56
HE 240 A	396	332	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	56	112	0	0	0
HE 240 A	396	332	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	56	112	0	0	0
HE 240 A	396	332	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	123	0	0	60
HE 240 A	396	332	Peso Proprio	UnifG	0	0	0	52	4	0	0	101
HE 240 A	396	332	QP Solai	PolG	4	0	0	101	109	0	0	105
HE 240 A	396	332	QP Solai	PolG	109	0	0	105	123	0	0	53
HE 240 A	396	332	QP Solai	PolG	109	0	0	17	4	0	0	32
HE 240 A	396	332	QP Solai	PolG	4	0	0	32	109	0	0	34
HE 240 A	396	332	Neve	PolG	109	0	0	34	123	0	0	17
HE 240 A	396	332	Neve	PolG	4	0	0	1	4	0	0	32
HE 240 A	396	332	Neve	PolG	4	0	0	32	123	0	0	32
HE 240 A	396	332	Neve	PolG	109	0	0	31	109	0	0	34
HE 240 A	396	332	Vento X	PolG	109	0	0	34	123	0	0	1
HE 240 A	396	332	Vento X	PolG	4	0	0	49	123	0	0	49
HE 240 A	396	332	Vento X	PolG	4	0	0	48	109	0	0	52
HE 240 A	396	332	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	52	123	0	0	2
HE 240 A	396	332	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	113	0	0	60
HE 240 A	396	332	Peso Proprio	UnifG	0	0	0	55	4	0	0	106
HE 240 A	396	332	QP Solai	PolG	4	0	0	106	101	0	0	110
HE 240 A	396	332	QP Solai	PolG	101	0	0	110	113	0	0	55
HE 240 A	396	332	QP Solai	PolG	101	0	0	18	4	0	0	34
HE 240 A	396	332	QP Solai	PolG	4	0	0	34	101	0	0	35
HE 240 A	396	332	Neve	PolG	101	0	0	35	113	0	0	1
HE 240 A	396	332	Vento X	PolG	101	0	0	50	101	0	0	55
HE 240 A	396	332	Vento X	PolG	101	0	0	55	113	0	0	2
HE 240 A	396	332	Vento X	PolG	4	0	0	2	4	0	0	51
HE 240 A	396	332	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	51	113	0	0	51

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYL	QZi	Xf	QXf	QYf	QZf
HE 240 A	34	359	Carichi termici	Termico	0	0	0	60	182	0	0	60
HE 240 A	107	168	Peso Proprio	UnifG	0	0	0	38	3	0	0	73
HE 240 A	107	168	QP Solai	PolG	3	0	0	73	167	0	0	77
					167	0	0	77	182	0	0	39
HE 240 A	107	168	QV Solai	PolG	0	0	0	12	3	0	0	23
					3	0	0	23	167	0	0	25
HE 240 A	107	168	Neve	PolG	167	0	0	25	182	0	0	13
					167	0	0	22	167	0	0	25
HE 240 A	107	168	Neve	PolG	0	0	0	25	182	0	0	1
					167	0	0	1	3	0	0	23
HE 240 A	107	168	Vento X	PolG	0	0	0	34	167	0	0	38
					167	0	0	38	182	0	0	2
HE 240 A	107	168	Vento X	PolG	0	0	0	2	3	0	0	36
					3	0	0	36	182	0	0	36
HE 240 A	107	168	Carichi termici	Termico	0	0	0	60	178	0	0	60
HE 240 A	168	169	Peso Proprio	UnifG	0	0	0	40	4	0	0	77
HE 240 A	168	169	QP Solai	PolG	4	0	0	77	163	0	0	82
					163	0	0	82	178	0	0	42
HE 240 A	168	169	QV Solai	PolG	0	0	0	13	4	0	0	25
					4	0	0	25	163	0	0	26
HE 240 A	168	169	Neve	PolG	163	0	0	26	178	0	0	13
					163	0	0	24	163	0	0	26
HE 240 A	168	169	Neve	PolG	0	0	0	26	178	0	0	1
					163	0	0	1	4	0	0	24
HE 240 A	168	169	Vento X	PolG	4	0	0	36	163	0	0	41
					163	0	0	41	178	0	0	2
HE 240 A	168	169	Vento X	PolG	0	0	0	2	4	0	0	38
					4	0	0	38	178	0	0	38
HE 240 A	168	169	Carichi termici	Termico	0	0	0	60	178	0	0	60
HE 240 A	169	170	Peso Proprio	UnifG	0	0	0	43	4	0	0	82
HE 240 A	169	170	QP Solai	PolG	4	0	0	82	162	0	0	86
					162	0	0	86	178	0	0	44
HE 240 A	169	170	QV Solai	PolG	0	0	0	14	4	0	0	26
					4	0	0	26	162	0	0	28
HE 240 A	169	170	Neve	PolG	162	0	0	28	178	0	0	14
					162	0	0	1	4	0	0	26
HE 240 A	169	170	Neve	PolG	4	0	0	26	178	0	0	26
					162	0	0	25	162	0	0	28
HE 240 A	169	170	Vento X	PolG	0	0	0	28	178	0	0	1
					162	0	0	2	4	0	0	40
HE 240 A	169	170	Vento X	PolG	4	0	0	40	178	0	0	40
					162	0	0	39	162	0	0	43
HE 240 A	169	170	Vento X	PolG	0	0	0	43	178	0	0	2
HE 240 A	169	170	Carichi termici	Termico	0	0	0	60	151	0	0	60
HE 240 A	170	171	Peso Proprio	UnifG	0	0	0	45	4	0	0	87
HE 240 A	170	171	QP Solai	PolG	4	0	0	87	137	0	0	91
					137	0	0	91	151	0	0	46
HE 240 A	170	171	QV Solai	PolG	0	0	0	14	4	0	0	28
					4	0	0	28	137	0	0	29
HE 240 A	170	171	Neve	PolG	137	0	0	29	151	0	0	15
					137	0	0	1	4	0	0	27
HE 240 A	170	171	Neve	PolG	4	0	0	27	151	0	0	27
					137	0	0	29	151	0	0	29
HE 240 A	170	171	Vento X	PolG	0	0	0	2	4	0	0	42
					4	0	0	42	151	0	0	42
HE 240 A	170	171	Vento X	PolG	0	0	0	41	137	0	0	45
					137	0	0	45	151	0	0	2
HE 240 A	170	171	Carichi termici	Termico	0	0	0	60	148	0	0	60
HE 240 A	171	172	Peso Proprio	UnifG	0	0	0	60	148	0	0	104

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	171	172	QP Solai	PolG	0	0	0	48	4	0	0	92
					4	0	0	92	133	0	0	96
HE 240 A	171	172	QV Solai	PolG	133	0	0	96	148	0	0	49
					4	0	0	15	4	0	0	29
HE 240 A	171	172	Neve	PolG	4	0	0	29	133	0	0	31
					133	0	0	31	148	0	0	16
HE 240 A	171	172	Neve	PolG	0	0	0	1	4	0	0	29
					4	0	0	29	148	0	0	29
HE 240 A	171	172	Neve	PolG	0	0	0	28	133	0	0	31
					133	0	0	31	148	0	0	1
HE 240 A	171	172	Vento X	PolG	0	0	0	2	4	0	0	44
					4	0	0	44	148	0	0	44
HE 240 A	171	172	Vento X	PolG	0	0	0	43	133	0	0	48
					133	0	0	48	148	0	0	2
HE 240 A	171	172	Carichi termici	Termico	0	0	0	60	134	0	0	60
HE 240 A	172	33	Peso Proprio	UnifG	0	0	0	50	4	0	0	96
HE 240 A	172	33	QP Solai	PolG	0	0	0	96	121	0	0	100
					121	0	0	100	134	0	0	51
HE 240 A	172	33	QV Solai	PolG	0	0	0	16	4	0	0	31
					4	0	0	31	121	0	0	32
HE 240 A	172	33	Neve	PolG	121	0	0	32	134	0	0	16
					121	0	0	30	121	0	0	32
HE 240 A	172	33	Neve	PolG	0	0	0	32	134	0	0	1
					121	0	0	1	4	0	0	30
HE 240 A	172	33	Vento X	PolG	4	0	0	30	134	0	0	30
					4	0	0	46	121	0	0	50
HE 240 A	172	33	Vento X	PolG	121	0	0	50	134	0	0	2
					121	0	0	2	4	0	0	47
HE 240 A	172	33	Carichi termici	Termico	0	0	0	60	108	0	0	60
HE 240 A	359	360	Peso Proprio	UnifG	0	0	0	57	4	0	0	110
HE 240 A	359	360	QP Solai	PolG	0	0	0	110	96	0	0	114
					4	0	0	114	108	0	0	58
HE 240 A	359	360	QV Solai	PolG	96	0	0	18	4	0	0	35
					4	0	0	35	96	0	0	37
HE 240 A	359	360	Neve	PolG	96	0	0	37	108	0	0	19
					4	0	0	1	4	0	0	34
HE 240 A	359	360	Neve	PolG	4	0	0	34	108	0	0	34
					4	0	0	34	96	0	0	37
HE 240 A	359	360	Vento X	PolG	96	0	0	37	108	0	0	1
					96	0	0	2	4	0	0	53
HE 240 A	359	360	Vento X	PolG	4	0	0	53	108	0	0	53
					4	0	0	53	96	0	0	57
HE 240 A	359	360	Carichi termici	Termico	0	0	0	60	112	0	0	60
HE 240 A	360	333	Peso Proprio	UnifG	0	0	0	60	4	0	0	115
HE 240 A	360	333	QP Solai	PolG	0	0	0	115	99	0	0	119
					4	0	0	119	112	0	0	60
HE 240 A	360	333	QV Solai	PolG	99	0	0	19	4	0	0	37
					4	0	0	37	99	0	0	38
HE 240 A	360	333	Neve	PolG	99	0	0	38	112	0	0	19
					99	0	0	38	112	0	0	1
HE 240 A	360	333	Neve	PolG	0	0	0	1	4	0	0	36
					4	0	0	36	112	0	0	36
HE 240 A	360	333	Vento X	PolG	0	0	0	55	99	0	0	59
					99	0	0	59	112	0	0	2
HE 240 A	360	333	Vento X	PolG	0	0	0	2	4	0	0	55
					4	0	0	55	112	0	0	55
HE 240 A	360	333	Carichi termici	Termico	0	0	0	60	123	0	0	60
HE 240 A	39	40	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	39	40	QP Solai	PolG	0	0	0	54	13	0	0	104

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					13	0	0	104	102	0	0	107
					102	0	0	107	123	0	0	57
HE 240 A	39	40	QV Solai	PolG	0	0	0	17	13	0	0	33
					13	0	0	33	102	0	0	34
					102	0	0	34	123	0	0	18
HE 240 A	39	40	Neve	PolG	0	0	0	3	13	0	0	34
					13	0	0	34	123	0	0	32
HE 240 A	39	40	Neve	PolG	0	0	0	30	102	0	0	34
					102	0	0	34	123	0	0	3
HE 240 A	39	40	Vento X	PolG	0	0	0	5	13	0	0	52
					13	0	0	52	123	0	0	50
HE 240 A	39	40	Vento X	PolG	0	0	0	47	102	0	0	53
					102	0	0	53	123	0	0	5
HE 240 A	39	40	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	40	365	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	40	365	QP Solai	PolG	0	0	0	56	12	0	0	108
					12	0	0	108	93	0	0	112
					93	0	0	112	113	0	0	59
HE 240 A	40	365	QV Solai	PolG	0	0	0	18	12	0	0	35
					12	0	0	35	93	0	0	36
					93	0	0	36	113	0	0	19
HE 240 A	40	365	Neve	PolG	0	0	0	3	12	0	0	35
					12	0	0	35	113	0	0	34
HE 240 A	40	365	Neve	PolG	0	0	0	32	93	0	0	35
					93	0	0	35	113	0	0	3
HE 240 A	40	365	Vento X	PolG	0	0	0	49	93	0	0	55
					93	0	0	55	113	0	0	5
HE 240 A	40	365	Vento X	PolG	0	0	0	5	12	0	0	54
					12	0	0	54	113	0	0	52
HE 240 A	40	365	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	108	183	Peso Proprio	UnifG	0	0	0	40	13	0	0	60
HE 240 A	108	183	QP Solai	PolG	0	0	0	75	160	0	0	79
					13	0	0	79	182	0	0	42
HE 240 A	108	183	QV Solai	PolG	0	0	0	13	13	0	0	24
					13	0	0	24	160	0	0	25
					160	0	0	25	182	0	0	14
HE 240 A	108	183	Neve	PolG	0	0	0	3	13	0	0	25
					13	0	0	25	182	0	0	23
HE 240 A	108	183	Neve	PolG	0	0	0	22	160	0	0	26
					160	0	0	26	182	0	0	3
HE 240 A	108	183	Vento X	PolG	0	0	0	5	13	0	0	38
					13	0	0	38	182	0	0	36
HE 240 A	108	183	Vento X	PolG	0	0	0	34	160	0	0	40
					160	0	0	40	182	0	0	5
HE 240 A	108	183	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	183	184	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	183	184	QP Solai	PolG	0	0	0	42	14	0	0	80
					14	0	0	80	155	0	0	84
					155	0	0	84	178	0	0	45
HE 240 A	183	184	QV Solai	PolG	0	0	0	13	14	0	0	26
					14	0	0	26	155	0	0	27
					155	0	0	27	178	0	0	14
HE 240 A	183	184	Neve	PolG	0	0	0	3	14	0	0	26
					14	0	0	26	178	0	0	25
HE 240 A	183	184	Neve	PolG	0	0	0	23	155	0	0	27
					155	0	0	23	178	0	0	3
HE 240 A	183	184	Vento X	PolG	0	0	0	5	14	0	0	40
					14	0	0	40	178	0	0	38
HE 240 A	183	184	Vento X	PolG	0	0	0	36	155	0	0	42
					155	0	0	42	178	0	0	5
HE 240 A	183	184	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	184	185	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	184	185	QP Solai	PolG	0	0	0	44	15	0	0	85
					15	0	0	85	153	0	0	88

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	184	185		PolG	0	0	0	14	15	0	0	27
					15	0	0	27	153	0	0	28
HE 240 A	184	185	Neve	PolG	0	0	0	28	178	0	0	15
					153	0	0	25	153	0	0	28
HE 240 A	184	185	Neve	PolG	0	0	0	3	15	0	0	3
					15	0	0	28	178	0	0	28
HE 240 A	184	185	Vento X	PolG	0	0	0	5	15	0	0	43
					15	0	0	43	178	0	0	41
HE 240 A	184	185	Vento X	PolG	0	0	0	38	153	0	0	44
					153	0	0	44	178	0	0	5
HE 240 A	184	185	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	185	186	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	185	186	QP Solai	PolG	0	0	0	89	129	0	0	93
					13	0	0	89	129	0	0	50
HE 240 A	185	186	QV Solai	PolG	0	0	0	15	13	0	0	29
					13	0	0	29	129	0	0	30
HE 240 A	185	186	Neve	PolG	0	0	0	26	129	0	0	16
					129	0	0	30	151	0	0	30
HE 240 A	185	186	Neve	PolG	0	0	0	3	13	0	0	3
					13	0	0	29	151	0	0	29
HE 240 A	185	186	Vento X	PolG	0	0	0	5	13	0	0	45
					13	0	0	45	151	0	0	43
HE 240 A	185	186	Vento X	PolG	0	0	0	40	129	0	0	46
					129	0	0	46	151	0	0	5
HE 240 A	185	186	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	186	187	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	186	187	QP Solai	PolG	0	0	0	94	125	0	0	98
					14	0	0	94	125	0	0	52
HE 240 A	186	187	QV Solai	PolG	0	0	0	16	14	0	0	30
					14	0	0	30	125	0	0	31
HE 240 A	186	187	Neve	PolG	0	0	0	27	125	0	0	17
					125	0	0	31	148	0	0	31
HE 240 A	186	187	Neve	PolG	0	0	0	3	14	0	0	3
					14	0	0	31	148	0	0	29
HE 240 A	186	187	Vento X	PolG	0	0	0	5	14	0	0	47
					14	0	0	47	148	0	0	45
HE 240 A	186	187	Vento X	PolG	0	0	0	42	125	0	0	48
					125	0	0	48	148	0	0	5
HE 240 A	186	187	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	187	39	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	187	39	QP Solai	PolG	0	0	0	51	113	0	0	99
					13	0	0	99	113	0	0	102
					113	0	0	102	134	0	0	54
HE 240 A	187	39	QV Solai	PolG	0	0	0	16	13	0	0	32
					13	0	0	32	113	0	0	33
					113	0	0	33	134	0	0	17
HE 240 A	187	39	Neve	PolG	0	0	0	3	13	0	0	32
					13	0	0	32	134	0	0	31
HE 240 A	187	39	Neve	PolG	0	0	0	29	113	0	0	33
					113	0	0	33	134	0	0	3
HE 240 A	187	39	Vento X	PolG	0	0	0	5	13	0	0	50
					13	0	0	50	134	0	0	48
HE 240 A	187	39	Vento X	PolG	0	0	0	45	113	0	0	50
					113	0	0	50	134	0	0	5
HE 240 A	187	39	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	365	366	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
HE 240 A	365	366	QP Solai	PolG	0	0	0	58	12	0	0	113
					12	0	0	113	88	0	0	116
					88	0	0	116	108	0	0	62
HE 240 A	365	366	QV Solai	PolG	0	0	0	19	12	0	0	36
					12	0	0	36	88	0	0	37

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	365	366	Neve	PolG	88	0	0	37	108	0	0	20
	365	366		PolG	0	0	0	3	12	0	0	37
	365	366		PolG	12	0	0	37	108	0	0	35
HE 240 A	365	366	Neve	PolG	0	0	0	33	88	0	0	37
	365	366		PolG	88	0	0	37	108	0	0	3
	365	366		PolG	0	0	0	51	88	0	0	57
HE 240 A	365	366	Vento X	PolG	88	0	0	57	108	0	0	5
	365	366		PolG	0	0	0	5	12	0	0	57
	365	366		PolG	12	0	0	57	108	0	0	55
HE 240 A	365	366	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
	366	334		UnifG	0	0	0	60	112	0	0	60
	366	334		PolG	0	0	0	60	13	0	0	118
HE 240 A	366	334	QP Solai	PolG	13	0	0	118	90	0	0	121
	366	334		PolG	90	0	0	121	112	0	0	64
	366	334		PolG	0	0	0	19	13	0	0	38
HE 240 A	366	334	QV Solai	PolG	13	0	0	38	90	0	0	39
	366	334		PolG	90	0	0	39	112	0	0	21
	366	334		PolG	0	0	0	35	90	0	0	38
HE 240 A	366	334	Neve	PolG	90	0	0	38	112	0	0	3
	366	334		PolG	0	0	0	3	13	0	0	38
	366	334		PolG	13	0	0	38	112	0	0	37
HE 240 A	366	334	Vento X	PolG	0	0	0	54	90	0	0	59
	366	334		PolG	90	0	0	59	112	0	0	5
	366	334		PolG	0	0	0	5	13	0	0	59
HE 240 A	366	334	Vento X	PolG	13	0	0	59	112	0	0	57
	366	334		Termico	ΔXY=15°C, ΔXZ=15°C							
	366	334		Carichi termici								
Trave 8008	31	32	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
	31	32		PolG	0	0	0	57	20	0	0	105
	31	32		PolG	20	0	0	105	93	0	0	108
HE 240 A			QV Solai	PolG	93	0	0	108	123	0	0	57
				PolG	20	0	0	18	20	0	0	34
				PolG	93	0	0	34	93	0	0	35
HE 240 A	31	32	Neve	PolG	93	0	0	35	123	0	0	18
	31	32		PolG	20	0	0	4	20	0	0	34
	31	32		PolG	20	0	0	34	123	0	0	31
HE 240 A	31	32	Neve	PolG	0	0	0	31	93	0	0	35
	31	32		PolG	93	0	0	35	123	0	0	4
	31	32		PolG	0	0	0	48	93	0	0	55
HE 240 A			Vento X	PolG	93	0	0	55	123	0	0	7
				PolG	0	0	0	7	20	0	0	52
				PolG	20	0	0	52	123	0	0	48
HE 240 A	31	32	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
	32	357		UnifG	0	0	0	60	113	0	0	60
	32	357		PolG	0	0	0	59	19	0	0	110
HE 240 A			QP Solai	PolG	19	0	0	110	85	0	0	113
				PolG	85	0	0	113	113	0	0	60
				PolG	0	0	0	19	19	0	0	35
HE 240 A	32	357	QV Solai	PolG	19	0	0	35	85	0	0	36
				PolG	85	0	0	36	113	0	0	19
				PolG	0	0	0	32	85	0	0	37
HE 240 A	32	357	Neve	PolG	85	0	0	37	113	0	0	4
				PolG	0	0	0	4	19	0	0	35
				PolG	19	0	0	35	113	0	0	33
HE 240 A	32	357	Vento X	PolG	0	0	0	7	19	0	0	54
	32	357		PolG	19	0	0	54	113	0	0	51
	32	357		PolG	0	0	0	50	85	0	0	57
HE 240 A			Vento X	PolG	85	0	0	57	113	0	0	7
				Termico	ΔXY=15°C, ΔXZ=15°C							
				UnifG	0	0	0	60	182	0	0	60
HE 240 A	109	163	Peso Proprio	PolG	0	0	0	43	21	0	0	77
	109	163		PolG	21	0	0	77	149	0	0	81
				PolG	149	0	0	81	182	0	0	44
HE 240 A			QV Solai	PolG	0	0	0	14	21	0	0	25
				PolG	21	0	0	25	149	0	0	26
				PolG	149	0	0	26	182	0	0	14

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf	
HE 240 A	109	163	Neve	PolG	0	0	0	0	22	149	0	0	27
HE 240 A	109	163	Neve	PolG	149	0	0	0	27	182	0	0	4
HE 240 A	109	163	Neve	PolG	0	0	0	0	21	0	0	0	25
HE 240 A	109	163	Neve	PolG	21	0	0	0	25	182	0	0	23
HE 240 A	109	163	Vento X	PolG	0	0	0	0	34	149	0	0	42
HE 240 A	109	163	Vento X	PolG	149	0	0	0	42	182	0	0	7
HE 240 A	109	163	Vento X	PolG	0	0	0	0	7	21	0	0	39
HE 240 A	109	163	Vento X	PolG	21	0	0	0	39	182	0	0	35
HE 240 A	109	163	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	178	0	0	60
HE 240 A	163	164	Peso Proprio	UnifG	0	0	0	0	45	22	0	0	82
HE 240 A	163	164	QP Solai	PolG	22	0	0	0	82	144	0	0	85
HE 240 A	163	164	QP Solai	PolG	144	0	0	0	85	178	0	0	46
HE 240 A	163	164	QP Solai	PolG	0	0	0	0	14	22	0	0	26
HE 240 A	163	164	QP Solai	PolG	22	0	0	0	26	144	0	0	27
HE 240 A	163	164	QP Solai	PolG	144	0	0	0	27	178	0	0	15
HE 240 A	163	164	QP Solai	PolG	0	0	0	0	4	22	0	0	27
HE 240 A	163	164	QP Solai	PolG	22	0	0	0	23	144	0	0	24
HE 240 A	163	164	QP Solai	PolG	144	0	0	0	28	178	0	0	28
HE 240 A	163	164	QP Solai	PolG	0	0	0	0	7	22	0	0	4
HE 240 A	163	164	QP Solai	PolG	22	0	0	0	28	178	0	0	42
HE 240 A	163	164	QP Solai	PolG	0	0	0	0	42	178	0	0	37
HE 240 A	163	164	QP Solai	PolG	144	0	0	0	36	144	0	0	44
HE 240 A	163	164	QP Solai	PolG	0	0	0	0	44	178	0	0	7
HE 240 A	163	164	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	178	0	0	60
HE 240 A	164	165	Peso Proprio	UnifG	0	0	0	0	47	23	0	0	87
HE 240 A	164	165	QP Solai	PolG	23	0	0	0	87	142	0	0	90
HE 240 A	164	165	QP Solai	PolG	142	0	0	0	90	178	0	0	48
HE 240 A	164	165	QP Solai	PolG	0	0	0	0	15	23	0	0	28
HE 240 A	164	165	QP Solai	PolG	23	0	0	0	28	142	0	0	29
HE 240 A	164	165	QP Solai	PolG	142	0	0	0	29	178	0	0	16
HE 240 A	164	165	QP Solai	PolG	0	0	0	0	25	142	0	0	30
HE 240 A	164	165	QP Solai	PolG	142	0	0	0	30	178	0	0	4
HE 240 A	164	165	QP Solai	PolG	0	0	0	0	4	23	0	0	28
HE 240 A	164	165	QP Solai	PolG	23	0	0	0	28	178	0	0	26
HE 240 A	164	165	QP Solai	PolG	0	0	0	0	7	23	0	0	44
HE 240 A	164	165	QP Solai	PolG	23	0	0	0	44	178	0	0	40
HE 240 A	164	165	QP Solai	PolG	0	0	0	0	39	142	0	0	46
HE 240 A	164	165	QP Solai	PolG	142	0	0	0	46	178	0	0	7
HE 240 A	164	165	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	151	0	0	60
HE 240 A	165	166	Peso Proprio	UnifG	0	0	0	0	50	21	0	0	91
HE 240 A	165	166	QP Solai	PolG	21	0	0	0	91	119	0	0	95
HE 240 A	165	166	QP Solai	PolG	119	0	0	0	95	151	0	0	51
HE 240 A	165	166	QP Solai	PolG	0	0	0	0	16	21	0	0	29
HE 240 A	165	166	QP Solai	PolG	21	0	0	0	29	119	0	0	30
HE 240 A	165	166	QP Solai	PolG	119	0	0	0	30	151	0	0	16
HE 240 A	165	166	QP Solai	PolG	0	0	0	0	4	21	0	0	30
HE 240 A	165	166	QP Solai	PolG	21	0	0	0	30	151	0	0	27
HE 240 A	165	166	QP Solai	PolG	0	0	0	0	26	119	0	0	31
HE 240 A	165	166	QP Solai	PolG	119	0	0	0	31	151	0	0	4
HE 240 A	165	166	QP Solai	PolG	0	0	0	0	41	119	0	0	48
HE 240 A	165	166	QP Solai	PolG	119	0	0	0	48	151	0	0	7
HE 240 A	165	166	QP Solai	PolG	0	0	0	0	7	21	0	0	46
HE 240 A	165	166	QP Solai	PolG	21	0	0	0	46	151	0	0	42
HE 240 A	165	166	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	60	148	0	0	60
HE 240 A	166	167	Peso Proprio	UnifG	0	0	0	0	52	22	0	0	96
HE 240 A	166	167	QP Solai	PolG	22	0	0	0	96	115	0	0	99
HE 240 A	166	167	QP Solai	PolG	115	0	0	0	99	148	0	0	53
HE 240 A	166	167	QP Solai	PolG	0	0	0	0	17	22	0	0	31
HE 240 A	166	167	QP Solai	PolG	22	0	0	0	31	115	0	0	32
HE 240 A	166	167	QP Solai	PolG	115	0	0	0	32	148	0	0	17
HE 240 A	166	167	QP Solai	PolG	0	0	0	0	28	115	0	0	33
HE 240 A	166	167	QP Solai	PolG	115	0	0	0	33	148	0	0	4

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	166	167	Neve	PolG	0	0	0	4	22	0	0	31
HE 240 A	166	167	Vento X	PolG	22	0	0	31	148	0	0	28
HE 240 A	166	167	Vento X	PolG	0	0	0	43	115	0	0	50
HE 240 A	166	167	Vento X	PolG	115	0	0	50	148	0	0	7
HE 240 A	166	167	Vento X	PolG	0	0	0	7	22	0	0	48
HE 240 A	166	167	Carichi termici	Termico	22	0	0	48	148	0	0	44
HE 240 A	166	167	Peso Proprio	UnitG	AXY=15°C,AXZ=15°C	0	0	0	60	134	0	60
HE 240 A	167	31	QP Solai	PolG	0	0	0	54	21	0	0	101
HE 240 A	167	31	QP Solai	PolG	21	0	0	101	103	0	0	104
HE 240 A	167	31	QV Solai	PolG	103	0	0	104	134	0	0	55
HE 240 A	167	31	QV Solai	PolG	0	0	0	17	21	0	0	32
HE 240 A	167	31	QV Solai	PolG	21	0	0	32	103	0	0	33
HE 240 A	167	31	Neve	PolG	103	0	0	33	134	0	0	18
HE 240 A	167	31	Neve	PolG	0	0	0	4	21	0	0	32
HE 240 A	167	31	Neve	PolG	21	0	0	32	134	0	0	30
HE 240 A	167	31	Neve	PolG	0	0	0	29	103	0	0	34
HE 240 A	167	31	Vento X	PolG	103	0	0	34	134	0	0	4
HE 240 A	167	31	Vento X	PolG	0	0	0	45	103	0	0	52
HE 240 A	167	31	Vento X	PolG	103	0	0	52	134	0	0	7
HE 240 A	167	31	Vento X	PolG	0	0	0	7	21	0	0	50
HE 240 A	167	31	Vento X	PolG	21	0	0	50	134	0	0	46
HE 240 A	167	31	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	108	0	60
HE 240 A	357	358	Peso Proprio	UnitG	0	0	0	61	19	0	0	115
HE 240 A	357	358	QP Solai	PolG	19	0	0	115	80	0	0	117
HE 240 A	357	358	QP Solai	PolG	80	0	0	117	108	0	0	62
HE 240 A	357	358	QV Solai	PolG	0	0	0	20	19	0	0	37
HE 240 A	357	358	QV Solai	PolG	19	0	0	37	80	0	0	38
HE 240 A	357	358	QV Solai	PolG	80	0	0	38	108	0	0	20
HE 240 A	357	358	Neve	PolG	0	0	0	4	19	0	0	37
HE 240 A	357	358	Neve	PolG	19	0	0	37	108	0	0	34
HE 240 A	357	358	Neve	PolG	0	0	0	34	80	0	0	38
HE 240 A	357	358	Vento X	PolG	80	0	0	38	108	0	0	4
HE 240 A	357	358	Vento X	PolG	0	0	0	7	19	0	0	57
HE 240 A	357	358	Vento X	PolG	19	0	0	57	108	0	0	53
HE 240 A	357	358	Vento X	PolG	0	0	0	52	80	0	0	59
HE 240 A	357	358	Vento X	PolG	80	0	0	59	108	0	0	7
HE 240 A	357	358	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	112	0	60
HE 240 A	358	335	Peso Proprio	UnitG	0	0	0	64	21	0	0	120
HE 240 A	358	335	QP Solai	PolG	21	0	0	120	82	0	0	122
HE 240 A	358	335	QP Solai	PolG	82	0	0	122	112	0	0	64
HE 240 A	358	335	QV Solai	PolG	0	0	0	20	21	0	0	38
HE 240 A	358	335	QV Solai	PolG	21	0	0	38	82	0	0	39
HE 240 A	358	335	QV Solai	PolG	82	0	0	39	112	0	0	21
HE 240 A	358	335	Neve	PolG	0	0	0	35	82	0	0	40
HE 240 A	358	335	Neve	PolG	82	0	0	40	112	0	0	4
HE 240 A	358	335	Neve	PolG	0	0	0	4	21	0	0	38
HE 240 A	358	335	Vento X	PolG	21	0	0	38	112	0	0	35
HE 240 A	358	335	Vento X	PolG	0	0	0	55	82	0	0	61
HE 240 A	358	335	Vento X	PolG	82	0	0	61	112	0	0	7
HE 240 A	358	335	Vento X	PolG	0	0	0	7	21	0	0	59
HE 240 A	358	335	Vento X	PolG	21	0	0	59	112	0	0	55
HE 240 A	358	335	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	123	0	60
HE 240 A	37	38	Peso Proprio	UnitG	0	0	0	59	29	0	0	109
HE 240 A	37	38	QP Solai	PolG	29	0	0	109	85	0	0	111
HE 240 A	37	38	QP Solai	PolG	85	0	0	111	123	0	0	60
HE 240 A	37	38	QV Solai	PolG	0	0	0	19	29	0	0	35
HE 240 A	37	38	QV Solai	PolG	29	0	0	35	85	0	0	36
HE 240 A	37	38	QV Solai	PolG	85	0	0	36	123	0	0	19
HE 240 A	37	38	Neve	PolG	0	0	0	6	29	0	0	35
HE 240 A	37	38	Neve	PolG	29	0	0	35	123	0	0	32
HE 240 A	37	38	Vento X	PolG	0	0	0	31	85	0	0	36

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	37	38	Vento X	PolG	85	0	0	36	123	0	0	6
					PolG	0	0	48	85	0	0	56
					PolG	85	0	0	56	123	0	9
HE 240 A	37	38	Vento X	PolG	0	0	0	9	29	0	0	54
HE 240 A					29	0	0	54	123	0	0	49
HE 240 A	37	38	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	38	363	Peso Proprio	UnitG	0	0	0	60	113	0	0	60
HE 240 A	38	363	QP Solai	PolG	0	0	0	62	28	0	0	114
					28	0	0	114	77	0	0	116
HE 240 A					77	0	0	116	113	0	0	63
HE 240 A	38	363	QV Solai	PolG	0	0	0	20	28	0	0	36
					28	0	0	36	77	0	0	37
					77	0	0	37	113	0	0	20
HE 240 A	38	363	Neve	PolG	0	0	0	6	28	0	0	36
					28	0	0	36	113	0	0	33
HE 240 A	38	363	Neve	PolG	0	0	0	32	77	0	0	37
					77	0	0	37	113	0	0	6
HE 240 A	38	363	Vento X	PolG	0	0	0	50	77	0	0	58
					77	0	0	58	113	0	0	9
HE 240 A	38	363	Vento X	PolG	0	0	0	9	28	0	0	56
					28	0	0	9	28	0	0	51
HE 240 A	38	363	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	110	178	Peso Proprio	UnitG	0	0	0	60	182	0	0	60
HE 240 A	110	178	QP Solai	PolG	0	0	0	45	31	0	0	80
					31	0	0	80	141	0	0	83
HE 240 A					141	0	0	83	182	0	0	47
HE 240 A	110	178	QV Solai	PolG	0	0	0	14	31	0	0	26
					31	0	0	26	141	0	0	27
HE 240 A					141	0	0	27	182	0	0	15
HE 240 A	110	178	Neve	PolG	0	0	0	22	141	0	0	28
					141	0	0	28	182	0	0	6
HE 240 A	110	178	Neve	PolG	0	0	0	6	31	0	0	27
					31	0	0	27	182	0	0	23
HE 240 A	110	178	Vento X	PolG	0	0	0	34	141	0	0	43
					141	0	0	43	182	0	0	9
HE 240 A	110	178	Vento X	PolG	0	0	0	9	31	0	0	41
					31	0	0	9	31	0	0	41
HE 240 A	110	178	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	178	179	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	178	179	QP Solai	PolG	0	0	0	47	32	0	0	85
					32	0	0	85	135	0	0	88
HE 240 A					135	0	0	88	178	0	0	49
HE 240 A	178	179	QV Solai	PolG	0	0	0	15	32	0	0	27
					32	0	0	27	135	0	0	28
HE 240 A					135	0	0	28	178	0	0	16
HE 240 A	178	179	Neve	PolG	0	0	0	24	135	0	0	29
					135	0	0	29	178	0	0	6
HE 240 A	178	179	Neve	PolG	0	0	0	6	32	0	0	28
					32	0	0	28	178	0	0	24
HE 240 A	178	179	Vento X	PolG	0	0	0	36	135	0	0	45
					135	0	0	45	178	0	0	9
HE 240 A	178	179	Vento X	PolG	0	0	0	9	32	0	0	43
					32	0	0	9	32	0	0	43
HE 240 A	178	179	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	179	180	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	179	180	QP Solai	PolG	0	0	0	50	34	0	0	90
					34	0	0	90	133	0	0	93
HE 240 A					133	0	0	93	178	0	0	51
HE 240 A	179	180	QV Solai	PolG	0	0	0	16	34	0	0	29
					34	0	0	29	133	0	0	30
HE 240 A					133	0	0	30	178	0	0	16
HE 240 A	179	180	Neve	PolG	0	0	0	25	133	0	0	31
					133	0	0	31	178	0	0	6
HE 240 A	179	180	Neve	PolG	0	0	0	6	34	0	0	29
					34	0	0	29	178	0	0	26
HE 240 A	179	180	Vento X	PolG	0	0	0	39	133	0	0	47

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	179	180	Vento X	PolG	133	0	0	0	47	178	0	9
HE 240 A	179	180	Carichi termici	Termico	34	0	0	0	9	34	0	46
HE 240 A	180	181	Peso Proprio	UnifG	AXY=15°C, AXZ=15°C							
HE 240 A	180	181	QV Solai	PolG	0	0	0	0	60	151	0	60
					31	0	0	0	52	31	0	95
					111	0	0	0	95	111	0	97
HE 240 A	180	181	QV Solai	PolG	0	0	0	0	17	31	0	30
					31	0	0	0	30	111	0	31
					111	0	0	0	31	151	0	17
HE 240 A	180	181	Neve	PolG	0	0	0	0	26	111	0	32
					111	0	0	0	32	151	0	6
HE 240 A	180	181	Neve	PolG	0	0	0	0	6	31	0	31
					31	0	0	0	31	151	0	27
HE 240 A	180	181	Vento X	PolG	0	0	0	0	9	31	0	48
					31	0	0	0	48	151	0	42
HE 240 A	180	181	Vento X	PolG	0	0	0	0	41	111	0	49
					111	0	0	0	49	151	0	9
HE 240 A	180	181	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	181	182	Peso Proprio	UnifG	0	0	0	0	60	148	0	60
HE 240 A	181	182	QV Solai	PolG	0	0	0	0	55	31	0	99
					31	0	0	0	99	106	0	102
HE 240 A	181	182	QV Solai	PolG	106	0	0	0	102	148	0	56
					31	0	0	0	17	31	0	32
					106	0	0	0	32	106	0	33
HE 240 A	181	182	Neve	PolG	0	0	0	0	33	148	0	18
					106	0	0	0	28	106	0	33
HE 240 A	181	182	Neve	PolG	0	0	0	0	33	148	0	6
					31	0	0	0	6	31	0	32
HE 240 A	181	182	Vento X	PolG	0	0	0	0	32	148	0	29
					31	0	0	0	9	31	0	50
HE 240 A	181	182	Vento X	PolG	0	0	0	0	50	148	0	44
					106	0	0	0	43	106	0	52
HE 240 A	181	182	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	182	37	Peso Proprio	UnifG	0	0	0	0	60	134	0	60
HE 240 A	182	37	QV Solai	PolG	0	0	0	0	57	30	0	104
					30	0	0	0	104	95	0	106
HE 240 A	182	37	QV Solai	PolG	95	0	0	0	106	134	0	58
					30	0	0	0	18	30	0	33
					95	0	0	0	33	95	0	34
HE 240 A	182	37	Neve	PolG	0	0	0	0	34	134	0	19
					30	0	0	0	6	30	0	34
HE 240 A	182	37	Neve	PolG	0	0	0	0	34	134	0	30
					95	0	0	0	29	95	0	35
HE 240 A	182	37	Vento X	PolG	0	0	0	0	35	134	0	6
					95	0	0	0	46	95	0	54
HE 240 A	182	37	Vento X	PolG	0	0	0	0	54	134	0	9
					30	0	0	0	9	30	0	52
HE 240 A	182	37	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	363	364	Peso Proprio	UnifG	0	0	0	0	60	108	0	60
HE 240 A	363	364	QV Solai	PolG	0	0	0	0	64	28	0	118
					28	0	0	0	118	72	0	120
HE 240 A	363	364	QV Solai	PolG	72	0	0	0	120	108	0	65
					28	0	0	0	21	28	0	38
HE 240 A	363	364	QV Solai	PolG	0	0	0	0	38	72	0	39
					72	0	0	0	6	28	0	21
HE 240 A	363	364	Neve	PolG	0	0	0	0	38	108	0	38
					28	0	0	0	38	108	0	34
HE 240 A	363	364	Neve	PolG	0	0	0	0	34	72	0	39
					72	0	0	0	39	108	0	6
HE 240 A	363	364	Vento X	PolG	0	0	0	0	9	28	0	59
					28	0	0	0	59	108	0	53
HE 240 A	363	364	Vento X	PolG	0	0	0	0	52	72	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	363	364	Carichi termici	Termico	72	0	0	0	60	108	0	9
HE 240 A	364	336	Peso Proprio	UnifG	AXY=15°C, AXZ=15°C							
HE 240 A	364	336	QV Solai	PolG	0	0	0	0	60	112	0	60
					30	0	0	0	123	73	0	125
HE 240 A	364	336	QV Solai	PolG	73	0	0	0	125	112	0	67
					30	0	0	0	21	30	0	39
HE 240 A	364	336	Neve	PolG	73	0	0	0	39	73	0	40
					30	0	0	0	6	30	0	22
HE 240 A	364	336	Neve	PolG	30	0	0	0	39	112	0	36
					73	0	0	0	35	73	0	40
HE 240 A	364	336	Vento X	PolG	73	0	0	0	55	73	0	62
					73	0	0	0	62	112	0	9
HE 240 A	364	336	Vento X	PolG	0	0	0	0	9	30	0	61
HE 240 A	364	336	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	364	336	Peso Proprio	UnifG	0	0	0	0	60	123	0	60
HE 240 A	27	28	QV Solai	PolG	37	0	0	0	111	76	0	113
					76	0	0	0	113	123	0	63
HE 240 A	27	28	QV Solai	PolG	0	0	0	0	20	37	0	36
					37	0	0	0	36	76	0	36
HE 240 A	27	28	Neve	PolG	76	0	0	0	36	123	0	20
					0	0	0	0	7	37	0	36
HE 240 A	27	28	Neve	PolG	37	0	0	0	36	123	0	31
					76	0	0	0	31	76	0	36
HE 240 A	27	28	Vento X	PolG	76	0	0	0	48	76	0	56
					76	0	0	0	56	123	0	12
HE 240 A	27	28	Vento X	PolG	0	0	0	0	12	37	0	55
					37	0	0	0	55	123	0	49
HE 240 A	27	28	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	28	353	Peso Proprio	UnifG	0	0	0	0	60	113	0	60
HE 240 A	28	353	QV Solai	PolG	0	0	0	0	64	35	0	116
					35	0	0	0	116	68	0	118
HE 240 A	28	353	QV Solai	PolG	68	0	0	0	118	113	0	65
					35	0	0	0	21	35	0	37
					68	0	0	0	37	68	0	38
HE 240 A	28	353	Neve	PolG	0	0	0	0	38	113	0	21
					68	0	0	0	32	68	0	38
HE 240 A	28	353	Neve	PolG	68	0	0	0	38	113	0	8
					0	0	0	0	7	35	0	37
HE 240 A	28	353	Vento X	PolG	35	0	0	0	37	113	0	33
					68	0	0	0	50	68	0	58
HE 240 A	28	353	Vento X	PolG	68	0	0	0	58	113	0	12
					35	0	0	0	12	35	0	57
HE 240 A	28	353	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	111	153	Peso Proprio	UnifG	0	0	0	0	60	182	0	60
HE 240 A	111	153	QV Solai	PolG	0	0	0	0	47	39	0	83
					39	0	0	0	83	131	0	85
HE 240 A	111	153	QV Solai	PolG	131	0	0	0	85	182	0	49
					39	0	0	0	15	39	0	27
HE 240 A	111	153	Neve	PolG	131	0	0	0	27	131	0	27
					0	0	0	0	22	131	0	16
HE 240 A	111	153	Neve	PolG	131	0	0	0	29	182	0	29
					0	0	0	0	7	39	0	28
HE 240 A	111	153	Vento X	PolG	39	0	0	0	28	182	0	23
					39	0	0	0	12	39	0	43
HE 240 A	111	153	Vento X	PolG	39	0	0	0	43	182	0	35
					131	0	0	0	44	182	0	12

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYL	QZi	Xf	QXf	QYf	QZf
HE 240 A	153	153	Carichi termici	Termico	0	0	0	60	178	0	0	60
HE 240 A	153	154	Peso Proprio	UnifG	0	0	0	50	40	0	0	88
HE 240 A	153	154	QP Solai	PolG	40	0	0	88	125	0	0	90
					125	0	0	90	178	0	0	51
HE 240 A	153	154	QV Solai	PolG	0	0	0	16	40	0	0	28
					40	0	0	28	125	0	0	29
HE 240 A	153	154	Neve	PolG	125	0	0	29	178	0	0	16
					40	0	0	29	178	0	0	24
HE 240 A	153	154	Neve	PolG	0	0	0	23	125	0	0	30
HE 240 A	153	154	Vento X	PolG	125	0	0	30	178	0	0	8
HE 240 A	153	154	Vento X	PolG	0	0	0	36	125	0	0	46
HE 240 A	153	154	Vento X	PolG	125	0	0	46	178	0	0	12
					40	0	0	12	40	0	0	45
HE 240 A	153	154	Carichi termici	Termico	40	0	0	45	178	0	0	38
HE 240 A	154	155	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	154	155	QP Solai	PolG	0	0	0	52	43	0	0	92
					43	0	0	92	122	0	0	95
HE 240 A	154	155	QV Solai	PolG	122	0	0	95	178	0	0	54
					43	0	0	17	43	0	0	30
HE 240 A	154	155	Neve	PolG	122	0	0	30	122	0	0	30
HE 240 A	154	155	Neve	PolG	0	0	0	30	178	0	0	17
HE 240 A	154	155	Vento X	PolG	0	0	0	25	122	0	0	31
HE 240 A	154	155	Vento X	PolG	122	0	0	31	178	0	0	8
HE 240 A	154	155	Neve	PolG	0	0	0	7	43	0	0	30
HE 240 A	154	155	Vento X	PolG	43	0	0	30	178	0	0	26
HE 240 A	154	155	Vento X	PolG	0	0	0	12	43	0	0	47
HE 240 A	154	155	Vento X	PolG	43	0	0	47	178	0	0	40
HE 240 A	154	155	Vento X	PolG	0	0	0	39	122	0	0	48
HE 240 A	154	155	Carichi termici	Termico	122	0	0	48	178	0	0	12
HE 240 A	155	156	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	155	156	QP Solai	PolG	0	0	0	54	39	0	0	97
					39	0	0	97	101	0	0	99
HE 240 A	155	156	QV Solai	PolG	101	0	0	99	151	0	0	56
					39	0	0	31	101	0	0	31
HE 240 A	155	156	Neve	PolG	101	0	0	32	151	0	0	32
HE 240 A	155	156	Neve	PolG	0	0	0	26	101	0	0	33
HE 240 A	155	156	Vento X	PolG	101	0	0	33	151	0	0	8
HE 240 A	155	156	Vento X	PolG	0	0	0	7	39	0	0	32
HE 240 A	155	156	Vento X	PolG	39	0	0	32	151	0	0	27
HE 240 A	155	156	Vento X	PolG	0	0	0	12	39	0	0	49
HE 240 A	155	156	Vento X	PolG	39	0	0	49	151	0	0	42
HE 240 A	155	156	Vento X	PolG	0	0	0	41	101	0	0	50
HE 240 A	155	156	Carichi termici	Termico	101	0	0	50	151	0	0	12
HE 240 A	156	157	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	156	157	QP Solai	PolG	0	0	0	57	40	0	0	102
					40	0	0	102	97	0	0	104
HE 240 A	156	157	QV Solai	PolG	97	0	0	104	148	0	0	58
					40	0	0	18	40	0	0	33
HE 240 A	156	157	Neve	PolG	97	0	0	33	148	0	0	19
HE 240 A	156	157	Neve	PolG	0	0	0	28	97	0	0	34
HE 240 A	156	157	Neve	PolG	97	0	0	34	148	0	0	8
HE 240 A	156	157	Vento X	PolG	0	0	0	7	40	0	0	33
HE 240 A	156	157	Vento X	PolG	40	0	0	33	148	0	0	29
HE 240 A	156	157	Vento X	PolG	0	0	0	43	97	0	0	52
HE 240 A	156	157	Vento X	PolG	97	0	0	52	148	0	0	12
HE 240 A	156	157	Vento X	PolG	0	0	0	12	40	0	0	51
HE 240 A	156	157	Carichi termici	Termico	40	0	0	51	148	0	0	44
HE 240 A	157	27	Peso Proprio	UnifG	0	0	0	60	134	0	0	60

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	157	27	QP Solai	PolG	0	0	0	59	38	0	0	107
					38	0	0	107	85	0	0	108
HE 240 A	157	27	QV Solai	PolG	0	0	0	108	134	0	0	61
					38	0	0	19	38	0	0	34
HE 240 A	157	27	Neve	PolG	85	0	0	34	85	0	0	35
					85	0	0	35	134	0	0	19
HE 240 A	157	27	Neve	PolG	0	0	0	7	38	0	0	34
HE 240 A	157	27	Neve	PolG	38	0	0	34	134	0	0	30
HE 240 A	157	27	Vento X	PolG	85	0	0	35	134	0	0	8
HE 240 A	157	27	Vento X	PolG	0	0	0	45	85	0	0	54
HE 240 A	157	27	Vento X	PolG	85	0	0	54	134	0	0	12
HE 240 A	157	27	Vento X	PolG	0	0	0	12	38	0	0	53
HE 240 A	157	27	Carichi termici	Termico	38	0	0	53	134	0	0	46
HE 240 A	353	354	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
HE 240 A	353	354	QP Solai	PolG	0	0	0	66	35	0	0	121
					35	0	0	121	63	0	0	122
HE 240 A	353	354	QV Solai	PolG	63	0	0	122	108	0	0	67
					35	0	0	21	35	0	0	39
HE 240 A	353	354	Neve	PolG	63	0	0	39	63	0	0	39
					63	0	0	39	108	0	0	22
HE 240 A	353	354	Neve	PolG	0	0	0	34	63	0	0	39
HE 240 A	353	354	Neve	PolG	63	0	0	39	108	0	0	8
HE 240 A	353	354	Vento X	PolG	35	0	0	38	108	0	0	34
HE 240 A	353	354	Vento X	PolG	0	0	0	52	63	0	0	60
HE 240 A	353	354	Vento X	PolG	63	0	0	60	108	0	0	12
HE 240 A	353	354	Vento X	PolG	0	0	0	12	35	0	0	59
HE 240 A	353	354	Carichi termici	Termico	35	0	0	59	108	0	0	53
HE 240 A	354	337	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
HE 240 A	354	337	QP Solai	PolG	0	0	0	69	38	0	0	126
					38	0	0	126	64	0	0	127
HE 240 A	354	337	QV Solai	PolG	64	0	0	127	112	0	0	70
					38	0	0	22	38	0	0	40
HE 240 A	354	337	Neve	PolG	64	0	0	40	64	0	0	41
					64	0	0	41	112	0	0	22
HE 240 A	354	337	Neve	PolG	0	0	0	7	38	0	0	40
HE 240 A	354	337	Neve	PolG	38	0	0	40	112	0	0	36
HE 240 A	354	337	Vento X	PolG	64	0	0	35	64	0	0	40
HE 240 A	354	337	Vento X	PolG	0	0	0	12	38	0	0	61
HE 240 A	354	337	Vento X	PolG	38	0	0	61	112	0	0	55
HE 240 A	354	337	Vento X	PolG	0	0	0	55	64	0	0	62
HE 240 A	354	337	Carichi termici	Termico	64	0	0	62	112	0	0	12
Trave 8011												
HE 240 A	41	42	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	41	42	QP Solai	PolG	0	0	0	64	45	0	0	114
					45	0	0	114	66	0	0	115
HE 240 A	41	42	QV Solai	PolG	66	0	0	115	123	0	0	65
					45	0	0	21	45	0	0	37
HE 240 A	41	42	Neve	PolG	66	0	0	37	123	0	0	21
HE 240 A	41	42	Neve	PolG	0	0	0	9	45	0	0	36
HE 240 A	41	42	Neve	PolG	45	0	0	36	123	0	0	31
HE 240 A	41	42	Vento X	PolG	66	0	0	37	123	0	0	9
HE 240 A	41	42	Vento X	PolG	0	0	0	14	45	0	0	56
HE 240 A	41	42	Vento X	PolG	45	0	0	56	123	0	0	48
HE 240 A	41	42	Vento X	PolG	0	0	0	48	66	0	0	57
HE 240 A	41	42	Carichi termici	Termico	66	0	0	57	123	0	0	14
HE 240 A	42	367	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	42	367	QP Solai	PolG	0	0	0	67	44	0	0	119

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					44	0	0	119	59	0	0	120
					59	0	0	120	113	0	0	67
HE 240 A	42	367	QV Solai	PolG	0	0	0	21	44	0	0	38
					44	0	0	38	59	0	0	38
					59	0	0	38	113	0	0	22
HE 240 A	42	367	Neve	PolG	0	0	0	9	44	0	0	37
					44	0	0	37	113	0	0	33
HE 240 A	42	367	Neve	PolG	0	0	0	33	59	0	0	38
					59	0	0	38	113	0	0	9
HE 240 A	42	367	Vento X	PolG	0	0	0	14	44	0	0	58
					44	0	0	58	113	0	0	50
HE 240 A	42	367	Vento X	PolG	0	0	0	50	59	0	0	59
					59	0	0	59	113	0	0	14
HE 240 A	42	367	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	112	188	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	112	188	QP Solai	PolG	0	0	0	50	48	0	0	85
					48	0	0	85	121	0	0	87
					121	0	0	87	182	0	0	51
HE 240 A	112	188	QV Solai	PolG	0	0	0	16	48	0	0	27
					48	0	0	27	121	0	0	28
					121	0	0	28	182	0	0	16
HE 240 A	112	188	Neve	PolG	0	0	0	22	121	0	0	29
					121	0	0	29	182	0	0	9
HE 240 A	112	188	Neve	PolG	0	0	0	9	48	0	0	23
					48	0	0	28	182	0	0	23
HE 240 A	112	188	Vento X	PolG	0	0	0	14	48	0	0	44
					48	0	0	44	182	0	0	35
HE 240 A	112	188	Vento X	PolG	0	0	0	34	121	0	0	45
					121	0	0	45	182	0	0	14
HE 240 A	112	188	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	188	189	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	188	189	QP Solai	PolG	0	0	0	52	50	0	0	90
					50	0	0	90	115	0	0	92
					115	0	0	92	178	0	0	54
HE 240 A	188	189	QV Solai	PolG	0	0	0	17	50	0	0	29
					50	0	0	29	115	0	0	30
					115	0	0	30	178	0	0	17
HE 240 A	188	189	Neve	PolG	0	0	0	9	50	0	0	30
					50	0	0	30	178	0	0	24
HE 240 A	188	189	Neve	PolG	0	0	0	24	115	0	0	30
					115	0	0	30	178	0	0	9
HE 240 A	188	189	Vento X	PolG	0	0	0	14	50	0	0	46
					50	0	0	46	178	0	0	37
HE 240 A	188	189	Vento X	PolG	0	0	0	36	115	0	0	47
					115	0	0	47	178	0	0	14
HE 240 A	188	189	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	189	190	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	189	190	QP Solai	PolG	0	0	0	55	53	0	0	95
					53	0	0	95	111	0	0	97
					111	0	0	97	178	0	0	56
HE 240 A	189	190	QV Solai	PolG	0	0	0	18	53	0	0	30
					53	0	0	30	111	0	0	31
					111	0	0	31	178	0	0	18
HE 240 A	189	190	Neve	PolG	0	0	0	9	53	0	0	31
					53	0	0	31	178	0	0	26
HE 240 A	189	190	Neve	PolG	0	0	0	25	111	0	0	32
					111	0	0	32	178	0	0	9
HE 240 A	189	190	Vento X	PolG	0	0	0	39	111	0	0	49
					111	0	0	49	178	0	0	14
HE 240 A	189	190	Vento X	PolG	0	0	0	14	53	0	0	48
					53	0	0	48	178	0	0	39
HE 240 A	189	190	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	190	191	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	190	191	QP Solai	PolG	0	0	0	57	48	0	0	100
					48	0	0	100	91	0	0	101
HE 240 A					91	0	0	101	151	0	0	58

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	190	191	QV Solai	PolG	0	0	0	18	48	0	0	32
					48	0	0	32	91	0	0	32
HE 240 A	190	191	Neve	PolG	0	0	0	32	151	0	0	19
					91	0	0	27	91	0	0	33
HE 240 A	190	191	Neve	PolG	0	0	0	33	151	0	0	9
					91	0	0	9	48	0	0	32
HE 240 A	190	191	Vento X	PolG	0	0	0	32	151	0	0	27
					91	0	0	41	91	0	0	51
HE 240 A	190	191	Vento X	PolG	0	0	0	14	48	0	0	50
					48	0	0	50	151	0	0	42
HE 240 A	190	191	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	191	192	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	191	192	QP Solai	PolG	0	0	0	60	50	0	0	105
					50	0	0	105	86	0	0	106
					86	0	0	106	148	0	0	60
HE 240 A	191	192	QV Solai	PolG	0	0	0	19	50	0	0	34
					50	0	0	34	86	0	0	34
HE 240 A	191	192	Neve	PolG	0	0	0	28	86	0	0	34
					86	0	0	34	148	0	0	9
HE 240 A	191	192	Neve	PolG	0	0	0	9	50	0	0	33
					50	0	0	33	148	0	0	28
HE 240 A	191	192	Vento X	PolG	0	0	0	43	86	0	0	53
					86	0	0	53	148	0	0	14
HE 240 A	191	192	Vento X	PolG	0	0	0	14	50	0	0	52
					50	0	0	52	148	0	0	44
HE 240 A	191	192	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	192	41	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	192	41	QP Solai	PolG	0	0	0	62	47	0	0	109
					47	0	0	109	76	0	0	110
					76	0	0	110	134	0	0	63
HE 240 A	192	41	QV Solai	PolG	0	0	0	20	47	0	0	35
					47	0	0	35	76	0	0	35
HE 240 A	192	41	Neve	PolG	0	0	0	30	76	0	0	36
					76	0	0	36	134	0	0	9
HE 240 A	192	41	Neve	PolG	0	0	0	9	47	0	0	35
					47	0	0	35	134	0	0	30
HE 240 A	192	41	Vento X	PolG	0	0	0	14	47	0	0	54
					47	0	0	54	134	0	0	46
HE 240 A	192	41	Vento X	PolG	0	0	0	46	76	0	0	55
					76	0	0	55	134	0	0	14
HE 240 A	192	41	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	367	368	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
HE 240 A	367	368	QP Solai	PolG	0	0	0	69	44	0	0	124
					44	0	0	124	54	0	0	124
					54	0	0	124	108	0	0	70
HE 240 A	367	368	QV Solai	PolG	0	0	0	22	44	0	0	40
					44	0	0	40	54	0	0	40
					54	0	0	40	108	0	0	22
HE 240 A	367	368	Neve	PolG	0	0	0	34	54	0	0	39
					54	0	0	39	108	0	0	9
HE 240 A	367	368	Neve	PolG	0	0	0	9	44	0	0	39
					44	0	0	39	108	0	0	34
HE 240 A	367	368	Vento X	PolG	0	0	0	53	54	0	0	61
					54	0	0	61	108	0	0	14
HE 240 A	367	368	Vento X	PolG	0	0	0	14	44	0	0	60
					44	0	0	60	108	0	0	53
HE 240 A	367	368	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	368	338	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
HE 240 A	368	338	QP Solai	PolG	0	0	0	72	48	0	0	129
					48	0	0	129	54	0	0	129
					54	0	0	129	112	0	0	72
HE 240 A	368	338	QV Solai	PolG	0	0	0	23	48	0	0	41
					48	0	0	41	54	0	0	41

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	368	338	Neve	PolG	54	0	0	41	112	0	0	23
HE 240 A					0	0	0	9	48	0	0	40
HE 240 A	368	338	Neve	PolG	48	0	0	40	112	0	0	35
HE 240 A					0	0	0	36	54	0	0	41
HE 240 A	368	338	Vento X	PolG	54	0	0	41	112	0	0	9
HE 240 A					0	0	0	55	54	0	0	63
HE 240 A	368	338	Vento X	PolG	54	0	0	63	112	0	0	14
HE 240 A					0	0	0	14	48	0	0	62
HE 240 A	368	338	Carichi termici	Termico	48	0	0	62	112	0	0	55
Trave 8012 AXY=15°C, AXZ=15°C												
HE 240 A	43	44	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	43	44	QP Solai	PolG	55	0	0	67	55	0	0	117
HE 240 A					57	0	0	117	123	0	0	68
HE 240 A	43	44	QV Solai	PolG	0	0	0	22	55	0	0	38
HE 240 A					55	0	0	38	57	0	0	38
HE 240 A	43	44	Neve	PolG	57	0	0	38	123	0	0	22
HE 240 A					0	0	0	31	57	0	0	37
HE 240 A	43	44	Neve	PolG	57	0	0	37	123	0	0	11
HE 240 A					0	0	0	11	55	0	0	36
HE 240 A	43	44	Vento X	PolG	55	0	0	36	123	0	0	31
HE 240 A					0	0	0	48	57	0	0	57
HE 240 A	43	44	Vento X	PolG	57	0	0	57	123	0	0	17
HE 240 A					0	0	0	17	55	0	0	56
HE 240 A	43	44	Vento X	PolG	55	0	0	56	123	0	0	48
Trave 8013 AXY=15°C, AXZ=15°C												
HE 240 A	43	44	Carichi termici	Termico	55	0	0	60	113	0	0	60
HE 240 A	44	369	Peso Proprio	UnifG	0	0	0	70	50	0	0	119
HE 240 A	44	369	QP Solai	PolG	50	0	0	119	53	0	0	119
HE 240 A					53	0	0	119	113	0	0	70
HE 240 A	44	369	QV Solai	PolG	0	0	0	22	50	0	0	38
HE 240 A					50	0	0	38	53	0	0	38
HE 240 A	44	369	Neve	PolG	53	0	0	38	113	0	0	22
HE 240 A					53	0	0	33	50	0	0	33
HE 240 A	44	369	Neve	PolG	50	0	0	38	113	0	0	11
HE 240 A					0	0	0	17	53	0	0	58
HE 240 A	44	369	Vento X	PolG	53	0	0	58	113	0	0	50
HE 240 A					0	0	0	50	50	0	0	59
HE 240 A	44	369	Vento X	PolG	50	0	0	59	113	0	0	17
Trave 8014 AXY=15°C, AXZ=15°C												
HE 240 A	44	369	Carichi termici	Termico	50	0	0	60	182	0	0	60
HE 240 A	113	193	Peso Proprio	UnifG	0	0	0	53	58	0	0	89
HE 240 A	113	193	QP Solai	PolG	58	0	0	89	112	0	0	90
HE 240 A					112	0	0	90	182	0	0	54
HE 240 A	113	193	QV Solai	PolG	0	0	0	17	58	0	0	28
HE 240 A					58	0	0	28	112	0	0	29
HE 240 A	113	193	Neve	PolG	112	0	0	29	182	0	0	17
HE 240 A					0	0	0	11	58	0	0	29
HE 240 A	113	193	Neve	PolG	58	0	0	29	182	0	0	23
HE 240 A					112	0	0	22	112	0	0	30
HE 240 A	113	193	Vento X	PolG	0	0	0	34	112	0	0	46
HE 240 A					112	0	0	46	182	0	0	17
HE 240 A	113	193	Vento X	PolG	0	0	0	17	58	0	0	45
HE 240 A					58	0	0	45	182	0	0	35
Trave 8015 AXY=15°C, AXZ=15°C												
HE 240 A	113	193	Carichi termici	Termico	0	0	0	60	178	0	0	60
HE 240 A	193	194	Peso Proprio	UnifG	0	0	0	55	61	0	0	93
HE 240 A	193	194	QP Solai	PolG	61	0	0	93	105	0	0	95
HE 240 A					105	0	0	95	178	0	0	56
HE 240 A	193	194	QV Solai	PolG	0	0	0	18	61	0	0	30
HE 240 A					61	0	0	30	105	0	0	30

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf	
HE 240 A	193	194	Neve	PolG	0	0	0	0	11	61	0	0	30
HE 240 A					61	0	0	0	30	178	0	0	24
HE 240 A	193	194	Neve	PolG	0	0	0	0	24	105	0	0	31
HE 240 A					105	0	0	0	31	178	0	0	11
HE 240 A	193	194	Vento X	PolG	0	0	0	0	37	105	0	0	48
HE 240 A					105	0	0	0	48	178	0	0	17
HE 240 A	193	194	Vento X	PolG	0	0	0	0	17	61	0	0	47
HE 240 A					61	0	0	0	47	178	0	0	37
Trave 8016 ΔXY=15°C,ΔXZ=15°C													
HE 240 A	193	194	Carichi termici	Termico	0	0	0	0	60	178	0	0	60
HE 240 A	194	195	Peso Proprio	UnifG	64	0	0	0	58	64	0	0	98
HE 240 A	194	195	QP Solai	PolG	100	0	0	0	98	100	0	0	99
HE 240 A					100	0	0	0	99	178	0	0	58
HE 240 A	194	195	QV Solai	PolG	64	0	0	0	19	64	0	0	31
HE 240 A					64	0	0	0	31	100	0	0	32
HE 240 A	194	195	Neve	PolG	100	0	0	0	32	178	0	0	19
HE 240 A					0	0	0	0	11	64	0	0	31
HE 240 A	194	195	Neve	PolG	64	0	0	0	31	178	0	0	25
HE 240 A					0	0	0	0	25	100	0	0	32
HE 240 A	194	195	Vento X	PolG	100	0	0	0	32	178	0	0	11
HE 240 A					0	0	0	0	17	64	0	0	48
HE 240 A	194	195	Vento X	PolG	64	0	0	0	48	178	0	0	39
HE 240 A					0	0	0	0	39	100	0	0	50
HE 240 A	194	195	Vento X	PolG	100	0	0	0	50	178	0	0	17
Trave 8017 ΔXY=15°C,ΔXZ=15°C													
HE 240 A	194	195	Carichi termici	Termico	0	0	0	0	60	151	0	0	60
HE 240 A	195	196	Peso Proprio	UnifG	58	0	0	0	60	58	0	0	103
HE 240 A	195	196	QP Solai	PolG	82	0	0	0	103	82	0	0	104
HE 240 A					82	0	0	0	104	151	0	0	61
HE 240 A	195	196	QV Solai	PolG	58	0	0	0	19	58	0	0	33
HE 240 A					58	0	0	0	33	82	0	0	33
HE 240 A	195	196	Neve	PolG	82	0	0	0	33	151	0	0	19
HE 240 A					0	0	0	0	11	58	0	0	33
HE 240 A	195	196	Neve	PolG	58	0	0	0	33	151	0	0	27
HE 240 A					82	0	0	0	27	82	0	0	33
HE 240 A	195	196	Vento X	PolG	82	0	0	0	33	151	0	0	11
HE 240 A					0	0	0	0	17	58	0	0	50
HE 240 A	195	196	Vento X	PolG	58	0	0	0	50	151	0	0	42
HE 240 A					0	0	0	0	41	82	0	0	52
HE 240 A	195	196	Vento X	PolG	82	0	0	0	52	151	0	0	17
Trave 8018 ΔXY=15°C,ΔXZ=15°C													
HE 240 A	196	197	Carichi termici	Termico	0	0	0	0	60	148	0	0	60
HE 240 A	196	197	Peso Proprio	UnifG	60	0	0	0	62	60	0	0	108
HE 240 A	196	197	QP Solai	PolG	76	0	0	0	108	76	0	0	108
HE 240 A					76	0	0	0	108	148	0	0	63
HE 240 A	196	197	QV Solai	PolG	60	0	0	0	20	60	0	0	35
HE 240 A					60	0	0	0	35	76	0	0	35
HE 240 A	196	197	Neve	PolG	76	0	0	0	35	148	0	0	20
HE 240 A					0	0	0	0	11	60	0	0	34
HE 240 A	196	197	Neve	PolG	60	0	0	0	34	148	0	0	28
HE 240 A					0	0	0	0	28	76	0	0	35
HE 240 A	196	197	Vento X	PolG	76	0	0	0	35	148	0	0	11
HE 240 A					0	0	0	0	44	76	0	0	53
HE 240 A	196	197	Vento X	PolG	76	0	0	0	53	148	0	0	17
HE 240 A					0	0	0	0	17	60	0	0	52
HE 240 A	196	197	Vento X	PolG	60	0	0	0	52	148	0	0	44
Trave 8019 ΔXY=15°C,ΔXZ=15°C													
HE 240 A	196	197	Carichi termici	Termico	0	0	0	0	60	134	0	0	60
HE 240 A	197	43	Peso Proprio	UnifG	57	0	0	0	65	57	0	0	113
HE 240 A	197	43	QP Solai	PolG	66	0	0	0	113	66	0	0	113
HE 240 A					66	0	0	0	113	134	0	0	65
HE 240 A	197	43	QV Solai	PolG	0	0	0	0	21	57	0	0	36
HE 240 A					57	0	0	0	36	66	0	0	36
HE 240 A					66	0	0	0	36	134	0	0	21
HE 240 A	197	43	Neve	PolG	66	0	0	0	30	66	0	0	36
HE 240 A					66	0	0	0	36	134	0	0	11

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	197	43		PolG	0	0	0	11	57	0	0	35
HE 240 A	197	43	Vento X	PolG	57	0	0	35	134	0	0	30
HE 240 A	197	43	Vento X	PolG	66	0	0	55	134	0	0	17
HE 240 A	197	43	Vento X	PolG	57	0	0	17	57	0	0	54
HE 240 A	197	43	Carichi termici	Termico	57	0	0	54	134	0	0	46
HE 240 A	369	370	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	108	0	60
HE 240 A	369	370	QP Solai	PolG	0	0	0	72	45	0	0	119
HE 240 A	369	370		PolG	45	0	0	119	53	0	0	120
HE 240 A	369	370	QV Solai	PolG	53	0	0	120	108	0	0	72
HE 240 A	369	370		PolG	0	0	0	23	45	0	0	38
HE 240 A	369	370		PolG	45	0	0	38	53	0	0	38
HE 240 A	369	370	Neve	PolG	53	0	0	38	108	0	0	23
HE 240 A	369	370	Neve	PolG	45	0	0	39	108	0	0	11
HE 240 A	369	370	Neve	PolG	0	0	0	11	53	0	0	39
HE 240 A	369	370	Vento X	PolG	53	0	0	39	108	0	0	34
HE 240 A	369	370	Vento X	PolG	0	0	0	17	53	0	0	60
HE 240 A	369	370	Vento X	PolG	53	0	0	60	108	0	0	53
HE 240 A	369	370	Vento X	PolG	0	0	0	53	45	0	0	61
HE 240 A	369	370	Carichi termici	Termico	45	0	0	61	108	0	0	17
HE 240 A	370	339	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	112	0	60
HE 240 A	370	339	QP Solai	PolG	0	0	0	74	44	0	0	118
HE 240 A	370	339		PolG	44	0	0	118	57	0	0	120
HE 240 A	370	339	QV Solai	PolG	57	0	0	120	112	0	0	75
HE 240 A	370	339		PolG	0	0	0	24	44	0	0	38
HE 240 A	370	339	Neve	PolG	44	0	0	38	57	0	0	38
HE 240 A	370	339	Neve	PolG	57	0	0	38	112	0	0	24
HE 240 A	370	339	Neve	PolG	0	0	0	11	57	0	0	40
HE 240 A	370	339	Neve	PolG	57	0	0	40	112	0	0	36
HE 240 A	370	339	Vento X	PolG	44	0	0	36	44	0	0	40
HE 240 A	370	339	Vento X	PolG	0	0	0	40	112	0	0	11
HE 240 A	370	339	Vento X	PolG	44	0	0	55	44	0	0	62
HE 240 A	370	339	Vento X	PolG	0	0	0	62	112	0	0	17
HE 240 A	370	339	Vento X	PolG	44	0	0	17	57	0	0	62
HE 240 A	370	339	Carichi termici	Termico	57	0	0	62	112	0	0	55
HE 240 A	29	30	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	123	0	60
HE 240 A	29	30	QP Solai	PolG	0	0	0	70	47	0	0	107
HE 240 A	29	30		PolG	47	0	0	107	64	0	0	109
HE 240 A	29	30	QV Solai	PolG	64	0	0	109	123	0	0	70
HE 240 A	29	30		PolG	0	0	0	23	47	0	0	34
HE 240 A	29	30	Neve	PolG	47	0	0	34	64	0	0	35
HE 240 A	29	30	Neve	PolG	64	0	0	35	123	0	0	23
HE 240 A	29	30	Neve	PolG	0	0	0	31	47	0	0	37
HE 240 A	29	30	Neve	PolG	47	0	0	37	123	0	0	13
HE 240 A	29	30	Vento X	PolG	0	0	0	12	64	0	0	36
HE 240 A	29	30	Vento X	PolG	64	0	0	36	123	0	0	31
HE 240 A	29	30	Vento X	PolG	0	0	0	48	47	0	0	57
HE 240 A	29	30	Vento X	PolG	47	0	0	57	123	0	0	20
HE 240 A	29	30	Carichi termici	Termico	64	0	0	56	123	0	0	56
HE 240 A	29	30	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	0	60	113	0	60
HE 240 A	29	30	QP Solai	PolG	0	0	0	73	40	0	0	107
HE 240 A	29	30		PolG	40	0	0	107	62	0	0	109
HE 240 A	29	30	QV Solai	PolG	62	0	0	109	113	0	0	73
HE 240 A	29	30	Neve	PolG	0	0	0	23	40	0	0	34
HE 240 A	29	30	Neve	PolG	40	0	0	34	62	0	0	35
HE 240 A	29	30	Neve	PolG	62	0	0	35	113	0	0	23
HE 240 A	29	30	Vento X	PolG	0	0	0	12	62	0	0	37
HE 240 A	29	30	Vento X	PolG	62	0	0	37	113	0	0	32
HE 240 A	29	30	Carichi termici	Termico	62	0	0	33	40	0	0	38

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	30	355	Vento X	PolG	40	0	0	38	113	0	0	13
HE 240 A	30	355	Vento X	PolG	0	0	0	51	40	0	0	59
HE 240 A	30	355	Vento X	PolG	40	0	0	59	113	0	0	20
HE 240 A	30	355	Vento X	PolG	0	0	0	19	62	0	0	58
HE 240 A	30	355	Carichi termici	Termico	62	0	0	58	113	0	0	50
HE 240 A	114	158	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	60	182	0	0	60
HE 240 A	114	158	QP Solai	PolG	0	0	0	56	67	0	0	92
HE 240 A	114	158		PolG	67	0	0	92	100	0	0	93
HE 240 A	114	158	QV Solai	PolG	100	0	0	93	182	0	0	57
HE 240 A	114	158		PolG	0	0	0	18	67	0	0	29
HE 240 A	114	158	Neve	PolG	67	0	0	29	100	0	0	30
HE 240 A	114	158	Neve	PolG	100	0	0	30	182	0	0	18
HE 240 A	114	158	Vento X	PolG	0	0	0	12	67	0	0	23
HE 240 A	114	158	Vento X	PolG	67	0	0	22	100	0	0	30
HE 240 A	114	158	Vento X	PolG	100	0	0	30	182	0	0	13
HE 240 A	114	158	Vento X	PolG	0	0	0	19	67	0	0	46
HE 240 A	114	158	Vento X	PolG	67	0	0	46	182	0	0	35
HE 240 A	114	158	Vento X	PolG	0	0	0	35	100	0	0	47
HE 240 A	114	158	Carichi termici	Termico	100	0	0	47	182	0	0	20
HE 240 A	158	159	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	60	178	0	0	60
HE 240 A	158	159	QP Solai	PolG	0	0	0	58	70	0	0	97
HE 240 A	158	159		PolG	70	0	0	97	93	0	0	97
HE 240 A	158	159	QV Solai	PolG	93	0	0	97	178	0	0	59
HE 240 A	158	159	Neve	PolG	0	0	0	19	70	0	0	31
HE 240 A	158	159	Neve	PolG	70	0	0	31	93	0	0	31
HE 240 A	158	159	Neve	PolG	93	0	0	31	178	0	0	19
HE 240 A	158	159	Neve	PolG	0	0	0	24	93	0	0	31
HE 240 A	158	159	Neve	PolG	93	0	0	31	178	0	0	13
HE 240 A	158	159	Vento X	PolG	0	0	0	12	70	0	0	31
HE 240 A	158	159	Vento X	PolG	70	0	0	31	178	0	0	24
HE 240 A	158	159	Vento X	PolG	0	0	0	19	70	0	0	47
HE 240 A	158	159	Vento X	PolG	70	0	0	47	178	0	0	37
HE 240 A	158	159	Vento X	PolG	0	0	0	37	93	0	0	48
HE 240 A	158	159	Carichi termici	Termico	93	0	0	48	178	0	0	20
HE 240 A	159	160	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	60	178	0	0	60
HE 240 A	159	160	QP Solai	PolG	0	0	0	61	75	0	0	102
HE 240 A	159	160		PolG	75	0	0	102	88	0	0	102
HE 240 A	159	160	QV Solai	PolG	88	0	0	102	178	0	0	61
HE 240 A	159	160	Neve	PolG	0	0	0	19	75	0	0	33
HE 240 A	159	160	Neve	PolG	75	0	0	33	88	0	0	33
HE 240 A	159	160	Neve	PolG	88	0	0	33	178	0	0	20
HE 240 A	159	160	Neve	PolG	0	0	0	25	88	0	0	32
HE 240 A	159	160	Neve	PolG	88	0	0	32	178	0	0	13
HE 240 A	159	160	Neve	PolG	0	0	0	12	75	0	0	32
HE 240 A	159	160	Vento X	PolG	75	0	0	32	178	0	0	25
HE 240 A	159	160	Vento X	PolG	0	0	0	19	75	0	0	49
HE 240 A	159	160	Vento X	PolG	75	0	0	49	178	0	0	39
HE 240 A	159	160	Vento X	PolG	0	0	0	39	88	0	0	50
HE 240 A	159	160	Carichi termici	Termico	88	0	0	50	178	0	0	20
HE 240 A	160	161	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C	0	0	60	151	0	0	60
HE 240 A	160	161	QP Solai	PolG	0	0	0	63	68	0	0	106
HE 240 A	160	161		PolG	68	0	0	106	71	0	0	106
HE 240 A	160	161	QV Solai	PolG	71	0	0	106	151	0	0	64
HE 240 A	160	161	Neve	PolG	0	0	0	20	68	0	0	34
HE 240 A	160	161	Neve	PolG	68	0	0	34	71	0	0	34
HE 240 A	160	161	Neve	PolG	71	0	0	34	151	0	0	20
HE 240 A	160	161	Neve	PolG	0	0	0	27	71	0	0	34
HE 240 A	160	161	Neve	PolG	71	0	0	34	151	0	0	13
HE 240 A	160	161	Neve	PolG	0	0	0	12	68	0	0	33
HE 240 A	160	161	Vento X	PolG	68	0	0	33	151	0	0	27
HE 240 A	160	161	Vento X	PolG	0	0	0	19	68	0	0	51

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	160	161	Vento X	PolG	68	0	0	0	51	151	0	41
HE 240 A	160	161			71	0	0	0	42	71	0	52
HE 240 A	161	162	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	161	162	Peso Proprio	UnifG	0	0	0	0	60	148	0	60
HE 240 A	161	162	QP Solai	PolG	65	0	0	0	65	65	0	108
HE 240 A	161	162			70	0	0	0	108	70	0	108
HE 240 A	161	162	QV Solai	PolG	70	0	0	0	108	148	0	66
HE 240 A	161	162			65	0	0	0	21	65	0	35
HE 240 A	161	162			70	0	0	0	35	70	0	35
HE 240 A	161	162	Neve	PolG	70	0	0	0	35	148	0	21
HE 240 A	161	162			65	0	0	0	28	65	0	35
HE 240 A	161	162	Neve	PolG	70	0	0	0	35	148	0	13
HE 240 A	161	162			70	0	0	0	34	148	0	28
HE 240 A	161	162	Vento X	PolG	70	0	0	0	19	70	0	53
HE 240 A	161	162			70	0	0	0	53	148	0	44
HE 240 A	161	162	Vento X	PolG	70	0	0	0	44	65	0	53
HE 240 A	161	162			65	0	0	0	53	148	0	20
HE 240 A	162	29	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	162	29	Peso Proprio	UnifG	0	0	0	0	60	134	0	60
HE 240 A	162	29	QP Solai	PolG	55	0	0	0	68	55	0	108
HE 240 A	162	29			67	0	0	0	108	67	0	109
HE 240 A	162	29	QV Solai	PolG	67	0	0	0	109	134	0	68
HE 240 A	162	29			55	0	0	0	22	55	0	34
HE 240 A	162	29			67	0	0	0	34	67	0	35
HE 240 A	162	29			67	0	0	0	35	134	0	22
HE 240 A	162	29	Neve	PolG	67	0	0	0	12	67	0	35
HE 240 A	162	29			67	0	0	0	35	134	0	30
HE 240 A	162	29	Neve	PolG	55	0	0	0	30	55	0	36
HE 240 A	162	29			67	0	0	0	36	134	0	13
HE 240 A	162	29	Vento X	PolG	67	0	0	0	19	67	0	54
HE 240 A	162	29			67	0	0	0	54	134	0	46
HE 240 A	162	29	Vento X	PolG	55	0	0	0	46	55	0	55
HE 240 A	162	29			55	0	0	0	55	134	0	20
HE 240 A	355	356	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	355	356	Peso Proprio	UnifG	0	0	0	0	60	108	0	60
HE 240 A	355	356	QP Solai	PolG	36	0	0	0	75	36	0	107
HE 240 A	355	356			62	0	0	0	107	62	0	109
HE 240 A	355	356	QV Solai	PolG	62	0	0	0	109	108	0	75
HE 240 A	355	356			36	0	0	0	24	36	0	34
HE 240 A	355	356			62	0	0	0	34	62	0	35
HE 240 A	355	356	Neve	PolG	62	0	0	0	35	108	0	24
HE 240 A	355	356			36	0	0	0	34	36	0	39
HE 240 A	355	356	Neve	PolG	62	0	0	0	39	108	0	13
HE 240 A	355	356			62	0	0	0	12	62	0	39
HE 240 A	355	356	Vento X	PolG	36	0	0	0	53	36	0	60
HE 240 A	355	356			36	0	0	0	60	108	0	20
HE 240 A	355	356	Vento X	PolG	62	0	0	0	19	62	0	60
HE 240 A	355	356			62	0	0	0	60	108	0	52
HE 240 A	356	340	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	356	340	Peso Proprio	UnifG	0	0	0	0	60	112	0	60
HE 240 A	356	340	QP Solai	PolG	34	0	0	0	106	67	0	106
HE 240 A	356	340			67	0	0	0	109	112	0	77
HE 240 A	356	340	QV Solai	PolG	34	0	0	0	25	34	0	34
HE 240 A	356	340			67	0	0	0	34	67	0	35
HE 240 A	356	340	Neve	PolG	67	0	0	0	35	112	0	25
HE 240 A	356	340			67	0	0	0	12	67	0	40
HE 240 A	356	340	Neve	PolG	67	0	0	0	40	112	0	35
HE 240 A	356	340			34	0	0	0	36	34	0	40
HE 240 A	356	340	Vento X	PolG	34	0	0	0	40	112	0	13
HE 240 A	356	340			34	0	0	0	55	34	0	62
HE 240 A	356	340	Vento X	PolG	34	0	0	0	62	112	0	20
HE 240 A	356	340			76	0	0	0	50	178	0	23

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	356	340		Termico	67	0	0	0	61	112	0	55
Trave 8014												
HE 240 A		0	47	Peso Proprio	UnifG	0	0	0	60	134	0	60
HE 240 A		0		Peso Proprio	UnifG	0	0	0	60	178	0	60
HE 240 A		0		Peso Proprio	UnifG	0	0	0	60	148	0	60
HE 240 A		0		Peso Proprio	UnifG	0	0	0	60	178	0	60
HE 240 A		0		Peso Proprio	UnifG	0	0	0	60	151	0	60
HE 240 A		0		QP Solai	PolG	0	0	0	61	82	0	100
HE 240 A		0				82	0	0	100	178	0	62
HE 240 A		0		QP Solai	PolG	0	0	0	68	53	0	99
						53	0	0	99	81	0	100
HE 240 A		0	47	QP Solai	PolG	81	0	0	100	148	0	69
						44	0	0	99	77	0	101
HE 240 A		0				77	0	0	101	134	0	71
HE 240 A		0		QP Solai	PolG	0	0	0	64	76	0	99
						76	0	0	99	87	0	100
HE 240 A		0				87	0	0	100	178	0	64
HE 240 A		0		QP Solai	PolG	0	0	0	66	60	0	99
						60	0	0	99	78	0	100
HE 240 A		0				78	0	0	100	151	0	67
HE 240 A		0		QV Solai	PolG	0	0	0	20	82	0	32
						82	0	0	32	178	0	20
HE 240 A		0	47	QV Solai	PolG	0	0	0	23	44	0	32
						44	0	0	32	77	0	32
HE 240 A		0				77	0	0	32	134	0	23
HE 240 A		0		QV Solai	PolG	0	0	0	21	60	0	32
						60	0	0	32	78	0	32
HE 240 A		0				78	0	0	32	151	0	21
HE 240 A		0		QV Solai	PolG	0	0	0	20	76	0	32
						76	0	0	32	87	0	32
HE 240 A		0				87	0	0	32	178	0	21
HE 240 A		0		QV Solai	PolG	0	0	0	22	53	0	32
						53	0	0	32	81	0	32
HE 240 A		0				81	0	0	32	148	0	22
HE 240 A		0		Neve	PolG	0	0	0	28	53	0	34
						53	0	0	34	148	0	15
HE 240 A		0		Neve	PolG	0	0	0	27	60	0	33
HE 240 A		0				60	0	0	33	151	0	15
HE 240 A		0		Neve	PolG	0	0	0	14	82	0	31
HE 240 A		0				82	0	0	31	178	0	24
HE 240 A		0		Neve	PolG	0	0	0	25	76	0	32
HE 240 A		0				76	0	0	32	178	0	15
HE 240 A		0		Neve	PolG	0	0	0	14	87	0	32
HE 240 A		0				87	0	0	32	178	0	25
HE 240 A		0		Neve	PolG	0	0	0	24	82	0	31
HE 240 A		0				82	0	0	31	178	0	15
HE 240 A		0		Neve	PolG	0	0	0	14	78	0	33
HE 240 A		0				78	0	0	33	151	0	27
HE 240 A		0	47	Neve	PolG	0	0	0	30	44	0	35
HE 240 A		0				44	0	0	35	134	0	15
HE 240 A		0		Neve	PolG	0	0	0	14	81	0	34
HE 240 A		0				81	0	0	34	148	0	28
HE 240 A		0	47	Neve	PolG	0	0	0	14	77	0	35
HE 240 A		0	47	Vento X	PolG	0	0	0	35	134	0	30
HE 240 A		0				77	0	0	22	77	0	54
HE 240 A		0		Vento X	PolG	0	0	0	54	134	0	46
HE 240 A		0				81	0	0	22	81	0	53
HE 240 A		0		Vento X	PolG	0	0	0	37	82	0	48
HE 240 A		0				82	0	0	48	178	0	23
HE 240 A		0		Vento X	PolG	0	0	0	22	78	0	51
HE 240 A		0				78	0	0	51	151	0	41
HE 240 A		0		Vento X	PolG	0	0	0	39	76	0	50
HE 240 A						76	0	0	50	178	0	23

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Vento X	PolG	60	0	0	42	60	0	0	51
HE 240 A	0	0	Vento X	PolG	0	0	0	51	151	0	0	23
HE 240 A	0	0	Vento X	PolG	53	0	0	44	53	0	0	23
HE 240 A	0	47	Vento X	PolG	0	0	0	53	148	0	0	23
HE 240 A	0	0	Vento X	PolG	44	0	0	46	44	0	0	54
HE 240 A	0	0	Vento X	PolG	0	0	0	54	134	0	0	23
HE 240 A	0	0	Vento X	PolG	0	0	0	22	82	0	0	48
HE 240 A	0	0	Vento X	PolG	82	0	0	48	178	0	0	37
HE 240 A	0	0	Vento X	PolG	0	0	0	22	87	0	0	49
HE 240 A	0	0	Vento X	PolG	87	0	0	49	178	0	0	39
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	0	47	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	47	48	Peso Proprio	UnitG	0	0	0	60	123	0	0	60
HE 240 A	47	48	QP Solai	PolG	36	0	0	73	36	0	0	98
HE 240 A	47	48	QP Solai	PolG	74	0	0	98	74	0	0	101
HE 240 A	47	48	QP Solai	PolG	0	0	0	101	123	0	0	73
HE 240 A	47	48	QP Solai	PolG	0	0	0	23	36	0	0	31
HE 240 A	47	48	QP Solai	PolG	36	0	0	31	74	0	0	32
HE 240 A	47	48	QP Solai	PolG	74	0	0	32	123	0	0	24
HE 240 A	47	48	QP Solai	PolG	0	0	0	14	74	0	0	36
HE 240 A	47	48	QP Solai	PolG	74	0	0	36	123	0	0	31
HE 240 A	47	48	QP Solai	PolG	0	0	0	31	36	0	0	36
HE 240 A	47	48	QP Solai	PolG	36	0	0	36	123	0	0	15
HE 240 A	47	48	QP Solai	PolG	0	0	0	22	74	0	0	56
HE 240 A	47	48	QP Solai	PolG	74	0	0	56	123	0	0	48
HE 240 A	47	48	QP Solai	PolG	0	0	0	49	36	0	0	56
HE 240 A	47	48	QP Solai	PolG	36	0	0	56	123	0	0	23
HE 240 A	47	48	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	48	373	Peso Proprio	UnitG	0	0	0	60	113	0	0	60
HE 240 A	48	373	Peso Proprio	UnitG	0	0	0	76	30	0	0	98
HE 240 A	48	373	Peso Proprio	UnitG	30	0	0	98	72	0	0	101
HE 240 A	48	373	Peso Proprio	UnitG	72	0	0	101	113	0	0	76
HE 240 A	48	373	Peso Proprio	UnitG	0	0	0	24	30	0	0	31
HE 240 A	48	373	Peso Proprio	UnitG	30	0	0	31	72	0	0	32
HE 240 A	48	373	Peso Proprio	UnitG	72	0	0	32	113	0	0	24
HE 240 A	48	373	Peso Proprio	UnitG	0	0	0	14	72	0	0	37
HE 240 A	48	373	Peso Proprio	UnitG	72	0	0	37	113	0	0	32
HE 240 A	48	373	Peso Proprio	UnitG	0	0	0	33	30	0	0	37
HE 240 A	48	373	Peso Proprio	UnitG	30	0	0	37	113	0	0	15
HE 240 A	48	373	Peso Proprio	UnitG	0	0	0	51	30	0	0	58
HE 240 A	48	373	Peso Proprio	UnitG	30	0	0	58	113	0	0	23
HE 240 A	48	373	Peso Proprio	UnitG	0	0	0	22	72	0	0	57
HE 240 A	48	373	Peso Proprio	UnitG	72	0	0	57	113	0	0	50
HE 240 A	48	373	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	115	0	Peso Proprio	UnitG	0	0	0	60	182	0	0	60
HE 240 A	115	0	Peso Proprio	UnitG	0	0	0	59	79	0	0	95
HE 240 A	115	0	Peso Proprio	UnitG	79	0	0	95	89	0	0	95
HE 240 A	115	0	Peso Proprio	UnitG	89	0	0	95	182	0	0	60
HE 240 A	115	0	Peso Proprio	UnitG	0	0	0	19	79	0	0	30
HE 240 A	115	0	Peso Proprio	UnitG	79	0	0	30	89	0	0	31
HE 240 A	115	0	Peso Proprio	UnitG	89	0	0	31	182	0	0	19
HE 240 A	115	0	Peso Proprio	UnitG	0	0	0	14	79	0	0	30
HE 240 A	115	0	Peso Proprio	UnitG	79	0	0	30	182	0	0	23
HE 240 A	115	0	Peso Proprio	UnitG	0	0	0	22	89	0	0	30
HE 240 A	115	0	Peso Proprio	UnitG	89	0	0	30	182	0	0	15
HE 240 A	115	0	Peso Proprio	UnitG	0	0	0	35	89	0	0	47
HE 240 A	115	0	Peso Proprio	UnitG	89	0	0	47	182	0	0	23
HE 240 A	115	0	Peso Proprio	UnitG	0	0	0	22	79	0	0	46
HE 240 A	115	0	Peso Proprio	UnitG	79	0	0	46	182	0	0	35
HE 240 A	115	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	373	374	Peso Proprio	UnitG	0	0	0	60	108	0	0	60
HE 240 A	373	374	Peso Proprio	UnitG	0	0	0	78	25	0	0	98

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					25	0	0	98	71	0	0	101
					71	0	0	101	108	0	0	78
HE 240 A	373	374	QV Solai	PolG	0	0	0	25	25	0	0	31
					25	0	0	31	71	0	0	33
					71	0	0	33	108	0	0	25
HE 240 A	373	374	Neve	PolG	0	0	0	14	71	0	0	38
					71	0	0	38	108	0	0	34
HE 240 A	373	374	Neve	PolG	0	0	0	34	25	0	0	38
					25	0	0	38	108	0	0	15
HE 240 A	373	374	Vento X	PolG	0	0	0	53	25	0	0	59
					25	0	0	59	108	0	0	23
HE 240 A	373	374	Vento X	PolG	0	0	0	22	71	0	0	59
					71	0	0	59	108	0	0	52
HE 240 A	373	374	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	374	341	Peso Proprio	UnitG	0	0	0	60	112	0	0	60
HE 240 A	374	341	Peso Proprio	UnitG	0	0	0	81	22	0	0	97
HE 240 A	374	341	QP Solai	PolG	22	0	0	97	77	0	0	102
					77	0	0	102	112	0	0	80
HE 240 A	374	341	QV Solai	PolG	0	0	0	26	22	0	0	31
					22	0	0	31	77	0	0	33
					77	0	0	33	112	0	0	26
HE 240 A	374	341	Neve	PolG	0	0	0	14	77	0	0	39
					77	0	0	39	112	0	0	35
HE 240 A	374	341	Neve	PolG	0	0	0	36	22	0	0	39
					22	0	0	39	112	0	0	15
HE 240 A	374	341	Vento X	PolG	0	0	0	22	77	0	0	61
					77	0	0	61	112	0	0	54
HE 240 A	374	341	Vento X	PolG	0	0	0	56	22	0	0	61
					22	0	0	61	112	0	0	23
HE 240 A	374	341	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 80.15												
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	0	57	Peso Proprio	UnitG	0	0	0	60	134	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	148	0	0	60
HE 240 A	0	0	QP Solai	PolG	0	0	0	64	70	0	0	93
					70	0	0	93	93	0	0	94
HE 240 A	0	0	QP Solai	PolG	93	0	0	94	178	0	0	65
					49	0	0	69	49	0	0	93
					90	0	0	93	90	0	0	95
HE 240 A	0	57	QP Solai	PolG	0	0	0	95	151	0	0	69
					33	0	0	74	33	0	0	92
					89	0	0	92	89	0	0	95
HE 240 A	0	0	QP Solai	PolG	0	0	0	95	134	0	0	74
					63	0	0	67	63	0	0	93
					99	0	0	93	99	0	0	94
HE 240 A	0	0	QP Solai	PolG	0	0	0	94	178	0	0	67
					42	0	0	72	42	0	0	93
					93	0	0	93	93	0	0	95
					93	0	0	95	148	0	0	72
HE 240 A	0	0	QV Solai	PolG	0	0	0	22	49	0	0	30
					49	0	0	30	90	0	0	30
					90	0	0	30	151	0	0	22
HE 240 A	0	0	QV Solai	PolG	0	0	0	21	63	0	0	30
					63	0	0	30	99	0	0	30
					99	0	0	30	178	0	0	22
HE 240 A	0	0	QV Solai	PolG	0	0	0	23	42	0	0	30
					42	0	0	30	93	0	0	30
					93	0	0	30	148	0	0	23
HE 240 A	0	0	QV Solai	PolG	0	0	0	21	70	0	0	30
					70	0	0	30	93	0	0	30
					93	0	0	30	178	0	0	21
HE 240 A	0	57	QV Solai	PolG	0	0	0	24	33	0	0	30
					33	0	0	30	89	0	0	30
					89	0	0	30	134	0	0	24

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0		PolG	0	0	0	16	99	0	0	32
HE 240 A	0	0	Neve		99	0	0	32	178	0	0	25
HE 240 A	0	0	Neve	PolG	0	0	0	24	70	0	0	31
HE 240 A	0	0			70	0	0	31	178	0	0	17
HE 240 A	0	0	Neve	PolG	0	0	0	25	63	0	0	32
HE 240 A	0	0			63	0	0	32	178	0	0	17
HE 240 A	0	0	Neve	PolG	0	0	0	16	93	0	0	31
HE 240 A	0	57	Neve	PolG	93	0	0	31	178	0	0	24
HE 240 A	0	0			89	0	0	34	134	0	0	29
HE 240 A	0	0	Neve	PolG	0	0	0	16	90	0	0	33
HE 240 A	0	57	Neve	PolG	90	0	0	33	151	0	0	27
HE 240 A	0	0	Neve		33	0	0	34	134	0	0	17
HE 240 A	0	0	Neve	PolG	0	0	0	16	93	0	0	33
HE 240 A	0	0	Neve	PolG	93	0	0	33	148	0	0	28
HE 240 A	0	0			49	0	0	33	151	0	0	17
HE 240 A	0	0	Neve	PolG	0	0	0	28	42	0	0	34
HE 240 A	0	57	Vento X	PolG	42	0	0	34	148	0	0	17
HE 240 A	0	0			89	0	0	53	134	0	0	53
HE 240 A	0	0	Vento X	PolG	0	0	0	44	42	0	0	52
HE 240 A	0	0			42	0	0	52	148	0	0	26
HE 240 A	0	0	Vento X	PolG	0	0	0	39	63	0	0	49
HE 240 A	0	0			63	0	0	49	178	0	0	26
HE 240 A	0	0	Vento X	PolG	0	0	0	25	93	0	0	47
HE 240 A	0	57	Vento X	PolG	93	0	0	46	33	0	0	37
HE 240 A	0	0			33	0	0	53	134	0	0	26
HE 240 A	0	0	Vento X	PolG	0	0	0	52	148	0	0	43
HE 240 A	0	0			90	0	0	25	90	0	0	50
HE 240 A	0	0	Vento X	PolG	0	0	0	42	49	0	0	51
HE 240 A	0	0			49	0	0	25	99	0	0	49
HE 240 A	0	0	Vento X	PolG	99	0	0	37	70	0	0	39
HE 240 A	0	0			70	0	0	48	178	0	0	26
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	0	57	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	57	58	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	57	58	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	57	58	QV Solai	PolG	26	0	0	92	85	0	0	95
HE 240 A	57	58			85	0	0	95	123	0	0	76
HE 240 A	57	58	QV Solai	PolG	0	0	0	25	26	0	0	30
HE 240 A					26	0	0	30	85	0	0	31
HE 240 A					85	0	0	31	123	0	0	24
HE 240 A	57	58	Neve	PolG	0	0	0	32	26	0	0	35
HE 240 A	57	58	Neve	PolG	26	0	0	35	123	0	0	17
HE 240 A					85	0	0	35	123	0	0	31
HE 240 A	57	58	Vento X	PolG	0	0	0	49	26	0	0	55
HE 240 A	57	58			26	0	0	55	123	0	0	26
HE 240 A	57	58	Vento X	PolG	0	0	0	25	85	0	0	55
HE 240 A	57	58			85	0	0	55	123	0	0	48
HE 240 A	57	58	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	58	383	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	58	383	QV Solai	PolG	0	0	0	79	20	0	0	92
HE 240 A					20	0	0	92	82	0	0	95
HE 240 A	58	383	QV Solai	PolG	0	0	0	95	113	0	0	79

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	58	383	Neve	PolG	82	0	0	31	113	0	0	31
HE 240 A	58	383	Neve	PolG	0	0	0	16	82	0	0	36
HE 240 A	58	383	Neve	PolG	82	0	0	33	20	0	0	36
HE 240 A	58	383	Vento X	PolG	20	0	0	36	113	0	0	17
HE 240 A	58	383	Vento X	PolG	20	0	0	56	113	0	0	26
HE 240 A	58	383	Vento X	PolG	0	0	0	25	82	0	0	56
HE 240 A	58	383	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	116	0	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	116	0	QV Solai	PolG	78	0	0	94	182	0	0	94
HE 240 A	116	0	QV Solai	PolG	89	0	0	94	182	0	0	63
HE 240 A	116	0			78	0	0	20	78	0	0	30
HE 240 A	116	0	Neve	PolG	89	0	0	30	182	0	0	20
HE 240 A	116	0	Neve	PolG	78	0	0	22	78	0	0	30
HE 240 A	116	0	Neve	PolG	78	0	0	30	182	0	0	17
HE 240 A	116	0	Vento X	PolG	89	0	0	16	89	0	0	30
HE 240 A	116	0	Vento X	PolG	0	0	0	25	89	0	0	46
HE 240 A	116	0	Vento X	PolG	89	0	0	46	182	0	0	35
HE 240 A	116	0			78	0	0	47	182	0	0	47
HE 240 A	116	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	383	384	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
HE 240 A	383	384	QV Solai	PolG	15	0	0	81	15	0	0	92
HE 240 A	383	384			82	0	0	96	108	0	0	81
HE 240 A	383	384	QV Solai	PolG	0	0	0	26	15	0	0	29
HE 240 A	383	384	Neve	PolG	15	0	0	31	108	0	0	26
HE 240 A	383	384	Neve	PolG	15	0	0	37	108	0	0	17
HE 240 A	383	384	Neve	PolG	82	0	0	37	108	0	0	37
HE 240 A	383	384	Vento X	PolG	0	0	0	53	15	0	0	57
HE 240 A	383	384	Vento X	PolG	15	0	0	57	108	0	0	26
HE 240 A	383	384	Vento X	PolG	0	0	0	25	82	0	0	58
HE 240 A	383	384	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	384	342	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
HE 240 A	384	342	QV Solai	PolG	12	0	0	84	12	0	0	92
HE 240 A	384	342			89	0	0	96	112	0	0	83
HE 240 A	384	342	QV Solai	PolG	0	0	0	27	12	0	0	29
HE 240 A	384	342	Neve	PolG	12	0	0	29	89	0	0	31
HE 240 A	384	342	Neve	PolG	89	0	0	31	112	0	0	27
HE 240 A	384	342	Neve	PolG	0	0	0	16	89	0	0	38
HE 240 A	384	342	Neve	PolG	89	0	0	38	112	0	0	35
HE 240 A	384	342	Neve	PolG	0	0	0	36	12	0	0	38
HE 240 A	384	342	Vento X	PolG	12	0	0	38	112	0	0	17
HE 240 A	384	342	Vento X	PolG	0	0	0	25	89	0	0	59
HE 240 A	384	342	Vento X	PolG	89	0	0	59	112	0	0	54
HE 240 A	384	342			0	0	0	56	12	0	0	59
HE 240 A	384	342	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
HE 240 A	0	49	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	49	QV Solai	PolG	0	0	0	78	19	0	0	87

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					19	0	0	0	87	100	0	91
					100	0	0	0	91	134	0	77
HE 240 A	0	0	QP Solai	PolG					75	27	0	88
					27	0	0	0	88	104	0	91
					104	0	0	0	91	148	0	75
HE 240 A	0	0	QP Solai	PolG					73	34	0	88
					34	0	0	0	88	101	0	91
					101	0	0	0	91	151	0	73
HE 240 A	0	0	QP Solai	PolG					68	55	0	88
					55	0	0	0	88	105	0	90
					105	0	0	0	90	178	0	68
HE 240 A	0	0	QP Solai	PolG					71	47	0	88
					47	0	0	0	88	112	0	90
					112	0	0	0	90	178	0	71
HE 240 A	0	0	QV Solai	PolG					24	27	0	28
					27	0	0	0	28	104	0	29
					104	0	0	0	29	148	0	24
HE 240 A	0	0	QV Solai	PolG					22	55	0	28
					55	0	0	0	28	105	0	29
					105	0	0	0	29	178	0	22
HE 240 A	0	0	QV Solai	PolG					23	34	0	28
					34	0	0	0	28	101	0	29
					101	0	0	0	29	151	0	23
HE 240 A	0	0	QV Solai	PolG					23	47	0	28
					47	0	0	0	28	112	0	29
					112	0	0	0	29	178	0	23
HE 240 A	0	49	QV Solai	PolG					25	19	0	28
					19	0	0	0	28	100	0	29
HE 240 A	0	0	Neve	PolG					29	134	0	25
					100	0	0	0	26	47	0	31
HE 240 A	0	0	Neve	PolG					31	178	0	19
					47	0	0	0	18	105	0	30
HE 240 A	0	0	Neve	PolG					30	178	0	24
					105	0	0	0	18	112	0	31
HE 240 A	0	0	Neve	PolG					31	178	0	25
					112	0	0	0	18	101	0	32
HE 240 A	0	0	Neve	PolG					32	151	0	26
					101	0	0	0	32	151	0	19
HE 240 A	0	0	Neve	PolG					29	27	0	33
					27	0	0	0	33	148	0	19
HE 240 A	0	0	Neve	PolG					18	104	0	33
					104	0	0	0	33	148	0	28
HE 240 A	0	0	Neve	PolG					27	34	0	32
					34	0	0	0	32	151	0	19
HE 240 A	0	0	Neve	PolG					24	55	0	31
					55	0	0	0	31	178	0	19
HE 240 A	0	49	Neve	PolG					30	19	0	33
					19	0	0	0	33	134	0	19
HE 240 A	0	49	Neve	PolG					18	100	0	34
					100	0	0	0	34	134	0	29
HE 240 A	0	0	Vento X	PolG					45	27	0	50
					27	0	0	0	50	148	0	29
HE 240 A	0	0	Vento X	PolG					28	104	0	51
					104	0	0	0	51	148	0	43
HE 240 A	0	0	Vento X	PolG					28	101	0	49
					101	0	0	0	49	151	0	41
HE 240 A	0	0	Vento X	PolG					28	112	0	48
					112	0	0	0	48	178	0	39
HE 240 A	0	0	Vento X	PolG					42	34	0	49
					34	0	0	0	49	151	0	29
HE 240 A	0	0	Vento X	PolG					28	105	0	47
					105	0	0	0	47	178	0	36
HE 240 A	0	49	Vento X	PolG					47	19	0	51
					19	0	0	0	51	134	0	29
HE 240 A	0	0	Vento X	PolG					38	55	0	47
					55	0	0	0	47	178	0	29
HE 240 A	0	49	Vento X	PolG					28	100	0	52

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Vento X	PolG					52	134	0	45
					100	0	0	0	40	47	0	48
HE 240 A	0	0	Carichi termici	Termico					47	0	0	29
					47	0	0	0	48	178	0	0
HE 240 A	0	0	Carichi termici	Termico					15°C,AXZ=15°C			
HE 240 A	0	0	Carichi termici	Termico					15°C,AXZ=15°C			
HE 240 A	0	49	Carichi termici	Termico					15°C,AXZ=15°C			
HE 240 A	0	0	Carichi termici	Termico					15°C,AXZ=15°C			
HE 240 A	0	0	Carichi termici	Termico					15°C,AXZ=15°C			
HE 240 A	49	50	Peso Proprio	UnifG					60	123	0	60
HE 240 A	49	50	QP Solai	PolG					80	13	0	87
					13	0	0	0	87	96	0	92
					96	0	0	0	92	123	0	80
HE 240 A	49	50	QV Solai	PolG					26	13	0	28
					13	0	0	0	28	96	0	29
					96	0	0	0	29	123	0	26
HE 240 A	49	50	Neve	PolG					18	96	0	34
					96	0	0	0	34	123	0	31
HE 240 A	49	50	Neve	PolG					32	13	0	34
					13	0	0	0	34	123	0	19
HE 240 A	49	50	Vento X	PolG					28	96	0	53
					96	0	0	0	53	123	0	47
HE 240 A	49	50	Vento X	PolG					49	13	0	52
					13	0	0	0	52	123	0	29
HE 240 A	49	50	Carichi termici	Termico					60	113	0	60
HE 240 A	50	375	Peso Proprio	UnifG					83	7	0	87
HE 240 A	50	375	QP Solai	PolG					87	92	0	92
					7	0	0	0	92	113	0	82
HE 240 A	50	375	QV Solai	PolG					26	7	0	28
					7	0	0	0	28	92	0	29
					92	0	0	0	29	113	0	26
HE 240 A	50	375	Neve	PolG					33	7	0	35
					7	0	0	0	35	113	0	19
HE 240 A	50	375	Neve	PolG					18	92	0	35
					92	0	0	0	35	113	0	32
HE 240 A	50	375	Vento X	PolG					52	7	0	54
					7	0	0	0	54	113	0	29
HE 240 A	50	375	Vento X	PolG					28	92	0	54
					92	0	0	0	54	113	0	50
HE 240 A	50	375	Carichi termici	Termico					60	182	0	60
HE 240 A	117	0	Peso Proprio	UnifG					66	63	0	89
HE 240 A	117	0	QP Solai	PolG					89	101	0	90
					63	0	0	0	90	182	0	66
HE 240 A	117	0	QV Solai	PolG					21	63	0	28
					63	0	0	0	28	101	0	29
					101	0	0	0	29	182	0	21
HE 240 A	117	0	Neve	PolG					18	101	0	30
					101	0	0	0	30	182	0	22
HE 240 A	117	0	Neve	PolG					23	63	0	30
					63	0	0	0	30	182	0	19
HE 240 A	117	0	Vento X	PolG					35	63	0	46
					63	0	0	0	46	182	0	29
HE 240 A	117	0	Vento X	PolG					28	101	0	46
					101	0	0	0	46	182	0	34
HE 240 A	117	0	Carichi termici	Termico					60	108	0	60
HE 240 A	375	376	Peso Proprio	UnifG					85	2	0	87
HE 240 A	375	376	QP Solai	PolG					87	92	0	92
					2	0	0	0	92	108	0	84
HE 240 A	375	376	QV Solai	PolG					27	2	0	28
					2	0	0	0	28	92	0	29
HE 240 A	375	376	Neve	PolG					29	108	0	27
					92	0	0	0	35	2	0	35
HE 240 A	375	376	Neve	PolG					108	0	0	19

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	375	376	Neve	PolG	0	0	0	18	92	0	0	36
HE 240 A	375	376	Vento X	PolG	92	0	0	36	108	0	0	33
HE 240 A	375	376	Vento X	PolG	0	0	0	28	92	0	0	56
HE 240 A	375	376	Vento X	PolG	92	0	0	56	108	0	0	52
HE 240 A	375	376	Vento X	PolG	0	0	0	54	2	0	0	55
HE 240 A	375	376	Carichi termici	Termico	2	0	0	55	108	0	0	29
HE 240 A	376	343	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
HE 240 A	376	343	QP Solai	PolG	100	0	0	86	100	0	0	92
HE 240 A	376	343	QV Solai	PolG	0	0	0	28	100	0	0	30
HE 240 A	376	343	Neve	PolG	100	0	0	30	112	0	0	28
HE 240 A	376	343	Neve	PolG	0	0	0	18	100	0	0	37
HE 240 A	376	343	Neve	PolG	100	0	0	37	112	0	0	35
HE 240 A	376	343	Vento X	PolG	0	0	0	36	112	0	0	19
HE 240 A	376	343	Vento X	PolG	0	0	0	28	100	0	0	57
HE 240 A	376	343	Vento X	PolG	100	0	0	57	112	0	0	54
HE 240 A	376	343	Carichi termici	Termico	0	0	0	55	112	0	0	29
Trave 8017												
HE 240 A	35	36	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	35	36	QP Solai	PolG	0	0	0	84	109	0	0	89
HE 240 A	35	36	QV Solai	PolG	109	0	0	89	123	0	0	84
HE 240 A	35	36	Neve	PolG	0	0	0	27	109	0	0	28
HE 240 A	35	36	Neve	PolG	109	0	0	28	123	0	0	27
HE 240 A	35	36	Neve	PolG	0	0	0	20	109	0	0	33
HE 240 A	35	36	Neve	PolG	109	0	0	33	123	0	0	31
HE 240 A	35	36	Neve	PolG	0	0	0	32	123	0	0	21
HE 240 A	35	36	Vento X	PolG	0	0	0	31	109	0	0	51
HE 240 A	35	36	Vento X	PolG	109	0	0	51	123	0	0	47
HE 240 A	35	36	Vento X	PolG	0	0	0	49	123	0	0	33
HE 240 A	35	36	Carichi termici	Termico	0	0	0	49	123	0	0	33
HE 240 A	36	361	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	36	361	QP Solai	PolG	0	0	0	84	106	0	0	89
HE 240 A	36	361	QV Solai	PolG	106	0	0	89	113	0	0	86
HE 240 A	36	361	Neve	PolG	0	0	0	27	106	0	0	28
HE 240 A	36	361	Neve	PolG	106	0	0	28	113	0	0	27
HE 240 A	36	361	Neve	PolG	0	0	0	32	113	0	0	21
HE 240 A	36	361	Neve	PolG	0	0	0	20	106	0	0	33
HE 240 A	36	361	Vento X	PolG	106	0	0	33	113	0	0	32
HE 240 A	36	361	Vento X	PolG	0	0	0	31	106	0	0	52
HE 240 A	36	361	Vento X	PolG	106	0	0	52	113	0	0	50
HE 240 A	36	361	Vento X	PolG	0	0	0	49	113	0	0	33
HE 240 A	36	361	Carichi termici	Termico	0	0	0	49	113	0	0	33
HE 240 A	118	173	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	118	173	QP Solai	PolG	0	0	0	69	51	0	0	85
HE 240 A	118	173	QV Solai	PolG	51	0	0	85	116	0	0	87
HE 240 A	118	173	Neve	PolG	116	0	0	87	182	0	0	70
HE 240 A	118	173	Neve	PolG	0	0	0	22	51	0	0	27
HE 240 A	118	173	Neve	PolG	51	0	0	27	116	0	0	28
HE 240 A	118	173	Neve	PolG	116	0	0	28	182	0	0	22
HE 240 A	118	173	Neve	PolG	0	0	0	23	51	0	0	29
HE 240 A	118	173	Neve	PolG	51	0	0	29	182	0	0	21
HE 240 A	118	173	Neve	PolG	0	0	0	20	116	0	0	29
HE 240 A	118	173	Neve	PolG	116	0	0	29	182	0	0	22
HE 240 A	118	173	Vento X	PolG	0	0	0	31	116	0	0	45
HE 240 A	118	173	Vento X	PolG	116	0	0	45	182	0	0	35
HE 240 A	118	173	Vento X	PolG	0	0	0	35	51	0	0	45
HE 240 A	118	173	Vento X	PolG	51	0	0	45	182	0	0	33
HE 240 A	118	173	Carichi termici	Termico	0	0	0	60	178	0	0	60
HE 240 A	173	174	Peso Proprio	UnifG	0	0	0	71	42	0	0	85
HE 240 A	173	174	QP Solai	PolG	42	0	0	85	121	0	0	88
HE 240 A	173	174	QV Solai	PolG	121	0	0	88	178	0	0	72
HE 240 A	173	174	Neve	PolG	0	0	0	23	42	0	0	27

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	173	174	Neve	PolG	121	0	0	28	178	0	0	23
HE 240 A	173	174	Neve	PolG	0	0	0	20	121	0	0	30
HE 240 A	173	174	Neve	PolG	121	0	0	30	178	0	0	24
HE 240 A	173	174	Vento X	PolG	0	0	0	24	42	0	0	29
HE 240 A	173	174	Vento X	PolG	42	0	0	29	178	0	0	21
HE 240 A	173	174	Vento X	PolG	0	0	0	37	42	0	0	45
HE 240 A	173	174	Vento X	PolG	42	0	0	45	178	0	0	33
HE 240 A	173	174	Vento X	PolG	0	0	0	31	121	0	0	46
HE 240 A	173	174	Carichi termici	Termico	121	0	0	46	178	0	0	37
HE 240 A	174	175	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	174	175	QP Solai	PolG	0	0	0	74	34	0	0	85
HE 240 A	174	175	QV Solai	PolG	34	0	0	85	128	0	0	88
HE 240 A	174	175	QV Solai	PolG	128	0	0	88	178	0	0	75
HE 240 A	174	175	QV Solai	PolG	0	0	0	24	34	0	0	27
HE 240 A	174	175	QV Solai	PolG	34	0	0	27	128	0	0	28
HE 240 A	174	175	QV Solai	PolG	128	0	0	28	178	0	0	24
HE 240 A	174	175	Neve	PolG	0	0	0	20	128	0	0	30
HE 240 A	174	175	Neve	PolG	128	0	0	30	178	0	0	25
HE 240 A	174	175	Neve	PolG	0	0	0	26	34	0	0	30
HE 240 A	174	175	Vento X	PolG	34	0	0	30	178	0	0	21
HE 240 A	174	175	Vento X	PolG	0	0	0	31	128	0	0	47
HE 240 A	174	175	Vento X	PolG	128	0	0	47	178	0	0	39
HE 240 A	174	175	Vento X	PolG	0	0	0	40	34	0	0	46
HE 240 A	174	175	Carichi termici	Termico	34	0	0	46	178	0	0	33
HE 240 A	175	176	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	175	176	QP Solai	PolG	0	0	0	76	22	0	0	85
HE 240 A	175	176	QP Solai	PolG	22	0	0	85	116	0	0	88
HE 240 A	175	176	QP Solai	PolG	116	0	0	88	151	0	0	77
HE 240 A	175	176	QV Solai	PolG	0	0	0	24	22	0	0	27
HE 240 A	175	176	QV Solai	PolG	22	0	0	27	116	0	0	28
HE 240 A	175	176	QV Solai	PolG	116	0	0	28	151	0	0	25
HE 240 A	175	176	Neve	PolG	0	0	0	27	22	0	0	30
HE 240 A	175	176	Neve	PolG	22	0	0	30	151	0	0	21
HE 240 A	175	176	Neve	PolG	0	0	0	20	116	0	0	31
HE 240 A	175	176	Vento X	PolG	116	0	0	31	151	0	0	27
HE 240 A	175	176	Vento X	PolG	0	0	0	31	116	0	0	48
HE 240 A	175	176	Vento X	PolG	116	0	0	48	151	0	0	41
HE 240 A	175	176	Vento X	PolG	0	0	0	42	22	0	0	47
HE 240 A	175	176	Vento X	PolG	22	0	0	47	151	0	0	33
HE 240 A	176	177	Carichi termici	Termico	0	0	0	60	148	0	0	60
HE 240 A	176	177	Peso Proprio	UnifG	0	0	0	79	14	0	0	84
HE 240 A	176	177	QP Solai	PolG	14	0	0	84	119	0	0	88
HE 240 A	176	177	QP Solai	PolG	119	0	0	88	148	0	0	79
HE 240 A	176	177	QV Solai	PolG	0	0	0	25	14	0	0	27
HE 240 A	176	177	QV Solai	PolG	14	0	0	27	119	0	0	28
HE 240 A	176	177	Neve	PolG	119	0	0	28	148	0	0	25
HE 240 A	176	177	Neve	PolG	0	0	0	29	14	0	0	31
HE 240 A	176	177	Neve	PolG	14	0	0	31	148	0	0	21
HE 240 A	176	177	Neve	PolG	0	0	0	20	119	0	0	32
HE 240 A	176	177	Neve	PolG	119	0	0	32	148	0	0	28
HE 240 A	176	177	Vento X	PolG	0	0	0	44	14	0	0	48
HE 240 A	176	177	Vento X	PolG	14	0	0	48	148	0	0	33
HE 240 A	176	177	Vento X	PolG	0	0	0	31	119	0	0	49
HE 240 A	176	177	Vento X	PolG	119	0	0	49	148	0	0	43
HE 240 A	176	177	Carichi termici	Termico	0	0	0	60	134	0	0	60
HE 240 A	177	35	Peso Proprio	UnifG	0	0	0	81	7	0	0	84
HE 240 A	177	35	QP Solai	PolG	7	0	0	84	114	0	0	88
HE 240 A	177	35	QP Solai	PolG	114	0	0	88	134	0	0	81
HE 240 A	177	35	QV Solai	PolG	0	0	0	26	7	0	0	27
HE 240 A	177	35	QV Solai	PolG	7	0	0	27	114	0	0	2

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	177	35	Neve	PolG	114	0	0	32	134	0	0	29
HE 240 A	177	35	Neve	PolG	7	0	0	30	7	0	0	31
HE 240 A	177	35	Vento X	PolG	7	0	0	31	134	0	0	21
HE 240 A	177	35	Vento X	PolG	7	0	0	47	7	0	0	48
HE 240 A	177	35	Vento X	PolG	7	0	0	48	134	0	0	33
HE 240 A	177	35	Vento X	PolG	114	0	0	31	114	0	0	50
HE 240 A	177	35	Carichi termici	Termico	114	0	0	50	134	0	0	45
HE 240 A	361	362	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
HE 240 A	361	362	QP Solai	PolG	0	0	0	84	106	0	0	89
HE 240 A	361	362	QP Solai	PolG	106	0	0	89	108	0	0	88
HE 240 A	361	362	QP Solai	PolG	0	0	0	27	106	0	0	29
HE 240 A	361	362	Neve	PolG	106	0	0	29	108	0	0	28
HE 240 A	361	362	Neve	PolG	106	0	0	34	108	0	0	34
HE 240 A	361	362	Neve	PolG	106	0	0	32	108	0	0	33
HE 240 A	361	362	Vento X	PolG	0	0	0	31	106	0	0	21
HE 240 A	361	362	Vento X	PolG	106	0	0	52	108	0	0	52
HE 240 A	361	362	Vento X	PolG	0	0	0	49	108	0	0	33
HE 240 A	361	362	Vento X	Termico	0	0	0	60	112	0	0	60
HE 240 A	362	344	Carichi termici	UnifG	0	0	0	84	112	0	0	89
HE 240 A	362	344	Peso Proprio	PolG	0	0	0	27	112	0	0	29
HE 240 A	362	344	QP Solai	PolG	0	0	0	32	112	0	0	21
HE 240 A	362	344	Neve	PolG	0	0	0	20	112	0	0	34
HE 240 A	362	344	Neve	PolG	0	0	0	49	112	0	0	33
HE 240 A	362	344	Vento X	PolG	0	0	0	31	112	0	0	53
HE 240 A	362	344	Vento X	PolG	0	0	0	31	112	0	0	53

Trave 8018

HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	0	53	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	QP Solai	PolG	16	0	0	83	142	0	0	83
HE 240 A	0	0	QP Solai	PolG	142	0	0	86	178	0	0	86
HE 240 A	0	0	QP Solai	PolG	133	0	0	87	148	0	0	87
HE 240 A	0	0	QP Solai	PolG	6	0	0	81	6	0	0	83
HE 240 A	0	0	QP Solai	PolG	129	0	0	83	129	0	0	86
HE 240 A	0	53	QP Solai	PolG	0	0	0	86	151	0	0	80
HE 240 A	0	0	QP Solai	PolG	127	0	0	87	134	0	0	85
HE 240 A	0	0	QP Solai	PolG	0	0	0	76	25	0	0	83
HE 240 A	0	0	QP Solai	PolG	25	0	0	83	134	0	0	85
HE 240 A	0	0	QP Solai	PolG	134	0	0	85	174	0	0	76
HE 240 A	0	0	QP Solai	PolG	174	0	0	76	178	0	0	75
HE 240 A	0	0	QP Solai	PolG	133	0	0	27	133	0	0	28
HE 240 A	0	0	QP Solai	PolG	0	0	0	28	148	0	0	26
HE 240 A	0	0	QP Solai	PolG	25	0	0	24	25	0	0	27
HE 240 A	0	0	QP Solai	PolG	134	0	0	27	134	0	0	27
HE 240 A	0	0	QP Solai	PolG	174	0	0	27	174	0	0	24
HE 240 A	0	0	QP Solai	PolG	0	0	0	24	178	0	0	24
HE 240 A	0	0	QP Solai	PolG	6	0	0	27	129	0	0	28
HE 240 A	0	0	QP Solai	PolG	129	0	0	28	151	0	0	26
HE 240 A	0	0	QP Solai	PolG	16	0	0	25	16	0	0	27
HE 240 A	0	0	QP Solai	PolG	142	0	0	28	178	0	0	25
HE 240 A	0	53	QP Solai	PolG	127	0	0	26	127	0	0	28
HE 240 A	0	0	Neve	PolG	0	0	0	23	134	0	0	27
HE 240 A	0	53	Neve	PolG	134	0	0	29	178	0	0	23
HE 240 A	0	53	Neve	PolG	0	0	0	23	127	0	0	30

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Neve	PolG	129	0	0	23	129	0	0	29
HE 240 A	0	0	Neve	PolG	0	0	0	29	151	0	0	26
HE 240 A	0	0	Neve	PolG	142	0	0	23	142	0	0	29
HE 240 A	0	0	Neve	PolG	142	0	0	29	178	0	0	25
HE 240 A	0	0	Neve	PolG	0	0	0	29	148	0	0	24
HE 240 A	0	0	Neve	PolG	6	0	0	27	6	0	0	29
HE 240 A	0	53	Neve	PolG	0	0	0	29	151	0	0	24
HE 240 A	0	0	Neve	PolG	0	0	0	29	134	0	0	24
HE 240 A	0	0	Neve	PolG	133	0	0	30	148	0	0	28
HE 240 A	0	0	Neve	PolG	16	0	0	26	16	0	0	28
HE 240 A	0	0	Neve	PolG	0	0	0	28	178	0	0	24
HE 240 A	0	0	Neve	PolG	25	0	0	24	25	0	0	23
HE 240 A	0	0	Vento X	PolG	174	0	0	23	178	0	0	23
HE 240 A	0	0	Vento X	PolG	0	0	0	38	25	0	0	43
HE 240 A	0	0	Vento X	PolG	25	0	0	43	174	0	0	36
HE 240 A	0	0	Vento X	PolG	174	0	0	36	178	0	0	36
HE 240 A	0	0	Vento X	PolG	16	0	0	40	16	0	0	44
HE 240 A	0	53	Vento X	PolG	0	0	0	35	127	0	0	46
HE 240 A	0	53	Vento X	PolG	127	0	0	46	134	0	0	45
HE 240 A	0	53	Vento X	PolG	0	0	0	44	134	0	0	37
HE 240 A	0	0	Vento X	PolG	133	0	0	46	148	0	0	43
HE 240 A	0	0	Vento X	PolG	0	0	0	35	129	0	0	45
HE 240 A	0	0	Vento X	PolG	129	0	0	45	151	0	0	40
HE 240 A	0	0	Vento X	PolG	0	0	0	44	148	0	0	37
HE 240 A	0	0	Vento X	PolG	142	0	0	45	178	0	0	38
HE 240 A	0	0	Vento X	PolG	134	0	0	35	134	0	0	44
HE 240 A	0	0	Vento X	PolG	0	0	0	44	178	0	0	36
HE 240 A	0	0	Vento X	PolG	6	0	0	43	6	0	0	44
HE 240 A	0	0	Carichi termici	Termico	0	0	0	44	151	0	0	37
HE 240 A	0	0	Carichi termici	Termico	0	0	0	44	148	0	0	37
HE 240 A	0	0	Carichi termici	Termico	0	0	0	44	178	0	0	45
HE 240 A	0	0	Carichi termici	Termico	0	0	0	44	178	0	0	44
HE 240 A	0	0	Carichi termici	Termico	0	0	0	44	178	0	0	44
HE 240 A	0	53	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	53	54	QP Solai	PolG	0	0	0	83	123	0	0	87
HE 240 A	53	54	QP Solai	PolG	0	0	0	26	123	0	0	28
HE 240 A	53	54	QP Solai	PolG	0	0	0	23	123	0	0	30
HE 240 A	53	54	Neve	PolG	0	0	0	29	113	0	0	24
HE 240 A	53	54	Neve	PolG	0	0	0	23	113	0	0	30
HE 240 A	53	54	Vento X	PolG	0	0	0	44	113	0	0	37
HE 240 A	53	54	Vento X	PolG	0	0	0	35	123	0	0	47
HE 240 A	53	54	Vento X	PolG	0	0	0	44	123	0	0	37
HE 240 A	53	54	Carichi termici	Termico	0	0	0	60	113	0	0	60
HE 240 A	54	379	Peso Proprio	UnifG	0	0	0	83	113	0	0	87
HE 240 A	54	379	QP Solai	PolG	0	0	0	26	113	0	0	28
HE 240 A	54	379	QP Solai	PolG	0	0	0	29	113	0	0	24
HE 240 A	54	379	Neve	PolG	0	0	0	23	113	0	0	30
HE 240 A	54	379	Vento X	PolG	0	0	0	44	113	0	0	37
HE 240 A	54	379	Vento X	PolG	0	0	0	35	113	0	0	47
HE 240 A	54	379	Carichi termici	Termico	0	0	0	60	182	0	0	60
HE 240 A	119	0	Peso Proprio	UnifG	0	0	0	73	35	0	0	84
HE 240 A	119	0	QP Solai	PolG	35	0	0	84	128	0	0	83
HE 240 A	119	0	QP Solai	PolG	128	0	0	83	167	0	0	73
HE 240 A	119	0	QP Solai	PolG	167	0	0	73	182	0	0	70
HE 240 A	119	0	QP Solai	PolG	0	0	0	24	35	0	0	27
HE 240 A	119	0	QP Solai	PolG	35	0	0	27	128	0	0	27
HE 240 A	119	0	QP Solai	PolG	128	0	0	27	167	0	0	23
HE 240 A	119	0	Neve	PolG	167	0	0	23	182	0	0	28
HE 240 A	119	0	Neve	PolG	128	0	0	28	182	0	0	22

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	119	0	Neve	PolG	0	0	0	23	35	0	0	28
					35	0	0	28	167	0	0	22
HE 240 A	119	0	Vento X	PolG	0	0	0	22	182	0	0	22
					167	0	0	35	128	0	0	44
HE 240 A	119	0	Vento X	PolG	0	0	0	44	182	0	0	34
					128	0	0	35	35	0	0	43
HE 240 A	119	0			35	0	0	43	167	0	0	34
					167	0	0	34	182	0	0	34
HE 240 A	119	0	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	379	380	Peso Proprio	UnifG	0	0	0	60	108	0	0	60
HE 240 A	379	380	QP Solai	PolG	0	0	0	83	108	0	0	87
HE 240 A	379	380	QV Solai	PolG	0	0	0	26	108	0	0	28
HE 240 A	379	380	Neve	PolG	0	0	0	29	108	0	0	24
HE 240 A	379	380	Neve	PolG	0	0	0	23	108	0	0	30
HE 240 A	379	380	Vento X	PolG	0	0	0	35	108	0	0	47
HE 240 A	379	380	Vento X	PolG	0	0	0	44	108	0	0	37
HE 240 A	379	380	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	380	345	Peso Proprio	UnifG	0	0	0	60	112	0	0	60
HE 240 A	380	345	QP Solai	PolG	0	0	0	83	112	0	0	87
HE 240 A	380	345	QV Solai	PolG	0	0	0	26	112	0	0	28
HE 240 A	380	345	Neve	PolG	0	0	0	29	112	0	0	24
HE 240 A	380	345	Neve	PolG	0	0	0	23	112	0	0	30
HE 240 A	380	345	Vento X	PolG	0	0	0	44	112	0	0	37
HE 240 A	380	345	Vento X	PolG	0	0	0	35	112	0	0	47
HE 240 A	380	345	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	0	59	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	59	QP Solai	PolG	0	0	0	82	134	0	0	87
HE 240 A	0	0	QP Solai	PolG	0	0	0	82	145	0	0	86
					145	0	0	86	151	0	0	84
HE 240 A	0	0	QP Solai	PolG	0	0	0	82	160	0	0	83
					160	0	0	83	163	0	0	83
					163	0	0	83	178	0	0	80
HE 240 A	0	0	QP Solai	PolG	0	0	0	79	3	0	0	80
					3	0	0	80	7	0	0	81
					7	0	0	81	151	0	0	81
					151	0	0	81	153	0	0	80
					153	0	0	80	178	0	0	75
HE 240 A	0	0	QP Solai	PolG	0	0	0	82	148	0	0	87
HE 240 A	0	59	QV Solai	PolG	0	0	0	26	134	0	0	28
HE 240 A	0	0	QV Solai	PolG	0	0	0	26	145	0	0	27
					145	0	0	27	151	0	0	27
HE 240 A	0	0	QV Solai	PolG	0	0	0	26	160	0	0	27
					160	0	0	27	178	0	0	26
HE 240 A	0	0	QV Solai	PolG	0	0	0	26	148	0	0	28
HE 240 A	0	0	QV Solai	PolG	0	0	0	25	3	0	0	26
					3	0	0	26	7	0	0	26
					7	0	0	26	151	0	0	26
					151	0	0	26	153	0	0	26
					153	0	0	26	178	0	0	24
HE 240 A	0	0	Neve	PolG	0	0	0	25	148	0	0	27
HE 240 A	0	0	Neve	PolG	0	0	0	26	151	0	0	26
HE 240 A	0	0	Neve	PolG	0	0	0	26	148	0	0	27
HE 240 A	0	0	Neve	PolG	0	0	0	25	3	0	0	25
					3	0	0	25	151	0	0	27
					151	0	0	27	178	0	0	27
HE 240 A	0	59	Neve	PolG	0	0	0	26	134	0	0	27
HE 240 A	0	0	Neve	PolG	0	0	0	24	7	0	0	26
					7	0	0	26	153	0	0	23
					153	0	0	23	178	0	0	23
HE 240 A	0	0	Neve	PolG	0	0	0	25	160	0	0	27
					160	0	0	27	178	0	0	25

Sezione	Ni	NF	Cond.	Tipoc	Xi	QXi	QYi	QZi	Xf	QXF	QYf	QZF
HE 240 A	0	59	Neve	PolG	0	0	0	25	134	0	0	27
HE 240 A	0	0	Neve	PolG	0	0	0	26	163	0	0	25
HE 240 A	0	0	Neve	PolG	163	0	0	25	178	0	0	25
HE 240 A	0	0	Neve	PolG	0	0	0	25	145	0	0	27
HE 240 A	0	0	Vento X	PolG	145	0	0	27	151	0	0	26
HE 240 A	0	0	Vento X	PolG	0	0	0	39	160	0	0	42
HE 240 A	0	0	Vento X	PolG	160	0	0	42	178	0	0	38
HE 240 A	0	0	Vento X	PolG	0	0	0	38	3	0	0	38
					3	0	0	38	151	0	0	42
HE 240 A	0	0	Vento X	PolG	151	0	0	42	178	0	0	36
HE 240 A	0	0	Vento X	PolG	0	0	0	39	148	0	0	42
HE 240 A	0	0	Vento X	PolG	0	0	0	40	151	0	0	40
HE 240 A	0	59	Vento X	PolG	0	0	0	40	134	0	0	41
HE 240 A	0	59	Vento X	PolG	0	0	0	39	134	0	0	42
HE 240 A	0	0	Vento X	PolG	0	0	0	40	148	0	0	41
HE 240 A	0	0	Vento X	PolG	0	0	0	38	7	0	0	40
					7	0	0	40	153	0	0	36
HE 240 A	0	0	Vento X	PolG	153	0	0	36	178	0	0	36
HE 240 A	0	0	Vento X	PolG	0	0	0	40	163	0	0	38
HE 240 A	0	0	Vento X	PolG	163	0	0	38	178	0	0	38
HE 240 A	0	0	Vento X	PolG	0	0	0	39	145	0	0	42
					145	0	0	42	151	0	0	40
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	59	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	59	60	QP Solai	PolG	0	0	0	82	123	0	0	87
HE 240 A	59	60	QV Solai	PolG	0	0	0	26	123	0	0	28
HE 240 A	59	60	Neve	PolG	0	0	0	25	123	0	0	27
HE 240 A	59	60	Neve	PolG	0	0	0	26	123	0	0	27
HE 240 A	59	60	Vento X	PolG	0	0	0	39	123	0	0	42
HE 240 A	59	60	Vento X	PolG	0	0	0	40	123	0	0	41
HE 240 A	59	60	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	60	385	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	60	385	QP Solai	PolG	0	0	0	82	113	0	0	87
HE 240 A	60	385	QV Solai	PolG	0	0	0	26	113	0	0	28
HE 240 A	60	385	Neve	PolG	0	0	0	26	113	0	0	27
HE 240 A	60	385	Neve	PolG	0	0	0	25	113	0	0	27
HE 240 A	60	385	Vento X	PolG	0	0	0	40	113	0	0	41
HE 240 A	60	385	Vento X	PolG	0	0	0	39	113	0	0	42
HE 240 A	60	385	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
HE 240 A	120	0	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	120	0	QP Solai	PolG	0	0	0	74	13	0	0	78
					13	0	0	78	18	0	0	79
					18	0	0	79	144	0	0	78
					144	0	0	78	146	0	0	78
HE 240 A	120	0	QV Solai	PolG	146	0	0	78	182	0	0	71
					13	0	0	24	13	0	0	25
					13	0	0	25	18	0	0	25
					18	0	0	25	144	0	0	25
					144	0	0	25	146	0	0	25
HE 240 A	120	0	Neve	PolG	146	0	0	25	182	0	0	23
					18	0	0	23	18	0	0	26
					146	0	0	22	146	0	0	22
HE 240 A	120	0	Neve	PolG	0	0	0	23	13	0	0	23
					0	0	0	23	13	0	0	23
HE 240 A	120	0	Vento X	PolG	13	0	0	23	144	0	0	27
					13	0	0	27	182	0	0	22
HE 240 A	120	0	Vento X	PolG	144	0	0	36	13	0	0	36
					13	0	0	36	144	0	0	42
					144	0	0	42	182	0	0	34
HE 240 A	120	0	Vento X	PolG	0	0	0	35	18	0	0	40
					18	0	0	40	146	0	0	33
					146	0	0	33	182	0	0	34

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYL	QZi	Xf	QXf	QYf	QZf
HE 240 A	120	0	Carichi termici	Termico	0	0	0	60	108	0	0	60
HE 240 A	385	386	Peso Proprio	UnifG	0	0	0	82	108	0	0	87
HE 240 A	385	386	QP Solai	PolG	0	0	0	26	108	0	0	28
HE 240 A	385	386	QV Solai	PolG	0	0	0	26	108	0	0	27
HE 240 A	385	386	Neve	PolG	0	0	0	25	108	0	0	27
HE 240 A	385	386	Neve	PolG	0	0	0	39	108	0	0	42
HE 240 A	385	386	Vento X	PolG	0	0	0	40	108	0	0	41
HE 240 A	385	386	Vento X	PolG	0	0	0	40	108	0	0	41
HE 240 A	385	386	Carichi termici	Termico	0	0	0	60	112	0	0	60
HE 240 A	386	346	Peso Proprio	UnifG	0	0	0	82	112	0	0	86
HE 240 A	386	346	QP Solai	PolG	0	0	0	26	112	0	0	28
HE 240 A	386	346	Neve	PolG	0	0	0	26	112	0	0	27
HE 240 A	386	346	Neve	PolG	0	0	0	25	112	0	0	27
HE 240 A	386	346	Vento X	PolG	0	0	0	39	112	0	0	42
HE 240 A	386	346	Vento X	PolG	0	0	0	40	112	0	0	41
HE 240 A	386	346	Carichi termici	Termico	0	0	0	60	134	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	82	134	0	0	86
HE 240 A	0	0	QP Solai	PolG	130	0	0	86	134	0	0	86
HE 240 A	0	0	QV Solai	PolG	136	0	0	84	148	0	0	83
HE 240 A	0	0	Neve	PolG	130	0	0	26	130	0	0	27
HE 240 A	0	0	QV Solai	PolG	130	0	0	27	134	0	0	27
HE 240 A	0	0	Neve	PolG	136	0	0	27	148	0	0	27
HE 240 A	0	0	Neve	PolG	136	0	0	23	136	0	0	24
HE 240 A	0	0	Neve	PolG	136	0	0	27	148	0	0	28
HE 240 A	0	0	Neve	PolG	130	0	0	28	148	0	0	24
HE 240 A	0	0	Neve	PolG	130	0	0	29	134	0	0	29
HE 240 A	0	0	Vento X	PolG	130	0	0	44	148	0	0	37
HE 240 A	0	0	Vento X	PolG	130	0	0	43	134	0	0	38
HE 240 A	0	0	Vento X	PolG	136	0	0	36	136	0	0	42
HE 240 A	0	0	Vento X	PolG	136	0	0	42	148	0	0	43
HE 240 A	0	0	Vento X	PolG	130	0	0	36	130	0	0	45
HE 240 A	0	0	Vento X	PolG	130	0	0	45	134	0	0	45
HE 240 A	0	0	Carichi termici	Termico	0	0	0	60	123	0	0	60
HE 240 A	45	46	Peso Proprio	UnifG	0	0	0	82	123	0	0	87
HE 240 A	45	46	QP Solai	PolG	0	0	0	26	123	0	0	28
HE 240 A	45	46	QV Solai	PolG	0	0	0	23	123	0	0	30
HE 240 A	45	46	Neve	PolG	0	0	0	28	123	0	0	24
HE 240 A	45	46	Neve	PolG	0	0	0	43	123	0	0	38
HE 240 A	45	46	Vento X	PolG	0	0	0	36	123	0	0	46
HE 240 A	45	46	Carichi termici	Termico	0	0	0	60	113	0	0	60
HE 240 A	46	371	Peso Proprio	UnifG	0	0	0	82	113	0	0	87
HE 240 A	46	371	QP Solai	PolG	0	0	0	26	113	0	0	28
HE 240 A	46	371	QV Solai	PolG	0	0	0	23	113	0	0	30
HE 240 A	46	371	Neve	PolG	0	0	0	28	113	0	0	24
HE 240 A	46	371	Neve	PolG	0	0	0	36	113	0	0	46
HE 240 A	46	371	Vento X	PolG	0	0	0	43	113	0	0	38
HE 240 A	46	371	Vento X	PolG	0	0	0	60	182	0	0	60
HE 240 A	121	198	Peso Proprio	UnifG	0	0	0	74	34	0	0	74
HE 240 A	121	198	QP Solai	PolG	34	0	0	74	131	0	0	74
HE 240 A			QV Solai	PolG	131	0	0	74	163	0	0	75
HE 240 A			Neve	PolG	163	0	0	75	182	0	0	70
HE 240 A	121	198	QV Solai	PolG	163	0	0	24	163	0	0	24
HE 240 A	121	198	Neve	PolG	163	0	0	24	182	0	0	23
HE 240 A	121	198	Vento X	PolG	0	0	0	23	34	0	0	23

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	121	198	Neve	PolG	163	0	0	25	163	0	0	25
HE 240 A	121	198	Vento X	PolG	131	0	0	22	182	0	0	22
HE 240 A	121	198	Vento X	PolG	131	0	0	36	182	0	0	34
HE 240 A	121	198	Vento X	PolG	131	0	0	34	182	0	0	34
HE 240 A	121	198	Vento X	PolG	34	0	0	36	163	0	0	38
HE 240 A	121	198	Vento X	PolG	163	0	0	38	182	0	0	34
HE 240 A	121	198	Carichi termici	Termico	0	0	0	60	178	0	0	60
HE 240 A	198	199	Peso Proprio	UnifG	0	0	0	76	170	0	0	77
HE 240 A	198	199	QP Solai	PolG	170	0	0	77	178	0	0	75
HE 240 A	198	199	QV Solai	PolG	0	0	0	24	178	0	0	24
HE 240 A	198	199	Neve	PolG	0	0	0	23	178	0	0	23
HE 240 A	198	199	Neve	PolG	0	0	0	24	170	0	0	24
HE 240 A	198	199	Vento X	PolG	170	0	0	24	178	0	0	23
HE 240 A	198	199	Vento X	PolG	0	0	0	36	178	0	0	36
HE 240 A	198	199	Vento X	PolG	0	0	0	38	170	0	0	38
HE 240 A	198	199	Carichi termici	Termico	0	0	0	60	178	0	0	60
HE 240 A	199	200	Peso Proprio	UnifG	0	0	0	79	14	0	0	79
HE 240 A	199	200	QP Solai	PolG	14	0	0	79	146	0	0	79
HE 240 A	199	200	QV Solai	PolG	146	0	0	25	178	0	0	25
HE 240 A	199	200	Neve	PolG	0	0	0	26	14	0	0	26
HE 240 A	199	200	Neve	PolG	14	0	0	23	146	0	0	25
HE 240 A	199	200	Vento X	PolG	146	0	0	25	178	0	0	25
HE 240 A	199	200	Vento X	PolG	0	0	0	36	146	0	0	38
HE 240 A	199	200	Vento X	PolG	146	0	0	38	178	0	0	38
HE 240 A	199	200	Vento X	PolG	0	0	0	40	14	0	0	40
HE 240 A	199	200	Carichi termici	Termico	0	0	0	60	151	0	0	60
HE 240 A	200	0	Peso Proprio	UnifG	0	0	0	81	4	0	0	82
HE 240 A	200	0	QP Solai	PolG	4	0	0	82	132	0	0	81
HE 240 A	200	0	QV Solai	PolG	132	0	0	81	151	0	0	81
HE 240 A	200	0	Neve	PolG	4	0	0	26	4	0	0	26
HE 240 A	200	0	Neve	PolG	132	0	0	26	132	0	0	26
HE 240 A	200	0	Vento X	PolG	4	0	0	23	132	0	0	26
HE 240 A	200	0	Vento X	PolG	132	0	0	27	4	0	0	28
HE 240 A	200	0	Vento X	PolG	4	0	0	28	151	0	0	24
HE 240 A	200	0	Vento X	PolG	4	0	0	42	4	0	0	43
HE 240 A	200	0	Vento X	PolG	4	0	0	43	151	0	0	37
HE 240 A	200	0	Vento X	PolG	132	0	0	36	132	0	0	40
HE 240 A	200	0	Carichi termici	Termico	0	0	0	60	108	0	0	60
HE 240 A	371	372	Peso Proprio	UnifG	0	0	0	82	108	0	0	87
HE 240 A	371	372	QP Solai	PolG	0	0	0	26	108	0	0	28
HE 240 A	371	372	QV Solai	PolG	0	0	0	23	108	0	0	30
HE 240 A	371	372	Neve	PolG	0	0	0	28	108	0	0	24
HE 240 A	371	372	Neve	PolG	0	0	0	36	108	0	0	46
HE 240 A	371	372	Vento X	PolG	0	0	0	43	108	0	0	38
HE 240 A	371	372	Vento X	PolG	0	0	0	60	112	0	0	60
HE 240 A	372	347	Peso Proprio	UnifG	0	0	0	82	112	0	0	87
HE 240 A	372	347	QP Solai	PolG	0	0	0	26	112	0	0	28
HE 240 A	372	347	QV Solai	PolG	0	0	0	23	112	0	0	30
HE 240 A	372	347	Neve	PolG	0	0	0	28	112	0	0	24
HE 240 A	372	347	Neve	PolG	0	0	0	43	112	0	0	38
HE 240 A	372	347	Vento X	PolG	0	0	0	36	112	0	0	46

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	372	347		Termico	ΔXY=15°C, ΔXZ=15°C							
Trave 8021												
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	148	0	0	60
HE 240 A	0	61	Peso Proprio	UnitG	0	0	0	60	134	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	0	61	QP Solai	PolG	4	0	0	82	4	0	0	83
HE 240 A	0	0			116	0	0	83	116	0	0	83
HE 240 A	0	0	QP Solai	PolG	0	0	0	75	30	0	0	77
HE 240 A	0	0			30	0	0	77	131	0	0	77
HE 240 A	0	0	QP Solai	PolG	0	0	0	72	178	0	0	75
HE 240 A	0	0			39	0	0	74	123	0	0	74
HE 240 A	0	0	QP Solai	PolG	0	0	0	80	12	0	0	81
HE 240 A	0	0			12	0	0	81	121	0	0	81
HE 240 A	0	0	QP Solai	PolG	0	0	0	77	19	0	0	79
HE 240 A	0	0			19	0	0	79	118	0	0	79
HE 240 A	0	61	QV Solai	PolG	0	0	0	26	4	0	0	26
HE 240 A	0	0			4	0	0	26	116	0	0	27
HE 240 A	0	0	QV Solai	PolG	0	0	0	27	134	0	0	26
HE 240 A	0	0			30	0	0	24	30	0	0	25
HE 240 A	0	0			30	0	0	25	131	0	0	25
HE 240 A	0	0	QV Solai	PolG	0	0	0	25	178	0	0	24
HE 240 A	0	0			39	0	0	24	123	0	0	24
HE 240 A	0	0	QV Solai	PolG	0	0	0	26	12	0	0	26
HE 240 A	0	0			12	0	0	26	121	0	0	26
HE 240 A	0	0	QV Solai	PolG	0	0	0	25	19	0	0	25
HE 240 A	0	0			19	0	0	25	118	0	0	25
HE 240 A	0	0	Neve	PolG	0	0	0	25	151	0	0	25
HE 240 A	0	61	Neve	PolG	0	0	0	30	4	0	0	30
HE 240 A	0	61	Neve	PolG	0	0	0	30	134	0	0	22
HE 240 A	0	0	Neve	PolG	0	0	0	29	134	0	0	29
HE 240 A	0	0	Neve	PolG	0	0	0	21	121	0	0	28
HE 240 A	0	0	Neve	PolG	0	0	0	28	148	0	0	28
HE 240 A	0	0	Neve	PolG	0	0	0	26	30	0	0	26
HE 240 A	0	0	Neve	PolG	0	0	0	29	12	0	0	22
HE 240 A	0	0	Neve	PolG	0	0	0	29	148	0	0	22
HE 240 A	0	0	Neve	PolG	0	0	0	21	118	0	0	26
HE 240 A	0	0	Neve	PolG	0	0	0	26	151	0	0	26
HE 240 A	0	0	Neve	PolG	0	0	0	21	123	0	0	23
HE 240 A	0	0	Neve	PolG	0	0	0	23	178	0	0	24
HE 240 A	0	0	Neve	PolG	0	0	0	25	178	0	0	25
HE 240 A	0	0	Neve	PolG	0	0	0	27	19	0	0	27
HE 240 A	0	0	Vento X	PolG	0	0	0	32	131	0	0	38
HE 240 A	0	0	Vento X	PolG	0	0	0	32	178	0	0	39
HE 240 A	0	0	Vento X	PolG	0	0	0	40	151	0	0	40
HE 240 A	0	61	Vento X	PolG	0	0	0	47	4	0	0	47
HE 240 A	0	0	Vento X	PolG	4	0	0	47	134	0	0	34
HE 240 A	0	0	Vento X	PolG	0	0	0	37	39	0	0	38
HE 240 A	0	0	Vento X	PolG	39	0	0	38	178	0	0	33

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Vento X	PolG	30	0	0	40	178	0	0	33
HE 240 A	0	0	Vento X	PolG	123	0	0	36	178	0	0	37
HE 240 A	0	0	Vento X	PolG	121	0	0	43	148	0	0	43
HE 240 A	0	0	Vento X	PolG	19	0	0	42	151	0	0	42
HE 240 A	0	0	Vento X	PolG	12	0	0	44	12	0	0	45
HE 240 A	0	61	Vento X	PolG	0	0	0	32	116	0	0	45
HE 240 A	0	0			116	0	0	45	134	0	0	45
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	61	62	Peso Proprio	UnitG	0	0	0	60	123	0	0	60
HE 240 A	61	62	QP Solai	PolG	0	0	0	84	111	0	0	85
HE 240 A	61	62	QV Solai	PolG	0	0	0	85	123	0	0	84
HE 240 A	61	62	Neve	PolG	111	0	0	27	111	0	0	27
HE 240 A	61	62	Neve	PolG	0	0	0	21	111	0	0	30
HE 240 A	61	62	Neve	PolG	0	0	0	30	123	0	0	31
HE 240 A	61	62	Vento X	PolG	0	0	0	31	123	0	0	22
HE 240 A	61	62	Vento X	PolG	0	0	0	48	123	0	0	34
HE 240 A	61	62			111	0	0	32	111	0	0	47
HE 240 A	61	62	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	62	387	Peso Proprio	UnitG	0	0	0	60	113	0	0	60
HE 240 A	62	387	QP Solai	PolG	0	0	0	84	107	0	0	87
HE 240 A	62	387	QV Solai	PolG	107	0	0	87	113	0	0	86
HE 240 A	62	387	Neve	PolG	0	0	0	27	107	0	0	28
HE 240 A	62	387	Neve	PolG	107	0	0	28	113	0	0	28
HE 240 A	62	387	Neve	PolG	0	0	0	31	113	0	0	22
HE 240 A	62	387	Neve	PolG	0	0	0	21	107	0	0	32
HE 240 A	62	387	Vento X	PolG	107	0	0	32	113	0	0	32
HE 240 A	62	387	Vento X	PolG	0	0	0	48	113	0	0	34
HE 240 A	62	387	Vento X	PolG	0	0	0	32	107	0	0	49
HE 240 A	62	387	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	122	0	Peso Proprio	UnitG	0	0	0	60	182	0	0	60
HE 240 A	122	0	QP Solai	PolG	0	0	0	70	48	0	0	71
HE 240 A	122	0	QV Solai	PolG	48	0	0	71	119	0	0	71
HE 240 A	122	0	Neve	PolG	119	0	0	71	182	0	0	23
HE 240 A	122	0	Neve	PolG	0	0	0	22	182	0	0	23
HE 240 A	122	0	Neve	PolG	48	0	0	23	182	0	0	22
HE 240 A	122	0	Vento X	PolG	0	0	0	21	182	0	0	22
HE 240 A	122	0	Vento X	PolG	0	0	0	35	48	0	0	36
HE 240 A	122	0	Vento X	PolG	48	0	0	36	182	0	0	33
HE 240 A	122	0	Vento X	PolG	0	0	0	32	119	0	0	34
HE 240 A	122	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	387	388	Peso Proprio	UnitG	0	0	0	60	108	0	0	60
HE 240 A	387	388	QP Solai	PolG	0	0	0	84	107	0	0	89
HE 240 A	387	388	QV Solai	PolG	107	0	0	35	108	0	0	35
HE 240 A	387	388	Neve	PolG	0	0	0	27	107	0	0	28
HE 240 A	387	388	Neve	PolG	107	0	0	11	108	0	0	11
HE 240 A	387	388	Neve	PolG	0	0	0	31	108	0	0	22
HE 240 A	387	388	Vento X	PolG	0	0	0	21	107	0	0	33
HE 240 A	387	388	Vento X	PolG	0	0	0	32	107	0	0	51
HE 240 A	387	388	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	388	348	Peso Proprio	UnitG	0	0	0	60	112	0	0	60
HE 240 A	388	348	QP Solai	PolG	0	0	0	84	112	0	0	89

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	388	348	QV Solai	PolG	0	0	0	27	112	0	0	29
HE 240 A	388	348	Neve	PolG	0	0	0	31	112	0	0	22
HE 240 A	388	348	Neve	PolG	0	0	0	21	112	0	0	34
HE 240 A	388	348	Vento X	PolG	0	0	0	48	112	0	0	34
HE 240 A	388	348	Vento X	PolG	0	0	0	32	112	0	0	52
HE 240 A	388	348	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 8022												
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	51	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	0	0	QP Solai	PolG	45	0	0	71	45	0	0	76
					115	0	0	76	115	0	0	76
HE 240 A	0	0	QP Solai	PolG	0	0	0	69	52	0	0	71
					52	0	0	73	108	0	0	73
HE 240 A	0	0	QP Solai	PolG	108	0	0	73	178	0	0	69
					32	0	0	78	32	0	0	78
HE 240 A	0	51	QP Solai	PolG	104	0	0	78	104	0	0	78
					104	0	0	78	151	0	0	74
HE 240 A	0	0	QP Solai	PolG	0	0	0	78	18	0	0	82
					18	0	0	82	103	0	0	82
HE 240 A	0	0	QP Solai	PolG	103	0	0	82	134	0	0	78
					26	0	0	76	26	0	0	80
HE 240 A	0	0	QP Solai	PolG	26	0	0	80	107	0	0	80
					107	0	0	80	148	0	0	76
HE 240 A	0	0	QP Solai	PolG	0	0	0	23	45	0	0	24
					45	0	0	24	115	0	0	24
HE 240 A	0	51	QP Solai	PolG	115	0	0	24	178	0	0	23
					18	0	0	25	18	0	0	26
HE 240 A	0	0	QP Solai	PolG	18	0	0	26	103	0	0	26
					103	0	0	26	134	0	0	25
HE 240 A	0	0	QP Solai	PolG	0	0	0	24	32	0	0	25
					32	0	0	25	104	0	0	25
HE 240 A	0	0	QP Solai	PolG	104	0	0	25	151	0	0	24
					26	0	0	24	26	0	0	26
HE 240 A	0	0	QP Solai	PolG	26	0	0	26	107	0	0	26
					107	0	0	26	148	0	0	24
HE 240 A	0	0	QP Solai	PolG	0	0	0	22	52	0	0	23
					52	0	0	23	108	0	0	23
HE 240 A	0	51	Neve	PolG	108	0	0	23	178	0	0	22
					103	0	0	18	103	0	0	29
HE 240 A	0	0	Neve	PolG	103	0	0	29	134	0	0	29
					0	0	0	27	32	0	0	28
HE 240 A	0	0	Neve	PolG	32	0	0	28	151	0	0	19
					19	0	0	30	18	0	0	30
HE 240 A	0	51	Neve	PolG	0	0	0	30	134	0	0	19
					18	0	0	30	134	0	0	19
HE 240 A	0	0	Neve	PolG	0	0	0	24	52	0	0	25
					52	0	0	25	178	0	0	19
HE 240 A	0	0	Neve	PolG	0	0	0	18	115	0	0	25
					115	0	0	25	178	0	0	25
HE 240 A	0	0	Neve	PolG	0	0	0	26	45	0	0	26
					45	0	0	26	178	0	0	19
HE 240 A	0	0	Neve	PolG	0	0	0	18	107	0	0	28
					107	0	0	28	148	0	0	28
HE 240 A	0	0	Neve	PolG	0	0	0	18	104	0	0	26
					104	0	0	26	151	0	0	26
HE 240 A	0	0	Neve	PolG	0	0	0	18	108	0	0	23
					108	0	0	23	178	0	0	24
HE 240 A	0	0	Neve	PolG	0	0	0	29	26	0	0	29
					26	0	0	29	148	0	0	19
HE 240 A	0	0	Vento X	PolG	0	0	0	29	108	0	0	36
					108	0	0	36	178	0	0	37
HE 240 A	0	0	Vento X	PolG	0	0	0	29	115	0	0	38
					115	0	0	38	178	0	0	39

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Vento X	PolG	45	0	0	40	178	0	0	40
HE 240 A	0	0	Vento X	PolG	104	0	0	29	104	0	0	40
HE 240 A	0	0	Vento X	PolG	52	0	0	37	52	0	0	38
HE 240 A	0	0	Vento X	PolG	107	0	0	43	148	0	0	43
HE 240 A	0	0	Vento X	PolG	32	0	0	43	151	0	0	30
HE 240 A	0	51	Vento X	PolG	103	0	0	29	103	0	0	45
HE 240 A	0	0	Vento X	PolG	26	0	0	44	26	0	0	45
HE 240 A	0	51	Vento X	PolG	18	0	0	47	18	0	0	47
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	51	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	51	52	Peso Proprio	UnifG	0	0	0	60	123	0	0	60
HE 240 A	51	52	QP Solai	PolG	0	0	0	81	11	0	0	83
					98	0	0	84	123	0	0	80
HE 240 A	51	52	QV Solai	PolG	0	0	0	26	11	0	0	27
					11	0	0	27	98	0	0	27
HE 240 A	51	52	Neve	PolG	98	0	0	32	11	0	0	32
					11	0	0	32	123	0	0	19
HE 240 A	51	52	Neve	PolG	0	0	0	18	98	0	0	30
					98	0	0	30	123	0	0	31
HE 240 A	51	52	Vento X	PolG	0	0	0	49	11	0	0	49
					11	0	0	49	123	0	0	30
HE 240 A	51	52	Vento X	PolG	0	0	0	29	98	0	0	47
					98	0	0	47	123	0	0	48
HE 240 A	51	52	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	52	377	Peso Proprio	UnifG	0	0	0	60	113	0	0	60
HE 240 A	52	377	QP Solai	PolG	0	0	0	83	6	0	0	85
					6	0	0	85	95	0	0	86
HE 240 A	52	377	QV Solai	PolG	95	0	0	86	113	0	0	83
					6	0	0	27	6	0	0	27
HE 240 A	52	377	Neve	PolG	95	0	0	28	113	0	0	26
					95	0	0	18	95	0	0	32
HE 240 A	52	377	Neve	PolG	0	0	0	32	113	0	0	32
					6	0	0	33	113	0	0	33
HE 240 A	52	377	Vento X	PolG	6	0	0	51	6	0	0	19
					6	0	0	51	113	0	0	30
HE 240 A	52	377	Vento X	PolG	95	0	0	29	95	0	0	49
					95	0	0	49	113	0	0	50
HE 240 A	52	377	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	123	0	Peso Proprio	UnifG	0	0	0	60	182	0	0	60
HE 240 A	123	0	QP Solai	PolG	60	0	0	70	104	0	0	70
					104	0	0	70	182	0	0	67
HE 240 A	123	0	QV Solai	PolG	60	0	0	21	60	0	0	22
					104	0	0	22	182	0	0	21
HE 240 A	123	0	Neve	PolG	0	0	0	18	104	0	0	22
					104	0	0	22	182	0	0	22
HE 240 A	123	0	Neve	PolG	0	0	0	23	60	0	0	23
					60	0	0	23	182	0	0	19
HE 240 A	123	0	Vento X	PolG	0	0	0	29	104	0	0	33

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	123	0	Vento X	PolG	60	0	0	35	60	182	0	36
HE 240 A	123	0	Carichi termici	Termico	60	0	0	35	60	182	0	36
HE 240 A	377	378	Peso Proprio	UnifG	60	0	0	36	182	0	0	30
HE 240 A	377	378	QP Solai	PolG	0	0	0	60	108	0	0	60
HE 240 A	377	378	QV Solai	PolG	95	0	0	88	108	0	0	88
HE 240 A	377	378	Neve	PolG	0	0	0	27	95	0	0	28
HE 240 A	377	378	Neve	PolG	95	0	0	18	95	0	0	27
HE 240 A	377	378	Neve	PolG	95	0	0	33	108	0	0	34
HE 240 A	377	378	Vento X	PolG	0	0	0	35	108	0	0	19
HE 240 A	377	378	Vento X	PolG	0	0	0	29	95	0	0	52
HE 240 A	377	378	Vento X	PolG	95	0	0	52	108	0	0	52
HE 240 A	377	378	Vento X	PolG	0	0	0	54	108	0	0	30
HE 240 A	377	378	Vento X	PolG	0	0	0	60	112	0	0	60
HE 240 A	378	349	Carichi termici	Termico	103	0	0	86	103	0	0	89
HE 240 A	378	349	Peso Proprio	UnifG	103	0	0	89	112	0	0	87
HE 240 A	378	349	QP Solai	PolG	0	0	0	28	103	0	0	29
HE 240 A	378	349	QV Solai	PolG	103	0	0	29	112	0	0	28
HE 240 A	378	349	Neve	PolG	0	0	0	18	103	0	0	35
HE 240 A	378	349	Neve	PolG	103	0	0	35	112	0	0	35
HE 240 A	378	349	Neve	PolG	0	0	0	29	103	0	0	54
HE 240 A	378	349	Vento X	PolG	103	0	0	54	112	0	0	54
HE 240 A	378	349	Vento X	PolG	0	0	0	54	112	0	0	30
HE 240 A	378	349	Carichi termici	Termico	60	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	0	55	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	QP Solai	PolG	60	0	0	67	60	0	0	76
HE 240 A	0	0	QP Solai	PolG	102	0	0	76	102	0	0	68
HE 240 A	0	0	QP Solai	PolG	0	0	0	65	67	0	0	74
HE 240 A	0	0	QP Solai	PolG	67	0	0	74	96	0	0	74
HE 240 A	0	0	QP Solai	PolG	96	0	0	74	178	0	0	66
HE 240 A	0	0	QP Solai	PolG	0	0	0	70	46	0	0	78
HE 240 A	0	0	QP Solai	PolG	46	0	0	78	92	0	0	79
HE 240 A	0	0	QP Solai	PolG	92	0	0	79	151	0	0	70
HE 240 A	0	0	QP Solai	PolG	0	0	0	72	39	0	0	80
HE 240 A	0	0	QP Solai	PolG	39	0	0	80	95	0	0	81
HE 240 A	0	55	QP Solai	PolG	95	0	0	81	148	0	0	72
HE 240 A	0	0	QP Solai	PolG	0	0	0	75	30	0	0	82
HE 240 A	0	0	QP Solai	PolG	30	0	0	82	91	0	0	83
HE 240 A	0	0	QP Solai	PolG	91	0	0	83	134	0	0	75
HE 240 A	0	0	QP Solai	PolG	0	0	0	21	67	0	0	24
HE 240 A	0	0	QP Solai	PolG	67	0	0	24	96	0	0	24
HE 240 A	0	0	QP Solai	PolG	96	0	0	24	178	0	0	21
HE 240 A	0	0	QP Solai	PolG	0	0	0	22	60	0	0	24
HE 240 A	0	0	QP Solai	PolG	60	0	0	24	102	0	0	24
HE 240 A	0	0	QP Solai	PolG	102	0	0	24	178	0	0	22
HE 240 A	0	0	QP Solai	PolG	0	0	0	22	46	0	0	25
HE 240 A	0	0	QP Solai	PolG	46	0	0	25	92	0	0	25
HE 240 A	0	0	QP Solai	PolG	92	0	0	25	151	0	0	22
HE 240 A	0	55	QP Solai	PolG	0	0	0	24	30	0	0	26
HE 240 A	0	0	QP Solai	PolG	30	0	0	26	91	0	0	27
HE 240 A	0	0	QP Solai	PolG	91	0	0	27	134	0	0	24
HE 240 A	0	0	QP Solai	PolG	0	0	0	23	39	0	0	26
HE 240 A	0	0	QP Solai	PolG	39	0	0	26	95	0	0	26
HE 240 A	0	55	Neve	PolG	95	0	0	26	148	0	0	23
HE 240 A	0	0	Neve	PolG	0	0	0	16	91	0	0	29
HE 240 A	0	0	Neve	PolG	91	0	0	29	134	0	0	29
HE 240 A	0	0	Neve	PolG	0	0	0	16	92	0	0	26

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Neve	PolG	92	0	0	26	151	0	0	27
HE 240 A	0	0	Neve	PolG	0	0	0	16	96	0	0	23
HE 240 A	0	0	Neve	PolG	96	0	0	23	178	0	0	24
HE 240 A	0	0	Neve	PolG	95	0	0	28	148	0	0	28
HE 240 A	0	0	Neve	PolG	0	0	0	27	46	0	0	28
HE 240 A	0	55	Neve	PolG	46	0	0	28	151	0	0	17
HE 240 A	0	0	Neve	PolG	30	0	0	30	30	0	0	30
HE 240 A	0	0	Neve	PolG	30	0	0	30	134	0	0	17
HE 240 A	0	0	Neve	PolG	39	0	0	29	39	0	0	29
HE 240 A	0	0	Neve	PolG	39	0	0	29	148	0	0	17
HE 240 A	0	0	Neve	PolG	102	0	0	25	178	0	0	25
HE 240 A	0	0	Neve	PolG	67	0	0	24	67	0	0	25
HE 240 A	0	0	Neve	PolG	60	0	0	26	60	0	0	26
HE 240 A	0	0	Vento X	PolG	0	0	0	42	46	0	0	43
HE 240 A	0	0	Vento X	PolG	46	0	0	43	151	0	0	26
HE 240 A	0	0	Vento X	PolG	0	0	0	25	96	0	0	36
HE 240 A	0	0	Vento X	PolG	96	0	0	36	178	0	0	37
HE 240 A	0	0	Vento X	PolG	0	0	0	44	39	0	0	45
HE 240 A	0	0	Vento X	PolG	39	0	0	45	148	0	0	26
HE 240 A	0	0	Vento X	PolG	0	0	0	39	60	0	0	40
HE 240 A	0	0	Vento X	PolG	60	0	0	40	178	0	0	26
HE 240 A	0	0	Vento X	PolG	0	0	0	25	92	0	0	40
HE 240 A	0	55	Vento X	PolG	92	0	0	40	151	0	0	41
HE 240 A	0	55	Vento X	PolG	0	0	0	47	30	0	0	47
HE 240 A	0	0	Vento X	PolG	30	0	0	47	134	0	0	26
HE 240 A	0	0	Vento X	PolG	67	0	0	38	178	0	0	26
HE 240 A	0	0	Vento X	PolG	0	0	0	25	102	0	0	38
HE 240 A	0	0	Vento X	PolG	102	0	0	38	178	0	0	39
HE 240 A	0	0	Vento X	PolG	0	0	0	25	95	0	0	43
HE 240 A	0	55	Vento X	PolG	95	0	0	43	148	0	0	43
HE 240 A	0	55	Vento X	PolG	0	0	0	25	91	0	0	46
HE 240 A	0	55	Vento X	PolG	91	0	0	45	134	0	0	45
HE 240 A	0	55	Carichi termici	Termico	60	0	0	60	123	0	0	60
HE 240 A	0	0	Carichi termici	Termico	60	0	0	77	23	0	0	84
HE 240 A	0	0	Carichi termici	Termico	60	0	0	84	87	0	0	85
HE 240 A	0	0	Carichi termici	Termico	60	0	0	85	123	0	0	77
HE 240 A	55	56	Peso Proprio	UnifG	0	0	0	25	23	0	0	27
HE 240 A	55	56	QP Solai	PolG	23	0	0	27	87	0	0	27
HE 240 A	55	56	QP Solai	PolG	87	0	0	32	23	0	0	32
HE 240 A	55	56	QP Solai	PolG	23	0	0	32	123	0	0	17
HE 240 A	55	56	QP Solai	PolG	0	0	0	16	87	0	0	30
HE 240 A	55	56	QP Solai	PolG	87	0	0	30	123	0	0	31
HE 240 A	55	56	QP Solai	PolG	0	0	0	25	87	0	0	47
HE 240 A	55	56	QP Solai	PolG	87	0	0	47	123	0	0	48
HE 240 A	55	56	QP Solai	PolG	0	0	0	49	23	0	0	49
HE 240 A	55	56	QP Solai	PolG	23	0	0	49	123	0	0	26
HE 240 A	55	56	Carichi termici	Termico	60	0	0	60	113	0	0	60
HE 240 A	56	381	Peso Proprio	UnifG	0	0	0	80	17	0	0	85
HE 240 A	56	381	QP Solai	PolG	17	0	0	85	84	0	0	87
HE 240 A	56	381	QP Solai	PolG	84	0	0	87	113	0	0	79
HE 240 A	56	381	QP Solai	PolG	0	0	0	26	17	0	0	27
HE 240 A	56	381	QP Solai	PolG	17	0	0	27	84	0	0	28
HE 240 A	56	381	QP Solai	PolG	84	0	0	28	113	0	0	25
HE 240 A	56	381	QP Solai	PolG	0	0	0	33	17	0	0	33

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	56	381	Neve	PolG	17	0	0	33	113	0	0	17
HE 240 A					0	0	0	16	84	0	0	32
HE 240 A	56	381	Vento X	PolG	84	0	0	32	113	0	0	32
HE 240 A					0	0	0	51	17	0	0	52
HE 240 A	56	381	Vento X	PolG	17	0	0	52	113	0	0	26
HE 240 A					0	0	0	25	84	0	0	49
HE 240 A	56	381	Carichi termici	Termico	84	0	0	49	113	0	0	50
HE 240 A	124	0	Peso Proprio	UnifG	AXY=15°C, AXZ=15°C	0	0	60	182	0	0	60
HE 240 A	124	0	QP Solai	PolG	0	0	0	63	75	0	0	71
HE 240 A					75	0	0	71	92	0	0	71
HE 240 A	124	0	QV Solai	PolG	92	0	0	71	182	0	0	63
HE 240 A					0	0	0	20	75	0	0	23
HE 240 A	124	0	Neve	PolG	92	0	0	23	182	0	0	20
HE 240 A					0	0	0	16	92	0	0	22
HE 240 A	124	0	Neve	PolG	92	0	0	22	182	0	0	22
HE 240 A					0	0	0	22	75	0	0	23
HE 240 A	124	0	Vento X	PolG	75	0	0	23	182	0	0	17
HE 240 A					0	0	0	35	75	0	0	36
HE 240 A	124	0	Vento X	PolG	75	0	0	36	182	0	0	26
HE 240 A					0	0	0	25	92	0	0	34
HE 240 A	124	0	QV Solai	PolG	92	0	0	34	182	0	0	35
HE 240 A	124	0	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	108	0	0	60
HE 240 A	381	382	Peso Proprio	UnifG	0	0	0	82	12	0	0	86
HE 240 A	381	382	QP Solai	PolG	12	0	0	86	84	0	0	88
HE 240 A					84	0	0	88	108	0	0	81
HE 240 A	381	382	QV Solai	PolG	12	0	0	26	12	0	0	28
HE 240 A					84	0	0	28	84	0	0	26
HE 240 A	381	382	Neve	PolG	0	0	0	16	84	0	0	33
HE 240 A					84	0	0	33	108	0	0	34
HE 240 A	381	382	Neve	PolG	12	0	0	35	12	0	0	35
HE 240 A					84	0	0	25	84	0	0	52
HE 240 A	381	382	Vento X	PolG	84	0	0	52	108	0	0	52
HE 240 A					12	0	0	54	12	0	0	54
HE 240 A	381	382	Vento X	PolG	12	0	0	54	108	0	0	26
HE 240 A					AXY=15°C, AXZ=15°C	0	0	60	112	0	0	60
HE 240 A	381	382	Carichi termici	Termico	0	0	0	85	9	0	0	88
HE 240 A	382	350	Peso Proprio	UnifG	0	0	0	88	91	0	0	90
HE 240 A	382	350	QP Solai	PolG	9	0	0	90	112	0	0	84
HE 240 A					91	0	0	27	9	0	0	28
HE 240 A	382	350	QV Solai	PolG	9	0	0	28	91	0	0	29
HE 240 A					91	0	0	29	112	0	0	27
HE 240 A	382	350	Neve	PolG	0	0	0	36	9	0	0	36
HE 240 A					9	0	0	36	112	0	0	17
HE 240 A	382	350	Neve	PolG	0	0	0	16	91	0	0	35
HE 240 A					91	0	0	35	112	0	0	35
HE 240 A	382	350	Vento X	PolG	0	0	0	25	91	0	0	54
HE 240 A					91	0	0	54	112	0	0	54
HE 240 A	382	350	Vento X	PolG	0	0	0	56	9	0	0	56
HE 240 A					9	0	0	56	112	0	0	26
HE 240 A	382	350	Carichi termici	Termico	AXY=15°C, AXZ=15°C	0	0	60	151	0	0	60
HE 240 A					UnifG	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	134	0	0	60
HE 240 A	0	63	Peso Proprio	UnifG	0	0	0	60	148	0	0	60
HE 240 A	0	0	Peso Proprio	UnifG	0	0	0	60	178	0	0	60
HE 240 A	0	0	QP Solai	PolG	0	0	0	64	73	0	0	79
HE 240 A					73	0	0	79	90	0	0	79
HE 240 A					90	0	0	79	178	0	0	65
HE 240 A	0	0	QP Solai	PolG	0	0	0	62	79	0	0	76

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A					79	0	0	76	85	0	0	76
HE 240 A					85	0	0	76	178	0	0	62
HE 240 A	0	63	QP Solai	PolG	0	0	0	72	42	0	0	85
HE 240 A					42	0	0	85	80	0	0	85
HE 240 A					80	0	0	85	134	0	0	72
HE 240 A	0	0	QP Solai	PolG	0	0	0	69	51	0	0	83
HE 240 A					51	0	0	83	84	0	0	83
HE 240 A	0	0	QP Solai	PolG	84	0	0	83	148	0	0	69
HE 240 A					57	0	0	81	81	0	0	81
HE 240 A					81	0	0	81	151	0	0	67
HE 240 A	0	0	QV Solai	PolG	0	0	0	20	79	0	0	24
HE 240 A					79	0	0	24	85	0	0	24
HE 240 A	0	63	QV Solai	PolG	85	0	0	23	42	0	0	20
HE 240 A					42	0	0	27	80	0	0	27
HE 240 A					80	0	0	27	134	0	0	23
HE 240 A	0	0	QV Solai	PolG	0	0	0	21	57	0	0	26
HE 240 A					57	0	0	26	81	0	0	26
HE 240 A					81	0	0	26	151	0	0	21
HE 240 A	0	0	QV Solai	PolG	0	0	0	22	51	0	0	27
HE 240 A					51	0	0	27	84	0	0	27
HE 240 A					84	0	0	27	148	0	0	22
HE 240 A	0	0	QV Solai	PolG	0	0	0	21	73	0	0	25
HE 240 A					73	0	0	25	90	0	0	25
HE 240 A					90	0	0	25	178	0	0	21
HE 240 A	0	0	Neve	PolG	0	0	0	28	51	0	0	29
HE 240 A					51	0	0	29	148	0	0	15
HE 240 A	0	0	Neve	PolG	0	0	0	15	90	0	0	25
HE 240 A					90	0	0	25	178	0	0	25
HE 240 A	0	63	Neve	PolG	0	0	0	30	42	0	0	30
HE 240 A					42	0	0	30	134	0	0	15
HE 240 A	0	0	Neve	PolG	0	0	0	15	84	0	0	28
HE 240 A					84	0	0	28	148	0	0	28
HE 240 A					85	0	0	23	178	0	0	24
HE 240 A	0	0	Neve	PolG	0	0	0	27	57	0	0	28
HE 240 A					57	0	0	28	151	0	0	15
HE 240 A	0	0	Neve	PolG	0	0	0	24	79	0	0	25
HE 240 A					79	0	0	25	178	0	0	15
HE 240 A	0	63	Neve	PolG	0	0	0	15	80	0	0	29
HE 240 A					80	0	0	29	134	0	0	30
HE 240 A	0	0	Neve	PolG	0	0	0	25	73	0	0	26
HE 240 A					73	0	0	26	178	0	0	15
HE 240 A	0	0	Neve	PolG	0	0	0	15	81	0	0	26
HE 240 A					81	0	0	26	151	0	0	27
HE 240 A	0	0	Vento X	PolG	0	0	0	23	90	0	0	38
HE 240 A					90	0	0	38	178	0	0	39
HE 240 A	0	0	Vento X	PolG	0	0	0	22	81	0	0	40
HE 240 A					81	0	0	40	151	0	0	41
HE 240 A	0	0	Vento X	PolG	0	0	0	22	84	0	0	43
HE 240 A					84	0	0	43	148	0	0	43
HE 240 A	0	63	Vento X	PolG	42	0	0	46	42	0	0	47
HE 240 A					42	0	0	47	134	0	0	23
HE 240 A	0	0	Vento X	PolG	0	0	0	44	51	0	0	45
HE 240 A					51	0	0	45	148	0	0	23
HE 240 A	0	0	Vento X	PolG	0	0	0	37	79	0	0	38
HE 240 A					79	0	0	38	178	0	0	23
HE 240 A	0	0	Vento X	PolG	0	0	0	42	57	0	0	43
HE 240 A					57	0	0	43	151	0	0	23
HE 240 A	0	0	Vento X	PolG	0	0	0	23	85	0	0	36
HE 240 A					85	0	0	36	178	0	0	37
HE 240 A	0	63	Vento X	PolG	0	0	0	22	80	0	0	45
HE 240 A					80	0	0	45	134	0	0	46
HE 240 A	0	0	Vento X	PolG	0	0	0	39	73	0	0	40

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	63	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	63	64	Peso Proprio	UnitG	0	0	0	60	123	0	0	60
HE 240 A	63	64	QP Solai	PolG	34	0	0	74	34	0	0	86
					77	0	0	86	77	0	0	87
HE 240 A	63	64	QV Solai	PolG	0	0	0	87	123	0	0	74
					34	0	0	24	34	0	0	28
					77	0	0	28	77	0	0	28
HE 240 A	63	64	Neve	PolG	77	0	0	28	123	0	0	24
HE 240 A	63	64	Neve	PolG	77	0	0	15	77	0	0	30
HE 240 A	63	64	Neve	PolG	0	0	0	30	123	0	0	31
HE 240 A	63	64	Neve	PolG	0	0	0	31	34	0	0	32
HE 240 A	63	64	Vento X	PolG	34	0	0	32	123	0	0	15
HE 240 A	63	64	Vento X	PolG	0	0	0	22	77	0	0	47
HE 240 A	63	64	Vento X	PolG	77	0	0	47	123	0	0	48
HE 240 A	63	64	Vento X	PolG	0	0	0	49	34	0	0	49
HE 240 A	63	64	Vento X	PolG	34	0	0	49	123	0	0	23
HE 240 A	63	64	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	64	389	Peso Proprio	UnitG	0	0	0	60	113	0	0	60
HE 240 A	64	389	QP Solai	PolG	0	0	0	76	28	0	0	88
					28	0	0	88	74	0	0	89
HE 240 A	64	389	QV Solai	PolG	74	0	0	89	113	0	0	76
					0	0	0	24	28	0	0	28
					28	0	0	28	74	0	0	28
HE 240 A	64	389	Neve	PolG	74	0	0	28	113	0	0	24
HE 240 A	64	389	Neve	PolG	0	0	0	15	74	0	0	32
HE 240 A	64	389	Neve	PolG	74	0	0	32	113	0	0	32
HE 240 A	64	389	Neve	PolG	0	0	0	33	28	0	0	33
HE 240 A	64	389	Vento X	PolG	28	0	0	33	113	0	0	15
HE 240 A	64	389	Vento X	PolG	0	0	0	51	28	0	0	52
HE 240 A	64	389	Vento X	PolG	28	0	0	52	113	0	0	23
HE 240 A	64	389	Vento X	PolG	0	0	0	22	74	0	0	49
HE 240 A	64	389	Vento X	PolG	74	0	0	22	74	0	0	50
HE 240 A	64	389	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	125	0	Peso Proprio	UnitG	0	0	0	60	182	0	0	60
HE 240 A	125	0	QP Solai	PolG	0	0	0	60	81	0	0	72
					81	0	0	72	87	0	0	72
HE 240 A	125	0	QV Solai	PolG	87	0	0	72	182	0	0	60
					0	0	0	19	81	0	0	23
					81	0	0	23	87	0	0	23
HE 240 A	125	0	Neve	PolG	87	0	0	23	182	0	0	19
HE 240 A	125	0	Neve	PolG	0	0	0	15	81	0	0	22
HE 240 A	125	0	Neve	PolG	81	0	0	22	182	0	0	22
HE 240 A	125	0	Neve	PolG	0	0	0	22	87	0	0	23
HE 240 A	125	0	Vento X	PolG	87	0	0	23	182	0	0	15
HE 240 A	125	0	Vento X	PolG	0	0	0	35	87	0	0	36
HE 240 A	125	0	Vento X	PolG	87	0	0	36	182	0	0	23
HE 240 A	125	0	Vento X	PolG	0	0	0	23	81	0	0	34
HE 240 A	125	0	Vento X	PolG	81	0	0	34	182	0	0	35
HE 240 A	125	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	389	390	Peso Proprio	UnitG	0	0	0	60	108	0	0	60
HE 240 A	389	390	QP Solai	PolG	0	0	0	79	23	0	0	89
					23	0	0	89	74	0	0	90
HE 240 A	389	390	QV Solai	PolG	74	0	0	90	108	0	0	78
					0	0	0	25	23	0	0	28
HE 240 A	389	390	Neve	PolG	23	0	0	28	74	0	0	29
HE 240 A	389	390	Neve	PolG	74	0	0	29	108	0	0	25
HE 240 A	389	390	Neve	PolG	0	0	0	15	74	0	0	33
HE 240 A	389	390	Neve	PolG	74	0	0	33	108	0	0	34
HE 240 A	389	390	Vento X	PolG	0	0	0	34	23	0	0	35
HE 240 A	389	390	Vento X	PolG	23	0	0	35	108	0	0	15
HE 240 A	389	390	Vento X	PolG	0	0	0	22	74	0	0	52

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	389	390	Vento X	PolG	74	0	0	52	108	0	0	52
HE 240 A	389	390	Carichi termici Peso Proprio QP Solai	PolG	23	0	0	53	23	0	0	54
HE 240 A	390	351		UnitG	0	0	0	60	112	0	0	60
HE 240 A	390	351		PolG	20	0	0	81	20	0	0	90
					80	0	0	90	80	0	0	92
HE 240 A	390	351	QV Solai	PolG	0	0	0	92	112	0	0	81
					20	0	0	26	20	0	0	29
					20	0	0	29	80	0	0	29
					80	0	0	29	112	0	0	26
HE 240 A	390	351	Neve	PolG	0	0	0	36	20	0	0	36
					20	0	0	36	112	0	0	15
HE 240 A	390	351	Neve	PolG	0	0	0	15	80	0	0	35
					80	0	0	35	112	0	0	35
HE 240 A	390	351	Vento X	PolG	0	0	0	56	20	0	0	56
					20	0	0	56	112	0	0	23
HE 240 A	390	351	Vento X	PolG	0	0	0	22	80	0	0	54
					80	0	0	54	112	0	0	54
HE 240 A	390	351	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
Trave 8025												
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	151	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	178	0	0	60
HE 240 A	0	67	Peso Proprio	UnitG	0	0	0	60	134	0	0	60
HE 240 A	0	0	Peso Proprio	UnitG	0	0	0	60	148	0	0	60
HE 240 A	0	0	QP Solai	PolG	0	0	0	46	62	0	0	47
					62	0	0	47	148	0	0	21
HE 240 A	0	0	QP Solai	PolG	0	0	0	38	90	0	0	40
					90	0	0	40	178	0	0	21
HE 240 A	0	67	QP Solai	PolG	0	0	0	48	53	0	0	49
					53	0	0	49	134	0	0	21
HE 240 A	0	0	QP Solai	PolG	0	0	0	41	85	0	0	42
					85	0	0	42	178	0	0	21
HE 240 A	0	0	QP Solai	PolG	0	0	0	43	68	0	0	44
					68	0	0	44	151	0	0	21
HE 240 A	0	0	QV Solai	PolG	0	0	0	12	90	0	0	13
					90	0	0	13	178	0	0	7
HE 240 A	0	0	QV Solai	PolG	0	0	0	13	85	0	0	13
					85	0	0	13	178	0	0	7
HE 240 A	0	67	QV Solai	PolG	0	0	0	15	53	0	0	16
					53	0	0	16	134	0	0	7
HE 240 A	0	0	QV Solai	PolG	0	0	0	14	68	0	0	14
					68	0	0	14	151	0	0	7
HE 240 A	0	0	QV Solai	PolG	0	0	0	15	62	0	0	15
					62	0	0	15	148	0	0	7
HE 240 A	0	0	Neve	PolG	0	0	0	27	68	0	0	28
					68	0	0	28	151	0	0	13
HE 240 A	0	67	Neve	PolG	0	0	0	30	53	0	0	30
					53	0	0	30	134	0	0	13
HE 240 A	0	0	Neve	PolG	0	0	0	25	85	0	0	26
					85	0	0	26	178	0	0	13
HE 240 A	0	0	Neve	PolG	0	0	0	28	62	0	0	29
					62	0	0	29	148	0	0	13
HE 240 A	0	0	Neve	PolG	0	0	0	24	90	0	0	25
					90	0	0	25	178	0	0	13
HE 240 A	0	0	Vento X	PolG	0	0	0	37	90	0	0	38
					90	0	0	38	178	0	0	20
HE 240 A	0	0	Vento X	PolG	0	0	0	39	85	0	0	40
					85	0	0	40	178	0	0	20
HE 240 A	0	0	Vento X	PolG	0	0	0	44	62	0	0	45
					62	0	0	45	148	0	0	20
HE 240 A	0	67	Vento X	PolG	0	0	0	46	53	0	0	47
					53	0	0	47	134	0	0	20
HE 240 A	0	0	Vento X	PolG	0	0	0	41	68	0	0	43
					68	0	0	43	151	0	0	20

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	QXf	QYf	QZf
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	67	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C							
HE 240 A	67	68	Peso Proprio	UnitG	0	0	0	60	123	0	0	60
HE 240 A	67	68	QP Solai	PolG	0	0	0	50	45	0	0	51
HE 240 A	67	68	QV Solai	PolG	45	0	0	51	123	0	0	21
HE 240 A	67	68	QV Solai	PolG	0	0	0	16	45	0	0	16
HE 240 A	67	68	QV Solai	PolG	45	0	0	16	123	0	0	7
HE 240 A	67	68	Neve	PolG	0	0	0	31	45	0	0	32
HE 240 A	67	68	Vento X	PolG	45	0	0	32	123	0	0	13
HE 240 A	67	68	Vento X	PolG	0	0	0	48	45	0	0	49
HE 240 A	67	68	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	45	0	0	49	123	0	20
HE 240 A	68	393	Peso Proprio	UnitG	0	0	0	60	113	0	0	60
HE 240 A	68	393	QP Solai	PolG	0	0	0	53	38	0	0	54
HE 240 A	68	393	QV Solai	PolG	38	0	0	54	113	0	0	21
HE 240 A	68	393	QV Solai	PolG	0	0	0	17	38	0	0	17
HE 240 A	68	393	Neve	PolG	38	0	0	17	113	0	0	7
HE 240 A	68	393	Vento X	PolG	0	0	0	33	38	0	0	33
HE 240 A	68	393	Vento X	PolG	38	0	0	33	113	0	0	13
HE 240 A	68	393	Vento X	PolG	0	0	0	51	38	0	0	52
HE 240 A	68	393	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	38	0	0	52	113	0	20
HE 240 A	126	0	Peso Proprio	UnitG	0	0	0	60	182	0	0	60
HE 240 A	126	0	QP Solai	PolG	0	0	0	36	98	0	0	37
HE 240 A	126	0	QV Solai	PolG	98	0	0	37	182	0	0	21
HE 240 A	126	0	QV Solai	PolG	0	0	0	12	98	0	0	12
HE 240 A	126	0	Neve	PolG	98	0	0	12	182	0	0	7
HE 240 A	126	0	Vento X	PolG	0	0	0	22	98	0	0	23
HE 240 A	126	0	Vento X	PolG	98	0	0	23	182	0	0	13
HE 240 A	126	0	Vento X	PolG	0	0	0	35	98	0	0	36
HE 240 A	126	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	98	0	0	36	182	0	20
HE 240 A	393	394	Peso Proprio	UnitG	0	0	0	60	108	0	0	60
HE 240 A	393	394	QP Solai	PolG	0	0	0	55	33	0	0	56
HE 240 A	393	394	QV Solai	PolG	33	0	0	56	108	0	0	21
HE 240 A	393	394	QV Solai	PolG	0	0	0	18	33	0	0	18
HE 240 A	393	394	Neve	PolG	33	0	0	18	108	0	0	7
HE 240 A	393	394	Vento X	PolG	0	0	0	34	33	0	0	35
HE 240 A	393	394	Vento X	PolG	33	0	0	35	108	0	0	13
HE 240 A	393	394	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	33	0	0	53	33	0	54
HE 240 A	393	394	Peso Proprio	UnitG	0	0	0	60	112	0	0	60
HE 240 A	393	394	QP Solai	PolG	0	0	0	58	31	0	0	58
HE 240 A	393	394	QV Solai	PolG	31	0	0	58	112	0	0	21
HE 240 A	393	394	QV Solai	PolG	0	0	0	18	31	0	0	19
HE 240 A	393	394	Neve	PolG	31	0	0	19	112	0	0	7
HE 240 A	393	394	Vento X	PolG	0	0	0	36	31	0	0	36
HE 240 A	393	394	Vento X	PolG	31	0	0	36	112	0	0	13
HE 240 A	393	394	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	31	0	0	55	31	0	56
HE 240 A	393	394	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	31	0	0	56	112	0	20
Trave 8028	101	102	Peso Proprio	UnitG	0	0	0	8	78	0	0	8
IPE 100	101	102	QP Solai	PolG	0	0	0	71	65	0	0	71
IPE 100	101	102	QV Solai	PolG	65	0	0	71	90	0	0	15
IPE 100	101	102	Neve	PolG	0	0	0	23	65	0	0	23
IPE 100	101	102	Vento X	PolG	65	0	0	23	90	0	0	5
IPE 100	101	102	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	65	0	0	44	65	0	44
IPE 100	101	102	Peso Proprio	UnitG	0	0	0	8	90	0	0	9
IPE 100	101	102	QP Solai	PolG	0	0	0	68	65	0	0	68
IPE 100	101	102	QV Solai	PolG	65	0	0	68	90	0	0	14

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	OYi	QZi	Xf	QXf	QYf	QZf
IPE 100	101	102	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	8	90	0	8
IPE 100	102	103	Peso Proprio	UnitG	0	0	0	71	71	0	0	71
IPE 100	102	103	QP Solai	PolG	71	0	0	71	90	0	0	11
IPE 100	102	103	QV Solai	PolG	0	0	0	23	71	0	0	23
IPE 100	102	103	Neve	PolG	71	0	0	23	90	0	0	4
IPE 100	102	103	Vento X	PolG	0	0	0	44	71	0	0	44
IPE 100	102	103	Vento X	PolG	71	0	0	44	90	0	0	7
IPE 100	102	103	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	71	0	0	68	71	0	68
IPE 100	103	104	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	103	104	QP Solai	PolG	77	0	0	71	89	0	0	9
IPE 100	103	104	QV Solai	PolG	0	0	0	23	77	0	0	23
IPE 100	103	104	Neve	PolG	77	0	0	23	89	0	0	3
IPE 100	103	104	Vento X	PolG	0	0	0	44	77	0	0	44
IPE 100	103	104	Vento X	PolG	77	0	0	44	89	0	0	5
IPE 100	103	104	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	77	0	0	68	77	0	68
IPE 100	104	105	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	104	105	QP Solai	PolG	83	0	0	71	89	0	0	5
IPE 100	104	105	QV Solai	PolG	0	0	0	23	83	0	0	23
IPE 100	104	105	Neve	PolG	83	0	0	23	89	0	0	1
IPE 100	104	105	Vento X	PolG	0	0	0	44	89	0	0	3
IPE 100	104	105	Vento X	PolG	83	0	0	44	89	0	0	68
IPE 100	104	105	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	83	0	0	68	89	0	4
IPE 100	105	106	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	105	106	QP Solai	PolG	0	0	0	71	89	0	0	72
IPE 100	105	106	QV Solai	PolG	83	0	0	23	89	0	0	23
IPE 100	105	106	Neve	PolG	0	0	0	44	89	0	0	45
IPE 100	105	106	Vento X	PolG	0	0	0	68	89	0	0	69
IPE 100	106	107	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	0	0	0	8	89	0	8
IPE 100	106	107	Peso Proprio	UnitG	0	0	0	72	89	0	0	8
IPE 100	106	107	QP Solai	PolG	0	0	0	23	89	0	0	23
IPE 100	106	107	QV Solai	PolG	0	0	0	45	89	0	0	44
IPE 100	106	107	Neve	PolG	0	0	0	69	89	0	0	68
IPE 100	106	107	Vento X	PolG	0	0	0	8	90	0	0	8
IPE 100	107	108	Peso Proprio	UnitG	0	0	0	5	6	0	0	71
IPE 100	107	108	QP Solai	PolG	6	0	0	71	90	0	0	71
IPE 100	107	108	QV Solai	PolG	0	0	0	2	6	0	0	23
IPE 100	107	108	Neve	PolG	6	0	0	23	90	0	0	23
IPE 100	107	108	Vento X	PolG	0	0	0	3	6	0	0	44
IPE 100	107	108	Vento X	PolG	6	0	0	44	90	0	0	44
IPE 100	107	108	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	6	0	0	68	90	0	68
IPE 100	108	109	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	108	109	QP Solai	PolG	12	0	0	8	12	0	0	71
IPE 100	108	109	QV Solai	PolG	0	0	0	3	12	0	0	23
IPE 100	108	109	Neve	PolG	12	0	0	23	89	0	0	23
IPE 100	108	109	Vento X	PolG	0	0	0	5	12	0	0	44
IPE 100	108	109	Vento X	PolG	12	0	0	44	89	0	0	44
IPE 100	108	109	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C	12	0	0	68	89	0	68
IPE 100	109	110	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	109	110	QP Solai	PolG	0	0	0	12	18	0	0	71

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	109	110	QV Solai	PolG	18	0	0	71	90	0	0	71
IPE 100	109	110	QV Solai	PolG	0	0	0	4	18	0	0	23
IPE 100	109	110	Neve	PolG	18	0	0	23	90	0	0	23
IPE 100	109	110	Neve	PolG	0	0	0	8	18	0	0	44
IPE 100	109	110	Vento X	PolG	18	0	0	44	90	0	0	44
IPE 100	109	110	Vento X	PolG	0	0	0	12	18	0	0	68
IPE 100	109	110	Vento X	PolG	18	0	0	68	90	0	0	68
IPE 100	109	110	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	110	111	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	110	111	QV Solai	PolG	25	0	0	15	25	0	0	71
IPE 100	110	111	QV Solai	PolG	0	0	0	71	90	0	0	71
IPE 100	110	111	QV Solai	PolG	0	0	0	5	25	0	0	23
IPE 100	110	111	Neve	PolG	25	0	0	23	90	0	0	23
IPE 100	110	111	Neve	PolG	0	0	0	9	25	0	0	44
IPE 100	110	111	Neve	PolG	25	0	0	44	90	0	0	44
IPE 100	110	111	Vento X	PolG	0	0	0	14	25	0	0	68
IPE 100	110	111	Vento X	PolG	25	0	0	68	90	0	0	68
IPE 100	110	111	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	111	112	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	111	112	QV Solai	PolG	0	0	0	19	31	0	0	71
IPE 100	111	112	QV Solai	PolG	31	0	0	71	89	0	0	71
IPE 100	111	112	QV Solai	PolG	0	0	0	6	31	0	0	23
IPE 100	111	112	Neve	PolG	31	0	0	23	89	0	0	23
IPE 100	111	112	Neve	PolG	0	0	0	12	31	0	0	44
IPE 100	111	112	Neve	PolG	31	0	0	44	89	0	0	44
IPE 100	111	112	Vento X	PolG	0	0	0	18	31	0	0	68
IPE 100	111	112	Vento X	PolG	31	0	0	68	89	0	0	68
IPE 100	111	112	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	112	113	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	112	113	QV Solai	PolG	0	0	0	23	38	0	0	71
IPE 100	112	113	QV Solai	PolG	38	0	0	71	89	0	0	71
IPE 100	112	113	QV Solai	PolG	0	0	0	7	38	0	0	23
IPE 100	112	113	Neve	PolG	38	0	0	23	89	0	0	23
IPE 100	112	113	Neve	PolG	0	0	0	14	38	0	0	44
IPE 100	112	113	Neve	PolG	38	0	0	44	89	0	0	44
IPE 100	112	113	Vento X	PolG	0	0	0	22	38	0	0	68
IPE 100	112	113	Vento X	PolG	38	0	0	68	89	0	0	68
IPE 100	112	113	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	113	114	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	113	114	QV Solai	PolG	0	0	0	26	45	0	0	71
IPE 100	113	114	QV Solai	PolG	45	0	0	71	90	0	0	71
IPE 100	113	114	QV Solai	PolG	0	0	0	8	45	0	0	23
IPE 100	113	114	Neve	PolG	45	0	0	23	90	0	0	23
IPE 100	113	114	Neve	PolG	0	0	0	16	45	0	0	44
IPE 100	113	114	Neve	PolG	45	0	0	44	90	0	0	44
IPE 100	113	114	Vento X	PolG	0	0	0	25	45	0	0	68
IPE 100	113	114	Vento X	PolG	45	0	0	68	90	0	0	68
IPE 100	113	114	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	114	115	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	114	115	QV Solai	PolG	0	0	0	31	52	0	0	71
IPE 100	114	115	QV Solai	PolG	52	0	0	71	90	0	0	71
IPE 100	114	115	QV Solai	PolG	0	0	0	10	52	0	0	23
IPE 100	114	115	Neve	PolG	52	0	0	23	90	0	0	23
IPE 100	114	115	Neve	PolG	0	0	0	19	52	0	0	44
IPE 100	114	115	Neve	PolG	52	0	0	44	90	0	0	44
IPE 100	114	115	Vento X	PolG	0	0	0	29	52	0	0	68
IPE 100	114	115	Vento X	PolG	52	0	0	68	90	0	0	68
IPE 100	114	115	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	115	116	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	115	116	QV Solai	PolG	0	0	0	35	60	0	0	71
IPE 100	115	116	QV Solai	PolG	60	0	0	71	89	0	0	71
IPE 100	115	116	QV Solai	PolG	0	0	0	11	60	0	0	23
IPE 100	115	116	Neve	PolG	60	0	0	23	89	0	0	23
IPE 100	115	116	Neve	PolG	0	0	0	22	60	0	0	44
IPE 100	115	116	Neve	PolG	60	0	0	44	89	0	0	44
IPE 100	115	116	Vento X	PolG	0	0	0	33	60	0	0	68

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	115	116	Carichi termici Peso Proprio QV Solai	Termico	AXY=15°C,AXZ=15°C							
	116	117		UnitG	0	0	0	8	89	0	0	8
	116	117		PolG	0	0	0	39	68	0	0	71
	116	117		PolG	68	0	0	71	89	0	0	71
IPE 100	116	117	QV Solai	PolG	0	0	0	13	68	0	0	23
	116	117		PolG	68	0	0	23	89	0	0	23
	116	117		PolG	0	0	0	24	68	0	0	44
	116	117		PolG	68	0	0	44	89	0	0	44
IPE 100	116	117	Vento X	PolG	0	0	0	38	68	0	0	68
	116	117		PolG	68	0	0	68	89	0	0	68
	116	117		Termico	AXY=15°C,AXZ=15°C							
	117	118		UnitG	0	0	0	8	90	0	0	8
IPE 100	117	118	Peso Proprio QV Solai	PolG	0	0	0	45	78	0	0	71
	117	118		PolG	78	0	0	71	90	0	0	71
	117	118		PolG	0	0	0	14	78	0	0	23
	117	118		PolG	78	0	0	23	90	0	0	23
IPE 100	117	118	Neve	PolG	0	0	0	28	78	0	0	44
	117	118		PolG	78	0	0	44	90	0	0	44
	117	118		PolG	0	0	0	43	78	0	0	68
	117	118		PolG	78	0	0	68	90	0	0	68
IPE 100	117	118	Carichi termici Peso Proprio QV Solai	Termico	AXY=15°C,AXZ=15°C							
	118	119		UnitG	0	0	0	8	89	0	0	8
	118	119		PolG	0	0	0	50	87	0	0	71
	118	119		PolG	0	0	0	16	87	0	0	23
IPE 100	118	119	Neve	PolG	0	0	0	31	87	0	0	44
	118	119		PolG	0	0	0	48	87	0	0	68
	118	119		Termico	AXY=15°C,AXZ=15°C							
	119	120		UnitG	0	0	0	8	90	0	0	8
IPE 100	119	120	Peso Proprio QV Solai	PolG	0	0	0	56	90	0	0	65
	119	120		PolG	0	0	0	18	90	0	0	21
	119	120		PolG	0	0	0	35	90	0	0	41
	119	120		PolG	0	0	0	54	90	0	0	63
IPE 100	119	120	Vento X	Termico	AXY=15°C,AXZ=15°C							
	120	121		UnitG	0	0	0	8	89	0	0	8
	120	121		PolG	0	0	0	64	89	0	0	57
	120	121		PolG	0	0	0	20	89	0	0	18
IPE 100	120	121	Neve	PolG	0	0	0	40	89	0	0	35
	120	121		PolG	0	0	0	61	89	0	0	55
	120	121		Termico	AXY=15°C,AXZ=15°C							
	121	122		UnitG	0	0	0	8	89	0	0	8
IPE 100	121	122	Peso Proprio QV Solai	PolG	0	0	0	71	89	0	0	51
	121	122		PolG	0	0	0	23	89	0	0	16
	121	122		PolG	0	0	0	44	89	0	0	32
	121	122		PolG	0	0	0	68	89	0	0	49
IPE 100	121	122	Vento X	Termico	AXY=15°C,AXZ=15°C							
	122	123		UnitG	0	0	0	8	90	0	0	8
	122	123		PolG	0	0	0	71	10	0	0	76
	122	123		PolG	10	0	0	76	90	0	0	46
IPE 100	122	123	QV Solai	PolG	0	0	0	23	10	0	0	24
	122	123		PolG	10	0	0	24	90	0	0	15
	122	123		PolG	0	0	0	44	10	0	0	47
	122	123		PolG	10	0	0	47	90	0	0	29
IPE 100	122	123	Vento X	PolG	0	0	0	68	10	0	0	73
	122	123		PolG	10	0	0	73	90	0	0	44
	122	123		Termico	AXY=15°C,AXZ=15°C							
	123	124		UnitG	0	0	0	8	89	0	0	8
IPE 100	123	124	Peso Proprio QV Solai	PolG	0	0	0	71	19	0	0	79
	123	124		PolG	0	0	0	79	89	0	0	40
	123	124		PolG	19	0	0	23	19	0	0	25
	123	124		PolG	19	0	0	25	89	0	0	13
IPE 100	123	124	Neve	PolG	0	0	0	44	19	0	0	49
	123	124		PolG	19	0	0	49	89	0	0	25
	123	124		PolG	0	0	0	68	19	0	0	76
	123	124		PolG	19	0	0	76	89	0	0	39

IPE 100	Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100		0	0	Neve	PolG	29	0	0	0	44	29	0	44
IPE 100		0	0	Neve	PolG	0	0	0	0	44	95	0	22
IPE 100		0	0	Neve	PolG	76	0	0	0	26	76	0	49
IPE 100		0	0	Neve	PolG	0	0	0	0	49	95	0	44
IPE 100		0	0	Neve	PolG	0	0	0	0	41	96	0	35
IPE 100		0	0	Neve	PolG	0	0	0	0	23	60	0	43
IPE 100		0	0	Neve	PolG	60	0	0	0	43	95	0	43
IPE 100		0	0	Neve	PolG	0	0	0	0	23	68	0	51
IPE 100		0	0	Neve	PolG	68	0	0	0	51	96	0	44
IPE 100		0	0	Neve	PolG	0	0	0	0	3	12	0	44
IPE 100		0	0	Neve	PolG	12	0	0	0	44	95	0	44
IPE 100		0	168	Neve	PolG	0	0	0	0	44	95	0	43
IPE 100		0	173	Neve	PolG	0	0	0	0	29	78	0	43
IPE 100		0	0	Neve	PolG	78	0	0	0	43	96	0	43
IPE 100		0	0	Neve	PolG	89	0	0	0	43	95	0	3
IPE 100		0	198	Neve	PolG	0	0	0	0	41	95	0	37
IPE 100		0	0	Neve	PolG	0	0	0	0	29	86	0	47
IPE 100		0	0	Neve	PolG	86	0	0	0	47	96	0	44
IPE 100		0	0	Neve	PolG	0	0	0	0	10	30	0	44
IPE 100		0	0	Neve	PolG	30	0	0	0	44	96	0	44
IPE 100		0	0	Neve	PolG	0	0	0	0	43	78	0	43
IPE 100		0	0	Neve	PolG	78	0	0	0	43	96	0	7
IPE 100		0	0	Neve	PolG	60	0	0	0	20	60	0	52
IPE 100		0	0	Neve	PolG	0	0	0	0	52	95	0	44
IPE 100		0	0	Neve	PolG	0	0	0	0	8	24	0	44
IPE 100		0	0	Neve	PolG	24	0	0	0	44	96	0	44
IPE 100		0	0	Neve	PolG	0	0	0	0	6	18	0	44
IPE 100		0	0	Neve	PolG	18	0	0	0	44	95	0	43
IPE 100		0	0	Neve	PolG	0	0	0	0	26	68	0	43
IPE 100		0	198	Neve	PolG	68	0	0	0	43	95	0	43
IPE 100		0	0	Neve	PolG	0	0	0	0	36	95	0	40
IPE 100		0	0	Neve	PolG	0	0	0	0	44	20	0	44
IPE 100		0	0	Neve	PolG	20	0	0	0	44	95	0	25
IPE 100		0	0	Neve	PolG	0	0	0	0	43	25	0	42
IPE 100		0	0	Neve	PolG	25	0	0	0	50	95	0	26
IPE 100		0	0	Vento X	PolG	0	0	0	0	31	60	0	80
IPE 100		0	0	Vento X	PolG	60	0	0	0	80	95	0	68
IPE 100		0	0	Vento X	PolG	0	0	0	0	67	78	0	67
IPE 100		0	0	Vento X	PolG	78	0	0	0	67	96	0	11
IPE 100		0	0	Vento X	PolG	0	0	0	0	9	18	0	68
IPE 100		0	0	Vento X	PolG	18	0	0	0	68	95	0	68
IPE 100		0	0	Vento X	PolG	0	0	0	0	39	68	0	67
IPE 100		0	0	Vento X	PolG	68	0	0	0	67	95	0	67
IPE 100		0	0	Vento X	PolG	0	0	0	0	12	24	0	68
IPE 100		0	0	Vento X	PolG	24	0	0	0	68	96	0	68
IPE 100		0	0	Vento X	PolG	0	0	0	0	68	20	0	68
IPE 100		0	0	Vento X	PolG	20	0	0	0	68	95	0	39
IPE 100		0	198	Vento X	PolG	0	0	0	0	56	95	0	61
IPE 100		0	198	Vento X	PolG	0	0	0	0	64	95	0	57
IPE 100		0	0	Vento X	PolG	0	0	0	0	15	30	0	68
IPE 100		0	0	Vento X	PolG	30	0	0	0	68	96	0	68
IPE 100		0	0	Vento X	PolG	0	0	0	0	67	25	0	77
IPE 100		0	0	Vento X	PolG	25	0	0	0	77	95	0	41
IPE 100		0	0	Vento X	PolG	0	0	0	0	5	12	0	68
IPE 100		0	0	Vento X	PolG	12	0	0	0	68	95	0	68
IPE 100		0	0	Vento X	PolG	0	0	0	0	67	89	0	67
IPE 100		0	0	Vento X	PolG	89	0	0	0	67	95	0	5
IPE 100		0	0	Vento X	PolG	0	0	0	0	57	96	0	65
IPE 100		0	0	Vento X	PolG	0	0	0	0	45	86	0	73
IPE 100		0	168	Vento X	PolG	86	0	0	0	73	96	0	68
IPE 100		0	0	Vento X	PolG	0	0	0	0	68	89	0	68
IPE 100		0	0	Vento X	PolG	89	0	0	0	68	95	0	1
IPE 100		0	0	Vento X	PolG	0	0	0	0	36	68	0	78
IPE 100		0	0	Vento X	PolG	68	0	0	0	78	96	0	68

IPE 100	Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100		0	0	Vento X	PolG	34	0	0	0	67	34	0	79
IPE 100		0	0	Vento X	PolG	0	0	0	0	79	96	0	36
IPE 100		0	0	Vento X	PolG	6	0	0	0	1	6	0	68
IPE 100		0	173	Vento X	PolG	0	0	0	0	68	95	0	68
IPE 100		0	0	Vento X	PolG	12	0	0	0	68	96	0	44
IPE 100		0	0	Vento X	PolG	0	0	0	0	67	16	0	74
IPE 100		0	0	Vento X	PolG	16	0	0	0	74	96	0	46
IPE 100		0	0	Vento X	PolG	60	0	0	0	35	60	0	67
IPE 100		0	0	Vento X	PolG	0	0	0	0	67	95	0	67
IPE 100		0	0	Vento X	PolG	83	0	0	0	67	95	0	67
IPE 100		0	0	Vento X	PolG	0	0	0	0	40	76	0	76
IPE 100		0	0	Vento X	PolG	76	0	0	0	76	95	0	68
IPE 100		0	0	Vento X	PolG	0	0	0	0	67	95	0	68
IPE 100		0	0	Vento X	PolG	0	0	0	0	67	41	0	80
IPE 100		0	0	Vento X	PolG	41	0	0	0	80	95	0	32
IPE 100		0	0	Vento X	PolG	0	0	0	0	68	29	0	68
IPE 100		0	0	Vento X	PolG	29	0	0	0	68	95	0	35
IPE 100		0	173	Vento X	PolG	0	0	0	0	45	78	0	67
IPE 100		0	0	Vento X	PolG	78	0	0	0	67	96	0	67
IPE 100		0	0	Vento X	PolG	71	0	0	0	67	96	0	15
IPE 100		0	168	Vento X	PolG	0	0	0	0	63	96	0	55
IPE 100		0	0	Vento X	PolG	0	0	0	0	68	95	0	67
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	198	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	168	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	173	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		0	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		153	188	Peso Proprio	UnitG	0	0	0	0	8	95	0	8
IPE 100		153	188	QP Solai	PolG	0	0	0	0	90	31	0	140
IPE 100		153	188			31	0	0	0	140	58	0	140
IPE 100		153	188	QV Solai	PolG	58	0	0	0	140	95	0	89
IPE 100		153	188			31	0	0	0	29	31	0	45
IPE 100		153	188			31	0	0	0	45	58	0	45
IPE 100		153	188	Neve	PolG	58	0	0	0	45	95	0	28
IPE 100		153	188	Neve	PolG	0	0	0	0	44	58	0	44
IPE 100		153	188	Neve	PolG	58	0	0	0	44	95	0	12
IPE 100		153	188	Neve	PolG	0	0	0	0	12	31	0	43
IPE 100		153	188	Vento X	PolG	31	0	0	0	43	95	0	43
IPE 100		153	188			0	0	0	0	19	31	0	67
IPE 100		153	188	Vento X	PolG	31	0	0	0	67	95	0	67
IPE 100		153	188	Vento X	PolG	0	0	0	0	68	58	0	68
IPE 100		153	188			58	0	0	0	68	95	0	19
IPE 100		153	188	Carchi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100		158	0	Peso Proprio	UnitG	0	0	0	0	8	96	0	8
IPE 100		158	0	QP Solai	PolG	0	0	0	0	103	38	0	130
IPE 100		158	0			38	0	0	0	130	52	0	130
IPE 100		158	0	QV Solai	PolG	52	0	0	0	130	96	0	101
IPE 100		158	0			0	0	0	0	33	38	0	42
IPE 100		158	0			38	0	0	0	42	52	0	42
IPE 100		158	0	Neve	PolG	52	0	0	0	42	96	0	32
IPE 100		158	0	Neve	PolG	0	0	0	0	44	38	0	44
IPE 100		158	0	Neve	PolG	38	0	0	0	44	96	0	20

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	158	0	Neve	PolG	0	0	0	0	20	52	0	0
IPE 100	158	0	Vento X	PolG	52	0	0	0	43	96	0	0
IPE 100	158	0	Vento X	PolG	52	0	0	0	31	52	0	0
IPE 100	158	0	Vento X	PolG	0	0	0	0	67	96	0	0
IPE 100	158	0		PolG	0	0	0	0	68	38	0	0
IPE 100	158	0		PolG	38	0	0	0	68	96	0	0
IPE 100	163	178	Carichi termici Peso Proprio QP Solai	Termico UnifG	AXY=15°C,AXZ=15°C	0	0	0	8	96	0	0
IPE 100	163	178		PolG	0	0	0	0	83	18	0	0
IPE 100	163	178		PolG	18	0	0	0	140	71	0	0
IPE 100	163	178		PolG	71	0	0	0	140	96	0	0
IPE 100	163	178	QV Solai	PolG	0	0	0	0	27	18	0	0
IPE 100	163	178		PolG	18	0	0	0	45	71	0	0
IPE 100	163	178		PolG	71	0	0	0	45	96	0	0
IPE 100	163	178	Neve	PolG	0	0	0	0	44	71	0	0
IPE 100	163	178		PolG	71	0	0	0	44	96	0	0
IPE 100	163	178	Neve	PolG	0	0	0	0	8	18	0	0
IPE 100	163	178		PolG	18	0	0	0	43	96	0	0
IPE 100	163	178	Vento X	PolG	0	0	0	0	12	18	0	0
IPE 100	163	178		PolG	18	0	0	0	67	96	0	0
IPE 100	163	178	Vento X	PolG	0	0	0	0	68	71	0	0
IPE 100	163	178		PolG	71	0	0	0	68	96	0	0
IPE 100	163	178	Carichi termici Peso Proprio QP Solai	Termico UnifG	AXY=15°C,AXZ=15°C	0	0	0	8	97	0	0
IPE 100	168	183		PolG	0	0	0	0	76	6	0	0
IPE 100	168	183		PolG	6	0	0	0	140	84	0	0
IPE 100	168	183	QV Solai	PolG	84	0	0	0	140	97	0	0
IPE 100	168	183		PolG	0	0	0	0	24	6	0	0
IPE 100	168	183		PolG	6	0	0	0	45	84	0	0
IPE 100	168	183	Neve	PolG	84	0	0	0	45	97	0	0
IPE 100	168	183		PolG	0	0	0	0	3	6	0	0
IPE 100	168	183	Neve	PolG	6	0	0	0	43	97	0	0
IPE 100	168	183		PolG	0	0	0	0	44	84	0	0
IPE 100	168	183	Vento X	PolG	84	0	0	0	44	97	0	0
IPE 100	168	183		PolG	0	0	0	0	5	6	0	0
IPE 100	168	183	Vento X	PolG	6	0	0	0	67	97	0	0
IPE 100	168	183		PolG	0	0	0	0	68	84	0	0
IPE 100	168	183		PolG	84	0	0	0	68	97	0	0
IPE 100	168	183	Carichi termici Peso Proprio QP Solai	Termico UnifG	AXY=15°C,AXZ=15°C	0	0	0	8	95	0	0
IPE 100	173	0		PolG	0	0	0	0	123	87	0	0
IPE 100	173	0	QV Solai	PolG	87	0	0	0	122	95	0	0
IPE 100	173	0		PolG	0	0	0	0	39	87	0	0
IPE 100	173	0	QV Solai	PolG	87	0	0	0	39	95	0	0
IPE 100	173	0	Neve	PolG	0	0	0	0	32	87	0	0
IPE 100	173	0		PolG	87	0	0	0	43	95	0	0
IPE 100	173	0	Neve	PolG	0	0	0	0	44	95	0	0
IPE 100	173	0	Vento X	PolG	0	0	0	0	50	87	0	0
IPE 100	173	0		PolG	87	0	0	0	67	95	0	0
IPE 100	173	0	Vento X	PolG	0	0	0	0	68	95	0	0
IPE 100	173	0	Carichi termici Peso Proprio QP Solai	Termico UnifG	AXY=15°C,AXZ=15°C	0	0	0	8	96	0	0
IPE 100	178	153		PolG	0	0	0	0	87	25	0	0
IPE 100	178	153	QV Solai	PolG	25	0	0	0	140	65	0	0
IPE 100	178	153		PolG	65	0	0	0	140	96	0	0
IPE 100	178	153	QV Solai	PolG	0	0	0	0	28	25	0	0
IPE 100	178	153		PolG	25	0	0	0	45	65	0	0
IPE 100	178	153	Neve	PolG	65	0	0	0	45	96	0	0
IPE 100	178	153	Neve	PolG	0	0	0	0	10	25	0	0
IPE 100	178	153		PolG	25	0	0	0	43	96	0	0
IPE 100	178	153	Neve	PolG	0	0	0	0	44	65	0	0
IPE 100	178	153	Vento X	PolG	65	0	0	0	68	65	0	0
IPE 100	178	153	Vento X	PolG	0	0	0	0	68	96	0	0
IPE 100	178	153		PolG	65	0	0	0	15	25	0	0
IPE 100	178	153	Vento X	PolG	0	0	0	0	15	25	0	0
IPE 100	178	153		PolG	25	0	0	0	67	96	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	178	153	Carichi termici Peso Proprio QP Solai	Termico UnifG	AXY=15°C,AXZ=15°C	0	0	0	8	95	0	0
IPE 100	183	163		PolG	0	0	0	0	79	12	0	0
IPE 100	183	163		PolG	12	0	0	0	140	76	0	0
IPE 100	183	163		PolG	76	0	0	0	140	95	0	0
IPE 100	183	163	QV Solai	PolG	0	0	0	0	25	12	0	0
IPE 100	183	163		PolG	12	0	0	0	45	76	0	0
IPE 100	183	163	Neve	PolG	76	0	0	0	45	95	0	0
IPE 100	183	163	Neve	PolG	0	0	0	0	5	12	0	0
IPE 100	183	163		PolG	12	0	0	0	43	95	0	0
IPE 100	183	163		PolG	0	0	0	0	44	76	0	0
IPE 100	183	163	Vento X	PolG	76	0	0	0	44	95	0	0
IPE 100	183	163	Vento X	PolG	0	0	0	0	68	76	0	0
IPE 100	183	163		PolG	76	0	0	0	68	95	0	0
IPE 100	183	163	Vento X	PolG	0	0	0	0	8	12	0	0
IPE 100	183	163		PolG	12	0	0	0	67	95	0	0
IPE 100	183	163	Carichi termici Peso Proprio QP Solai	Termico UnifG	AXY=15°C,AXZ=15°C	0	0	0	8	95	0	0
IPE 100	188	193		PolG	0	0	0	0	94	38	0	0
IPE 100	188	193		PolG	38	0	0	0	140	51	0	0
IPE 100	188	193	QV Solai	PolG	51	0	0	0	140	95	0	0
IPE 100	188	193		PolG	0	0	0	0	30	38	0	0
IPE 100	188	193	Neve	PolG	38	0	0	0	45	51	0	0
IPE 100	188	193	Neve	PolG	51	0	0	0	44	51	0	0
IPE 100	188	193		PolG	0	0	0	0	15	38	0	0
IPE 100	188	193	Vento X	PolG	38	0	0	0	23	38	0	0
IPE 100	188	193	Vento X	PolG	0	0	0	0	67	95	0	0
IPE 100	188	193		PolG	38	0	0	0	67	95	0	0
IPE 100	188	193	Vento X	PolG	0	0	0	0	68	51	0	0
IPE 100	188	193		PolG	51	0	0	0	68	95	0	0
IPE 100	188	193	Carichi termici Peso Proprio QP Solai	Termico UnifG	AXY=15°C,AXZ=15°C	0	0	0	8	96	0	0
IPE 100	193	158		PolG	0	0	0	0	98	45	0	0
IPE 100	193	158	QV Solai	PolG	45	0	0	0	140	96	0	0
IPE 100	193	158		PolG	0	0	0	0	31	45	0	0
IPE 100	193	158	Neve	PolG	45	0	0	0	45	96	0	0
IPE 100	193	158	Neve	PolG	0	0	0	0	17	45	0	0
IPE 100	193	158		PolG	45	0	0	0	43	96	0	0
IPE 100	193	158	Neve	PolG	0	0	0	0	44	45	0	0
IPE 100	193	158	Vento X	PolG	45	0	0	0	44	96	0	0
IPE 100	193	158	Vento X	PolG	0	0	0	0	68	45	0	0
IPE 100	193	158	Vento X	PolG	45	0	0	0	68	96	0	0
IPE 100	193	158		PolG	0	0	0	0	26	45	0	0
IPE 100	193	158	Vento X	PolG	0	0	0	0	67	96	0	0
IPE 100	193	158	Carichi termici Peso Proprio QP Solai	Termico UnifG	AXY=15°C,AXZ=15°C	0	0	0	8	95	0	0
IPE 100	198	0		PolG	0	0	0	0	121	6	0	0
IPE 100	198	0	QV Solai	PolG	6	0	0	0	126	95	0	0
IPE 100	198	0		PolG	0	0	0	0	39	6	0	0
IPE 100	198	0	Neve	PolG	6	0	0	0	40	95	0	0
IPE 100	198	0	Neve	PolG	0	0	0	0	43	6	0	0
IPE 100	198	0		PolG	6	0	0	0	45	95	0	0
IPE 100	198	0	Vento X	PolG	0	0	0	0	32	95	0	0
IPE 100	198	0	Vento X	PolG	0	0	0	0	67	6	0	0
IPE 100	198	0		PolG	6	0	0	0	70	95	0	0
IPE 100	198	0	Vento X	PolG	0	0	0	0	50	95	0	0
IPE 100	198	0	Carichi termici Peso Proprio QP Solai	Termico UnifG	AXY=15°C,AXZ=15°C	0	0	0	8	102	0	0
IPE 100	199	0		PolG	0	0	0	0	8	101	0	0
IPE 100	199	0	Peso Proprio	UnifG	0	0	0	0	8	101	0	0
IPE 100	199	0	Peso Proprio	UnifG	0	0	0	0	8	101	0	0
IPE 100	199	0	Peso Proprio	UnifG	0	0	0	0	8	102	0	0
IPE 100	199	0	Peso Proprio	UnifG	0	0	0	0	8	101	0	0
IPE 100	199	0	Peso Proprio	UnifG	0	0	0	0	8	102	0	0
IPE 100	199	0	Peso Proprio	UnifG	0	0	0	0	8	102	0	0
IPE 100	199	0	Peso Proprio	UnifG	0	0	0	0	8	102	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	Peso Proprio	UnifG	0	0	0	8	102	0	0	8
IPE 100	0	0	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	0	0	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	0	0	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	0	0	Peso Proprio	UnifG	0	0	0	8	102	0	0	8
IPE 100	0	0	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	0	0	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	0	0	Peso Proprio	UnifG	0	0	0	8	101	0	0	8
IPE 100	0	0	Peso Proprio	UnifG	0	0	0	8	102	0	0	8
IPE 100	0	0	QP Solai	PolG	0	0	0	112	31	0	0	141
					31	0	0	141	76	0	0	139
IPE 100	0	0	QP Solai	PolG	76	0	0	139	101	0	0	114
					40	0	0	108	40	0	0	149
					40	0	0	149	68	0	0	147
IPE 100	0	0	QP Solai	PolG	68	0	0	147	102	0	0	109
					30	0	0	86	30	0	0	139
					77	0	0	139	77	0	0	139
IPE 100	0	0	QP Solai	PolG	0	0	0	139	102	0	0	86
					22	0	0	118	22	0	0	137
					86	0	0	137	86	0	0	134
IPE 100	0	0	QP Solai	PolG	0	0	0	134	102	0	0	120
					35	0	0	108	35	0	0	126
					60	0	0	126	60	0	0	126
IPE 100	0	0	QP Solai	PolG	0	0	0	126	101	0	0	107
					18	0	0	79	18	0	0	139
					89	0	0	139	89	0	0	138
IPE 100	0	0	QP Solai	PolG	0	0	0	138	101	0	0	79
					26	0	0	113	26	0	0	123
					68	0	0	123	68	0	0	123
IPE 100	0	0	QP Solai	PolG	0	0	0	123	101	0	0	111
					47	0	0	103	47	0	0	158
					60	0	0	158	60	0	0	157
IPE 100	0	169	QP Solai	PolG	0	0	0	157	101	0	0	104
					95	0	0	140	95	0	0	139
IPE 100	0	199	QP Solai	PolG	0	0	0	139	101	0	0	71
IPE 100	0	0	QP Solai	PolG	0	0	0	130	101	0	0	130
					98	0	0	130	98	0	0	129
IPE 100	0	0	QP Solai	PolG	0	0	0	129	102	0	0	129
					6	0	0	71	6	0	0	139
IPE 100	0	0	QP Solai	PolG	0	0	0	139	101	0	0	140
					24	0	0	82	24	0	0	139
IPE 100	0	0	QP Solai	PolG	0	0	0	82	24	0	0	139
					84	0	0	139	84	0	0	139
IPE 100	0	174	QP Solai	PolG	0	0	0	139	102	0	0	82
					18	0	0	119	18	0	0	124
					78	0	0	124	78	0	0	123
IPE 100	0	0	QP Solai	PolG	0	0	0	123	102	0	0	117
					12	0	0	74	12	0	0	138
					95	0	0	138	95	0	0	139
IPE 100	0	0	QV Solai	PolG	0	0	0	139	101	0	0	74
					30	0	0	27	30	0	0	44
					30	0	0	44	77	0	0	44
IPE 100	0	0	QP Solai	PolG	0	0	0	44	102	0	0	28
					77	0	0	44	102	0	0	42
IPE 100	0	199	QV Solai	PolG	0	0	0	42	101	0	0	44
IPE 100	0	0	QV Solai	PolG	0	0	0	23	6	0	0	44
					6	0	0	44	101	0	0	45
IPE 100	0	0	QV Solai	PolG	0	0	0	38	22	0	0	44
					22	0	0	44	86	0	0	43
					86	0	0	43	102	0	0	39
IPE 100	0	0	QV Solai	PolG	0	0	0	35	40	0	0	48
					40	0	0	48	68	0	0	47
IPE 100	0	0	QV Solai	PolG	68	0	0	47	102	0	0	35
					31	0	0	36	31	0	0	45
					76	0	0	45	76	0	0	44
IPE 100	0	174	QV Solai	PolG	0	0	0	44	101	0	0	37
					18	0	0	38	18	0	0	40
					18	0	0	40	78	0	0	40

Sezione	Ni	Nf	Cond.	Tiplo c.	Xi	QXgi	QZi	Xf	QXf	QVf	QZF
IPE 100	0	169	QV Solai	PolG	78	0	0	40	192	0	38
					0	0	0	45	95	0	0
IPE 100	0	0	QV Solai	PolG	95	0	0	44	101	0	23
					0	0	0	42	98	0	41
IPE 100	0	0	QV Solai	PolG	98	0	0	41	102	0	41
					0	0	0	25	18	0	44
IPE 100	0	0	QV Solai	PolG	18	0	0	44	89	0	44
					89	0	0	44	101	0	25
IPE 100	0	0	QV Solai	PolG	0	0	0	35	35	0	40
					35	0	0	40	60	0	41
IPE 100	0	0	QV Solai	PolG	60	0	0	41	101	0	34
					0	0	0	33	47	0	51
IPE 100	0	0	QV Solai	PolG	47	0	0	51	60	0	50
					60	0	0	50	101	0	33
IPE 100	0	0	QV Solai	PolG	0	0	0	26	24	0	44
					24	0	0	44	84	0	44
IPE 100	0	0	QV Solai	PolG	84	0	0	44	102	0	26
					0	0	0	24	12	0	44
IPE 100	0	0	QV Solai	PolG	12	0	0	44	95	0	44
					0	0	0	44	101	0	24
IPE 100	0	0	QV Solai	PolG	95	0	0	36	26	0	39
					0	0	0	39	68	0	39
IPE 100	0	0	Neve	PolG	68	0	0	39	101	0	36
					0	0	0	6	18	0	43
IPE 100	0	174	Neve	PolG	18	0	0	43	101	0	43
					0	0	0	43	18	0	43
IPE 100	0	169	Neve	PolG	18	0	0	43	102	0	30
					0	0	0	43	95	0	43
IPE 100	0	0	Neve	PolG	95	0	0	43	101	0	1
					0	0	0	43	84	0	43
IPE 100	0	0	Neve	PolG	84	0	0	43	102	0	8
					0	0	0	43	24	0	43
IPE 100	0	0	Neve	PolG	24	0	0	43	102	0	43
					0	0	0	42	102	0	37
IPE 100	0	0	Neve	PolG	0	0	0	43	26	0	43
					26	0	0	43	101	0	26
IPE 100	0	0	Neve	PolG	0	0	0	27	68	0	43
					68	0	0	43	101	0	43
IPE 100	0	0	Neve	PolG	0	0	0	43	47	0	53
					47	0	0	53	101	0	22
IPE 100	0	0	Neve	PolG	0	0	0	10	30	0	43
					30	0	0	43	102	0	43
IPE 100	0	0	Neve	PolG	0	0	0	43	89	0	43
					89	0	0	43	101	0	6
IPE 100	0	0	Neve	PolG	0	0	0	21	60	0	52
					60	0	0	52	101	0	43
IPE 100	0	0	Neve	PolG	0	0	0	39	98	0	43
					98	0	0	43	102	0	43
IPE 100	0	0	Neve	PolG	0	0	0	43	40	0	53
					40	0	0	53	102	0	25
IPE 100	0	174	Neve	PolG	0	0	0	31	78	0	43
					78	0	0	43	102	0	43
IPE 100	0	199	Neve	PolG	0	0	0	37	101	0	41
					0	0	0	24	60	0	43
IPE 100	0	0	Neve	PolG	0	0	0	43	101	0	43
					60	0	0	43	35	0	43
IPE 100	0	0	Neve	PolG	0	0	0	43	101	0	23
					35	0	0	43	101	0	43
IPE 100	0	0	Neve	PolG	0	0	0	3	12	0	43
					12	0	0	43	101	0	43
IPE 100	0	199	Neve	PolG	0	0	0	44	101	0	40
					0	0	0	24	68	0	51
IPE 100	0	0	Neve	PolG	0	0	0	51	102	0	43
					68	0	0	43	77	0	43
IPE 100	0	0	Neve	PolG	0	0	0	43	102	0	10
					77	0	0	44	101	0	43
IPE 100	0	169	Neve	PolG	0	0	0	44	101	0	43
					0	0	0	43	95	0	43

Sezione	Ni	NF	Cond.	Type c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZF
IPE 100	0	0	Neve	PoG	95	0	0	0	43	76	0	3
IPE 100					76	0	0	0	27	76	0	50
IPE 100	0	0	Neve	PoG	0	0	0	0	50	101	0	43
IPE 100	0	0	Neve	PoG	22	0	0	0	43	22	0	50
IPE 100	0	0	Neve	PoG	0	0	0	0	50	102	0	32
IPE 100	0	0	Neve	PoG	6	0	0	0	1	6	0	43
IPE 100	0	0	Neve	PoG	0	0	0	0	43	101	0	43
IPE 100	0	0	Neve	PoG	86	0	0	0	30	86	0	48
IPE 100	0	0	Neve	PoG	0	0	0	0	48	102	0	43
IPE 100	0	0	Neve	PoG	0	0	0	0	43	31	0	52
IPE 100	0	0	Neve	PoG	31	0	0	0	52	101	0	28
IPE 100	0	0	Neve	PoG	0	0	0	0	43	101	0	44
IPE 100	174		Vento X	PoG	0	0	0	0	67	18	0	67
IPE 100	0	0			18	0	0	0	67	102	0	46
IPE 100	0	0	Vento X	PoG	0	0	0	0	37	68	0	79
IPE 100	0	0	Vento X	PoG	68	0	0	0	79	102	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	33	60	0	80
IPE 100			Vento X	PoG	60	0	0	0	80	101	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	77	0	67
IPE 100			Vento X	PoG	77	0	0	0	67	102	0	16
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	40	0	82
IPE 100	0	0	Vento X	PoG	40	0	0	0	82	102	0	38
IPE 100	0	0	Vento X	PoG	0	0	0	0	37	60	0	67
IPE 100			Vento X	PoG	60	0	0	0	67	101	0	67
IPE 100	0	174	Vento X	PoG	78	0	0	0	48	78	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	102	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	101	0	68
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	35	0	67
IPE 100			Vento X	PoG	35	0	0	0	67	101	0	36
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	47	0	82
IPE 100			Vento X	PoG	47	0	0	0	82	101	0	34
IPE 100	0	0	Vento X	PoG	0	0	0	0	16	30	0	67
IPE 100			Vento X	PoG	30	0	0	0	67	102	0	67
IPE 100	0	169	Vento X	PoG	0	0	0	0	67	95	0	67
IPE 100			Vento X	PoG	95	0	0	0	67	101	0	1
IPE 100	0	169	Vento X	PoG	0	0	0	0	68	101	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	60	98	0	67
IPE 100			Vento X	PoG	98	0	0	0	67	102	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	42	76	0	77
IPE 100			Vento X	PoG	76	0	0	0	77	101	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	1	6	0	67
IPE 100	0	0	Vento X	PoG	6	0	0	0	67	101	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	84	0	67
IPE 100			Vento X	PoG	84	0	0	0	67	102	0	12
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	26	0	67
IPE 100			Vento X	PoG	26	0	0	0	67	101	0	40
IPE 100	0	0	Vento X	PoG	0	0	0	0	12	24	0	67
IPE 100	0	0	Vento X	PoG	24	0	0	0	67	102	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	5	12	0	67
IPE 100			Vento X	PoG	12	0	0	0	67	101	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	42	68	0	67
IPE 100			Vento X	PoG	68	0	0	0	67	101	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	65	102	0	57
IPE 100	0	199	Vento X	PoG	0	0	0	0	58	101	0	64
IPE 100	0	0	Vento X	PoG	0	0	0	0	47	86	0	74
IPE 100			Vento X	PoG	86	0	0	0	74	102	0	67
IPE 100	0	199	Vento X	PoG	0	0	0	0	68	101	0	61
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	31	0	80
IPE 100	0	0	Vento X	PoG	31	0	0	0	80	101	0	43
IPE 100			Vento X	PoG	0	0	0	0	67	89	0	67
IPE 100			Vento X	PoG	89	0	0	0	67	101	0	9
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	95	0	67
IPE 100			Vento X	PoG	95	0	0	0	67	101	0	5
IPE 100	0	0	Vento X	PoG	0	0	0	0	9	18	0	67
IPE 100	0	0	Vento X	PoG	18	0	0	0	67	101	0	67
IPE 100	0	0	Vento X	PoG	0	0	0	0	67	22	0	77

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	169	Carichi termici	Termico	22	0	0	0	102	0	0	49
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	199	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	174	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	154	189	Peso Proprio	Unitif	0	0	0	8	101	0	0	8
IPE 100	154	189	QP Solai	Polig	0	0	0	90	31	0	0	139
					31	0	0	139	64	0	0	139
IPE 100	154	189	QV Solai	Polig	64	0	0	139	101	0	0	90
					0	0	0	29	31	0	0	44
					31	0	0	44	64	0	0	44
IPE 100	154	189	Neve	Polig	64	0	0	44	101	0	0	29
					0	0	0	13	31	0	0	43
IPE 100	154	189	Neve	Polig	31	0	0	43	101	0	0	43
					0	0	0	43	64	0	0	43
IPE 100	154	189	Vento X	Polig	64	0	0	40	101	0	0	13
					0	0	0	23	31	0	0	67
IPE 100	154	189	Vento X	Polig	31	0	0	67	101	0	0	67
					0	0	0	67	64	0	0	67
IPE 100	154	189	Vento X	Polig	64	0	0	67	101	0	0	20
					AXY=15°C,AXZ=15°C							
IPE 100	154	189	Carichi termici	Termico	0	0	0	8	102	0	0	8
IPE 100	159	0	Peso Proprio	Unitif	0	0	0	103	43	0	0	133
IPE 100	159	0	QP Solai	Polig	43	0	0	133	52	0	0	133
					52	0	0	133	102	0	0	102
IPE 100	159	0	QV Solai	Polig	0	0	0	33	43	0	0	42
					43	0	0	42	52	0	0	43
IPE 100	159	0	Neve	Polig	52	0	0	43	102	0	0	33
					0	0	0	43	43	0	0	43
IPE 100	159	0	Neve	Polig	43	0	0	43	102	0	0	21
					0	0	0	21	52	0	0	43
IPE 100	159	0	Vento X	Polig	52	0	0	43	102	0	0	43
					0	0	0	33	52	0	0	67
IPE 100	159	0	Vento X	Polig	52	0	0	67	102	0	0	67
					0	0	0	67	43	0	0	67
IPE 100	159	0	Vento X	Polig	0	0	0	67	102	0	0	32
					43	0	0	67	102	0	0	32
IPE 100	159	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	164	179	Peso Proprio	Unitif	0	0	0	8	102	0	0	8
IPE 100	164	179	QP Solai	Polig	0	0	0	83	18	0	0	138
					18	0	0	138	77	0	0	139
					77	0	0	139	102	0	0	82
IPE 100	164	179	QV Solai	Polig	0	0	0	26	18	0	0	44
					18	0	0	44	77	0	0	44
					77	0	0	44	102	0	0	26
IPE 100	164	179	Neve	Polig	0	0	0	8	18	0	0	43
					18	0	0	43	102	0	0	43
IPE 100	164	179	Neve	Polig	0	0	0	43	77	0	0	43
					77	0	0	43	102	0	0	8
IPE 100	164	179	Vento X	Polig	0	0	0	67	77	0	0	67
					77	0	0	67	102	0	0	13
IPE 100	164	179	Vento X	Polig	0	0	0	13	18	0	0	67
					18	0	0	67	102	0	0	67
IPE 100	164	179	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	169	184	Peso Proprio	Unitif	0	0	0	8	103	0	0	8

Sezione	Ni	Nf	Cond.	Tiplo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	169	184	QP Solai	PolG	6	0	0	0	75	6	0	138
	169	184		PolG	6	0	0	0	138	90	0	139
				90	0	0	0	0	139	103	0	75
IPE 100	169	184	QV Solai	PolG	0	0	0	0	24	6	0	44
				6	0	0	0	0	24	90	0	44
				90	0	0	0	0	44	103	0	24
IPE 100	169	184	Neve	PolG	0	0	0	4	6	0	0	43
				6	0	0	0	0	43	103	0	43
				90	0	0	0	0	43	90	0	43
IPE 100	169	184	Neve	PolG	0	0	0	0	43	103	0	4
				90	0	0	0	0	67	90	0	67
				90	0	0	0	0	67	103	0	6
IPE 100	169	184	Vento X	PolG	0	0	0	0	6	6	0	67
				6	0	0	0	0	67	103	0	67
				6	0	0	0	0	67	103	0	67
IPE 100	169	184	Carichi termici	Termico	ΔXY=15°C;ΔXZ=15°C							
				UnifG	0	0	0	0	8	101	0	8
				PolG	0	0	0	0	125	7	0	126
			QP Solai	PolG	7	0	0	0	126	87	0	125
				87	0	0	0	125	101	0	122	
				87	0	0	0	40	7	0	40	
IPE 100	174	0	QV Solai	PolG	0	0	0	0	40	7	0	40
				7	0	0	0	40	87	0	40	
				87	0	0	0	40	101	0	39	
IPE 100	174	0	Neve	PolG	0	0	0	0	43	7	0	43
				7	0	0	0	43	101	0	33	
				7	0	0	0	35	87	0	43	
IPE 100	174	0	Neve	PolG	0	0	0	0	43	101	0	43
				87	0	0	0	67	7	0	67	
				7	0	0	0	67	101	0	51	
IPE 100	174	0	Vento X	PolG	0	0	0	0	53	87	0	67
				87	0	0	0	67	101	0	67	
				87	0	0	0	67	101	0	67	
IPE 100	174	0	Carichi termici	Termico	ΔXY=15°C;ΔXZ=15°C							
				UnifG	0	0	0	0	8	102	0	8
				PolG	0	0	0	0	86	25	0	139
IPE 100	179	154	QP Solai	PolG	25	0	0	0	139	71	0	139
				71	0	0	0	139	102	0	86	
				71	0	0	0	28	25	0	44	
IPE 100	179	154	QV Solai	PolG	0	0	0	0	28	25	0	44
				25	0	0	0	44	71	0	44	
				71	0	0	0	44	102	0	27	
IPE 100	179	154	Neve	PolG	0	0	0	0	43	71	0	43
				71	0	0	0	43	102	0	10	
				71	0	0	0	10	25	0	43	
IPE 100	179	154	Neve	PolG	0	0	0	0	10	25	0	43
				25	0	0	0	43	102	0	43	
				71	0	0	0	67	71	0	67	
IPE 100	179	154	Vento X	PolG	0	0	0	0	67	102	0	16
				71	0	0	0	67	102	0	67	
				71	0	0	0	16	25	0	67	
IPE 100	179	154	Vento X	PolG	0	0	0	0	67	102	0	67
				25	0	0	0	67	102	0	67	
				25	0	0	0	67	102	0	67	
IPE 100	179	154	Carichi termici	Termico	ΔXY=15°C;ΔXZ=15°C							
				UnifG	0	0	0	0	8	101	0	8
				PolG	0	0	0	0	78	12	0	139
IPE 100	184	164	Peso Proprio	PolG	12	0	0	0	139	82	0	138
				82	0	0	0	138	101	0	78	
				82	0	0	0	25	12	0	44	
IPE 100	184	164	QV Solai	PolG	0	0	0	0	25	12	0	44
				12	0	0	0	44	82	0	44	
				82	0	0	0	44	101	0	25	
IPE 100	184	164	Neve	PolG	0	0	0	0	6	12	0	43
				12	0	0	0	43	101	0	43	
				12	0	0	0	43	82	0	43	
IPE 100	184	164	Neve	PolG	0	0	0	0	43	101	0	43
				82	0	0	0	67	82	0	67	
				82	0	0	0	67	82	0	67	
IPE 100	184	164	Vento X	PolG	0	0	0	0	67	101	0	9
				82	0	0	0	9	12	0	67	
				82	0	0	0	9	12	0	67	
IPE 100	184	164	Vento X	PolG	0	0	0	0	67	101	0	67
				12	0	0	0	67	101	0	67	
				12	0	0	0	67	101	0	67	
IPE 100	184	164	Carichi termici	Termico	ΔXY=15°C;ΔXZ=15°C							
				UnifG	0	0	0	0	8	101	0	8
				PolG	0	0	0	0	94	38	0	139
IPE 100	189	194	Peso Proprio	PolG	38	0	0	0	139	57	0	139
				38	0	0	0	94	38	0	139	
				38	0	0	0	94	38	0	139	

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf	
IPE 100	189	194	QV Solai	PolG	57	0	0	139	101	0	0	94	
								30	38	0	0	44	
					38	0	0	44	57	0	0	44	
IPE 100	189	194	Neve	PolG	57	0	0	44	101	0	0	30	
								16	38	0	0	43	
					38	0	0	43	101	0	0	43	
IPE 100	189	194	Neve	PolG	38	0	0	43	57	0	0	43	
								43	57	0	0	15	
					57	0	0	43	101	0	0	67	
IPE 100	189	194	Vento X	PolG	57	0	0	67	57	0	0	67	
								67	101	0	0	24	
					57	0	0	67	101	0	0	67	
IPE 100	189	194	Vento X	PolG	38	0	0	24	38	0	0	67	
								67	101	0	0	67	
					38	0	0	67	101	0	0	67	
IPE 100	189	194	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$								
					UnifG	0	0	0	8	101	0	0	8
						PolG	0	0	0	98	45	0	0
IPE 100	194	159	Peso Proprio	UnifG	45	0	0	139	50	0	0	139	
					PolG	50	0	0	139	101	0	0	98
						50	0	0	32	45	0	0	44
IPE 100	194	159	QV Solai	PolG	45	0	0	44	50	0	0	44	
								44	50	0	0	31	
					50	0	0	44	101	0	0	43	
IPE 100	194	159	Neve	PolG	45	0	0	43	101	0	0	43	
								43	101	0	0	43	
					PolG	0	0	0	43	50	0	0	18
IPE 100	194	159	Vento X	PolG	50	0	0	43	101	0	0	18	
								43	101	0	0	67	
					PolG	0	0	0	28	45	0	0	67
IPE 100	194	159	Vento X	PolG	45	0	0	67	101	0	0	67	
								67	50	0	0	67	
					PolG	0	0	0	67	101	0	0	27
IPE 100	194	159	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$								
					UnifG	0	0	0	8	101	0	0	8
						PolG	0	0	0	123	12	0	0
IPE 100	199	0	Peso Proprio	UnifG	12	0	0	133	95	0	0	131	
					PolG	95	0	0	131	101	0	0	126
						95	0	0	40	12	0	0	42
IPE 100	199	0	QV Solai	PolG	12	0	0	42	95	0	0	42	
								42	95	0	0	40	
					95	0	0	34	95	0	0	45	
IPE 100	199	0	Neve	PolG	95	0	0	45	101	0	0	43	
								45	101	0	0	47	
					PolG	0	0	0	43	12	0	0	35
IPE 100	199	0	Vento X	PolG	12	0	0	47	101	0	0	35	
								52	95	0	0	70	
					PolG	0	0	0	70	101	0	0	67
IPE 100	199	0	Vento X	PolG	95	0	0	67	12	0	0	73	
								67	12	0	0	73	
					PolG	0	0	0	73	101	0	0	55
IPE 100	199	0	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$								
					UnifG	0	0	0	8	107	0	0	8
						PolG	0	0	0	123	12	0	0
IPE 100	170	0	Peso Proprio	UnifG	12	0	0	133	95	0	0	126	
					PolG	95	0	0	131	101	0	0	42
						95	0	0	42	95	0	0	40
IPE 100	0	0	Neve	PolG	95	0	0	34	95	0	0	45	
								45	101	0	0	43	
					PolG	0	0	0	43	12	0	0	47
IPE 100	0	0	Neve	PolG	12	0	0	47	101	0	0	35	
								52	95	0	0	70	
					PolG	0	0	0	70	101	0	0	67
IPE 100	199	0	Vento X	PolG	95	0	0	67	12	0	0	73	
								67	12	0	0	73	
					PolG	0	0	0	73	101	0	0	55
IPE 100	199	0	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$								
					UnifG	0	0	0	8	107	0	0	8
						PolG	0	0	0	123	12	0	0
IPE 100	0	0	Peso Proprio	UnifG	12	0	0	133	95	0	0	126	
					PolG	95	0	0	131	101	0	0	42
						95	0	0	42	95	0	0	40
IPE 100	0	0	Neve	PolG	95	0	0	34	95	0	0	45	
								45	101	0	0	43	
					PolG	0	0	0	43	12	0	0	47
IPE 100	0	0	Neve	PolG	12	0	0	47	101	0	0	35	
								52	95	0	0	70	
					PolG	0	0	0	70	101	0	0	67
IPE 100	199	0	Vento X	PolG	95	0	0	67	12	0	0	73	
								67	12	0	0	73	
					PolG	0	0	0	73	101	0	0	55
IPE 100	199	0	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$								
					UnifG	0	0	0	8	107	0	0	8
						PolG	0	0	0	123	12	0	0
IPE 100	0	0	Peso Proprio	UnifG	12	0	0	133	95	0	0	126	
					PolG	95	0	0	131	101	0	0	42
						95	0	0	42	95	0	0	40
IPE 100	0	0	Neve	PolG	95	0	0	34	95	0	0	45	
								45	101	0	0	43	
					PolG	0	0	0	43	12	0	0	47
IPE 100	0	0	Neve	PolG	12	0	0	47	101	0	0	35	
								52	95	0	0	70	
					PolG	0	0	0	70	101	0	0	67
IPE 100	199	0	Vento X	PolG	95	0	0	67	12	0	0	73	
								67	12	0	0	73	
					PolG	0	0	0	73	101	0	0	55
IPE 100	199	0	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$								
					UnifG	0	0	0	8	107	0	0	8
						PolG	0	0	0	123	12	0	0
IPE 100	0	0	Peso Proprio	UnifG	12	0	0	133	95	0	0	126	
					PolG	95	0	0	131	101	0	0	42
						95	0	0	42	95	0	0	40
IPE 100	0	0	Neve	PolG	95	0	0	34	95	0	0	45	
								45	101	0	0	43	
					PolG	0	0	0	43	12	0	0	47
IPE 100	0	0	Neve	PolG	12	0	0	47	101	0	0	35	
								52	95	0	0	70	
					PolG	0	0	0	70	101	0	0	67
IPE 100	199	0	Vento X	PolG	95	0	0	67	12	0	0	73	
								67	12	0	0	73	
					PolG	0	0	0	73	101	0	0	55
IPE 100	199	0	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$								
					UnifG	0	0	0	8	107	0	0	8
						PolG	0	0	0	123	12	0	0
IPE 100	0	0	Peso Proprio	UnifG	12	0	0	133	95	0	0	126	
					PolG	95	0	0	131	101	0	0	42
						95	0	0	42	95	0	0	40
IPE 100	0	0	Neve	PolG	95	0	0	34	95	0	0	45	
								45	101	0	0	43	
					PolG	0	0	0	43	12	0	0	47
IPE 100	0	0	Neve	PolG	12	0	0	47	101	0	0	35	
								52	95	0	0	70	
					PolG	0	0	0	70	101	0	0	67
IPE 100	199	0	Vento X	PolG	95	0	0	67	12	0	0	73	
								67	12	0	0	73	
					PolG	0	0	0	73	101	0	0	55
IPE 100	199	0	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$								
					UnifG	0	0	0	8	107	0	0	8
						PolG	0	0	0	123	12	0	0
IPE 100	0	0	Peso Proprio	UnifG	12	0	0	133	95	0	0	126	
					PolG	95	0	0	131	101	0	0	42
						95	0	0	42	95	0	0	40
IPE 100	0	0	Neve	PolG	95	0	0	34	95	0	0	45	
								45	101	0	0	43	
					PolG	0	0	0	43	12	0	0	47
IPE 100	0	0	Neve	PolG	12	0	0	47	101	0	0	35	
								52	95	0	0	70	
					PolG	0	0	0	70	101	0	0	67
IPE 100	199	0	Vento X	PolG	95	0	0	67	12	0	0	73	
								67	12	0	0	73	
					PolG	0	0	0	73	101	0	0	55
IPE 100	199	0	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$								
					UnifG	0	0	0	8	107	0	0	8
						PolG	0	0	0	123	12	0	0
IPE 100	0	0	Peso Proprio	UnifG	12	0	0	133	95	0	0	126	
					PolG	95	0	0	131	101	0	0	42
						95	0	0	42	95	0	0	40
IPE 100	0	0	Neve	PolG	95	0	0	34	95	0	0	45	
								45	101	0	0	43	
					PolG	0	0	0	43	12	0	0	47
IPE 100	0	0	Neve	PolG	12	0	0	47	101	0	0	35	
								52	95	0	0	70	
					PolG	0	0	0	70	101	0	0	67
IPE 100	199	0	Vento X	PolG	95	0	0	67	12	0	0	73	
								67	12	0	0	73	
					PolG	0	0	0	73	101	0	0	55
IPE 100	199	0	Carichi termici	Termico	$\Delta XY=15^{\circ}C, \Delta XZ=15^{\circ}C$								
					UnifG	0	0	0	8	107	0	0	8
						PolG	0	0	0	123	12	0	0
IPE 100	0	0	Peso Proprio	UnifG	12	0	0	133	95	0	0	126	
					PolG	95	0	0	131	101	0	0	42
						95	0	0	42	95	0	0	40
IPE 100	0	0	Neve	PolG	95	0	0	34	95	0	0	45	
								45	101	0	0	43	

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	QP Solai	PolG	68	0	0	0	116	107	0	104
					0	0	0	0	104	41	0	121
					41	0	0	0	121	60	0	120
IPE 100	0	170	QP Solai	PolG	60	0	0	0	120	107	0	99
					0	0	0	0	130	101	0	128
IPE 100	0	0	QP Solai	PolG	101	0	0	0	128	107	0	61
					0	0	0	0	61	6	0	128
IPE 100	0	200	QP Solai	PolG	6	0	0	0	128	107	0	130
					0	0	0	0	123	8	0	127
IPE 100	0	0	QP Solai	PolG	8	0	0	0	127	106	0	128
					106	0	0	0	58	107	0	57
IPE 100	0	0	QP Solai	PolG	0	0	0	0	69	18	0	128
					18	0	0	0	128	95	0	128
IPE 100	0	0	QP Solai	PolG	95	0	0	0	128	107	0	78
					12	0	0	0	64	12	0	128
IPE 100	0	0	QP Solai	PolG	101	0	0	0	128	107	0	74
					0	0	0	0	76	30	0	128
IPE 100	0	0	QP Solai	PolG	30	0	0	0	128	83	0	128
					83	0	0	0	128	108	0	84
IPE 100	0	0	QP Solai	PolG	0	0	0	0	105	37	0	137
					37	0	0	0	137	76	0	138
IPE 100	0	0	QP Solai	PolG	76	0	0	0	138	107	0	110
					28	0	0	0	111	28	0	132
IPE 100	0	0	QP Solai	PolG	0	0	0	0	132	86	0	133
					86	0	0	0	133	108	0	115
IPE 100	0	0	QP Solai	PolG	0	0	0	0	72	24	0	128
					24	0	0	0	128	90	0	128
IPE 100	0	175	QP Solai	PolG	90	0	0	0	128	108	0	81
					0	0	0	0	114	24	0	119
IPE 100	0	0	QP Solai	PolG	24	0	0	0	119	78	0	116
					78	0	0	0	116	108	0	110
IPE 100	0	0	QP Solai	PolG	0	0	0	0	95	53	0	155
					53	0	0	0	155	60	0	155
IPE 100	0	0	QP Solai	PolG	60	0	0	0	155	107	0	101
					0	0	0	0	126	4	0	126
IPE 100	0	0	QP Solai	PolG	4	0	0	0	126	98	0	122
					98	0	0	0	122	108	0	122
IPE 100	0	0	QP Solai	PolG	0	0	0	0	35	28	0	42
					28	0	0	0	42	86	0	43
IPE 100	0	200	QP Solai	PolG	86	0	0	0	43	108	0	37
					8	0	0	0	39	8	0	41
IPE 100	0	0	QP Solai	PolG	106	0	0	0	41	106	0	41
					0	0	0	0	18	107	0	18
IPE 100	0	0	QP Solai	PolG	0	0	0	0	33	41	0	39
					41	0	0	0	39	60	0	38
IPE 100	0	0	QP Solai	PolG	60	0	0	0	38	107	0	32
					0	0	0	0	19	6	0	41
IPE 100	0	0	QP Solai	PolG	6	0	0	0	41	107	0	42
					32	0	0	0	35	32	0	38
IPE 100	0	0	QP Solai	PolG	32	0	0	0	38	68	0	37
					68	0	0	0	37	107	0	33
IPE 100	0	0	QP Solai	PolG	0	0	0	0	32	46	0	46
					46	0	0	0	46	68	0	46
IPE 100	0	0	QP Solai	PolG	68	0	0	0	46	108	0	34
					30	0	0	0	24	30	0	41
IPE 100	0	170	QP Solai	PolG	83	0	0	0	41	108	0	27
					0	0	0	0	42	101	0	41
IPE 100	0	0	QP Solai	PolG	101	0	0	0	41	107	0	19
					18	0	0	0	22	18	0	41
IPE 100	0	175	QP Solai	PolG	95	0	0	0	41	107	0	25
					24	0	0	0	37	24	0	38
IPE 100	0	0	QP Solai	PolG	78	0	0	0	37	108	0	35

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	QV Solai	PolG	37	0	0	0	34	37	0	44
					76	0	0	0	44	107	0	35
IPE 100	0	0	QV Solai	PolG	12	0	0	0	41	101	0	41
					101	0	0	0	41	107	0	24
IPE 100	0	0	QV Solai	PolG	0	0	0	0	23	24	0	41
					24	0	0	0	41	90	0	41
IPE 100	0	0	QV Solai	PolG	90	0	0	0	41	108	0	26
					53	0	0	0	30	53	0	50
IPE 100	0	0	QV Solai	PolG	60	0	0	0	50	107	0	32
					4	0	0	0	40	4	0	40
IPE 100	0	0	Neve	PolG	4	0	0	0	40	108	0	39
					12	0	0	0	43	107	0	43
IPE 100	0	0	Neve	PolG	0	0	0	0	37	95	0	37
					95	0	0	0	37	107	0	5
IPE 100	0	0	Neve	PolG	0	0	0	0	43	41	0	43
					41	0	0	0	43	107	0	25
IPE 100	0	0	Neve	PolG	0	0	0	0	37	101	0	37
					101	0	0	0	37	107	0	3
IPE 100	0	0	Neve	PolG	0	0	0	0	43	4	0	43
					4	0	0	0	43	108	0	39
IPE 100	0	0	Neve	PolG	0	0	0	0	43	32	0	43
					32	0	0	0	43	107	0	28
IPE 100	0	0	Neve	PolG	0	0	0	0	24	68	0	37
					68	0	0	0	37	107	0	37
IPE 100	0	0	Neve	PolG	0	0	0	0	6	18	0	43
					18	0	0	0	43	107	0	43
IPE 100	0	0	Neve	PolG	0	0	0	0	22	60	0	37
					60	0	0	0	37	107	0	37
IPE 100	0	0	Neve	PolG	0	0	0	0	37	83	0	37
					83	0	0	0	37	108	0	9
IPE 100	0	170	Neve	PolG	0	0	0	0	43	101	0	43
					101	0	0	0	43	107	0	1
IPE 100	0	0	Neve	PolG	0	0	0	0	37	107	0	38
					0	0	0	0	32	86	0	50
IPE 100	0	0	Neve	PolG	86	0	0	0	50	108	0	43
					76	0	0	0	28	76	0	51
IPE 100	0	0	Neve	PolG	0	0	0	0	51	107	0	43
					30	0	0	0	43	108	0	43
IPE 100	0	170	Neve	PolG	0	0	0	0	38	107	0	37
					0	0	0	0	37	8	0	39
IPE 100	0	200	Neve	PolG	8	0	0	0	39	107	0	36
					60	0	0	0	22	60	0	53
IPE 100	0	0	Neve	PolG	60	0	0	0	53	107	0	43
					24	0	0	0	8	24	0	43
IPE 100	0	0	Neve	PolG	0	0	0	0	37	53	0	46
					53	0	0	0	46	107	0	20
IPE 100	0	0	Neve	PolG	0	0	0	0	37	46	0	46
					46	0	0	0	46	108	0	22
IPE 100	0	175	Neve	PolG	78	0	0	0	37	108	0	37
					0	0	0	0	25	68	0	52

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	Neve	PolG	68	0	0	52	108	0	0	43
IPE 100	0	0	Neve	PolG	0	0	0	37	90	0	0	37
IPE 100	0	175	Neve	PolG	90	0	0	37	108	0	0	7
IPE 100	0	0	Vento X	PolG	24	0	0	43	108	0	0	32
IPE 100	0	0	Vento X	PolG	0	0	0	57	53	0	0	72
IPE 100	0	0	Vento X	PolG	53	0	0	72	107	0	0	30
IPE 100	0	0	Vento X	PolG	18	0	0	67	107	0	0	67
IPE 100	0	175	Vento X	PolG	0	0	0	67	24	0	0	67
IPE 100	0	0	Vento X	PolG	24	0	0	67	108	0	0	49
IPE 100	0	0	Vento X	PolG	60	0	0	35	60	0	0	82
IPE 100	0	175	Vento X	PolG	0	0	0	82	107	0	0	67
IPE 100	0	0	Vento X	PolG	78	0	0	43	78	0	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	44	76	0	0	79
IPE 100	0	0	Vento X	PolG	76	0	0	79	107	0	0	67
IPE 100	0	0	Vento X	PolG	0	0	0	57	37	0	0	70
IPE 100	0	0	Vento X	PolG	37	0	0	70	107	0	0	39
IPE 100	0	0	Vento X	PolG	0	0	0	57	107	0	0	58
IPE 100	0	0	Vento X	PolG	0	0	0	2	6	0	0	67
IPE 100	0	0	Vento X	PolG	6	0	0	67	107	0	0	67
IPE 100	0	0	Vento X	PolG	0	0	0	57	101	0	0	57
IPE 100	0	200	Vento X	PolG	101	0	0	57	107	0	0	4
IPE 100	0	0	Vento X	PolG	0	0	0	57	8	0	0	61
IPE 100	0	200	Vento X	PolG	8	0	0	61	107	0	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	57	95	0	0	57
IPE 100	0	0	Vento X	PolG	95	0	0	34	60	0	0	8
IPE 100	0	0	Vento X	PolG	60	0	0	57	107	0	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	38	68	0	0	57
IPE 100	0	170	Vento X	PolG	68	0	0	57	107	0	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	67	107	0	0	67
IPE 100	0	0	Vento X	PolG	32	0	0	67	107	0	0	43
IPE 100	0	0	Vento X	PolG	0	0	0	57	28	0	0	68
IPE 100	0	170	Vento X	PolG	28	0	0	58	107	0	0	44
IPE 100	0	0	Vento X	PolG	0	0	0	13	24	0	0	67
IPE 100	0	0	Vento X	PolG	24	0	0	67	108	0	0	67
IPE 100	0	0	Vento X	PolG	0	0	0	50	86	0	0	77
IPE 100	0	0	Vento X	PolG	86	0	0	77	108	0	0	67
IPE 100	0	0	Vento X	PolG	0	0	0	57	90	0	0	57
IPE 100	0	0	Vento X	PolG	90	0	0	57	108	0	0	11
IPE 100	0	0	Vento X	PolG	0	0	0	57	46	0	0	71
IPE 100	0	0	Vento X	PolG	46	0	0	71	108	0	0	34
IPE 100	0	0	Vento X	PolG	0	0	0	67	4	0	0	67
IPE 100	0	0	Vento X	PolG	4	0	0	67	108	0	0	60
IPE 100	0	0	Vento X	PolG	30	0	0	67	108	0	0	67
IPE 100	0	0	Vento X	PolG	0	0	0	5	12	0	0	67
IPE 100	0	0	Vento X	PolG	12	0	0	67	107	0	0	67
IPE 100	0	0	Vento X	PolG	0	0	0	39	68	0	0	81
IPE 100	0	0	Vento X	PolG	68	0	0	81	108	0	0	67
IPE 100	0	0	Vento X	PolG	0	0	0	54	98	0	0	57
IPE 100	0	0	Vento X	PolG	98	0	0	57	108	0	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	57	83	0	0	57
IPE 100	0	0	Vento X	PolG	83	0	0	57	108	0	0	14
IPE 100	0	0	Vento X	PolG	0	0	0	67	41	0	0	67
IPE 100	0	0	Vento X	PolG	41	0	0	67	107	0	0	38
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	175	Carichi termici	Termico	AXY=15°C,AXZ=15°C							

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	200	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	170	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	155	190	Peso Proprio	UnifG	0	0	0	8	107	0	0	8
IPE 100	155	190	QP Solai	PolG	0	0	0	88	31	0	0	128
IPE 100	155	190	QV Solai	PolG	0	0	0	128	70	0	0	128
IPE 100	155	190	Neve	PolG	0	0	0	28	31	0	0	41
IPE 100	155	190	Neve	PolG	0	0	0	41	70	0	0	41
IPE 100	155	190	Vento X	PolG	0	0	0	18	31	0	0	37
IPE 100	155	190	Vento X	PolG	0	0	0	57	107	0	0	57
IPE 100	155	190	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	160	0	Peso Proprio	UnifG	0	0	0	8	108	0	0	8
IPE 100	160	0	QP Solai	PolG	0	0	0	100	49	0	0	127
IPE 100	160	0	QV Solai	PolG	0	0	0	127	52	0	0	127
IPE 100	160	0	Neve	PolG	0	0	0	32	49	0	0	41
IPE 100	160	0	Neve	PolG	0	0	0	41	52	0	0	41
IPE 100	160	0	Vento X	PolG	0	0	0	19	52	0	0	37
IPE 100	160	0	Vento X	PolG	0	0	0	37	108	0	0	37
IPE 100	160	0	Vento X	PolG	0	0	0	43	49	0	0	43
IPE 100	160	0	Vento X	PolG	0	0	0	29	52	0	0	57
IPE 100	160	0	Vento X	PolG	0	0	0	57	108	0	0	57
IPE 100	160	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	165	180	Peso Proprio	UnifG	0	0	0	8	108	0	0	8
IPE 100	165	180	QP Solai	PolG	0	0	0	81	18	0	0	128
IPE 100	165	180	QV Solai	PolG	0	0	0	128	83	0	0	128
IPE 100	165	180	Neve	PolG	0	0	0	26	18	0	0	73
IPE 100	165	180	Neve	PolG	0	0	0	41	83	0	0	41
IPE 100	165	180	Vento X	PolG	0	0	0	41	108	0	0	23
IPE 100	165	180	Vento X	PolG	0	0	0	43	83	0	0	43
IPE 100	165	180	Vento X	PolG	0	0	0	43	108	0	0	9
IPE 100	165	180	Vento X	PolG	0	0	0	7	18	0	0	37
IPE 100	165	180	Vento X	PolG	0	0	0	37	108	0	0	37
IPE 100	165	180	Vento X	PolG	0	0	0	67	83	0	0	67
IPE 100	165	180	Vento X	PolG	0	0	0	67	108	0	0	13
IPE 100	165	180	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	165	180	Peso Proprio	UnifG	0	0	0	8	109	0	0	8
IPE 100	170	185	QP Solai	PolG	0	0	0	74	6	0	0	128
IPE 100	170	185	QV Solai	PolG	0	0	0	128	109	0	0	65
IPE 100	170	185	Neve	PolG	0	0	0	24	6	0	0	41
IPE 100	170	185	Neve	PolG	0	0	0	41	97	0	0	41

Sezione	Ni	NF	Cond.	Tip. c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	170	185	Neve	PolG	97	0	0	0	41	109	0	21
	170	185										
IPE 100	170	185	Neve	PolG	97	0	0	0	43	97	0	43
	170	185										
IPE 100	170	185	Neve	PolG	97	0	0	0	43	109	0	4
	170	185										
IPE 100	170	185	Vento X	PolG	6	0	0	0	37	109	0	37
	170	185										
IPE 100	170	185	Vento X	PolG	97	0	0	0	67	97	0	67
	170	185										
IPE 100	170	185	Vento X	PolG	97	0	0	0	67	109	0	6
	170	185										
IPE 100	170	185	Vento X	PolG	6	0	0	0	5	6	0	57
	170	185										
IPE 100	170	185	Carichi termici	Termico	6	0	0	0	57	109	0	57
	170	185										
IPE 100	175	0	Peso Proprio	UnifG	0	0	0	0	8	107	0	8
	175	0	QV Solai	PolG	0	0	0	0	119	13	0	121
	175	0										
IPE 100	175	0	QV Solai	PolG	13	0	0	0	118	88	0	118
	175	0										
IPE 100	175	0	QV Solai	PolG	88	0	0	0	118	107	0	115
	175	0										
IPE 100	175	0	QV Solai	PolG	13	0	0	0	38	13	0	39
	175	0										
IPE 100	175	0	QV Solai	PolG	88	0	0	0	39	88	0	38
	175	0										
IPE 100	175	0	QV Solai	PolG	88	0	0	0	38	107	0	37
	175	0										
IPE 100	175	0	QV Solai	PolG	88	0	0	0	31	88	0	37
	175	0										
IPE 100	175	0	QV Solai	PolG	88	0	0	0	37	107	0	37
	175	0										
IPE 100	175	0	QV Solai	PolG	0	0	0	0	43	13	0	43
	175	0										
IPE 100	175	0	QV Solai	PolG	13	0	0	0	43	107	0	35
	175	0										
IPE 100	175	0	QV Solai	PolG	0	0	0	0	48	88	0	57
	175	0										
IPE 100	175	0	QV Solai	PolG	88	0	0	0	57	107	0	57
	175	0										
IPE 100	175	0	QV Solai	PolG	0	0	0	0	67	13	0	67
	175	0										
IPE 100	175	0	QV Solai	PolG	13	0	0	0	67	107	0	54
	175	0										
IPE 100	175	0	Carichi termici	Termico	0	0	0	0	8	108	0	8
	175	0										
IPE 100	180	155	Peso Proprio	UnifG	0	0	0	0	84	25	0	128
	180	155	QV Solai	PolG	0	0	0	0	128	77	0	128
	180	155										

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					24	0	0	0	124	95	0	123
IPE 100	0	0	QP Solai	PolG	95	0	0	0	123	113	0	112
IPE 100	0	0	QP Solai	PolG	60	0	0	0	90	60	0	149
IPE 100	0	0	QP Solai	PolG	0	0	0	0	149	113	0	92
					24	0	0	0	70	24	0	117
IPE 100	0	0	QP Solai	PolG	24	0	0	0	117	96	0	117
IPE 100	0	0	QP Solai	PolG	96	0	0	0	117	114	0	71
IPE 100	0	0	QP Solai	PolG	30	0	0	0	73	30	0	117
IPE 100	0	0	QP Solai	PolG	89	0	0	0	117	89	0	117
IPE 100	0	0	QP Solai	PolG	0	0	0	0	117	114	0	75
					14	0	0	0	115	14	0	123
IPE 100	0	0	QP Solai	PolG	106	0	0	0	123	106	0	121
					110	0	0	0	121	110	0	118
IPE 100	0	0	QP Solai	PolG	6	0	0	0	118	113	0	117
IPE 100	0	0	QP Solai	PolG	6	0	0	0	59	6	0	117
IPE 100	0	0	QP Solai	PolG	39	0	0	0	117	113	0	118
IPE 100	0	0	QP Solai	PolG	39	0	0	0	100	39	0	109
IPE 100	0	0	QP Solai	PolG	68	0	0	0	109	68	0	109
IPE 100	0	0	QP Solai	PolG	0	0	0	0	109	113	0	98
					34	0	0	0	104	34	0	128
IPE 100	0	0	QP Solai	PolG	34	0	0	0	128	85	0	126
					85	0	0	0	126	114	0	106
IPE 100	0	0	QP Solai	PolG	0	0	0	0	126	114	0	106
IPE 100	0	0	QP Solai	PolG	10	0	0	0	117	10	0	117
IPE 100	0	0	QP Solai	PolG	0	0	0	0	117	114	0	114
					43	0	0	0	99	43	0	133
IPE 100	0	0	QP Solai	PolG	76	0	0	0	133	76	0	131
IPE 100	0	176	QP Solai	PolG	0	0	0	0	131	113	0	101
					30	0	0	0	106	30	0	110
IPE 100	0	0	QP Solai	PolG	30	0	0	0	110	78	0	109
IPE 100	0	0	QP Solai	PolG	78	0	0	0	109	114	0	103
					12	0	0	0	63	12	0	117
IPE 100	0	0	QP Solai	PolG	12	0	0	0	117	107	0	117
					107	0	0	0	117	113	0	64
IPE 100	0	0	QP Solai	PolG	47	0	0	0	95	47	0	112
					60	0	0	0	112	60	0	93
IPE 100	0	0	QP Solai	PolG	14	0	0	0	37	14	0	39
					106	0	0	0	39	106	0	39
					110	0	0	0	39	110	0	38
IPE 100	0	0	QP Solai	PolG	18	0	0	0	38	113	0	37
					101	0	0	0	21	18	0	37
IPE 100	0	0	QP Solai	PolG	18	0	0	0	37	101	0	37
					101	0	0	0	37	113	0	22
IPE 100	0	0	QP Solai	PolG	0	0	0	0	24	30	0	37
					30	0	0	0	37	89	0	37
IPE 100	0	0	QP Solai	PolG	89	0	0	0	37	114	0	24
					24	0	0	0	35	24	0	40
IPE 100	0	0	QP Solai	PolG	24	0	0	0	40	95	0	40
					95	0	0	0	40	113	0	36
IPE 100	0	0	QP Solai	PolG	0	0	0	0	32	39	0	35
					39	0	0	0	35	68	0	35
IPE 100	0	0	QP Solai	PolG	68	0	0	0	35	113	0	31
					6	0	0	0	19	6	0	37
IPE 100	0	0	QP Solai	PolG	6	0	0	0	37	113	0	38
					60	0	0	0	29	60	0	48
IPE 100	0	0	QP Solai	PolG	60	0	0	0	48	113	0	29
					52	0	0	0	30	52	0	45
IPE 100	0	0	QP Solai	PolG	52	0	0	0	45	68	0	44
					68	0	0	0	44	114	0	31
IPE 100	0	0	QP Solai	PolG	0	0	0	0	22	24	0	37
					24	0	0	0	37	96	0	37
IPE 100	0	0	QP Solai	PolG	96	0	0	0	37	114	0	23
					47	0	0	0	30	47	0	36
IPE 100	0	0	QP Solai	PolG	47	0	0	0	36	60	0	36
					60	0	0	0	36	113	0	30
IPE 100	0	0	QP Solai	PolG	60	0	0	0	36	113	0	43

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					43	0	0	0	43	76	0	42
IPE 100	0	0	QP Solai	PolG	76	0	0	0	42	113	0	32
IPE 100	0	171	QP Solai	PolG	0	0	0	0	37	114	0	37
IPE 100	0	0	QP Solai	PolG	107	0	0	0	38	107	0	37
IPE 100	0	0	QP Solai	PolG	0	0	0	0	37	113	0	19
					12	0	0	0	20	12	0	37
IPE 100	0	0	QP Solai	PolG	107	0	0	0	37	107	0	37
IPE 100	0	0	QP Solai	PolG	0	0	0	0	33	34	0	41
IPE 100	0	0	QP Solai	PolG	34	0	0	0	41	85	0	41
					85	0	0	0	41	114	0	34
IPE 100	0	176	QP Solai	PolG	0	0	0	0	34	30	0	35
					30	0	0	0	35	78	0	35
IPE 100	0	0	Neve	PolG	78	0	0	0	35	114	0	33
IPE 100	0	0	Neve	PolG	0	0	0	0	7	24	0	37
IPE 100	0	0	Neve	PolG	24	0	0	0	37	114	0	37
IPE 100	0	0	Neve	PolG	47	0	0	0	37	47	0	37
IPE 100	0	0	Neve	PolG	0	0	0	0	23	68	0	46
IPE 100	0	128	Neve	PolG	68	0	0	0	46	114	0	37
IPE 100	0	171	Neve	PolG	0	0	0	0	37	107	0	37
IPE 100	0	0	Neve	PolG	107	0	0	0	37	113	0	1
IPE 100	0	0	Neve	PolG	0	0	0	0	3	12	0	37
IPE 100	0	0	Neve	PolG	12	0	0	0	37	113	0	37
IPE 100	0	0	Neve	PolG	0	0	0	0	36	89	0	36
IPE 100	0	0	Neve	PolG	89	0	0	0	36	114	0	10
IPE 100	0	0	Neve	PolG	0	0	0	0	36	107	0	36
IPE 100	0	0	Neve	PolG	107	0	0	0	36	113	0	3
IPE 100	0	0	Neve	PolG	0	0	0	0	37	10	0	37
IPE 100	0	0	Neve	PolG	10	0	0	0	37	114	0	35
IPE 100	0	0	Neve	PolG	43	0	0	0	36	43	0	46
IPE 100	0	0	Neve	PolG	0	0	0	0	46	113	0	26
IPE 100	0	0	Neve	PolG	68	0	0	0	25	68	0	36
IPE 100	0	0	Neve	PolG	59	0	0	0	36	59	0	46
IPE 100	0	0	Neve	PolG	0	0	0	0	46	113	0	20
IPE 100	0	0	Neve	PolG	76	0	0	0	26	76	0	45
IPE 100	0	0	Neve	PolG	0	0	0	0	45	113	0	37
IPE 100	0	0	Neve	PolG	6	0	0	0	1	6	0	37
IPE 100	0	0	Neve	PolG	6	0	0	0	37	113	0	37
IPE 100	0	0	Neve	PolG	60	0	0	0	20	60	0	46
IPE 100	0	0	Neve	PolG	60	0	0	0	46	113	0	37
IPE 100	0	0	Neve	PolG	60	0	0	0	22	60	0	36
IPE 100	0	0	Neve	PolG	0	0	0	0	36	113	0	36
IPE 100	0	0	Neve	PolG	0	0	0	0	36	24	0	43
IPE 100	0	0	Neve	PolG	24	0	0	0	43	113	0	33
IPE 100	0	0	Neve	PolG	0	0	0	0	10	30	0	37
IPE 100	0	0	Neve	PolG	30	0	0	0	37	114	0	37
IPE 100	0	0	Neve	PolG	0	0	0	0	36	34	0	45
IPE 100	0	0	Neve	PolG	34	0	0	0	45	114	0	29
IPE 100	0	0	Neve	PolG	0	0	0	0	36	114	0	36
IPE 100	0	0	Neve	PolG	0	0	0	0	37	39	0	37
IPE 100	0	0	Neve	PolG	39	0	0	0	37	113	0	25
IPE 100	0	0	Neve	PolG	0	0	0	0	32	95	0	42
IPE 100	0	0	Neve	PolG	95	0	0	0	42	113	0	37
IPE 100	0	0	Neve	PolG	0	0	0	0	29	85	0	44
IPE 100	0	0	Neve	PolG	85	0	0	0	44	114	0	37
IPE 100	0	0	Neve	PolG	0	0	0	0	36	113	0	37
IPE 100	0	0	Neve	PolG	106	0	0	0	36	106	0	39
IPE 100	0	176	Neve	PolG	0	0	0	0	39	113	0	37
IPE 100	0	0	Neve	PolG	78	0	0	0	29	78	0	36
IPE 100	0	0	Neve	PolG	0	0	0	0	36	114	0	36
IPE 100	0	0	Neve	PolG	18	0	0	0	5	18	0	37
IPE 100	0	0	Neve	PolG	0	0	0	0	37	113	0	37
IPE 100	0	0	Neve	PolG	101	0	0	0	36	101	0	36
IPE 100	0	0	Neve	PolG	101	0	0	0	36	113	0	5

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	Neve	PolG	0	0	0	0	36	14	0	40
					14	0	0	0	40	110	0	36
IPE 100	0	176	Neve	PolG	0	0	0	0	36	113	0	36
					110	0	0	0	37	30	0	37
IPE 100	0	0	Neve	PolG	0	0	0	0	37	114	0	28
					30	0	0	0	36	52	0	46
IPE 100	0	0	Neve	PolG	0	0	0	0	46	114	0	23
					52	0	0	0	37	113	0	36
IPE 100	0	171	Neve	PolG	0	0	0	0	36	96	0	36
					0	0	0	0	36	114	0	7
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	101	0	55
					101	0	0	0	55	113	0	8
IPE 100	0	0	Vento X	PolG	0	0	0	0	57	47	0	57
					47	0	0	0	57	113	0	34
IPE 100	0	0	Vento X	PolG	0	0	0	0	35	68	0	71
					68	0	0	0	71	114	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	106	0	60
					106	0	0	0	60	113	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	8	18	0	57
					18	0	0	0	57	113	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	52	0	72
					52	0	0	0	72	114	0	36
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	24	0	66
					24	0	0	0	66	113	0	51
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	107	0	55
					107	0	0	0	55	113	0	5
IPE 100	0	0	Vento X	PolG	0	0	0	0	5	12	0	57
					12	0	0	0	57	113	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	35	60	0	55
					60	0	0	0	55	113	0	55
IPE 100	0	171	Vento X	PolG	0	0	0	0	57	113	0	55
					0	0	0	0	55	34	0	69
IPE 100	0	0	Vento X	PolG	0	0	0	0	69	114	0	45
					34	0	0	0	55	114	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	0	57	10	0	54
					10	0	0	0	57	114	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	12	24	0	57
					24	0	0	0	57	114	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	1	6	0	57
					6	0	0	0	57	113	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	45	85	0	68
					85	0	0	0	68	114	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	14	0	62
					14	0	0	0	62	110	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	113	0	55
					110	0	0	0	15	30	0	57
IPE 100	0	176	Vento X	PolG	0	0	0	0	57	114	0	57
					30	0	0	0	57	30	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	57	30	0	57
					30	0	0	0	55	89	0	15
IPE 100	0	0	Vento X	PolG	0	0	0	0	45	78	0	55
					78	0	0	0	55	114	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	113	0	57
					0	0	0	0	31	60	0	71
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	96	0	55
					96	0	0	0	55	114	0	11
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	59	0	72
					59	0	0	0	72	113	0	31
IPE 100	0	0	Vento X	PolG	0	0	0	0	40	76	0	70
					76	0	0	0	70	113	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	57	39	0	57
					39	0	0	0	57	113	0	39
IPE 100	0	0	Vento X	PolG	0	0	0	0	55	43	0	71
					43	0	0	0	71	113	0	40

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	Vento X	PolG	0	0	0	0	50	95	0	65
					95	0	0	0	65	113	0	57
IPE 100	0	0	Vento X	PolG	0	0	0	0	39	68	0	55
					68	0	0	0	55	113	0	55
IPE 100	0	171	Vento X	PolG	0	0	0	0	57	107	0	57
					107	0	0	0	57	113	0	1
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
					Termico	AXY=15°C,ΔXZ=15°C						
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
					Termico	AXY=15°C,ΔXZ=15°C						
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
					Termico	AXY=15°C,ΔXZ=15°C						
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
					Termico	AXY=15°C,ΔXZ=15°C						
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
					Termico	AXY=15°C,ΔXZ=15°C						
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
					Termico	AXY=15°C,ΔXZ=15°C						
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
					Termico	AXY=15°C,ΔXZ=15°C						
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
					Termico	AXY=15°C,ΔXZ=15°C						
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
					Termico	AXY=15°C,ΔXZ=15°C						
IPE 100	156	191	Peso Proprio	UnifG	0	0	0	0	8	113	0	0
	156	191	QP Solai	PolG	31	0	0	0	78	31	0	0
					76	0	0	0	117	76	0	117
IPE 100	156	191	QV Solai	PolG	31	0	0	0	25	31	0	0
					31	0	0	0	37	76	0	37
IPE 100	156	191	Neve	PolG	76	0	0	0	37	113	0	0
					0	0	0	0	12	31	0	0
IPE 100	156	191	Neve	PolG	31	0	0	0	36	113	0	0
					0	0	0	0	37	76	0	37
IPE 100	156	191	Vento X	PolG	76	0	0	0	37	113	0	0
					0	0	0	0	19	31	0	0
IPE 100	156	191	Vento X	PolG	31	0	0	0	55	113	0	0
					0	0	0	0	57	76	0	57
IPE 100	156	191	Vento X	PolG	76	0	0	0	57	113	0	0
					0	0	0	0	57	113	0	19
IPE 100	156	191	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
	161	0	Peso Proprio	UnifG	0	0	0	0	8	114	0	0
IPE 100	161	0	QP Solai	PolG	0	0	0	0	91	52	0	0
					52	0	0	0	117	55	0	0
					55	0	0	0	117	114	0	0
IPE 100	161	0	QV Solai	PolG	0	0	0	0	29	52	0	0
					52	0	0	0	37	55	0	0
					55	0	0	0	37	114	0	0
IPE 100	161	0	Neve	PolG	0	0	0	0	20	52	0	0
					52	0	0	0	36	114	0	0
IPE 100	161	0	Neve	PolG	0	0	0	0	37	55	0	0
					55	0	0	0	37	114	0	0
IPE 100	161	0	Vento X	PolG	0	0	0	0	57	55	0	0
					55	0	0	0	57	114	0	0
IPE 100	161	0	Vento X	PolG	0	0	0	0	30	52	0	0
					52	0	0	0	30	52	0	0
IPE 100	161	0	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C							
	166	181	Peso Proprio	UnifG	0	0	0	0	8	114	0	0
IPE 100	166	181	QP Solai	PolG	0	0	0	0	71	18	0	0
					18	0	0	0	117	89	0	0
					89	0	0	0	117	114	0	0
IPE 100	166	181	QV Solai	PolG	0	0	0	0	23	18	0	0
					18	0	0	0	37	89	0	0
					89	0	0	0	37	114	0	0
IPE 100	166	181	Neve	PolG	0	0	0	0	37	89	0	0
					89	0	0	0	37	114	0	0
IPE 100	166	181	Neve	PolG	0	0	0	0	37	114	0	0
					89	0	0	0	37	114	0	0
IPE 100	166	181	Neve	PolG	0	0	0	0	36	114	0	0
					18	0	0	0	36	114	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	QP Solai	PolG	68	0	0	138	120	0	0	93
					0	0	0	61	18	0	0	110
					18	0	0	110	107	0	0	110
IPE 100	0	0	QP Solai	PolG	107	0	0	110	119	0	0	66
					0	0	0	97	45	0	0	105
					45	0	0	105	68	0	0	105
					68	0	0	105	119	0	0	94
IPE 100	0	0	QP Solai	PolG	0	0	0	86	60	0	0	142
					60	0	0	142	65	0	0	142
					65	0	0	142	119	0	0	89
IPE 100	0	177	QP Solai	PolG	0	0	0	102	36	0	0	106
					36	0	0	106	78	0	0	105
					78	0	0	105	120	0	0	99
IPE 100	0	0	QP Solai	PolG	0	0	0	100	40	0	0	126
					40	0	0	126	85	0	0	126
					85	0	0	126	120	0	0	103
IPE 100	0	0	QP Solai	PolG	0	0	0	54	6	0	0	110
					6	0	0	110	120	0	0	112
IPE 100	0	0	QP Solai	PolG	0	0	0	65	24	0	0	110
					24	0	0	110	102	0	0	110
					102	0	0	110	120	0	0	69
IPE 100	0	172	QP Solai	PolG	0	0	0	112	112	0	0	110
					112	0	0	110	119	0	0	54
IPE 100	0	0	QP Solai	PolG	0	0	0	92	53	0	0	108
					53	0	0	108	60	0	0	108
					60	0	0	108	119	0	0	89
IPE 100	0	0	QP Solai	PolG	0	0	0	110	3	0	0	112
					3	0	0	112	19	0	0	120
					19	0	0	120	106	0	0	117
					106	0	0	117	110	0	0	115
					110	0	0	115	120	0	0	110
IPE 100	0	0	QP Solai	PolG	0	0	0	106	30	0	0	123
					30	0	0	123	95	0	0	123
					95	0	0	123	119	0	0	108
IPE 100	0	0	QV Solai	PolG	0	0	0	29	58	0	0	44
					58	0	0	44	68	0	0	44
					68	0	0	44	120	0	0	30
IPE 100	0	172	QV Solai	PolG	0	0	0	36	112	0	0	35
					112	0	0	35	119	0	0	17
IPE 100	0	0	QV Solai	PolG	0	0	0	20	18	0	0	35
					18	0	0	35	107	0	0	35
					107	0	0	35	119	0	0	21
IPE 100	0	0	QV Solai	PolG	0	0	0	30	49	0	0	42
					49	0	0	42	76	0	0	42
					76	0	0	42	120	0	0	31
IPE 100	0	0	QV Solai	PolG	0	0	0	34	30	0	0	39
					30	0	0	39	95	0	0	39
					95	0	0	39	119	0	0	35
IPE 100	0	0	QV Solai	PolG	0	0	0	17	6	0	0	35
					6	0	0	35	120	0	0	36
IPE 100	0	0	QV Solai	PolG	0	0	0	27	60	0	0	46
					60	0	0	46	65	0	0	46
					65	0	0	46	119	0	0	28
IPE 100	0	0	QV Solai	PolG	0	0	0	30	53	0	0	35
					53	0	0	35	60	0	0	35
					60	0	0	35	119	0	0	29
IPE 100	0	177	QV Solai	PolG	0	0	0	33	36	0	0	34
					36	0	0	34	78	0	0	34
					78	0	0	34	120	0	0	32
IPE 100	0	0	QV Solai	PolG	0	0	0	32	40	0	0	40
					40	0	0	40	85	0	0	40
					85	0	0	40	120	0	0	33
IPE 100	0	0	QV Solai	PolG	0	0	0	35	3	0	0	36
					3	0	0	36	19	0	0	39
					19	0	0	39	106	0	0	38
					106	0	0	38	110	0	0	37

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	QV Solai	PolG	110	0	0	37	120	0	0	35
					0	0	0	18	12	0	0	35
					12	0	0	35	113	0	0	35
IPE 100	0	0	QV Solai	PolG	113	0	0	35	119	0	0	20
					0	0	0	31	45	0	0	34
					45	0	0	34	68	0	0	34
					68	0	0	34	119	0	0	30
IPE 100	0	0	QV Solai	PolG	0	0	0	21	24	0	0	35
					24	0	0	35	102	0	0	35
					102	0	0	35	120	0	0	22
IPE 100	0	0	QV Solai	PolG	0	0	0	22	30	0	0	35
					30	0	0	35	95	0	0	35
					95	0	0	35	120	0	0	23
IPE 100	0	0	QV Solai	PolG	0	0	0	35	7	0	0	36
					7	0	0	36	98	0	0	35
					98	0	0	35	120	0	0	35
IPE 100	0	0	Neve	PolG	0	0	0	36	3	0	0	36
					3	0	0	36	106	0	0	40
					106	0	0	40	120	0	0	36
IPE 100	0	0	Neve	PolG	0	0	0	33	49	0	0	43
					49	0	0	43	120	0	0	25
IPE 100	0	0	Neve	PolG	0	0	0	33	113	0	0	33
					113	0	0	33	119	0	0	3
IPE 100	0	0	Neve	PolG	0	0	0	23	68	0	0	46
					68	0	0	46	120	0	0	36
IPE 100	0	0	Neve	PolG	0	0	0	33	7	0	0	35
					7	0	0	35	98	0	0	33
					98	0	0	33	120	0	0	33
IPE 100	0	0	Neve	PolG	0	0	0	26	76	0	0	45
					76	0	0	45	120	0	0	36
IPE 100	0	0	Neve	PolG	0	0	0	36	45	0	0	36
					45	0	0	36	119	0	0	26
IPE 100	0	0	Neve	PolG	0	0	0	22	60	0	0	33
					60	0	0	33	119	0	0	33
IPE 100	0	0	Neve	PolG	0	0	0	3	12	0	0	36
					12	0	0	36	119	0	0	36
IPE 100	0	172	Neve	PolG	0	0	0	33	119	0	0	33
					0	0	0	24	68	0	0	33
IPE 100	0	0	Neve	PolG	68	0	0	33	119	0	0	33
					40	0	0	42	120	0	0	42
IPE 100	0	0	Neve	PolG	0	0	0	33	107	0	0	33
					107	0	0	33	119	0	0	5
IPE 100	0	0	Neve	PolG	0	0	0	33	95	0	0	33
					95	0	0	33	120	0	0	9
IPE 100	0	0	Neve	PolG	0	0	0	10	30	0	0	36
					30	0	0	36	120	0	0	36
IPE 100	0	172	Neve	PolG	0	0	0	36	112	0	0	36
					112	0	0	36	119	0	0	1
IPE 100	0	0	Neve	PolG	0	0	0	33	30	0	0	40
					30	0	0	40	119	0	0	32
IPE 100	0	0	Neve	PolG	0	0	0	33	65	0	0	43
					65	0	0	43	119	0	0	19
IPE 100	0	0	Neve	PolG	0	0	0	33	120	0	0	33
					0	0	0	30	85	0	0	44
IPE 100	0	0	Neve	PolG	85	0	0	44	120	0	0	36
					0	0	0	28	78	0	0	33
IPE 100	0	177	Neve	PolG	0	0	0	33	120	0	0	33
					78	0	0	33	95	0	0	42
IPE 100	0	0	Neve	PolG	0	0	0	42	119	0	0	36
					95	0	0	21	60	0	0	46
IPE 100	0	0	Neve	PolG	60	0	0	46	119	0	0	36
					0	0	0	8	24	0	0	36
IPE 100	0	0	Neve	PolG	24	0	0	36	120	0	0	36
					0	0	0	36	53	0	0	36
IPE 100	0	0	Neve	PolG	0	0	0	36	119	0	0	23

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	Neve	PolG	0	0	0	33	102	0	0	33
IPE 100	0	0	Neve	PolG	102	0	0	33	120	0	0	7
IPE 100	0	0	Neve	PolG	0	0	0	36	120	0	0	36
IPE 100	0	0	Neve	PolG	0	0	0	33	19	0	0	38
					19	0	0	38	110	0	0	33
IPE 100	0	0	Neve	PolG	110	0	0	33	120	0	0	33
IPE 100	0	0	Neve	PolG	0	0	0	6	18	0	0	36
IPE 100	0	177	Neve	PolG	18	0	0	36	119	0	0	36
IPE 100	0	0	Neve	PolG	36	0	0	36	36	0	0	36
IPE 100	0	0	Neve	PolG	0	0	0	1	6	0	0	36
IPE 100	0	0	Neve	PolG	6	0	0	36	120	0	0	36
IPE 100	0	0	Neve	PolG	0	0	0	33	58	0	0	43
IPE 100	0	0	Vento X	PolG	58	0	0	43	120	0	0	22
IPE 100	0	0	Vento X	PolG	0	0	0	36	68	0	0	71
IPE 100	0	177	Vento X	PolG	68	0	0	71	120	0	0	55
IPE 100	0	172	Vento X	PolG	36	0	0	55	36	0	0	55
IPE 100	0	0	Vento X	PolG	112	0	0	55	112	0	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	55	119	0	0	2
					3	0	0	55	3	0	0	55
					106	0	0	55	106	0	0	62
IPE 100	0	0	Vento X	PolG	0	0	0	62	120	0	0	55
					19	0	0	50	19	0	0	59
					110	0	0	59	110	0	0	50
IPE 100	0	177	Vento X	PolG	0	0	0	43	78	0	0	50
IPE 100	0	0	Vento X	PolG	78	0	0	50	120	0	0	50
IPE 100	0	0	Vento X	PolG	95	0	0	66	119	0	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	50	107	0	0	50
IPE 100	0	0	Vento X	PolG	107	0	0	50	119	0	0	8
IPE 100	0	0	Vento X	PolG	0	0	0	50	30	0	0	63
IPE 100	0	0	Vento X	PolG	30	0	0	63	119	0	0	49
IPE 100	0	0	Vento X	PolG	0	0	0	55	53	0	0	55
IPE 100	0	0	Vento X	PolG	53	0	0	55	119	0	0	35
IPE 100	0	0	Vento X	PolG	0	0	0	50	65	0	0	67
IPE 100	0	0	Vento X	PolG	65	0	0	67	119	0	0	30
IPE 100	0	0	Vento X	PolG	40	0	0	50	40	0	0	65
IPE 100	0	0	Vento X	PolG	0	0	0	65	120	0	0	43
IPE 100	0	0	Vento X	PolG	0	0	0	33	60	0	0	50
IPE 100	0	0	Vento X	PolG	60	0	0	50	119	0	0	50
IPE 100	0	0	Vento X	PolG	0	0	0	16	30	0	0	55
IPE 100	0	0	Vento X	PolG	30	0	0	55	120	0	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	50	58	0	0	67
IPE 100	0	0	Vento X	PolG	58	0	0	67	120	0	0	34
					7	0	0	54	98	0	0	54
IPE 100	0	0	Vento X	PolG	98	0	0	50	120	0	0	50
IPE 100	0	0	Vento X	PolG	0	0	0	50	95	0	0	50
IPE 100	0	172	Vento X	PolG	95	0	0	50	120	0	0	14
IPE 100	0	0	Vento X	PolG	0	0	0	52	119	0	0	50
IPE 100	0	0	Vento X	PolG	60	0	0	32	60	0	0	71
IPE 100	0	0	Vento X	PolG	0	0	0	71	119	0	0	55
IPE 100	0	0	Vento X	PolG	12	0	0	55	119	0	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	37	68	0	0	50
IPE 100	0	0	Vento X	PolG	68	0	0	50	119	0	0	50
IPE 100	0	0	Vento X	PolG	0	0	0	41	76	0	0	70
IPE 100	0	0	Vento X	PolG	76	0	0	70	120	0	0	55
IPE 100	0	0	Vento X	PolG	113	0	0	50	119	0	0	50
IPE 100	0	0	Vento X	PolG	0	0	0	50	120	0	0	4
IPE 100	0	0	Vento X	PolG	0	0	0	12	24	0	0	52
IPE 100	0	0	Vento X	PolG	24	0	0	55	120	0	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	46	85	0	0	69

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	0	0	Vento X	PolG	85	0	0	69	120	0	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	55	45	0	0	55
IPE 100	0	0	Vento X	PolG	45	0	0	55	119	0	0	40
IPE 100	0	0	Vento X	PolG	0	0	0	55	120	0	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	50	49	0	0	66
IPE 100	0	0	Vento X	PolG	49	0	0	66	120	0	0	39
IPE 100	0	0	Vento X	PolG	0	0	0	2	6	0	0	55
IPE 100	0	0	Vento X	PolG	6	0	0	55	120	0	0	55
IPE 100	0	0	Vento X	PolG	18	0	0	55	119	0	0	55
IPE 100	0	0	Vento X	PolG	0	0	0	50	102	0	0	50
IPE 100	0	0	Vento X	PolG	102	0	0	50	120	0	0	11
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	177	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	172	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	157	192	Peso Proprio	UnitG	0	0	0	8	119	0	0	8
IPE 100	157	192	QP Solai	PolG	0	0	0	76	31	0	0	110
IPE 100	157	192	QP Solai	PolG	31	0	0	110	82	0	0	110
IPE 100	157	192	QV Solai	PolG	82	0	0	110	119	0	0	72
IPE 100	157	192	Neve	PolG	31	0	0	24	31	0	0	35
IPE 100	157	192	Neve	PolG	82	0	0	35	82	0	0	23
IPE 100	157	192	Neve	PolG	0	0	0	11	31	0	0	33
IPE 100	157	192	Neve	PolG	31	0	0	33	119	0	0	33
IPE 100	157	192	Neve	PolG	0	0	0	36	82	0	0	36
IPE 100	157	192	Vento X	PolG	82	0	0	36	119	0	0	12
IPE 100	157	192	Vento X	PolG	0	0	0	55	82	0	0	55
IPE 100	157	192	Vento X	PolG	82	0	0	55	119	0	0	19
IPE 100	157	192	Vento X	PolG	0	0	0	18	31	0	0	50
IPE 100	157	192	Vento X	PolG	31	0	0	50	119	0	0	50
IPE 100	157	192	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	162	0	Peso Proprio	UnitG	0	0	0	8	120	0	0	8
IPE 100	162	0	QP Solai	PolG	0	0	0	88	52	0	0	110
IPE 100	162	0	QP Solai	PolG	52	0	0	110	61	0	0	110
IPE 100	162	0	QV Solai	PolG	61	0	0	110	120	0	0	85
IPE 100	162	0	QV Solai	PolG	0	0	0	28	52	0	0	35
IPE 100	162	0	Neve	PolG	52	0	0	35	61	0	0	35
IPE 100	162	0	Neve	PolG	61	0	0	35	120	0	0	27
IPE 100	162	0	Neve	PolG	0	0	0	36	61	0	0	36
IPE 100	162	0	Neve	PolG	61	0	0	36	120	0	0	20
IPE 100	162	0	Neve	PolG	0	0	0	19	52	0	0	33
IPE 100	162	0	Vento X	PolG	52	0	0	33	120	0	0	33
IPE 100	162	0	Vento X	PolG	0	0	0	55	61	0	0	55
IPE 100	162	0	Vento X	PolG	61	0	0	55	120	0	0	31
IPE 100	162	0	Vento X	PolG	0	0	0	29	52	0	0	50
IPE 100	162	0	Vento X	PolG	52	0	0	50	120	0	0	50
IPE 100	162	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	167	182	Peso Proprio	UnitG	0	0	0	8	120	0	0	8
IPE 100	167	182	QP Solai	PolG	0	0	0	69	18	0	0	110
IPE 100	167	182	QP Solai	PolG	18	0	0	110	95	0	0	110
IPE 100	167	182	QP Solai	PolG	95	0	0	110	120	0	0	65
IPE 100	167	182	QP Solai	PolG	0	0	0	22	18	0	0	35

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					18	0	0	35	95	0	0	35
IPE 100	167	182	Neve	PolG	0	0	0	35	120	0	0	21
IPE 100	167	182	Neve	PolG	95	0	0	36	95	0	0	36
IPE 100	167	182	Neve	PolG	0	0	0	36	120	0	0	8
IPE 100	167	182	Vento X	PolG	18	0	0	33	120	0	0	33
IPE 100	167	182	Vento X	PolG	0	0	0	11	18	0	0	50
IPE 100	167	182	Vento X	PolG	18	0	0	50	120	0	0	50
IPE 100	167	182	Vento X	PolG	0	0	0	55	95	0	0	55
IPE 100	167	182	Carichi termici Peso Proprio QP Solai	Termico UnifG PolG	95	0	0	55	120	0	0	12
IPE 100	172	187	QV Solai	PolG	0	0	0	8	121	0	0	8
IPE 100	172	187	QV Solai	PolG	6	0	0	20	6	0	0	35
IPE 100	172	187	QV Solai	PolG	0	0	0	35	109	0	0	35
IPE 100	172	187	QV Solai	PolG	109	0	0	35	121	0	0	19
IPE 100	172	187	QV Solai	PolG	0	0	0	3	6	0	0	33
IPE 100	172	187	QV Solai	PolG	6	0	0	33	121	0	0	33
IPE 100	172	187	QV Solai	PolG	0	0	0	36	109	0	0	36
IPE 100	172	187	QV Solai	PolG	109	0	0	36	121	0	0	3
IPE 100	172	187	QV Solai	PolG	0	0	0	55	109	0	0	55
IPE 100	172	187	QV Solai	PolG	109	0	0	55	121	0	0	5
IPE 100	172	187	QV Solai	PolG	0	0	0	5	6	0	0	50
IPE 100	172	187	QV Solai	PolG	6	0	0	50	121	0	0	50
IPE 100	177	0	QV Solai	PolG	0	0	0	8	119	0	0	8
IPE 100	177	0	QV Solai	PolG	0	0	0	107	25	0	0	108
IPE 100	177	0	QV Solai	PolG	25	0	0	108	88	0	0	106
IPE 100	177	0	QV Solai	PolG	88	0	0	106	119	0	0	104
IPE 100	177	0	QV Solai	PolG	0	0	0	34	25	0	0	35
IPE 100	177	0	QV Solai	PolG	25	0	0	35	119	0	0	33
IPE 100	177	0	QV Solai	PolG	0	0	0	36	25	0	0	36
IPE 100	177	0	QV Solai	PolG	25	0	0	36	119	0	0	32
IPE 100	177	0	QV Solai	PolG	0	0	0	31	88	0	0	33
IPE 100	177	0	QV Solai	PolG	88	0	0	33	119	0	0	33
IPE 100	177	0	QV Solai	PolG	0	0	0	48	88	0	0	50
IPE 100	177	0	QV Solai	PolG	88	0	0	50	119	0	0	50
IPE 100	177	0	QV Solai	PolG	0	0	0	55	25	0	0	55
IPE 100	177	0	QV Solai	PolG	25	0	0	55	119	0	0	50
IPE 100	182	157	QV Solai	PolG	0	0	0	8	120	0	0	8
IPE 100	182	157	QV Solai	PolG	0	0	0	73	25	0	0	110
IPE 100	182	157	QV Solai	PolG	25	0	0	110	89	0	0	110
IPE 100	182	157	QV Solai	PolG	89	0	0	110	120	0	0	69
IPE 100	182	157	QV Solai	PolG	0	0	0	23	25	0	0	35
IPE 100	182	157	QV Solai	PolG	25	0	0	35	89	0	0	35
IPE 100	182	157	QV Solai	PolG	89	0	0	35	120	0	0	22
IPE 100	182	157	QV Solai	PolG	0	0	0	9	25	0	0	33
IPE 100	182	157	QV Solai	PolG	25	0	0	33	120	0	0	33
IPE 100	182	157	QV Solai	PolG	0	0	0	36	89	0	0	36
IPE 100	182	157	QV Solai	PolG	89	0	0	36	120	0	0	10
IPE 100	182	157	QV Solai	PolG	0	0	0	55	89	0	0	55
IPE 100	182	157	QV Solai	PolG	89	0	0	55	120	0	0	16
IPE 100	182	157	QV Solai	PolG	0	0	0	14	25	0	0	50
IPE 100	182	157	QV Solai	PolG	25	0	0	50	120	0	0	50
IPE 100	182	157	QV Solai	PolG	0	0	0	8	118	0	0	8
IPE 100	182	157	QV Solai	PolG	0	0	0	66	12	0	0	110
IPE 100	182	157	QV Solai	PolG	12	0	0	110	100	0	0	110
IPE 100	182	157	QV Solai	PolG	100	0	0	110	118	0	0	61
IPE 100	182	157	QV Solai	PolG	0	0	0	21	12	0	0	35
IPE 100	182	157	QV Solai	PolG	12	0	0	35	100	0	0	35
IPE 100	182	157	QV Solai	PolG	100	0	0	35	118	0	0	20
IPE 100	182	157	QV Solai	PolG	0	0	0	36	100	0	0	36

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	187	167	Neve	PolG	100	0	0	36	118	0	0	6
IPE 100	187	167	Neve	PolG	0	0	0	33	118	0	0	33
IPE 100	187	167	Neve	PolG	12	0	0	35	100	0	0	55
IPE 100	187	167	Neve	PolG	100	0	0	55	118	0	0	9
IPE 100	187	167	Neve	PolG	0	0	0	8	12	0	0	50
IPE 100	187	167	Neve	PolG	12	0	0	50	118	0	0	50
IPE 100	187	167	Neve	PolG	0	0	0	8	139	0	0	8
IPE 100	187	167	Neve	PolG	38	0	0	110	75	0	0	110
IPE 100	187	167	Neve	PolG	75	0	0	110	119	0	0	76
IPE 100	187	167	Neve	PolG	0	0	0	26	38	0	0	35
IPE 100	187	167	Neve	PolG	38	0	0	35	119	0	0	24
IPE 100	187	167	Neve	PolG	75	0	0	35	119	0	0	24
IPE 100	187	167	Neve	PolG	0	0	0	14	38	0	0	33
IPE 100	187	167	Neve	PolG	38	0	0	33	119	0	0	33
IPE 100	187	167	Neve	PolG	0	0	0	36	75	0	0	36
IPE 100	187	167	Neve	PolG	75	0	0	36	119	0	0	15
IPE 100	187	167	Neve	PolG	0	0	0	55	75	0	0	55
IPE 100	187	167	Neve	PolG	75	0	0	55	119	0	0	23
IPE 100	187	167	Neve	PolG	0	0	0	21	38	0	0	50
IPE 100	187	167	Neve	PolG	38	0	0	50	119	0	0	50
IPE 100	187	167	Neve	PolG	0	0	0	8	119	0	0	8
IPE 100	187	167	Neve	PolG	45	0	0	110	68	0	0	110
IPE 100	187	167	Neve	PolG	68	0	0	110	119	0	0	80
IPE 100	187	167	Neve	PolG	0	0	0	27	45	0	0	35
IPE 100	187	167	Neve	PolG	45	0	0	35	68	0	0	35
IPE 100	187	167	Neve	PolG	68	0	0	35	119	0	0	26
IPE 100	187	167	Neve	PolG	0	0	0	36	68	0	0	36
IPE 100	187	167	Neve	PolG	68	0	0	36	119	0	0	17
IPE 100	187	167	Neve	PolG	0	0	0	16	45	0	0	33
IPE 100	187	167	Neve	PolG	45	0	0	33	119	0	0	33
IPE 100	187	167	Neve	PolG	0	0	0	55	68	0	0	55
IPE 100	187	167	Neve	PolG	68	0	0	55	119	0	0	27
IPE 100	187	167	Neve	PolG	0	0	0	25	45	0	0	50
IPE 100	187	167	Neve	PolG	45	0	0	50	119	0	0	50
IPE 100	187	167	Neve	PolG	0	0	0	8	125	0	0	8
IPE 100	187	167	Neve	PolG	0	0	0	70	31	0	0	100
IPE 100	187	167	Neve	PolG	31	0	0	100	88	0	0	100
IPE 100	187	167	Neve	PolG	88	0	0	100	125	0	0	67
IPE 100	187	167	Neve	PolG	0	0	0	22	31	0	0	32
IPE 100	187	167	Neve	PolG	31	0	0	32	88	0	0	32
IPE 100	187	167	Neve	PolG	88	0	0	32	125	0	0	21
IPE 100	187	167	Neve	PolG	0	0	0	11	31	0	0	30
IPE 100	187	167	Neve	PolG	31	0	0	30	125	0	0	30
IPE 100	187	167	Neve	PolG	0	0	0	33	88	0	0	33
IPE 100	187	167	Neve	PolG	88	0	0	33	125	0	0	12
IPE 100	187	167	Neve	PolG	0	0	0	50	88	0	0	50
IPE 100	187	167	Neve	PolG	88	0	0	50	125	0	0	18
IPE 100	187	167	Neve	PolG	0	0	0	17	31	0	0	46
IPE 100	187	167	Neve	PolG	31	0	0	46	125	0	0	46
IPE 100	187	167	Neve	PolG	0	0	0	8	126	0	0	8
IPE 100	187	167	Neve	PolG	0	0	0	81	52	0	0	100
IPE 100	187	167	Neve	PolG	52	0	0	100	67	0	0	100
IPE 100	187	167	Neve	PolG	67	0	0	100	126	0	0	79
IPE 100	187	167	Neve	PolG	0	0	0	26	52	0	0	32
IPE 100	187	167	Neve	PolG	52	0	0	32	67	0	0	32
IPE 100	187	167	Neve	PolG	67	0	0	32	126	0	0	25
IPE 100	187	167	Neve	PolG	0	0	0	18	52	0	0	30
IPE 100	187	167	Neve	PolG	52	0	0	30	126	0	0	30

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	29	47	Neve	PolG	0	0	0	33	67	0	0	33
IPE 100	29	47	Vento X	PolG	67	0	0	33	126	0	0	19
IPE 100	29	47	Vento X	PolG	67	0	0	50	67	0	0	50
IPE 100	29	47	Vento X	PolG	67	0	0	50	126	0	0	30
IPE 100	29	47	Vento X	PolG	0	0	0	28	52	0	0	46
IPE 100	29	47	Carichi termici	Termico	52	0	0	46	126	0	0	46
IPE 100	31	37	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C							
IPE 100	31	37	QP Solai	PolG	0	0	0	8	126	0	0	8
IPE 100	31	37	Neve	PolG	0	0	0	64	18	0	0	100
IPE 100	31	37	Neve	PolG	18	0	0	100	101	0	0	100
IPE 100	31	37	QV Solai	PolG	101	0	0	100	126	0	0	60
IPE 100	31	37	Neve	PolG	0	0	0	20	18	0	0	32
IPE 100	31	37	Neve	PolG	18	0	0	32	101	0	0	52
IPE 100	31	37	Neve	PolG	101	0	0	32	126	0	0	19
IPE 100	31	37	Neve	PolG	0	0	0	7	18	0	0	30
IPE 100	31	37	Neve	PolG	18	0	0	30	126	0	0	30
IPE 100	31	37	Neve	PolG	0	0	0	33	101	0	0	33
IPE 100	31	37	Vento X	PolG	101	0	0	33	126	0	0	8
IPE 100	31	37	Vento X	PolG	0	0	0	50	101	0	0	50
IPE 100	31	37	Vento X	PolG	101	0	0	50	126	0	0	12
IPE 100	31	37	Vento X	PolG	0	0	0	11	18	0	0	46
IPE 100	31	37	Carichi termici	Termico	18	0	0	46	126	0	0	46
IPE 100	33	39	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C							
IPE 100	33	39	QP Solai	PolG	0	0	0	8	128	0	0	8
IPE 100	33	39	Neve	PolG	0	0	0	57	6	0	0	100
IPE 100	33	39	Neve	PolG	6	0	0	100	115	0	0	100
IPE 100	33	39	QV Solai	PolG	115	0	0	100	128	0	0	53
IPE 100	33	39	Neve	PolG	0	0	0	18	6	0	0	32
IPE 100	33	39	Neve	PolG	6	0	0	32	115	0	0	32
IPE 100	33	39	Neve	PolG	115	0	0	32	128	0	0	17
IPE 100	33	39	Neve	PolG	0	0	0	3	6	0	0	30
IPE 100	33	39	Neve	PolG	6	0	0	30	128	0	0	30
IPE 100	33	39	Neve	PolG	0	0	0	33	115	0	0	33
IPE 100	33	39	Vento X	PolG	115	0	0	33	128	0	0	3
IPE 100	33	39	Vento X	PolG	0	0	0	50	115	0	0	50
IPE 100	33	39	Vento X	PolG	115	0	0	50	128	0	0	5
IPE 100	33	39	Vento X	PolG	0	0	0	5	6	0	0	46
IPE 100	33	39	Vento X	PolG	6	0	0	46	128	0	0	46
IPE 100	35	53	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	35	53	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	35	53	QP Solai	PolG	0	0	0	100	31	0	0	100
IPE 100	35	53	QV Solai	PolG	31	0	0	100	125	0	0	98
IPE 100	35	53	Neve	PolG	0	0	0	32	125	0	0	31
IPE 100	35	53	Neve	PolG	0	0	0	33	31	0	0	33
IPE 100	35	53	Neve	PolG	31	0	0	30	125	0	0	31
IPE 100	35	53	Vento X	PolG	0	0	0	30	125	0	0	30
IPE 100	35	53	Vento X	PolG	0	0	0	50	31	0	0	50
IPE 100	35	53	Vento X	PolG	31	0	0	50	125	0	0	48
IPE 100	35	53	Carichi termici	Termico	0	0	0	46	125	0	0	46
IPE 100	37	27	Peso Proprio	UnifG	AXY=15°C,AXZ=15°C							
IPE 100	37	27	QP Solai	PolG	0	0	0	8	126	0	0	8
IPE 100	37	27	Neve	PolG	0	0	0	67	25	0	0	100
IPE 100	37	27	Neve	PolG	25	0	0	100	95	0	0	100
IPE 100	37	27	QV Solai	PolG	95	0	0	100	126	0	0	63
IPE 100	37	27	Neve	PolG	0	0	0	21	25	0	0	32
IPE 100	37	27	Neve	PolG	25	0	0	32	95	0	0	32
IPE 100	37	27	Neve	PolG	95	0	0	32	126	0	0	20
IPE 100	37	27	Neve	PolG	0	0	0	33	95	0	0	33
IPE 100	37	27	Neve	PolG	95	0	0	33	126	0	0	10
IPE 100	37	27	Vento X	PolG	0	0	0	9	25	0	0	30
IPE 100	37	27	Vento X	PolG	25	0	0	30	126	0	0	30
IPE 100	37	27	Vento X	PolG	0	0	0	14	25	0	0	46
IPE 100	37	27	Vento X	PolG	25	0	0	46	126	0	0	46
IPE 100	37	27	Carichi termici	Termico	95	0	0	50	95	0	0	50
IPE 100	37	27	Carichi termici	Termico	0	0	0	50	126	0	0	15

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf	
IPE 100	39	31	Peso Proprio QP Solai	UnifG	0	0	0	0	124	0	0	8	
IPE 100	39	31		PolG	0	0	0	60	12	0	0	100	
				12	0	0	100	106	0	0	100		
					106	0	0	100	124	0	0	56	
IPE 100	39	31	QV Solai	PolG	0	0	0	19	12	0	0	32	
					12	0	0	32	106	0	0	32	
					106	0	0	32	124	0	0	18	
IPE 100	39	31	Neve	PolG	0	0	0	33	106	0	0	33	
					106	0	0	33	124	0	0	5	
IPE 100	39	31	Neve	PolG	0	0	0	5	12	0	0	30	
					12	0	0	30	124	0	0	30	
IPE 100	39	31	Vento X	PolG	0	0	0	8	12	0	0	46	
					12	0	0	46	124	0	0	46	
IPE 100	39	31	Vento X	PolG	0	0	0	50	106	0	0	50	
					106	0	0	50	124	0	0	8	
IPE 100	39	31	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C								
IPE 100	41	43	Peso Proprio QP Solai	UnifG	0	0	0	0	8	125	0	0	8
IPE 100	41	43		PolG	0	0	0	74	38	0	0	100	
				38	0	0	100	81	0	0	100		
					81	0	0	100	125	0	0	71	
IPE 100	41	43	QV Solai	PolG	0	0	0	24	38	0	0	32	
					38	0	0	32	81	0	0	32	
					81	0	0	32	125	0	0	23	
IPE 100	41	43	Neve	PolG	0	0	0	13	38	0	0	30	
					38	0	0	30	125	0	0	30	
IPE 100	41	43	Neve	PolG	0	0	0	33	81	0	0	33	
					81	0	0	33	125	0	0	14	
IPE 100	41	43	Vento X	PolG	0	0	0	21	38	0	0	46	
					38	0	0	46	125	0	0	46	
IPE 100	41	43	Vento X	PolG	0	0	0	50	81	0	0	50	
					81	0	0	50	125	0	0	22	
IPE 100	41	43	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C								
IPE 100	43	29	Peso Proprio QP Solai	UnifG	0	0	0	0	8	125	0	0	8
IPE 100	43	29		PolG	0	0	0	77	45	0	0	100	
				45	0	0	100	74	0	0	100		
					74	0	0	100	125	0	0	75	
IPE 100	43	29	QV Solai	PolG	0	0	0	25	45	0	0	32	
					45	0	0	32	74	0	0	32	
					74	0	0	32	125	0	0	24	
IPE 100	43	29	Neve	PolG	0	0	0	33	74	0	0	33	
					74	0	0	33	125	0	0	17	
IPE 100	43	29	Neve	PolG	0	0	0	16	45	0	0	30	
					45	0	0	30	125	0	0	30	
IPE 100	43	29	Vento X	PolG	0	0	0	24	45	0	0	46	
					45	0	0	46	125	0	0	46	
IPE 100	43	29	Vento X	PolG	0	0	0	50	74	0	0	50	
					74	0	0	50	125	0	0	26	
IPE 100	43	29	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C								
IPE 100	45	61	Peso Proprio QP Solai	UnifG	0	0	0	0	8	125	0	0	8
IPE 100	45	61		PolG	0	0	0	99	36	0	0	118	
				36	0	0	118	95	0	0	117		
					95	0	0	117	123	0	0	101	
					123	0	0	53	125	0	0	52	
IPE 100	45	61	QV Solai	PolG	0	0	0	32	36	0	0	38	
					36	0	0	38	95	0	0	37	
					95	0	0	37	123	0	0	32	
					123	0	0	17	125	0	0	17	
IPE 100	45	61	Neve	PolG	0	0	0	30	36	0	0	38	
					36	0	0	38	123	0	0	30	
IPE 100	45	61	Neve	PolG	0	0	0	32	95	0	0	40	
					95	0	0	40	125	0	0	33	
IPE 100	45	61	Vento X	PolG	0	0	0	49	95	0	0	62	
					95	0	0	62	125	0	0	50	
IPE 100	45	61	Vento X	PolG	0	0	0	46	36	0	0	59	
					36	0	0	59	123	0	0	46	
IPE 100	45	61	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C								

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	47	57	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	47	57	QP Solai	PolG	0	0	0	86	59	0	0	100
IPE 100	47	57	QV Solai	PolG	59	0	0	100	126	0	0	83
IPE 100	47	57	Neve	PolG	59	0	0	32	126	0	0	27
IPE 100	47	57	Neve	PolG	59	0	0	33	59	0	0	33
IPE 100	47	57	Neve	PolG	59	0	0	33	126	0	0	22
IPE 100	47	57	Neve	PolG	60	0	0	21	60	0	0	30
IPE 100	47	57	Vento X	PolG	60	0	0	30	126	0	0	30
IPE 100	47	57	Vento X	PolG	0	0	0	32	60	0	0	46
IPE 100	47	57	Vento X	PolG	60	0	0	46	126	0	0	46
IPE 100	47	57	Vento X	PolG	59	0	0	50	59	0	0	50
IPE 100	47	57	Vento X	PolG	59	0	0	50	126	0	0	34
IPE 100	47	57	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	49	35	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	49	35	QP Solai	PolG	0	0	0	95	42	0	0	98
IPE 100	49	35	QP Solai	PolG	42	0	0	98	78	0	0	97
IPE 100	49	35	QV Solai	PolG	78	0	0	97	126	0	0	93
IPE 100	49	35	QV Solai	PolG	0	0	0	30	42	0	0	31
IPE 100	49	35	Vento X	PolG	42	0	0	31	78	0	0	31
IPE 100	49	35	Vento X	PolG	78	0	0	31	126	0	0	30
IPE 100	49	35	Neve	PolG	0	0	0	33	42	0	0	33
IPE 100	49	35	Neve	PolG	42	0	0	33	126	0	0	28
IPE 100	49	35	Neve	PolG	0	0	0	27	78	0	0	30
IPE 100	49	35	Vento X	PolG	78	0	0	30	126	0	0	30
IPE 100	49	35	Vento X	PolG	0	0	0	50	42	0	0	50
IPE 100	49	35	Vento X	PolG	42	0	0	50	126	0	0	43
IPE 100	49	35	Vento X	PolG	0	0	0	41	78	0	0	46
IPE 100	49	35	Vento X	PolG	78	0	0	41	78	0	0	46
IPE 100	49	35	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	51	55	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	51	55	QP Solai	PolG	0	0	0	88	55	0	0	125
IPE 100	51	55	QP Solai	PolG	55	0	0	125	76	0	0	125
IPE 100	51	55	QV Solai	PolG	76	0	0	125	126	0	0	91
IPE 100	51	55	QV Solai	PolG	0	0	0	28	55	0	0	40
IPE 100	51	55	Neve	PolG	55	0	0	40	76	0	0	40
IPE 100	51	55	Neve	PolG	76	0	0	40	126	0	0	29
IPE 100	51	55	Neve	PolG	0	0	0	30	55	0	0	40
IPE 100	51	55	Neve	PolG	55	0	0	40	126	0	0	24
IPE 100	51	55	Vento X	PolG	0	0	0	25	76	0	0	42
IPE 100	51	55	Vento X	PolG	76	0	0	42	126	0	0	33
IPE 100	51	55	Vento X	PolG	0	0	0	46	55	0	0	62
IPE 100	51	55	Vento X	PolG	55	0	0	62	126	0	0	37
IPE 100	51	55	Vento X	PolG	0	0	0	39	76	0	0	66
IPE 100	51	55	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	53	59	Peso Proprio	UnifG	76	0	0	66	126	0	0	50
IPE 100	53	59	QP Solai	PolG	0	0	0	8	126	0	0	8
IPE 100	53	59	QP Solai	PolG	13	0	0	100	13	0	0	107
IPE 100	53	59	QV Solai	PolG	13	0	0	107	22	0	0	106
IPE 100	53	59	QV Solai	PolG	22	0	0	106	98	0	0	103
IPE 100	53	59	Neve	PolG	98	0	0	103	118	0	0	104
IPE 100	53	59	Neve	PolG	118	0	0	104	126	0	0	100
IPE 100	53	59	QV Solai	PolG	0	0	0	32	13	0	0	34
IPE 100	53	59	QV Solai	PolG	13	0	0	34	22	0	0	34
IPE 100	53	59	Neve	PolG	22	0	0	34	98	0	0	33
IPE 100	53	59	Neve	PolG	98	0	0	33	118	0	0	33
IPE 100	53	59	Neve	PolG	118	0	0	33	126	0	0	32
IPE 100	53	59	QV Solai	PolG	0	0	0	30	13	0	0	34
IPE 100	53	59	QV Solai	PolG	13	0	0	34	98	0	0	30
IPE 100	53	59	Neve	PolG	98	0	0	30	126	0	0	30
IPE 100	53	59	Neve	PolG	0	0	0	33	22	0	0	33
IPE 100	53	59	Neve	PolG	22	0	0	33	118	0	0	35
IPE 100	53	59	Vento X	PolG	118	0	0	35	126	0	0	33
IPE 100	53	59	Vento X	PolG	0	0	0	50	22	0	0	50
IPE 100	53	59	Vento X	PolG	22	0	0	50	118	0	0	54
IPE 100	53	59	Vento X	PolG	118	0	0	54	126	0	0	50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	53	59	Vento X	PolG								
					13	0	0	46	13	0	0	52
								52	98	0	0	46
					98	0	0	46	126	0	0	46
IPE 100	53	59	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
IPE 100	55	63	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	55	63	QP Solai	PolG	0	0	0	84	64	0	0	132
					64	0	0	132	68	0	0	132
IPE 100	55	63	QV Solai	PolG	68	0	0	132	126	0	0	86
					0	0	0	27	64	0	0	42
IPE 100	55	63	QV Solai	PolG	64	0	0	42	68	0	0	42
					68	0	0	42	126	0	0	28
IPE 100	55	63	Neve	PolG	0	0	0	22	68	0	0	43
IPE 100	55	63	Neve	PolG	68	0	0	43	126	0	0	33
					0	0	0	30	64	0	0	40
IPE 100	55	63	Vento X	PolG	64	0	0	40	126	0	0	21
					0	0	0	46	64	0	0	63
IPE 100	55	63	Vento X	PolG	64	0	0	63	126	0	0	33
					0	0	0	35	68	0	0	66
IPE 100	55	63	Vento X	PolG	68	0	0	66	126	0	0	50
IPE 100	55	63	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
IPE 100	57	49	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	57	49	QP Solai	PolG	0	0	0	90	51	0	0	97
					51	0	0	97	68	0	0	97
IPE 100	57	49	QV Solai	PolG	68	0	0	97	125	0	0	87
					0	0	0	29	51	0	0	31
					51	0	0	31	68	0	0	31
					68	0	0	31	125	0	0	28
IPE 100	57	49	Neve	PolG	0	0	0	33	51	0	0	33
IPE 100	57	49	Neve	PolG	51	0	0	33	125	0	0	24
					0	0	0	23	68	0	0	30
IPE 100	57	49	Vento X	PolG	68	0	0	30	125	0	0	30
					0	0	0	36	68	0	0	46
IPE 100	57	49	Vento X	PolG	68	0	0	46	125	0	0	46
					0	0	0	50	51	0	0	50
IPE 100	57	49	Vento X	PolG	51	0	0	50	125	0	0	38
IPE 100	57	49	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
IPE 100	59	45	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	59	45	QP Solai	PolG	0	0	0	100	10	0	0	104
					10	0	0	104	25	0	0	113
					25	0	0	113	106	0	0	109
					106	0	0	109	110	0	0	107
IPE 100	59	45	QV Solai	PolG	110	0	0	107	126	0	0	100
					0	0	0	32	10	0	0	33
					10	0	0	33	25	0	0	36
					25	0	0	36	106	0	0	35
					106	0	0	35	110	0	0	34
IPE 100	59	45	Neve	PolG	110	0	0	34	126	0	0	32
					0	0	0	33	10	0	0	33
					10	0	0	33	106	0	0	38
IPE 100	59	45	Neve	PolG	106	0	0	38	126	0	0	33
					0	0	0	30	25	0	0	37
					25	0	0	37	110	0	0	30
IPE 100	59	45	Vento X	PolG	110	0	0	30	126	0	0	30
					0	0	0	46	25	0	0	57
					25	0	0	57	110	0	0	46
IPE 100	59	45	Vento X	PolG	110	0	0	46	126	0	0	46
					0	0	0	50	10	0	0	50
					10	0	0	50	106	0	0	59
IPE 100	59	45	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C							
IPE 100	61	51	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	61	51	QP Solai	PolG	0	0	0	93	46	0	0	121
					46	0	0	121	85	0	0	121
					85	0	0	121	125	0	0	96
IPE 100	61	51	QV Solai	PolG	46	0	0	30	46	0	0	39
					46	0	0	39	85	0	0	39

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	61	51	Neve	PolG	85	0	0	39	125	0	0	31
IPE 100					0	0	0	0	46	0	0	40
IPE 100	61	51	Neve	PolG	46	0	0	40	125	0	0	27
IPE 100					0	0	0	28	85	0	0	42
IPE 100			Vento X	PolG	85	0	0	42	125	0	0	33
IPE 100	61	51	Vento X	PolG	0	0	0	46	46	0	0	61
IPE 100	61	51	Vento X	PolG	46	0	0	61	125	0	0	42
IPE 100					85	0	0	44	85	0	0	64
IPE 100	61	51	Carichi termici	Termico	85	0	0	64	125	0	0	50
IPE 100	63	67	Peso Proprio	UnifG	AXY=15°C, AXZ=15°C							
IPE 100	63	67	QP Solai	PolG	0	0	0	8	125	0	0	8
					60	0	0	131	71	0	0	131
IPE 100	63	67	QV Solai	PolG	71	0	0	131	125	0	0	82
					60	0	0	26	60	0	0	42
					60	0	0	42	71	0	0	26
IPE 100	63	67	Neve	PolG	71	0	0	42	125	0	0	42
IPE 100					0	0	0	20	60	0	0	43
IPE 100	63	67	Neve	PolG	60	0	0	43	125	0	0	33
IPE 100					0	0	0	30	71	0	0	40
IPE 100	63	67	Vento X	PolG	71	0	0	40	125	0	0	19
IPE 100					0	0	0	31	60	0	0	66
IPE 100	63	67	Vento X	PolG	60	0	0	66	125	0	0	50
IPE 100	63	67	Vento X	PolG	0	0	0	46	71	0	0	62
IPE 100					71	0	0	62	125	0	0	29
IPE 100	63	67	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	65	77	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	65	77	QP Solai	PolG	0	0	0	53	12	0	0	100
					12	0	0	100	119	0	0	100
IPE 100					119	0	0	100	125	0	0	57
IPE 100	65	77	QV Solai	PolG	0	0	0	17	12	0	0	32
					12	0	0	32	119	0	0	32
IPE 100	65	77	Neve	PolG	119	0	0	32	125	0	0	18
IPE 100					0	0	0	30	119	0	0	30
IPE 100	65	77	Neve	PolG	119	0	0	30	125	0	0	3
IPE 100					12	0	0	3	12	0	0	33
IPE 100	65	77	Vento X	PolG	0	0	0	46	119	0	0	46
IPE 100					119	0	0	46	125	0	0	4
IPE 100	65	77	Vento X	PolG	0	0	0	5	12	0	0	50
					12	0	0	50	125	0	0	50
IPE 100	65	77	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	69	33	Peso Proprio	UnifG	0	0	0	8	124	0	0	8
IPE 100	69	33	QP Solai	PolG	0	0	0	102	118	0	0	100
IPE 100					118	0	0	100	124	0	0	49
IPE 100	69	33	QV Solai	PolG	0	0	0	33	118	0	0	32
IPE 100					118	0	0	32	124	0	0	16
IPE 100	69	33	Neve	PolG	0	0	0	33	118	0	0	33
IPE 100					118	0	0	33	124	0	0	1
IPE 100	69	33	Neve	PolG	0	0	0	31	124	0	0	30
IPE 100	69	33	Vento X	PolG	0	0	0	47	124	0	0	46
IPE 100	69	33	Vento X	PolG	0	0	0	50	118	0	0	50
IPE 100					118	0	0	50	124	0	0	1
IPE 100	69	33	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	71	65	Peso Proprio	UnifG	0	0	0	8	125	0	0	8
IPE 100	71	65	QP Solai	PolG	0	0	0	56	18	0	0	100
					18	0	0	100	113	0	0	100
IPE 100					113	0	0	100	125	0	0	60
IPE 100	71	65	QV Solai	PolG	0	0	0	18	18	0	0	32
					18	0	0	32	113	0	0	32
IPE 100					113	0	0	32	125	0	0	19
IPE 100	71	65	Neve	PolG	0	0	0	30	113	0	0	30
IPE 100					113	0	0	30	125	0	0	5
IPE 100	71	65	Neve	PolG	0	0	0	5	18	0	0	33
IPE 100					18	0	0	33	125	0	0	33
IPE 100	71	65	Vento X	PolG	0	0	0	8	18	0	0	50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	71	65	Vento X	PolG	18	0	0	50	125	0	0	50
IPE 100					0	0	0	46	113	0	0	46
IPE 100	71	65	Carichi termici	Termico	113	0	0	46	125	0	0	7
IPE 100	73	75	Peso Proprio	UnifG	AXY=15°C, AXZ=15°C							
IPE 100	73	75	QP Solai	PolG	0	0	0	8	126	0	0	8
					30	0	0	63	30	0	0	100
IPE 100					101	0	0	100	126	0	0	67
IPE 100	73	75	QV Solai	PolG	0	0	0	20	30	0	0	32
					30	0	0	32	101	0	0	32
IPE 100					101	0	0	32	126	0	0	21
IPE 100	73	75	Neve	PolG	0	0	0	10	30	0	0	33
IPE 100					30	0	0	33	126	0	0	33
IPE 100	73	75	Neve	PolG	0	0	0	30	101	0	0	30
IPE 100					101	0	0	30	126	0	0	9
IPE 100	73	75	Vento X	PolG	0	0	0	15	30	0	0	50
IPE 100					30	0	0	50	126	0	0	50
IPE 100	73	75	Vento X	PolG	0	0	0	46	101	0	0	46
IPE 100					101	0	0	46	126	0	0	14
IPE 100	73	75	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	75	71	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	75	71	QP Solai	PolG	0	0	0	60	24	0	0	100
					24	0	0	100	108	0	0	100
IPE 100					108	0	0	100	126	0	0	63
IPE 100	75	71	QV Solai	PolG	0	0	0	19	24	0	0	32
					24	0	0	32	108	0	0	32
IPE 100					108	0	0	32	126	0	0	20
IPE 100	75	71	Neve	PolG	0	0	0	30	108	0	0	30
IPE 100					108	0	0	30	126	0	0	7
IPE 100	75	71	Neve	PolG	0	0	0	7	24	0	0	33
IPE 100					24	0	0	33	126	0	0	33
IPE 100	75	71	Vento X	PolG	0	0	0	11	24	0	0	50
IPE 100					24	0	0	50	126	0	0	50
IPE 100	75	71	Vento X	PolG	0	0	0	46	108	0	0	46
					108	0	0	46	126	0	0	11
IPE 100	75	71	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	77	69	Peso Proprio	UnifG	0	0	0	8	126	0	0	8
IPE 100	77	69	QP Solai	PolG	0	0	0	49	6	0	0	100
IPE 100					6	0	0	100	126	0	0	102
IPE 100	77	69	QV Solai	PolG	0	0	0	16	6	0	0	32
					6	0	0	32	126	0	0	33
IPE 100	77	69	Neve	PolG	0	0	0	1	6	0	0	33
IPE 100					6	0	0	33	126	0	0	33
IPE 100	77	69	Neve	PolG	0	0	0	30	126	0	0	31
IPE 100	77	69	Vento X	PolG	0	0	0	46	126	0	0	47
IPE 100	77	69	Vento X	PolG	0	0	0	1	6	0	0	50
IPE 100					6	0	0	50	126	0	0	50
IPE 100	77	69	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	28	42	Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	28	42	QP Solai	PolG	0	0	0	65	31	0	0	92
					31	0	0	92	94	0	0	92
IPE 100					94	0	0	92	131	0	0	62
IPE 100	28	42	QV Solai	PolG	0	0	0	21	31	0	0	29
					31	0	0	29	94	0	0	29
IPE 100					94	0	0	29	131	0	0	20
IPE 100	28	42	Neve	PolG	0	0	0	30	94	0	0	30
IPE 100					94	0	0	30	131	0	0	11
IPE 100	28	42	Neve	PolG	0	0	0	11	31	0	0	27
IPE 100					31	0	0	27	131	0	0	27
IPE 100	28	42	Vento X	PolG	0	0	0	16	31	0	0	42
IPE 100					31	0	0	42	131	0	0	42
IPE 100	28	42	Vento X	PolG	0	0	0	46	94	0	0	46
IPE 100					94	0	0	46	131	0	0	18
IPE 100	28	42	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	30	48	Peso Proprio	UnifG	0	0	0	8	132	0	0	8

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	30	48	QP Solai	PolG	0	0	0	76	52	0	0	92
					52	0	0	92	73	0	0	92
IPE 100	30	48	QV Solai	PolG	0	0	0	24	52	0	0	74
					52	0	0	29	73	0	0	29
IPE 100	30	48	Neve	PolG	73	0	0	29	132	0	0	24
					0	0	0	30	73	0	0	30
IPE 100	30	48	Neve	PolG	73	0	0	17	52	0	0	18
					52	0	0	27	132	0	0	27
IPE 100	30	48	Vento X	PolG	0	0	0	46	73	0	0	46
					73	0	0	46	132	0	0	28
IPE 100	30	48	Vento X	PolG	0	0	0	27	52	0	0	42
					52	0	0	42	132	0	0	42
IPE 100	30	48	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
			Peso Proprio	UnifG	0	0	0	8	132	0	0	8
IPE 100	32	38	QP Solai	PolG	0	0	0	59	18	0	0	92
					18	0	0	92	107	0	0	92
IPE 100	32	38	QV Solai	PolG	107	0	0	19	18	0	0	56
					18	0	0	29	107	0	0	29
IPE 100	32	38	Neve	PolG	107	0	0	29	132	0	0	18
					0	0	0	7	18	0	0	27
IPE 100	32	38	Neve	PolG	18	0	0	30	107	0	0	30
					107	0	0	30	132	0	0	7
IPE 100	32	38	Vento X	PolG	0	0	0	46	107	0	0	46
					107	0	0	46	132	0	0	11
IPE 100	34	40	Vento X	PolG	0	0	0	10	18	0	0	42
					18	0	0	42	132	0	0	42
IPE 100	32	38	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
			Peso Proprio	UnifG	0	0	0	8	134	0	0	8
IPE 100	34	40	QP Solai	PolG	0	0	0	53	6	0	0	92
					6	0	0	92	122	0	0	92
IPE 100	34	40	QV Solai	PolG	122	0	0	92	134	0	0	49
					0	0	0	17	6	0	0	29
IPE 100	34	40	Neve	PolG	6	0	0	29	122	0	0	29
					122	0	0	29	134	0	0	16
IPE 100	34	40	Neve	PolG	0	0	0	30	122	0	0	30
					122	0	0	30	134	0	0	3
IPE 100	34	40	Neve	PolG	0	0	0	3	6	0	0	27
					6	0	0	27	134	0	0	27
IPE 100	34	40	Vento X	PolG	0	0	0	46	122	0	0	46
					122	0	0	46	134	0	0	5
IPE 100	34	40	Vento X	PolG	0	0	0	5	6	0	0	42
					6	0	0	42	134	0	0	42
IPE 100	34	40	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
			Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	36	54	QP Solai	PolG	0	0	0	92	5	0	0	95
					5	0	0	95	88	0	0	92
IPE 100	36	54	QV Solai	PolG	88	0	0	92	131	0	0	92
					0	0	0	29	131	0	0	29
IPE 100	36	54	Neve	PolG	0	0	0	30	131	0	0	30
					0	0	0	27	5	0	0	29
IPE 100	36	54	Neve	PolG	5	0	0	29	88	0	0	27
					88	0	0	27	131	0	0	27
IPE 100	36	54	Vento X	PolG	0	0	0	46	131	0	0	46
					0	0	0	42	5	0	0	45
IPE 100	36	54	Vento X	PolG	5	0	0	45	88	0	0	42
					88	0	0	42	131	0	0	42
IPE 100	36	54	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
			Peso Proprio	UnifG	0	0	0	8	132	0	0	8
IPE 100	38	28	QP Solai	PolG	0	0	0	62	25	0	0	92
					25	0	0	92	101	0	0	92
IPE 100	38	28	QV Solai	PolG	101	0	0	92	132	0	0	59
					0	0	0	20	25	0	0	29

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					25	0	0	29	101	0	0	29
IPE 100	38	28	Neve	PolG	101	0	0	29	132	0	0	19
					0	0	0	30	101	0	0	30
IPE 100	38	28	Neve	PolG	101	0	0	30	132	0	0	9
					0	0	0	9	25	0	0	27
IPE 100	38	28	Vento X	PolG	25	0	0	27	132	0	0	27
					0	0	0	13	25	0	0	42
IPE 100	38	28	Vento X	PolG	25	0	0	42	132	0	0	42
					0	0	0	46	101	0	0	46
IPE 100	38	28	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
			Peso Proprio	UnifG	0	0	0	8	130	0	0	8
IPE 100	40	32	QP Solai	PolG	12	0	0	92	112	0	0	92
					112	0	0	92	130	0	0	52
IPE 100	40	32	QV Solai	PolG	0	0	0	18	12	0	0	29
					12	0	0	29	112	0	0	29
IPE 100	40	32	Neve	PolG	0	0	0	5	12	0	0	27
					12	0	0	27	130	0	0	27
IPE 100	40	32	Neve	PolG	0	0	0	30	112	0	0	30
					112	0	0	30	130	0	0	5
IPE 100	40	32	Vento X	PolG	0	0	0	46	112	0	0	46
					112	0	0	46	130	0	0	8
IPE 100	40	32	Vento X	PolG	0	0	0	7	12	0	0	42
					12	0	0	42	130	0	0	42
IPE 100	40	32	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
			Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	42	44	QP Solai	PolG	38	0	0	92	87	0	0	92
					87	0	0	92	131	0	0	66
IPE 100	42	44	QV Solai	PolG	0	0	0	22	38	0	0	29
					38	0	0	22	87	0	0	29
IPE 100	42	44	Neve	PolG	87	0	0	29	131	0	0	21
					0	0	0	13	38	0	0	27
IPE 100	42	44	Neve	PolG	38	0	0	27	131	0	0	27
					0	0	0	30	87	0	0	30
IPE 100	42	44	Vento X	PolG	87	0	0	30	131	0	0	14
					0	0	0	46	87	0	0	46
IPE 100	42	44	Vento X	PolG	87	0	0	46	131	0	0	21
					0	0	0	20	38	0	0	42
IPE 100	42	44	Vento X	PolG	38	0	0	42	131	0	0	42
					AXY=15°C, AXZ=15°C							
IPE 100	42	44	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
			Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	44	30	QP Solai	PolG	0	0	0	72	45	0	0	92
					45	0	0	92	80	0	0	92
IPE 100	44	30	QV Solai	PolG	80	0	0	23	45	0	0	29
					0	0	0	29	80	0	0	29
IPE 100	44	30	Neve	PolG	45	0	0	29	131	0	0	22
					80	0	0	30	80	0	0	30
IPE 100	44	30	Neve	PolG	80	0	0	30	131	0	0	16
					0	0	0	15	45	0	0	27
IPE 100	44	30	Vento X	PolG	45	0	0	23	45	0	0	27
					0	0	0	42	131	0	0	42
IPE 100	44	30	Vento X	PolG	45	0	0	42	131	0	0	46
					0	0	0	46	80	0	0	46
IPE 100	44	30	Vento X	PolG	80	0	0	46	131	0	0	25
					AXY=15°C, AXZ=15°C							
IPE 100	44	30	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
			Peso Proprio	UnifG	0	0	0	8	131	0	0	8
IPE 100	46	62	QP Solai	PolG	0	0	0	92	42	0	0	113
					42	0	0	113	95	0	0	110
IPE 100	46	62	QV Solai	PolG	95	0	0	110	123	0	0	95
					123	0	0	95	131	0	0	92
IPE 100	46	62	QV Solai	PolG	0	0	0	29	42	0	0	36
					42	0	0	36	95	0	0	35

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					95	0	0	0	35	123	0	0
					123	0	0	0	30	131	0	0
IPE 100	46	62	Neve	PolG	0	0	0	0	30	95	0	0
					95	0	0	0	38	131	0	0
IPE 100	46	62	Neve	PolG	0	0	0	0	27	42	0	0
					42	0	0	0	37	123	0	0
					123	0	0	0	27	131	0	0
IPE 100	46	62	Vento X	PolG	0	0	0	0	46	95	0	0
					95	0	0	0	59	131	0	0
IPE 100	46	62	Vento X	PolG	0	0	0	0	42	42	0	0
					42	0	0	0	57	123	0	0
					123	0	0	0	42	131	0	0
IPE 100	46	62	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	48	58	Peso Proprio	UnitG	0	0	0	0	8	132	0	0
IPE 100	48	58	QP Solai	PolG	0	0	0	0	80	60	0	0
					60	0	0	0	92	65	0	0
					65	0	0	0	92	132	0	0
IPE 100	48	58	QV Solai	PolG	0	0	0	0	26	60	0	0
					60	0	0	0	29	65	0	0
					65	0	0	0	29	132	0	0
IPE 100	48	58	Neve	PolG	0	0	0	0	30	65	0	0
					65	0	0	0	30	132	0	0
IPE 100	48	58	Neve	PolG	0	0	0	0	20	60	0	0
					60	0	0	0	27	132	0	0
IPE 100	48	58	Vento X	PolG	0	0	0	0	46	65	0	0
					65	0	0	0	46	132	0	0
IPE 100	48	58	Vento X	PolG	0	0	0	0	31	60	0	0
					60	0	0	0	42	132	0	0
IPE 100	48	58	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	50	36	Peso Proprio	UnitG	0	0	0	0	8	132	0	0
IPE 100	50	36	QP Solai	PolG	0	0	0	0	89	48	0	0
					48	0	0	0	91	78	0	0
					78	0	0	0	90	132	0	0
IPE 100	50	36	QV Solai	PolG	0	0	0	0	29	48	0	0
					48	0	0	0	29	132	0	0
					48	0	0	0	30	48	0	0
IPE 100	50	36	Neve	PolG	0	0	0	0	26	78	0	0
					78	0	0	0	27	132	0	0
IPE 100	50	36	Vento X	PolG	0	0	0	0	40	78	0	0
					78	0	0	0	42	132	0	0
IPE 100	50	36	Vento X	PolG	0	0	0	0	46	48	0	0
					48	0	0	0	46	132	0	0
IPE 100	50	36	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	52	56	Peso Proprio	UnitG	0	0	0	0	8	132	0	0
IPE 100	52	56	QP Solai	PolG	0	0	0	0	83	61	0	0
					61	0	0	0	121	76	0	0
					76	0	0	0	120	132	0	0
IPE 100	52	56	QV Solai	PolG	0	0	0	0	27	61	0	0
					61	0	0	0	39	76	0	0
					76	0	0	0	39	132	0	0
IPE 100	52	56	Neve	PolG	0	0	0	0	27	61	0	0
					61	0	0	0	38	132	0	0
IPE 100	52	56	Neve	PolG	0	0	0	0	24	76	0	0
					76	0	0	0	40	132	0	0
IPE 100	52	56	Vento X	PolG	0	0	0	0	37	76	0	0
					76	0	0	0	62	132	0	0
IPE 100	52	56	Vento X	PolG	0	0	0	0	42	61	0	0
					61	0	0	0	59	132	0	0
IPE 100	52	56	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	54	60	Peso Proprio	UnitG	0	0	0	0	8	131	0	0
IPE 100	54	60	QP Solai	PolG	0	0	0	0	92	19	0	0
					19	0	0	0	100	28	0	0
					28	0	0	0	100	98	0	0
					98	0	0	0	97	118	0	0
					118	0	0	0	98	131	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	54	60	QV Solai	PolG	0	0	0	0	29	19	0	0
					19	0	0	0	32	28	0	0
					28	0	0	0	32	98	0	0
					98	0	0	0	31	118	0	0
IPE 100	54	60	Neve	PolG	0	0	0	0	31	131	0	0
					28	0	0	0	30	28	0	0
					118	0	0	0	33	131	0	0
IPE 100	54	60	Neve	PolG	0	0	0	0	27	19	0	0
					19	0	0	0	33	98	0	0
					98	0	0	0	27	131	0	0
IPE 100	54	60	Vento X	PolG	0	0	0	0	46	28	0	0
					28	0	0	0	46	118	0	0
IPE 100	54	60	Vento X	PolG	0	0	0	0	52	131	0	0
					118	0	0	0	42	19	0	0
					19	0	0	0	51	98	0	0
					98	0	0	0	42	131	0	0
IPE 100	54	60	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	56	64	Peso Proprio	UnitG	0	0	0	0	8	131	0	0
IPE 100	56	64	QP Solai	PolG	0	0	0	0	79	68	0	0
					68	0	0	0	126	70	0	0
					70	0	0	0	125	131	0	0
IPE 100	56	64	QV Solai	PolG	0	0	0	0	25	68	0	0
					68	0	0	0	40	70	0	0
					70	0	0	0	40	131	0	0
IPE 100	56	64	Neve	PolG	0	0	0	0	21	68	0	0
					68	0	0	0	40	131	0	0
IPE 100	56	64	Neve	PolG	0	0	0	0	27	70	0	0
					70	0	0	0	38	131	0	0
IPE 100	56	64	Vento X	PolG	0	0	0	0	42	70	0	0
					70	0	0	0	59	131	0	0
IPE 100	56	64	Vento X	PolG	0	0	0	0	33	68	0	0
					68	0	0	0	62	131	0	0
IPE 100	56	64	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	58	50	Peso Proprio	UnitG	0	0	0	0	8	131	0	0
IPE 100	58	50	QP Solai	PolG	0	0	0	0	84	57	0	0
					57	0	0	0	91	68	0	0
					68	0	0	0	90	131	0	0
IPE 100	58	50	QV Solai	PolG	0	0	0	0	27	57	0	0
					57	0	0	0	29	68	0	0
					68	0	0	0	29	131	0	0
IPE 100	58	50	Neve	PolG	0	0	0	0	22	68	0	0
					68	0	0	0	27	131	0	0
IPE 100	58	50	Neve	PolG	0	0	0	0	30	57	0	0
					57	0	0	0	30	131	0	0
IPE 100	58	50	Vento X	PolG	0	0	0	0	46	57	0	0
					57	0	0	0	46	131	0	0
IPE 100	58	50	Vento X	PolG	0	0	0	0	35	68	0	0
					68	0	0	0	42	131	0	0
IPE 100	58	50	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	60	46	Peso Proprio	UnitG	0	0	0	0	8	132	0	0
IPE 100	60	46	QP Solai	PolG	0	0	0	0	92	16	0	0
					16	0	0	0	98	31	0	0
					31	0	0	0	106	106	0	0
					106	0	0	0	103	110	0	0
					110	0	0	0	101	132	0	0
IPE 100	60	46	QV Solai	PolG	0	0	0	0	29	16	0	0
					16	0	0	0	32	31	0	0
					106	0	0	0	34	106	0	0
					110	0	0	0	33	110	0	0
IPE 100	60	46	Neve	PolG	0	0	0	0	32	132	0	0
					16	0	0	0	30	16	0	0
					106	0	0	0	36	106	0	0
IPE 100	60	46	Neve	PolG	0	0	0	0	27	31	0	0
					31	0	0	0	35	110	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf		
IPE 100	60	46	Vento X	PolG	110	0	0	0	27	132	0	0	27	
					0	0	0	0	46	16	0	0	46	
					16	0	0	0	46	106	0	0	56	
IPE 100	60	46	Vento X	PolG	106	0	0	0	56	132	0	0	46	
					0	0	0	0	42	31	0	0	55	
					31	0	0	0	55	110	0	0	42	
IPE 100	60	46	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C									
	62	52			UnifG	0	0	0	0	8	131	0	0	8
	62	52			PolG	0	0	0	0	88	52	0	0	116
IPE 100	62	52	QP Solai		52	0	0	0	116	85	0	0	116	
					85	0	0	0	116	131	0	0	90	
	IPE 100	62	52	QV Solai	PolG	0	0	0	0	28	52	0	0	37
					52	0	0	0	37	85	0	0	37	
					85	0	0	0	37	131	0	0	29	
IPE 100	62	52	Neve	PolG	0	0	0	0	27	85	0	0	39	
					85	0	0	0	39	131	0	0	30	
	IPE 100	62	52	Neve	PolG	0	0	0	0	27	52	0	0	38
					52	0	0	0	38	131	0	0	26	
IPE 100		62	52	Vento X	PolG	0	0	0	0	42	85	0	0	61
					85	0	0	0	61	131	0	0	46	
	IPE 100	62	52	Vento X	PolG	0	0	0	0	42	52	0	0	58
					52	0	0	0	58	131	0	0	40	
IPE 100		62	52	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C								
	64	68	UnifG			0	0	0	0	8	131	0	0	8
	64	68	PolG			0	0	0	0	75	60	0	0	122
IPE 100	64	68	QP Solai		60	0	0	0	122	77	0	0	121	
					77	0	0	0	121	131	0	0	77	
	IPE 100	64	68	QV Solai	PolG	0	0	0	0	24	60	0	0	39
					60	0	0	0	39	77	0	0	39	
					77	0	0	0	39	131	0	0	25	
IPE 100	64	68	Neve	PolG	0	0	0	0	19	60	0	0	40	
					60	0	0	0	40	131	0	0	30	
	IPE 100	64	68	Neve	PolG	0	0	0	0	27	77	0	0	38
					77	0	0	0	38	131	0	0	18	
IPE 100		64	68	Vento X	PolG	0	0	0	0	42	77	0	0	59
					77	0	0	0	59	131	0	0	28	
	IPE 100	64	68	Vento X	PolG	0	0	0	0	29	60	0	0	62
					60	0	0	0	62	131	0	0	46	
IPE 100		64	68	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C								
	66	78	UnifG			0	0	0	0	8	131	0	0	8
	66	78	PolG			0	0	0	0	49	12	0	0	92
IPE 100	66	78	QP Solai		12	0	0	0	92	125	0	0	92	
					125	0	0	0	92	131	0	0	52	
	IPE 100	66	78	QV Solai	PolG	0	0	0	0	16	12	0	0	29
					12	0	0	0	29	125	0	0	29	
					125	0	0	0	29	131	0	0	17	
IPE 100	66	78	Neve	PolG	0	0	0	0	27	125	0	0	27	
					125	0	0	0	27	131	0	0	3	
	IPE 100	66	78	Neve	PolG	0	0	0	0	3	12	0	0	30
					12	0	0	0	30	131	0	0	30	
IPE 100		66	78	Vento X	PolG	0	0	0	0	42	125	0	0	42
					125	0	0	0	42	131	0	0	4	
	IPE 100	66	78	Vento X	PolG	0	0	0	0	4	12	0	0	46
					12	0	0	0	46	131	0	0	46	
IPE 100		66	78	Carichi termici	Termico	AXY=15°C,ΔXZ=15°C								
	70	34	UnifG			0	0	0	0	8	130	0	0	8
	70	34	PolG			0	0	0	0	93	124	0	0	92
IPE 100	70	34	QP Solai		124	0	0	0	92	130	0	0	46	
					PolG	0	0	0	30	124	0	0	29	
	IPE 100	70	34	QV Solai	PolG	0	0	0	0	29	130	0	0	15
					124	0	0	0	29	130	0	0	27	
IPE 100		70	34	Neve	PolG	0	0	0	0	28	130	0	0	30
					PolG	0	0	0	30	124	0	0	30	
	IPE 100	70	34	Neve	PolG	0	0	0	0	30	130	0	0	1
					124	0	0	0	46	124	0	0	46	
					124	0	0	0	46	130	0	0	1	

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf	
IPE 100	70	34	Vento X	PolG	0	0	0	0	44	130	0	0	42
IPE 100	70	34	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C								
IPE 100	72	66	Peso Proprio	UnifG	0	0	0	0	8	131	0	0	8
IPE 100	72	66	QP Solai	PolG	0	0	0	0	52	18	0	0	92
					18	0	0	0	92	119	0	0	92
					119	0	0	0	92	131	0	0	55
IPE 100	72	66	QV Solai	PolG	0	0	0	0	17	18	0	0	29
					18	0	0	0	29	119	0	0	29
IPE 100	72	66	Neve	PolG	0	0	0	0	29	131	0	0	18
					119	0	0	0	27	119	0	0	27
IPE 100	72	66	Neve	PolG	0	0	0	0	27	131	0	0	5
IPE 100	72	66	Neve	PolG	0	0	0	0	5	18	0	0	30
					18	0	0	0	30	131	0	0	30
IPE 100	72	66	Vento X	PolG	0	0	0	0	8	18	0	0	46
					18	0	0	0	46	131	0	0	46
IPE 100	72	66	Vento X	PolG	0	0	0	0	42	119	0	0	42
					119	0	0	0	42	131	0	0	7
IPE 100	72	66	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C								
IPE 100	74	76	Peso Proprio	UnifG	0	0	0	0	8	132	0	0	8
IPE 100	74	76	QP Solai	PolG	0	0	0	0	59	30	0	0	92
					30	0	0	0	92	107	0	0	92
					107	0	0	0	92	132	0	0	62
IPE 100	74	76	QV Solai	PolG	0	0	0	0	19	30	0	0	29
					30	0	0	0	29	107	0	0	29
					107	0	0	0	29	132	0	0	20
IPE 100	74	76	Neve	PolG	0	0	0	0	9	30	0	0	30
					30	0	0	0	30	132	0	0	30
IPE 100	74	76	Neve	PolG	0	0	0	0	27	107	0	0	27
					107	0	0	0	27	132	0	0	9
IPE 100	74	76	Vento X	PolG	0	0	0	0	42	107	0	0	42
					107	0	0	0	42	132	0	0	13
IPE 100	74	76	Vento X	PolG	0	0	0	0	14	30	0	0	46
					30	0	0	0	46	132	0	0	46
IPE 100	74	76	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C								
IPE 100	76	72	Peso Proprio	UnifG	0	0	0	0	8	132	0	0	8
IPE 100	76	72	QP Solai	PolG	0	0	0	0	56	24	0	0	92
					24	0	0	0	92	114	0	0	92
					114	0	0	0	92	132	0	0	58
IPE 100	76	72	QV Solai	PolG	0	0	0	0	18	24	0	0	29
					24	0	0	0	29	114	0	0	29
					114	0	0	0	29	132	0	0	19
IPE 100	76	72	Neve	PolG	0	0	0	0	27	114	0	0	27
					114	0	0	0	27	132	0	0	7
IPE 100	76	72	Neve	PolG	0	0	0	0	7	24	0	0	30
					24	0	0	0	30	132	0	0	30
IPE 100	76	72	Vento X	PolG	0	0	0	0	42	114	0	0	42
					114	0	0	0	42	132	0	0	10
IPE 100	76	72	Vento X	PolG	0	0	0	0	11	24	0	0	46
					24	0	0	0	46	132	0	0	46
IPE 100	76	72	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C								
IPE 100	78	70	Peso Proprio	UnifG	0	0	0	0	8	132	0	0	8
IPE 100	78	70	QP Solai	PolG	0	0	0	0	46	6	0	0	92
					6	0	0	0	92	132	0	0	93
IPE 100	78	70	QV Solai	PolG	0	0	0	0	15	6	0	0	29
					6	0	0	0	29	132	0	0	30
IPE 100	78	70	Neve	PolG	0	0	0	0	27	132	0	0	28
IPE 100	78	70	Neve	PolG	0	0	0	0	1	6	0	0	30
IPE 100	78	70	Vento X	PolG	0	0	0	0	30	132	0	0	30
					6	0	0	0	1	6	0	0	46
IPE 100	78	70	Vento X	PolG	0	0	0	0	46	132	0	0	46
					6	0	0	0	46	132	0	0	44
IPE 100	78	70	Carichi termici	Termico	ΔXY=15°C,ΔXZ=15°C								
Trave 8036													
IPE 100	0	395	Peso Proprio	UnifG	0	0	0	0	8	138	0	0	8
IPE 100	0	397	Peso Proprio	UnifG	0	0	0	0	8	138	0	0	8
IPE 100	0	397	QP Solai	PolG	0	0	0	0	53	24	0	0	86

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					24	0	0	0	86	120	0	0
					120	0	0	0	86	138	0	0
IPE 100	0	395	QP Solai	PolG	0	0	0	0	44	6	0	0
					6	0	0	0	86	138	0	0
IPE 100	0	395	QV Solai	PolG	0	0	0	0	14	6	0	0
					6	0	0	0	28	138	0	0
IPE 100	0	397	QV Solai	PolG	0	0	0	0	17	24	0	0
					24	0	0	0	28	120	0	0
IPE 100	0	397	Neve	PolG	0	0	0	0	26	120	0	0
					120	0	0	0	26	138	0	0
IPE 100	0	395	Neve	PolG	0	0	0	0	1	6	0	0
					6	0	0	0	27	138	0	0
IPE 100	0	395	Neve	PolG	0	0	0	0	26	138	0	0
IPE 100	0	397	Neve	PolG	0	0	0	0	7	24	0	0
					24	0	0	0	27	138	0	0
IPE 100	0	397	Vento X	PolG	0	0	0	0	11	24	0	0
					24	0	0	0	42	138	0	0
IPE 100	0	395	Vento X	PolG	0	0	0	0	41	138	0	0
IPE 100	0	397	Vento X	PolG	0	0	0	0	41	120	0	0
					120	0	0	0	41	138	0	0
IPE 100	0	395	Vento X	PolG	0	0	0	0	1	6	0	0
					6	0	0	0	42	138	0	0
IPE 100	0	395	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	397	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	353	367	Peso Proprio	UnifG	0	0	0	0	8	137	0	0
IPE 100	353	367	QP Solai	PolG	0	0	0	0	61	31	0	0
					31	0	0	0	86	100	0	0
					100	0	0	0	86	137	0	0
IPE 100	353	367	QV Solai	PolG	0	0	0	0	20	31	0	0
					31	0	0	0	28	100	0	0
					100	0	0	0	28	137	0	0
IPE 100	353	367	Neve	PolG	0	0	0	0	27	100	0	0
					100	0	0	0	27	137	0	0
IPE 100	353	367	Neve	PolG	0	0	0	0	11	31	0	0
					31	0	0	0	26	137	0	0
IPE 100	353	367	Vento X	PolG	0	0	0	0	42	100	0	0
					100	0	0	0	42	137	0	0
IPE 100	353	367	Vento X	PolG	0	0	0	0	16	31	0	0
					31	0	0	0	41	137	0	0
IPE 100	353	367	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	355	373	Peso Proprio	UnifG	0	0	0	0	8	137	0	0
IPE 100	355	373	QP Solai	PolG	0	0	0	0	72	52	0	0
					52	0	0	0	86	79	0	0
IPE 100	355	373	QV Solai	PolG	0	0	0	0	86	137	0	0
					79	0	0	0	23	52	0	0
					52	0	0	0	28	79	0	0
					79	0	0	0	28	137	0	0
IPE 100	355	373	Neve	PolG	0	0	0	0	27	79	0	0
					79	0	0	0	27	137	0	0
IPE 100	355	373	Neve	PolG	0	0	0	0	17	52	0	0
					52	0	0	0	26	137	0	0
IPE 100	355	373	Vento X	PolG	0	0	0	0	27	52	0	0
					52	0	0	0	41	137	0	0
IPE 100	355	373	Vento X	PolG	0	0	0	0	42	79	0	0
					79	0	0	0	42	137	0	0
IPE 100	355	373	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	357	363	Peso Proprio	UnifG	0	0	0	0	8	138	0	0
IPE 100	357	363	QP Solai	PolG	0	0	0	0	55	18	0	0
					18	0	0	0	86	113	0	0
					113	0	0	0	86	138	0	0
IPE 100	357	363	QV Solai	PolG	0	0	0	0	18	18	0	0
					18	0	0	0	28	113	0	0
					113	0	0	0	28	138	0	0
IPE 100	357	363	Neve	PolG	0	0	0	0	7	18	0	0
					18	0	0	0	26	138	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	357	363	Neve	PolG	0	0	0	0	27	113	0	0
					113	0	0	0	27	138	0	0
IPE 100	357	363	Vento X	PolG	0	0	0	0	42	113	0	0
					113	0	0	0	42	138	0	0
IPE 100	357	363	Vento X	PolG	0	0	0	0	10	18	0	0
					18	0	0	0	41	138	0	0
IPE 100	357	363	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	359	365	Peso Proprio	UnifG	0	0	0	0	8	140	0	0
IPE 100	359	365	QP Solai	PolG	0	0	0	0	49	6	0	0
					6	0	0	0	86	128	0	0
IPE 100	359	365	QV Solai	PolG	0	0	0	0	16	6	0	0
					128	0	0	0	28	128	0	0
IPE 100	359	365	Neve	PolG	0	0	0	0	28	140	0	0
					128	0	0	0	3	6	0	0
IPE 100	359	365	Neve	PolG	0	0	0	0	26	140	0	0
					128	0	0	0	27	128	0	0
IPE 100	359	365	Vento X	PolG	0	0	0	0	42	128	0	0
					128	0	0	0	42	140	0	0
IPE 100	359	365	Vento X	PolG	0	0	0	0	5	6	0	0
					6	0	0	0	41	140	0	0
IPE 100	359	365	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	361	379	Peso Proprio	UnifG	0	0	0	0	8	137	0	0
IPE 100	361	379	QP Solai	PolG	0	0	0	0	86	11	0	0
					11	0	0	0	92	43	0	0
					43	0	0	0	89	88	0	0
					88	0	0	0	88	132	0	0
IPE 100	361	379	QV Solai	PolG	0	0	0	0	89	137	0	0
					11	0	0	0	28	11	0	0
					88	0	0	0	29	88	0	0
IPE 100	361	379	Neve	PolG	0	0	0	0	28	137	0	0
					43	0	0	0	27	43	0	0
IPE 100	361	379	Neve	PolG	0	0	0	0	29	137	0	0
					132	0	0	0	26	11	0	0
IPE 100	361	379	Vento X	PolG	0	0	0	0	26	137	0	0
					88	0	0	0	42	43	0	0
IPE 100	361	379	Vento X	PolG	0	0	0	0	42	132	0	0
					43	0	0	0	45	137	0	0
IPE 100	361	379	Vento X	PolG	0	0	0	0	41	11	0	0
					11	0	0	0	46	88	0	0
IPE 100	361	379	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	363	379	Peso Proprio	UnifG	0	0	0	0	8	138	0	0
IPE 100	363	353	QP Solai	PolG	0	0	0	0	58	25	0	0
					25	0	0	0	86	107	0	0
					107	0	0	0	86	138	0	0
IPE 100	363	353	QV Solai	PolG	0	0	0	0	19	25	0	0
					25	0	0	0	28	107	0	0
					107	0	0	0	28	138	0	0
IPE 100	363	353	Neve	PolG	0	0	0	0	9	25	0	0
					25	0	0	0	26	138	0	0
IPE 100	363	353	Neve	PolG	0	0	0	0	27	107	0	0
					107	0	0	0	27	138	0	0
IPE 100	363	353	Vento X	PolG	0	0	0	0	13	25	0	0
					25	0	0	0	41	138	0	0
IPE 100	363	353	Vento X	PolG	0	0	0	0	42	107	0	0
					107	0	0	0	42	138	0	0
IPE 100	363	353	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	365	357	Peso Proprio	UnifG	0	0	0	0	8	136	0	0
IPE 100	365	357	QP Solai	PolG	0	0	0	0	52	12	0	0
					12	0	0	0	86	117	0	0
					117	0	0	0	86	136	0	0
IPE 100	365	357	QV Solai	PolG	0	0	0	0	17	12	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					12	0	0	28	117	0	0	28
					117	0	0	28	136	0	0	16
IPE 100	365	357	Neve	PolG	0	0	0	27	117	0	0	27
					117	0	0	27	136	0	0	5
IPE 100	365	357	Neve	PolG	0	0	0	5	12	0	0	26
					12	0	0	26	136	0	0	26
IPE 100	365	357	Vento X	PolG	0	0	0	42	117	0	0	42
					117	0	0	42	136	0	0	8
IPE 100	365	357	Vento X	PolG	0	0	0	7	12	0	0	41
					12	0	0	41	136	0	0	41
IPE 100	365	357	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	367	369	Peso Proprio	UnitG	0	0	0	8	138	0	0	8
IPE 100	367	369	QP Solai	PolG	0	0	0	65	38	0	0	86
					38	0	0	86	93	0	0	86
IPE 100	367	369	QV Solai	PolG	93	0	0	86	138	0	0	63
					0	0	0	21	38	0	0	28
					38	0	0	28	93	0	0	28
IPE 100	367	369	Neve	PolG	0	0	0	13	38	0	0	26
					38	0	0	26	138	0	0	26
IPE 100	367	369	Neve	PolG	0	0	0	27	93	0	0	27
					93	0	0	27	138	0	0	13
IPE 100	367	369	Vento X	PolG	0	0	0	42	93	0	0	42
					93	0	0	42	138	0	0	20
IPE 100	367	369	Vento X	PolG	0	0	0	20	38	0	0	41
					38	0	0	41	138	0	0	41
IPE 100	367	369	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	369	355	Peso Proprio	UnitG	0	0	0	8	137	0	0	8
IPE 100	369	355	QP Solai	PolG	0	0	0	68	45	0	0	86
					45	0	0	86	86	0	0	86
IPE 100	369	355	QV Solai	PolG	86	0	0	86	137	0	0	67
					0	0	0	22	45	0	0	28
					45	0	0	28	86	0	0	28
IPE 100	369	355	Neve	PolG	86	0	0	28	137	0	0	21
					0	0	0	26	137	0	0	26
IPE 100	369	355	Neve	PolG	45	0	0	27	86	0	0	27
					86	0	0	27	137	0	0	15
IPE 100	369	355	Vento X	PolG	0	0	0	42	86	0	0	42
					86	0	0	42	137	0	0	24
IPE 100	369	355	Vento X	PolG	0	0	0	23	45	0	0	41
					45	0	0	41	137	0	0	41
IPE 100	369	355	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	371	387	Peso Proprio	UnitG	0	0	0	8	137	0	0	8
IPE 100	371	387	QP Solai	PolG	0	0	0	86	8	0	0	89
					8	0	0	89	48	0	0	109
					48	0	0	109	95	0	0	107
					95	0	0	107	123	0	0	91
IPE 100	371	387	QV Solai	PolG	123	0	0	91	137	0	0	86
					0	0	0	28	8	0	0	29
					8	0	0	29	48	0	0	35
					48	0	0	35	95	0	0	34
					95	0	0	34	123	0	0	29
					123	0	0	29	137	0	0	28
IPE 100	371	387	Neve	PolG	0	0	0	26	48	0	0	36
					48	0	0	36	123	0	0	26
					123	0	0	26	137	0	0	26
IPE 100	371	387	Neve	PolG	0	0	0	27	8	0	0	27
					8	0	0	27	95	0	0	36
					95	0	0	36	137	0	0	27
IPE 100	371	387	Vento X	PolG	0	0	0	41	48	0	0	56
					48	0	0	56	123	0	0	41
					123	0	0	41	137	0	0	41
IPE 100	371	387	Vento X	PolG	0	0	0	42	8	0	0	42
					8	0	0	42	95	0	0	56
					95	0	0	56	137	0	0	42

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	371	387	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	373	383	Peso Proprio	UnitG	0	0	0	8	138	0	0	8
IPE 100	373	383	QP Solai	PolG	0	0	0	76	60	0	0	86
					60	0	0	86	71	0	0	86
					71	0	0	86	138	0	0	75
IPE 100	373	383	QV Solai	PolG	0	0	0	24	60	0	0	28
					60	0	0	28	71	0	0	28
					71	0	0	28	138	0	0	24
IPE 100	373	383	Neve	PolG	0	0	0	20	60	0	0	26
					60	0	0	26	138	0	0	26
IPE 100	373	383	Neve	PolG	0	0	0	27	71	0	0	27
					71	0	0	27	138	0	0	20
IPE 100	373	383	Vento X	PolG	0	0	0	31	60	0	0	41
					60	0	0	41	138	0	0	41
IPE 100	373	383	Vento X	PolG	0	0	0	42	71	0	0	42
					71	0	0	42	138	0	0	31
IPE 100	373	383	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	375	361	Peso Proprio	UnitG	0	0	0	8	138	0	0	8
IPE 100	375	361	QP Solai	PolG	0	0	0	85	54	0	0	86
					54	0	0	86	138	0	0	84
IPE 100	375	361	QV Solai	PolG	0	0	0	27	138	0	0	27
					27	0	0	26	138	0	0	26
IPE 100	375	361	Neve	PolG	0	0	0	27	54	0	0	27
					54	0	0	27	138	0	0	26
IPE 100	375	361	Vento X	PolG	0	0	0	42	54	0	0	42
					54	0	0	42	138	0	0	40
IPE 100	375	361	Vento X	PolG	0	0	0	40	138	0	0	41
IPE 100	375	361	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	377	381	Peso Proprio	UnitG	0	0	0	8	138	0	0	8
IPE 100	377	381	QP Solai	PolG	0	0	0	80	68	0	0	119
					68	0	0	119	76	0	0	118
					76	0	0	118	138	0	0	81
IPE 100	377	381	QV Solai	PolG	0	0	0	26	68	0	0	38
					68	0	0	38	138	0	0	26
IPE 100	377	381	Neve	PolG	0	0	0	23	76	0	0	38
					76	0	0	38	138	0	0	27
IPE 100	377	381	Neve	PolG	0	0	0	26	68	0	0	38
					68	0	0	38	138	0	0	23
IPE 100	377	381	Vento X	PolG	0	0	0	41	68	0	0	58
					68	0	0	58	138	0	0	36
IPE 100	377	381	Vento X	PolG	0	0	0	36	76	0	0	59
					76	0	0	59	138	0	0	42
IPE 100	377	381	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	379	385	Peso Proprio	UnitG	0	0	0	8	137	0	0	8
IPE 100	379	385	QP Solai	PolG	0	0	0	86	25	0	0	97
					25	0	0	97	34	0	0	96
					34	0	0	96	98	0	0	92
					98	0	0	92	118	0	0	94
IPE 100	379	385	QV Solai	PolG	118	0	0	94	137	0	0	86
					0	0	0	28	25	0	0	31
					25	0	0	31	34	0	0	31
					34	0	0	31	98	0	0	30
					98	0	0	30	118	0	0	30
IPE 100	379	385	Neve	PolG	0	0	0	30	137	0	0	28
					0	0	0	27	34	0	0	27
					34	0	0	27	118	0	0	32
					118	0	0	32	137	0	0	27
IPE 100	379	385	Neve	PolG	0	0	0	26	25	0	0	33
					25	0	0	33	98	0	0	26
IPE 100	379	385	Vento X	PolG	98	0	0	26	137	0	0	26
					0	0	0	40	25	0	0	51
					25	0	0	51	98	0	0	41
					98	0	0	41	137	0	0	41
IPE 100	379	385	Vento X	PolG	0	0	0	42	34	0	0	42
					34	0	0	42	118	0	0	50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	379	385			118	0	0	0	50	137	0	42
IPE 100	381	389	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	381	389	Peso Proprio	UnitG	0	0	0	0	8	137	0	8
IPE 100	381	389	QP Solai	PolG	0	0	0	0	75	68	0	119
					68	0	0	0	119	76	0	119
					76	0	0	0	119	137	0	77
IPE 100	381	389	QV Solai	PolG	0	0	0	0	24	68	0	38
					68	0	0	0	38	76	0	38
IPE 100	381	389	Neve	PolG	76	0	0	0	38	137	0	25
IPE 100	381	389	Neve	PolG	68	0	0	0	38	137	0	27
IPE 100	381	389	Neve	PolG	0	0	0	0	26	76	0	37
IPE 100	381	389	Vento X	PolG	76	0	0	0	37	137	0	20
IPE 100	381	389	Vento X	PolG	76	0	0	0	41	76	0	58
IPE 100	381	389	Vento X	PolG	76	0	0	0	58	137	0	32
IPE 100	381	389	Vento X	PolG	68	0	0	0	32	68	0	59
IPE 100	381	389	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	383	375	Peso Proprio	UnitG	0	0	0	0	8	137	0	8
IPE 100	383	375	QP Solai	PolG	0	0	0	0	80	63	0	86
					63	0	0	0	86	68	0	86
IPE 100	383	375	QV Solai	PolG	68	0	0	0	86	137	0	78
					63	0	0	0	26	63	0	27
IPE 100	383	375	Neve	PolG	63	0	0	0	27	68	0	27
IPE 100	383	375	Neve	PolG	0	0	0	0	27	137	0	25
IPE 100	383	375	Neve	PolG	63	0	0	0	27	63	0	27
IPE 100	383	375	Neve	PolG	0	0	0	0	22	68	0	26
IPE 100	383	375	Vento X	PolG	68	0	0	0	26	137	0	26
IPE 100	383	375	Vento X	PolG	63	0	0	0	42	63	0	42
IPE 100	383	375	Vento X	PolG	63	0	0	0	42	137	0	35
IPE 100	383	375	Vento X	PolG	68	0	0	0	35	68	0	41
IPE 100	383	375	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	385	371	Peso Proprio	UnitG	0	0	0	0	8	138	0	8
IPE 100	385	371	QP Solai	PolG	0	0	0	0	86	22	0	95
					22	0	0	0	95	37	0	103
					37	0	0	0	103	106	0	99
IPE 100	385	371	QV Solai	PolG	106	0	0	0	99	110	0	86
					110	0	0	0	97	138	0	28
IPE 100	385	371	Neve	PolG	0	0	0	0	28	22	0	30
					22	0	0	0	30	37	0	33
					37	0	0	0	33	106	0	32
IPE 100	385	371	Neve	PolG	106	0	0	0	32	110	0	31
IPE 100	385	371	Neve	PolG	110	0	0	0	31	138	0	28
IPE 100	385	371	Neve	PolG	0	0	0	0	27	22	0	27
IPE 100	385	371	Neve	PolG	22	0	0	0	35	138	0	35
IPE 100	385	371	Neve	PolG	106	0	0	0	26	37	0	35
IPE 100	385	371	Vento X	PolG	37	0	0	0	35	110	0	26
IPE 100	385	371	Vento X	PolG	110	0	0	0	26	138	0	26
IPE 100	385	371	Vento X	PolG	22	0	0	0	42	22	0	42
IPE 100	385	371	Vento X	PolG	22	0	0	0	42	106	0	54
IPE 100	385	371	Vento X	PolG	106	0	0	0	54	138	0	42
IPE 100	385	371	Vento X	PolG	37	0	0	0	41	37	0	54
IPE 100	385	371	Vento X	PolG	37	0	0	0	54	110	0	40
IPE 100	385	371	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	387	377	Peso Proprio	UnitG	0	0	0	0	8	137	0	8
IPE 100	387	377	QP Solai	PolG	0	0	0	0	84	58	0	114
					58	0	0	0	114	85	0	114
IPE 100	387	377	QV Solai	PolG	85	0	0	0	114	137	0	86
					0	0	0	0	27	58	0	37
IPE 100	387	377	Neve	PolG	58	0	0	0	37	85	0	36
IPE 100	387	377	Neve	PolG	0	0	0	0	36	137	0	27

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	387	377	Neve	PolG	58	0	0	0	37	137	0	26
IPE 100	387	377	Vento X	PolG	85	0	0	0	37	137	0	37
IPE 100	387	377	Vento X	PolG	85	0	0	0	40	85	0	58
IPE 100	387	377	Vento X	PolG	85	0	0	0	58	137	0	42
IPE 100	387	377	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	389	393	Peso Proprio	UnitG	0	0	0	0	8	137	0	8
IPE 100	389	393	QP Solai	PolG	60	0	0	0	71	60	0	115
					83	0	0	0	115	137	0	73
IPE 100	389	393	QV Solai	PolG	0	0	0	0	23	60	0	37
					60	0	0	0	37	83	0	37
IPE 100	389	393	Neve	PolG	83	0	0	0	37	137	0	23
IPE 100	389	393	Neve	PolG	83	0	0	0	26	83	0	37
IPE 100	389	393	Neve	PolG	0	0	0	0	18	60	0	38
IPE 100	389	393	Vento X	PolG	60	0	0	0	38	137	0	27
IPE 100	389	393	Vento X	PolG	83	0	0	0	41	83	0	57
IPE 100	389	393	Vento X	PolG	83	0	0	0	57	137	0	28
IPE 100	389	393	Vento X	PolG	60	0	0	0	28	60	0	58
IPE 100	389	393	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	391	0	Peso Proprio	UnitG	0	0	0	0	8	137	0	8
IPE 100	391	0	QP Solai	PolG	0	0	0	0	47	12	0	86
					12	0	0	0	86	131	0	86
IPE 100	391	0	QV Solai	PolG	131	0	0	0	86	137	0	48
					12	0	0	0	15	12	0	28
IPE 100	391	0	Neve	PolG	131	0	0	0	28	131	0	28
IPE 100	391	0	Neve	PolG	131	0	0	0	28	137	0	16
IPE 100	391	0	Neve	PolG	12	0	0	0	3	12	0	27
IPE 100	391	0	Neve	PolG	12	0	0	0	27	137	0	27
IPE 100	391	0	Vento X	PolG	131	0	0	0	26	137	0	26
IPE 100	391	0	Vento X	PolG	131	0	0	0	41	131	0	41
IPE 100	391	0	Vento X	PolG	131	0	0	0	41	137	0	4
IPE 100	391	0	Vento X	PolG	0	0	0	0	4	12	0	42
IPE 100	391	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	395	359	Peso Proprio	UnitG	0	0	0	0	8	136	0	8
IPE 100	395	359	QP Solai	PolG	0	0	0	0	88	130	0	86
IPE 100	395	359	QV Solai	PolG	130	0	0	0	86	136	0	44
IPE 100	395	359	Neve	PolG	130	0	0	0	28	130	0	28
IPE 100	395	359	Neve	PolG	130	0	0	0	28	136	0	14
IPE 100	395	359	Neve	PolG	130	0	0	0	27	130	0	27
IPE 100	395	359	Neve	PolG	130	0	0	0	27	136	0	1
IPE 100	395	359	Neve	PolG	0	0	0	0	27	136	0	26
IPE 100	395	359	Vento X	PolG	0	0	0	0	42	130	0	42
IPE 100	395	359	Vento X	PolG	130	0	0	0	42	136	0	1
IPE 100	395	359	Vento X	PolG	0	0	0	0	42	136	0	41
IPE 100	395	359	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	397	391	Peso Proprio	UnitG	0	0	0	0	8	137	0	8
IPE 100	397	391	QP Solai	PolG	0	0	0	0	50	18	0	86
IPE 100	397	391	QP Solai	PolG	18	0	0	0	86	125	0	86
IPE 100	397	391	QP Solai	PolG	125	0	0	0	86	137	0	51
IPE 100	397	391	QV Solai	PolG	0	0	0	0	16	18	0	28
					18	0	0	0	28	125	0	28
IPE 100	397	391	Neve	PolG	125	0	0	0	28	137	0	17
IPE 100	397	391	Neve	PolG	0	0	0	0	5	18	0	27
IPE 100	397	391	Neve	PolG	18	0	0	0	27	137	0	27
IPE 100	397	391	Neve	PolG	0	0	0	0	26	125	0	26
IPE 100	397	391	Vento X	PolG	125	0	0	0	26	137	0	5
IPE 100	397	391	Vento X	PolG	0	0	0	0	7	18	0	42
IPE 100	397	391	Vento X	PolG	18	0	0	0	42	137	0	42

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	397	391			125	0	0	0	41	137	0	7
IPE 100	399	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	399	0	Peso Proprio	UnitG	0	0	0	0	8	138	0	8
IPE 100	399	0	QP Solai	PolG	0	0	0	0	56	30	0	86
					30	0	0	0	86	113	0	86
IPE 100	399	0			113	0	0	0	86	138	0	58
IPE 100	399	0	QV Solai	PolG	0	0	0	0	18	30	0	28
					30	0	0	0	28	113	0	28
IPE 100	399	0	Neve	PolG	113	0	0	0	28	138	0	19
					0	0	0	9	30	0	0	27
IPE 100	399	0	Neve	PolG	30	0	0	0	27	138	0	27
					0	0	0	26	113	0	0	26
IPE 100	399	0	Vento X	PolG	113	0	0	0	26	138	0	9
					0	0	0	41	113	0	0	41
IPE 100	399	0	Vento X	PolG	113	0	0	0	41	138	0	13
					0	0	0	14	30	0	0	42
IPE 100	399	0	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	399	0			30	0	0	0	42	138	0	42
Trave 8037												
IPE 100	0	396	Peso Proprio	UnitG	0	0	0	0	8	144	0	8
IPE 100	0	398	Peso Proprio	UnitG	0	0	0	0	8	144	0	8
IPE 100	0	396	QP Solai	PolG	0	0	0	0	45	6	0	86
IPE 100	0	398			6	0	0	0	86	144	0	87
IPE 100	0	398	QP Solai	PolG	0	0	0	0	55	24	0	86
					24	0	0	0	86	126	0	86
IPE 100	0	398			126	0	0	0	86	144	0	54
IPE 100	0	398	QV Solai	PolG	0	0	0	0	18	24	0	28
					24	0	0	0	28	126	0	28
IPE 100	0	396	QV Solai	PolG	126	0	0	0	28	144	0	17
					0	0	0	15	6	0	0	28
IPE 100	0	398	Neve	PolG	6	0	0	0	28	144	0	28
IPE 100	0	396	Neve	PolG	24	0	0	0	26	144	0	26
IPE 100	0	398	Neve	PolG	0	0	0	0	27	144	0	28
IPE 100	0	398	Neve	PolG	126	0	0	0	27	126	0	27
IPE 100	0	396	Neve	PolG	0	0	0	0	27	144	0	7
IPE 100	0	396	Vento X	PolG	6	0	0	0	26	144	0	26
IPE 100	0	398	Vento X	PolG	0	0	0	0	42	126	0	44
IPE 100	0	398	Vento X	PolG	126	0	0	0	42	144	0	11
IPE 100	0	396	Vento X	PolG	0	0	0	0	1	6	0	41
IPE 100	0	398	Vento X	PolG	6	0	0	0	41	144	0	41
IPE 100	0	398	Vento X	PolG	0	0	0	0	11	24	0	41
IPE 100	0	398	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	0	398			24	0	0	0	41	144	0	41
IPE 100	0	396	Peso Proprio	UnitG	0	0	0	0	8	143	0	8
IPE 100	354	368	QP Solai	PolG	0	0	0	0	61	31	0	86
IPE 100	354	368			31	0	0	0	86	106	0	86
IPE 100	354	368			106	0	0	0	86	143	0	61
IPE 100	354	368	QV Solai	PolG	0	0	0	0	19	31	0	28
					31	0	0	0	28	106	0	28
IPE 100	354	368	Neve	PolG	106	0	0	0	28	143	0	20
					0	0	0	12	31	0	0	27
IPE 100	354	368	Neve	PolG	31	0	0	0	27	143	0	27
IPE 100	354	368	Vento X	PolG	0	0	0	0	26	106	0	26
IPE 100	354	368	Vento X	PolG	106	0	0	0	26	143	0	11
IPE 100	354	368	Vento X	PolG	31	0	0	0	42	143	0	42
IPE 100	354	368	Vento X	PolG	0	0	0	0	41	106	0	41
IPE 100	354	368	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	356	374	Peso Proprio	UnitG	0	0	0	0	8	143	0	8
IPE 100	356	374	QP Solai	PolG	0	0	0	0	72	52	0	86
IPE 100	362	380	Vento X	PolG	52	0	0	0	86	85	0	86

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	356	374			85	0	0	0	86	143	0	72
IPE 100	356	374	QV Solai	PolG	0	0	0	0	23	52	0	28
					52	0	0	0	28	85	0	28
IPE 100	356	374	Neve	PolG	0	0	0	0	19	52	0	27
					52	0	0	0	27	143	0	27
IPE 100	356	374	Neve	PolG	0	0	0	0	26	85	0	26
					85	0	0	0	26	143	0	18
IPE 100	356	374	Vento X	PolG	0	0	0	0	41	85	0	41
					85	0	0	0	41	143	0	27
IPE 100	356	374	Vento X	PolG	0	0	0	0	29	52	0	42
					52	0	0	0	42	143	0	42
IPE 100	356	374	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	358	364	Peso Proprio	UnitG	0	0	0	0	8	144	0	8
IPE 100	358	364	QP Solai	PolG	0	0	0	0	54	18	0	86
IPE 100	358	364			18	0	0	0	86	119	0	86
IPE 100	358	364	QV Solai	PolG	119	0	0	0	86	144	0	55
					0	0	0	0	17	18	0	28
IPE 100	358	364	Neve	PolG	119	0	0	0	28	119	0	28
					0	0	0	7	18	0	0	27
IPE 100	358	364	Neve	PolG	18	0	0	0	27	144	0	27
					0	0	0	26	119	0	0	26
IPE 100	358	364	Vento X	PolG	119	0	0	0	26	144	0	7
					0	0	0	41	119	0	0	41
IPE 100	358	364	Vento X	PolG	119	0	0	0	41	144	0	11
					0	0	0	11	18	0	0	42
IPE 100	358	364	Vento X	PolG	18	0	0	0	42	144	0	42
					AXY=15°C,AXZ=15°C							
IPE 100	358	364	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	360	366	Peso Proprio	UnitG	0	0	0	0	8	146	0	8
IPE 100	360	366	QP Solai	PolG	0	0	0	0	47	6	0	86
					6	0	0	0	86	134	0	86
IPE 100	360	366			134	0	0	0	86	146	0	49
IPE 100	360	366	QV Solai	PolG	0	0	0	0	15	6	0	28
					6	0	0	0	28	134	0	28
IPE 100	360	366	Neve	PolG	134	0	0	0	28	146	0	16
					0	0	0	26	134	0	0	26
IPE 100	360	366	Neve	PolG	134	0	0	0	26	146	0	3
					0	0	0	3	6	0	0	27
IPE 100	360	366	Vento X	PolG	6	0	0	0	27	146	0	27
					6	0	0	5	6	0	0	42
IPE 100	360	366	Vento X	PolG	6	0	0	0	42	146	0	42
					0	0	0	41	134	0	0	41
IPE 100	360	366	Vento X	PolG	134	0	0	0	41	146	0	5
					AXY=15°C,AXZ=15°C							
IPE 100	360	366	Carichi termici	Termico	AXY=15°C,AXZ=15°C							
IPE 100	362	380	Peso Proprio	UnitG	0	0	0	0	8	143	0	8
IPE 100	362	380	QP Solai	PolG	0	0	0	0	86	18	0	95
					18	0	0	0	95	49	0	91
					49	0	0	0	91	88	0	88
					88	0	0	0	88	132	0	91
IPE 100	362	380	QV Solai	PolG	132	0	0	0	91	143	0	86
					0	0	0	28	18	0	0	30
					18	0	0	0	30	49	0	29
					49	0	0	0	29	88	0	28
					88	0	0	0	28	132	0	29
IPE 100	362	380	Neve	PolG	132	0	0	0	29	143	0	28
					0	0	0	26	49	0	0	26
					49	0	0	0	26	132	0	29
IPE 100	362	380	Neve	PolG	132	0	0	0	29	143	0	26
					0	0	0	27	18	0	0	33
IPE 100	362	380	Vento X	PolG	18	0	0	0	33	88	0	27
					88	0	0	0	27	143	0	27
IPE 100	362	380	Vento X	PolG	0	0	0	0	42	18	0	51
					18	0	0	0	51	88	0	42
IPE 100	362	380	Vento X	PolG	88	0	0	0	42	143	0	42
					0	0	0	41	49	0	0	41

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					49	0	0	0	41	132	0	0
					132	0	0	0	45	143	0	0
					AXY=15°C,AXZ=15°C							
IPE 100	362	380	Carichi termici	Termico	0	0	0	0	8	144	0	0
IPE 100	364	354	Peso Proprio	UnitG	0	0	0	0	57	25	0	0
IPE 100	364	354	QP Solai	PolG	25	0	0	0	86	113	0	0
					113	0	0	0	86	144	0	0
IPE 100	364	354	QV Solai	PolG	0	0	0	0	18	25	0	0
					25	0	0	0	28	113	0	0
					113	0	0	0	28	144	0	0
IPE 100	364	354	Neve	PolG	0	0	0	0	9	25	0	0
					25	0	0	0	27	144	0	0
IPE 100	364	354	Neve	PolG	0	0	0	0	26	113	0	0
					113	0	0	0	26	144	0	0
IPE 100	364	354	Vento X	PolG	0	0	0	0	14	25	0	0
					25	0	0	0	42	144	0	0
IPE 100	364	354	Vento X	PolG	0	0	0	0	41	113	0	0
					113	0	0	0	41	144	0	0
					AXY=15°C,AXZ=15°C							
IPE 100	364	354	Carichi termici	Termico	0	0	0	0	8	142	0	0
IPE 100	366	358	Peso Proprio	UnitG	0	0	0	0	50	12	0	0
IPE 100	366	358	QP Solai	PolG	12	0	0	0	86	123	0	0
					123	0	0	0	86	142	0	0
IPE 100	366	358	QV Solai	PolG	12	0	0	0	16	12	0	0
					12	0	0	0	28	123	0	0
IPE 100	366	358	Neve	PolG	123	0	0	0	28	142	0	0
					123	0	0	0	26	123	0	0
IPE 100	366	358	Neve	PolG	0	0	0	0	5	12	0	0
					12	0	0	0	27	142	0	0
IPE 100	366	358	Vento X	PolG	0	0	0	0	41	123	0	0
					123	0	0	0	41	142	0	0
IPE 100	366	358	Vento X	PolG	0	0	0	0	8	12	0	0
					12	0	0	0	42	142	0	0
					AXY=15°C,AXZ=15°C							
IPE 100	366	358	Carichi termici	Termico	0	0	0	0	8	144	0	0
IPE 100	368	370	Peso Proprio	UnitG	0	0	0	0	64	38	0	0
IPE 100	368	370	QP Solai	PolG	38	0	0	0	86	100	0	0
					100	0	0	0	86	144	0	0
IPE 100	368	370	QV Solai	PolG	0	0	0	0	21	38	0	0
					38	0	0	0	28	100	0	0
IPE 100	368	370	Neve	PolG	100	0	0	0	28	144	0	0
					0	0	0	0	14	38	0	0
IPE 100	368	370	Neve	PolG	38	0	0	0	27	144	0	0
					100	0	0	0	26	100	0	0
IPE 100	368	370	Vento X	PolG	100	0	0	0	26	144	0	0
					0	0	0	0	41	100	0	0
IPE 100	368	370	Vento X	PolG	100	0	0	0	41	144	0	0
					0	0	0	0	21	38	0	0
IPE 100	368	370	Vento X	PolG	38	0	0	0	42	144	0	0
					AXY=15°C,AXZ=15°C							
IPE 100	368	370	Carichi termici	Termico	0	0	0	0	8	143	0	0
IPE 100	370	356	Peso Proprio	UnitG	0	0	0	0	68	45	0	0
IPE 100	370	356	QP Solai	PolG	45	0	0	0	86	92	0	0
					92	0	0	0	86	143	0	0
IPE 100	370	356	QV Solai	PolG	0	0	0	0	22	45	0	0
					45	0	0	0	28	92	0	0
IPE 100	370	356	Neve	PolG	92	0	0	0	28	143	0	0
					0	0	0	0	26	92	0	0
IPE 100	370	356	Neve	PolG	92	0	0	0	26	143	0	0
					0	0	0	0	16	45	0	0
IPE 100	370	356	Vento X	PolG	45	0	0	0	27	143	0	0
					0	0	0	0	25	45	0	0
IPE 100	370	356	Vento X	PolG	45	0	0	0	42	143	0	0
					92	0	0	0	41	92	0	0
					92	0	0	0	41	143	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	370	356	Carichi termici	Termico	0	0	0	0	8	143	0	0
IPE 100	372	388	Peso Proprio	UnitG	0	0	0	0	86	14	0	0
IPE 100	372	388	QP Solai	PolG	14	0	0	0	91	53	0	0
					53	0	0	0	113	95	0	0
					95	0	0	0	109	123	0	0
IPE 100	372	388	QV Solai	PolG	123	0	0	0	92	143	0	0
					14	0	0	0	28	14	0	0
					53	0	0	0	36	95	0	0
					95	0	0	0	35	123	0	0
IPE 100	372	388	Neve	PolG	123	0	0	0	30	143	0	0
					0	0	0	0	26	14	0	0
IPE 100	372	388	Neve	PolG	14	0	0	0	26	95	0	0
					95	0	0	0	36	143	0	0
IPE 100	372	388	Neve	PolG	0	0	0	0	27	53	0	0
					53	0	0	0	39	123	0	0
IPE 100	372	388	Vento X	PolG	123	0	0	0	27	143	0	0
					53	0	0	0	42	53	0	0
IPE 100	372	388	Vento X	PolG	123	0	0	0	42	143	0	0
					0	0	0	0	41	14	0	0
					14	0	0	0	41	95	0	0
					95	0	0	0	55	143	0	0
					AXY=15°C,AXZ=15°C							
IPE 100	372	388	Carichi termici	Termico	0	0	0	0	8	144	0	0
IPE 100	374	384	Peso Proprio	UnitG	0	0	0	0	77	60	0	0
IPE 100	374	384	QP Solai	PolG	60	0	0	0	86	77	0	0
					77	0	0	0	86	144	0	0
IPE 100	374	384	QV Solai	PolG	0	0	0	0	25	60	0	0
					60	0	0	0	28	77	0	0
IPE 100	374	384	Neve	PolG	77	0	0	0	28	144	0	0
					0	0	0	0	26	77	0	0
IPE 100	374	384	Neve	PolG	77	0	0	0	26	144	0	0
					60	0	0	0	27	144	0	0
IPE 100	374	384	Vento X	PolG	0	0	0	0	41	77	0	0
					77	0	0	0	41	144	0	0
IPE 100	374	384	Vento X	PolG	0	0	0	0	34	60	0	0
					60	0	0	0	42	144	0	0
					AXY=15°C,AXZ=15°C							
IPE 100	374	384	Carichi termici	Termico	0	0	0	0	8	144	0	0
IPE 100	376	362	Peso Proprio	UnitG	0	0	0	0	86	3	0	0
IPE 100	376	362	QP Solai	PolG	3	0	0	0	88	78	0	0
					78	0	0	0	85	144	0	0
IPE 100	376	362	QV Solai	PolG	0	0	0	0	28	144	0	0
					0	0	0	0	27	144	0	0
IPE 100	376	362	Neve	PolG	0	0	0	0	26	144	0	0
IPE 100	376	362	Neve	PolG	0	0	0	0	42	3	0	0
IPE 100	376	362	Vento X	PolG	3	0	0	0	44	78	0	0
					78	0	0	0	42	144	0	0
IPE 100	376	362	Vento X	PolG	0	0	0	0	41	144	0	0
					AXY=15°C,AXZ=15°C							
IPE 100	376	362	Carichi termici	Termico	0	0	0	0	8	144	0	0
IPE 100	376	362	Peso Proprio	UnitG	0	0	0	0	86	3	0	0
IPE 100	378	382	QP Solai	PolG	0	0	0	0	81	74	0	0
					74	0	0	0	123	76	0	0
					76	0	0	0	123	144	0	0
IPE 100	378	382	QV Solai	PolG	0	0	0	0	26	74	0	0
					74	0	0	0	40	76	0	0
IPE 100	378	382	Neve	PolG	76	0	0	0	39	144	0	0
					0	0	0	0	27	74	0	0
IPE 100	378	382	Neve	PolG	74	0	0	0	40	144	0	0
					0	0	0	0	23	76	0	0
IPE 100	378	382	Vento X	PolG	76	0	0	0	37	144	0	0
					76	0	0	0	36	76	0	0
					76	0	0	0	57	144	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	378	382	Vento X	PolG	74	0	0	0	42	74	0	62
IPE 100	378	382	Carichi termici	Termico	0	0	0	0	8	143	0	8
IPE 100	380	386	Peso Proprio	UnifG	0	0	0	0	86	31	0	100
IPE 100	380	386	QP Solai	PolG	31	0	0	0	100	39	0	98
					39	0	0	0	98	98	0	93
					98	0	0	0	93	118	0	96
IPE 100	380	386	QV Solai	PolG	118	0	0	0	96	143	0	86
					0	0	0	0	28	31	0	32
					31	0	0	0	32	39	0	31
					39	0	0	0	31	98	0	30
					98	0	0	0	30	118	0	31
IPE 100	380	386	Neve	PolG	118	0	0	0	31	143	0	28
					0	0	0	0	26	39	0	26
IPE 100	380	386	Neve	PolG	39	0	0	0	26	118	0	33
					118	0	0	0	33	143	0	26
					0	0	0	0	27	31	0	36
IPE 100	380	386	Vento X	PolG	31	0	0	0	36	98	0	27
					98	0	0	0	27	143	0	27
IPE 100	380	386	Vento X	PolG	0	0	0	0	42	31	0	55
					31	0	0	0	55	98	0	42
IPE 100	380	386	Vento X	PolG	98	0	0	0	42	143	0	42
					39	0	0	0	40	39	0	40
IPE 100	380	386	Vento X	PolG	118	0	0	0	40	118	0	50
					0	0	0	0	50	143	0	41
IPE 100	380	386	Carichi termici	Termico	0	0	0	0	8	143	0	8
IPE 100	382	390	Peso Proprio	UnifG	0	0	0	0	77	68	0	120
IPE 100	382	390	QP Solai	PolG	68	0	0	0	120	82	0	78
					82	0	0	0	120	143	0	78
IPE 100	382	390	QV Solai	PolG	0	0	0	0	25	68	0	39
					68	0	0	0	39	82	0	39
IPE 100	382	390	Neve	PolG	82	0	0	0	39	143	0	25
					68	0	0	0	37	143	0	37
IPE 100	382	390	Neve	PolG	0	0	0	0	27	82	0	40
IPE 100	382	390	Vento X	PolG	82	0	0	0	40	143	0	22
IPE 100	382	390	Vento X	PolG	0	0	0	0	42	82	0	62
IPE 100	382	390	Vento X	PolG	82	0	0	0	62	143	0	34
					0	0	0	0	32	68	0	57
IPE 100	382	390	Carichi termici	Termico	68	0	0	0	57	143	0	41
IPE 100	384	376	Peso Proprio	UnifG	0	0	0	0	8	143	0	8
IPE 100	384	376	QP Solai	PolG	69	0	0	0	81	69	0	86
IPE 100	384	376	QV Solai	PolG	0	0	0	0	86	143	0	80
IPE 100	384	376	Neve	PolG	69	0	0	0	26	69	0	28
IPE 100	384	376	Neve	PolG	69	0	0	0	28	143	0	26
IPE 100	384	376	Neve	PolG	0	0	0	0	24	68	0	27
IPE 100	384	376	Neve	PolG	68	0	0	0	27	143	0	27
IPE 100	384	376	Vento X	PolG	69	0	0	0	26	69	0	26
IPE 100	384	376	Vento X	PolG	0	0	0	0	38	68	0	42
IPE 100	384	376	Vento X	PolG	68	0	0	0	42	143	0	42
IPE 100	384	376	Vento X	PolG	69	0	0	0	41	69	0	41
IPE 100	384	376	Carichi termici	Termico	69	0	0	0	41	143	0	35
IPE 100	386	372	Peso Proprio	UnifG	0	0	0	0	8	144	0	8
IPE 100	386	372	QP Solai	PolG	28	0	0	0	86	28	0	97
					43	0	0	0	97	43	0	106
					106	0	0	0	106	106	0	100
					110	0	0	0	98	144	0	98
IPE 100	386	372	QV Solai	PolG	110	0	0	0	98	144	0	86
					28	0	0	0	31	43	0	34
					43	0	0	0	34	106	0	32

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	386	372	Neve	PolG	110	0	0	0	32	110	0	32
IPE 100	386	372	Neve	PolG	0	0	0	0	26	28	0	26
IPE 100	386	372	Neve	PolG	106	0	0	0	35	144	0	26
					43	0	0	0	27	43	0	38
IPE 100	386	372	Vento X	PolG	110	0	0	0	27	144	0	27
					43	0	0	0	59	110	0	42
IPE 100	386	372	Vento X	PolG	110	0	0	0	42	144	0	42
					28	0	0	0	41	106	0	54
IPE 100	386	372	Carichi termici	Termico	106	0	0	0	54	144	0	41
IPE 100	388	378	Peso Proprio	UnifG	0	0	0	0	8	143	0	8
IPE 100	388	378	QP Solai	PolG	64	0	0	0	119	85	0	117
					85	0	0	0	117	139	0	87
IPE 100	388	378	QV Solai	PolG	139	0	0	0	87	143	0	86
					64	0	0	0	27	64	0	38
					85	0	0	0	38	85	0	38
IPE 100	388	378	Neve	PolG	139	0	0	0	28	143	0	28
					85	0	0	0	37	143	0	26
IPE 100	388	378	Neve	PolG	64	0	0	0	40	139	0	27
IPE 100	388	378	Vento X	PolG	139	0	0	0	27	143	0	27
IPE 100	388	378	Vento X	PolG	85	0	0	0	40	85	0	57
IPE 100	388	378	Vento X	PolG	85	0	0	0	57	143	0	41
					64	0	0	0	62	139	0	42
IPE 100	388	378	Carichi termici	Termico	139	0	0	0	42	143	0	42
IPE 100	390	394	Peso Proprio	UnifG	0	0	0	0	8	143	0	8
IPE 100	390	394	QP Solai	PolG	60	0	0	0	73	60	0	116
					89	0	0	0	116	143	0	73
IPE 100	390	394	QV Solai	PolG	60	0	0	0	37	89	0	37
					89	0	0	0	37	143	0	24
IPE 100	390	394	Neve	PolG	60	0	0	0	18	60	0	37
IPE 100	390	394	Neve	PolG	0	0	0	0	37	143	0	26
IPE 100	390	394	Vento X	PolG	89	0	0	0	39	143	0	19
IPE 100	390	394	Vento X	PolG	89	0	0	0	42	89	0	61
IPE 100	390	394	Vento X	PolG	89	0	0	0	61	143	0	30
IPE 100	390	394	Vento X	PolG	60	0	0	0	28	60	0	57
IPE 100	390	394	Carichi termici	Termico	60	0	0	0	57	143	0	41
IPE 100	392	0	Peso Proprio	UnifG	0	0	0	0	8	143	0	8
IPE 100	392	0	QP Solai	PolG	12	0	0	0	48	12	0	86
					137	0	0	0	86	143	0	47
IPE 100	392	0	QV Solai	PolG	12	0	0	0	15	12	0	28
					137	0	0	0	28	137	0	28
IPE 100	392	0	Neve	PolG	0	0	0	0	3	12	0	15
IPE 100	392	0	Neve	PolG	12	0	0	0	26	143	0	26
IPE 100	392	0	Vento X	PolG	137	0	0	0	27	137	0	27
IPE 100	392	0	Vento X	PolG	0	0	0	0	42	137	0	3
IPE 100	392	0	Vento X	PolG	137	0	0	0	42	143	0	5
IPE 100	392	0	Vento X	PolG	0	0	0	0	4	12	0	41
					12	0	0	0	41	143	0	41

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	OXi	OYi	QZi	Xf	QXf	QYf	QZf	
IPE 100	392	0	Carichi termici Peso Proprio QP Solai QV Solai	Termico	0	0	0	0	8	142	0	0	
	396	360		UnifG	136	0	0	0	88	136	0	0	
	396	360		PolG	0	0	0	0	86	142	0	45	
	396	360		PolG	0	0	0	0	28	136	0	28	
IPE 100	396	360	Neve Neve Vento X Vento X	PolG	136	0	0	0	28	142	0	15	
	396	360		PolG	0	0	0	0	28	142	0	27	
	396	360		PolG	0	0	0	0	26	136	0	26	
	396	360		PolG	136	0	0	0	26	142	0	1	
IPE 100	396	360	Vento X Vento X	PolG	136	0	0	0	41	136	0	41	
	396	360		PolG	0	0	0	0	41	142	0	1	
	396	360		PolG	0	0	0	0	44	142	0	42	
	396	360		Termico	0	0	0	0	8	143	0	8	
IPE 100	398	392	Carichi termici Peso Proprio QP Solai	UnifG	18	0	0	0	51	18	0	86	
	398	392		PolG	0	0	0	0	86	131	0	86	
	398	392		PolG	131	0	0	0	86	143	0	50	
	398	392		PolG	0	0	0	0	16	18	0	28	
IPE 100	398	392	Neve Neve Vento X Vento X	PolG	18	0	0	0	28	131	0	28	
	398	392		PolG	131	0	0	0	28	143	0	16	
	398	392		PolG	0	0	0	0	27	131	0	27	
	398	392		PolG	131	0	0	0	27	143	0	5	
IPE 100	398	392	Vento X Vento X	PolG	18	0	0	0	26	143	0	26	
	398	392		PolG	0	0	0	0	42	131	0	42	
	398	392		PolG	131	0	0	0	42	143	0	8	
	398	392		PolG	0	0	0	0	7	18	0	41	
IPE 100	398	392	Carichi termici Peso Proprio QP Solai	Termico	18	0	0	0	41	143	0	41	
	398	392		UnifG	0	0	0	0	8	144	0	8	
	400	0		PolG	0	0	0	0	58	30	0	86	
	400	0		PolG	30	0	0	0	86	119	0	86	
IPE 100	400	0	QV Solai	PolG	119	0	0	0	86	144	0	57	
	400	0		PolG	0	0	0	0	19	30	0	28	
	400	0		PolG	30	0	0	0	28	119	0	28	
	400	0		PolG	119	0	0	0	28	144	0	18	
IPE 100	400	0	Neve Neve Vento X Vento X	PolG	0	0	0	0	9	30	0	26	
	400	0		PolG	30	0	0	0	26	144	0	26	
	400	0		PolG	0	0	0	0	27	119	0	27	
	400	0		PolG	119	0	0	0	27	144	0	9	
IPE 100	400	0	Vento X Vento X	PolG	0	0	0	0	42	119	0	42	
	400	0		PolG	119	0	0	0	42	144	0	14	
	400	0		PolG	0	0	0	0	14	30	0	41	
	400	0		PolG	30	0	0	0	14	30	0	41	
IPE 100	400	0	Carichi termici	Termico	30	0	0	0	41	144	0	41	
	327	328		Peso Proprio	UnifG	0	0	0	0	8	138	0	8
	327	328		QP Solai	PolG	0	0	0	0	15	30	0	44
	327	328		QV Solai	PolG	30	0	0	0	44	150	0	44
IPE 100	327	328	Neve Neve Vento X Vento X	PolG	0	0	0	0	5	30	0	14	
	327	328		PolG	30	0	0	0	14	150	0	14	
	327	328		PolG	0	0	0	0	10	30	0	27	
	327	328		PolG	30	0	0	0	27	150	0	27	
IPE 100	327	328	Carichi termici Peso Proprio QP Solai	Termico	30	0	0	0	15	30	0	42	
	327	328		UnifG	0	0	0	0	42	150	0	42	
	328	329		PolG	0	0	0	0	8	150	0	8	
	328	329		PolG	24	0	0	0	12	24	0	44	
IPE 100	328	329	QV Solai Neve Vento X Vento X	PolG	0	0	0	0	44	150	0	44	
	328	329		PolG	0	0	0	0	4	24	0	14	
	328	329		PolG	24	0	0	0	14	150	0	14	
	328	329		PolG	0	0	0	0	7	24	0	27	
IPE 100	328	329	Vento X Vento X	PolG	24	0	0	0	27	150	0	27	
	328	329		PolG	0	0	0	0	11	24	0	42	
	328	329		PolG	24	0	0	0	42	150	0	42	
	328	329		Termico	0	0	0	0	8	150	0	8	

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	329	330	Peso Proprio QP Solai	UnifG	0	0	0	0	8	149	0	0
	329	330		PolG	0	0	0	0	8	18	0	0
	329	330		PolG	18	0	0	0	44	149	0	0
IPE 100	329	330	QV Solai	PolG	0	0	0	0	3	18	0	0
	329	330		PolG	0	0	0	0	3	18	0	0
	329	330		PolG	18	0	0	0	14	149	0	0
IPE 100	329	330	Neve	PolG	0	0	0	0	5	18	0	0
	329	330		PolG	18	0	0	0	27	149	0	0
	329	330		PolG	0	0	0	0	8	18	0	0
IPE 100	329	330	Vento X	PolG	0	0	0	0	8	18	0	0
	329	330		PolG	18	0	0	0	42	149	0	0
	329	330		PolG	18	0	0	0	42	149	0	0
IPE 100	329	330	Carichi termici	Termico	$\Delta XY=15^{\circ}; \Delta XZ=15^{\circ}$	0	0	0	8	148	0	0
	329	330		UnifG	0	0	0	0	5	12	0	0
	329	330		PolG	0	0	0	0	44	148	0	0
IPE 100	330	331	Peso Proprio QP Solai	PolG	12	0	0	0	44	148	0	0
	330	331		PolG	0	0	0	0	2	12	0	0
	330	331		PolG	12	0	0	0	14	148	0	0
IPE 100	330	331	Neve	PolG	0	0	0	0	3	12	0	0
	330	331		PolG	0	0	0	0	27	148	0	0
	330	331		PolG	12	0	0	0	5	12	0	0
IPE 100	330	331	Vento X	PolG	0	0	0	0	8	150	0	0
	330	331		PolG	6	0	0	0	44	150	0	0
	330	331		PolG	6	0	0	0	1	6	0	0
IPE 100	331	332	Neve	PolG	0	0	0	0	1	6	0	0
	331	332		PolG	6	0	0	0	27	150	0	0
	331	332		PolG	0	0	0	0	2	6	0	0
IPE 100	331	332	Vento X	PolG	0	0	0	0	42	150	0	0
	331	332		PolG	6	0	0	0	42	150	0	0
	331	332		PolG	6	0	0	0	42	150	0	0
IPE 100	331	332	Carichi termici	Termico	$\Delta XY=15^{\circ}; \Delta XZ=15^{\circ}$	0	0	0	8	148	0	0
	331	332		UnifG	0	0	0	0	44	142	0	0
	331	332		PolG	0	0	0	0	44	148	0	0
IPE 100	332	333	Peso Proprio QP Solai	PolG	142	0	0	0	14	142	0	0
	332	333		PolG	0	0	0	0	14	142	0	0
	332	333		PolG	0	0	0	0	14	148	0	0
IPE 100	332	333	QV Solai	PolG	0	0	0	0	27	142	0	0
	332	333		PolG	142	0	0	0	27	142	0	0
	332	333		PolG	0	0	0	0	27	148	0	0
IPE 100	332	333	Neve	PolG	0	0	0	0	42	142	0	0
	332	333		PolG	0	0	0	0	42	142	0	0
	332	333		PolG	142	0	0	0	42	148	0	0
IPE 100	332	333	Vento X	PolG	0	0	0	0	8	153	0	0
	332	333		PolG	0	0	0	0	44	140	0	0
	332	333		PolG	0	0	0	0	44	153	0	0
IPE 100	333	334	Peso Proprio QP Solai	PolG	140	0	0	0	14	140	0	0
	333	334		PolG	0	0	0	0	14	140	0	0
	333	334		PolG	0	0	0	0	14	153	0	0
IPE 100	333	334	QV Solai	PolG	140	0	0	0	27	140	0	0
	333	334		PolG	0	0	0	0	27	140	0	0
	333	334		PolG	0	0	0	0	27	153	0	0
IPE 100	333	334	Neve	PolG	140	0	0	0	42	140	0	0
	333	334		PolG	0	0	0	0	42	140	0	0
	333	334		PolG	140	0	0	0	42	153	0	0
IPE 100	333	334	Vento X	PolG	0	0	0	0	8	148	0	0
	333	334		PolG	0	0	0	0	44	129	0	0
	333	334		PolG	0	0	0	0	44	148	0	0
IPE 100	334	335	Peso Proprio QP Solai	PolG	129	0	0	0	14	129	0	0
	334	335		PolG	0	0	0	0	14	129	0	0
	334	335		PolG	0	0	0	0	14	148	0	0
IPE 100	334	335	QV Solai	PolG	129	0	0	0	27	129	0	0
	334	335		PolG	0	0	0	0	27	129	0	0
	334	335		PolG	0	0	0	0	27	148	0	0
IPE 100	334	335	Neve	PolG	129	0	0	0	42	129	0	0
	334	335		PolG	0	0	0	0	42	129	0	0
	334	335		PolG	129	0	0	0	42	148	0	0
IPE 100	334	335	Vento X	PolG	0	0	0	0	8	150	0	0
	334	335		PolG	0	0	0	0	44	125	0	0
	334	335		PolG	0	0	0	0	44	150	0	0
IPE 100	335	336	Peso Proprio QP Solai	PolG	125	0	0	0	14	125	0	0
	335	336		PolG	0	0	0	0	14	125	0	0
	335	336		PolG	0	0	0	0	14	125	0	0
IPE 100	335	336	QV Solai	PolG	125	0	0	0	27	125	0	0
	335	336		PolG	0	0	0	0	27	125	0	0
	335	336		PolG	0	0	0	0	27	125	0	0
IPE 100	335	336	Neve	PolG	0	0	0	0	4	4	0	0
	335	336		PolG	0	0	0	0	14	150	0	0
	335	336		PolG	0	0	0	0	27	125	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	335	336	Vento X	PolG	125	0	0	27	150	0	0	7
IPE 100	335	336	Carichi termici	Termico	125	0	0	42	150	0	0	11
IPE 100	336	337	Peso Proprio	UnitG	AXY=15°C, AXZ=15°C							
IPE 100	336	337	QP Solai	PolG	0	0	0	8	150	0	0	8
IPE 100	336	337	QV Solai	PolG	119	0	0	44	119	0	0	44
IPE 100	336	337	Neve	PolG	119	0	0	14	119	0	0	14
IPE 100	336	337	Vento X	PolG	119	0	0	27	119	0	0	27
IPE 100	336	337	Vento X	PolG	119	0	0	27	150	0	0	10
IPE 100	336	337	Vento X	PolG	119	0	0	42	119	0	0	42
IPE 100	336	337	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	337	338	Peso Proprio	UnitG	0	0	0	8	161	0	0	8
IPE 100	337	338	QP Solai	PolG	112	0	0	44	112	0	0	44
IPE 100	337	338	QV Solai	PolG	112	0	0	44	149	0	0	19
IPE 100	337	338	Neve	PolG	112	0	0	14	112	0	0	14
IPE 100	337	338	Neve	PolG	112	0	0	14	149	0	0	6
IPE 100	337	338	Neve	PolG	112	0	0	27	112	0	0	27
IPE 100	337	338	Vento X	PolG	112	0	0	27	149	0	0	12
IPE 100	337	338	Vento X	PolG	112	0	0	42	112	0	0	42
IPE 100	337	338	Vento X	PolG	112	0	0	42	149	0	0	18
IPE 100	337	338	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	338	339	Peso Proprio	UnitG	0	0	0	8	138	0	0	8
IPE 100	338	339	QP Solai	PolG	106	0	0	44	106	0	0	44
IPE 100	338	339	QV Solai	PolG	106	0	0	44	150	0	0	23
IPE 100	338	339	Neve	PolG	106	0	0	14	106	0	0	14
IPE 100	338	339	Neve	PolG	106	0	0	14	150	0	0	7
IPE 100	338	339	Neve	PolG	106	0	0	27	106	0	0	27
IPE 100	338	339	Vento X	PolG	106	0	0	27	150	0	0	14
IPE 100	338	339	Vento X	PolG	106	0	0	42	106	0	0	42
IPE 100	338	339	Vento X	PolG	106	0	0	42	150	0	0	22
IPE 100	338	339	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	339	340	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	339	340	QP Solai	PolG	0	0	0	44	98	0	0	44
IPE 100	339	340	QV Solai	PolG	98	0	0	44	149	0	0	27
IPE 100	339	340	Neve	PolG	98	0	0	14	98	0	0	14
IPE 100	339	340	Neve	PolG	98	0	0	14	149	0	0	9
IPE 100	339	340	Neve	PolG	98	0	0	27	98	0	0	27
IPE 100	339	340	Vento X	PolG	98	0	0	27	149	0	0	17
IPE 100	339	340	Vento X	PolG	98	0	0	42	98	0	0	42
IPE 100	339	340	Vento X	PolG	98	0	0	42	149	0	0	26
IPE 100	339	340	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	340	341	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	340	341	QP Solai	PolG	0	0	0	44	91	0	0	44
IPE 100	340	341	QV Solai	PolG	91	0	0	44	149	0	0	31
IPE 100	340	341	Neve	PolG	91	0	0	14	91	0	0	14
IPE 100	340	341	Neve	PolG	91	0	0	14	149	0	0	10
IPE 100	340	341	Neve	PolG	91	0	0	27	91	0	0	27
IPE 100	340	341	Vento X	PolG	91	0	0	27	149	0	0	19
IPE 100	340	341	Vento X	PolG	91	0	0	42	91	0	0	42
IPE 100	340	341	Vento X	PolG	91	0	0	42	149	0	0	29
IPE 100	340	341	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	341	342	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	341	342	QP Solai	PolG	0	0	0	44	83	0	0	44
IPE 100	341	342	QV Solai	PolG	83	0	0	44	150	0	0	35
IPE 100	341	342	Neve	PolG	83	0	0	14	83	0	0	14
IPE 100	341	342	Neve	PolG	83	0	0	14	150	0	0	11
IPE 100	341	342	Neve	PolG	83	0	0	27	83	0	0	27
IPE 100	341	342	Vento X	PolG	83	0	0	27	150	0	0	22
IPE 100	341	342	Vento X	PolG	83	0	0	42	83	0	0	42
IPE 100	341	342	Vento X	PolG	83	0	0	42	150	0	0	34
IPE 100	341	342	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	342	343	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	342	343	QP Solai	PolG	0	0	0	44	75	0	0	44

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	342	343	QV Solai	PolG	75	0	0	44	149	0	0	39
IPE 100	342	343	Neve	PolG	75	0	0	14	149	0	0	13
IPE 100	342	343	Vento X	PolG	75	0	0	27	149	0	0	24
IPE 100	342	343	Vento X	PolG	75	0	0	42	75	0	0	42
IPE 100	342	343	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	343	344	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	343	344	QP Solai	PolG	66	0	0	44	147	0	0	45
IPE 100	343	344	QV Solai	PolG	147	0	0	45	150	0	0	44
IPE 100	343	344	Neve	PolG	0	0	0	14	150	0	0	14
IPE 100	343	344	Vento X	PolG	0	0	0	27	150	0	0	27
IPE 100	343	344	Vento X	PolG	66	0	0	42	66	0	0	42
IPE 100	343	344	Vento X	PolG	66	0	0	42	147	0	0	44
IPE 100	343	344	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	344	345	Peso Proprio	UnitG	147	0	0	44	150	0	0	42
IPE 100	344	345	QP Solai	PolG	0	0	0	8	149	0	0	8
IPE 100	344	345	QV Solai	PolG	55	0	0	44	55	0	0	44
IPE 100	344	345	Neve	PolG	131	0	0	17	149	0	0	14
IPE 100	344	345	Neve	PolG	55	0	0	27	131	0	0	27
IPE 100	344	345	Vento X	PolG	131	0	0	32	149	0	0	27
IPE 100	344	345	Vento X	PolG	55	0	0	42	55	0	0	42
IPE 100	344	345	Vento X	PolG	55	0	0	42	131	0	0	50
IPE 100	344	345	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	345	346	Peso Proprio	UnitG	131	0	0	50	149	0	0	42
IPE 100	345	346	QP Solai	PolG	0	0	0	8	149	0	0	8
IPE 100	345	346	QV Solai	PolG	45	0	0	44	45	0	0	44
IPE 100	345	346	Neve	PolG	118	0	0	57	149	0	0	44
IPE 100	345	346	Neve	PolG	45	0	0	14	45	0	0	14
IPE 100	345	346	Neve	PolG	118	0	0	18	149	0	0	14
IPE 100	345	346	Neve	PolG	45	0	0	27	45	0	0	27
IPE 100	345	346	Neve	PolG	45	0	0	27	118	0	0	35
IPE 100	345	346	Vento X	PolG	118	0	0	35	149	0	0	27
IPE 100	345	346	Vento X	PolG	45	0	0	42	45	0	0	42
IPE 100	345	346	Vento X	PolG	45	0	0	42	118	0	0	55
IPE 100	345	346	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	346	347	Peso Proprio	UnitG	118	0	0	55	149	0	0	42
IPE 100	346	347	QP Solai	PolG	0	0	0	8	150	0	0	8
IPE 100	346	347	QV Solai	PolG	34	0	0	44	34	0	0	44
IPE 100	346	347	Neve	PolG	106	0	0	60	106	0	0	60
IPE 100	346	347	Neve	PolG	106	0	0	60	150	0	0	44
IPE 100	346	347	QV Solai	PolG	34	0	0	14	34	0	0	14
IPE 100	346	347	QV Solai	PolG	34	0	0	14	106	0	0	19
IPE 100	346	347	Neve	PolG	106	0	0	19	150	0	0	14
IPE 100	346	347	Neve	PolG	34	0	0	27	34	0	0	27
IPE 100	346	347	Vento X	PolG	106	0	0	37	150	0	0	27
IPE 100	346	347	Vento X	PolG	34	0	0	42	34	0	0	42
IPE 100	346	347	Vento X	PolG	34	0	0	42	106	0	0	58
IPE 100	346	347	Carichi termici	Termico	AXY=15°C, AXZ=15°C							
IPE 100	347	348	Peso Proprio	UnitG	106	0	0	58	150	0	0	42
IPE 100	347	348	QP Solai	PolG	0	0	0	8	149	0	0	8
IPE 100	347	348	QP Solai	PolG	20	0	0	44	20	0	0	44
IPE 100	347	348	QP Solai	PolG	95	0	0	62	149	0	0	62
IPE 100	347	348	QP Solai	PolG	0	0	0	14	20	0	0	14
IPE 100	347	348	QP Solai	PolG	20	0	0	14	95	0	0	20

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	347	348	Neve	PolG	0	0	0	20	149	0	0	14
					20	0	0	27	95	0	0	39
IPE 100	347	348	Vento X	PolG	95	0	0	39	149	0	0	27
					20	0	0	42	20	0	0	42
					95	0	0	42	95	0	0	60
IPE 100	347	348	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	149	0	42
IPE 100	348	349	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	348	349	QP Solai	PolG	4	0	0	44	4	0	0	44
					85	0	0	63	149	0	0	44
IPE 100	348	349	QV Solai	PolG	0	0	0	14	4	0	0	14
					4	0	0	14	85	0	0	20
IPE 100	348	349	Neve	PolG	85	0	0	20	149	0	0	14
					4	0	0	27	4	0	0	27
IPE 100	348	349	Vento X	PolG	85	0	0	39	149	0	0	27
					4	0	0	42	4	0	0	42
IPE 100	348	349			85	0	0	61	149	0	0	42
IPE 100	348	349	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	61	149	0	42
IPE 100	349	350	Peso Proprio	UnitG	0	0	0	8	150	0	0	8
IPE 100	349	350	QP Solai	PolG	76	0	0	64	150	0	0	44
IPE 100	349	350	QV Solai	PolG	0	0	0	13	76	0	0	20
IPE 100	349	350	Neve	PolG	76	0	0	20	150	0	0	14
IPE 100	349	350	Vento X	PolG	76	0	0	40	150	0	0	27
IPE 100	349	350			76	0	0	39	76	0	0	61
IPE 100	349	350	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	61	150	0	42
IPE 100	350	351	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	350	351	QP Solai	PolG	68	0	0	63	149	0	0	63
IPE 100	350	351	QV Solai	PolG	0	0	0	11	68	0	0	20
IPE 100	350	351	Neve	PolG	68	0	0	20	149	0	0	14
IPE 100	350	351	Vento X	PolG	68	0	0	39	149	0	0	27
IPE 100	350	351			68	0	0	34	68	0	0	61
IPE 100	350	351	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	61	149	0	42
IPE 100	351	352	Peso Proprio	UnitG	0	0	0	8	149	0	0	8
IPE 100	351	352	QP Solai	PolG	60	0	0	32	60	0	0	63
IPE 100	351	352	QV Solai	PolG	0	0	0	63	149	0	0	44
IPE 100	351	352	Neve	PolG	60	0	0	10	60	0	0	20
IPE 100	351	352	Vento X	PolG	60	0	0	20	149	0	0	14
IPE 100	351	352			60	0	0	20	60	0	0	39
IPE 100	351	352	Vento X	PolG	60	0	0	39	149	0	0	27
IPE 100	351	352			60	0	0	30	60	0	0	60
IPE 100	351	352	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	60	149	0	42
Trave 8039												
IPE 100	53	55	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	53	55	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	54	53	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	54	53	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	55	56	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	55	56	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	56	71	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	56	71	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	57	59	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	57	59	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	58	66	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	58	66	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
IPE 100	59	65	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	59	65	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	60	57	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	60	57	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	61	62	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	61	62	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	62	63	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	62	63	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	63	64	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	63	64	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	64	60	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	64	60	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	65	58	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	65	58	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	66	67	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	66	67	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	67	68	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	67	68	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	69	77	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	69	77	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	70	69	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	70	69	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	71	74	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	71	74	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	72	70	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	72	70	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	73	61	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	73	61	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	74	76	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	74	76	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	75	72	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	75	72	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	76	75	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	76	75	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
IPE 100	77	78	Peso Proprio	UnitG	0	0	0	8	89	0	0	8
IPE 100	77	78	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	89	0	8
IPE 100	78	73	Peso Proprio	UnitG	0	0	0	8	90	0	0	8
IPE 100	78	73	Carichi termici	Termico	AXY=15°C,AXZ=15°C	0	0	0	8	90	0	8
Fondazione 9009												
F60x100	1	2	Peso Proprio	UnitG	0	0	0	1500	90	0	0	1500
F60x100	2	3	Peso Proprio	UnitG	0	0	0	1500	90	0	0	1500
F60x100	3	4	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	4	5	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	5	6	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	6	7	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	7	8	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	8	9	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	9	10	Peso Proprio	UnitG	0	0	0	1500	90	0	0	1500
F60x100	10	11	Peso Proprio	UnitG	0	0	0	1500	90	0	0	1500
F60x100	11	12	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	12	13	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	13	14	Peso Proprio	UnitG	0	0	0	1500	90	0	0	1500
F60x100	14	15	Peso Proprio	UnitG	0	0	0	1500	90	0	0	1500
F60x100	15	16	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	16	17	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	17	18	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	18	19	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	19	20	Peso Proprio	UnitG	0	0	0	1500	90	0	0	1500
F60x100	20	21	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	21	22	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	22	23	Peso Proprio	UnitG	0	0	0	1500	90	0	0	1500
F60x100	23	24	Peso Proprio	UnitG	0	0	0	1500	89	0	0	1500
F60x100	24	25	Peso Proprio	UnitG	0	0	0	1500	90	0	0	1500
F60x100	25	26	Peso Proprio	UnitG	0	0	0	1500	101	0	0	1500
Fondazione 9010												

Sezione	Ni	NF	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Genericia 7001	F60x100	1	2	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
	F60x100	2	3	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
	F60x100	3	4	Peso Proprio	UnifG	0	0	0	1500	149	0	1500
	F60x100	4	5	Peso Proprio	UnifG	0	0	0	1500	148	0	1500
	F60x100	5	6	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
	F60x100	6	7	Peso Proprio	UnifG	0	0	0	1500	148	0	1500
	F60x100	7	8	Peso Proprio	UnifG	0	0	0	1500	153	0	1500
	F60x100	8	9	Peso Proprio	UnifG	0	0	0	1500	148	0	1500
	F60x100	9	10	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
	F60x100	10	11	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
	F60x100	11	12	Peso Proprio	UnifG	0	0	0	1500	149	0	1500
	F60x100	12	13	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
Genericia 7002	F60x100	13	14	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
	F60x100	14	15	Peso Proprio	UnifG	0	0	0	1500	149	0	1500
	F60x100	15	16	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
	F60x100	16	17	Peso Proprio	UnifG	0	0	0	1500	149	0	1500
	F60x100	17	18	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
	F60x100	18	19	Peso Proprio	UnifG	0	0	0	1500	149	0	1500
	F60x100	19	20	Peso Proprio	UnifG	0	0	0	1500	149	0	1500
	F60x100	20	21	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
	F60x100	21	22	Peso Proprio	UnifG	0	0	0	1500	149	0	1500
	F60x100	22	23	Peso Proprio	UnifG	0	0	0	1500	149	0	1500
	F60x100	23	24	Peso Proprio	UnifG	0	0	0	1500	150	0	1500
	F60x100	24	25	Peso Proprio	UnifG	0	0	0	1500	149	0	1500
Genericia 7003	F60x100	25	26	Peso Proprio	UnifG	0	0	0	1500	161	0	1500
	F60x100	25	26	Peso Proprio	UnifG	0	0	0	1500	161	0	1500
Genericia 7004	F60x100	1	53	Peso Proprio	UnifG	0	0	0	2	256	0	2
	F60x100	1	53	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7005	F60x100	53	101	Peso Proprio	UnifG	0	0	0	2	190	0	2
	F60x100	53	101	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7006	F60x100	101	0	Peso Proprio	UnifG	0	0	0	2	372	0	2
	F60x100	101	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7007	F60x100	0	0	Peso Proprio	UnifG	0	0	0	2	345	0	2
	F60x100	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7008	F60x100	0	75	Peso Proprio	UnifG	0	0	0	2	306	0	2
	F60x100	0	75	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7009	F60x100	75	399	Peso Proprio	UnifG	0	0	0	2	269	0	2
	F60x100	75	399	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7010	F60x100	399	328	Peso Proprio	UnifG	0	0	0	2	261	0	2
	F60x100	399	328	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7011	F60x100	327	0	Peso Proprio	UnifG	0	0	0	2	261	0	2
	F60x100	327	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7012	F60x100	0	73	Peso Proprio	UnifG	0	0	0	2	269	0	2
	F60x100	0	73	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7013	F60x100	73	0	Peso Proprio	UnifG	0	0	0	2	306	0	2
	F60x100	73	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7014	F60x100	0	0	Peso Proprio	UnifG	0	0	0	2	345	0	2
	F60x100	0	0	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7015	F60x100	0	102	Peso Proprio	UnifG	0	0	0	2	372	0	2
	F60x100	0	102	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						
Genericia 7016	F60x100	102	54	Peso Proprio	UnifG	0	0	0	2	189	0	2
	F60x100	102	54	Carichi termici	Termico	ΔXY=15°C, ΔXZ=15°C						

Sezione	Ni	NF	Cond	Tiplo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
F20	54	2	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	256	0	0	2
Generico 7015												
F20	25	68	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	256	0	0	2
Generico 7016												
F20	68	125	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	189	0	0	2
Generico 7017												
F16	125	0	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	372	0	0	2
Generico 7018												
F16	0	0	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	345	0	0	2
Generico 7019												
F16	0	67	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	306	0	0	2
Generico 7020												
F16	67	389	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	269	0	0	2
Generico 7021												
F16	389	352	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	261	0	0	2
Generico 7022												
F16	351	393	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	260	0	0	2
Generico 7023												
F16	393	63	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	269	0	0	2
Generico 7024												
F16	63	0	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	306	0	0	2
Generico 7025												
F16	0	0	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	345	0	0	2
Generico 7026												
F16	0	126	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	370	0	0	2
Generico 7027												
F20	126	67	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	189	0	0	2
Generico 7028												
F20	67	26	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	256	0	0	2
Generico 7029												
F16	102	0	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	407	0	0	2
Generico 7030												
F16	104	0	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	406	0	0	2
Generico 7031												
F16	328	391	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	360	0	0	2
Generico 7032												
F16	330	0	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	358	0	0	2
Generico 7033												
F20	19	64	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	247	0	0	2
Generico 7034												
F20	64	119	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	185	0	0	2
Generico 7035												
F16	119	174	Peso Proprio Carchi termiei	UnifG Termico	0	0	0	2	371	0	0	2

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Generica 7036												
Fi16	174	0	Peso Proprio	UnitG	0	0	0	0	2	345	0	0
Fi16	174	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7037												
Fi16	0	35	Peso Proprio	UnitG	0	0	0	0	2	306	0	0
Fi16	0	35	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7038												
Fi16	35	379	Peso Proprio	UnitG	0	0	0	0	2	244	0	0
Fi16	35	379	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7039												
Fi16	379	344	Peso Proprio	UnitG	0	0	0	0	2	261	0	0
Fi16	379	344	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7040												
Fi16	345	361	Peso Proprio	UnitG	0	0	0	0	2	260	0	0
Fi16	345	361	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7041												
Fi16	361	53	Peso Proprio	UnitG	0	0	0	0	2	269	0	0
Fi16	361	53	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7042												
Fi16	53	176	Peso Proprio	UnitG	0	0	0	0	2	306	0	0
Fi16	53	176	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7043												
Fi16	176	0	Peso Proprio	UnitG	0	0	0	0	2	339	0	0
Fi16	176	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7044												
Fi16	0	118	Peso Proprio	UnitG	0	0	0	0	2	371	0	0
Fi16	0	118	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7045												
Fi20	118	60	Peso Proprio	UnitG	0	0	0	0	2	189	0	0
Fi20	118	60	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7046												
Fi20	60	18	Peso Proprio	UnitG	0	0	0	0	2	256	0	0
Fi20	60	18	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7047												
Fi16	199	123	Peso Proprio	UnitG	0	0	0	0	2	401	0	0
Fi16	199	123	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7048												
Fi16	123	0	Peso Proprio	UnitG	0	0	0	0	2	406	0	0
Fi16	123	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7049												
Fi16	125	0	Peso Proprio	UnitG	0	0	0	0	2	407	0	0
Fi16	125	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7050												
Fi16	0	121	Peso Proprio	UnitG	0	0	0	0	2	407	0	0
Fi16	0	121	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7051												
Fi16	121	0	Peso Proprio	UnitG	0	0	0	0	2	406	0	0
Fi16	121	0	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7052												
Fi16	379	347	Peso Proprio	UnitG	0	0	0	0	2	360	0	0
Fi16	379	347	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7053												
Fi16	347	377	Peso Proprio	UnitG	0	0	0	0	2	359	0	0
Fi16	347	377	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7054												
Fi16	377	351	Peso Proprio	UnitG	0	0	0	0	2	360	0	0
Fi16	377	351	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7055												
Fi16	371	345	Peso Proprio	UnitG	0	0	0	0	2	360	0	0
Fi16	371	345	Carchi termici	Termico	AXY=15°C,AXZ=15°C							2
Generica 7056												
Fi16	389	349	Peso Proprio	UnitG	0	0	0	0	2	360	0	0
Fi16	349	371	Peso Proprio	UnitG	0	0	0	0	2	359	0	0
Generica 7058												

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Generica 7059												
Fi20	108	76	Peso Proprio	UnitG	0	0	0	0	2	190	0	0
Generica 7060												
Fi20	76	8	Peso Proprio	UnitG	0	0	0	0	2	256	0	0
Generica 7061												
Fi20	7	75	Peso Proprio	UnitG	0	0	0	0	2	256	0	0
Generica 7062												
Fi20	75	107	Peso Proprio	UnitG	0	0	0	0	2	190	0	0
Generica 7063												
Fi16	107	184	Peso Proprio	UnitG	0	0	0	0	2	370	0	0
Generica 7064												
Fi16	184	171	Peso Proprio	UnitG	0	0	0	0	2	346	0	0
Generica 7065												
Fi16	171	39	Peso Proprio	UnitG	0	0	0	0	2	306	0	0
Generica 7066												
Fi16	39	359	Peso Proprio	UnitG	0	0	0	0	2	270	0	0
Generica 7067												
Fi16	359	334	Peso Proprio	UnitG	0	0	0	0	2	260	0	0
Generica 7068												
Fi16	333	365	Peso Proprio	UnitG	0	0	0	0	2	262	0	0
Generica 7069												
Fi16	365	33	Peso Proprio	UnitG	0	0	0	0	2	270	0	0
Generica 7070												
Fi16	33	186	Peso Proprio	UnitG	0	0	0	0	2	307	0	0
Generica 7071												
Fi16	186	169	Peso Proprio	UnitG	0	0	0	0	2	346	0	0
Generica 7072												
Fi16	169	108	Peso Proprio	UnitG	0	0	0	0	2	372	0	0
Generica 7073												
Fi16	0	107	Peso Proprio	UnitG	0	0	0	0	2	458	0	0
Generica 7074												
Fi16	104	169	Peso Proprio	UnitG	0	0	0	0	2	458	0	0
Generica 7075												
Fi16	391	333	Peso Proprio	UnitG	0	0	0	0	2	480	0	0
Generica 7076												
Fi16	359	330	Peso Proprio	UnitG	0	0	0	0	2	480	0	0
Generica 7077												
Fi16	108	154	Peso Proprio	UnitG	0	0	0	0	2	459	0	0
Generica 7078												
Fi16	184	111	Peso Proprio	UnitG	0	0	0	0	2	458	0	0
Generica 7079												
Fi16	111	194	Peso Proprio	UnitG	0	0	0	0	2	405	0	0
Generica 7080												
Fi16	194	114	Peso Proprio	UnitG	0	0	0	0	2	371	0	0
Generica 7081												
Fi20	114	78	Peso Proprio	UnitG	0	0	0	0	2	189	0	0
Generica 7082												
Fi20	78	14	Peso Proprio	UnitG	0	0	0	0	2	256	0	0
Generica 7083												
Fi20	13	73	Peso Proprio	UnitG	0	0	0	0	2	256	0	0
Generica 7084												
Fi20	73	113	Peso Proprio	UnitG	0	0	0	0	2	189	0	0
Generica 7085												
Fi16	113	159	Peso Proprio	UnitG	0	0	0	0	2	372	0	0
Generica 7086												
Fi16	159	196	Peso Proprio	UnitG	0	0	0	0	2	345	0	0
Generica 7087												
Fi16	196	29	Peso Proprio	UnitG	0	0	0	0	2	306	0	0
Generica 7088												
Fi16	161	194	Peso Proprio	UnitG	0	0	0	0	2	345	0	0
Generica 7089												
Fi16	154	113	Peso Proprio	UnitG	0	0	0	0	2	406	0	0
Generica 7090												
Fi16	161	43	Peso Proprio	UnitG	0	0	0	0	2	306	0	0
Generica 7091												

3	196-195-160-161	Vetro strutturale
3	197-196-161-162	Vetro strutturale
3	0-0-0	Vetro strutturale
3	167-166-181-182	Vetro strutturale
3	166-165-180-181	Vetro strutturale
3	0-0-176-177	Vetro strutturale
3	0-0-175-176	Vetro strutturale
3	0-0-171-172	Vetro strutturale
3	162-161-0-0	Vetro strutturale
3	0-200-0-0	Vetro strutturale
3	0-0-0-0	Vetro strutturale
3	161-160-0-0	Vetro strutturale
3	157-156-191-192	Vetro strutturale
3	0-0-0-0	Vetro strutturale
3	0-0-0-0	Vetro strutturale
3	156-155-190-191	Vetro strutturale
3	182-181-156-157	Vetro strutturale
4	41-192-197-43	Vetro strutturale
4	59-0-0-45	Vetro strutturale
4	37-182-157-27	Vetro strutturale
4	47-0-0-57	Vetro strutturale
4	33-172-187-39	Vetro strutturale
4	63-0-0-67	Vetro strutturale
4	53-0-0-59	Vetro strutturale
4	69-0-172-33	Vetro strutturale
4	39-187-167-31	Vetro strutturale
4	45-0-0-61	Vetro strutturale
4	31-167-182-37	Vetro strutturale
4	27-157-192-41	Vetro strutturale
4	49-0-177-35	Vetro strutturale
4	61-0-0-51	Vetro strutturale
4	57-0-0-49	Vetro strutturale
4	35-177-0-53	Vetro strutturale
4	51-0-0-55	Vetro strutturale
4	29-162-0-47	Vetro strutturale
4	43-197-162-29	Vetro strutturale
4	55-0-0-63	Vetro strutturale
5	58-57-49-50	Vetro strutturale
5	30-29-47-48	Vetro strutturale
5	52-51-55-56	Vetro strutturale
5	36-35-53-54	Vetro strutturale
5	50-49-35-36	Vetro strutturale
5	28-27-41-42	Vetro strutturale
5	32-31-37-38	Vetro strutturale
5	46-45-61-62	Vetro strutturale
5	42-41-43-44	Vetro strutturale
5	62-61-51-52	Vetro strutturale
5	70-69-33-34	Vetro strutturale
5	54-53-59-60	Vetro strutturale
5	34-33-39-40	Vetro strutturale
5	56-55-63-64	Vetro strutturale
5	64-63-67-68	Vetro strutturale
5	38-37-27-28	Vetro strutturale
5	48-47-57-58	Vetro strutturale
5	44-43-29-30	Vetro strutturale
5	40-39-31-32	Vetro strutturale
5	60-59-45-46	Vetro strutturale
6	389-64-68-393	Vetro strutturale
6	381-56-64-389	Vetro strutturale
6	379-54-60-385	Vetro strutturale
6	359-34-40-365	Vetro strutturale
6	367-42-44-369	Vetro strutturale
6	387-62-52-377	Vetro strutturale
6	353-28-42-367	Vetro strutturale
6	363-38-28-353	Vetro strutturale
6	377-52-56-381	Vetro strutturale
6	369-44-30-355	Vetro strutturale

6	383-58-50-375	Vetro strutturale
6	357-32-38-363	Vetro strutturale
6	375-50-36-361	Vetro strutturale
6	373-48-58-383	Vetro strutturale
6	371-46-62-387	Vetro strutturale
6	361-36-54-379	Vetro strutturale
6	385-60-46-371	Vetro strutturale
6	395-70-34-359	Vetro strutturale
6	365-40-32-357	Vetro strutturale
6	355-30-48-373	Vetro strutturale
7	386-385-371-372	Vetro strutturale
7	356-355-373-374	Vetro strutturale
7	396-395-359-360	Vetro strutturale
7	372-371-387-388	Vetro strutturale
7	384-383-375-376	Vetro strutturale
7	374-373-383-384	Vetro strutturale
7	364-363-353-354	Vetro strutturale
7	370-369-355-356	Vetro strutturale
7	376-375-361-362	Vetro strutturale
7	388-387-377-378	Vetro strutturale
7	354-353-367-368	Vetro strutturale
7	360-359-365-366	Vetro strutturale
7	378-377-381-382	Vetro strutturale
7	382-381-389-390	Vetro strutturale
7	366-365-357-358	Vetro strutturale
7	368-367-369-370	Vetro strutturale
7	358-357-363-364	Vetro strutturale
7	380-379-385-386	Vetro strutturale
7	390-389-393-394	Vetro strutturale
7	362-361-379-380	Vetro strutturale
8	335-358-364-336	Vetro strutturale
8	345-380-386-346	Vetro strutturale
8	334-366-358-335	Vetro strutturale
8	349-378-382-350	Vetro strutturale
8	350-382-390-351	Vetro strutturale
8	348-388-378-349	Vetro strutturale
8	337-354-368-338	Vetro strutturale
8	338-368-370-339	Vetro strutturale
8	343-376-362-344	Vetro strutturale
8	336-364-354-337	Vetro strutturale
8	347-372-388-348	Vetro strutturale
8	339-370-356-340	Vetro strutturale
8	340-356-374-341	Vetro strutturale
8	341-374-384-342	Vetro strutturale
8	333-360-366-334	Vetro strutturale
8	342-384-376-343	Vetro strutturale
8	344-362-380-345	Vetro strutturale
8	332-396-360-333	Vetro strutturale
8	346-386-372-347	Vetro strutturale
8	351-390-394-352	Vetro strutturale
9	0-0-0-0	Vetro strutturale
9	0-0-0-0	Vetro strutturale
9	0-0-0-0	Vetro strutturale
9	0-0-0-0	Vetro strutturale
9	0-0-0-0	Vetro strutturale
9	0-0-0-0	Vetro strutturale
9	0-0-0-0	Vetro strutturale
9	0-0-0-0	Vetro strutturale
10	0-71-75-0	Vetro strutturale
10	0-75-73-0	Vetro strutturale
10	0-77-65-0	Vetro strutturale
10	0-65-71-0	Vetro strutturale
10	69-77-0-0	Vetro strutturale
11	75-76-74-73	Vetro strutturale
11	65-66-72-71	Vetro strutturale

11	70-78-77-69	Vetro strutturale
11	71-78-66-65	Vetro strutturale
11	71-72-76-75	Vetro strutturale
12	66-391-397-72	Vetro strutturale
12	76-0-399-74	Vetro strutturale
12	78-0-391-66	Vetro strutturale
12	395-0-78-70	Vetro strutturale
12	72-397-0-76	Vetro strutturale
13	396-0-0-395	Vetro strutturale
13	391-392-398-397	Vetro strutturale
13	0-0-400-399	Vetro strutturale
13	0-0-392-391	Vetro strutturale
13	397-398-0-0	Vetro strutturale
14	392-330-329-398	Vetro strutturale
14	0-331-330-392	Vetro strutturale
14	0-328-327-400	Vetro strutturale
14	332-331-0-396	Vetro strutturale
14	398-329-328-0	Vetro strutturale

TABULATI DI VERIFICA

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Forze sismiche e masse
- Taglienti di piano
- Spostamenti Relativi dei nodi (SLD)
- Fattori di partecipazione e masse modali
- Massime tensioni sul terreno aste
- Massime reazioni vincolari
- Massime sollecitazioni travi
- Massime sollecitazioni pilastri
- Massime sollecitazioni aste generiche

Risultati Analisi Dinamica - Baricentri masse e masse	
Scenario di calcolo : Set NT_SLV_A2_STRGEO	

Combinazione masse 1						
Piano	Rigido	Massa	X	Y	Z	
		kg	cm	cm	cm	cm
0	No	0	0	0	0	0
1	No	87661	847	1402	1504	893
2	No	0	0	0	0	0
3	No	4770	330	1665		1188

Combinazione masse 2						
Piano	Rigido	Massa	X	Y	Z	
		kg	cm	cm	cm	cm
0	No	0	0	0	0	0
1	No	87661	903	1504		893
2	No	0	0	0	0	0
3	No	4770	364	1738		1188

Combinazione masse 3						
Piano	Rigido	Massa	X	Y	Z	
		kg	cm	cm	cm	cm
0	No	0	0	0	0	0
1	No	87661	847	1606		893
2	No	0	0	0	0	0

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Piano	Rigido	Massa	X	Y	Z
3	No	4770	330	1811	1188

Combinazione masse 4

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	0	0	0	0
1	No	87661	792	1504	893
2	No	0	0	0	0
3	No	4770	296	1738	1188

Taglienti di piano	
Scenario di calcolo : Set NT_SLV_A2_STRGEO	

I taglienti sono dati per combinazioni di calcolo C-S-Pm con C=Combinazione(1,2,...) S=Sisma(1,1l) Pm=posizione masse(1,2,...) Azioni compressive, riferite al sistema WCS,con origine in (0,0,0),i momenti sono comprensivi dei momenti di trasporto

$$\Theta = F_z \ast dr / (F_h \ast H)$$

con:

F_z=forza verticale,

dr=spost medio del piano rispetto al piano inferiore,

F_h=tagliante,

H=altezza del piano

Combinazione 12-1-1 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-32182	1943	62442	42762	-71123	11927	12472	13241	0	--
1	31449	7982	-90616	75524	-68241	57556	7909	15482	8258	0.002104
2	0	0	0	0	0	0	0	0	0	0.000000
3	3740	8570	-39804	79243	17756	109365	3378	17339	11880	0.004662

Piano	FxPil/Isol.	FyPil/Isol.	FzPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg
0	-29783	5191	0	0	0	0	0	-32182	1943
1	29783	-5191	0	0	0	0	0	31449	7982
2	0	0	0	0	0	0	0	0	0
3	3740	8570	0	0	0	0	0	3740	8570

Percentuali assorbite in direzione X

Piano	%dPil/Isol. FX	%dPar. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Percentuali assorbite in direzione Y

Piano	%dPil/Isol. FY	%dPar. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--
3	100.00	0.00	0.00

Combinazione 12-1-2 (SISMAX_SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
	kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
0	-29399	1161	62748	41660	-70177	57139	12472	13241	0	--
1	28518	7771	-91829	-13098	-16085	-40076	7909	15482	8258	0.002340
2	0	0	0	0	0	0	0	0	0	0.000000
3	-2647	9634	-41457	39341	34173	2327	3378	17339	11880	0.004604

Piano	FxPil/Isol.	FyPil/Isol.	FzPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg

838

Percentuali assorbite in direzione X									
Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-26661	5230	0	0	0	0	-29399	1161	
1	26661	-5230	0	0	0	0	28518	7771	
2	0	0	0	0	0	0	0	0	
3	-2647	9634	0	0	0	0	-2647	9634	

Percentuali assorbite in direzione X

Percentuali assorbite in direzione X									
Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-26661	5230	0	0	0	0	-29399	1161	
1	26661	-5230	0	0	0	0	28518	7771	
2	0	0	0	0	0	0	0	0	
3	-2647	9634	0	0	0	0	-2647	9634	

Percentuali assorbite in direzione Y

Percentuali assorbite in direzione Y									
Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-26661	5230	0	0	0	0	-29399	1161	
1	26661	-5230	0	0	0	0	28518	7771	
2	0	0	0	0	0	0	0	0	
3	-2647	9634	0	0	0	0	-2647	9634	

Combinazione 12-I-3 (SISMAX SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
0	-31222	962	63717	42357	-72060	47305	12472	13241	0	--
1	29361	9719	-84802	4256	-1668	-60577	7909	15482	8258	0.001882
2	0	0	0	0	0	0	0	0	0	0.000000
3	-2587	10502	-35258	-9876	35816	-33700	3378	17339	11880	0.003014

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-28428	5139	0	0	0	0	-31222	962	
1	28428	-5139	0	0	0	0	29361	9719	
2	0	0	0	0	0	0	0	0	
3	-2587	10502	0	0	0	0	-2587	10502	

Percentuali assorbite in direzione X

Percentuali assorbite in direzione X									
Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-28428	5139	0	0	0	0	-31222	962	
1	28428	-5139	0	0	0	0	29361	9719	
2	0	0	0	0	0	0	0	0	
3	-2587	10502	0	0	0	0	-2587	10502	

Percentuali assorbite in direzione Y

Percentuali assorbite in direzione Y									
Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-28428	5139	0	0	0	0	-31222	962	
1	28428	-5139	0	0	0	0	29361	9719	
2	0	0	0	0	0	0	0	0	
3	-2587	10502	0	0	0	0	-2587	10502	

Combinazione 12-I-4 (SISMAX SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
0	-32139	2260	59844	51850	-78849	25943	12472	13241	0	--
1	33253	7982	-85640	-4280	47147	5897	7909	15482	8258	0.001755
2	0	0	0	0	0	0	0	0	0	0.000000
3	-619	10467	-36846	21974	20161	16045	3378	17339	11880	0.003467

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-32139	2260	51850	-78849	25943	12472	13241	0	
1	29676	5739	0	0	0	0	-32139	2260	
2	0	0	0	0	0	0	0	0	
3	-619	10467	0	0	0	0	-619	10467	

Percentuali assorbite in direzione X

Percentuali assorbite in direzione X									
Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-26661	5230	0	0	0	0	-29399	1161	
1	26661	-5230	0	0	0	0	28518	7771	
2	0	0	0	0	0	0	0	0	
3	-2647	9634	0	0	0	0	-2647	9634	

Percentuali assorbite in direzione Y

Percentuali assorbite in direzione Y									
Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-26661	5230	0	0	0	0	-29399	1161	
1	26661	-5230	0	0	0	0	28518	7771	
2	0	0	0	0	0	0	0	0	
3	-2647	9634	0	0	0	0	-2647	9634	

Combinazione 13-I-1 (SISMAX SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
0	-26991	-16507	73836	137573	-77244	70909	12472	13241	0	--
1	7931	45371	-81784	76385	55040	-5391	7909	15482	8258	0.001246
2	0	0	0	0	0	0	0	0	0	0.000000
3	-20856	27928	-17904	43217	5577	20427	3378	17339	11880	0.000115

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-22241	-7422	0	0	0	0	-26991	-16507	
1	22241	7422	0	0	0	0	7931	45371	
2	0	0	0	0	0	0	0	0	
3	-20856	27928	0	0	0	0	-20856	27928	

Percentuali assorbite in direzione X

Percentuali assorbite in direzione X									
Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-22241	-7422	0	0	0	0	-26991	-16507	
1	22241	7422	0	0	0	0	7931	45371	
2	0	0	0	0	0	0	0	0	
3	-20856	27928	0	0	0	0	-20856	27928	

Percentuali assorbite in direzione Y

Percentuali assorbite in direzione Y									
Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-22241	-7422	0	0	0	0	-26991	-16507	
1	22241	7422	0	0	0	0	7931	45371	
2	0	0	0	0	0	0	0	0	
3	-20856	27928	0	0	0	0	-20856	27928	

Combinazione 13-I-2 (SISMAX SLV)

Piano	Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
0	-28006	-15406	73552	133736	-80165	65913	12472	13241	0	--
1	8195	44317	-81000	75869	46684	13016	7909	15482	8258	0.001248
2	0	0	0	0	0	0	0	0	0	0.000000
3	-20718	27912	-17356	47954	1284	42262	3378	17339	11880	0.000116

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-23319	-6645	0	0	0	0	-28006	-15406	
1	23319	6645	0	0	0	0	8195	44317	
2	0	0	0	0	0	0	0	0	
3	-20718	27912	0	0	0	0	-20718	27912	

Percentuali assorbite in direzione X

Percentuali assorbite in direzione X									
Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot	
0	-23319	-6645	0	0	0	0	-28006	-15406	
1	23319	6645	0	0	0	0	8195	44317	
2	0	0	0	0	0	0	0	0	
3	-20718	27912	0	0	0	0	-20718	27912	

Percentuali assorbite in direzione Y

Piano		%aPl/Isol. FY		%aPar. FY		%Shell. FY	
	0	100.00		0.00		0.00	0.00
	1	100.00		0.00		0.00	0.00
	2		--	--		--	--
	3	100.00		0.00		0.00	0.00

Combinazione 13-I-3 (SISMAY SLV)

Piano		Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
		kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
	0	-24768	-14140	75805	141739	-81612	62122	12472	13241	0	--
	1	8336	43959	-81523	37936	105851	-20536	7909	15482	8258	0.001185
	2	0	0	0	0	0	0	0	0	0	0.000000
	3	-15170	26603	-17291	36117	6312	-3268	3378	17339	11880	0.000122

Piano	FxPl/Isol.	FyPl/Isol.	FzPl/Isol.	FxPar	FyPar	FzPar	FxShell	FyShell	FzTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg	kg
	0	-20380	-6192	0	0	0	0	0	-24768	-14140
	1	20380	6192	0	0	0	0	0	8336	43959
	2	0	0	0	0	0	0	0	0	0
	3	-15170	26603	0	0	0	0	0	-15170	26603

Percentuali assorbite in direzione X

Piano		%aPl/Isol. FX		%aPar. FX		%Shell. FX	
	0	100.00		0.00		0.00	0.00
	1	100.00		0.00		0.00	0.00
	2		--	--		--	--
	3	100.00		0.00		0.00	0.00

Percentuali assorbite in direzione Y

Piano		%aPl/Isol. FY		%aPar. FY		%Shell. FY	
	0	100.00		0.00		0.00	0.00
	1	100.00		0.00		0.00	0.00
	2		--	--		--	--
	3	100.00		0.00		0.00	0.00

Combinazione 13-I-4 (SISMAY SLV)

Piano		Fx	Fy	Fz	Mx	My	Mz	X	Y	Z	Θ
		kg	kg	kg	kg*m	kg*m	kg*m	mm	mm	mm	
	0	-26662	-13114	72280	125892	-77161	77085	12472	13241	0	--
	1	11996	41949	-81270	13386	84038	-64521	7909	15482	8258	0.001238
	2	0	0	0	0	0	0	0	0	0	0.000000
	3	-14801	27699	-19753	7122	25295	195	3378	17339	11880	0.000136

Piano	FxPl/Isol.	FyPl/Isol.	FzPl/Isol.	FxPar	FyPar	FzPar	FxShell	FyShell	FzTot	FyTot
	kg	kg	kg	kg	kg	kg	kg	kg	kg	kg
	0	-22215	-4873	0	0	0	0	0	-26662	-13114
	1	22215	4873	0	0	0	0	0	11996	41949
	2	0	0	0	0	0	0	0	0	0
	3	-14801	27699	0	0	0	0	0	-14801	27699

Percentuali assorbite in direzione X

Piano		%aPl/Isol. FX		%aPar. FX		%Shell. FX	
	0	100.00		0.00		0.00	0.00
	1	100.00		0.00		0.00	0.00
	2		--	--		--	--
	3	100.00		0.00		0.00	0.00

Percentuali assorbite in direzione Y

Piano		%aPl/Isol. FY		%aPar. FY		%Shell. FY	
	0	100.00		0.00		0.00	0.00
	1	100.00		0.00		0.00	0.00
	2		--	--		--	--

Piano	3	%aPl/Isol. FY		%aPar. FY		%Shell. FY	
		100.00		0.00		0.00	0.00

Verifica Degli Spostamenti Relativi

Scenario di calcolo : **Set NT SLV_A2 STR/GEO**

Attenzione calcolo agli SLU. Gli spostamenti dovuti al sisma sono stati calcolati in via approssimata moltiplicando gli spostamenti derivanti dagli spettri al limite ultimo per il coefficiente c=Sd(T0)/Su(T0),dove T0 è il periodo fondamentale nella direzione considerata, Sd(T0) e Su(T0) il valore dello spettro in T0 rispettivamente di danno e ultimo

Combinazione	Spettro	
	SISMAX SLV	SISMAV SLV
	SpettroNI(q=1)	SpettroNI(q=1)
	c=0.426	c=0.417

Interp.	Comb.	ηXv mm	ηXh mm	ηYv mm	ηYh mm	Nodo1	Nodo2	η mm	ηAmm mm	Cs
0-1	(12+13)-III-3	2.87	1.82	0.91	0.23	1	54	4.69	12.00	2.56
0-1	(12+13)-I-3	3.38	1.95	0.79	0.19	2	53	5.33	12.00	2.25
0-1	(12+13)-I-3	3.61	1.90	0.77	0.19	3	55	5.52	12.00	2.17
0-1	(12+13)-III-3	3.55	1.63	0.81	0.22	4	56	5.18	12.00	2.32
0-1	(12+13)-III-4	3.53	1.58	0.85	1.40	5	71	5.11	12.00	2.35
0-1	(12+13)-III-4	3.50	1.45	0.90	1.41	6	74	4.94	12.00	2.43
0-1	(12+13)-III-3	3.41	1.28	0.95	0.22	7	76	4.69	12.00	2.56
0-1	(12+13)-III-3	3.44	1.23	1.01	0.23	8	75	4.66	12.00	2.57
0-1	(12+13)-III-3	3.15	1.13	1.04	0.22	9	72	4.28	12.00	2.80
0-1	(12+13)-III-4	3.14	1.09	1.10	1.36	10	70	4.22	12.00	2.84
0-1	(12+13)-III-4	3.15	1.09	1.18	1.34	11	69	4.24	12.00	2.83
0-1	(12+13)-VII-4	2.98	1.11	1.20	1.55	12	77	4.09	12.00	2.94
0-1	(12+13)-VII-4	3.03	1.31	1.30	2.16	13	78	4.34	12.00	2.77
0-1	(12+13)-VII-4	2.99	1.10	1.35	1.59	14	73	4.09	12.00	2.93
0-1	(12+13)-VI-4	2.89	1.27	1.39	2.17	15	61	4.16	12.00	2.88
0-1	(12+13)-VI-4	2.96	1.48	1.51	2.05	16	62	4.43	12.00	2.71
0-1	(12+13)-VI-4	2.87	1.67	1.54	1.94	17	63	4.54	12.00	2.64
0-1	(12+13)-VI-4	2.99	1.92	1.71	1.78	18	64	4.92	12.00	2.44
0-1	(12+13)-VI-4	2.95	1.66	1.75	2.02	19	60	4.60	12.00	2.61
0-1	(12+13)-VI-4	2.92	1.86	1.81	1.85	20	57	4.78	12.00	2.51
0-1	(12+13)-VI-4	2.99	2.00	1.96	1.70	21	59	4.99	12.00	2.41
0-1	(12+13)-VI-4	2.98	2.14	2.03	1.61	22	65	5.12	12.00	2.34
0-1	(12+13)-VI-4	2.96	2.30	2.07	1.04	23	58	5.26	12.00	2.28
0-1	(12+13)-VI-4	2.97	2.41	2.13	1.06	24	66	5.38	12.00	2.23
0-1	(12+13)-VI-4	2.84	2.62	1.94	0.85	25	67	5.46	12.00	2.20
0-1	(12+13)-VI-4	2.60	2.55	1.51	0.93	26	68	5.15	12.00	2.33
1-1	(12+13)-I-3	1.37	1.59	0.68	0.18	53	102	2.97	8.35	2.81
1-1	(12+13)-VI-4	1.14	0.60	0.74	2.27	54	101	3.01	8.35	2.77
1-1	(12+13)-I-3	1.60	1.58	0.65	0.19	55	103	3.19	8.35	2.62
1-1	(12+13)-VI-4	1.60	0.27	0.64	2.41	56	104	3.05	8.35	2.74
1-1	(12+13)-VI-4	1.47	1.82	0.69	1.92	57	120	3.29	8.35	2.54
1-1	(12+13)-VI-4	1.56	2.24	0.75	1.88	58	123	3.80	8.35	2.20
1-1	(12+13)-VI-4	1.53	2.01	0.74	1.76	59	121	3.54	8.35	2.36
1-1	(12+13)-VI-4	1.44	1.54	0.69	2.08	60	119	2.99	8.35	2.80
1-1	(12+13)-VI-4	1.34	1.21	0.59	2.23	61	115	2.82	8.35	2.96
1-1	(12+13)-VI-4	1.40	1.46	0.64	2.12	62	116	2.86	8.35	2.92
1-1	(12+13)-VI-4	1.36	1.68	0.61	1.96	63	117	3.04	8.35	2.75
1-1	(12+13)-VI-4	1.45	1.89	0.70	1.77	64	118	3.34	8.35	2.50
1-1	(12+13)-VI-4	1.56	2.12	0.76	1.66	65	122	3.68	8.35	2.27
1-1	(12+13)-VI-4	1.56	2.31	0.75	1.75	66	124	3.88	8.35	2.15
1-1	(12+13)-VI-4	1.44	2.47	0.57	1.77	67	125	3.91	8.35	2.14
1-1	(12+13)-VI-4	1.33	2.16	0.36	1.57	68	126	3.49	8.35	2.39
1-1	(12+13)-VI-4	1.46	0.85	0.61	2.40	69	111	3.01	8.35	2.77
1-1	(12+13)-VI-4	1.40	0.70	0.59	2.43	70	110	3.02	8.35	2.76
1-1	(12+13)-VI-4	1.61	0.11	0.64	2.43	71	105	3.07	8.35	2.72
1-1	(12+13)-VI-4	1.41	0.11	0.59	2.45	72	109	3.04	8.35	2.75
1-1	(12+13)-VI-4	1.39	0.93	0.61	2.34	73	114	2.95	8.35	2.83
1-1	(12+13)-VI-4	1.59	0.05	0.63	2.43	74	106	3.05	8.35	2.73
1-1	(12+13)-VI-4	1.58	0.02	0.60	2.45	75	108	3.05	8.35	2.74
1-1	(12+13)-VI-4	1.57	0.23	0.60	2.40	76	107	3.00	8.35	2.79
1-1	(12+13)-VI-4	1.35	1.07	0.58	2.30	77	112	2.88	8.35	2.90
1-1	(12+13)-VI-4	1.39	1.35	0.60	2.14	78	113	2.74	8.35	3.05

Interp.	Comb.	nXv	nXh	nYv	nYh	Nodo1	Nodo2	η	nAmm	Cs
2-3	(12+13)-III-4	0.23	0.33	0.03	0.07	1	327	0.56	3.00	5.35
2-3	(12+13)-III-3	0.18	0.36	0.02	0.04	2	328	0.54	3.00	5.57
2-3	(12+13)-I-4	0.22	0.35	0.02	0.05	3	329	0.57	3.00	5.30
2-3	(12+13)-I-3	0.22	0.31	0.02	0.01	4	330	0.55	3.00	5.45
2-3	(12+13)-III-3	0.23	0.31	0.01	0.01	5	331	0.54	3.00	5.54
2-3	(12+13)-III-3	0.23	0.30	0.00	0.00	6	332	0.52	3.00	5.73
2-3	(12+13)-III-4	0.23	0.30	0.02	0.01	7	333	0.54	3.00	5.60
2-3	(12+13)-III-3	0.23	0.30	0.03	0.05	8	334	0.52	3.00	5.75
2-3	(12+13)-III-3	0.22	0.25	0.04	0.05	9	335	0.47	3.00	6.44
2-3	(12+13)-III-3	0.21	0.23	0.05	0.06	10	336	0.45	3.00	6.73
2-3	(12+13)-III-3	0.22	0.22	0.06	0.07	11	337	0.44	3.00	6.82
2-3	(12+13)-III-3	0.21	0.21	0.07	0.08	12	338	0.41	3.00	7.24
2-3	(12+13)-VII-4	0.21	0.23	0.08	0.06	13	339	0.44	3.00	6.82
2-3	(12+13)-VII-3	0.20	0.22	0.10	0.12	14	340	0.42	3.00	7.19
2-3	(12+13)-V-3	0.19	0.20	0.10	0.11	15	341	0.39	3.00	7.69
2-3	(12+13)-V-3	0.19	0.20	0.12	0.12	16	342	0.39	3.00	7.75
2-3	(12+13)-V-3	0.18	0.20	0.12	0.13	17	343	0.37	3.00	8.02
2-3	(12+13)-V-4	0.17	0.21	0.14	0.09	18	344	0.39	3.00	7.76
2-3	(12+13)-V-3	0.17	0.18	0.15	0.17	19	345	0.35	3.00	8.63
2-3	(12+13)-V-3	0.16	0.17	0.15	0.16	20	346	0.32	3.00	9.30
2-3	(12+13)-VI-3	0.15	0.16	0.16	0.17	21	347	0.34	3.00	8.94
2-3	(12+13)-VI-3	0.14	0.16	0.17	0.19	22	348	0.36	3.00	8.38
2-3	(12+13)-VI-3	0.13	0.16	0.18	0.20	23	349	0.38	3.00	7.93
2-3	(12+13)-VI-3	0.13	0.16	0.18	0.22	24	350	0.40	3.00	7.54
2-3	(12+13)-VI-3	0.11	0.11	0.15	0.24	25	351	0.39	3.00	7.76
2-3	(12+13)-VI-3	0.13	0.14	0.19	0.23	26	352	0.42	3.00	7.07
Minimo										
1-1	(12+13)-VI-4	1.44	2.47	0.77	0.77	67	125	3.91	8.35	2.14

Periodi di vibrazione e Masse modali

Scenario di calcolo : Set_NT_S1V_A2_STR/GEO

Posizione masse 1

Numero di Frequenze calcolate =155, filtrate=74

N	T(s)	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2911	24.323	68.604	5802	46156	6.28	49.94
2(2)	0.1838	-55.714	3.216	30440	101	32.93	0.11
3(3)	0.1664	26.810	-32.924	7049	10630	7.63	11.50
4(4)	0.1564	6.927	-9.107	471	813	0.51	0.88
5(5)	0.1507	5.574	3.171	305	99	0.33	0.11
6(6)	0.1479	20.076	-0.414	3952	2	4.28	0.00
7(7)	0.1432	-5.484	-14.168	295	1969	0.32	2.13
8(8)	0.1420	-0.749	-7.808	6	598	0.01	0.65
9(10)	0.1363	9.264	0.134	842	0	0.91	0.00
10(11)	0.1332	-2.456	6.908	59	468	0.06	0.51
11(12)	0.1312	5.628	-0.514	311	3	0.34	0.00
12(13)	0.1286	13.172	-3.928	1702	151	1.84	0.16
13(14)	0.1272	-1.119	-3.294	12	106	0.01	0.12
14(15)	0.1256	-7.362	7.925	532	616	0.58	0.67
15(16)	0.1253	5.861	-8.174	337	655	0.36	0.71
16(22)	0.1170	-0.360	-4.272	1	179	0.00	0.19
17(27)	0.1119	0.639	-5.776	4	327	0.00	0.35
18(29)	0.1093	-5.892	-14.587	340	2087	0.37	2.26
19(30)	0.1084	-9.027	-21.986	799	4740	0.86	5.13
20(31)	0.1081	1.936	3.376	37	112	0.04	0.12
21(32)	0.1073	-3.592	-5.031	127	248	0.14	0.27
22(35)	0.1030	2.335	2.782	151	3.925	0.16	0.08
23(41)	0.0935	-2.341	-4.237	54	176	0.06	0.19
24(43)	0.0919	8.054	16.945	636	2816	0.69	3.05
25(44)	0.0869	0.861	-4.827	7	228	0.01	0.25
26(50)	0.0709	10.871	-1.558	1159	24	1.25	0.03
27(52)	0.0677	18.231	-4.471	3260	196	3.53	0.21
28(53)	0.0674	4.787	-3.381	225	112	0.24	0.12

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N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
		13.761	-8.043	1857	634	2.01	0.69
29(55)	0.0644	3.654	0.340	131	1	0.14	0.00
30(56)	0.0629	-3.644	3.767	130	139	0.14	0.15
31(57)	0.0617	-5.195	2.049	265	41	0.29	0.04
32(58)	0.0587	-15.936	-4.980	2490	243	2.69	0.26
33(59)	0.0578	-3.852	-0.022	145	0	0.16	0.00
34(63)	0.0540	-6.496	1.911	414	36	0.45	0.04
35(64)	0.0526	-5.228	1.564	268	24	0.29	0.03
36(65)	0.0520	-3.882	-1.158	13	148	0.01	0.16
37(66)	0.0518	5.529	-5.607	300	308	0.32	0.33
38(67)	0.0510	-5.879	10.635	339	1109	0.37	1.20
39(68)	0.0506	-7.615	2.025	569	40	0.62	0.04
40(69)	0.0497	2.824	-7.327	78	526	0.08	0.57
41(70)	0.0489	3.394	3.394	587	113	0.64	0.12
42(71)	0.0486	-2.681	4.710	268	70	0.29	0.08
43(72)	0.0481	-4.163	-4.710	170	218	0.18	0.24
44(73)	0.0477	2.322	2.322	2061	53	2.23	0.06
45(83)	0.0430	-4.637	-4.542	211	202	0.23	0.22
46(84)	0.0421	0.993	0.993	128	10	0.14	0.01
47(87)	0.0402	-0.264	-0.264	276	1	0.30	0.00
48(88)	0.0400	3.925	3.925	36	151	0.04	0.16
49(90)	0.0388	6.464	6.464	32	410	0.04	0.44
50(91)	0.0381	-1.818	10.745	2357	1132	2.55	1.22
51(92)	0.0378	3.303	1.626	107	26	0.12	0.03
52(93)	0.0376	4.991	0.253	244	1	0.26	0.00
53(94)	0.0373	4.119	-7.420	166	540	0.18	0.58
54(95)	0.0372	-7.428	3.405	541	114	0.59	0.12
55(96)	0.0367	-6.887	-0.987	465	10	0.50	0.01
61(126)	0.0297	-5.043	2.060	249	42	0.27	0.05
62(132)	0.0276	7.543	-5.189	558	264	0.60	0.29
63(133)	0.0275	4.446	-5.026	194	248	0.21	0.27
64(134)	0.0273	-4.765	2.736	223	73	0.24	0.08
65(135)	0.0273	4.446	-5.026	194	248	0.21	0.27
66(138)	0.0262	-3.634	-1.499	130	22	0.14	0.02
67(139)	0.0260	3.542	2.918	123	83	0.13	0.09
68(140)	0.0256	12.728	0.354	1589	1	1.72	0.00
69(141)	0.0251	7.273	-8.632	519	731	0.56	0.79
70(142)	0.0249	10.853	-3.087	1155	93	1.25	0.10
71(143)	0.0246	-3.743	3.523	137	122	0.15	0.13
72(150)	0.0236	-4.315	-1.004	183	10	0.20	0.01
73(151)	0.0232	4.726	0.396	219	2	0.24	0.00
74(155)	0.0225	-4.225	1.194	175	14	0.19	0.02
Somma delle Masse Modali [kgm*g]							
				81466	84180		
Masse strutturali libere [kgm*g]				92431	92431		
Percentuale				88.14	91.07	88.14	91.07

Posizione masse 2

Numero di Frequenze calcolate =155, filtrate=76

N	T(s)	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2913	30.588	65.666	9175	42286	9.93	45.75
2(2)	0.1789	55.796	-31.967	30530	10021	33.03	10.84
3(3)	0.1719	-23.327	-21.169	5336	4395	5.77	4.75
4(4)	0.1554	-7.930	5.070	7.930	252	0.67	0.27
5(6)	0.1426	9.499	-7.113	885	496	0.96	0.54
6(7)	0.1415	-9.239	-12.307	837	1485	0.91	1.61
7(8)	0.1392	10.090	-14.530	998	2071	1.08	2.24
8(9)	0.1377	1.642	-3.502	26	120	0.03	0.13
9(10)	0.1359	17.821	-0.037	3115	0	3.37	0.00
10(13)	0.1286	6.158	-3.368	372	111	0.40	0.12

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N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
11(14)	0.1284	3,226	102	0.11
12(15)	0.1276	-7,158	502	0.54
13(17)	0.1237	3,382	112	0.12
14(18)	0.1229	4,199	3,022	0.19
15(22)	0.1174	3,662	14	0.02
16(23)	0.1165	3,527	122	0.13
17(27)	0.1114	-3,974	147	0.16
18(28)	0.1100	4,274	24	0.03
19(30)	0.1085	-26,320	1220	1.32
20(37)	0.1009	-3,603	127	0.14
21(38)	0.0986	-4,140	168	0.18
22(40)	0.0959	-0,238	1	0.00
23(41)	0.0941	-4,635	20	0.02
24(42)	0.0936	-2,122	44	0.05
25(43)	0.0909	-7,553	560	0.61
26(51)	0.0695	-5,187	264	0.29
27(53)	0.0675	4,168	3583	3.88
28(54)	0.0671	10,326	1046	1.13
29(55)	0.0637	-1,910	560	0.61
30(56)	0.0625	-5,093	254	0.28
31(57)	0.0604	5,156	261	0.28
32(58)	0.0588	-5,450	291	0.32
33(60)	0.0576	7,002	481	0.52
34(61)	0.0555	-2,373	118	0.13
35(62)	0.0546	-4,243	177	0.19
36(63)	0.0541	-4,797	1834	0.24
37(67)	0.0501	15,669	0	0.00
38(68)	0.0498	-3,862	124	0.16
39(69)	0.0490	6,251	42	0.05
40(70)	0.0489	-2,080	383	0.05
41(71)	0.0484	-8,162	653	0.71
42(72)	0.0483	3,347	110	0.12
43(73)	0.0479	-5,943	346	0.37
44(74)	0.0476	7,411	539	0.58
45(85)	0.0411	-1,655	27	0.13
46(86)	0.0403	-3,470	118	0.13
47(87)	0.0401	0,905	117	0.01
48(88)	0.0400	-3,448	193	0.21
49(89)	0.0386	-12,409	1510	0.21
50(91)	0.0379	1,211	98	0.02
51(92)	0.0374	3,098	1401	1.52
52(93)	0.0369	-2,564	1447	1.57
53(94)	0.0366	4,811	1346	1.46
54(95)	0.0365	-1,704	227	0.25
55(96)	0.0359	-5,516	28	0.03
56(97)	0.0359	-1,384	298	0.02
57(99)	0.0355	6,655	19	0.02
58(100)	0.0354	-7,333	527	0.57
59(101)	0.0352	4,663	213	0.23
60(102)	0.0350	-4,037	160	0.17
61(103)	0.0348	2,287	6	0.01
62(111)	0.0331	-0,804	175	0.01
63(113)	0.0329	4,227	324	0.35
64(125)	0.0302	-5,748	9	0.01
65(128)	0.0290	-0,964	86	0.09
66(130)	0.0286	5,482	295	0.32
67(131)	0.0286	-0,017	159	0.17
68(134)	0.0273	4,022	734	0.79
69(139)	0.0256	-1,344	18	0.02
70(140)	0.0254	-3,371	480	0.52
71(141)	0.0254	3,182	5	0.01
72(142)	0.0249	-0,737	99	0.01
73(150)	0.0230	-12,618	1561	1.69
74(151)	0.0228	8,392	691	0.75
75(153)	0.0224	7,021	483	0.52
76(154)	0.0223	-4,479	286	0.31
		11,587	1317	1.42
		6,122	130	0.14
		-6,033	357	0.39
		-5,080	253	0.27
		4,033	203	0.22
		-4,549	159	0.22

N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
Somma delle Masse Modali [kgm*g]				
Masse strutturali libere [kgm*g]				
Percentuale				
			81,50	84,925
			9,2431	9,2431
			87,80	91,88

Posizione masse 3

Numero di Frequenze calcolate =155, filtrate=89

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2897	35.277	66.363	12204	43188	13.20	46.73
2(2)	0.1756	43.640	-31.370	18677	9650	20.21	10.44
3(3)	0.1607	-18.808	-8.797	3469	759	3.75	0.82
4(4)	0.1490	28.344	-14.884	7879	2173	8.52	2.35
5(5)	0.1475	15.166	2.108	2255	44	2.44	0.05
6(6)	0.1463	9.453	-18.984	876	3534	0.95	3.82
7(7)	0.1413	-3.894	3.121	149	96	0.16	0.10
8(8)	0.1401	7.651	9.456	574	877	0.62	0.95
9(9)	0.1379	-4.794	-1.777	225	31	0.24	0.03
10(10)	0.1366	12.984	0.498	1653	2	1.79	0.00
11(11)	0.1347	-5.285	4.203	274	173	0.30	0.19
12(12)	0.1342	-5.830	5.893	333	331	0.36	0.37
13(13)	0.1325	4.502	0.198	0	0	0.22	0.00
14(14)	0.1311	7.350	2.271	530	51	0.57	0.05
15(15)	0.1305	0.611	-3.292	4	106	0.00	0.12
16(16)	0.1278	7.217	0.185	511	0	0.55	0.00
17(17)	0.1241	-4.735	34	220	0.04	0.24	0.24
18(20)	0.1237	-5.249	-7.764	270	591	0.29	0.64
19(21)	0.1221	6.483	2.246	412	49	0.45	0.05
20(22)	0.1201	7.589	-1.530	565	23	0.61	0.02
21(23)	0.1191	-3.160	-3.914	98	150	0.11	0.16
22(28)	0.1122	-4.587	-1.878	206	35	0.22	0.04
23(30)	0.1094	-7.992	-6.378	626	399	0.68	0.43
24(31)	0.1084	10.392	25.816	1059	6536	1.15	7.07
25(35)	0.1044	-4.541	1.076	7	11	0.22	0.11
26(36)	0.1008	-0.817	-3.218	202	102	0.01	0.11
27(40)	0.0960	3.334	5.659	109	314	0.12	0.34
28(41)	0.0927	-6.812	-14.195	455	1976	0.49	2.14
29(42)	0.0910	-5.698	-2.427	318	220	0.34	0.24
30(43)	0.0898	-1.054	3.123	11	96	0.01	0.10
31(44)	0.0885	1.265	7.145	16	501	0.02	0.54
32(50)	0.0731	9.047	-5.991	803	352	0.87	0.38
33(51)	0.0710	-4.604	2.178	208	467	0.22	0.05
34(52)	0.0701	13.451	-6.887	1774	465	1.92	0.50
35(53)	0.0679	-18.062	8.649	3199	734	3.46	0.79
36(55)	0.0661	7.725	-4.047	585	161	0.63	0.17
37(58)	0.0598	4.682	-4.740	215	220	0.23	0.24
38(59)	0.0587	4.793	4.847	225	230	0.24	0.25
39(60)	0.0563	-8.694	11.252	741	1242	0.80	1.34
40(61)	0.0555	0.840	7.389	535	535	0.01	0.58
41(63)	0.0528	17.961	-9.135	3164	818	3.42	0.89
42(64)	0.0519	-10.346	-0.323	1050	1	1.14	0.00
43(65)	0.0514	5.525	-0.580	278	3	0.30	0.00
44(66)	0.0508	-0.548	3.212	3	101	0.00	0.11
45(67)	0.0507	4.540	0.647	202	4	0.22	0.00
46(69)	0.0497	-3.902	-2.427	149	58	0.16	0.06
47(70)	0.0493	8.981	-3.832	791	144	0.86	0.16
48(71)	0.0493	7.378	-4.320	534	183	0.58	0.20
49(72)	0.0484	3.420	-1.375	115	19	0.12	0.02
50(75)	0.0477	4.860	232	1.46	13	0.25	0.01
51(82)	0.0440	3.215	1.474	101	1.21	0.10	0.02
52(83)	0.0416	-2.708	7.030	72	485	0.08	0.52
53(84)	0.0416	-3.778	5.911	140	343	0.15	0.37
54(85)	0.0411	4.277	-2.823	179	78	0.19	0.08
55(86)	0.0408	3.210	7.874	101	608	0.11	0.66
0.0399		6.103	2.476	365	60	0.40	0.07

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
57(89)	0.0396	-3.507	4.296	121	181	0.13	0.20
58(90)	0.0391	18.491	-10.816	3353	1147	3.63	1.24
59(91)	0.0385	-6.434	0.125	406	0	0.44	0.00
60(92)	0.0381	-3.423	100	3.193	115	-3.423	0.11
61(93)	0.0378	-6.494	-3.100	414	94	0.45	0.10
62(95)	0.0375	-3.379	1.366	112	18	0.12	0.02
63(96)	0.0374	4.401	0.287	190	1	0.21	0.00
64(101)	0.0368	-0.6433	-3.809	4	142	0.00	0.15
65(102)	0.0366	-2.056	-3.188	41	100	0.04	0.11
66(103)	0.0364	-5.028	-5.954	248	348	0.27	0.38
67(104)	0.0362	-5.708	-7.860	320	606	0.35	0.66
68(105)	0.0362	2.328	4.678	53	215	0.06	0.23
69(106)	0.0361	2.123	-5.896	44	341	0.05	0.37
70(111)	0.0348	-0.928	-3.726	8	136	0.01	0.15
71(112)	0.0346	5.804	1.843	330	33	0.36	0.04
72(115)	0.0335	-4.397	-0.468	190	2	0.21	0.00
73(116)	0.0333	7.677	2.137	578	45	0.63	0.05
74(118)	0.0325	4.096	0.880	165	8	0.18	0.01
75(122)	0.0303	3.171	-1.300	99	17	0.11	0.02
76(130)	0.0276	-0.793	4.614	6	209	0.01	0.23
77(131)	0.0274	5.780	-6.149	328	371	0.35	0.40
78(133)	0.0271	6.891	-3.225	466	102	0.50	0.11
79(134)	0.0267	6.727	-1.166	444	13	0.48	0.01
80(135)	0.0265	6.590	-3.371	426	111	0.46	0.12
81(136)	0.0265	4.181	-1.369	171	18	0.19	0.02
82(138)	0.0258	6.306	-3.638	390	130	0.42	0.14
83(139)	0.0251	-1.189	8.815	1228	762	1.33	0.82
84(140)	0.0250	7.825	2.565	600	65	0.65	0.07
85(141)	0.0249	-4.880	-0.939	234	9	0.25	0.01
86(143)	0.0245	-1.137	1.488	148	0	0.16	0.00
87(152)	0.0224	8.180	-5.367	656	282	0.71	0.31
88(154)	0.0223	7.086	6.660	492	435	0.53	0.47
89(155)	0.0223	-3.425	1.384	115	19	0.12	0.02
Somma delle Masse Modali [kgm*g]							
Masse strutturali libere [kgm*g]				81913	85247		
Percentuale				92431	92431		
				88.62	92.23	88.62	92.23

Posizione masse 4

Numero di Frequenze calcolate = 155, filtrate=82

N	T(s)	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2895	29.369	69.385	8459	47212	9.15	51.08
2(2)	0.1737	50.480	-18.850	24990	3485	27.04	3.77
3(3)	0.1600	-2.257	-17.763	50	3094	0.05	3.35
4(4)	0.1481	27.163	-10.079	7236	996	7.83	1.08
5(5)	0.1472	-0.715	14.598	5	2090	0.01	2.26
6(6)	0.1466	25.391	-8.448	6322	700	6.84	0.76
7(7)	0.1438	-4.932	-5.714	239	320	0.26	0.35
8(8)	0.1403	2.448	10.042	59	989	0.06	1.07
9(9)	0.1371	10.071	1.897	995	35	1.08	0.04
10(10)	0.1351	6.266	-0.080	385	0	0.42	0.00
11(11)	0.1347	-5.011	12.052	19	1424	0.02	1.54
12(12)	0.1344	5.011	-5.459	246	292	0.27	0.32
13(13)	0.1317	6.825	-1.232	457	15	0.49	0.02
14(14)	0.1308	6.254	-2.023	384	40	0.41	0.04
15(16)	0.1278	-6.997	1.708	480	29	0.52	0.03
16(17)	0.1274	-0.244	-7.792	1	595	0.00	0.64
17(19)	0.1232	5.462	0.278	293	1	0.32	0.00
18(20)	0.1223	-0.036	-9.547	0	894	0.00	0.97
19(24)	0.1192	-4.906	1.911	236	36	0.26	0.04
20(25)	0.1171	3.089	1.208	94	14	0.10	0.02
21(27)	0.1145	-3.425	-0.379	115	1	0.12	0.00
22(28)	0.1139	1.777	-6.129	31	368	0.03	0.40
23(30)	0.1098	-6.472	-13.342	411	1746	0.44	1.89
847							

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
24(31)	0.1090	4.852	14.980	231	2201	0.25	2.38
25(32)	0.1082	8.816	18.854	762	3486	0.82	3.77
26(38)	0.0984	-3.635	-0.229	130	1	0.14	0.00
27(39)	0.0971	-1.320	1.111	17	95	0.02	0.10
28(41)	0.0943	1.381	5.907	19	342	0.02	0.37
29(42)	0.0935	4.101	9.289	165	846	0.18	0.92
30(43)	0.0914	-4.652	-12.124	212	1442	0.23	1.56
31(44)	0.0906	3.825	8.217	143	662	0.16	0.72
32(52)	0.0708	7.712	-3.164	583	98	0.63	0.11
33(53)	0.0698	23.363	-9.678	5353	918	5.79	0.99
34(54)	0.0674	-8.249	3.511	667	121	0.72	0.13
35(56)	0.0646	-4.294	2.166	181	46	0.20	0.05
36(57)	0.0638	-4.428	1.395	192	19	0.21	0.02
37(58)	0.0599	3.031	-7.478	548	90	0.59	0.10
38(59)	0.0562	-10.480	-4.652	1077	212	1.17	0.23
39(60)	0.0556	0.764	9.306	6	849	0.01	0.92
40(61)	0.0543	-8.420	3.442	695	116	0.75	0.13
41(62)	0.0530	5.612	0.336	309	1	0.33	0.00
42(63)	0.0529	-20.416	9.782	4088	938	4.42	1.02
43(64)	0.0519	-0.282	3.800	1	142	0.00	0.15
44(65)	0.0514	4.086	-5.125	164	258	0.18	0.28
45(71)	0.0493	10.200	-1.411	1020	20	1.10	0.02
46(72)	0.0489	-7.492	6.680	550	438	0.60	0.47
47(73)	0.0486	-4.430	-0.152	192	0	0.21	0.00
48(82)	0.0423	0.541	3.085	3	93	0.00	0.10
49(83)	0.0421	-2.182	-3.261	47	104	0.05	0.11
50(84)	0.0415	-3.349	-3.349	72	110	0.08	0.12
51(85)	0.0411	6.800	4.308	453	182	0.49	0.20
52(86)	0.0403	-1.148	-5.088	13	254	0.01	0.27
53(88)	0.0397	-10.277	8.769	1036	754	1.12	0.82
54(89)	0.0396	-7.412	0.261	539	1	0.58	0.00
55(90)	0.0389	15.875	-8.376	2471	688	2.67	0.74
56(91)	0.0389	-10.392	-2.259	1059	50	1.15	0.05
57(92)	0.0383	0.022	3.261	0	104	0.00	0.11
58(93)	0.0378	4.542	-3.746	202	138	0.22	0.15
59(94)	0.0377	-0.753	-3.402	6	113	0.01	0.12
60(96)	0.0374	3.209	-1.295	101	16	0.11	0.02
61(98)	0.0371	-3.416	0.891	114	8	0.12	0.01
62(99)	0.0370	0.811	5.102	6	255	0.01	0.28
63(102)	0.0366	1.897	3.728	35	136	0.04	0.15
64(103)	0.0364	0.247	6.256	1	384	0.00	0.42
65(104)	0.0363	5.801	8.195	330	659	0.36	0.71
66(105)	0.0362	-2.190	4.306	47	182	0.05	0.20
67(106)	0.0361	1.191	7.947	14	619	0.02	0.67
68(107)	0.0360	-2.034	3.146	41	97	0.04	0.10
69(111)	0.0345	-1.487	3.587	22	126	0.02	0.14
70(115)	0.0339	0.212	-3.411	0	114	0.00	0.12
71(117)	0.0333	-4.279	-2.448	180	59	0.19	0.06
72(118)	0.0331	-6.775	-1.805	450	32	0.49	0.03
73(127)	0.0285	-3.817	0.872	143	7	0.15	0.01
74(133)	0.0268	-8.993	0.652	793	4	0.86	0.00
75(134)	0.0267	3.850	-1.786	145	31	0.16	0.03
76(135)	0.0267	-8.395	5.008	691	246	0.75	0.27
77(136)	0.0266	-6.108	4.308	366	182	0.40	0.20
78(137)	0.0254	11.181	-3.979	1226	155	1.33	0.17
79(138)	0.0251	11.364	-4.083	1266	163	1.37	0.18
80(139)	0.0250	-0.296	-7.786	1	595	0.00	0.64
81(142)	0.0246	-3.294	0.525	106	3	0.12	0.00
82(155)	0.0222	-9.020	2.692	798	71	0.86	0.08
Somma delle Masse Modali [kgm*g]							
Masse strutturali libere [kgm*g]				81587	84454		
Percentuale				92431	92431		
				88.27	91.37	88.27	91.37

Risultati Analisi Dinamica - Massime tensioni sul terreno aste

Scenario di calcolo : Set NT SLV A2 STR/GEO									
Asta	N.in.	N.fin.	0/5	1/5	2/5	3/5	4/5	5/5	
			kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
9009	1	2	2.12(3)	2.05(3)	1.99(3)	1.93(3)	1.87(3)	1.82(3)	
9009	18	19	1.46(3)	1.46(3)	1.46(3)	1.46(3)	1.46(3)	1.45(3)	
9009	14	15	1.48(3)	1.48(3)	1.49(3)	1.48(3)	1.48(3)	1.48(3)	
9009	13	14	1.50(3)	1.50(3)	1.50(3)	1.49(3)	1.49(3)	1.48(3)	
9009	10	11	1.48(3)	1.48(3)	1.48(3)	1.48(3)	1.48(3)	1.48(3)	
9009	24	25	1.52(3)	1.54(3)	1.57(3)	1.60(3)	1.62(3)	1.63(3)	
9009	19	20	1.45(3)	1.45(3)	1.45(3)	1.44(3)	1.44(3)	1.43(3)	
9009	22	23	1.43(3)	1.44(3)	1.44(3)	1.45(3)	1.45(3)	1.45(3)	
9009	3	4	1.65(3)	1.62(3)	1.60(3)	1.57(3)	1.55(3)	1.53(3)	
9009	5	6	1.49(3)	1.49(3)	1.49(3)	1.49(3)	1.48(3)	1.48(3)	
9009	7	8	1.47(3)	1.47(3)	1.47(3)	1.47(3)	1.47(3)	1.46(3)	
9009	9	10	1.46(3)	1.47(3)	1.47(3)	1.47(3)	1.48(3)	1.48(3)	
9009	25	26	1.65(3)	1.69(3)	1.74(3)	1.79(3)	1.85(13-12)	1.95(13-12)	
9009	21	22	1.43(3)	1.43(3)	1.43(3)	1.43(3)	1.43(3)	1.43(3)	
9009	12	13	1.49(3)	1.49(3)	1.50(3)	1.50(3)	1.50(3)	1.50(3)	
9009	16	17	1.47(3)	1.47(3)	1.47(3)	1.47(3)	1.47(3)	1.46(3)	
9009	17	18	1.46(3)	1.47(3)	1.47(3)	1.47(3)	1.47(3)	1.46(3)	
9009	8	9	1.46(3)	1.47(3)	1.47(3)	1.47(3)	1.46(3)	1.46(3)	
9009	15	16	1.48(3)	1.48(3)	1.48(3)	1.48(3)	1.47(3)	1.47(3)	
9009	20	21	1.43(3)	1.43(3)	1.43(3)	1.43(3)	1.43(3)	1.43(3)	
9009	11	12	1.48(3)	1.49(3)	1.49(3)	1.49(3)	1.49(3)	1.49(3)	
9009	23	24	1.45(3)	1.46(3)	1.48(3)	1.49(3)	1.51(3)	1.52(3)	
9009	6	7	1.48(3)	1.48(3)	1.48(3)	1.48(3)	1.47(3)	1.47(3)	
9009	2	3	1.83(3)	1.78(3)	1.74(3)	1.71(3)	1.64(3)	1.64(3)	
9009	4	5	1.53(3)	1.52(3)	1.51(3)	1.51(3)	1.50(3)	1.49(3)	
9010	1	2	1.10(12-11)	1.06(12-11)	1.03(12-11)	1.00(12-11)	0.97(12-11)	0.94(12-11)	
9010	25	26	0.74(13-11-2)	0.70(13-11-2)	0.78(13-11-2)	0.81(13-11-2)	0.83(13-11-2)	0.86(13-11-2)	
9010	24	25	0.69(13-11-2)	0.70(13-11-2)	0.71(13-11-2)	0.72(13-11-2)	0.74(13-11-2)	0.74(13-11-2)	
9010	23	24	0.67(13-11-2)	0.68(13-11-2)	0.68(13-11-2)	0.69(13-11-2)	0.69(13-11-2)	0.69(13-11-2)	
9010	22	23	0.65(13-11-2)	0.66(13-11-2)	0.66(13-11-2)	0.66(13-11-2)	0.67(13-11-2)	0.67(13-11-2)	
9010	21	22	0.65(12-12)	0.65(12-12)	0.65(12-12)	0.65(12-12)	0.65(13-11-2)	0.65(13-11-2)	
9010	20	21	0.66(12-12)	0.66(12-12)	0.66(12-12)	0.66(12-12)	0.65(12-12)	0.65(12-12)	
9010	19	20	0.66(12-12)	0.66(12-12)	0.66(12-12)	0.66(12-12)	0.66(12-12)	0.66(12-12)	
9010	18	19	0.66(12-12)	0.66(12-12)	0.66(12-12)	0.66(12-12)	0.66(12-12)	0.66(12-12)	
9010	17	18	0.66(12-13)	0.66(12-13)	0.66(12-13)	0.66(12-13)	0.66(12-12)	0.66(12-12)	
9010	16	17	0.67(12-13)	0.67(12-13)	0.67(12-13)	0.67(12-13)	0.66(12-13)	0.66(12-13)	
9010	15	16	0.67(12-14)	0.67(12-14)	0.67(12-14)	0.67(12-14)	0.67(12-13)	0.67(12-13)	
9010	14	15	0.69(12-14)	0.69(12-14)	0.69(12-14)	0.69(12-14)	0.68(12-14)	0.67(12-14)	
9010	13	14	0.70(12-14)	0.70(12-14)	0.70(12-14)	0.70(12-14)	0.69(12-14)	0.69(12-14)	
9010	12	13	0.71(12-14)	0.71(12-14)	0.71(12-14)	0.70(12-14)	0.70(12-14)	0.70(12-14)	
9010	11	12	0.71(12-14)	0.71(12-14)	0.71(12-14)	0.71(12-14)	0.71(12-14)	0.71(12-14)	
9010	10	11	0.72(12-11)	0.72(12-11)	0.72(12-11)	0.72(12-14)	0.71(12-14)	0.71(12-14)	
9010	9	10	0.75(12-11)	0.75(12-11)	0.75(12-11)	0.74(12-11)	0.73(12-11)	0.72(12-11)	
9010	8	9	0.77(12-11)	0.77(12-11)	0.77(12-11)	0.76(12-11)	0.76(12-11)	0.75(12-11)	
9010	7	8	0.79(12-11)	0.79(12-11)	0.79(12-11)	0.79(12-11)	0.78(12-11)	0.77(12-11)	
9010	6	7	0.81(12-11)	0.81(12-11)	0.81(12-11)	0.81(12-11)	0.80(12-11)	0.79(12-11)	
9010	5	6	0.83(12-11)	0.83(12-11)	0.83(12-11)	0.83(12-11)	0.82(12-11)	0.81(12-11)	
9010	4	5	0.84(12-11)	0.84(12-11)	0.84(12-11)	0.84(12-11)	0.83(12-11)	0.83(12-11)	
9010	3	4	0.87(12-11)	0.86(12-11)	0.85(12-11)	0.85(12-11)	0.84(12-11)	0.84(12-11)	
9010	2	3	0.94(12-11)	0.92(12-11)	0.91(12-11)	0.89(12-11)	0.88(12-11)	0.86(12-11)	

Risultati Analisi Dinamica - Reazioni massime - Nodi

Scenario di calcolo : Set NT SLV A2 STR/GEO									
Nodo	Rx	Ry	Rz	Mx	My	Mz			
	kg	kg	kg	kg*m	kg*m	kg*m			
1	4319(13-11-4)	1927(13-11-4)		0	0	0			
1	-1387(13-11-1)	2038(13-11-1)		0	0	0			7(13-11-4)
2	3957(13-1-4)	702(6)		0	0	0			6(13-11-4)
2	-1817(2)	1972(13-11-1)		0	0	0			4(13-1-1)
3	2680(12-11-7)	865(13-11-4)		0	0	0			7(13-11-4)
3	-1750(2)	712(13-11-1)		0	0	0			0
4	2656(6)	901(13-11-4)		0	0	0			7(13-11-4)

4	-1716(2)	749(13-11-1)	0	0	0	0	0	0	0
5	-1712(2)	789(13-11-1)	0	0	0	0	0	0	0
5	2598(6)	667(13-11-4)	0	0	0	0	0	0	7(13-11-4)
6	-1706(2)	828(13-11-1)	0	0	0	0	0	0	-1(13-11-1)
6	2669(6)	532(13-11-4)	0	0	0	0	0	0	7(13-11-4)
7	4005(13-11-4)	-588(13-1-4)	0	0	0	0	0	0	7(13-11-4)
7	-1562(2)	2235(13-11-1)	0	0	0	0	0	0	0
8	4122(13-1-4)	-1100(13-1-4)	0	0	0	0	0	0	6(13-11-1)
8	-1725(2)	2192(13-11-1)	0	0	0	0	0	0	3(13-11-1)
9	2459(6)	-706(13-1-4)	0	0	0	0	0	0	6(13-11-4)
9	-1535(2)	888(13-11-1)	0	0	0	0	0	0	-1(13-11-1)
10	-1531(2)	884(13-11-1)	0	0	0	0	0	0	0
10	2445(6)	-784(13-1-4)	0	0	0	0	0	0	6(13-11-4)
11	-1531(2)	887(13-11-1)	0	0	0	0	0	0	0
11	2312(6)	-922(13-1-4)	0	0	0	0	0	0	6(13-11-4)
12	2366(6)	-899(13-1-4)	0	0	0	0	0	0	0
12	-1410(2)	878(13-11-1)	0	0	0	0	0	0	-1(13-11-1)
13	3505(13-11-4)	-1071(6)	0	0	0	0	0	0	6(13-11-4)
13	-1535(13-1-1)	1985(13-11-1)	0	0	0	0	0	0	0
14	3060(13-1-4)	-2296(13-1-4)	0	0	0	0	0	0	-6(13-1-4)
14	-1449(2)	2011(13-11-1)	0	0	0	0	0	0	0
15	2082(6)	-1373(13-1-4)	0	0	0	0	0	0	-6(13-1-4)
15	-1382(2)	955(13-11-1)	0	0	0	0	0	0	1(13-1-1)
16	-1416(2)	947(13-11-1)	0	0	0	0	0	0	0
16	2027(6)	-1326(13-1-4)	0	0	0	0	0	0	-6(13-1-4)
17	-1358(2)	928(13-11-1)	0	0	0	0	0	0	0
17	2020(6)	-1468(6)	0	0	0	0	0	0	-6(13-1-4)
18	-2048(13-1-1)	1715(13-11-1)	0	0	0	0	0	0	2(13-1-1)
18	3284(13-1-3)	-1864(13-11-3)	0	0	0	0	0	0	-6(13-1-4)
19	2390(13-1-4)	-304(13-1-4)	0	0	0	0	0	0	-6(13-1-4)
19	-1934(13-1-1)	1819(13-11-1)	0	0	0	0	0	0	-2(13-1-1)
20	1765(6)	-1804(6)	0	0	0	0	0	0	-6(13-1-3)
20	-1350(2)	1009(13-11-1)	0	0	0	0	0	0	2(13-1-1)
21	-1383(2)	1058(2)	0	0	0	0	0	0	0
21	1694(6)	-1939(6)	0	0	0	0	0	0	-6(13-1-3)
22	1599(6)	-2053(6)	0	0	0	0	0	0	-6(13-1-3)
22	-1350(2)	1085(2)	0	0	0	0	0	0	0
23	1559(6)	-2268(6)	0	0	0	0	0	0	-6(13-1-3)
23	-1274(2)	1086(2)	0	0	0	0	0	0	0
24	1418(13-1-2)	-2355(6)	0	0	0	0	0	0	-7(13-1-3)
24	-1282(13-1-2)	1153(2)	0	0	0	0	0	0	-1(13-11-1)
25	-2360(13-1-1)	1130(13-11-2)	0	0	0	0	0	0	-2(6)
25	2301(13-11-4)	-3189(13-11-4)	0	0	0	0	0	0	-6(13-1-4)
26	1515(13-1-4)	-4296(13-1-4)	0	0	0	0	0	0	-7(13-1-3)
26	-2392(13-1-2)	772(13-11-2)	0	0	0	0	0	0	-3(13-11-3)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Travi

Scenario di calcolo : Set NT SLV A2 STR/GEO									
Asta	N.in	N.fin	N	Tx	Ty	Tz	Mx	My	Mz
			kg	kg	kg	kg	kg*m	kg*m	kg*m
8000	0	0	-4732(13-1-4)	-137(12-1-1)	-660(8)	-660(8)	7(8)	-1438(8)	408(9)
			-4588(13-1-4)	-137(12-1-1)	-534(13-11-4)	-534(13-11-4)	7(8)	-2436(8)	424(8)
8000	0	0	-4553(13-1-4)	-100(13-1-4)	-552(12-1-1)	-552(12-1-1)	-12(13-1-1)	-2411(8)	469(8)
			-4443(13-1-4)	-100(13-1-4)	-441(12-1-1)	-441(12-1-1)	-12(13-1-1)	-2963(8)	579(8)
8000	0	0	-3382(13-1-4)	136(8)	707(13-1-1)	707(13-1-1)	-21(13-1-4)	-3278(8)	383(8)
	73	73	-3297(13-1-4)	136(8)	774(13-11-1)	774(13-11-1)	-21(13-1-4)	-3157(8)	200(8)
8000	0	0	-3501(13-1-4)	167(8)	-493(13-1-1)	-493(13-1-1)	5(12-1-1)	-3040(8)	588(8)
			-3524(13-1-4)	167(8)	439(13-11-1)	439(13-11-1)	5(12-1-1)	-3294(8)	341(8)
8000	0	0	-3012(10)	-246(8)	-246(8)	-943(8)	14(8)	1462(12-1-1)	-46(13-11-1)
			-2790(10)	-246(8)	-246(8)	-746(8)	14(8)	-1549(8)	374(9)
8000	73	73	-1949(13-11-1)	118(8)	988(13-11-4)	988(13-11-4)	-6(13-11-2)	-3190(8)	219(8)
	74	74	-1886(13-11-1)	118(8)	1105(13-11-4)	1105(13-11-4)	-6(13-11-2)	-2817(8)	79(9)
8000	74	74	-2041(13-1-1)	189(13-1-4)	842(13-11-4)	842(13-11-4)	11(13-11-4)	-2818(8)	98(9)
	399	399	-2203(13-1-1)	189(13-1-4)	961(13-11-4)	961(13-11-4)	11(13-11-4)	-2130(9)	-184(13-1-4)
			-3426(6)	278(13-11-1)	-1223(3)	-1223(3)	15(13-1-1)	2420(3)	-84(13-1-1)
8000	101	101	-3134(6)	278(13-11-1)	-1025(8)	-1025(8)	15(13-1-1)	1439(12-1-1)	-443(13-11-1)
	0	0							

8000	399	-4302(3-11-4)	151(3-11-4)	1017(12-1-1)	-24(3-11-1)	-217(0-9)	-166(13-1-4)
8000	400	-4297(3-11-4)	151(3-11-4)	1163(3)	-24(3-11-1)	1331(3-11-4)	-77(13-11-3)
8000	400	-4102(3-11-4)	-90(13-11-3)	2123(13-11-4)	19(13-11-4)	1354(13-11-4)	-71(13-11-3)
8001	327	-4137(3-11-4)	-90(13-11-3)	2245(13-11-4)	19(13-11-4)	1957(12-1-1)	37(8)
8001	0	-3560(3-11-4)	116(8)	713(12-1-1)	8(13-1-4)	-3537(8)	687(8)
8001	0	-3409(3-11-4)	116(8)	772(12-1-1)	8(13-1-4)	-3756(8)	515(8)
8001	0	-4749(3-11-4)	-122(3-11-1)	-933(12-1-1)	-13(13-1-1)	-260(0-8)	693(8)
8001	0	-4594(3-11-4)	-122(3-11-1)	-775(12-1-1)	-13(13-1-1)	-3688(8)	647(8)
8001	0	-3315(3-11-4)	273(13-1-4)	644(13-1-4)	-14(13-1-4)	-3733(8)	594(8)
8001	75	-3193(3-11-4)	273(13-1-4)	810(13-1-1)	-14(13-1-4)	-3457(8)	278(8)
8001	0	-4440(3-11-4)	101(13-11-4)	1201(12-1-1)	-25(13-11-4)	-2034(9)	61(9)
8001	0	-4431(13-1-1)	101(13-11-4)	1377(12-1-1)	-25(13-11-4)	1056(10)	-71(13-11-3)
8001	0	-5554(6)	-259(13-1-4)	-800(12-1-1)	10(13-1-4)	-1663(8)	457(9)
8001	0	-5072(6)	-259(13-1-4)	-646(12-1-1)	10(13-1-4)	-2729(8)	618(8)
8001	0	-6901(6)	-281(8)	-1355(3)	7(8)	1963(12-1-1)	-589(13-11-1)
8001	0	-6435(6)	-281(8)	-1006(3)	7(8)	-1765(8)	418(9)
8001	0	-4047(13-1-4)	-96(13-1-1)	1988(13-11-4)	20(13-1-4)	1043(10)	-38(13-11-1)
8001	328	-4099(13-1-4)	-96(13-1-1)	2168(13-11-1)	20(13-1-4)	2546(13-11-1)	49(13-11-1)
8001	75	-2895(12-1-1)	175(8)	897(13-1-4)	-6(13-11-3)	-3440(8)	356(8)
8001	76	-2804(12-1-1)	175(8)	1066(13-1-4)	-6(13-11-3)	-2896(9)	144(9)
8001	0	-2886(12-1-1)	154(13-1-4)	891(12-1-1)	12(13-11-4)	-2900(9)	208(9)
8001	0	-2831(12-1-1)	154(13-1-4)	1199(3)	12(13-11-4)	-1998(9)	-45(13-1-1)
8001	102	-7692(6)	286(13-11-1)	-1828(3)	4(12-11-1)	3748(3)	-66(12-11-1)
8002	0	-2227(6)	286(13-11-1)	-1492(3)	4(12-11-1)	1923(12-1-1)	-552(13-11-1)
8002	0	-6107(6)	-291(8)	-1443(3)	6(13-11-1)	2162(12-1-1)	-606(13-11-1)
8002	0	-5644(6)	-291(8)	-1096(3)	6(13-11-1)	-1712(8)	449(9)
8002	0	-3763(6)	114(8)	-733(12-1-1)	10(13-1-4)	-368(18)	670(8)
8002	0	-3393(6)	114(8)	745(12-1-1)	10(13-1-4)	-3850(8)	565(13-1-4)
8002	0	-3143(6)	356(13-1-4)	518(12-1-1)	-9(13-1-4)	-3825(8)	671(13-1-4)
8002	71	-2841(6)	356(13-1-4)	685(12-1-1)	-9(13-1-4)	-3527(8)	289(8)
8002	0	-5334(6)	-356(13-1-4)	-813(8)	10(13-1-4)	-168(18)	455(9)
8002	0	-4453(6)	-356(13-1-4)	-652(12-1-1)	10(13-1-4)	-2843(8)	645(13-1-1)
8002	0	-4845(6)	224(13-1-1)	-920(12-1-1)	-13(13-1-1)	-2802(8)	756(13-1-1)
8002	0	-4078(6)	224(13-1-1)	-762(12-1-1)	-13(13-1-1)	-3710(8)	638(8)
8002	71	-2722(12-1-1)	181(8)	493(12-1-1)	-6(13-11-2)	-3513(8)	365(8)
8002	72	-2631(12-1-1)	181(8)	865(6)	-6(13-11-2)	-2864(9)	143(8)
8002	37	-2721(12-1-1)	-195(13-11-4)	842(12-1-1)	12(13-11-4)	-1958(9)	207(8)
8002	392	-2666(12-1-1)	-195(13-11-4)	1205(3)	12(13-11-4)	-1958(9)	83(13-11-4)
8002	103	-6882(6)	221(13-11-1)	-1955(3)	5(13-11-4)	4206(3)	-169(13-11-1)
8002	397	-2661(12-1-1)	144(13-11-3)	1394(12-1-1)	-25(13-11-4)	-1983(9)	94(13-11-1)
8002	398	-2652(12-1-1)	144(13-11-3)	1573(12-1-1)	-25(13-11-4)	1101(10)	-67(13-11-4)
8002	398	-2980(6)	-83(13-11-1)	1873(12-1-1)	20(13-11-4)	1074(10)	-51(13-11-4)
8002	329	-3112(6)	-83(13-11-1)	2056(12-1-1)	20(13-11-4)	2758(12-1-1)	43(13-11-1)
8003	0	-4464(6)	183(13-1-1)	-878(12-1-1)	-11(13-1-1)	-2768(8)	668(8)
8003	0	-4090(6)	183(13-1-1)	-720(12-1-1)	-11(13-1-1)	-3684(8)	626(8)
8003	0	-6421(6)	-262(8)	-1419(3)	-7(13-1-1)	1998(12-1-1)	-534(13-11-1)
8003	0	-5960(6)	-262(8)	-1074(3)	-7(13-1-1)	-1733(8)	449(9)
8003	0	-3129(6)	313(13-1-4)	457(12-1-1)	-11(13-1-4)	-3808(8)	600(13-1-4)
8003	65	-2825(6)	313(13-1-4)	623(12-1-1)	-11(13-1-4)	-3520(8)	283(8)
8003	0	-3760(6)	115(8)	-702(12-1-1)	7(13-1-4)	-3655(8)	638(8)
8003	0	-3390(6)	115(8)	684(12-1-1)	7(13-1-4)	-3833(8)	503(13-1-4)
8003	0	-5365(6)	-286(13-1-4)	-810(8)	13(13-1-4)	-1653(8)	458(9)
8003	0	-4886(6)	-286(13-1-4)	-589(12-1-1)	13(13-1-4)	-2810(8)	596(8)
8003	65	-2675(6)	176(8)	435(3)	-5(13-11-2)	-3506(8)	360(8)
8003	66	-2447(6)	176(8)	855(6)	-5(13-11-2)	-2854(9)	154(13-1-4)
8003	66	-2513(12-1-1)	143(9)	778(3)	14(13-11-4)	-2858(9)	212(13-1-4)
8003	391	-2458(12-1-1)	143(9)	1206(3)	14(13-11-4)	-1957(9)	213(13-1-4)
8003	104	-72708(6)	194(13-11-1)	-1919(3)	4(13-11-4)	4125(3)	-152(13-11-1)
8003	0	-6751(6)	194(13-11-1)	-1588(3)	4(13-11-4)	1960(12-1-1)	-500(13-11-1)
8003	391	-2527(6)	225(13-1-4)	1309(12-1-1)	-27(13-11-4)	-1979(9)	232(13-1-4)
8003	392	-2506(6)	225(13-1-4)	1489(12-1-1)	-27(13-11-4)	1082(10)	-67(13-11-4)
8003	392	-2936(6)	-89(13-11-4)	1796(12-1-1)	20(13-1-4)	1054(10)	-80(13-11-4)
8003	330	-3070(6)	-89(13-11-4)	1980(12-1-1)	20(13-1-4)	2595(12-1-1)	42(13-11-4)
8004	0	-2970(6)	-81(13-11-1)	1751(12-1-1)	19(13-11-4)	1079(10)	-49(13-11-1)
8004	331	-3106(6)	-81(13-11-1)	1938(12-1-1)	19(13-11-4)	2607(12-1-1)	42(13-11-1)
8004	0	-4468(6)	-174(13-11-1)	-862(12-1-1)	-11(13-1-1)	-2789(8)	654(8)

	0	-4093(6)	-174(13-11-1)	-704(12-1-1)	-11(13-1-1)	-3720(8)	610(8)
8004	0	-3755(6)	116(8)	-668(12-1-1)	6(13-1-4)	-3689(8)	641(8)
8004	0	-3383(6)	116(8)	642(12-11-1)	6(13-1-4)	-3876(8)	491(13-1-4)
8004	0	-3110(6)	313(13-1-4)	422(12-11-1)	-10(13-1-4)	-3850(8)	588(13-1-4)
77	-2804(6)	313(13-1-4)	590(12-11-1)	-10(13-1-4)	-10(13-1-4)	-3565(8)	277(8)
8004	0	-6207(6)	-237(8)	-1427(3)	5(13-11-1)	2012(12-1-1)	-546(13-11-1)
0	-5748(6)	-237(8)	-1083(3)	5(13-11-1)	-1690(8)	-1690(8)	461(9)
8004	0	-5383(6)	-307(13-1-4)	-831(3)	9(13-1-4)	-1656(8)	467(9)
8004	0	-4904(6)	-307(13-1-4)	-595(12-1-1)	9(13-1-4)	-2832(8)	584(8)
8004	0	-2541(6)	138(13-11-1)	1312(12-1-1)	-25(13-11-4)	-1983(9)	91(13-11-1)
0	-2520(6)	138(13-11-1)	1493(12-1-1)	-25(13-11-4)	1109(10)	-62(13-11-3)	
8004	77	-2651(6)	171(8)	446(3)	-5(13-11-2)	-3551(8)	351(8)
78	-2421(6)	171(8)	870(6)		-5(13-11-2)	-2867(9)	142(8)
8004	78	-2433(6)	-191(13-11-4)	806(3)	12(13-11-4)	-2871(9)	204(8)
0	-2362(12-1-1)	-191(13-11-4)	1239(3)	12(13-11-4)	-1957(9)	83(13-11-4)	
8004	105	-6986(6)	191(13-11-1)	-1960(6)	3(13-11-4)	4268(3)	-166(13-11-1)
0	-6531(6)	191(13-11-1)	-1630(3)	3(13-11-4)	1975(12-1-1)	-510(13-11-1)	
8005	0	-3176(6)	339(13-1-4)	4121(12-11-1)	-9(13-1-4)	-3846(8)	647(13-1-4)
69	-2872(6)	339(13-1-4)	578(12-11-1)	-9(13-1-4)	-3542(8)	267(8)	
8005	0	-6266(6)	-233(8)	-1443(3)	6(13-11-1)	1895(12-1-1)	-551(13-11-1)
0	-5813(6)	-233(8)	-1104(3)	6(13-11-1)	-1724(8)	470(9)	
8005	0	-5450(6)	-332(13-1-4)	-825(3)	10(13-1-4)	-1690(8)	476(9)
0	-4976(6)	-332(13-1-4)	-549(12-1-1)	10(13-1-4)	-2859(8)	613(13-1-1)	
8005	0	-4533(6)	196(13-1-1)	-826(3)	-12(13-1-1)	-2817(8)	716(13-1-1)
0	-4161(6)	196(13-1-1)	-651(12-1-1)	-12(13-1-1)	-3741(8)	585(8)	
8005	0	-3824(6)	113(8)	-622(12-1-1)	9(13-1-4)	-3710(8)	614(8)
0	-3456(6)	113(8)	601(12-11-1)	9(13-1-4)	-3872(8)	541(13-1-4)	
8005	69	-2717(6)	162(8)	458(12-11-4)	-5(13-11-2)	-3528(8)	339(8)
70	-2488(6)	162(8)	877(6)		-2828(9)	140(8)	
8005	70	-2497(6)	-199(13-11-4)	809(3)	11(13-11-4)	-2831(9)	201(8)
395	-2358(6)	-199(13-11-4)	1240(3)	11(13-11-4)	-1925(9)	81(13-11-4)	
8005	106	-7040(6)	198(13-11-1)	-1989(3)	5(13-11-4)	4330(3)	-164(13-11-1)
0	-6593(6)	198(13-11-1)	-1665(3)	5(13-11-4)	1860(12-1-1)	-516(13-11-1)	
8005	395	-2606(6)	138(13-11-1)	1229(12-1-1)	-25(13-11-4)	-1951(9)	91(13-11-1)
396	-2585(6)	138(13-11-1)	1482(3)	-25(13-11-4)	1120(10)	-42(13-11-3)	
8005	396	-3034(6)	-81(13-11-1)	1645(12-1-1)	19(13-11-4)	1089(10)	-49(13-11-1)
332	-3169(6)	-81(13-11-1)	1831(12-1-1)	19(13-11-4)	2453(12-1-1)	421(13-11-1)	
8006	33	-2711(6)	180(8)	965(13-11-4)	-5(13-11-2)	-3448(8)	375(8)
34	-2480(6)	180(8)	1138(13-11-4)	-5(13-11-2)	-2691(9)	155(8)	
8006	34	-2493(6)	205(13-1-4)	873(13-11-4)	11(13-11-4)	-2696(9)	216(8)
359	-2353(6)	205(13-1-4)	1220(3)	11(13-11-4)	-1760(9)	-82(13-1-4)	
8006	107	-6746(6)	204(13-11-1)	-1966(3)	4(13-1-1)	4227(3)	-67(13-11-1)
168	-4250(13-1-4)	204(13-11-1)	-1636(3)	4(13-1-1)	1691(12-1-1)	-427(13-11-1)	
8006	168	-6290(6)	204(13-11-1)	-1636(3)	4(13-1-1)	1723(12-1-1)	-455(13-11-1)
168	-5952(6)	-205(8)	-1442(3)	-1442(3)	-5(13-1-1)	-1805(8)	478(9)
8006	169	-5491(6)	-205(8)	-1097(3)	-5(13-1-1)	-1805(8)	478(9)
8006	169	-5126(13-1-1)	-246(13-1-4)	-876(8)	8(13-1-4)	-1662(8)	499(9)
170	-4926(13-1-1)	-246(13-1-4)	-558(9)	8(13-1-4)	-2934(8)	586(8)	
8006	170	-4938(13-1-1)	-81(13-11-1)	-736(3)	-13(13-1-1)	-2890(8)	655(8)
171	-4782(13-1-1)	-81(13-11-1)	-545(12-1-1)	-13(13-1-1)	-3663(8)	609(8)	
8006	171	-4322(13-1-4)	120(8)	-582(12-1-1)	6(8)	-3735(8)	631(8)
360	-4241(13-11-4)	97(13-11-1)	1425(3)	-25(13-11-4)	1182(13-11-4)	-66(13-11-3)	
8006	360	-4008(13-11-4)	-83(13-11-1)	2177(13-11-4)	19(13-11-4)	1207(13-11-4)	-54(13-11-1)
333	-4062(13-11-4)	-83(13-11-1)	2364(13-1-4)	19(13-11-4)	2434(13-1-4)	39(13-11-3)	
8007	39	-2385(12-1-4)	148(8)	1000(13-1-4)	-5(13-11-2)	-3698(8)	326(8)
40	-2293(12-1-4)	148(8)	1171(13-1-4)	-5(13-11-2)	-3120(9)	366(8)	
8007	40	-2414(12-1-4)	201(13-1-4)	920(13-1-4)	11(13-11-4)	-3123(9)	205(8)
365	-2358(12-1-4)	201(13-1-4)	1299(3)	11(13-11-4)	-2200(9)	-85(13-1-4)	
8007	108	-8302(6)	188(13-11-1)	-1977(3)	3(13-1-1)	4319(3)	-80(13-11-2)
183	-7843(6)	188(13-11-1)	-1645(3)	3(13-1-1)	1650(12-1-1)	-414(13-11-1)	
8007	183	-7567(6)	-181(8)	-1418(3)	6(13-11-1)	1680(12-1-1)	-440(13-11-1)
184	-7104(6)	-181(8)	-1071(3)	6(13-11-1)	-1636(8)	474(9)	
8007	184	-5941(6)	-231(13-1-4)	-840(3)	9(13-1-4)	-1521(8)	509(9)
185	-5549(6)	-231(13-1-4)	-485(12-1-1)	-2661(8)	-1521(8)	567(8)	

8007	185	-5027(6)	-71(13-II-1)	-923(3)	-12(13-I-1)	-2620(8)	637(8)
8007	186	-4786(13-II-1)	-71(13-II-1)	-642(12-I-1)	-12(13-I-1)	-3714(8)	551(8)
8007	186	-3962(13-II-4)	113(9)	-632(12-I-4)	5(13-I-4)	-3549(8)	592(8)
8007	187	-3810(13-II-4)	113(9)	558(12-II-4)	5(13-I-4)	-3918(8)	440(13-I-4)
8007	187	-3738(13-II-4)	222(13-I-4)	584(13-I-1)	-12(13-I-4)	-3891(8)	522(13-I-4)
8007	39	-3614(13-II-4)	222(13-I-4)	751(13-I-1)	-12(13-I-4)	-3760(8)	253(8)
8007	365	-4445(13-I-4)	97(13-II-1)	1223(8)	-25(13-I-4)	-2235(9)	81(9)
8007	366	-4437(13-I-4)	97(13-II-1)	1618(3)	-25(13-I-4)	1236(13-I-4)	-65(13-II-3)
8007	366	-4193(13-I-4)	-90(13-II-1)	2157(13-I-4)	18(13-II-4)	1261(13-I-4)	-52(13-II-4)
8007	334	-4246(13-I-4)	-90(13-II-1)	2342(13-I-4)	18(13-II-4)	2489(13-II-1)	53(13-II-4)
8008	31	-2533(6)	152(8)	493(12-I-4)	-5(13-I-2)	-3512(8)	324(8)
8008	32	-2307(6)	152(8)	828(6)	-5(13-I-2)	-2870(9)	137(8)
8008	32	2361(12-II-4)	-202(13-II-4)	771(3)	11(13-I-4)	-2874(9)	197(8)
8008	357	-2307(12-II-4)	-202(13-II-4)	1194(3)	11(13-I-4)	-1988(9)	80(13-II-4)
8008	109	-6855(6)	175(13-II-1)	-1887(6)	6(13-II-4)	403(13)	-478(13-II-1)
8008	163	-6395(6)	175(13-II-1)	-1552(3)	6(13-II-4)	1520(12-I-1)	-180(13-II-1)
8008	163	-6095(6)	-203(8)	-1354(3)	6(13-II-1)	1548(12-I-1)	-516(13-II-1)
8008	164	-5632(6)	-203(8)	-1007(3)	6(13-II-1)	-1662(8)	517(9)
8008	164	-5268(6)	-320(13-I-4)	-792(3)	10(13-I-4)	-1629(8)	524(9)
8008	165	-4787(6)	-320(13-I-4)	-473(9)	10(13-I-4)	-2744(8)	595(13-I-1)
8008	165	-4348(6)	-185(13-II-1)	-814(3)	-12(13-I-1)	-2703(8)	692(13-I-1)
8008	166	-3974(6)	-185(13-II-1)	-544(12-I-4)	-12(13-I-1)	-3619(8)	549(8)
8008	166	-3633(6)	117(8)	-592(12-I-4)	8(13-I-4)	-3589(8)	576(8)
8008	167	-3264(6)	117(8)	556(12-II-4)	8(13-I-4)	-3800(8)	524(13-I-4)
8008	167	-2991(6)	326(13-I-4)	468(12-II-4)	-8(13-I-4)	-3774(8)	628(13-I-4)
8008	31	-2690(6)	326(13-I-4)	634(12-II-4)	-8(13-I-4)	-3526(8)	255(8)
8008	357	-2433(6)	134(13-II-1)	1061(12-I-4)	-25(13-I-4)	-2013(9)	88(13-II-1)
8008	358	-2412(6)	134(13-II-1)	1445(3)	-25(13-I-4)	1065(12-II-4)	-60(13-II-3)
8008	358	-2854(6)	-79(13-II-1)	1469(12-I-4)	18(13-II-4)	1056(12-II-4)	-48(13-II-1)
8008	335	-2985(6)	-79(13-II-1)	1651(12-I-4)	18(13-II-4)	2135(12-I-4)	41(13-II-1)
8009	37	-2541(6)	149(8)	493(12-II-4)	-4(13-II-2)	-3487(8)	319(8)
8009	38	-2316(6)	149(8)	829(6)	-4(13-II-2)	-2840(9)	136(8)
8009	38	-2332(6)	-194(13-II-4)	769(3)	12(13-II-4)	-2844(9)	196(8)
8009	363	-2246(12-II-4)	-194(13-II-4)	1190(3)	12(13-II-4)	-1964(9)	82(13-II-4)
8009	110	-6828(6)	166(13-II-1)	-1908(6)	2(8)	4068(3)	-125(13-II-1)
8009	178	-6073(6)	166(13-II-1)	-1571(3)	2(8)	1519(12-I-4)	-424(13-II-1)
8009	178	-5607(6)	-177(8)	-1019(3)	4(13-II-1)	1546(12-I-4)	-433(13-II-1)
8009	179	-5260(6)	-282(13-I-4)	-790(3)	8(13-I-4)	-1651(8)	546(9)
8009	180	-4777(6)	-282(13-I-4)	-473(9)	8(13-I-4)	-2768(8)	541(8)
8009	180	-4349(6)	150(13-I-1)	-805(3)	-10(13-I-1)	-2728(8)	606(8)
8009	181	-3973(6)	150(13-I-1)	-549(12-I-4)	-10(13-I-1)	-3629(8)	543(8)
8009	181	-3639(6)	120(8)	-582(12-I-4)	5(13-I-4)	-3599(8)	570(8)
8009	182	-3270(6)	120(8)	551(12-I-4)	5(13-I-4)	-3789(8)	456(13-I-4)
8009	182	-2999(6)	291(13-I-4)	454(12-I-4)	-9(13-I-4)	-3763(8)	549(13-I-4)
8009	37	-2697(6)	291(13-I-4)	620(12-II-4)	-9(13-I-4)	-3501(8)	252(8)
8009	363	-2446(6)	131(13-II-1)	1062(12-I-4)	-25(13-II-4)	-1989(9)	87(13-II-1)
8009	364	-2425(6)	131(13-II-1)	1435(3)	-25(13-II-4)	1078(12-II-4)	-58(13-II-1)
8009	364	-2865(6)	-77(13-II-4)	1447(12-I-4)	18(13-II-4)	1067(12-I-4)	-48(13-II-4)
8009	336	-2995(6)	-77(13-II-4)	1627(12-I-4)	18(13-II-4)	2152(12-I-4)	39(13-II-1)
8010	27	-2384(6)	146(8)	495(12-II-4)	-4(13-II-2)	-3529(8)	316(8)
8010	28	-2161(6)	146(8)	823(6)	-4(13-II-2)	-2883(9)	151(13-I-4)
8010	28	-2258(12-II-4)	140(9)	789(3)	14(13-II-4)	-2091(3-I-4)	209(13-I-4)
8010	353	-2204(12-II-4)	140(9)	1204(3)	14(13-II-4)	-1997(9)	-174(13-II-4)
8010	111	-7209(6)	-132(9)	-1937(3)	4(13-II-4)	4130(3)	-164(13-II-4)
8010	153	-6741(6)	-132(9)	-1598(3)	4(13-II-4)	1483(13-I-1)	-384(13-I-1)
8010	153	-6484(6)	-164(8)	-1373(3)	-8(13-I-1)	1509(12-I-4)	-409(13-II-1)
8010	154	-6017(6)	-254(13-I-4)	-1023(3)	-8(13-I-1)	-1700(8)	535(8)
8010	154	-5105(6)	-254(13-I-4)	-817(3)	13(13-I-4)	-1600(8)	556(9)
8010	155	-4622(6)	-254(13-I-4)	-487(9)	13(13-I-4)	-2746(8)	530(8)
8010	155	-4195(6)	150(13-I-1)	-817(3)	-9(13-I-1)	-2705(8)	594(8)
8010	156	-3821(6)	150(13-I-1)	-545(12-I-4)	-9(13-I-1)	-3617(8)	532(8)
8010	156	-3482(6)	120(8)	-590(12-I-4)	6(13-I-4)	-3588(8)	559(8)
8010	157	-3115(6)	120(8)	539(12-II-4)	6(13-I-4)	-3808(8)	455(13-I-4)
8010	157	-2840(6)	284(13-I-4)	456(12-I-4)	-9(13-I-4)	-3782(8)	547(13-I-4)
8010	27	-2540(6)	284(13-I-4)	620(12-I-4)	-9(13-I-4)	-3543(8)	249(8)
8010	353	-2293(12-II-4)	187(13-I-4)	1055(12-I-4)	-27(13-II-4)	-2017(9)	19(13-I-4)

	354	-2285(12-I-4)	187(13-I-4)	1472(3)	-27(13-I-4)	1088(12-II-4)	-62(13-II-1)
8010	354	-2691(6)	-93(13-II-4)	1492(12-I-4)	18(13-I-4)	1078(12-II-4)	-73(13-II-4)
8011	337	-2819(6)	-93(13-II-4)	1670(12-I-4)	18(13-I-4)	2163(12-I-4)	36(13-II-1)
8011	41	-2515(6)	138(8)	491(12-II-4)	-5(13-II-2)	-3424(8)	302(8)
8011	42	-2295(6)	138(8)	811(6)	-5(13-II-2)	-2792(9)	133(8)
8011	42	-2313(6)	-207(13-II-4)	750(3)	12(13-I-4)	-2796(9)	191(8)
8011	367	-2249(12-I-4)	-207(13-II-4)	1160(3)	12(13-I-4)	-1941(9)	80(13-II-4)
8011	112	-6739(6)	162(13-II-1)	-1875(6)	4(13-II-4)	3938(3)	-144(13-II-1)
8011	188	-6269(6)	162(13-II-1)	-1534(3)	4(13-II-4)	1477(12-I-4)	-434(13-II-1)
8011	188	-6006(6)	-176(13-II-1)	-1325(3)	5(13-II-1)	1502(12-I-4)	-464(13-II-1)
8011	189	-5538(6)	-176(13-II-1)	-974(3)	5(13-II-1)	-1706(8)	573(9)
8011	189	-5189(6)	-309(13-I-4)	-774(3)	9(13-I-4)	-1676(8)	580(9)
8011	190	-4706(6)	-309(13-I-4)	-451(9)	9(13-I-4)	-2750(8)	568(13-I-1)
8011	190	-4290(6)	-173(13-II-1)	-791(3)	-12(13-I-1)	-2711(8)	659(13-I-1)
8011	191	-3917(6)	-173(13-II-1)	-541(12-I-4)	-12(13-I-1)	-3580(8)	506(8)
8011	191	-3590(6)	120(9)	-582(12-I-4)	-8(13-I-4)	-3551(8)	531(8)
8011	192	-3224(6)	120(9)	543(12-II-4)	-8(13-I-4)	-3726(8)	501(13-I-4)
8011	192	-2961(6)	317(13-I-4)	456(12-II-4)	-8(13-I-4)	-3702(8)	602(13-I-4)
8011	41	-2665(6)	317(13-I-4)	620(12-II-4)	-8(13-I-4)	-3438(8)	238(8)
8011	367	-2432(6)	129(13-II-1)	1042(12-I-4)	-25(13-II-4)	-1966(9)	86(13-II-1)
8011	368	-2412(6)	129(13-II-1)	1391(3)	-25(13-II-4)	1065(12-II-4)	-57(13-II-1)
8011	368	-2838(6)	-79(13-II-4)	1434(12-I-4)	18(13-I-4)	1055(12-II-4)	-47(13-II-4)
8011	338	-2963(6)	-79(13-II-4)	1610(12-I-4)	18(13-I-4)	2100(12-I-4)	41(13-II-1)
8012	43	-2472(6)	146(8)	970(13-II-4)	5(13-I-2)	-3450(8)	329(8)
8012	44	-2254(6)	146(8)	1136(13-II-4)	5(13-I-2)	-2662(9)	150(8)
8012	44	-2361(12-I-4)	217(13-I-4)	881(13-II-4)	12(13-I-4)	-2669(9)	209(8)
8012	369	-2308(12-I-4)	217(13-I-4)	1235(3)	12(13-I-4)	-1701(9)	92(13-II-4)
8012	113	-6949(6)	199(13-II-1)	-1909(3)	-3(13-II-1)	4018(3)	80(8)
8012	193	-6475(6)	199(13-II-1)	-1567(3)	-3(13-II-1)	1440(12-I-4)	-349(13-II-1)
8012	193	-6196(6)	-146(8)	-1388(3)	-6(13-I-1)	1464(12-I-4)	-370(13-II-1)
8012	194	-5725(6)	-146(8)	-1036(3)	-6(13-I-1)	-1808(8)	579(8)
8012	194	-5141(13-I-1)	-191(13-I-4)	-866(8)	8(13-I-4)	-1618(8)	597(9)
8012	195	-4939(13-I-1)	-191(13-I-4)	-547(8)	8(13-I-4)	-2872(8)	536(8)
8012	195	-4943(13-I-1)	-75(13-II-1)	-764(3)	-11(13-I-1)	-2831(8)	601(8)
8012	196	-4788(13-I-1)	-75(13-II-1)	-523(12-I-4)	-11(13-I-1)	-3648(8)	519(8)
8012	196	-4702(13-I-4)	125(8)	-585(12-I-4)	5(8)	-3661(8)	549(8)
8012	197	-3952(13-I-4)	125(8)	533(12-I-4)	5(8)	-3791(8)	415(13-I-4)
8012	197	-3893(13-I-4)	-187(13-II-4)	588(13-II-3)	-12(13-I-4)	-3767(8)	492(13-I-4)
8012	43	-3773(13-I-4)	-187(13-II-4)	751(13-II-3)	-12(13-I-4)	-3348(8)	269(8)
8012	369	-4031(13-I-4)	104(13-II-3)	1186(13-I-3)	-25(13-II-4)	-1761(9)	89(8)
8012	370	-4023(13-I-4)	104(13-II-3)	1356(13-I-3)	-25(13-II-4)	1144(12-II-4)	-60(13-II-1)
8012	370	-3764(13-I-4)	-78(13-II-1)	2145(13-I-3)	17(13-II-4)	1147(13-II-3)	-49(13-II-1)
8012	339	-3814(13-I-4)	-78(13-II-1)	2318(13-I-3)	17(13-II-4)	2467(13-I-3)	39(13-II-1)
8013	29	-2248(12-I-4)	-134(13-II-4)	1016(13-I-4)	-5(13-I-2)	-3535(8)	288(9)
8013	30	-2160(12-I-4)	-134(13-II-4)	1181(13-I-4)	-5(13-I-2)	-3071(9)	141(9)
8013	30	-2266(12-I-4)	-212(13-II-4)	909(13-I-4)	-12(13-I-4)	-3073(9)	199(9)
8013	355	-2213(12-I-4)	-212(13-II-4)	1146(3)	-12(13-I-4)	-2263(9)	-83(13-I-4)
8013	114	-7741(6)	-191(13-I-1)	-191(13)	3(13-I-1)	4027(3)	65(9)
8013	158	-7263(6)	-191(13-I-1)	-1565(3)	3(13-I-1)	1407(12-I-4)	356(13-I-1)
8013	158	-7028(6)	-138(9)	-1344(3)	5(13-II-1)	1431(12-I-4)	378(13-I-1)
8013	159	-6554(6)	-138(9)	-989(3)	5(13-II-1)	-1673(8)	589(9)
8013	159	-5518(6)	210(13-II-4)	-777(3)	-6(13-I-4)	-1570(8)	624(8)
8013	160	-5033(6)	210(13-II-4)	-478(13-I-4)	-6(13-I-4)	-2606(8)	523(9)
8013	160	-4866(13-I-1)	93(8)	-826(3)	13(13-I-1)	-2567(8)	589(9)
8013	161	-4712(13-II-1)	93(8)	-524(12-I-4)	13(13-II-1)	-3529(8)	-488(13-II-4)
8013	161	-4710(13-II-4)	103(9)	-586(12-I-4)	-6(13-II-4)	-3410(8)	490(9)
8013	162	-3961(13-I-4)	103(9)	524(12-II-4)	-6(13-II-4)	-3750(8)	-426(13-II-4)
8013	162	-3888(13-I-4)	196(13-I-4)	611(13-I-4)	12(13-I-4)	-3725(8)	-502(13-II-4)
8013	29	-3768(13-I-4)	196(13-I-4)	773(13-I-4)	12(13-I-4)	-3633(8)	-253(13-II-4)
8013	355	-4235(13-I-4)	-102(13-I-1)	1187(13-II-4)	25(13-I-4)	-2271(9)	85(9)
8013	356	-4227(13-I-4)	-102(13-I-1)	1539(3)	25(13-I-4)	1207(13-I-4)	61(13-I-1)
8013	356	-3959(13-I-4)	78(13-I-1)	2233(13-I-4)	-17(13-I-4)	1234(13-I-4)	30(13-I-1)
8013	340	-4008(13-I-4)	78(13-I-1)	2	-17(13-I-4)	2487(13-II-4)	-37(13-I-1)
8014	0	-3480(6)	126(8)	-531(12-I-4)	-8(13-I-4)	-3551(8)	504(9)
8014	0	-3119(6)	126(8)	497(12-II-4)	-8(13-I-4)	-3761(8)	-508(13-II-4)
8014	0	-4180(6)	-177(13-II-1)	-801(3)	11(13-II-1)	-2676(8)	-659(13-II-4)
8014	0	-3579(6)	-177(13-II-1)	-497(12-I-4)	11(13-II-1)	-3579(8)	480(9)

8014	0	-2847(6)	-324(13-II-4)	406(12-II-4)	8(13-II-4)	-3735(8)	-610(13-II-4)
47	-2556(6)	-324(13-II-4)	567(12-II-4)	8(13-II-4)	-3498(8)	230(9)	
8014	0	-5926(6)	171(13-I-1)	-1322(3)	-6(13-I-1)	1414(12-I-4)	464(13-I-1)
8014	0	-5451(6)	171(13-I-1)	-966(3)	-6(13-I-1)	-1639(8)	640(8)
8014	0	-5697(6)	303(13-II-4)	-785(3)	-9(13-II-4)	-1608(8)	648(8)
8014	0	-4607(6)	303(13-II-4)	-470(9)	-9(13-II-4)	-2716(8)	-567(13-I-1)
8014	47	-2399(6)	131(9)	443(12-II-4)	5(13-I-2)	-3484(8)	292(9)
8014	48	-2185(6)	131(9)	802(6)	5(13-I-2)	-2865(9)	131(9)
8014	48	-2202(6)	209(13-I-4)	765(3)	-12(13-I-4)	-2869(9)	187(9)
373	-2079(12-II-3)	209(13-I-4)	1159(3)	-12(13-I-4)	-1994(9)	-80(13-I-4)	-80(13-I-4)
8014	115	-6682(6)	-172(8)	-1853(6)	-4(13-I-4)	391(63)	141(13-I-1)
8014	0	-6201(6)	-172(8)	-1504(3)	-4(13-I-4)	1390(12-I-4)	435(13-I-1)
8014	373	-2319(6)	-130(13-I-1)	1004(3)	25(13-I-4)	-2020(9)	-86(13-I-1)
374	-2300(6)	-130(13-I-1)	1405(3)	25(13-I-4)	1022(10)	58(13-I-1)	
8014	374	-2738(6)	76(13-I-4)	1325(12-I-4)	-18(13-I-4)	994(10)	48(13-I-1)
341	-2856(6)	76(13-I-4)	1492(12-I-4)	-18(13-I-4)	1989(12-I-4)	-38(13-I-1)	
8015	0	-2811(6)	-298(13-II-4)	402(12-II-3)	10(13-II-4)	-3756(8)	-560(13-II-4)
8015	57	-2522(6)	-298(13-II-4)	562(12-II-3)	10(13-II-4)	-3504(8)	231(9)
8015	0	-6504(6)	-116(9)	-1373(3)	7(13-II-1)	1406(12-I-3)	421(13-I-2)
8015	0	-6027(6)	-116(9)	-1016(3)	7(13-II-1)	-1729(8)	614(8)
8015	0	-5043(6)	264(13-II-4)	-807(3)	-12(13-II-4)	-1616(8)	656(8)
8015	0	-4557(6)	264(13-II-4)	-483(9)	-12(13-II-4)	-2752(8)	-510(13-II-1)
8015	0	-4141(6)	158(13-I-1)	-801(3)	9(13-II-1)	-2713(8)	-591(13-II-1)
8015	0	-3769(6)	158(13-I-1)	-496(12-I-3)	9(13-II-1)	-3609(8)	475(9)
8015	0	-3441(6)	126(9)	-525(12-I-3)	-6(13-II-4)	-3580(8)	499(9)
8015	0	-3081(6)	126(9)	486(12-II-3)	-6(13-II-4)	-3781(8)	-466(13-II-4)
8015	57	-2364(6)	132(9)	449(12-I-3)	4(13-I-2)	-2854(9)	293(9)
8015	58	-2153(6)	132(9)	811(6)	4(13-I-2)	-2854(9)	-151(13-II-4)
8015	58	-2168(6)	142(8)	784(3)	-15(13-I-4)	-2858(9)	-210(13-II-4)
8015	383	-2043(6)	142(8)	1172(3)	-15(13-I-4)	-1979(9)	-155(13-II-4)
8015	116	-7233(6)	-198(8)	-1934(3)	-4(13-I-4)	4073(3)	153(13-I-1)
8015	0	-6749(6)	-198(8)	-1584(3)	-4(13-I-4)	1383(12-I-3)	407(8)
8015	383	-2226(6)	-177(13-II-4)	1024(3)	27(13-I-4)	-2000(9)	-173(13-II-4)
8015	384	-2208(6)	-177(13-II-4)	1416(3)	27(13-I-4)	1043(10)	61(13-I-1)
8015	384	-2655(6)	92(13-I-4)	1343(12-I-3)	-18(13-II-4)	1013(10)	701(13-I-4)
8015	342	-2771(6)	92(13-I-4)	1507(12-I-3)	-18(13-II-4)	2004(12-I-3)	-37(13-I-1)
8016	0	-5999(6)	173(13-I-1)	-1350(3)	-6(13-I-1)	1441(12-I-3)	486(13-I-2)
8016	0	-5518(6)	173(13-I-1)	-990(3)	-6(13-I-1)	-1734(8)	678(8)
8016	0	-5180(6)	316(13-II-4)	-774(3)	-10(13-II-4)	-1704(8)	686(8)
8016	0	-4692(6)	316(13-II-4)	-450(9)	-10(13-II-4)	-2777(8)	-573(13-II-1)
8016	0	-4274(6)	179(13-I-1)	-780(3)	11(13-II-1)	-2738(8)	-669(13-II-4)
8016	0	-3903(6)	179(13-I-1)	-501(12-I-3)	11(13-II-1)	-3595(8)	-461(13-II-4)
8016	0	-3568(6)	125(9)	-530(12-I-3)	-8(13-II-4)	-3566(8)	-509(13-II-4)
8016	0	-3210(6)	125(9)	498(12-II-3)	-8(13-II-4)	-3729(8)	-521(13-II-4)
8016	0	-2941(6)	-331(13-II-4)	417(12-I-3)	9(13-II-4)	-3704(8)	-624(13-II-4)
8016	49	-2655(6)	-331(13-II-4)	576(12-II-3)	9(13-II-4)	-3429(8)	222(9)
8016	49	-2493(6)	125(9)	458(12-II-3)	5(13-I-1)	-3414(8)	282(9)
8016	50	-2284(6)	125(9)	807(6)	5(13-I-1)	-2781(9)	128(9)
8016	50	-2299(6)	210(13-I-4)	765(3)	-13(13-I-4)	-2790(9)	-188(13-II-4)
8016	375	-2175(6)	210(13-I-4)	1148(3)	-13(13-I-4)	-1933(9)	-81(13-I-4)
8016	117	-6735(6)	-197(8)	-1904(6)	-5(13-I-4)	3978(3)	152(13-I-1)
8016	0	-6265(6)	-197(8)	-1548(3)	-5(13-I-4)	1416(12-I-3)	457(13-I-1)
8016	375	-2429(6)	-133(13-I-1)	987(12-I-3)	25(13-I-4)	-1959(9)	-87(13-I-1)
8016	376	-2411(6)	-133(13-I-1)	1366(3)	25(13-I-4)	1032(10)	591(13-I-1)
8016	376	-2835(6)	77(13-I-4)	1338(12-I-3)	-18(13-I-4)	1003(10)	49(13-I-4)
8016	343	-2948(6)	77(13-I-4)	1500(12-I-3)	-18(13-I-4)	2007(12-I-3)	-38(13-I-1)
8017	35	-2456(13-II-3)	127(9)	1044(13-II-4)	6(13-I-1)	-3541(8)	300(9)
8017	36	-2371(13-II-3)	127(9)	1202(13-II-4)	6(13-I-1)	-2674(9)	144(8)
8017	36	-2513(13-II-3)	-211(13-II-4)	957(13-II-4)	-13(13-I-4)	-2681(9)	201(9)
8017	361	-2464(13-II-3)	-211(13-II-4)	1311(3)	-13(13-I-4)	1820(13-II-3)	115(13-II-4)
8017	118	-7653(6)	-205(8)	-1958(6)	-4(13-I-2)	4152(3)	102(8)
8017	173	-7159(6)	-205(8)	-1601(3)	-4(13-I-2)	473(8)	473(8)
8017	173	-6882(6)	118(13-I-2)	-1419(3)	-5(13-I-2)	1445(12-I-3)	482(8)
8017	174	-6399(6)	118(13-I-2)	-1057(3)	-5(13-I-2)	-1790(8)	683(8)
8017	174	-5209(13-I-1)	241(13-II-4)	-897(8)	-6(13-I-4)	-1584(8)	706(8)
8017	175	-5006(13-I-1)	241(13-II-4)	-574(8)	-6(13-I-4)	-2891(8)	505(9)
8017	175	-4989(13-I-1)	83(9)	-839(3)	15(13-II-4)	-2848(8)	567(9)

	176	-4835(13-I-1)	83(9)	-556(12-I-3)	15(13-I-4)	-3769(8)	-543(13-II-4)
8017	176	-4049(13-I-4)	119(8)	-568(12-I-3)	-7(13-I-4)	-3707(8)	-560(13-II-4)
8017	177	-3902(13-I-4)	119(8)	492(12-I-3)	-7(13-I-4)	-3883(8)	-474(13-II-4)
8017	177	-3861(13-I-4)	-135(13-II-4)	636(13-II-3)	11(13-I-4)	-3857(8)	-550(13-II-4)
8017	35	-3744(13-I-4)	-135(13-II-4)	794(13-II-3)	11(13-I-4)	-3445(8)	-381(13-II-4)
8017	361	-4223(13-I-3)	-111(13-I-3)	1290(13-I-3)	25(13-I-4)	-1715(9)	94(13-I-4)
362	4216(13-I-3)	-111(13-I-3)	1448(13-I-3)	25(13-I-4)	1208(13-I-3)	65(13-I-4)	
8017	362	-3927(13-I-3)	81(13-I-1)	2265(13-I-3)	-18(13-I-4)	1235(13-I-3)	52(13-I-1)
344	-3973(13-I-3)	81(13-I-1)	2423(13-I-3)	-18(13-I-4)	2620(13-I-3)	-39(13-I-1)	
8018	0	-4068(13-I-1)	100(8)	-755(3)	12(13-I-1)	-2649(8)	556(9)
8018	0	-4454(13-I-1)	100(8)	-442(12-I-3)	12(13-I-1)	-3518(8)	-468(13-I-4)
8018	0	-4067(13-I-4)	121(9)	-482(12-I-3)	-5(13-I-4)	-3488(8)	456(9)
8018	0	-3920(13-I-4)	121(9)	457(12-I-3)	-5(13-I-4)	-3759(8)	-450(13-I-4)
8018	0	-3850(13-I-4)	-188(13-II-4)	623(13-I-4)	14(13-I-4)	-3752(8)	-529(13-I-4)
53	-3734(13-I-4)	-188(13-II-4)	779(13-I-4)	14(13-I-4)	-3585(8)	-280(13-I-4)	
8018	0	-6670(6)	112(13-I-2)	-1407(3)	5(13-I-2)	1392(12-I-3)	515(8)
0	-6186(6)	112(13-I-2)	-1045(3)	5(13-I-2)	-1723(8)	718(8)	
8018	0	-5166(6)	239(13-I-4)	-798(3)	-8(13-I-4)	-1618(8)	718(8)
0	-4676(6)	239(13-I-4)	-501(13-I-3)	-2698(8)	-8(13-I-4)	494(9)	
8018	53	-2251(6)	-158(13-II-4)	1009(13-I-4)	-5(13-I-1)	-3481(8)	-286(13-I-4)
54	-2151(13-I-4)	-158(13-II-4)	1165(13-I-4)	-3045(9)	-5(13-I-1)	137(9)	
8018	54	-2298(13-I-4)	-252(13-II-4)	892(13-I-3)	-12(13-I-4)	-3046(9)	192(9)
379	-2248(13-I-4)	-252(13-II-4)	1083(3)	-12(13-I-4)	-2285(9)	132(13-I-4)	
8018	119	-7438(6)	-230(8)	-1957(6)	-3(13-I-2)	4142(3)	128(13-I-1)
0	-6947(6)	-120(13-I-4)	-1602(3)	-3(13-I-2)	1368(12-I-3)	505(8)	
8018	379	-4257(13-I-4)	-120(13-I-4)	1220(13-II-3)	25(13-I-4)	-2269(9)	66(13-I-4)
380	-4250(13-I-4)	-120(13-I-4)	1522(3)	25(13-I-4)	1215(13-I-4)	104(13-I-4)	
8018	380	-3977(13-I-4)	81(13-I-1)	2298(13-II-4)	-18(13-I-4)	1243(13-I-4)	52(13-I-1)
345	-4022(13-I-4)	81(13-I-1)	2455(13-II-4)	-18(13-I-4)	2538(13-I-4)	-40(13-I-1)	
8019	0	-3655(6)	126(9)	-472(12-I-3)	-8(13-I-4)	-3636(8)	-549(13-I-4)
0	-3302(6)	126(9)	445(12-I-3)	-8(13-I-4)	-3840(8)	-543(13-I-4)	
8019	0	-6171(6)	176(13-I-2)	-1378(3)	-6(13-I-1)	1419(12-I-3)	526(8)
0	-5697(6)	176(13-I-2)	-1024(3)	-6(13-I-1)	-1655(8)	739(8)	
8019	0	-5318(6)	345(13-I-4)	-815(3)	-9(13-I-4)	-1621(8)	749(8)
0	-4837(6)	345(13-I-4)	-490(9)	-9(13-I-4)	-2773(8)	-592(13-I-4)	
8019	0	-4377(6)	173(13-I-2)	-824(3)	12(13-I-1)	-2729(8)	-689(13-I-4)
0	-4099(6)	173(13-I-2)	-489(12-I-3)	12(13-I-1)	-3668(8)	-499(13-I-4)	
8019	0	-3001(6)	-340(13-I-4)	360(12-II-3)	9(13-I-4)	-3811(8)	-647(13-I-4)
59	-2721(6)	-340(13-I-4)	516(12-II-3)	9(13-I-4)	-3550(8)	210(9)	
8019	59	-2553(6)	-119(13-II-4)	460(3)	5(13-I-1)	-3534(8)	268(9)
60	-2351(6)	-119(13-II-4)	833(6)	5(13-I-1)	-2871(9)	126(9)	
8019	60	-2347(6)	211(13-I-4)	821(3)	-13(13-I-4)	-1891(13-I-4)	-83(13-I-4)
385	-2229(6)	211(13-I-4)	1188(3)	-13(13-I-4)	-1972(9)	-83(13-I-4)	
8019	120	-6934(6)	-236(8)	-1922(6)	-5(13-I-4)	4122(3)	171(13-I-1)
0	-6457(6)	-236(8)	-1576(3)	-5(13-I-4)	1395(12-I-3)	517(8)	
8019	385	-2457(6)	-137(13-I-1)	1054(3)	26(13-I-4)	-1996(9)	-90(13-I-1)
386	-2439(6)	-137(13-I-1)	1421(3)	26(13-I-4)	1077(10)	61(13-I-1)	
8019	386	-2889(6)	80(13-I-3)	1211(12-I-3)	-19(13-I-4)	1047(10)	51(13-I-3)
346	-2998(6)	80(13-I-3)	1442(8)	-19(13-I-4)	1948(12-I-3)	-39(13-I-4)	
8020	0	-3068(6)	-303(13-II-4)	351(13-I-3)	10(13-I-4)	-3828(8)	-588(13-I-4)
45	-2790(6)	-303(13-II-4)	507(13-I-3)	10(13-I-4)	-3557(8)	209(9)	
8020	0	-3719(6)	126(9)	-453(13-II-3)	-6(13-I-4)	-3658(8)	-493(13-I-4)
0	-3371(6)	126(9)	418(13-I-3)	-6(13-I-4)	-3857(8)	-493(13-I-4)	
8020	45	-2611(6)	112(9)	465(3)	4(13-I-1)	-3540(8)	265(9)
46	-2408(6)	112(9)	841(6)	4(13-I-1)	-2865(9)	-149(13-I-4)	
8020	46	-2399(6)	134(8)	835(3)	-15(13-I-4)	-2867(9)	-210(13-I-4)
371	-2280(6)	134(8)	1204(3)	-15(13-I-4)	-1958(9)	-132(13-I-4)	
8020	121	-7489(6)	-259(8)	-1937(3)	-5(13-I-4)	4185(3)	153(13-I-1)
198	-7029(6)	-259(8)	-1604(3)	-5(13-I-4)	1392(13-I-2)	594(8)	
8020	198	-6730(6)	108(13-I-2)	-1433(3)	9(13-I-1)	1418(13-I-2)	608(8)
199	-6274(6)	108(13-I-2)	-1092(3)	9(13-I-1)	-1757(8)	654(8)	
8020	199	-5345(6)	251(13-II-4)	-828(3)	-14(13-I-4)	-1606(8)	684(8)
200	-4877(6)	251(13-II-4)	-510(8)	-14(13-I-4)	-2785(8)	-528(13-I-1)	
8020	200	-4434(6)	154(13-I-2)	-832(3)	9(13-I-1)	-2743(8)	-609(13-I-1)
0	-4074(6)	154(13-I-2)	-473(3)	9(13-I-1)	-3690(8)	-450(13-I-4)	
8020	371	-2468(6)	-166(13-II-4)	1071(3)	28(13-I-4)	-1981(9)	-154(13-I-4)
372	-2451(6)	-166(13-II-4)	1441(3)	28(13-I-4)	1166(10)	64(13-I-1)	

8020	372	-2911(6)	90(13-14)	1238(12-12)	-19(13-14)	1065(10)	71(13-14)
347	-3019(6)	90(13-14)	1455(3)	-19(13-14)	1950(13-12)	-38(13-11)	
8021	0	-5339(6)	319(13-14)	-803(3)	-8(13-14)	-1669(8)	772(8)
	0	-4884(6)	319(13-14)	-492(8)	-8(13-14)	-2810(8)	-517(13-11)
8021	0	-4443(6)	147(13-12)	-810(3)	11(13-11)	-2767(8)	-601(13-11)
	0	-4092(6)	147(13-12)	-502(13-12)	11(13-11)	-3688(8)	-465(13-14)
8021	0	-3087(6)	362(13-14)	362(13-13)	10(13-14)	-3521(8)	-591(13-14)
	61	-2811(6)	-308(13-14)	517(13-13)	10(13-14)	-3548(8)	204(9)
8021	0	-6114(6)	176(13-12)	-1417(3)	-4(13-12)	1529(13-12)	600(8)
	0	-5670(6)	176(13-12)	-1084(3)	-4(13-12)	-1701(8)	762(8)
8021	0	-3732(6)	122(9)	-463(13-12)	-5(13-14)	-3656(8)	-509(13-14)
	0	-3391(6)	122(9)	433(13-12)	-5(13-14)	-3849(8)	-496(13-14)
8021	61	-2628(6)	-113(13-14)	460(3)	5(13-14)	-3531(8)	260(9)
	62	-2425(6)	-113(13-14)	835(6)	5(13-11)	-2857(9)	127(9)
8021	62	-2912(6)	205(13-14)	830(3)	-14(13-14)	-2859(9)	181(9)
	387	-2292(6)	205(13-14)	1202(3)	-14(13-14)	-1952(9)	-86(13-14)
8021	122	-6858(6)	-269(8)	-193(13)	-3(13-14)	4212(3)	163(13-11)
	0	-6412(6)	-269(8)	-1608(3)	-3(13-14)	1501(13-12)	590(8)
8021	387	-2535(6)	-136(13-11)	1077(3)	26(13-14)	-1978(9)	-91(13-11)
	388	-2517(6)	-136(13-11)	1449(3)	26(13-14)	1097(10)	60(13-11)
8021	388	-2978(6)	80(13-13)	1287(13-12)	-19(13-14)	1065(10)	51(13-13)
	348	-3088(6)	80(13-13)	1457(3)	-19(13-14)	2053(13-12)	-40(13-14)
8022	0	-5344(6)	295(13-14)	-787(3)	-12(13-14)	-1619(8)	744(8)
	0	-4897(6)	295(13-14)	-490(9)	-12(13-14)	-2742(8)	-538(13-11)
8022	0	-3118(6)	-310(13-14)	361(13-13)	10(13-14)	-3758(8)	-602(13-14)
	51	-2847(6)	-310(13-14)	514(13-13)	10(13-14)	-3502(8)	199(9)
8022	0	-3750(6)	128(9)	-518(13-12)	-6(13-14)	-493(13-14)	-493(13-14)
	0	-3415(6)	128(9)	486(13-12)	-6(13-14)	-3787(8)	-507(13-14)
8022	0	-4458(6)	165(13-12)	-801(3)	10(13-11)	-2699(8)	-623(13-11)
	0	-4136(6)	165(13-12)	-547(13-12)	10(13-11)	-3614(8)	-452(13-14)
8022	0	-6459(6)	137(13-12)	-1375(3)	-6(13-11)	1575(13-12)	666(8)
	52	-2456(6)	137(13-12)	-1049(3)	-6(13-11)	-1703(8)	696(8)
8022	51	-2659(6)	102(9)	441(3)	5(13-14)	-3484(8)	253(9)
	52	-2456(6)	102(9)	809(6)	5(13-14)	-2847(9)	-151(13-14)
8022	52	-2437(6)	138(8)	799(3)	-15(13-14)	-2849(9)	-211(13-14)
	377	-2317(6)	138(8)	1170(3)	-15(13-14)	-1966(9)	-1966(9)
8022	123	-7226(6)	-294(8)	-1840(3)	-4(13-14)	1546(13-12)	161(13-11)
	0	-6789(6)	-189(13-14)	-1524(3)	-4(13-14)	1546(13-12)	652(8)
8022	377	-2550(6)	-189(13-14)	1049(3)	28(13-14)	-1991(9)	-181(13-14)
	378	-2532(6)	-189(13-14)	1424(3)	28(13-14)	1068(10)	651(13-14)
8022	378	-2981(6)	95(13-13)	1402(13-12)	-20(13-14)	1037(10)	72(13-14)
	349	-3093(6)	95(13-13)	1562(13-12)	-20(13-14)	2144(13-12)	-40(13-11)
8023	0	-5367(6)	361(13-14)	-765(3)	-11(13-14)	-1757(8)	752(8)
	0	-4927(6)	361(13-14)	-498(13-12)	-11(13-14)	-2850(8)	-641(13-14)
8023	0	-4518(6)	-207(13-12)	-760(3)	13(13-11)	-2808(8)	-740(13-14)
	0	-4178(6)	-207(13-12)	-594(13-12)	13(13-11)	-3667(8)	-499(13-14)
8023	0	-3833(6)	131(9)	-559(13-12)	-10(13-14)	-3635(8)	-544(13-14)
	0	-3500(6)	131(9)	559(13-12)	-10(13-14)	-3771(8)	-575(13-14)
8023	0	-3222(6)	-356(13-14)	394(13-12)	9(13-14)	-3744(8)	-680(13-14)
	55	-2953(6)	-356(13-14)	546(13-12)	9(13-14)	-3434(8)	-202(13-14)
8023	0	-6098(6)	202(13-12)	-1413(3)	-6(13-12)	1711(13-12)	675(8)
	0	-5670(6)	202(13-12)	-1093(3)	-6(13-12)	-1789(8)	744(8)
8023	55	-2772(6)	-132(13-14)	459(3)	5(13-11)	-3417(8)	-268(13-14)
	56	-2573(6)	-132(13-14)	825(6)	5(13-11)	-2768(9)	124(9)
8023	56	-2554(6)	201(13-14)	788(3)	-12(13-14)	-2770(9)	-184(13-14)
	381	-2435(6)	201(13-14)	1157(3)	-12(13-14)	-1895(9)	-81(13-14)
8023	124	-6821(6)	-311(8)	-1934(3)	-5(13-14)	4130(3)	171(13-11)
	0	-6391(6)	-144(13-11)	-1623(3)	-5(13-14)	1679(13-12)	662(8)
8023	381	-2676(6)	-144(13-11)	1140(13-12)	25(13-13)	-1921(9)	-93(13-11)
	382	-2658(6)	-144(13-11)	1368(3)	25(13-13)	1077(10)	66(8)
8023	382	-3082(6)	8(13-13)	1521(13-12)	-20(13-14)	1049(10)	51(13-13)
	350	-3194(6)	8(13-13)	1681(13-12)	-20(13-14)	2319(13-12)	-41(13-13)
8024	0	-3656(13-14)	130(9)	-624(13-12)	-8(13-14)	-3673(8)	-451(13-14)
	0	-3517(13-14)	130(9)	672(13-12)	-8(13-14)	-3666(8)	-502(13-14)
8024	0	-4809(13-14)	113(13-12)	-794(13-12)	13(13-14)	-2897(8)	-541(13-11)
	0	-4665(13-14)	113(13-12)	-648(13-12)	13(13-14)	-3679(8)	-475(13-14)
8024	0	-3429(13-14)	-268(13-14)	693(13-13)	14(13-14)	-3639(8)	-586(13-14)

8024	63	-3317(13-14)	-268(13-14)	845(13-13)	14(13-14)	-3050(8)	-228(13-14)
	0	-5057(13-14)	268(13-14)	-821(8)	-10(13-14)	-1742(8)	753(8)
8024	0	-4870(13-14)	268(13-14)	-540(9)	-10(13-14)	-2942(8)	-472(13-14)
	0	-5898(6)	173(13-12)	-1331(3)	-6(13-11)	1574(13-12)	707(8)
8024	63	-5474(6)	173(13-12)	-1013(3)	-6(13-11)	-1911(8)	739(8)
	64	-3321(6)	-139(13-14)	922(13-14)	6(13-11)	-3244(8)	266(9)
8024	64	-3122(6)	-139(13-14)	1076(13-14)	6(13-11)	-2388(9)	152(8)
	64	-3115(6)	-199(13-14)	863(3)	-11(13-14)	-2393(9)	208(8)
8024	389	-2996(6)	-199(13-14)	1232(3)	-11(13-14)	1832(13-13)	94(8)
	125	-6692(6)	-344(8)	-1757(3)	-3(13-12)	356(13)	94(13-12)
8024	0	-6267(6)	-344(8)	-1450(3)	-3(13-12)	1542(13-12)	694(8)
	389	-4414(13-14)	-100(13-11)	1321(13-12)	25(13-13)	1641(13-13)	95(8)
8024	390	-4407(13-14)	-100(13-11)	1480(13-12)	25(13-13)	1038(10)	75(8)
	390	-4030(13-14)	89(13-11)	2032(13-13)	-20(13-14)	1022(10)	56(13-11)
8024	351	-4076(13-14)	89(13-11)	2192(13-13)	-20(13-14)	2655(13-12)	-45(13-12)
8025	0	-3418(13-14)	-130(13-14)	-705(13-13)	21(13-14)	-3144(8)	-318(13-14)
	67	-3338(13-14)	-130(13-14)	757(13-13)	21(13-14)	-1252(8)	-148(13-14)
8025	0	-3899(6)	110(13-12)	-876(8)	-8(3)	1172(13-12)	749(8)
	0	-3631(6)	110(13-12)	-692(8)	-8(3)	-1494(8)	811(8)
8025	0	-4584(13-14)	120(8)	-530(8)	11(13-11)	-2224(8)	524(9)
	0	-4480(13-14)	120(8)	-376(13-12)	11(13-11)	-2872(8)	359(9)
8025	0	-3668(13-14)	135(9)	-527(13-12)	-5(13-12)	-2812(8)	418(9)
	0	-3568(13-14)	135(9)	461(13-12)	-5(13-12)	-3158(8)	-287(13-14)
8025	0	-4761(13-14)	198(8)	-643(13-13)	6(9)	-1517(8)	817(8)
	0	-4625(13-14)	198(8)	-539(13-13)	6(9)	-2244(8)	468(9)
8025	67	-2032(13-12)	-102(13-14)	979(13-14)	6(13-12)	-3072(8)	206(9)
	68	-1973(13-12)	-102(13-14)	1089(13-14)	6(13-12)	-2956(8)	136(8)
8025	68	-2121(13-12)	-201(13-14)	827(13-14)	-11(13-14)	-2956(8)	183(8)
	393	-2086(13-12)	-201(13-14)	938(13-14)	-11(13-14)	-2466(9)	197(13-14)
8025	126	-4036(6)	-351(8)	-1184(3)	-14(13-12)	2342(13-12)	-111(13-11)
	0	-4036(6)	-351(8)	-988(3)	-14(13-12)	1153(13-12)	736(8)
8025	393	-4245(13-14)	-158(13-14)	1027(8)	24(13-13)	-2428(9)	177(13-14)
	394	-4240(13-14)	-158(13-14)	1236(8)	24(13-13)	1307(13-14)	77(13-13)
8025	394	-4036(13-14)	85(13-11)	2150(13-14)	-19(13-14)	1331(13-14)	71(13-13)
	352	-4069(13-14)	85(13-11)	2263(13-14)	-19(13-14)	2013(13-12)	-25(13-11)
8028	101	-1609(13-11)	-139(8)	-91(6)	0	-40(13-11)	0
	102	-1609(13-11)	-139(8)	75(6)	0	0	71(8)
8028	102	-2953(13-11)	116(13-11)	-105(6)	0	0	53(13-11)
	103	-2953(13-11)	116(13-11)	90(6)	0	0	-51(13-11)
8028	103	-2681(13-14)	80(12-11)	-105(6)	0	0	-39(3)
	104	-2681(13-14)	80(12-11)	94(6)	0	0	-36(13-11)
8028	104	-2391(3)	97(13-14)	-106(6)	0	0	44(13-14)
	105	-2391(3)	97(13-14)	100(6)	0	0	-43(13-14)
8028	105	-2143(3)	84(13-11)	-106(6)	0	0	38(13-11)
	106	-2143(3)	84(13-11)	107(6)	0	0	-37(13-11)
8028	106	-1925(3)	92(13-11)	-107(6)	0	0	40(13-11)
	107	-1925(3)	92(13-11)	106(6)	0	0	-42(13-11)
8028	107	-3044(3)	95(13-11)	-101(6)	0	0	-32(13-11)
	108	-3044(3)	95(13-11)	107(6)	0	0	44(9)
8028	108	-4383(3)	117(13-11)	-94(6)	0	0	54(13-11)
	109	-4383(3)	117(13-11)	105(6)	0	0	-51(13-12)
8028	109	-4229(3)	69(13-11)	-91(6)	0	0	29(13-11)
	110	-4229(3)	69(13-11)	106(6)	0	0	-32(13-11)
8028	110	-4068(3)	58(13-14)	-87(6)	0	0	27(13-14)
	111	-4068(3)	58(13-14)	105(6)	0	0	26(13-14)
8028	111	-4162(3)	82(13-14)	-83(6)	0	0	37(13-14)
	112	-4162(3)	82(13-14)	103(6)	0	0	-36(13-14)
8028	112	-4059(3)	-93(13-11)	-81(6)	0	0	-40(13-11)
	113	-4059(3)	-93(13-11)	102(6)	0	0	43(13-11)
8028	113	-4229(3)	81(13-11)	-80(6)	0	0	36(13-11)
	114	-4229(3)	81(13-11)	101(6)	0	0	40(8)
8028	114	-4642(3)	81(13-11)	-80(6)	0	0	38(13-11)
	115	-4642(3)	81(13-11)	100(6)	0	0	-34(13-11)
8028	115	-4571(3)	-82(13-11)	-79(6)	0	0	37(13-14)
	116	-4571(3)	-82(13-11)	98(6)	0	0	-36(13-11)
8028	116	-3987(3)	64(13-14)	-80(6)	0	0	29(13-14)
	117	-3987(3)	64(13-14)	97(6)	0	0	-28(13-14)

8028	117	-3955(3)	-105(13-1-1)	-84(6)	0	0	-46(13-1-1)
8028	118	-3955(3)	-105(13-1-1)	98(6)	0	0	49(13-1-1)
8028	118	-3376(3)	-95(13-1-1)	-86(6)	0	0	-41(13-1-1)
8028	119	-3376(3)	-95(13-1-1)	93(6)	0	0	43(8)
8028	119	-2940(3)	-90(13-1-2)	-90(6)	0	0	-41(13-1-2)
8028	120	-2940(3)	-90(13-1-2)	95(6)	0	0	40(13-1-2)
8028	120	-2949(3)	-101(13-1-4)	-92(6)	0	0	-44(13-1-4)
8028	121	-2949(3)	-101(13-1-4)	89(6)	0	0	46(13-1-4)
8028	121	-1959(3)	-82(13-1-1)	-97(6)	0	0	-37(13-1-1)
8028	122	-1959(3)	-82(13-1-1)	88(6)	0	0	38(8)
8028	122	-2018(3)	-95(13-1-4)	-102(6)	0	0	-43(13-1-4)
8028	123	-2018(3)	-95(13-1-4)	87(6)	0	0	43(13-1-4)
8028	123	-2885(13-1-4)	-81(3)	-105(6)	0	0	-36(13-1-2)
8028	124	-2885(13-1-4)	-81(3)	86(6)	0	0	49(8)
8028	124	-3134(13-1-1)	-108(13-1-2)	-108(6)	0	0	-48(13-1-2)
8028	125	-3134(13-1-1)	-108(13-1-2)	87(6)	0	0	49(13-1-2)
8028	125	-1680(13-1-1)	71(13-1-2)	-109(6)	0	0	36(13-1-2)
8028	126	-1680(13-1-1)	71(13-1-2)	88(6)	0	0	29(9)
8029	0	-329(8)	44(13-1-1)	-194(6)	0	0	40(13-1-1)
8029	0	-329(8)	44(13-1-1)	198(6)	0	0	-31(13-1-4)
8029	0	-691(8)	127(13-1-1)	-198(6)	0	0	70(13-1-4)
8029	0	-691(8)	127(13-1-1)	202(6)	0	0	-52(13-1-1)
8029	0	-996(8)	58(12-1-1)	-201(6)	0	0	34(8)
8029	0	-996(8)	58(12-1-1)	206(6)	0	0	-26(12-1-1)
8029	0	-1243(8)	67(13-1-1)	-207(6)	0	0	32(13-1-1)
8029	0	-1243(8)	67(13-1-1)	212(6)	0	0	-32(13-1-1)
8029	0	-1445(8)	54(13-1-1)	-213(6)	0	0	30(13-1-1)
8029	0	-1445(8)	54(13-1-1)	220(6)	0	0	-22(13-1-1)
8029	0	-1626(8)	114(13-1-1)	-220(6)	0	0	42(13-1-1)
8029	168	-1626(8)	114(13-1-1)	212(6)	0	0	-67(13-1-1)
8029	0	-1200(8)	-63(13-1-2)	-200(6)	0	0	-31(13-1-2)
8029	0	-1200(8)	-63(13-1-2)	201(6)	0	0	31(9)
8029	0	-646(8)	-118(13-1-2)	-203(6)	0	0	-48(13-1-2)
8029	0	-646(8)	-118(13-1-2)	205(6)	0	0	65(13-1-2)
8029	0	-920(8)	-65(8)	-201(6)	0	0	-26(13-1-2)
8029	0	-920(8)	-65(8)	202(6)	0	0	50(8)
8029	0	-318(8)	-67(8)	-205(6)	0	0	-32(13-1-4)
8029	0	-318(8)	-67(8)	207(6)	0	0	43(8)
8029	0	-1615(8)	-48(13-1-2)	-194(6)	0	0	-21(13-1-2)
8029	198	-1615(8)	-48(13-1-2)	194(6)	0	0	35(8)
8029	0	-1732(8)	-103(13-1-2)	-196(6)	0	0	-60(13-1-2)
8029	0	-1732(8)	-103(13-1-2)	197(6)	0	0	39(13-1-2)
8029	0	-2110(8)	-43(13-1-1)	-185(6)	0	0	-18(13-1-1)
8029	0	-2110(8)	-43(13-1-1)	184(6)	0	0	29(8)
8029	0	-2023(8)	38(13-1-2)	-185(6)	0	0	19(13-1-2)
8029	0	-2023(8)	38(13-1-2)	184(6)	0	0	22(9)
8029	0	-1967(8)	-112(13-1-1)	-191(6)	0	0	-43(13-1-1)
8029	173	-1967(8)	-112(13-1-1)	190(6)	0	0	65(13-1-1)
8029	153	-2087(8)	41(13-1-1)	-193(6)	0	0	21(13-1-1)
8029	188	-2087(8)	41(13-1-1)	190(6)	0	0	-18(13-1-1)
8029	158	-2123(8)	104(13-1-1)	-187(6)	0	0	61(13-1-1)
8029	0	-2123(8)	104(13-1-1)	186(6)	0	0	-39(13-1-1)
8029	163	-1986(8)	45(13-1-1)	-203(6)	0	0	-17(13-1-1)
8029	178	-1986(8)	45(13-1-1)	198(6)	0	0	-28(13-1-1)
8029	168	-1780(8)	71(13-1-4)	-215(6)	0	0	34(13-1-4)
8029	183	-1780(8)	71(13-1-4)	210(6)	0	0	-35(13-1-4)
8029	173	-1874(8)	-63(13-1-4)	-191(6)	0	0	29(13-1-4)
8029	0	-1874(8)	-63(13-1-4)	190(6)	0	0	38(8)
8029	178	-2053(8)	-41(13-1-1)	-198(6)	0	0	23(13-1-2)
8029	153	-2053(8)	-41(13-1-1)	194(6)	0	0	21(8)
8029	183	-1882(8)	118(13-1-1)	-205(6)	0	0	68(13-1-1)
8029	163	-1882(8)	118(13-1-1)	200(6)	0	0	-44(13-1-1)
8029	188	-2123(8)	-110(13-1-1)	-189(6)	0	0	-43(13-1-1)
8029	193	-2123(8)	-110(13-1-1)	187(6)	0	0	61(13-1-1)
8029	193	-2139(8)	-59(13-1-4)	-188(6)	0	0	30(13-1-4)
8029	158	-2139(8)	-59(13-1-4)	186(6)	0	0	34(8)
8029	198	-1380(8)	-49(13-1-2)	-197(6)	0	0	-21(13-1-2)

8030	0	-1380(8)	-49(13-1-2)	196(6)	0	0	35(8)
8030	0	-733(13-1-1)	78(13-1-4)	-213(6)	0	0	39(13-1-4)
8030	0	-733(13-1-1)	78(13-1-4)	218(6)	0	0	-39(13-1-4)
8030	0	942(13-1-3)	46(13-1-4)	-218(6)	0	0	30(13-1-4)
8030	0	942(13-1-3)	46(13-1-4)	224(6)	0	0	27(8)
8030	0	717(13-1-1)	32(13-1-4)	-225(6)	0	0	11(13-1-4)
8030	0	717(13-1-1)	32(13-1-4)	232(6)	0	0	32(9)
8030	0	1417(13-1-1)	49(13-1-1)	-231(6)	0	0	12(13-1-1)
8030	169	1417(13-1-1)	49(13-1-1)	224(6)	0	0	-38(13-1-1)
8030	0	-629(9)	-60(13-1-1)	-210(6)	0	0	-39(13-1-1)
8030	0	-629(9)	-60(13-1-1)	214(6)	0	0	30(8)
8030	0	-312(12-1-1)	87(13-1-4)	-207(6)	0	0	-36(9)
8030	0	-312(12-1-1)	87(13-1-4)	210(6)	0	0	-70(13-1-4)
8030	0	-384(9)	-91(13-1-4)	-223(6)	0	0	-71(13-1-4)
8030	0	-384(9)	-91(13-1-4)	225(6)	0	0	32(8)
8030	0	-578(13-1-1)	56(13-1-2)	-222(6)	0	0	20(13-1-2)
8030	0	-578(13-1-1)	56(13-1-2)	224(6)	0	0	-38(13-1-2)
8030	0	1055(13-1-2)	-50(13-1-2)	-217(6)	0	0	-58(13-1-2)
8030	0	1055(13-1-2)	-50(13-1-2)	217(6)	0	0	26(8)
8030	0	-733(8)	-69(13-1-4)	-220(6)	0	0	-33(13-1-4)
8030	0	-733(8)	-69(13-1-4)	222(6)	0	0	44(8)
8030	0	520(13-1-4)	-34(13-1-4)	-221(6)	0	0	-91(13-1-4)
8030	0	520(13-1-4)	-34(13-1-4)	221(6)	0	0	37(8)
8030	0	95(13-1-4)	-75(13-1-4)	-217(6)	0	0	-33(13-1-4)
8030	199	95(13-1-4)	-75(13-1-4)	217(6)	0	0	52(8)
8030	0	1220(12-1-2)	-58(13-1-4)	-199(6)	0	0	-29(13-1-4)
8030	0	1220(12-1-2)	-58(13-1-4)	198(6)	0	0	41(8)
8030	0	119(13-1-3)	-56(13-1-4)	-200(6)	0	0	-29(13-1-4)
8030	0	119(13-1-3)	-56(13-1-4)	199(6)	0	0	34(8)
8030	0	988(13-1-1)	-48(13-1-3)	-206(6)	0	0	-15(13-1-3)
8030	174	988(13-1-1)	-48(13-1-3)	205(6)	0	0	36(13-1-4)
8030	154	1292(13-1-3)	67(13-1-4)	-205(6)	0	0	37(13-1-4)
8030	189	1292(13-1-3)	67(13-1-4)	202(6)	0	0	31(9)
8030	159	1278(12-1-2)	43(13-1-4)	-200(6)	0	0	-35(13-1-4)
8030	0	1278(12-1-2)	43(13-1-4)	199(6)	0	0	25(9)
8030	164	909(12-1-2)	-28(9)	-214(6)	0	0	-22(13-1-4)
8030	179	909(12-1-2)	-28(9)	210(6)	0	0	85(13-1-4)
8030	169	912(13-1-1)	169(13-1-4)	-227(6)	0	0	-88(13-1-4)
8030	184	912(13-1-1)	169(13-1-4)	222(6)	0	0	74(13-1-4)
8030	174	1002(12-1-2)	-148(13-1-4)	-208(6)	0	0	75(13-1-4)
8030	0	1002(12-1-2)	-148(13-1-4)	207(6)	0	0	15(13-1-4)
8030	179	1486(13-1-1)	47(13-1-4)	-210(6)	0	0	33(9)
8030	154	1486(13-1-1)	47(13-1-4)	206(6)	0	0	32(13-1-1)
8030	184	1285(13-1-3)	42(13-1-1)	-216(6)	0	0	22(9)
8030	164	1285(13-1-3)	42(13-1-1)	212(6)	0	0	-12(13-1-1)
8030	189	1279(13-1-1)	38(13-1-1)	-202(6)	0	0	-29(13-1-4)
8030	194	1279(13-1-1)	38(13-1-1)	200(6)	0	0	74(13-1-1)
8030	194	1305(12-1-2)	-152(13-1-4)	-201(6)	0	0	81(13-1-4)
8030	159	1305(12-1-2)	-152(13-1-4)	199(6)	0	0	76(13-1-4)
8030	199	718(13-1-2)	-63(13-1-4)	-218(6)	0	0	-45(13-1-4)
8030	0	718(13-1-2)	-63(13-1-4)	218(6)	0	0	38(8)
8031	0	814(12-1-1)	-135(13-1-1)	-214(6)	0	0	-71(13-1-1)
8031	0	814(12-1-1)	-135(13-1-1)	220(6)	0	0	74(13-1-1)
8031	0	559(13-1-1)	-214(13-1-1)	-206(6)	0	0	-123(13-1-1)
8031	0	559(13-1-1)	-214(13-1-1)	213(6)	0	0	108(13-1-1)
8031	0	1062(12-1-1)	-197(13-1-4)	-227(6)	0	0	-97(13-1-4)
8031	170	1062(12-1-1)	-197(13-1-4)	220(6)	0	0	113(13-1-4)
8031	0	588(12-1-2)	126(13-1-2)	-224(6)	0	0	71(13-1-3)
8031	0	588(12-1-2)	126(13-1-2)	228(6)	0	0	-65(13-1-2)
8031	0	324(13-1-1)	-138(9)	-203(6)	0	0	-67(9)
8031	0	324(13-1-1)	-138(9)	209(6)	0	0	82(9)
8031	0	1006(12-1-2)	121(13-1-3)	-225(6)	0	0	64(13-1-3)
8031	200	1006(12-1-2)	121(13-1-3)	222(6)	0	0	-67(13-1-4)
8031	0	953(12-1-1)	-132(13-1-1)	-221(6)	0	0	-75(13-1-1)
8031	0	953(12-1-1)	-132(13-1-1)	228(6)	0	0	73(8)
8031	0	657(12-1-1)	-132(13-1-1)	-209(6)	0	0	-48(13-1-1)
8031	0	657(12-1-1)	-132(13-1-1)	216(6)	0	0	74(8)

8031	0	747(12-12)	126(13-11-3)	-225(6)	0	0	69(13-11-3)
	0	747(12-12)	126(13-11-3)	228(6)	0	0	-66(13-11-3)
8031	0	313(13-12)	-115(8)	-223(6)	0	0	-48(8)
	0	313(13-12)	-115(8)	229(6)	0	0	76(8)
8031	0	533(13-12)	207(13-11-4)	-224(6)	0	0	104(13-11-4)
	0	533(13-12)	207(13-11-4)	229(6)	0	0	-119(13-11-3)
8031	0	1103(12-12)	190(13-11-4)	-221(6)	0	0	110(13-11-4)
	0	1103(12-12)	190(13-11-4)	219(6)	0	0	-94(13-11-4)
8031	0	1366(12-12)	118(13-11-4)	-201(6)	0	0	61(13-11-4)
	0	1366(12-12)	118(13-11-4)	197(6)	0	0	-66(13-11-4)
8031	0	1333(12-12)	120(13-11-4)	-202(6)	0	0	66(13-11-4)
	0	1333(12-12)	120(13-11-4)	198(6)	0	0	-62(13-11-4)
8031	0	1293(12-12)	182(13-11-4)	-208(6)	0	0	92(13-11-4)
	175	1293(12-12)	182(13-11-4)	205(6)	0	0	-105(13-11-4)
8031	155	1364(12-12)	-115(13-1-4)	-205(6)	0	0	-64(13-1-4)
	190	1364(12-12)	-115(13-1-4)	199(6)	0	0	64(8)
8031	160	1388(12-12)	182(13-11-4)	-202(6)	0	0	105(13-11-4)
	0	1388(12-12)	182(13-11-4)	197(6)	0	0	-91(13-11-4)
8031	165	1282(12-11)	-119(13-1-1)	-213(6)	0	0	-60(13-1-1)
	180	1282(12-11)	-119(13-1-1)	207(6)	0	0	68(13-1-4)
8031	170	1160(12-11)	-123(8)	-224(6)	0	0	-50(8)
	185	1160(12-11)	-123(8)	218(6)	0	0	85(8)
8031	175	1197(12-12)	-105(9)	-211(6)	0	0	-39(9)
	0	1197(12-12)	-105(9)	208(6)	0	0	73(9)
8031	180	1324(12-12)	-121(13-1-4)	-209(6)	0	0	-67(13-1-4)
	155	1324(12-12)	-121(13-1-4)	203(6)	0	0	67(8)
8031	185	1244(12-11)	-197(13-1-4)	-214(6)	0	0	-113(13-1-4)
	165	1244(12-11)	-197(13-1-4)	208(6)	0	0	97(13-1-4)
8031	190	1392(12-12)	-185(13-1-4)	-202(6)	0	0	-92(13-1-4)
	195	1392(12-12)	-185(13-1-4)	197(6)	0	0	-106(13-1-4)
8031	195	1391(12-12)	-116(8)	-201(6)	0	0	-45(9)
	160	1391(12-12)	-116(8)	196(6)	0	0	80(8)
8031	200	893(12-12)	121(13-11-4)	-224(6)	0	0	62(13-11-4)
	0	893(12-12)	121(13-11-4)	226(6)	0	0	-68(13-11-4)
8032	0	1359(13-1-3)	-44(8)	-204(6)	0	0	-58(8)
	0	1359(13-1-3)	-44(8)	208(6)	0	0	41(8)
8032	0	1022(13-1-3)	-42(8)	-207(6)	0	0	-21(13-1-4)
	0	1022(13-1-3)	-42(8)	212(6)	0	0	40(8)
8032	0	1020(12-11)	-43(8)	-214(6)	0	0	-20(13-1-4)
	0	1020(12-11)	-43(8)	220(6)	0	0	42(8)
8032	0	1316(13-1-1)	-79(13-1-4)	-218(6)	0	0	-38(13-1-4)
	171	1316(13-1-1)	-79(13-1-4)	212(6)	0	0	-51(13-11-4)
8032	0	1113(13-1-4)	-78(9)	-198(6)	0	0	-39(9)
	0	1113(13-1-4)	-78(9)	202(6)	0	0	50(9)
8032	0	1167(13-11-4)	-71(8)	-222(6)	0	0	-49(13-11-4)
	0	1167(13-11-4)	-71(8)	225(6)	0	0	55(8)
8032	0	1834(13-11-4)	74(13-11-3)	-224(6)	0	0	36(13-11-3)
	0	1834(13-11-4)	74(13-11-3)	226(6)	0	0	-49(13-11-3)
8032	0	1432(13-11-4)	-28(9)	-224(6)	0	0	20(13-11-3)
	0	1432(13-11-4)	-28(9)	227(6)	0	0	34(9)
8032	0	1078(13-11-4)	39(13-11-3)	-226(6)	0	0	23(13-11-3)
	0	1078(13-11-4)	39(13-11-3)	228(6)	0	0	31(9)
8032	0	972(3)	40(13-11-3)	-226(6)	0	0	22(13-11-3)
	0	972(3)	40(13-11-3)	227(6)	0	0	30(9)
8032	0	1090(12-12)	-29(9)	-227(6)	0	0	13(13-11-3)
	0	1090(12-12)	-29(9)	227(6)	0	0	32(9)
8032	0	1370(13-1-3)	81(13-11-4)	-217(6)	0	0	-54(13-1-4)
	0	1370(13-1-3)	81(13-11-4)	216(6)	0	0	-39(13-11-4)
8032	0	1416(12-12)	-33(9)	-196(6)	0	0	12(13-11-4)
	0	1416(12-12)	-33(9)	195(6)	0	0	35(9)
8032	0	1731(13-1-3)	-73(13-1-4)	-201(6)	0	0	-48(13-1-4)
	0	1731(13-1-3)	-73(13-1-4)	205(6)	0	0	40(8)
8032	0	1421(13-11-4)	62(13-11-4)	-204(6)	0	0	33(13-11-4)
	176	1421(13-11-4)	62(13-11-4)	203(6)	0	0	-38(13-11-4)
8032	0	1368(12-12)	-33(9)	-198(6)	0	0	20(13-11-4)
	0	1368(12-12)	-33(9)	196(6)	0	0	36(9)
8032	156	1424(12-12)	-38(8)	-198(6)	0	0	-20(13-1-4)

8032	191	1424(12-12)	-38(8)	195(6)	0	0	39(8)
	161	149(13-1-3)	-72(13-1-4)	-196(6)	0	0	-47(13-1-4)
8032	166	1491(13-1-3)	-38(8)	-205(6)	0	0	-9(13-1-4)
	181	1491(13-1-3)	-38(8)	201(6)	0	0	37(8)
8032	171	1332(3)	90(13-1-4)	-216(6)	0	0	52(13-1-4)
	186	1332(3)	90(13-1-4)	211(6)	0	0	-51(13-1-4)
8032	176	1363(3)	-106(13-11-4)	-208(6)	0	0	65(13-1-4)
	181	1398(12-1-2)	-42(13-1-4)	-201(6)	0	0	55(13-11-4)
8032	156	1398(12-1-2)	-42(13-1-4)	198(6)	0	0	-25(13-1-4)
8032	186	1856(13-1-3)	-85(13-1-4)	-206(6)	0	0	-55(13-1-4)
	166	1856(13-1-3)	-85(13-1-4)	202(6)	0	0	40(13-1-4)
8032	191	1698(13-11-1)	82(13-11-4)	-196(6)	0	0	39(13-11-4)
	196	1698(13-11-1)	82(13-11-4)	194(6)	0	0	-54(13-11-4)
8032	196	1561(3)	-94(13-11-4)	-195(6)	0	0	50(13-1-4)
	161	1561(3)	-94(13-11-4)	193(6)	0	0	-56(13-1-4)
8033	0	626(12-1-1)	-106(13-1-4)	-206(6)	0	0	-63(13-1-4)
	0	626(12-1-1)	-106(13-1-4)	211(6)	0	0	63(13-1-4)
8033	0	753(12-1-4)	-101(13-1-4)	-213(6)	0	0	-62(13-1-4)
	0	753(12-1-4)	-101(13-1-4)	219(6)	0	0	63(8)
8033	0	901(12-1-4)	-139(13-1-4)	-217(6)	0	0	-79(13-1-4)
	172	901(12-1-4)	-139(13-1-4)	211(6)	0	0	85(13-1-4)
8033	0	480(12-1-1)	-105(13-1-4)	-203(6)	0	0	-61(13-1-4)
	0	480(12-1-1)	-105(13-1-4)	208(6)	0	0	66(8)
8033	0	308(12-1-1)	-140(13-1-4)	-201(6)	0	0	-88(13-1-4)
	0	308(12-1-1)	-140(13-1-4)	205(6)	0	0	80(13-1-4)
8033	0	118(13-11-1)	-100(9)	-198(6)	0	0	-50(8)
	0	118(13-11-1)	-100(9)	202(6)	0	0	70(9)
8033	0	105(12-1-2)	57(13-11-4)	-227(6)	0	0	25(13-11-4)
	0	105(12-1-2)	57(13-11-4)	230(6)	0	0	47(9)
8033	0	280(12-1-2)	140(13-11-4)	-228(6)	0	0	80(13-11-4)
	0	280(12-1-2)	140(13-11-4)	232(6)	0	0	-87(13-11-4)
8033	0	433(12-1-2)	104(13-11-4)	-230(6)	0	0	64(13-11-4)
	0	433(12-1-2)	104(13-11-4)	233(6)	0	0	-60(13-11-4)
8033	0	591(12-1-3)	103(13-11-4)	-232(6)	0	0	62(13-11-4)
	0	591(12-1-3)	103(13-11-4)	233(6)	0	0	-62(13-11-4)
8033	0	738(12-1-3)	105(13-11-4)	-233(6)	0	0	62(13-11-4)
	0	738(12-1-3)	105(13-11-4)	235(6)	0	0	-63(13-11-4)
8033	0	873(12-1-3)	100(13-11-4)	-232(6)	0	0	58(13-11-4)
	0	873(12-1-3)	100(13-11-4)	231(6)	0	0	-62(13-11-4)
8033	0	1275(12-1-4)	98(13-11-4)	-199(6)	0	0	56(13-11-4)
	0	1275(12-1-4)	98(13-11-4)	196(6)	0	0	-60(13-11-4)
8033	0	1238(12-1-3)	99(13-11-4)	-201(6)	0	0	60(13-11-4)
	0	1238(12-1-3)	99(13-11-4)	198(6)	0	0	-57(13-11-4)
8033	0	1189(12-1-3)	128(13-11-4)	-207(6)	0	0	76(13-11-4)
	177	1189(12-1-3)	128(13-11-4)	205(6)	0	0	-78(13-11-4)
8033	0	988(12-1-3)	136(13-11-4)	-222(6)	0	0	84(13-11-4)
	0	988(12-1-3)	136(13-11-4)	219(6)	0	0	-78(13-11-4)
8033	157	1324(12-1-4)	-95(13-1-4)	-199(6)	0	0	-58(13-1-4)
	192	1324(12-1-4)	-95(13-1-4)	195(6)	0	0	55(13-1-4)
8033	162	1321(12-1-4)	128(13-11-4)	-198(6)	0	0	-79(13-1-4)
	0	1321(12-1-4)	128(13-11-4)	195(6)	0	0	-74(13-11-4)
8033	167	1209(12-1-4)	-95(13-1-4)	-205(6)	0	0	-54(13-1-4)
	182	1209(12-1-4)	-95(13-1-4)	201(6)	0	0	59(13-1-4)
8033	172	1005(12-1-4)	-74(8)	-216(6)	0	0	-28(8)
	187	1005(12-1-4)	-74(8)	211(6)	0	0	62(8)
8033	177	1078(12-1-3)	-59(9)	-211(6)	0	0	-18(9)
	0	1078(12-1-3)	-59(9)	209(6)	0	0	52(9)
8033	182	1277(12-1-4)	-100(13-1-4)	-202(6)	0	0	-60(13-1-4)
	157	1277(12-1-4)	-100(13-1-4)	198(6)	0	0	59(13-1-4)
8033	167	1116(12-1-4)	-140(13-1-4)	-206(6)	0	0	-86(13-1-4)
	187	1116(12-1-4)	-140(13-1-4)	201(6)	0	0	79(13-1-4)
8033	192	1349(12-1-4)	130(13-11-4)	-198(6)	0	0	-74(13-1-4)
	197	1349(12-1-4)	130(13-11-4)	194(6)	0	0	-81(13-11-4)
8033	197	1334(12-1-4)	-67(8)	-197(6)	0	0	-23(9)
	162	1334(12-1-4)	-67(8)	194(6)	0	0	57(8)

8034	27	973(12-14)	-61(8)	0	-192(6)	0	0	-27(13-14)
8034	41	973(12-14)	-61(8)	0	188(6)	0	0	55(8)
	29	1036(12-13)	-56(8)	0	-192(6)	0	0	-35(13-14)
	47	1036(12-13)	-56(8)	0	189(6)	0	0	52(8)
8034	31	937(12-14)	-61(8)	0	-198(6)	0	0	-27(13-14)
8034	37	937(12-14)	-61(8)	0	194(6)	0	0	55(8)
	33	856(12-14)	-61(9)	0	-207(6)	0	0	-22(9)
	39	856(12-14)	-61(9)	0	203(6)	0	0	56(8)
8034	35	925(12-13)	-65(8)	0	-206(6)	0	0	-24(9)
8034	53	925(12-13)	-65(8)	0	204(6)	0	0	58(8)
	37	945(12-14)	-60(8)	0	-195(6)	0	0	-29(13-14)
	27	945(12-14)	-60(8)	0	191(6)	0	0	54(8)
8034	39	986(13-13)	-63(8)	0	-198(6)	0	0	-39(13-14)
8034	31	986(13-13)	-63(8)	0	193(6)	0	0	55(8)
	41	1087(13-14)	57(13-14)	0	-191(6)	0	0	35(13-14)
	43	1087(13-14)	57(13-14)	0	188(6)	0	0	50(9)
8034	43	1087(12-14)	-64(8)	0	-191(6)	0	0	-23(9)
8034	29	1087(12-14)	-64(8)	0	188(6)	0	0	57(8)
	45	540(12-13)	-52(9)	0	-232(6)	0	0	30(13-14)
	61	540(12-13)	-52(9)	0	230(6)	0	0	49(9)
8034	47	952(12-13)	-57(9)	0	-193(6)	0	0	25(13-14)
8034	57	952(12-13)	-57(9)	0	191(6)	0	0	52(9)
	49	1064(13-14)	58(13-14)	0	-202(6)	0	0	36(13-14)
	35	1064(13-14)	58(13-14)	0	200(6)	0	0	49(9)
8034	51	841(13-14)	-50(9)	0	-228(6)	0	0	29(13-14)
8034	55	841(13-14)	-50(9)	0	231(6)	0	0	48(9)
	53	1001(13-13)	56(13-14)	0	-217(6)	0	0	35(13-14)
	59	1001(13-13)	56(13-14)	0	215(6)	0	0	49(9)
8034	55	1200(13-14)	57(13-14)	0	-225(6)	0	0	36(13-14)
8034	63	1200(13-14)	57(13-14)	0	228(6)	0	0	44(9)
	57	899(12-13)	-58(9)	0	-195(6)	0	0	26(13-14)
	49	899(12-13)	-58(9)	0	193(6)	0	0	53(9)
8034	59	712(12-13)	-53(9)	0	-227(6)	0	0	27(13-14)
8034	45	712(12-13)	-53(9)	0	226(6)	0	0	50(9)
	61	496(13-14)	-52(9)	0	-230(6)	0	0	30(13-14)
	51	496(13-14)	-52(9)	0	232(6)	0	0	49(9)
8034	63	802(13-14)	-66(8)	0	-223(6)	0	0	-25(8)
8034	67	802(13-14)	-66(8)	0	226(6)	0	0	59(8)
	65	514(12-11)	-66(8)	0	-198(6)	0	0	-28(13-14)
	77	514(12-11)	-66(8)	0	203(6)	0	0	58(8)
8034	69	-733(13-11)	-61(8)	0	-208(6)	0	0	-37(13-14)
8034	33	-733(13-11)	-61(8)	0	203(6)	0	0	54(8)
	71	689(13-13)	-68(8)	0	-196(6)	0	0	-27(13-14)
	65	689(13-13)	-68(8)	0	200(6)	0	0	59(8)
8034	73	731(13-14)	-72(9)	0	-191(6)	0	0	-32(9)
8034	75	731(13-14)	-72(9)	0	195(6)	0	0	59(9)
	75	1062(13-14)	-68(8)	0	-194(6)	0	0	-36(13-14)
	71	1062(13-14)	-68(8)	0	198(6)	0	0	59(8)
8034	77	544(12-11)	-65(8)	0	-205(6)	0	0	-30(13-14)
8035	69	544(12-11)	-65(8)	0	210(6)	0	0	57(8)
	28	-702(12-14)	-48(13-14)	0	-186(6)	0	0	-31(13-14)
	42	-702(12-14)	-48(13-14)	0	183(6)	0	0	

	30	-722(12-11-4)	-48(8)	183(6)	0	0	48(8)
8035	46	-410(12-11-3)	50(13-11-4)	-229(6)	0	0	32(13-11-4)
	62	-410(12-11-3)	50(13-11-4)	-229(6)	0	0	45(9)
8035	48	-693(12-11-4)	48(13-11-4)	-189(6)	0	0	32(13-11-4)
	58	-693(12-11-4)	48(13-11-4)	-187(6)	0	0	46(9)
8035	50	-633(12-11-3)	58(13-11-4)	-197(6)	0	0	38(13-11-4)
	36	-633(12-11-3)	58(13-11-4)	-196(6)	0	0	44(9)
8035	52	-234(12-11-3)	48(13-11-4)	-226(6)	0	0	31(13-11-4)
	56	-234(12-11-3)	48(13-11-4)	-229(6)	0	0	45(9)
8035	54	-548(12-11-3)	58(13-11-4)	-213(6)	0	0	38(13-11-4)
	60	-548(12-11-3)	58(13-11-4)	-212(6)	0	0	44(9)
8035	56	-143(12-11-3)	56(13-11-4)	-222(6)	0	0	37(13-11-4)
	64	-143(12-11-3)	56(13-11-4)	-225(6)	0	0	42(9)
8035	58	-666(12-11-4)	48(13-11-4)	-191(6)	0	0	31(13-11-4)
	50	-666(12-11-4)	48(13-11-4)	-189(6)	0	0	46(9)
8035	60	-492(12-11-3)	49(13-11-4)	-222(6)	0	0	32(13-11-4)
	46	-492(12-11-3)	49(13-11-4)	-228(6)	0	0	45(9)
8035	62	-333(12-11-3)	49(13-11-4)	-226(6)	0	0	33(13-11-4)
	52	-333(12-11-3)	49(13-11-4)	-231(6)	0	0	45(9)
8035	64	-96(13-1-4)	-50(8)	-220(6)	0	0	-21(13-1-4)
	68	-96(13-1-4)	-50(8)	-223(6)	0	0	50(8)
8035	66	-331(12-11-4)	-49(8)	-192(6)	0	0	-30(13-1-4)
	78	-331(12-11-4)	-49(8)	-196(6)	0	0	48(8)
8035	70	-480(12-11-4)	-57(13-1-4)	-201(6)	0	0	-37(13-1-4)
	34	-480(12-11-4)	-57(13-1-4)	-196(6)	0	0	47(8)
8035	72	-235(12-11-4)	-49(8)	-189(6)	0	0	-31(13-1-4)
	66	-235(12-11-4)	-49(8)	-193(6)	0	0	48(8)
8035	74	-86(13-1-4)	-52(9)	-186(6)	0	0	23(13-1-4)
	76	-86(13-1-4)	-52(9)	-189(6)	0	0	49(9)
8035	76	-143(12-11-4)	-55(13-1-4)	-188(6)	0	0	-36(13-1-4)
	72	-143(12-11-4)	-55(13-1-4)	-191(6)	0	0	49(8)
8035	78	-409(12-11-4)	-50(13-1-4)	-198(6)	0	0	-33(13-1-4)
	70	-409(12-11-4)	-50(13-1-4)	-203(6)	0	0	48(8)
8036	0	-1571(13-1-4)	-38(13-1-4)	-186(6)	0	0	-27(13-1-4)
	397	-1571(13-1-4)	-38(13-1-4)	-189(6)	0	0	26(8)
8036	0	-700(12-1-1)	-30(13-1-4)	-195(6)	0	0	-21(13-1-4)
	395	-700(12-1-1)	-30(13-1-4)	-200(6)	0	0	25(8)
8036	353	-1023(13-11-4)	-26(13-1-4)	-184(6)	0	0	-17(13-1-4)
	367	-1023(13-11-4)	-26(13-1-4)	-182(6)	0	0	23(9)
8036	355	-1171(13-1-3)	32(13-11-4)	-185(6)	0	0	22(13-11-4)
	373	-1171(13-1-3)	32(13-11-4)	-183(6)	0	0	-22(13-11-4)
8036	357	-1308(13-1-4)	-28(13-1-4)	-188(6)	0	0	-19(13-1-4)
	363	-1308(13-1-4)	-28(13-1-4)	-185(6)	0	0	24(8)
8036	359	-817(12-1-1)	-17(13-11-3)	-197(6)	0	0	-12(13-11-3)
	365	-817(12-1-1)	-17(13-11-3)	-194(6)	0	0	26(8)
8036	361	-746(12-1-2)	17(13-1-4)	-204(6)	0	0	12(13-1-4)
	379	-746(12-1-2)	17(13-1-4)	-202(6)	0	0	23(9)
8036	363	-1524(13-1-4)	-25(13-1-4)	-186(6)	0	0	-18(13-1-4)
	353	-1524(13-1-4)	-25(13-1-4)	-184(6)	0	0	24(8)
8036	365	-1150(13-1-4)	-35(13-1-4)	-188(6)	0	0	-24(13-1-4)
	357	-1150(13-1-4)	-35(13-1-4)	-185(6)	0	0	24(13-1-4)
8036	367	-955(3)	-31(13-1-4)	-184(6)	0	0	-22(13-1-4)
	369	-955(3)	-31(13-1-4)	-182(6)	0	0	22(8)
8036	369	-882(12-1-2)	16(13-1-1)	-184(6)	0	0	-11(13-11-1)
	355	-882(12-1-2)	16(13-1-1)	-182(6)	0	0	25(9)
8036	371	-727(13-11-4)	25(13-11-4)	-228(6)	0	0	17(13-11-4)
	387	-727(13-11-4)	25(13-11-4)	-228(6)	0	0	21(9)
8036	373	-1374(13-1-4)	25(13-11-4)	-187(6)	0	0	18(13-11-4)
	383	-1374(13-1-4)	25(13-11-4)	-186(6)	0	0	22(9)
8036	375	-1021(13-11-4)	32(13-11-4)	-196(6)	0	0	22(13-11-4)
	361	-1021(13-11-4)	32(13-11-4)	-195(6)	0	0	-22(13-11-4)
8036	377	-2068(13-11-4)	28(13-11-4)	-228(6)	0	0	19(13-11-4)
	381	-2068(13-11-4)	28(13-11-4)	-231(6)	0	0	20(9)
8036	379	-1187(13-1-4)	33(13-11-4)	-213(6)	0	0	23(13-11-4)
	385	-1187(13-1-4)	33(13-11-4)	-212(6)	0	0	-22(13-11-4)
8036	381	-1906(13-11-4)	37(13-11-4)	-224(6)	0	0	25(13-11-4)
	389	-1906(13-11-4)	37(13-11-4)	-227(6)	0	0	-26(13-11-4)

8036	383	-1203(13-II-4)	26(13-II-4)	-190(6)	0	0	18(13-II-4)
	375	-1203(13-II-4)	26(13-II-4)	189(6)	0	0	22(9)
8036	385	-1392(13-I-4)	26(13-II-4)	-222(6)	0	0	18(13-II-4)
8036	371	-1392(13-I-4)	26(13-II-4)	222(6)	0	0	21(9)
	387	-700(3)	26(13-II-4)	-23(6)	0	0	18(13-II-4)
	377	-700(3)	26(13-II-4)	23(6)	0	0	21(9)
8036	389	-1476(13-II-4)	19(13-I-3)	-22(6)	0	0	13(13-I-3)
	393	-1476(13-II-4)	19(13-I-3)	22(6)	0	0	22(8)
8036	391	-905(13-I-4)	-28(13-I-4)	-189(6)	0	0	-19(13-I-4)
	0	-905(13-I-4)	-28(13-I-4)	193(6)	0	0	26(8)
8036	395	-686(12-I-1)	-36(13-I-4)	-198(6)	0	0	-24(13-I-4)
	359	-686(12-I-1)	-36(13-I-4)	193(6)	0	0	24(13-I-4)
8036	397	-1715(13-I-4)	-28(13-I-4)	-187(6)	0	0	-20(13-I-4)
	391	-1715(13-I-4)	-28(13-I-4)	190(6)	0	0	25(8)
8036	399	-1362(13-I-4)	-19(13-II-3)	-184(6)	0	0	-13(13-II-3)
	0	-1362(13-I-4)	-19(13-II-3)	186(6)	0	0	26(9)
8037	396	-405(12-II-4)	-27(13-I-4)	-203(6)	0	0	-25(9)
	0	-405(12-II-4)	-27(13-I-4)	208(6)	0	0	19(13-I-4)
8037	398	-137(12-II-2)	-34(13-I-4)	-194(6)	0	0	-25(13-I-4)
	398	-137(12-II-2)	-34(13-I-4)	196(6)	0	0	25(13-I-4)
8037	354	-708(12-II-4)	25(13-II-4)	-192(6)	0	0	26(9)
	368	-708(12-II-4)	25(13-II-4)	190(6)	0	0	-18(13-II-4)
8037	356	-721(12-II-4)	29(13-II-4)	-194(6)	0	0	28(8)
	374	-721(12-II-4)	29(13-II-4)	193(6)	0	0	-21(13-II-4)
8037	358	-642(12-II-4)	-25(13-I-4)	-196(6)	0	0	26(9)
	364	-642(12-II-4)	-25(13-I-4)	194(6)	0	0	18(13-I-4)
8037	360	-543(12-II-4)	-10(13-I-4)	-206(6)	0	0	23(9)
	366	-543(12-II-4)	-10(13-I-4)	202(6)	0	0	10(8)
8037	362	-601(12-II-4)	12(8)	-216(6)	0	0	25(8)
	380	-601(12-II-4)	12(8)	214(6)	0	0	8(9)
8037	364	-678(12-II-4)	-25(13-I-4)	-194(6)	0	0	25(9)
	354	-678(12-II-4)	-25(13-I-4)	192(6)	0	0	18(13-I-4)
8037	366	-595(12-II-4)	-32(13-I-4)	-195(6)	0	0	27(9)
	358	-595(12-II-4)	-32(13-I-4)	193(6)	0	0	22(13-I-4)
8037	368	-723(12-II-4)	-29(13-I-4)	-192(6)	0	0	27(9)
	370	-723(12-II-4)	-29(13-I-4)	191(6)	0	0	21(13-I-4)
8037	370	-728(12-II-4)	11(9)	-192(6)	0	0	24(9)
	356	-728(12-II-4)	11(9)	191(6)	0	0	9(9)
8037	372	-407(12-II-4)	24(13-II-4)	-240(6)	0	0	28(8)
	388	-407(12-II-4)	24(13-II-4)	239(6)	0	0	-17(13-II-4)
8037	374	-704(12-II-4)	25(13-II-4)	-197(6)	0	0	27(8)
	384	-704(12-II-4)	25(13-II-4)	196(6)	0	0	-18(13-II-4)
8037	376	-642(12-II-4)	29(13-II-4)	-207(6)	0	0	28(8)
	362	-642(12-II-4)	29(13-II-4)	205(6)	0	0	-21(13-II-4)
8037	378	-237(12-II-4)	26(13-II-4)	-244(6)	0	0	29(8)
	382	-237(12-II-4)	26(13-II-4)	246(6)	0	0	-19(13-II-4)
8037	380	-548(12-II-4)	29(13-II-4)	-225(6)	0	0	29(8)
	386	-548(12-II-4)	29(13-II-4)	224(6)	0	0	-21(13-II-4)
8037	382	-163(13-I-3)	33(13-II-4)	-238(6)	0	0	32(8)
	390	-163(13-I-3)	33(13-II-4)	241(6)	0	0	-24(13-II-4)
8037	384	-679(12-II-4)	25(13-II-4)	-200(6)	0	0	27(8)
	376	-679(12-II-4)	25(13-II-4)	199(6)	0	0	-18(13-II-4)
8037	386	-484(12-II-4)	25(13-II-4)	-235(6)	0	0	28(8)
	372	-484(12-II-4)	25(13-II-4)	233(6)	0	0	-18(13-II-4)
8037	388	-324(12-II-4)	25(13-II-4)	-246(6)	0	0	28(8)
	378	-324(12-II-4)	25(13-II-4)	247(6)	0	0	-18(13-II-4)
8037	390	-130(13-I-4)	13(9)	-234(6)	0	0	25(9)
	394	-130(13-I-4)	13(9)	237(6)	0	0	7(8)
8037	392	-323(12-II-4)	-27(13-I-4)	-197(6)	0	0	25(9)
	0	-323(12-II-4)	-27(13-I-4)	200(6)	0	0	19(13-I-4)
8037	396	-480(12-II-4)	-32(13-I-4)	-206(6)	0	0	26(9)
	360	-480(12-II-4)	-32(13-I-4)	201(6)	0	0	23(13-I-4)
8037	398	-228(12-II-2)	-27(13-I-4)	-195(6)	0	0	25(9)
	392	-228(12-II-2)	-27(13-I-4)	198(6)	0	0	19(13-I-4)
8037	400	-128(13-II-4)	11(8)	-192(6)	0	0	24(8)
	0	-128(13-II-4)	11(8)	194(6)	0	0	9(9)
8038	327	-437(13-II-4)	28(13-II-1)	-92(6)	0	0	30(8)

8038	328	-437(13-I-4)	28(13-II-1)	103(6)	0	0	-19(13-II-1)
	328	-237(12-I-1)	22(13-II-4)	-102(6)	0	0	28(9)
8038	329	-237(12-I-1)	22(13-II-4)	113(6)	0	0	-17(13-II-4)
8038	329	-632(13-I-4)	22(13-II-4)	-103(6)	0	0	28(9)
	330	-632(13-I-4)	22(13-II-4)	112(6)	0	0	-16(13-II-4)
8038	330	-792(13-I-4)	22(13-II-4)	-105(6)	0	0	27(9)
	331	-792(13-I-4)	22(13-II-4)	112(6)	0	0	-17(13-II-4)
8038	331	-579(12-I-1)	21(13-II-1)	-109(6)	0	0	27(9)
	332	-579(12-I-1)	21(13-II-1)	113(6)	0	0	-16(13-II-1)
8038	332	-617(12-I-1)	23(13-II-4)	-112(6)	0	0	27(9)
	333	-617(12-I-1)	23(13-II-4)	108(6)	0	0	-17(13-II-4)
8038	333	-623(12-I-1)	19(13-II-1)	-115(6)	0	0	26(9)
	334	-623(12-I-1)	19(13-II-1)	108(6)	0	0	-14(13-II-1)
8038	334	-518(12-I-1)	22(13-II-4)	-111(6)	0	0	27(9)
	335	-518(12-I-1)	22(13-II-4)	101(6)	0	0	-16(13-II-4)
8038	335	-508(12-I-1)	20(13-II-4)	-112(6)	0	0	26(9)
	336	-508(12-I-1)	20(13-II-4)	101(6)	0	0	-15(13-II-4)
8038	336	-803(13-I-4)	20(13-II-4)	-112(6)	0	0	26(9)
	337	-803(13-I-4)	20(13-II-4)	100(6)	0	0	-15(13-II-4)
8038	337	-614(13-I-3)	16(13-II-1)	-120(6)	0	0	24(9)
	338	-614(13-I-3)	16(13-II-1)	107(6)	0	0	-13(13-II-1)
8038	338	-509(12-I-4)	26(13-II-4)	-103(6)	0	0	27(9)
	339	-509(12-I-4)	26(13-II-4)	92(6)	0	0	-18(13-II-4)
8038	339	-515(12-I-4)	-18(13-I-1)	-111(6)	0	0	24(9)
	340	-515(12-I-4)	-18(13-I-1)	100(6)	0	0	14(13-I-1)
8038	340	-498(12-I-4)	-20(13-I-4)	-111(6)	0	0	25(8)
	341	-498(12-I-4)	-20(13-I-4)	102(6)	0	0	15(13-I-4)
8038	341	-713(13-I-4)	-19(13-I-4)	-112(6)	0	0	25(9)
	342	-713(13-I-4)	-19(13-I-4)	105(6)	0	0	15(13-I-4)
8038	342	-699(13-I-3)	-19(13-I-3)	-112(6)	0	0	24(8)
	343	-699(13-I-3)	-19(13-I-3)	108(6)	0	0	15(13-I-3)
8038	343	-444(12-I-3)	-20(13-I-4)	-114(6)	0	0	24(8)
	344	-444(12-I-3)	-20(13-I-4)	115(6)	0	0	15(13-I-4)
8038	344	-468(12-I-2)	-19(13-I-1)	-116(6)	0	0	23(9)
	345	-468(12-I-2)	-19(13-I-1)	122(6)	0	0	14(13-I-1)
8038	345	-476(12-I-2)	-21(13-I-3)	-119(6)	0	0	24(8)
	346	-476(12-I-2)	-21(13-I-3)	128(6)	0	0	15(13-I-3)
8038	346	-669(13-I-4)	-20(13-I-4)	-124(6)	0	0	23(8)
	347	-669(13-I-4)	-20(13-I-4)	133(6)	0	0	15(13-I-4)
8038	347	-535(13-I-2)	-20(13-I-3)	-128(6)	0	0	23(8)
	348	-535(13-I-2)	-20(13-I-3)	135(6)	0	0	15(13-I-3)
8038	348	-560(13-I-4)	-21(13-I-1)	-134(6)	0	0	23(8)
	349	-560(13-I-4)	-21(13-I-1)	137(6)	0	0	15(13-I-1)
8038	349	-668(13-I-3)	-21(13-I-3)	-133(6)	0	0	23(8)
	350	-668(13-I-3)	-21(13-I-3)	136(6)	0	0	15(13-I-3)
8038	350	-217(13-II-2)	-21(13-I-3)	-130(6)	0	0	23(8)
	351	-217(13-II-2)	-21(13-I-3)	134(6)	0	0	16(13-I-3)
8038	351	-392(13-I-4)	-21(13-I-1)	-127(6)	0	0	21(9)
	352	-392(13-I-4)	-21(13-I-1)	133(6)	0	0	16(13-I-1)
8039	53	-1745(13-I-1)	-17(12-I-1)	-5(6)	0	0	12(13-I-1)
	55	-1745(13-I-1)	-17(12-I-1)	5(2)	0	0	21(8)
8039	54	-827(13-I-1)	13(13-II-1)	-5(9)	0	0	28(13-II-1)
	53	-827(13-I-1)	13(13-II-1)	5(6)	0	0	36(9)
8039	55	-1486(13-I-1)	23(12-I-1)	-5(1)	0	0	22(8)
	56	-1486(13-I-1)	23(12-I-1)	5(3)	0	0	15(9)
8039	56	-1308(10)	-13(12-I-1)	-5(1)	0	0	16(9)
	71	-1308(10)	-13(12-I-1)	5(6)	0	0	17(8)
8039	57	-2005(13-I-4)	-12(12-II-3)	-5(6)	0	0	12(8)
	59	-2005(13-I-4)	-12(12-II-3)	5(7)	0	0	18(9)
8039	58	-1625(13-II-2)	-22(13-II-2)	-5(1)	0	0	12(9)
	66	-1625(13-II-2)	-22(13-II-2)	5(8)	0	0	24(8)
8039	59	-1717(3)	-8(13-I-3)	-5(8)	0	0	17(9)
	65	-1717(3)	-8(13-I-3)	5(1)	0	0	19(8)
8039	60	-2648(13-I-1)	-40(13-I-1)	-5(1)	0	0	-27(13-I-1)
	57	-2648(13-I-1)	-40(13-I-1)	5(6)	0	0	13(8)
8039	61	-2596(3)	-11(3)	-5(9)	0	0	12(9)
	62	-2596(3)	-11(3)	5(1)	0	0	21(8)

8039	62	-2664(3)	14(13-14)	-5(8)	0	0	20(8)
	63	-2664(3)	14(13-14)	5(1)	0	0	13(9)
8039	63	-2661(3)	-19(13-14)	-5(2)	0	0	11(9)
	64	-2661(3)	-19(13-14)	5(6)	0	0	26(8)
8039	64	-2163(3)	51(13-1)	-5(1)	0	34(13-1)	0
	60	-2163(3)	51(13-1)	5(8)	0	0	21(8)
8039	65	-1454(3)	-13(13-1)	-5(1)	0	0	18(8)
	58	-1454(3)	-13(13-1)	5(6)	0	0	14(9)
8039	66	-1820(13-12)	-42(13-1)	-5(9)	0	0	23(8)
	67	-1820(13-12)	-42(13-1)	0	27(13-1)	0	0
8039	67	-808(13-12)	50(13-1)	-5(6)	0	0	20(8)
	68	-808(13-12)	50(13-1)	5(1)	0	-3(113-1)	0
8039	68	-2912(3)	15(13-14)	-5(1)	0	0	19(8)
	77	-2912(3)	15(13-14)	5(9)	0	0	15(9)
8039	70	-2622(3)	-12(12-1)	-5(8)	0	0	16(9)
	69	-2622(3)	-12(12-1)	5(1)	0	0	19(8)
8039	71	-1916(3)	7(13-1)	-5(9)	0	0	17(8)
	74	-1916(3)	7(13-1)	5(1)	0	0	19(8)
8039	72	-2250(3)	-10(12-1)	-5(4)	0	0	11(9)
	70	-2250(3)	-10(12-1)	5(6)	0	0	17(9)
8039	73	-2744(13-1)	21(13-12)	-5(3)	0	0	22(8)
	61	-2744(13-1)	21(13-12)	5(4)	0	0	12(9)
8039	74	-2482(3)	22(13-12)	-5(9)	0	0	21(8)
	76	-2482(3)	22(13-12)	5(1)	0	0	-14(13-12)
8039	75	-2561(13-1)	29(13-12)	-5(8)	0	0	27(8)
	72	-2561(13-1)	29(13-12)	5(1)	0	0	10(9)
8039	76	-1981(3)	-33(13-12)	-5(1)	0	0	-14(13-12)
	75	-1981(3)	-33(13-12)	5(6)	0	0	28(8)
8039	77	-3153(3)	-24(13-1)	-5(1)	0	0	15(9)
	78	-3153(3)	-24(13-1)	5(3)	0	0	14(8)
8039	78	-2566(3)	28(13-1)	-5(1)	0	0	13(13-1)
	73	-2566(3)	28(13-1)	5(5)	0	0	23(8)

Scenario di calcolo : Set NT, SLV, A2, STR/GEO													
Asta	N.in	N	kg	Ty	kg	Tz	kg	Mt	kg*m	My	kg*m	Mz	kg*m
		N fin.											
1	1	1	-16835(13-1)	-907(13-1)	-1102(12-1)	-6(13-1)	1975(12-1)	-1927(13-1)	660(8)	-1398(9)	694(8)	59(13-14)	-1919(13-1)
	54	54	-1669(13-1)	-907(13-1)	-1102(12-1)	-6(13-1)	-1398(9)	660(8)	-1552(9)	694(8)	59(13-14)	-1919(13-1)	656(8)
1	54	54	-7725(13-1)	401(8)	-1029(12-1)	6(8)	-1552(9)	694(8)	-2785(3)	2675(12-1)	-1706(2)	663(8)	140(13-1)
	101	101	-7624(13-1)	401(8)	-1302(10)	6(8)	-2785(3)	59(13-14)	-1919(13-1)	-1706(2)	663(8)	140(13-1)	-1915(13-1)
2	2	2	-11827(13-1)	-884(13-1)	-156(12)	-4(13-1)	2675(12-1)	-1919(13-1)	656(8)	-1847(9)	663(8)	140(13-1)	-1915(13-1)
	53	53	-11682(13-1)	-884(13-1)	-1589(3)	-4(13-1)	-1847(9)	663(8)	-1532(3)	-5(13-1)	-4575(3)	140(13-1)	-1915(13-1)
2	53	53	-5711(13-1)	382(8)	-1532(3)	-5(13-1)	-4575(3)	140(13-1)	-2062(6)	-5(13-1)	-4575(3)	140(13-1)	-1915(13-1)
	102	102	-5611(13-1)	382(8)	-1703(2)	-1703(2)	-1703(2)	0	3195(12-1)	3195(12-1)	-1707(2)	637(8)	600(8)
3	3	3	-7218(6)	-865(13-1)	-1807(3)	0	-1707(2)	637(8)	-1807(3)	0	-1707(2)	637(8)	600(8)
	55	55	-7030(6)	-865(13-1)	-1807(3)	0	-1707(2)	637(8)	-1835(3)	-2(10)	-1708(2)	600(8)	116(13-1)
3	55	55	-7021(6)	368(8)	-1835(3)	-2(10)	-1708(2)	600(8)	-2370(6)	-2(10)	-4952(3)	116(13-1)	-1916(13-1)
	103	103	-6890(6)	368(8)	-2370(6)	-2(10)	-4952(3)	116(13-1)	-1684(2)	0	2780(12-1)	-1916(13-1)	-1915(13-1)
4	4	4	-7044(6)	-855(13-1)	-1779(3)	0	-1695(9)	603(8)	-1779(3)	0	-1695(9)	603(8)	570(8)
	56	56	-6856(6)	-855(13-1)	-1779(3)	0	-1695(9)	603(8)	-1824(3)	-2(13-1)	-1694(9)	570(8)	95(13-14)
4	56	56	-6847(6)	337(9)	-1824(3)	-2(13-1)	-1694(9)	570(8)	-2351(6)	-2(13-1)	-4914(3)	95(13-14)	-1899(13-1)
	104	104	-6716(6)	337(9)	-2351(6)	-2(13-1)	-4914(3)	95(13-14)	-1696(2)	0	2926(12-1)	-1899(13-1)	-1899(13-1)
5	5	5	-7317(6)	-835(13-1)	-1696(2)	0	2926(12-1)	-1899(13-1)	-1820(3)	0	-1653(9)	590(8)	558(8)
	71	71	-7129(6)	-835(13-1)	-1820(3)	0	-1653(9)	590(8)	-1912(3)	-2(13-1)	-1655(9)	558(8)	127(13-1)
5	71	71	-7120(6)	336(8)	-1912(3)	-2(13-1)	-1655(9)	558(8)	-2449(6)	-2(13-1)	-5027(3)	127(13-1)	-1882(13-1)
	105	105	-6989(6)	336(8)	-2449(6)	-2(13-1)	-5027(3)	127(13-1)	-828(13-1)	1(13-1)	2825(12-1)	-1882(13-1)	-1882(13-1)
6	6	6	-7386(6)	-828(13-1)	-1706(2)	1(13-1)	2825(12-1)	-1882(13-1)	-1839(3)	1(13-1)	-1651(2)	583(8)	554(8)
	74	74	-7198(6)	-828(13-1)	-1839(3)	1(13-1)	-1651(2)	583(8)	-1952(3)	-2(13-1)	-1656(2)	554(8)	136(13-1)
6	74	74	-7188(6)	317(9)	-1952(3)	-2(13-1)	-1656(2)	554(8)	-2489(6)	-2(13-1)	-5097(3)	136(13-1)	-1842(13-1)
	106	106	-7057(6)	317(9)	-2489(6)	-2(13-1)	-5097(3)	136(13-1)	-801(13-1)	0	2540(12-1)	-1842(13-1)	-1842(13-1)
7	7	7	-17395(13-1)	-801(13-1)	-1624(2)	0	2540(12-1)	-1842(13-1)	-1744(3)	0	-1644(9)	561(8)	599(8)
	76	76	-17251(13-1)	-801(13-1)	-1744(3)	0	-1644(9)	561(8)	-1894(3)	-1(13-1)	-1646(9)	599(8)	138(13-12)
7	76	76	-9004(6)	330(9)	-1894(3)	-1(13-1)	-1646(9)	599(8)	-2427(6)	-1(13-1)	-4960(3)	138(13-12)	-1799(13-1)
	107	107	-8873(6)	330(9)	-2427(6)	-1(13-1)	-4960(3)	138(13-12)	-775(13-1)	0	2608(12-1)	-1799(13-1)	-1799(13-1)
8	8	8	-14817(13-1)	-775(13-1)	-1794(2)	0	2608(12-1)	-1799(13-1)					

8	75	-14672(13-1)	-775(13-1)	-1918(3)	0	-1650(9)	542(8)
	75	-7173(13-1)	294(9)	-2037(3)	-1(12-1)	-1653(9)	566(8)
108	108	-7073(13-1)	294(9)	-2566(6)	-1(12-1)	-5222(3)	149(13-12)
	9	-7159(6)	-748(13-1)	-1592(2)	1(13-1)	2470(12-1)	-1747(13-12)
8039	9	-6970(6)	-748(13-1)	-1695(3)	1(13-1)	-1628(9)	546(8)
	72	-6961(6)	322(8)	-1802(3)	-2(13-1)	-1629(9)	522(8)
8039	72	-6830(6)	322(8)	-2337(6)	-2(13-1)	-4772(3)	127(13-1)
	10	-7145(6)	-715(13-1)	-1605(2)	0	2564(12-1)	-1696(13-1)
8039	70	-6956(6)	-715(13-1)	-1708(3)	0	-1613(9)	523(8)
	70	-6947(6)	325(8)	-1821(3)	-1(13-1)	-1616(9)	501(8)
8039	110	-6816(6)	325(8)	-2356(6)	-1(13-1)	-4808(3)	95(13-1)
	11	-7435(6)	-690(13-1)	-1620(2)	0	2505(12-1)	-1650(13-1)
8039	69	-7247(6)	-690(13-1)	-1724(3)	0	-1597(9)	503(8)
	69	-7237(6)	306(9)	-1902(3)	-2(13-1)	-1602(9)	484(8)
8039	111	-7106(6)	306(9)	-2432(6)	-2(13-1)	-4908(3)	71(13-12)
	12	-7045(6)	-673(13-1)	-1511(2)	1(13-1)	2462(12-1)	-1611(13-1)
8039	77	-6856(6)	-673(13-1)	-1599(3)	1(13-1)	-1578(9)	497(8)
	77	-6847(6)	295(9)	-1771(3)	-2(13-1)	-1583(9)	479(8)
8039	112	-6716(6)	295(9)	-2304(6)	-2(13-1)	-4667(3)	125(13-1)
	13	-15685(13-1)	-655(13-1)	-1575(2)	0	2499(12-1)	-1569(13-1)
8039	78	-15540(13-1)	-655(13-1)	-1670(3)	0	-1634(9)	482(9)
	78	-7749(6)	328(9)	-1809(3)	1(8)	-1637(9)	519(8)
8039	113	-7618(6)	328(9)	-2341(6)	1(8)	-4785(3)	83(13-1)
	14	-15919(13-1)	662(13-1)	-1620(2)	0	2399(12-1)	1576(13-1)
8039	73	-15774(13-1)	662(13-1)	-1713(3)	0	-1587(9)	487(8)
	73	-7416(13-1)	349(8)	-1874(3)	0	-1591(9)	507(9)
8039	114	-7315(13-1)	349(8)	-2404(6)	0	-4848(3)	-78(8)
	15	-6982(6)	679(13-1)	-1545(2)	-1(13-1)	2321(12-1)	1610(13-1)
8039	61	-6794(6)	679(13-1)	-1630(3)	-1(13-1)	-1588(9)	471(9)
	61	-6785(6)	314(8)	-1748(3)	2(13-1)	-1590(9)	458(9)
8039	115	-6654(6)	314(8)	-2281(6)	2(13-1)	-4638(3)	-126(13-1)
	16	-7355(6)	696(13-1)	-1604(2)	0	2367(12-1)	1644(13-1)
8039	62	-7167(6)	696(13-1)	-1699(3)	0	-1601(9)	454(9)
	62	-7157(6)	314(8)	-1869(3)	2(13-1)	-1605(9)	442(9)
8039	116	-7026(6)	717(13-1)	-2398(6)	2(13-1)	-4857(3)	-86(8)
	17	-7072(6)	717(13-1)	-1554(2)	0	2395(12-1)	1680(13-1)
8039	63	-6883(6)	717(13-1)	-1645(3)	0	-1612(9)	441(9)
	63	-6874(6)	292(9)	-1773(3)	1(8)	-1615(9)	432(9)
8039	117	-6743(6)	292(9)	-2307(6)	1(8)	-4710(3)	-119(13-1)
	18	-14652(13-1)	777(13-1)	-1641(2)	-2(13-1)	2545(12-1)	1746(13-1)
8039	64	-14507(13-1)	777(13-1)	-1749(3)	-2(13-1)	-1627(9)	461(9)
	64	-7192(6)	292(9)	-1920(3)	4(13-1)	-1608(2)	413(9)
8039	118	-7061(6)	292(9)	-2450(6)	4(13-1)	-499(3)	-119(13-1)
	19	-16975(13-1)	759(13-1)	-1676(2)	2(13-1)	2337(12-1)	1760(13-1)
8039	60	-16830(13-1)	759(13-1)	-1785(3)	2(13-1)	-1621(9)	426(9)
	19	-7908(13-1)	345(8)	-1901(3)	2(8)	-1609(9)	446(9)
8039	119	-7808(13-1)	345(8)	-2436(6)	2(8)	-4953(3)	-139(8)
	20	-7235(6)	770(13-1)	-1627(2)	-2(13-1)	2363(12-1)	1790(13-1)
8039	57	-7047(6)	770(13-1)	-1738(3)	-2(13-1)	-1617(9)	410(9)
	57	-7037(6)	304(8)	-1863(3)	3(13-1)	-1618(9)	405(9)
8039	120	-6906(6)	304(8)	-2398(6)	3(13-1)	-4872(3)	-152(13-1)
	21	-7207(6)	782(13-1)	-1712(2)	0	2329(12-1)	1816(13-1)
8039	59	-7019(6)	782(13-1)	-1825(3)	0	-1646(9)	405(9)
	21	-7010(6)	340(8)	-1913(3)	2(13-1)	-1648(9)	400(9)
8039	121	-6879(6)	340(8)	-2444(6)	2(13-1)	-5013(3)	-179(3)
	22	-7179(6)	787(13-1)	-1693(2)	0	2407(13-12)	1831(13-1)
8039	65	-6990(6)	787(13-1)	-1807(3)	0	-1628(2)	384(9)
	22	-6981(6)	283(9)	-1890(3)	3(13-1)	-1632(2)	384(9)
8039	122	-6850(6)	283(9)	-2425(6)	3(13-1)	-4958(3)	-129(13-1)
	23	-6773(6)	813(13-1)	-1628(2)	0	2384(13-12)	1856(13-1)
8039	58	-6585(6)	813(13-1)	-1716(3)	0	-1627(2)	393(9)
	58	-6576(6)	314(8)	-1782(3)	3(3)	-35(3)	392(9)
8039	123	-6445(6)	314(8)	-2310(6)	3(3)	-4772(3)	-141(8)
	24	-7155(6)	835(13-1)	-1650(2)	1(13-1)	2628(13-12)	1868(13-1)
8039	66	-6966(6)	835(13-1)	-1749(3)	1(13-1)	-1656(2)	390(9)
	66	-6957(6)	275(9)	-1821(3)	3(13-1)	-1660(2)	392(9)
8039	124	-6826(6)	275(9)	-2355(6)	3(13-1)	-4870(3)	-122(13-1)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Pilastri

25	25	-11488(3-II-1)	839(13-I-1)	-1412(2)	2(6)	2324(13-II-2)	1864(13-I-1)
67	67	-11343(3-II-1)	839(13-I-1)	-1435(3)	2(6)	-1687(2)	408(9)
25	67	-5664(3-II-2)	330(8)	-1492(3)	2(13-II-1)	-1665(2)	426(9)
125	125	-5564(3-II-2)	330(8)	-2019(6)	2(13-II-1)	-431(3-I)	-189(13-I-1)
26	26	-16543(13-I-1)	897(13-I-1)	-1084(13-I-2)	3(13-II-3)	1720(13-II-2)	1899(13-I-1)
68	68	-16398(13-I-1)	897(13-I-1)	-1084(13-I-2)	3(13-II-3)	-1434(9)	422(9)
26	68	-7658(13-I-2)	330(9)	-1080(13-I-2)	6(13-I-2)	-1414(9)	436(9)
126	126	-7557(13-I-2)	330(9)	-1366(10)	6(13-I-2)	-279(3)	-121(8)
27	1	-1766(3)	-687(13-II-4)	4680(13-I-4)	-7(13-II-4)	3713(13-I-4)	-392(13-I-4)
327	327	-1719(3)	-687(13-II-4)	4680(13-I-4)	-7(13-II-4)	1895(12-I-1)	30(13-II-4)
28	25	-2065(13-I-2)	656(13-I-4)	3892(13-I-4)	6(13-I-3)	3194(13-I-3)	436(13-I-4)
351	351	-2029(13-I-2)	656(13-I-4)	3892(13-I-4)	6(13-I-3)	2587(13-I-2)	441(13-I-4)
29	24	-2425(3)	707(13-I-4)	2725(6)	7(13-I-3)	2449(13-II-2)	382(13-I-4)
350	350	-2378(3)	707(13-I-4)	2725(6)	7(13-I-3)	2366(13-II-2)	-501(3-I-4)
30	23	-2519(3)	829(13-I-4)	2751(6)	6(13-I-3)	2206(13-II-2)	532(13-I-4)
349	349	-2472(3)	829(13-I-4)	2751(6)	6(13-I-3)	2194(13-I-2)	-46(13-II-4)
348	348	-2463(3)	755(13-I-4)	2602(6)	6(13-I-3)	2045(13-II-2)	415(13-I-4)
32	21	-2492(3)	813(13-I-4)	2574(6)	6(13-I-3)	2120(13-II-2)	-44(13-I-4)
33	20	-2435(3)	657(13-I-4)	2523(6)	6(13-I-3)	1927(12-I-2)	504(13-I-4)
34	19	-2557(3)	-721(13-II-4)	3797(13-I-4)	6(13-I-4)	3521(13-II-4)	445(13-I-4)
35	18	-2275(3)	773(13-I-4)	3703(13-I-3)	6(13-I-4)	2338(13-II-3)	341(3-I-2)
344	344	-2228(3)	773(13-I-4)	3703(13-I-3)	6(13-I-4)	3444(13-I-3)	455(13-I-4)
36	17	-2319(3)	696(13-I-4)	2497(6)	6(13-I-4)	2457(13-I-3)	-30(13-II-3)
343	343	-2272(3)	696(13-I-4)	2497(6)	6(13-I-4)	2087(12-I-3)	382(13-I-4)
37	16	-2394(3)	797(13-I-4)	2405(6)	6(13-I-4)	2070(12-I-3)	-43(13-I-4)
342	342	-2347(3)	797(13-I-4)	2405(6)	6(13-I-4)	2080(12-I-3)	524(13-I-4)
38	15	-2356(3)	-699(13-II-4)	2391(6)	6(13-I-4)	2057(12-I-3)	461(3-I-4)
341	341	-2309(3)	-699(13-II-4)	2391(6)	6(13-I-4)	2059(12-I-4)	383(13-I-4)
39	14	-2538(3)	-782(13-II-4)	3748(13-I-4)	6(13-I-4)	2053(12-I-4)	47(13-II-4)
40	13	-2273(3)	-782(13-II-4)	3748(13-I-4)	6(13-I-4)	3412(13-II-4)	458(13-I-4)
41	12	-2370(3)	-686(13-II-4)	2503(6)	-6(13-II-4)	2291(13-II-4)	34(13-II-4)
338	338	-2323(3)	-686(13-II-4)	2503(6)	-6(13-II-4)	3278(13-I-4)	450(13-I-3)
42	11	-2483(3)	773(13-I-4)	2417(6)	-6(13-I-4)	2298(13-I-3)	-35(13-II-3)
337	337	-2436(3)	773(13-I-4)	2417(6)	-6(13-I-4)	2227(12-I-4)	-374(13-II-4)
43	10	-2422(3)	-570(13-II-4)	2513(6)	-6(13-II-4)	2161(12-I-4)	45(13-II-4)
336	336	-2375(3)	-570(13-II-4)	2513(6)	-6(13-II-4)	2277(12-I-4)	-313(13-II-4)
44	9	-2439(3)	-526(13-II-4)	2498(6)	-6(13-II-4)	2218(12-I-4)	37(13-II-4)
335	335	-2392(3)	-526(13-II-4)	2498(6)	-6(13-II-4)	2278(12-I-4)	-287(13-II-4)
45	8	-2663(3)	679(13-I-4)	4211(13-I-4)	-6(13-I-1)	2192(12-I-4)	39(13-I-4)
334	334	-2616(3)	679(13-I-4)	4211(13-I-4)	-6(13-I-1)	2192(12-I-4)	39(13-I-4)
46	7	-2458(3)	-712(13-II-4)	3975(13-I-4)	-7(13-II-4)	3547(13-II-4)	-448(13-II-4)
333	333	-2411(3)	-712(13-II-4)	3975(13-I-4)	-7(13-II-4)	2419(12-I-1)	-47(13-II-4)
47	6	-2517(3)	-532(13-II-4)	2669(6)	-7(13-II-4)	3523(13-I-4)	-440(13-II-4)
332	332	-2470(3)	-532(13-II-4)	2669(6)	-7(13-II-4)	2350(12-I-1)	-29(13-II-1)
48	5	-2516(3)	-615(13-II-4)	2603(6)	-7(13-II-4)	2622(12-I-1)	-300(13-II-4)
331	331	-2469(3)	-615(13-II-4)	2603(6)	-7(13-II-4)	2496(12-I-1)	-35(13-I-4)
49	4	-2467(3)	-864(13-II-4)	2676(6)	-7(13-II-4)	2817(12-I-1)	-340(13-I-4)
330	330	-2420(3)	-864(13-II-4)	2676(6)	-7(13-II-4)	2644(12-I-1)	38(13-II-4)
50	3	-2419(3)	-768(13-II-4)	2700(12-I-1)	-7(13-II-4)	2841(12-I-1)	-555(13-II-4)
329	329	-2372(3)	-768(13-II-4)	2700(12-I-1)	-7(13-II-4)	2615(12-I-1)	48(13-I-4)
51	2	-2170(8)	-761(13-II-4)	3928(13-I-4)	-7(13-II-4)	2615(12-I-1)	48(13-I-4)
328	328	-2123(8)	-761(13-II-4)	3928(13-I-4)	-7(13-II-4)	3030(12-I-1)	-415(13-II-4)
52	26	-1892(3)	559(13-I-4)	4521(13-I-4)	7(13-I-3)	2791(12-I-1)	55(13-I-4)
352	352	-1845(3)	559(13-I-4)	4521(13-I-4)	7(13-I-3)	3213(13-II-4)	-494(13-I-4)
						2442(13-II-1)	-40(13-II-4)
						3668(13-II-4)	32(13-I-4)
						1788(13-II-2)	32(13-II-4)

7002	53	-4041(13-I-1)	0	1(1)	0	0	2(9)
7003	53	5681(13-I-1)	0	-1(1)	0	0	1(9)
7004	101	5684(13-I-1)	0	1(1)	0	0	2(9)
7005	101	2167(13-I-1)	0	-2(1)	0	0	1(8)
7006	0	2172(13-I-1)	0	2(1)	0	0	1(9)
7007	0	-1162(13-I-4)	0	-2(1)	0	0	1(8)
7008	0	-1158(13-I-4)	0	2(1)	0	0	1(9)
7009	75	-2075(13-I-1)	0	-3(1)	0	0	1(9)
7010	75	2688(13-I-4)	0	-3(1)	0	0	1(9)
7011	399	2689(13-I-4)	0	3(8)	0	0	1(9)
7012	399	582(13-I-4)	0	-3(1)	0	0	1(9)
7013	328	582(13-II-4)	0	3(1)	0	0	1(9)
7014	327	-498(13-II-4)	0	-3(1)	0	0	1(8)
7015	0	-498(13-II-4)	0	3(1)	0	0	1(9)
7016	0	-2908(13-I-4)	0	-3(1)	0	0	1(8)
7017	73	-2909(13-I-4)	0	3(1)	0	0	1(8)
7018	73	1787(13-I-1)	0	-3(1)	0	0	1(8)
7019	0	835(13-I-4)	0	-2(1)	0	0	1(8)
7020	0	835(13-I-4)	0	2(1)	0	0	1(9)
7021	102	2231(13-I-1)	0	-2(1)	0	0	1(8)
7022	102	-5976(13-II-1)	0	-1(1)	0	0	2(9)
7023	54	-5979(13-II-1)	0	1(1)	0	0	2(8)
7024	54	3957(13-I-1)	0	-1(2)	0	0	2(8)
7025	2	3953(13-I-1)	0	1(1)	0	0	2(8)
7026	25	3790(13-I-1)	0	-1(1)	0	0	2(8)
7027	68	3795(13-I-1)	0	1(1)	0	0	2(9)
7028	68	-5899(13-I-1)	0	-1(1)	0	0	2(8)
7029	125	-5895(13-I-1)	0	1(8)	0	0	2(9)
7030	125	2194(13-I-2)	0	-2(1)	0	0	1(8)
7031	0	2199(13-I-2)	0	2(1)	0	0	1(9)
7032	0	871(13-II-4)	0	-2(1)	0	0	1(9)
7033	0	871(13-II-4)	0	2(1)	0	0	1(8)
7034	0	1755(13-II-4)	0	-3(1)	0	0	1(9)
7035	67	1758(13-I-4)	0	3(1)	0	0	1(8)
7036	67	-2965(13-I-4)	0	-3(1)	0	0	1(8)
7037	389	-2964(13-I-4)	0	3(1)	0	0	1(8)
7038	389	-393(13-I-4)	0	-3(1)	0	0	1(9)
7039	352	-393(13-I-4)	0	3(1)	0	0	1(8)
7040	351	467(13-I-4)	0	-3(1)	0	0	1(9)
7041	393	467(13-I-4)	0	3(8)	0	0	1(9)
7042	393	2721(13-I-4)	0	-3(1)	0	0	1(9)
7043	63	2719(13-II-4)	0	3(1)	0	0	1(9)
7044	63	-2067(13-II-4)	0	-3(2)	0	0	1(9)
7045	0	-2070(13-I-4)	0	3(1)	0	0	1(9)
7046	0	-1192(13-I-4)	0	-2(1)	0	0	1(9)
7047	0	-1196(13-I-4)	0	2(1)	0	0	1(8)
7048	126	2070(13-II-1)	0	-2(1)	0	0	1(9)
7049	126	2066(13-II-1)	0	2(1)	0	0	1(8)
7050	126	5753(13-I-1)	0	0	0	0	2(9)
7051	67	5750(13-I-1)	0	1(1)	0	0	2(8)
7052	67	-3928(13-I-1)	0	-1(1)	0	0	2(9)
7053	26	-3933(13-I-1)	0	1(1)	0	0	2(8)
7054	102	1655(13-I-4)	0	-3(1)	0	0	1(8)
7055	102	1655(13-I-4)	0	3(1)	0	0	1(9)
7056	104	-1395(13-I-4)	0	-3(1)	0	0	1(9)
7057	0	-1390(13-I-4)	0	3(1)	0	0	1(8)
7058	328	-1203(13-I-4)	0	-4(1)	0	0	1(9)
7059	391	-1203(13-I-4)	0	4(1)	0	0	1(8)
7060	330	-1416(13-I-4)	0	-4(1)	0	0	1(9)
7061	0	-1416(13-I-4)	0	4(1)	0	0	1(8)
7062	19	-3834(13-I-1)	0	-1(1)	0	0	2(8)
7063	64	-3829(13-I-1)	0	1(1)	0	0	2(8)
7064	64	6064(13-I-1)	0	-1(1)	0	0	2(9)
7065	119	6067(13-I-1)	0	1(2)	0	0	2(8)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi -ASTE generiche

Scenario di calcolo : Set NT SLV A2 STR/GEO							
Asta	N.in.	N	Ty	Tz	Mt	My	Mz
			kg	kg	kg*m	kg*m	kg*m
7001	N.fin	1	-4046(13-II-1)	0	-1(8)	0	2(8)

7035	119	2532(13-II-1)	0	-2(1)	0	0	0	1(9)
	174	2536(13-II-1)	0	2(1)	0	0	0	1(8)
7036	174	-1454(13-II-4)	0	2(1)	0	0	0	1(9)
	0	-1450(13-II-4)	0	-2(1)	0	0	0	1(9)
7037	0	-1818(13-II-1)	0	-3(1)	0	0	0	1(8)
	35	-1815(13-II-1)	0	3(1)	0	0	0	1(8)
7038	35	3119(13-II-4)	0	-2(1)	0	0	0	1(9)
	379	3121(13-II-4)	0	2(2)	0	0	0	1(8)
7039	379	272(13-I-4)	0	-3(8)	0	0	0	1(8)
	344	-272(13-II-4)	0	3(1)	0	0	0	1(8)
7040	345	-296(13-I-4)	0	-3(1)	0	0	0	1(8)
	361	-295(13-I-4)	0	3(1)	0	0	0	1(8)
7041	361	-302(13-II-4)	0	-3(1)	0	0	0	1(8)
	53	-3022(13-II-4)	0	3(1)	0	0	0	1(9)
7042	53	-1719(13-I-1)	0	-3(1)	0	0	0	1(8)
	176	-1722(13-I-1)	0	3(1)	0	0	0	1(8)
7043	176	1157(13-II-4)	0	-2(1)	0	0	0	1(9)
	0	1153(13-II-4)	0	2(1)	0	0	0	1(9)
7044	0	2316(13-I-1)	0	-2(1)	0	0	0	1(8)
	118	2312(13-I-1)	0	2(1)	0	0	0	1(9)
7045	123	1970(13-II-4)	0	-1(1)	0	0	0	2(8)
	60	-6304(13-I-1)	0	1(8)	0	0	0	2(9)
7046	60	3573(13-I-1)	0	-1(1)	0	0	0	2(8)
	18	3568(13-I-1)	0	1(1)	0	0	0	2(8)
7047	199	1975(13-II-4)	0	-3(1)	0	0	0	1(9)
	123	1970(13-II-4)	0	3(1)	0	0	0	1(8)
7048	123	-1408(13-II-3)	0	-3(1)	0	0	0	1(8)
	0	-1404(13-II-3)	0	3(8)	0	0	0	1(9)
7049	125	1622(13-II-4)	0	-3(8)	0	0	0	1(9)
	0	1626(13-II-4)	0	3(1)	0	0	0	1(8)
7050	0	-1782(13-II-4)	0	-3(1)	0	0	0	1(8)
	121	-1786(13-II-4)	0	3(1)	0	0	0	1(9)
7051	121	1946(13-II-4)	0	-3(1)	0	0	0	1(9)
	0	1950(13-II-4)	0	3(1)	0	0	0	1(8)
7052	379	-1166(13-I-4)	0	-4(1)	0	0	0	1(8)
	347	-1167(13-I-4)	0	4(1)	0	0	0	1(9)
7053	347	-835(13-II-4)	0	-4(1)	0	0	0	1(8)
	377	-834(13-II-4)	0	4(1)	0	0	0	1(9)
7054	377	-1010(13-I-4)	0	-4(1)	0	0	0	1(8)
	351	-1011(13-I-4)	0	4(1)	0	0	0	1(9)
7055	371	-969(13-II-4)	0	-4(1)	0	0	0	1(8)
	345	-970(13-II-4)	0	4(8)	0	0	0	1(9)
7056	389	-1354(13-II-4)	0	-4(1)	0	0	0	0
	349	-1354(13-II-4)	0	4(1)	0	0	0	0
7057	349	-907(13-I-4)	0	-4(1)	0	0	0	0
	371	-907(13-I-4)	0	4(1)	0	0	0	0
7058	199	-1755(13-II-4)	0	-3(1)	0	0	0	0
	119	-1760(13-II-4)	0	3(1)	0	0	0	0
7059	108	-6566(13-II-1)	0	-1(1)	0	0	0	0
	76	-6570(13-II-1)	0	1(1)	0	0	0	0
7060	76	3770(13-II-1)	0	-1(1)	0	0	0	0
	8	3766(13-II-1)	0	1(1)	0	0	0	0
7061	7	-3981(13-II-1)	0	-1(1)	0	0	0	0
	75	-3976(13-II-1)	0	1(1)	0	0	0	0
7062	75	6272(13-II-1)	0	-1(1)	0	0	0	0
	107	6275(13-II-1)	0	1(1)	0	0	0	0
7063	107	2570(13-I-1)	0	-2(1)	0	0	0	0
	184	2575(13-I-1)	0	2(1)	0	0	0	0
7064	184	-1492(13-I-4)	0	-2(1)	0	0	0	0
	171	-1488(13-I-4)	0	2(1)	0	0	0	0
7065	171	-1867(13-I-1)	0	-3(1)	0	0	0	0
	39	-1864(13-I-1)	0	3(1)	0	0	0	0
7066	39	2919(13-I-4)	0	-3(1)	0	0	0	0
	359	2921(13-I-4)	0	3(1)	0	0	0	0
7067	359	385(13-II-4)	0	-3(1)	0	0	0	0
	334	384(13-II-4)	0	3(1)	0	0	0	0
7068	333	-394(13-II-4)	0	-3(1)	0	0	0	0

7069	365	-394(13-I-4)	0	3(1)	0	0	0	0
	365	-3029(13-I-4)	0	-3(1)	0	0	0	0
7070	33	-1859(13-II-1)	0	3(1)	0	0	0	0
	33	-1859(13-II-1)	0	-3(1)	0	0	0	0
7071	186	1312(13-I-4)	0	3(1)	0	0	0	0
	186	1312(13-I-4)	0	-2(1)	0	0	0	0
7072	169	1308(13-I-4)	0	2(1)	0	0	0	0
	169	-2398(13-I-1)	0	-2(1)	0	0	0	0
7073	108	-2403(13-I-1)	0	2(1)	0	0	0	0
	107	-2090(13-I-4)	0	-4(1)	0	0	0	0
7074	107	-2095(13-I-4)	0	4(1)	0	0	0	0
	164	2209(13-I-4)	0	-4(1)	0	0	0	0
	169	2214(13-I-4)	0	4(1)	0	0	0	0
7075	391	-997(13-I-4)	0	-5(1)	0	0	0	0
	333	-997(13-I-4)	0	5(1)	0	0	0	0
7076	359	-1112(13-I-4)	0	-5(1)	0	0	0	0
	330	-1112(13-I-4)	0	5(1)	0	0	0	0
7077	108	2171(13-I-4)	0	-4(1)	0	0	0	0
	154	2175(13-I-4)	0	4(1)	0	0	0	0
7078	184	-2082(13-I-4)	0	-4(1)	0	0	0	0
	111	-2087(13-I-4)	0	4(1)	0	0	0	0
7079	111	1777(13-I-4)	0	-3(1)	0	0	0	0
	194	1781(13-I-4)	0	3(1)	0	0	0	0
7080	194	2399(13-II-1)	0	-2(1)	0	0	0	0
	114	2394(13-II-1)	0	2(1)	0	0	0	0
7081	114	-5979(13-II-1)	0	-1(1)	0	0	0	0
	78	-5982(13-II-1)	0	1(1)	0	0	0	0
7082	78	-3439(13-I-1)	0	-1(1)	0	0	0	0
	14	-3444(13-I-1)	0	1(1)	0	0	0	0
7083	13	-3435(13-II-1)	0	-1(1)	0	0	0	0
	73	-3430(13-II-1)	0	1(1)	0	0	0	0
7084	73	-6044(13-I-1)	0	-1(1)	0	0	0	0
	113	-6040(13-I-1)	0	1(1)	0	0	0	0
7085	113	2401(13-I-1)	0	-2(1)	0	0	0	0
	159	2405(13-I-1)	0	2(1)	0	0	0	0
7086	159	-1222(13-I-4)	0	-2(1)	0	0	0	0
	196	-1218(13-I-4)	0	2(1)	0	0	0	0
7087	196	-1880(13-I-1)	0	-3(1)	0	0	0	0
	29	-1877(13-I-1)	0	3(1)	0	0	0	0
7088	161	-1179(13-I-4)	0	-2(1)	0	0	0	0
	194	-1183(13-II-4)	0	2(1)	0	0	0	0
7089	154	-1614(13-I-4)	0	-3(1)	0	0	0	0
	113	-1619(13-I-4)	0	3(1)	0	0	0	0
7090	161	-1811(13-I-1)	0	-3(1)	0	0	0	0
	43	-1808(13-II-1)	0	3(1)	0	0	0	0
7091	43	-2959(13-I-4)	0	-3(1)	0	0	0	0
	355	-2957(13-I-4)	0	3(1)	0	0	0	0
7092	355	-293(13-I-4)	0	-3(1)	0	0	0	0
	339	-294(13-I-4)	0	3(1)	0	0	0	0
7093	340	-308(13-I-4)	0	-3(1)	0	0	0	0
	369	-308(13-I-4)	0	3(1)	0	0	0	0
7094	369	-2941(13-II-4)	0	-3(1)	0	0	0	0
	29	-2943(13-I-4)	0	3(1)	0	0	0	0
7095	114	-1614(13-I-4)	0	-3(1)	0	0	0	0
	0	-1609(13-II-4)	0	3(1)	0	0	0	0
7096	0	1821(13-II-4)	0	-3(1)	0	0	0	0
	118	1816(13-II-4)	0	3(1)	0	0	0	0
7097	174	-1692(13-I-4)	0	-3(1)	0	0	0	0
	116	-1697(13-I-4)	0	3(1)	0	0	0	0
7098	116	1722(13-I-4)	0	-3(1)	0	0	0	0
	159	1727(13-I-4)	0	3(1)	0	0	0	0
7099	340	-1076(13-II-4)	0	-4(1)	0	0	0	0
	383	-1076(13-II-4)	0	4(1)	0	0	0	0
7100	383	-1071(13-I-4)	0	-4(1)	0	0	0	0
	344	-1071(13-I-4)	0	4(1)	0	0	0	0
7101	361	-1221(13-I-4)	0	-4(1)	0	0	0	0
	342	-1221(13-II-4)	0	4(1)	0	0	0	0

7102	342	-1146(13-14)	0	4(1)	0	0	0	0
	355	-1146(13-14)	0	4(1)	0	0	0	0
7103	334	-926(13-II-4)	0	5(1)	0	0	0	0
	353	-926(13-II-4)	0	5(1)	0	0	0	0
7104	353	-1065(13-I-4)	0	4(1)	0	0	0	0
	339	-1065(13-I-4)	0	4(1)	0	0	0	0
7105	369	-1200(13-II-4)	0	4(1)	0	0	0	0
	337	-1200(13-II-4)	0	4(1)	0	0	0	0
7106	337	-1089(13-I-4)	0	5(1)	0	0	0	0
	365	-1089(13-I-4)	0	5(1)	0	0	0	0

VERIFICHE STATO LIMITE ULTIMO

Scenario di calcolo - Set_NT_SLV_A2_STR/GE0								
Verifica delle travi								

Trave di Fond.: 9009 | 1. 2. | Pilastro [1. 2.]
 Sez. R: B_y= 60.0 cm B_z= 100.0 cm L= 89.7 cm Ln= 89.7 cm Terreno: *Terrenol*

Criterio : CLS TravFondazione - Verifica a flessione : *Verificato*

X	M-	M+	AM-	AM+	AFs	cmq	AFi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	kg*m	cmq	kg*m	kg*m	kg*m			
ILN	2041	1221	8251	5494	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	4.12
9.0	3959	2370	7765	5483	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	3.61
CAMP	14563	10353	2253	2298	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	2.52
80.8	15727	11500	1089	1152	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	2.52
FLN	16816	12652	--	--	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	2.52

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
9.0	19.4	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
CAMP	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
80.8	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
FLN	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.

Verifica a taglio: cot(0) =2.500

Comb = (12+13)»V1-4

Sez	Td	VRdns	VRcds	VRsd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	22013	--	125983	91208	91208	0	42365	89.7	4.14
Des						42365			

Trave di Fond.: 9009 | 2. 3. | Pilastro [2. 3.]

Sez. R: B_y= 60.0 cm B_z= 100.0 cm L= 89.6 cm Ln= 89.6 cm Terreno: *Terrenol*

Criterio : CLS TravFondazione - Verifica a flessione : *Verificato*

X	M-	M+	AM-	AM+	AFs	cmq	AFi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	kg*m	cmq	kg*m	kg*m	kg*m			
ILN	18811	13835	--	--	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	2.25
9.0	18397	13613	413	222	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	2.25
CAMP	16763	12996	2047	839	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	2.25
80.7	12901	12179	3739	782	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	2.55
FLN	11982	12055	3982	721	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	2.65

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.5	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
9.0	19.5	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
CAMP	19.5	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
80.7	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
FLN	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.

Verifica a taglio: cot(0) =2.500

Comb = (12+13)»V1-4

Sez	Td	VRdns	VRcds	VRsd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10616	--	125983	84882	84882	0	42365	89.6	8.00
Des						42365			

Travo di Fond.: 9009 | 3. 4. | Pilastro [3. 4.]

Sez. R: B_y= 60.0 cm B_z= 100.0 cm L= 89.0 cm Ln= 89.0 cm Terreno: *Terrenol*

Criterio : CLS TravFondazione - Verifica a flessione : *Verificato*

X	M-	M+	AM-	AM+	AFs	cmq	AFi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	kg*m	cmq	kg*m	kg*m	kg*m			
ILN	13967	13236	--	--	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	3.03
8.9	13249	12860	718	376	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	3.03
CAMP	10860	11823	3107	1413	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	3.03
80.1	6207	10445	4524	1332	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	3.60
FLN	5193	10229	4665	1238	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	3.69

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
8.9	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
CAMP	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
80.1	19.3	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
FLN	19.3	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.

Verifica a taglio: cot(0) =2.500

Comb = (12+13)»V1-4

Sez	Td	VRdns	VRcds	VRsd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	11850	--	125983	84882	84882	0	42365	89.0	7.16
Des						42365			

Travo di Fond.: 9009 | 4. 5. | Pilastro [4. 5.]

Sez. R: B_y= 60.0 cm B_z= 100.0 cm L= 89.3 cm Ln= 89.3 cm Terreno: *Terrenol*

Criterio : CLS TravFondazione - Verifica a flessione : *Verificato*

X	M-	M+	AM-	AM+	AFs	cmq	AFi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	kg*m	cmq	kg*m	kg*m	kg*m			
ILN	7061	11401	--	--	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	3.72
8.9	6300	10988	761	413	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	3.72
CAMP	3879	9877	3182	1523	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	3.72
80.3	-256	8795	3999	1032	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	4.31
FLN	-1124	8665	4068	897	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	4.43

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.3	95.9	0.201	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
8.9	19.3	95.9	0.201	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.4	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
80.3	19.3	95.9	0.201	19.3	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.
FLN	19.2	95.9	0.201	19.3	95.9	0.202	42365	42365	(12+13)»V1-4	(12+13)»V1-1	Parz.	Parz.

Verifica a taglio: cot(0) =2.500

Comb = (12+13)»V1-4

Sez	Td	VRdns	VRcds	VRsd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	11303	--	125983	84882	84882	0	42365	89.3	7.51
Des						42365			

Travo di Fond.: 9009 | 5. 6. | Pilastro [5. 6.]

Sez. R: B_y= 60.0 cm B_z= 100.0 cm L= 89.0 cm Ln= 89.0 cm Terreno: *Terrenol*

Criterio : CLS TravFondazione - Verifica a flessione : *Verificato*

X	M-	M+	AM-	AM+	AFs	cmq	AFi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	kg*m	cmq	kg*m	kg*m	kg*m			
ILN	578	9751	--	--	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-1	4.34
8.9	-68	7166	646	2633	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-2	4.32
CAMP	-2067	10698	2645	1046	12.06	12.06	12.06	42365	42365	(12+13)»V1-4	(12+13)»V1-2	3.61

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
80.1	--	11192	--	552	12.06	12.06	42365	42365	1	(12+13)-III-2	3.61
FLN	--	11744	--	--	12.06	12.06	42365	42365	1	(12+13)-III-2	3.61

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*	kg*			
ILN	19.2	95.9	0.200	19.3	95.9	0.202	42365	42365	(12+13)-II-4	(12+13)-II-1	Parz.
8.9	19.2	95.9	0.200	19.3	95.9	0.202	42365	42365	(12+13)-II-4	(12+13)-III-2	Parz.
CAMP	19.2	95.9	0.200	19.4	95.9	0.202	42365	42365	(12+13)-II-4	(12+13)-I-2	Parz.
80.1	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--

Verifica a taglio: cot(0) = 2,500

Comb = (12+13)-VI-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
cm	cm	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	10727	--	125983	84882	84882	0	42365	89.0	10.05	7.91
Des										

Trave di Fond.: 9009 [6, 7] Pilastrate [6, 7]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.0 cm Ln= 89.0 cm Terreno: *Terrenol*

Criterio : CLS Travifondazione - Verifica a flessione - *Verificato*

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*	kg*	kg*	kg*	cmq	cmq	kg*	kg*			
ILN	--	11255	--	1611	12.06	12.06	42365	42365	1	(12+13)-III-2	3.29
8.9	--	11482	--	1819	12.06	12.06	42365	42365	1	(12+13)-III-2	3.19
CAMP	--	14321	--	1043	12.06	12.06	42365	42365	1	(12+13)-I-2	2.76
80.1	--	14833	--	531	12.06	12.06	42365	42365	1	(12+13)-I-2	2.76
FLN	--	15364	--	--	12.06	12.06	42365	42365	1	(12+13)-I-2	2.76

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*	kg*			
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--
8.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--
CAMP	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-2	--
80.1	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-2	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-2	--

Verifica a taglio: cot(0) = 2,500

Comb = (12+13)-VI-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
cm	cm	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	9839	--	125983	84882	84882	0	42365	89.0	10.05	8.63
Des										

Trave di Fond.: 9009 [7, 8] Pilastrate [7, 8]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 90.4 cm Ln= 89.2 cm Terreno: *Terrenol*

Criterio : CLS Travifondazione - Verifica a flessione - *Verificato*

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*	kg*	kg*	kg*	cmq	cmq	kg*	kg*			
ILN	--	14677	--	--	12.06	12.06	42365	42365	1	(12+13)-III-2	2.89
8.9	--	14269	--	408	12.06	12.06	42365	42365	1	(12+13)-III-2	2.89
CAMP	--	14214	--	801	12.06	12.06	42365	42365	1	(12+13)-I-1	2.82
80.2	--	14594	--	422	12.06	12.06	42365	42365	1	(12+13)-I-1	2.82
FLN	--	15015	--	--	12.06	12.06	42365	42365	1	(12+13)-I-1	2.82

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*	kg*			
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--
8.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--
CAMP	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-1	--
80.2	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-1	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-1	--

Verifica a taglio: cot(0) = 2,500

Comb = (12+13)-VI-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
cm	cm	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	12956	--	125983	90352	90352	0	42365	89.2	10.70	6.97
Des										

Trave di Fond.: 9009 [8, 9] Pilastrate [8, 9]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 88.8 cm Ln= 88.8 cm Terreno: *Terrenol*

Criterio : CLS Travifondazione - Verifica a flessione - *Verificato*

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*	kg*	kg*	kg*	cmq	cmq	kg*	kg*			
ILN	1182	16521	--	--	12.06	12.06	42365	42365	(12+13)-II-4	(12+13)-II-1	2.60
8.9	738	15821	445	500	12.06	12.06	42365	42365	(12+13)-II-4	(12+13)-II-1	2.60
CAMP	-675	14498	1858	1823	12.06	12.06	42365	42365	(12+13)-II-4	(12+13)-I-1	2.85
79.9	--	14541	--	325	12.06	12.06	42365	42365	1	(12+13)-I-1	2.85
FLN	--	14553	--	196	12.06	12.06	42365	42365	1	(12+13)-I-1	2.87

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*	kg*			
ILN	19.2	95.9	0.200	19.4	95.9	0.203	42365	42365	(12+13)-II-4	(12+13)-II-1	Parz.
8.9	19.2	95.9	0.200	19.4	95.9	0.203	42365	42365	(12+13)-II-4	(12+13)-II-1	Parz.
CAMP	19.2	95.9	0.200	19.4	95.9	0.203	42365	42365	(12+13)-II-4	(12+13)-II-1	Parz.
79.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-1	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-1	--

Verifica a taglio: cot(0) = 2,500

Comb = (12+13)-VI-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
cm	cm	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	7341	--	125983	84882	84882	0	42365	88.8	10.05	11.6
Des										

Trave di Fond.: 9009 [9, 10] Pilastrate [9, 10]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.8 cm Ln= 89.8 cm Terreno: *Terrenol*

Criterio : CLS Travifondazione - Verifica a flessione - *Verificato*

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*	kg*	kg*	kg*	cmq	cmq	kg*	kg*			
ILN	--	15084	--	--	12.06	12.06	42365	42365	1	(12+13)-I-1	2.81
9.0	--	14854	--	229	12.06	12.06	42365	42365	1	(12+13)-I-1	2.81
CAMP	--	14335	--	749	12.06	12.06	42365	42365	1	(12+13)-I-1	2.81
80.8	--	13230	--	1083	12.06	12.06	42365	42365	1	(12+13)-III-1	2.96
FLN	--	14305	--	--	12.06	12.06	42365	42365	1	(12+13)-III-2	2.96

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*	kg*			
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-1	--
9.0	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-1	--
CAMP	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-1	--
80.8	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-1	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--

Verifica a taglio: cot(0) = 2,500

Comb = (12+13)-VI-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
cm	cm	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	6691	--	125983	91092	91092	0	42365	89.8	10.79	13.6
Des										

Trave di Fond.: 9009 [10, 11] Pilastrate [10, 11]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.7 cm Ln= 89.7 cm Terreno: *Terrenol*

Criterio : CLS Travifondazione - Verifica a flessione - *Verificato*

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*	kg*	kg*	kg*	cmq	cmq	kg*	kg*			
ILN	--	14466	--	--	12.06	12.06	42365	42365	1	(12+13)-III-2	2.93
9.0	--	14282	--	185	12.06	12.06	42365	42365	1	(12+13)-III-2	2.93
CAMP	--	14246	--	359	12.06	12.06	42365	42365	1	(12+13)-I-2	2.90

Verifica a taglio: cot(θ) = 2,500

Comb = (12+13)-VI-4

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg	kg	cm	cmq/m	
Sin	6534	--	125983	84882	84882	0	42365	89.0	10.05	13.0
Des							42365			

Trave di Fond. : 9009 | 13, 14 | Pilastrate | 13, 14 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.6 cm Ln= 89.6 cm Terreno: Terreno I

Criterio : CLS_TraviFondazione - Verifica a flessione .Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	15896	--	--	12.06	12.06	42365	42365	1	(12+13)-VI-2	2.67
9.0	--	14806	--	1090	12.06	12.06	42365	42365	1	(12+13)-VI-2	2.67
CAMP	--	12252	--	3644	12.06	12.06	42365	42365	1	(12+13)-VI-2	2.67
80.6	--	14310	--	1023	12.06	12.06	42365	42365	1	(12+13)-II-1	2.76
FLN	--	15333	--	--	12.06	12.06	42365	42365	1	(12+13)-II-1	2.76

Verifica a taglio: cot(θ) = 2,500

Comb = (12+13)-VI-4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)-VI-2	--
9.0	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)-VI-2	--
CAMP	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)-VI-2	--
80.6	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-II-1	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-II-1	--

Verifica a taglio: cot(θ) = 2,500

Comb = (12+13)-VI-4

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg	kg	cm	cmq/m	
Sin	14337	--	125983	84882	84882	0	42365	89.6	10.05	5.92
Des							42365			

Trave di Fond. : 9009 | 14, 15 | Pilastrate | 14, 15 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.9 cm Ln= 89.9 cm Terreno: Terreno I

Criterio : CLS_TraviFondazione - Verifica a flessione .Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	16775	--	--	12.06	12.06	42365	42365	1	(12+13)-II-1	2.53
9.0	--	16255	--	519	12.06	12.06	42365	42365	1	(12+13)-II-1	2.53
CAMP	--	14898	--	1877	12.06	12.06	42365	42365	1	(12+13)-II-1	2.53
80.9	--	13415	--	1407	12.06	12.06	42365	42365	1	(12+13)-II-1	2.86
FLN	--	11894	--	2680	12.06	12.06	42365	42365	1	(12+13)-I-1	2.91

Verifica a taglio: cot(θ) = 2,500

Comb = (12+13)-VI-1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)-II-1	--
9.0	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)-II-1	--
CAMP	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)-II-1	--
80.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-II-1	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-1	--

Verifica a taglio: cot(θ) = 2,500

Comb = (12+13)-VI-1

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg	kg	cm	cmq/m	
Sin	6724	--	125983	90990	90990	0	42365	89.9	10.78	13.5
Des							42365			

Trave di Fond. : 9009 | 15, 16 | Pilastrate | 15, 16 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.2 cm Ln= 89.2 cm Terreno: Terreno I

Criterio : CLS_TraviFondazione - Verifica a flessione .Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	14612	--	--	12.06	12.06	42365	42365	1	(12+13)-I-1	2.90

X	M-	M+	AM-	AM+	Afs	Afi	Mr+	Mr-	C-	C+	CS
80.8	--	14410	--	195	12.06	12.06	42365	42365	1	(12+13)-I-2	2.90
FLN	--	14605	--	--	12.06	12.06	42365	42365	1	(12+13)-I-2	2.90

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--
9.0	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--
CAMP	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-2	--
80.8	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-2	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-I-2	--

Verifica a taglio: cot(θ) = 2,500

Comb = (12+13)-VI-4

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg	kg	cm	cmq/m	
Sin	6378	--	125983	91208	91208	0	42365	89.7	10.80	14.3
Des							42365			

Trave di Fond. : 9009 | 11, 12 | Pilastrate | 11, 12 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.2 cm Ln= 89.2 cm Terreno: Terreno I

Criterio : CLS_TraviFondazione - Verifica a flessione .Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	14361	--	--	12.06	12.06	42365	42365	1	(12+13)-III-2	2.95
8.9	--	14271	--	90	12.06	12.06	42365	42365	1	(12+13)-II-2	2.95
CAMP	--	14192	--	904	12.06	12.06	42365	42365	1	(12+13)-II-2	2.81
80.3	--	14628	--	467	12.06	12.06	42365	42365	1	(12+13)-II-2	2.81
FLN	--	15096	--	--	12.06	12.06	42365	42365	1	(12+13)-II-2	2.81

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--
8.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-III-2	--
CAMP	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-II-2	--
80.3	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-II-2	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-II-2	--

Verifica a taglio: cot(θ) = 2,500

Comb = (12+13)-VI-4

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
	kg	kg	kg	kg	kg	kg	kg	cm	cmq/m	
Sin	6343	--	125983	84882	84882	0	42365	89.2	10.05	13.4
Des							42365			

Trave di Fond. : 9009 | 12, 13 | Pilastrate | 12, 13 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.0 cm Ln= 89.0 cm Terreno: Terreno I

Criterio : CLS_TraviFondazione - Verifica a flessione .Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	13723	--	1382	12.06	12.06	42365	42365	1	(12+13)-II-2	2.80
8.9	--	13947	--	1533	12.06	12.06	42365	42365	1	(12+13)-II-2	2.74
CAMP	-432	16425	631	1040	12.06	12.06	42365	42365	(12+13)-VI-3	(12+13)-VI-2	2.43
80.1	-106	16930	306	535	12.06	12.06	42365	42365	(12+13)-VI-3	(12+13)-VI-2	2.43
FLN	200	17465	--	--	12.06	12.06	42365	42365	(12+13)-VI-3	(12+13)-VI-2	2.43

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-II-2	--
8.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)-II-2	--
CAMP	19.2	95.9	0.200	19.4	95.9	0.203	42365	42365	(12+13)-VI-3	(12+13)-VI-2	Parz.
80.1	19.2	95.9	0.200	19.4	95.9	0.203	42365	42365	(12+13)-VI-3	(12+13)-VI-2	Parz.
FLN	19.2	95.9	0.200	19.4	95.9	0.203	42365	42365	(12+13)-VI-3	(12+13)-VI-2	Parz.

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
8.9	--	14307	--	306	12.06	12.06	42365	42365	1	(12+13)÷I-1	2.90
CAMP	--	11577	--	3035	12.06	12.06	42365	42365	1	(12+13)÷I-1	2.90
80.3	--	13458	--	122	12.06	12.06	42365	42365	1	(12+13)÷V-2	3.12
FLN	--	13580	--	--	12.06	12.06	42365	42365	1	(12+13)÷V-2	3.12

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷I-1	--
8.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷I-1	--
CAMP	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷I-1	--
80.3	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--

Verifica a taglio: cot(θ) = 2.500

Comb = (12+13)÷VI-1

Sez	Td	VRdms	VRcd	VRsd	VRd	TPd	Mr	Dx	Stafle	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6727	--	125983	84882	84882	0	42365	89.2	10.05	12.6
Des							42365			

Trave di Fond.: 9009 | 16., 17 | Pilastrate [16., 17]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 88.8 cm Ln= 88.8 cm Terreno: **Terreno I**

Criterio: CLS_TraviFondazione - Verifica a flessione. **Verificato**

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	13745	--	--	12.06	12.06	42365	42365	1	(12+13)÷V-2	3.08
8.9	--	13509	--	196	12.06	12.06	42365	42365	1	(12+13)÷V-2	3.08
CAMP	--	13377	--	759	12.06	12.06	42365	42365	1	(12+13)÷V-2	3.00
79.9	--	13732	--	404	12.06	12.06	42365	42365	1	(12+13)÷V-2	3.00
FLN	--	14136	--	--	12.06	12.06	42365	42365	1	(12+13)÷V-2	3.00

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--
8.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--
CAMP	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--
79.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--

Verifica a taglio: cot(θ) = 2.500

Comb = (12+13)÷VI-1

Sez	Td	VRdms	VRcd	VRsd	VRd	TPd	Mr	Dx	Stafle	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6971	--	125983	84882	84882	0	42365	88.8	10.05	12.2
Des							42365			

Trave di Fond.: 9009 | 17., 18 | Pilastrate [17., 18]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 90.0 cm Ln= 88.8 cm Terreno: **Terreno I**

Criterio: CLS_TraviFondazione - Verifica a flessione. **Verificato**

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	13252	--	985	12.06	12.06	42365	42365	1	(12+13)÷V-2	2.98
8.9	--	13357	--	1214	12.06	12.06	42365	42365	1	(12+13)÷V-2	2.91
CAMP	-378	15414	739	939	12.06	12.06	42365	42365	(12+13)÷VI-3	(12+13)÷V-2	2.59
79.9	-3	15866	364	487	12.06	12.06	42365	42365	(12+13)÷VI-3	(12+13)÷V-2	2.59
FLN	361	16353	--	--	12.06	12.06	42365	42365	(12+13)÷VI-3	(12+13)÷V-2	2.59

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--
8.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--
CAMP	19.2	95.9	0.200	19.4	95.9	0.203	42365	42365	(12+13)÷VI-3	(12+13)÷V-2	Parz.
79.9	19.2	95.9	0.200	19.4	95.9	0.203	42365	42365	(12+13)÷VI-3	(12+13)÷V-2	Parz.
FLN	19.2	95.9	0.200	19.4	95.9	0.203	42365	42365	(12+13)÷VI-3	(12+13)÷V-2	Parz.

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Verifica a taglio: cot(θ) = 2.500

Comb = (12+13)÷VI-1

Sez	Td	VRdms	VRcd	VRsd	VRd	TPd	Mr	Dx	Stafle	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7189	--	125983	90843	90843	0	42365	88.8	10.76	12.6
Des							42365			

Trave di Fond.: 9009 | 18., 19 | Pilastrate [18., 19]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 88.7 cm Ln= 88.7 cm Terreno: **Terreno I**

Criterio: CLS_TraviFondazione - Verifica a flessione. **Verificato**

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	15191	--	--	12.06	12.06	42365	42365	1	(12+13)÷V-2	2.79
8.9	--	14392	--	800	12.06	12.06	42365	42365	1	(12+13)÷V-2	2.79
CAMP	--	14525	--	1850	12.06	12.06	42365	42365	1	(12+13)÷V-1	2.59
79.9	--	15398	--	977	12.06	12.06	42365	42365	1	(12+13)÷V-1	2.59
FLN	--	16375	--	--	12.06	12.06	42365	42365	1	(12+13)÷V-1	2.59

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--
8.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-2	--
CAMP	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)÷V-1	--
79.9	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)÷V-1	--
FLN	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)÷V-1	--

Verifica a taglio: cot(θ) = 2.500

Comb = (12+13)÷VI-1

Sez	Td	VRdms	VRcd	VRsd	VRd	TPd	Mr	Dx	Stafle	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	14127	--	125983	84882	84882	0	42365	88.7	10.05	6.01
Des							42365			

Trave di Fond.: 9009 | 19., 20 | Pilastrate [19., 20]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.9 cm Ln= 89.9 cm Terreno: **Terreno I**

Criterio: CLS_TraviFondazione - Verifica a flessione. **Verificato**

X	M-	M+	ΔM-	ΔM+	AfS	AfI	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	17902	--	--	12.06	12.06	42365	42365	1	(12+13)÷V-1	2.37
9.0	--	17230	--	672	12.06	12.06	42365	42365	1	(12+13)÷V-1	2.37
CAMP	--	15400	--	2502	12.06	12.06	42365	42365	1	(12+13)÷V-1	2.37
80.9	--	5168	--	10125	12.06	12.06	42365	42365	1	(12+13)÷V-1	2.77
FLN	--	5367	--	9390	12.06	12.06	42365	42365	1	(12+13)÷V-1	2.87

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)÷V-1	--
9.0	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)÷V-1	--
CAMP	--	--	--	19.4	95.9	0.203	42365	42365	1	(12+13)÷V-1	--
80.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-1	--
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)÷V-1	--

Verifica a taglio: cot(θ) = 2.500

Comb = (12+13)÷VI-1

Sez	Td	VRdms	VRcd	VRsd	VRd	TPd	Mr	Dx	Stafle	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8472	--	125983	91019	91019	0	42365	89.9	10.78	10.7
Des							42365			

Trave di Fond.: 9009 | 20., 21 | Pilastrate [20., 21]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.1 cm Ln= 89.1 cm Terreno: **Terreno I**

Criterio: CLS_TraviFondazione - Verifica a flessione. **Verificato**

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X	M-	M+	AM-	AM+	Afi	Afi	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	--	--	--	12.06	12.06	42365	42365	1	(12+13)∨V-1	3.06
8.9	--	--	--	530	12.06	12.06	42365	42365	1	(12+13)∨V-1	3.06
CAMP	--	--	--	3866	12.06	12.06	42365	42365	1	(12+13)∨V-1	3.06
80.2	--	--	--	10686	12.06	12.06	42365	42365	1	(12+13)∨V-2	3.56
FLN	--	--	--	10603	12.06	12.06	42365	42365	1	(12+13)∨V-2	3.67

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr+	Mr-	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)∨V-1	--	Parz.
8.9	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)∨V-1	--	Parz.
CAMP	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)∨V-1	--	Parz.
80.2	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)∨V-2	--	Parz.
FLN	--	--	--	19.4	95.9	0.202	42365	42365	1	(12+13)∨V-2	--	Parz.

Verifica a taglio:cof(0)=2,500

Comb=(12+13)∨V-1

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9043	--	125983	84882	84882	0	42365	89.1	10.05	9.39
Des							42365			

Trave di Fond. : 9009 | 21. 22.1 | Pilastrate [21. 22.1]

Sez. R: By= 60.0 cm Bz=100.0 cm L=89.4 cm Ln=89.4 cm Terreno: Terrenol

Criterio : CLS TravIFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afi	Afi	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	--	--	--	12.06	12.06	42365	42365	1	(12+13)∨V-2	3.89
8.9	--	--	--	414	12.06	12.06	42365	42365	1	(12+13)∨V-2	3.89
CAMP	-1305	8646	2820	2315	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-2	3.87
80.4	-808	8871	2322	2090	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.87
FLN	1514	10961	--	--	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.87

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr+	Mr-	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	--	--	--	19.3	95.9	0.202	42365	42365	1	(12+13)∨V-2	--	Parz.
8.9	--	--	--	19.3	95.9	0.202	42365	42365	1	(12+13)∨V-2	--	Parz.
CAMP	19.2	95.9	0.200	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
80.4	19.2	95.9	0.200	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
FLN	19.2	95.9	0.200	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.

Verifica a taglio:cof(0)=2,500

Comb=(12+13)∨V-1

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9589	--	125983	84882	84882	0	42365	89.4	10.05	8.85
Des							42365			

Trave di Fond. : 9009 | 22. 23.1 | Pilastrate [22. 23.1]

Sez. R: By= 60.0 cm Bz=100.0 cm L=89.8 cm Ln=89.8 cm Terreno: Terrenol

Criterio : CLS TravIFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afi	Afi	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	-1784	8310	5201	2233	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	4.02
9.0	-1068	8329	5209	2441	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.93
CAMP	5692	11376	1352	675	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.52
80.8	6376	11700	668	351	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.52
FLN	7044	12051	--	--	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.52

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr+	Mr-	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.2	95.9	0.201	19.3	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
9.0	19.3	95.9	0.201	19.3	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
CAMP	19.3	95.9	0.201	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr+	Mr-	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
80.8	19.3	95.9	0.201	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
FLN	19.3	95.9	0.201	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.

Verifica a taglio:cof(0)=2,500

Comb=(12+13)∨V-1

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10277	--	125983	91107	91107	0	42365	89.8	10.79	8.87
Des							42365			

Trave di Fond. : 9009 | 23. 24 | Pilastrate [23. 24]

Sez. R: By= 60.0 cm Bz=100.0 cm L=89.3 cm Ln=89.3 cm Terreno: Terrenol

Criterio : CLS TravIFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afi	Afi	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5196	10916	4283	1003	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.55
8.9	6120	11075	4178	1117	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.47
CAMP	11980	12855	1420	691	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.13
80.4	12707	13192	694	354	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.13
FLN	13401	13546	--	--	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	3.13

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr+	Mr-	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.3	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
8.9	19.3	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
CAMP	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
80.4	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
FLN	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.

Verifica a taglio:cof(0)=2,500

Comb=(12+13)∨V-1

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	11129	--	125983	84882	84882	0	42365	89.3	10.05	7.63
Des							42365			

Trave di Fond. : 9009 | 24. 25 | Pilastrate [24. 25]

Sez. R: By= 60.0 cm Bz=100.0 cm L=89.7 cm Ln=89.7 cm Terreno: Terrenol

Criterio : CLS TravIFondazione - Verifica a flessione :Verificato

X	M-	M+	AM-	AM+	Afi	Afi	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11425	12394	3923	629	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	2.76
9.0	12316	12494	3721	703	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	2.64
CAMP	17371	13616	980	426	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	2.31
80.7	17891	13825	461	217	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	2.31
FLN	18351	14042	--	--	12.06	12.06	42365	42365	(12+13)∨V-1	(12+13)∨V-4	2.31

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr+	Mr-	C-	C+	Stato-	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m				
ILN	19.4	95.9	0.202	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
9.0	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
CAMP	19.5	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
80.7	19.5	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.
FLN	19.5	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)∨V-1	(12+13)∨V-4	Parz.	Parz.

Verifica a taglio:cof(0)=2,500

Comb=(12+13)∨V-1

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10493	--	125983	84882	84882	0	42365	89.7	10.05	8.09
Des							42365			

Trave di Fond. : 9009 | 25. 26 | Pilastrate [25. 26]

Sez. R: By= 60.0 cm Bz=100.0 cm L=89.5 cm Ln=100.9 cm Terreno: Terrenol

Criterio : *CLS Travifondazione - Verifica a flessione -Verificato*

X	M-	M+	AM-	AM+	Af±	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	kg*m	kg*m			
ILN	16329	12882	--	--	12.06	12.06	42365	(12+13)-VI-1	(12+13)-VI-4	2.59
10.1	15100	11553	1228	1330	12.06	12.06	42365	(12+13)-VI-1	(12+13)-VI-4	2.59
CAMP	10882	7603	5446	5280	12.06	12.06	42365	(12+13)-VI-1	(12+13)-VI-4	2.59
90.8	1711	1038	8011	5617	12.06	12.06	42365	(12+13)-VI-1	(12+13)-VI-4	4.36
FLN	-508	-296	8547	5642	12.06	12.06	42365	(12+13)-VI-1	(12+13)-VI-4	5.27

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-VI-1	(12+13)-VI-4	Parz.	Parz.
10.1	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-VI-1	(12+13)-VI-4	Parz.	Parz.
CAMP	19.4	95.9	0.203	19.4	95.9	0.202	42365	42365	(12+13)-VI-1	(12+13)-VI-4	Parz.	Parz.
90.8	19.3	95.9	0.202	19.3	95.9	0.201	42365	42365	(12+13)-VI-1	(12+13)-VI-4	Parz.	Parz.
FLN	19.3	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-VI-1	(12+13)-VI-4	Parz.	Parz.

Verifica a taglio: cot(0) =2,500

Comb =(12+13)-VI-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	cm	kg*m	cm	cmq/m	
Sin	22615	--	125983	84882	0	42365	100.9	10.05		3.75
Des							42365			

Trave di Fond. : 9010 | 1, 2 | 3 | Pilastrate [27, 51]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.6 cm L=149.6 cm Terreno: **Terreno1**

Criterio : *CLS Travifondazione - Verifica a flessione -Verificato*

X	M-	M+	AM-	AM+	Af±	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	kg*m	kg*m			
ILN	60	457	537	--	12.06	12.06	42365	42365	3 (12+13)-VIII-1	71.0
15.0	297	278	387	180	12.06	12.06	42365	42365	3 (12+13)-VIII-1	62.0
CAMP	808	567	352	707	12.06	12.06	42365	42365	(12+13)-I-3	33.2
134.7	976	896	184	379	12.06	12.06	42365	42365	(12+13)-I-3	33.2
FLN	1160	1274	--	--	12.06	12.06	42365	42365	(12+13)-I-3	33.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	3 (12+13)-VIII-1	(12+13)-VIII-1	Parz.	Parz.
15.0	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	3 (12+13)-VIII-1	(12+13)-VIII-1	Parz.	Parz.
CAMP	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
134.7	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
FLN	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.

Verifica a taglio: cot(0) =2,500

Comb =(12+13)-III-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	cm	kg*m	cm	cmq/m	
Sin	2774	--	125983	88240	0	42365	149.6	10.45		31.8
Des							42365			

Trave di Fond. : 9010 | 2, 3 | Pilastrate [51, 50]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.8 cm L=149.8 cm Terreno: **Terreno1**

Criterio : *CLS Travifondazione - Verifica a flessione -Verificato*

X	M-	M+	AM-	AM+	Af±	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	kg*m	kg*m			
ILN	1025	1074	296	384	12.06	12.06	42365	42365	(12+13)-I-3	29.0
15.0	1120	1170	319	495	12.06	12.06	42365	42365	(12+13)-I-3	25.4
CAMP	1980	2867	282	763	12.06	12.06	42365	42365	(12+13)-I-3	11.7
134.8	2120	3236	142	395	12.06	12.06	42365	42365	(12+13)-I-3	11.7
FLN	2261	3630	--	--	12.06	12.06	42365	42365	(12+13)-I-3	11.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
15.0	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.

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X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
CAMP	19.2	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
134.8	19.2	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
FLN	19.2	95.9	0.201	19.2	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.

Verifica a taglio: cot(0) =2,500

Comb =(12+13)-I-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	cm	kg*m	cm	cmq/m	
Sin	2768	--	125983	88245	0	42365	149.8	10.45		31.9
Des							42365			

Trave di Fond. : 9010 | 3, 4 | Pilastrate [50, 49]

Sez. R: By= 60.0 cm Bz=100.0 cm L=149.3 cm L=149.3 cm Terreno: **Terreno1**

Criterio : *CLS Travifondazione - Verifica a flessione -Verificato*

X	M-	M+	AM-	AM+	Af±	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	kg*m	kg*m			
ILN	2225	3514	235	316	12.06	12.06	42365	42365	(12+13)-I-3	11.1
14.9	2307	3601	234	384	12.06	12.06	42365	42365	(12+13)-I-3	10.6
CAMP	2866	4861	151	562	12.06	12.06	42365	42365	(12+13)-I-3	7.81
134.4	2943	5131	75	292	12.06	12.06	42365	42365	(12+13)-I-3	7.81
FLN	3017	5423	--	--	12.06	12.06	42365	42365	(12+13)-I-3	7.81

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
14.9	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
CAMP	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
134.4	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
FLN	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.

Verifica a taglio: cot(0) =2,500

Comb =(12+13)-I-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	cm	kg*m	cm	cmq/m	
Sin	2063	--	125983	84882	0	42365	149.3	10.05		41.1
Des							42365			

Trave di Fond. : 9010 | 4, 5 | Pilastrate [49, 48]

Sez. R: By= 60.0 cm Bz=100.0 cm L=148.5 cm L=148.5 cm Terreno: **Terreno1**

Criterio : *CLS Travifondazione - Verifica a flessione -Verificato*

X	M-	M+	AM-	AM+	Af±	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	kg*m	kg*m			
ILN	3031	5375	100	46	12.06	12.06	42365	42365	(12+13)-I-3	7.81
14.8	3068	5371	95	109	12.06	12.06	42365	42365	(12+13)-I-3	7.73
CAMP	3282	5956	50	373	12.06	12.06	42365	42365	(12+13)-I-3	6.69
133.6	3308	6132	24	198	12.06	12.06	42365	42365	(12+13)-I-3	6.69
FLN	3332	6329	--	--	12.06	12.06	42365	42365	(12+13)-I-3	6.69

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
14.8	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
CAMP	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
133.6	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
FLN	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.

Verifica a taglio: cot(0) =2,500

Comb =(12+13)-III-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	cm	kg*m	cm	cmq/m	
Sin	1476	--	125983	84882	0	42365	148.5	10.05		57.5
Des							42365			

Trave di Fond. : 9010 | 5, 6 | Pilastrate [48, 47]

Sez. R: By= 60.0 cm Bz=100.0 cm L=150.1 cm L=150.1 cm Terreno: **Terreno1**

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Criterio : *CLS Travifondazione - Verifica a flessione :Verificato*

X	M-	M+	x-/d-	x+/d+	AM-	AM+	Afi	Mr-	Mr+	C-	C+	Stato+	CS
cm	kg*m	kg*m	cm	cm	kg*m	kg*m	cmq	kg*m	kg*m				
ILN	3399	6353	--	--	12.06	12.06	12.06	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	6.67
CAMP	3392	6261	7	92	12.06	12.06	12.06	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	6.67
CAMP	3384	6314	15	251	12.06	12.06	12.06	42365	42365	(12+13)-I-3	(12+13)-II-2	Parz.	6.45
I35.0	3310	6426	33	138	12.06	12.06	12.06	42365	42365	(12+13)-I-3	(12+13)-II-2	Parz.	6.45
FLN	3301	6564	30	--	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	6.45

X	x-	d-	x-/d-	x+/d+	AM-	AM+	Afi	Mr-	Mr+	C-	C+	Stato+	CS
cm	cm	cm	cm	cm	kg*m	kg*m	cmq	kg*m	kg*m				
ILN	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
ILN	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-I-3	(12+13)-I-2	Parz.	Parz.
CAMP	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-I-3	(12+13)-II-2	Parz.	Parz.
I35.0	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
FLN	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
cm	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1333	--	125983	87954	87954	0	42365	150.1	10.42	66.0
Des							42365			

Trave di Fond. : 9010 | 6, 7 | Pilastrate [47, 46]

Sez. R: *By= 60.0 cm Bz=100.0 cm L=148.1 cm Ln=148.1 cm Terreno: Terreno1*

Criterio : *CLS Travifondazione - Verifica a flessione :Verificato*

X	M-	M+	x-/d-	x+/d+	AM-	AM+	Afi	Mr-	Mr+	C-	C+	Stato+	CS
cm	kg*m	kg*m	cm	cm	kg*m	kg*m	cmq	kg*m	kg*m				
ILN	3400	6633	--	--	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.39	6.39
I4.8	3379	6494	31	140	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.39	6.39
CAMP	3339	6379	62	254	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.39	6.39
I33.2	3121	6328	90	99	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.59	6.59
FLN	3089	6427	92	--	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.59	6.59

X	x-	d-	x-/d-	x+/d+	AM-	AM+	Afi	Mr-	Mr+	C-	C+	Stato+	CS
cm	cm	cm	cm	cm	kg*m	kg*m	cmq	kg*m	kg*m				
ILN	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
I4.8	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
CAMP	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
I33.2	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
FLN	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
cm	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1235	--	125983	84882	84882	0	42365	148.1	10.05	68.7
Des							42365			

Trave di Fond. : 9010 | 7, 8 | Pilastrate [46, 45]

Sez. R: *By= 60.0 cm Bz=100.0 cm L=152.6 cm Ln=152.6 cm Terreno: Terreno1*

Criterio : *CLS Travifondazione - Verifica a flessione :Verificato*

X	M-	M+	x-/d-	x+/d+	AM-	AM+	Afi	Mr-	Mr+	C-	C+	Stato+	CS
cm	kg*m	kg*m	cm	cm	kg*m	kg*m	cmq	kg*m	kg*m				
ILN	3236	6560	--	--	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.46	6.46
I5.3	3185	6370	51	190	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.46	6.46
CAMP	3137	6212	99	348	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.46	6.46
I37.3	2995	6117	19	123	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.79	6.79
FLN	2994	6241	9	--	12.06	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.79	6.79

X	x-	d-	x-/d-	x+/d+	AM-	AM+	Mr-	Mr+	C-	C+	Stato+	CS
cm	cm	cm	cm	cm	kg*m	kg*m	kg*m	kg*m				
ILN	19.2	95.9	0.201	19.3	95.9	0.201	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.

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X	x-	d-	x-/d-	x+/d+	AM-	AM+	Afi	Mr-	Mr+	C-	C+	Stato+	CS
cm	cm	cm	cm	cm	kg*m	kg*m	cmq	kg*m	kg*m				
CAMP	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
I37.3	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
FLN	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)-IV-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
cm	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1720	--	125983	86234	86234	0	42365	152.6	10.21	50.1
Des							42365			

Trave di Fond. : 9010 | 8, 9 | Pilastrate [45, 44]

Sez. R: *By= 60.0 cm Bz=100.0 cm L=147.5 cm Ln=147.5 cm Terreno: Terreno1*

Criterio : *CLS Travifondazione - Verifica a flessione :Verificato*

X	M-	M+	ΔM-	ΔM+	Afi	Afi	Mr-	Mr+	C-	C+	Stato+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m				
ILN	3013	6252	--	--	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.78	6.78
I4.8	2982	6084	31	168	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.78	6.78
CAMP	2951	5943	62	309	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	6.78	6.78
I32.8	2732	5729	91	80	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	7.29	7.29
FLN	2700	5809	92	--	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	7.29	7.29

X	x-	d-	x-/d-	x+/d+	AM-	AM+	Afi	Mr-	Mr+	C-	C+	Stato+	CS
cm	cm	cm	cm	cm	kg*m	kg*m	cmq	kg*m	kg*m				
ILN	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
I4.8	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
CAMP	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
I32.8	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
FLN	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
cm	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1350	--	125983	84882	84882	0	42365	147.5	10.05	62.9
Des							42365			

Trave di Fond. : 9010 | 9, 10 | Pilastrate [44, 43]

Sez. R: *By= 60.0 cm Bz=100.0 cm L=149.8 cm Ln=149.8 cm Terreno: Terreno1*

Criterio : *CLS Travifondazione - Verifica a flessione :Verificato*

X	M-	M+	ΔM-	ΔM+	Afi	Afi	Mr-	Mr+	C-	C+	Stato+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m				
ILN	2750	5846	--	--	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	7.25	7.25
I5.0	2720	5684	29	162	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	7.25	7.25
CAMP	2691	5549	59	297	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	7.25	7.25
I34.8	2471	5398	93	89	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	7.72	7.72
FLN	2436	5487	96	--	12.06	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	7.72	7.72

X	x-	d-	x-/d-	x+/d+	AM-	AM+	Afi	Mr-	Mr+	C-	C+	Stato+	CS
cm	cm	cm	cm	cm	kg*m	kg*m	cmq	kg*m	kg*m				
ILN	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
I5.0	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
CAMP	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
I34.8	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.
FLN	19.2	95.9	0.201	19.3	95.9	0.201	12.06	42365	42365	(12+13)-II-3	(12+13)-II-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafle	CS
cm	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1319	--	125983	88108	88108	0	42365	149.8	10.44	66.8
Des							42365			

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Trave di Fond. : 9010 [10, 11] Pilastrate [43, 42]

Sez. R:	$B_y=60.0\text{ cm}$	$B_z=100.0\text{ cm}$	$L=149.6\text{ cm}$	$L_n=149.6\text{ cm}$	Terreno: Terreno I
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Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	M _r cm	M _w kg·m	AM _w kg·m	AM _w %	AF ₁ cmq	MF _r kg·m	C ⁻	C ⁺	CS
ILN	2494	5539	--	--	12.06	42365	(12+13)·III-3	(12+13)·III-2	7.65
15.0	2475	5597	19	142	12.06	42365	(12+13)·III-3	(12+13)·III-2	7.65
CAMP	2455	5282	40	258	12.06	42365	(12+13)·III-3	(12+13)·III-2	7.65
134.7	2575	5226	82	97	12.06	42365	(12+13)·III-3	(12+13)·III-2	7.96
FLN	2243	5323	88	--	12.06	42365	(12+13)·III-3	(12+13)·III-2	7.96

Verifica a taglio: $\cot(\theta) = 2.500$

Comb=3

Sez	Td	VRdms	VRd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg ^m	cm	cmq/m	
Sin	1243	--	125983	88205	88205	0	42365	149.7	10.45	71.0
Des							42365			

Trave di Fond.: 9010 [13, 14] | Pilastrate [40, 39]

Sez. R:	$B_y = 60.0 \text{ cm}$	$B_z = 100.0 \text{ cm}$	$L = 149.1 \text{ cm}$	$L_n = 149.1 \text{ cm}$	Terreno: Terrenol
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Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	M _r kg m ⁻³	M ₊ kg m ⁻³	AM _r kg m ⁻³	AF _r cmq	Mr ⁺ kg m ⁻³	C ⁻	C ⁺	CS
ILN	2118	5183	--	12.06	42365	(12+13)-VII-3	(12+13)-VII-2	8.17
ILN	2099	5040	19	143	42365	(12+13)-VII-3	(12+13)-VII-2	8.17
CAMP	2112	4939	49	262	42365	(12+13)-VII-3	(12+13)-VII-2	8.17
ILN	2135	5055	26	146	42365	(12+13)-VII-3	(12+13)-VII-2	8.14
FLN	2161	5202	--	12.06	42365	(12+13)-VII-3	(12+13)-VII-2	8.14

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafte	CS
	kg	kg	kg	kg	kg	kg	kg·m	cm	cmq/m	
Sin	1249	--	125983	88240	88240	0	42365	149.6	10.45	70.7
Des							42365			

Trave di Fond. : 9010 [11, 12 | Pilastrate [42, 41]

Sez. R:	$B_y=60.0\text{ cm}$	$B_z=100.0\text{ cm}$	$L=149.0\text{ cm}$	$L_n=149.0\text{ cm}$	Terreno: Terreno I
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Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	M _r	M _w	AM _n ^a	AM _w ^a	AF _n ^b	AF _w ^b	Mr ^c	C ⁻	C ⁺	CS
ILN	cm	kg ^a m	kg ^a m	kg ^a m	cm ^b	cm ^b	kg ^a m	(12+13)·III-2	(12+13)·III-2	7.85
ILN	2312	5598	--	--	12.06	12.06	42365	(12+13)·III-3	(12+13)·III-2	7.85
ILN	2302	5260	10	137	12.06	12.06	42365	(12+13)·III-3	(12+13)·III-2	7.85
CAMP	2290	5148	22	250	12.06	12.06	42365	(12+13)·III-3	(12+13)·III-2	7.85
134	134	5075	71	90	12.06	12.06	42365	(12+13)·III-3	(12+13)·III-2	8.20
2148	2148	5075	71	90	12.06	12.06	42365	(12+13)·III-3	(12+13)·III-2	8.20
2118	2118	5165	78	122	12.06	12.06	42365	(12+13)·III-3	(12+13)·III-2	8.20

Verifica a taglio: $\cot(\theta) = 2.500$

$$\text{Comb} = (12+13)\text{-VIII-4}$$

Sez	Td	VRdms	VRd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1803	--	125983	84882	84882	0	42365	149.1	10.05	47.1
Des							42365			

Trave di Fond.: 9010 [14, 15] | Pilastrate [39, 38]

Sez. R:	$B_y = 60.0 \text{ cm}$	$B_z = 100.0 \text{ cm}$	$L = 149.4 \text{ cm}$	$L_n = 149.4 \text{ cm}$	Terreno: Terrenol
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Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	M ₁ kg m ³	M ₂ kg m ³	AM ₁ kg m ³	AM ₂ kg m ³	Af ₁ cmq	Af ₂ cmq	Mr ₁ kg m ³	Mr ₂ kg m ³	C ⁻	C ⁺	CS
ILN	2085	5122	51	1206	12.06	12.06	42365	42365	(12+13)-V-3	(12+13)-V-2	8.27
	2104	5013	46	109	12.06	12.06	42365	42365	(12+13)-V-3	(12+13)-V-2	8.27
CAMP	2195	4972	13	221	12.06	12.06	42365	42365	(12+13)-V-3	(12+13)-V-2	8.16
	2202	5070	5	123	12.06	12.06	42365	42365	(12+13)-V-3	(12+13)-V-2	8.16
FLN	2207	5193	--	--	12.06	12.06	42365	42365	(12+13)-V-3	(12+13)-V-2	8.16

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 3

Sez	Td	VRdms	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafte	CS
	kg	kg	kg	kg	kg	kg	kg·m	cm	cmq/m	
Sin	1280	--	125983	84882	84882	0	42365	149.0	10.05	66.3
Des							42365			

Travedi Fond.: 9010 [12, 13] Pilastrate [41, 40]

Sez. R:	By= 60.0 cm	Bz=100.0 cm	L=149.7 cm	Ln=149.7 cm	Terreno: Terreno I
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Criterio : CLS_TraviFondazione - Verifica a flessione : Verificato

X	M _r cm	M _r kg m ⁻¹	AM _r kg m ⁻¹	AM ₊ kg m ⁻¹	AF _s cmq	AF _i cmq	Mr ⁻ kg m ⁻¹	Mr ⁺ kg m ⁻¹	C ⁻	C ⁺	CS
ILN	2204	5255	--	--	--	12.06	12.06	42.365	(12+13)II-2	(12+13)II-2	8.06
	2193	5120	11	135	12.06	12.06	42.365	42.365	(12+13)II-2	(12+13)II-2	8.06
CAMP	2179	5009	24	246	12.06	12.06	42.365	42.365	(12+13)II-3	(12+13)II-3	8.06
	2027	5001	77	122	12.06	12.06	42.365	42.365	(12+13)V-2	(12+13)V-2	8.27
FLN	1994	5123	86	--	12.06	12.06	42.365	42.365	(12+13)I-3	(12+13)V-2	8.27

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 3

Sez	Td	VRdms	VRd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*	cm	cmq/m	
Sin	1274	--	125983	84882	84882	0	42365	149.4	10.05	66.6
Des							42365			

Trave di Fond. : 9010 | 15, 16 | Pilastrate [38, 37]

Sez. R: By= 60,0 cm Bz=100,0 cm L=149,7 cm Terreno: Terreno1

Criterio : CLS Travifondazione - Verifica a flessione -Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2178	5166	30	--	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	8,20
15,0	2190	5056	26	110	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	8,20
CAMP	2236	5013	4	226	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	8,09
134,8	2239	5113	1	126	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	8,09
FLN	2240	5239	--	--	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	8,09

Verifica a taglio:cof(0) =2,500

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
15,0	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
CAMP	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
134,8	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
FLN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.

Verifica a taglio:cof(0) =2,500

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	1241	--	125983	88186	88186		42365	149,7	10,44	71,0
Des							42365			

Trave di Fond. : 9010 | 16, 17 | Pilastrate [37, 36]

Sez. R: By= 60,0 cm Bz=100,0 cm L=149,5 cm Terreno: Terreno1

Criterio : CLS Travifondazione - Verifica a flessione -Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2255	5257	37	--	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	8,06
14,9	2269	5149	33	108	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	8,06
CAMP	2334	5125	8	226	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,92
134,5	2339	5226	3	126	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,92
FLN	2342	5351	--	--	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,92

Verifica a taglio:cof(0) =2,500

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
14,9	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
CAMP	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
134,5	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
FLN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.

Verifica a taglio:cof(0) =2,500

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	1250	--	125983	84882	84882		42365	149,5	10,05	67,9
Des							42365			

Trave di Fond. : 9010 | 17, 18 | Pilastrate [36, 35]

Sez. R: By= 60,0 cm Bz=100,0 cm L=150,0 cm Terreno: Terreno1

Criterio : CLS Travifondazione - Verifica a flessione -Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2377	5396	--	--	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,85
15,0	2380	5281	--	115	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,85
CAMP	2380	5197	--	211	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,83
135,0	2348	5290	20	118	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,83
FLN	2338	5408	24	--	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,83

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
15,0	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
CAMP	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
135,0	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
FLN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.

Verifica a taglio:cof(0) =2,500

Comb =3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	1200	--	125983	87991	87991		42365	150,0	10,42	73,3
Des							42365			

Trave di Fond. : 9010 | 18, 19 | Pilastrate [35, 34]

Sez. R: By= 60,0 cm Bz=100,0 cm L=149,0 cm Terreno: Terreno1

Criterio : CLS Travifondazione - Verifica a flessione -Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2433	5526	--	--	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,67
14,9	2404	5375	30	150	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,67
CAMP	2376	5254	58	271	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,67
134,1	2264	5261	27	123	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,87
FLN	2260	5384	20	--	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,87

Verifica a taglio:cof(0) =2,500

Comb =(12+13)÷VIII+4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m			
ILN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
14,9	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
CAMP	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
134,1	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.
FLN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)÷V-3	(12+13)÷V-2	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)÷VIII+4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	1805	--	125983	84882	84882		42365	149,0	10,05	47,0
Des							42365			

Trave di Fond. : 9010 | 19, 20 | Pilastrate [34, 33]

Sez. R: By= 60,0 cm Bz=100,0 cm L=149,3 cm Terreno: Terreno1

Criterio : CLS Travifondazione - Verifica a flessione -Verificato

X	M-	M+	AM-	AM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2269	5401	13	--	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,84
14,9	2275	5284	9	117	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,84
CAMP	2284	5200	--	211	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,83
134,4	2269	5293	13	118	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,83
FLN	2261	5411	18	--	12,06	12,06	42365	42365	(12+13)÷V-3	(12+13)÷V-2	7,83

Verifica a taglio:cof(0) =2,500

Comb =3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Stafie	CS
kg	kg	kg	kg	kg	kg		kg*m	cm	cmq/m	
Sin	1252	--	125983	84882	84882		42365	149,3	10,05	67,8
Des							42365			

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
Des							42365			

Trave di Fond. : 9010 | 20, 21 | Pilastrate [33, 32]

Sez. R: By= 60,0 cm Bz=100,0 cm L=149,9 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alis	Ati	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2288	5453	--	--	12,06	12,06	42365	42365	(12+13)>V-3	(12+13)>V-2	7,77
15,0	2290	5334	--	--	118	12,06	42365	42365	(12+13)>V-3	(12+13)>V-2	7,77
CAMP	2374	5543	28	249	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,58
134,9	2390	5456	12	135	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,58
FLN	2402	5591	--	--	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,58

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V-3	(12+13)>V-2	Parz.	Parz.
15,0	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V-3	(12+13)>V-2	Parz.	Parz.
CAMP	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
134,9	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
FLN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1252	--	125983	88038	88038	0	42365	149,9	10,43	70,3
Des							42365			

Trave di Fond. : 9010 | 21, 22 | Pilastrate [32, 31]

Sez. R: By= 60,0 cm Bz=100,0 cm L=148,9 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alis	Ati	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2331	5547	67	--	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,64
14,9	2357	5438	56	108	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,64
CAMP	2445	5552	--	195	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,64
134,0	2443	5560	--	85	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,78
FLN	2436	5445	--	--	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,78

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
14,9	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
CAMP	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
134,0	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
FLN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1318	--	125983	84882	84882	0	42365	148,9	10,05	64,4
Des							42365			

Trave di Fond. : 9010 | 22, 23 | Pilastrate [31, 30]

Sez. R: By= 60,0 cm Bz=100,0 cm L=149,2 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alis	Ati	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2386	5439	--	--	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,79
14,9	2384	5269	2	169	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,79
CAMP	2278	5119	7	319	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	7,79
134,3	2235	4645	80	74	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	8,98
FLN	2200	4659	91	38	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	9,02

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X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
14,9	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
CAMP	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
134,3	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
FLN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1473	--	125983	84882	84882	0	42365	149,2	10,05	57,6
Des							42365			

Trave di Fond. : 9010 | 23, 24 | Pilastrate [30, 29]

Sez. R: By= 60,0 cm Bz=100,0 cm L=149,8 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alis	Ati	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2205	4728	--	--	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	8,96
15,0	2167	4475	38	253	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	8,96
CAMP	2126	4242	79	486	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	8,96
134,8	1760	3212	164	294	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	12,1
FLN	1699	3154	170	230	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	12,5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
15,0	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
CAMP	19,2	95,9	0,201	19,3	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
134,8	19,2	95,9	0,200	19,2	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
FLN	19,2	95,9	0,200	19,2	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)>V1-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1787	--	125983	88150	88150	0	42365	149,8	10,44	49,3
Des							42365			

Trave di Fond. : 9010 | 24, 25 | Pilastrate [29, 28]

Sez. R: By= 60,0 cm Bz=100,0 cm L=149,4 cm Terreno: **Terreno1**

Criterio : CLS_TraviFondazione - Verifica a flessione .**Verificato**

X	M-	M+	AM-	AM+	Alis	Ati	Mr+	Mr-	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1747	3286	--	--	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	12,9
14,9	1667	2958	80	328	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	12,9
CAMP	1587	2655	160	631	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	12,9
134,4	-978	-722	2255	2426	12,06	12,06	42365	42365	(12+13)>V1-3	(12+13)>V1-2	24,9
FLN	1051	-702	--	2013	12,06	12,06	42365	42365	(12+13)>V1-4	(12+13)>V1-2	32,3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	19,2	95,9	0,200	19,2	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
14,9	19,2	95,9	0,200	19,2	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
CAMP	19,2	95,9	0,200	19,2	95,9	0,201	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
134,4	19,2	95,9	0,200	19,2	95,9	0,200	42365	42365	(12+13)>V1-3	(12+13)>V1-2	Parz.	Parz.
FLN	19,2	95,9	0,200	19,2	95,9	0,200	42365	42365	(12+13)>V1-4	(12+13)>V1-2	Parz.	Parz.

Verifica a taglio:cof(0) =2,500

Comb =(12+13)>V1-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
kg	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin										
Des										

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Sez	Td	VRdms	VRcd	VRsd	VRd	Mr	Dx	Stafle	CS
Sin	2333	--	125983	84882	84882	0	42365	149.4	10.05
Des					42365				

Trave di Fond.: 9010 [25, 26.] Pilastrate [28., 52]

Sez. R: By=60.0 cm Bz=100.0 cm L=149.4 cm Ln=161.4 cm Terreno: Terreno I
 Criterio : CLS TravFondazione - Verifica a flessione : Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1270	1596	--	--	12.06	12.06	42365	42365	(12+13)÷V1-4	(12+13)÷V1-1
16.1	1110	1219	160	377	12.06	12.06	42365	42365	(12+13)÷V1-4	(12+13)÷V1-1
CAMP	955	885	315	710	12.06	12.06	42365	42365	(12+13)÷V1-4	(12+13)÷V1-1
145.3	162	342	511	208	12.06	12.06	42365	42365	8 (12+13)÷VIII-4	62.9
FLN	-113	551	631	--	12.06	12.06	42365	42365	8 (12+13)÷VIII-4	77.0

X	x-	d-	x÷d-	x+	d+	x÷d+	Mr-	Mr+	C-	C+	Stato+
cm	cm	cm	cm	cm	cm	cm	kg*m	kg*m			
ILN	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)÷V1-4	(12+13)÷V1-1	Parz.
16.1	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)÷V1-4	(12+13)÷V1-1	Parz.
CAMP	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	(12+13)÷V1-4	(12+13)÷V1-1	Parz.
145.3	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	8 (12+13)÷VIII-4	Parz.	Parz.
FLN	19.2	95.9	0.200	19.2	95.9	0.200	42365	42365	8 (12+13)÷VIII-4	Parz.	Parz.

Verifica a taglio cot(θ) =2.500

Comb =(12+13)÷V1-1

Sez	Td	VRdms	VRcd	VRsd	VRd	Mr	Dx	Stafle	CS
Sin	2544	--	125983	84882	84882	0	42365	161.4	10.05
Des					42365				33.4

Verifica Stabilità aste Metalliche

Scenario di calcolo : Set_NT_S1V_A2_STR/GEO

Asta : 1 [1., 54]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-17608	-914	-2034	211298	20492	9673	24	40	0.973	0.865	--	0.721	0.343

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	17608	659	699	195843	19516	9213	(12+13)÷I1-4	5.01
1	Z	17608	396	1164	174030	19516	9213	(12+13)÷I1-4	4.04

Asta : 1 [54., 101]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-6537	-2785	577	211298	20492	9673	17	28	0.955	0.936	--	0.792	0.381

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6537	2205	220	192094	19516	9213	3	5.85
1	Z	6537	1323	367	188346	19516	9213	3	7.03

Asta : 2 [2., 53]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-12837	-799	1219	211298	20492	9673	24	40	0.973	0.865	--	0.454	0.382

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	12837	363	466	195843	19516	9213	(12+13)÷V1-1	7.42
1	Z	12837	218	777	174030	19516	9213	(12+13)÷V1-1	5.91

Asta : 2 [53., 102]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-3088	-4575	540	211298	20492	9673	17	28	0.955	0.936	--	0.753	0.385

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3088	3445	208	192094	19516	9213	3	4.65
1	Z	3088	2067	347	188346	19516	9213	3	6.25

Asta : 3 [3., 55]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-2759	841	-2060	211298	20492	9673	24	40	0.973	0.865	--	0.400	0.343

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2759	337	707	195843	19516	9213	(12+13)÷V1-4	9.25
1	Z	2759	202	1179	174030	19516	9213	(12+13)÷V1-4	6.49

Asta : 3 [55., 103]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-6753	-4952	485	211298	20492	9673	17	28	0.955	0.936	--	0.733	0.363

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6753	3629	176	192094	19516	9213	3	4.16
1	Z	6753	2178	293	188346	19516	9213	3	5.58

Asta : 4 [4., 56]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-3419	960	-2064	211298	20492	9673	24	40	0.973	0.865	--	0.401	0.347

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3419	384	716	195843	19516	9213	(12+13)÷V1-4	8.71
1	Z	3419	231	1193	174030	19516	9213	(12+13)÷V1-4	6.21

Asta : 4 [56., 104]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

kg/cmq ft=4300 kg/cmq **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m							
-6600	-4914	447	211298	20492	9673	17	28	0.955	0.936	--	0.732	0.395

Clis	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6600	3598	176	192094	19516	9213	3	4.20

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Z	6600	2159	294	188346	19516	9213	3	5.63

Asta : 5 [5 , 71]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								
-3195	1001	-2048	211298	20492	9673	24	40	0.973	0.865	--	0.400	0.349	0.240
0.582													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	3195	401	715	195843	19516	9213	(12+13)·V/I-4	8.74
1	Z	3195	240	1191	174030	19516	9213	(12+13)·V/I-4	6.25

Asta : 5 [71 , 105]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								
-6849	-5027	433	211298	20492	9673	17	28	0.955	0.936	--	0.727	0.376	0.436
0.627													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	6849	3653	163	192094	19516	9213	3	4.16
1	Z	6849	2192	271	188346	19516	9213	3	5.61

Asta : 6 [6 , 74]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								
-2509	958	-2033	211298	20492	9673	24	40	0.973	0.865	--	0.400	0.349	0.240
0.582													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	2509	383	710	195843	19516	9213	(12+13)·V/I-4	9.13
1	Z	2509	230	1183	174030	19516	9213	(12+13)·V/I-4	6.47

Asta : 6 [74 , 106]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								
-6918	-5097	418	211298	20492	9673	17	28	0.955	0.936	--	0.725	0.394	0.435
0.657													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	6918	3697	165	192094	19516	9213	3	4.11
1	Z	6918	2218	274	188346	19516	9213	3	5.55

Asta : 7 [7 , 76]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								
-18710	834	-1994	211298	20492	9673	24	40	0.973	0.865	--	0.403	0.362	0.242
0.603													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	18710	336	721	195843	19516	9213	(12+13)·V/I-4	5.23
1	Z	18710	202	1202	174030	19516	9213	(12+13)·V/I-4	4.03

Asta : 7 [76 , 107]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								
-8804	-4960	442	211298	20492	9673	17	28	0.955	0.936	--	0.726	0.410	0.436
0.683													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	8804	3602	181	192094	19516	9213	3	4.00
1	Z	8804	2161	302	188346	19516	9213	3	5.26

Asta : 8 [8 , 75]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								
-15985	1386	1501	211298	20492	9673	24	40	0.973	0.865	--	0.422	0.378	0.253
0.631													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	15985	585	568	195843	19516	9213	(12+13)·V/I-1	5.77
1	Z	15985	351	947	174030	19516	9213	(12+13)·V/I-1	4.70

Asta : 8 [75 , 108]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								
-4657	-5222	398	211298	20492	9673	17	28	0.955	0.936	--	0.720	0.446	0.432
0.743													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	4657	3760	177	192094	19516	9213	3	4.23
1	Z	4657	2256	296	188346	19516	9213	3	5.80

Asta : 9 [9 , 72]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								
-3410	1519	-1819	211298	20492	9673	24	40	0.973	0.865	--	0.410	0.357	0.246
0.596													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	3410	623	650	195843	19516	9213	(12+13)·V/III-4	8.34
1	Z	3410	374	1083	174030	19516	9213	(12+13)·V/III-4	6.40

Asta : 9 [72 , 109]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								
-6698	-4772	363	211298	20492	9673	17	28	0.955	0.936	--	0.727	0.365	0.436
0.608													

Cls	Dir	N	Mveq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
1	Y	6698	3470	133	192094	19516	9213	3	4.40
1	Z	6698	2082	221	188346	19516	9213	3	6.02

Asta : 10 [10 , 70]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq: **Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg	kg*m	kg*m	kg*m								

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
-3390	1512	-1771	211298	20492	9673	24	40	0.973	0.865	--	0.456	0.362	0.273
													0.604
Cls	Dir	N	Mvseq	Mzseq	NRd	MyRd	MzRd				Comb.	SF	
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	3390	689	642	195843	19516	9213	(12+13)∖VIII-4	8.18				
1	Z	3390	413	1069	174030	19516	9213	(12+13)∖VIII-4	6.38				

Asta : 10 [70 , 110]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg*m								
-6685	-4808	341	211298	20492	9673	17	28	0.955	0.936	--	0.727	0.344	0.436

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	λY	λZ	χY	χZ	χLT	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m							
1	Y	6685	3494	117	192094	19516	9213	9213	(12+13)∖VII-4	8.23			
1	Z	6685	2096	195	188346	19516	9213	9213	(12+13)∖VII-4	6.32			

Asta : 11 [11 , 69]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg*m								
-3468	1437	-1812	211298	20492	9673	24	40	0.973	0.865	--	0.442	0.363	0.265

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	λY	λZ	χY	χZ	χLT	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m							
1	Y	3468	634	657	195843	19516	9213	9213	(12+13)∖VI-4	8.23			
1	Z	3468	381	1096	174030	19516	9213	9213	(12+13)∖VI-4	6.32			

Asta : 11 [69 , 111]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg*m								
-6990	-4908	316	211298	20492	9673	17	28	0.955	0.936	--	0.721	0.366	0.433

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	λY	λZ	χY	χZ	χLT	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m							
1	Y	6990	3541	116	192094	19516	9213	9213	(12+13)∖VIII-4	8.09			
1	Z	6990	2125	193	188346	19516	9213	9213	(12+13)∖VIII-4	6.46			

Asta : 12 [12 , 77]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg*m								
-3464	1588	-1691	211298	20492	9673	24	40	0.973	0.865	--	0.480	0.364	0.288

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	λY	λZ	χY	χZ	χLT	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m							
1	Y	3464	762	616	195843	19516	9213	9213	(12+13)∖VIII-4	8.09			
1	Z	3464	457	1027	174030	19516	9213	9213	(12+13)∖VIII-4	6.46			

Asta : 12 [77 , 112]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg*m								
-6589	-4667	304	211298	20492	9673	17	28	0.955	0.936	--	0.725	0.369	0.435

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	λY	λZ	χY	χZ	χLT	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m							
1	Y	6589	3385	112	192094	19516	9213	9213	(12+13)∖VIII-4	8.18			
1	Z	6589	2031	187	188346	19516	9213	9213	(12+13)∖VIII-4	6.28			

Asta : 13 [13 , 78]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg*m								
-16768	1650	-1652	211298	20492	9673	24	40	0.973	0.865	--	0.403	0.373	0.242

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	λY	λZ	χY	χZ	χLT	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m							
1	Y	16768	664	616	195843	19516	9213	9213	(12+13)∖VIII-4	5.36			
1	Z	16768	399	1027	174030	19516	9213	9213	(12+13)∖VIII-4	4.38			

Asta : 13 [78 , 113]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg*m								
-7487	-4785	522	211298	20492	9673	17	28	0.955	0.936	--	0.727	0.359	0.436

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	λY	λZ	χY	χZ	χLT	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m							
1	Y	7487	3480	116	192094	19516	9213	9213	(12+13)∖VII-4	8.23			
1	Z	7487	2088	193	188346	19516	9213	9213	(12+13)∖VII-4	5.96			

Asta : 14 [14 , 73]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg*m								
-17288	1172	1750	211298	20492	9673	24	40	0.973	0.865	--	0.403	0.368	0.242

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	λY	λZ	χY	χZ	χLT	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m							
1	Y	17288	472	644	195843	19516	9213	9213	(12+13)∖VI-1	5.48			
1	Z	17288	283	1074	174030	19516	9213	9213	(12+13)∖VI-1	4.34			

Asta : 14 [73 , 114]

Sez. G: HE 240 A L=167.0 cm Ln1=167.0 cm Ln2=167.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg*m								
-5462	-4848	292	211298	20492	9673	17	28	0.955	0.936	--	0.721	0.310	0.433

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	λY	λZ	χY	χZ	χLT	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m							
1	Y	5462	3496	91	192094	19516	9213	9213	(12+13)∖VIII-4	8.09			
1	Z	5462	2098	151	188346	19516	9213	9213	(12+13)∖VIII-4	6.54			

Asta : 15 [15 , 61]

Sez. G: HE 240 A L=240.0 cm Ln1=240.0 cm Ln2=240.0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619
kg/cmq ft=4300 kg/cmq;*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg	kg*m	kg*m								
-3284	1448	-1656	211298	20492	9673	24	40	0.973	0.865	--	0.454	0.367	0.273

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	λY	λZ	χY	χZ	χLT	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m							
1	Y	3284	658	607	195843	19516	9213	9213	(12+13)∖VI-4	8.59			
1	Z	3284	395	1012	174030	19516	9213	9213	(12+13)∖VI-4	6.71			

Asia : 15 [61 , 115]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6527	-4638	258	211298	20492	9673	17	28	0,955	0,936	--	0,727	0,305	0,436
0,508													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6527	3371	78	192094	19516	9213	3	4,65
1	Z	6527	2023	131	188346	19516	9213	3	6,56

Asia : 16 [16 , 62]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3526	1263	1826	211298	20492	9673	24	40	0,973	0,865	--	0,401	0,359	0,240
0,599													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3526	506	656	195843	19516	9213	(12+13)·V1-1	8,68
1	Z	3526	303	1094	174030	19516	9213	(12+13)·V1-1	6,47

Asia : 16 [62 , 116]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6909	-4857	236	211298	20492	9673	17	28	0,955	0,936	--	0,723	0,289	0,434
0,481													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6909	3512	68	192094	19516	9213	3	4,48
1	Z	6909	2107	114	188346	19516	9213	3	6,37

Asia : 17 [17 , 63]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2056	1148	1866	211298	20492	9673	24	40	0,973	0,865	--	0,492	0,358	0,295
0,597													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2056	565	668	195843	19516	9213	(12+13)·V1-1	8,93
1	Z	2056	339	1114	174030	19516	9213	(12+13)·V1-1	6,66

Asia : 17 [63 , 117]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6614	-4710	216	211298	20492	9673	17	28	0,955	0,936	--	0,728	0,309	0,437
0,514													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6614	3427	67	192094	19516	9213	3	4,60
1	Z	6614	2056	111	188346	19516	9213	3	6,56

Asia : 18 [18 , 64]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6771	-4872	165	211298	20492	9673	17	28	0,955	0,936	--	0,725	0,240	0,435
0,401													

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-16449	1872	-1575	211298	20492	9673	24	40	0,973	0,865	--	0,421	0,366	0,253
0,611													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	16449	788	577	195843	19516	9213	(12+13)·V1-4	5,35
1	Z	16449	473	962	174030	19516	9213	(12+13)·V1-4	4,48

Asia : 18 [64 , 118]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6886	-4991	194	211298	20492	9673	17	28	0,955	0,936	--	0,724	0,259	0,434
0,432													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6886	3612	50	192094	19516	9213	3	4,42
1	Z	6886	2167	84	188346	19516	9213	3	6,38

Asia : 19 [19 , 60]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-18620	908	1955	211298	20492	9673	24	40	0,973	0,865	--	0,403	0,367	0,242
0,611													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	18620	366	717	195843	19516	9213	(12+13)·V1-1	5,22
1	Z	18620	220	1195	174030	19516	9213	(12+13)·V1-1	4,03

Asia : 19 [60 , 119]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6519	-4953	192	211298	20492	9673	17	28	0,955	0,936	--	0,724	0,240	0,434
0,401													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6519	3586	46	192094	19516	9213	3	4,49
1	Z	6519	2152	77	188346	19516	9213	3	6,53

Asia : 20 [20 , 57]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3062	912	1988	211298	20492	9673	24	40	0,973	0,865	--	0,400	0,357	0,240
0,595													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3062	365	709	195843	19516	9213	(12+13)·V1-1	8,98
1	Z	3062	219	1182	174030	19516	9213	(12+13)·V1-1	6,36

Asia : 20 [57 , 120]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6771	-4872	165	211298	20492	9673	17	28	0,955	0,936	--	0,725	0,240	0,435
0,401													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6771	3530	40	192094	19516	9213	3	4.54
1	Z	6771	2118	66	188346	19516	9213	3	6.59

Asta : 21 [21 , 59]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-3085	936	2017	211298	20492	9673	24	40	0.973	0.865	--	0.400	0.357	0.240
											0.435	0.594	

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3085	375	719	195843	19516	9213	(12+13) > V1-1	8.85
1	Z	3085	225	1199	174030	19516	9213	(12+13) > V1-1	6.27

Asta : 21 [59 , 121]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-4756	-5013	-179	211298	20492	9673	17	28	0.955	0.936	--	0.726	0.240	0.435
											0.435	0.401	

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6756	3639	43	192094	19516	9213	3	4.42
1	Z	6756	2183	72	188346	19516	9213	3	6.43

Asta : 22 [22 , 65]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-3197	2254	1941	211298	20492	9673	24	40	0.973	0.865	--	0.469	0.357	0.282
											0.282	0.596	

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3197	1058	694	195843	19516	9213	(12+13) > VIII-1	6.86
1	Z	3197	635	1156	174030	19516	9213	(12+13) > VIII-1	5.67

Asta : 22 [65 , 122]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-4715	-4958	129	211298	20492	9673	17	28	0.955	0.936	--	0.726	0.240	0.435
											0.435	0.401	

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6715	3599	31	192094	19516	9213	3	4.49
1	Z	6715	2159	52	188346	19516	9213	3	6.58

Asta : 23 [23 , 58]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-3358	1148	1969	211298	20492	9673	24	40	0.973	0.865	--	0.489	0.351	0.294
											0.294	0.585	

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3358	562	690	195843	19516	9213	(12+13) > VIII-1	8.27
1	Z	3358	337	1151	174030	19516	9213	(12+13) > VIII-1	6.19

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Asta : 23 [58 , 123]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-6332	-4772	-139	211298	20492	9673	17	28	0.955	0.936	--	0.730	0.240	0.438
											0.438	0.401	

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6332	3483	33	192094	19516	9213	3	4.65
1	Z	6332	2090	56	188346	19516	9213	3	6.81

Asta : 24 [24 , 66]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-3783	-841	2074	211298	20492	9673	24	40	0.973	0.865	--	0.409	0.344	0.245
											0.245	0.573	

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3783	344	713	195843	19516	9213	(12+13) > V1-1	8.75
1	Z	3783	206	1188	174030	19516	9213	(12+13) > V1-1	6.20

Asta : 24 [66 , 124]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-6693	-4870	104	211298	20492	9673	17	28	0.955	0.936	--	0.730	0.240	0.438
											0.438	0.401	

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6693	3557	25	192094	19516	9213	3	4.55
1	Z	6693	2134	42	188346	19516	9213	3	6.69

Asta : 25 [25 , 67]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-13182	2136	-1207	211298	20492	9673	24	40	0.973	0.865	--	0.522	0.389	0.313
											0.313	0.648	

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	13182	1114	469	195843	19516	9213	(12+13) > V1-4	5.70
1	Z	13182	669	782	174030	19516	9213	(12+13) > V1-4	5.13

Asta : 25 [67 , 125]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-4701	-4313	-148	211298	20492	9673	17	28	0.955	0.936	--	0.745	0.240	0.447
											0.447	0.401	

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4701	3213	35	192094	19516	9213	3	5.18
1	Z	4701	1928	59	188346	19516	9213	3	7.68

Asta : 26 [26 , 68]

Sez. G: HE 240 A L=240,0 cm Ln1=240,0 cm Ln2=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1,05 f_{yk} \gamma M=2619$
kg/cm² ft=4300 kg/cm² **Verificato**

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-18495	-1185	2110	211298	20492	9673	24	40	0.973	0.865	--	0.695	0.340	0.417	0.567
Clis	Dir	N	Mvseq	Mzseq	NRd	MyRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	18495	824	718	195843	19516	9213	(12+13)-V1-1						4.66
1	Z	18495	494	1197	174030	19516	9213	(12+13)-V1-1						3.82

Asia : 26 [68 , 126]

Sez. G: HE 240 A L=167,0 cm Ln1=167,0 cm Ln2=167,0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg ^m	kg ^m	kg	kg ^m	kg ^m									
-8539	-2851	-276	211298	20492	9673	17	28	0.955	0.936	—	0.735	0.385	0.441	0.641

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	8539	2097	106	192094	19516	9213	(12+13)-V1-1						6.12
1	Z	8539	1258	177	188346	19516	9213	(12+13)-V1-1						7.75

Asia : 27 [1 , 327]

Sez. G: HE 240 A L=60,0 cm Ln1=60,0 cm Ln2=60,0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-1556	4283	244	211298	20492	9673	6	10	1.000	1.000	—	0.754	0.329	0.453	0.549

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	1556	3231	80	201236	19516	9213	(12+13)-IV-1						5.50
1	Z	1556	1938	134	201236	19516	9213	(12+13)-IV-1						8.23

Asia : 28 [25 , 351]

Sez. G: HE 240 A L=60,0 cm Ln1=60,0 cm Ln2=60,0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-2282	3674	439	211298	20492	9673	6	10	1.000	1.000	—	0.91	0.385	0.547	0.642

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	2282	3347	169	201236	19516	9213	(12+13)-V1-1						4.97
1	Z	2282	2008	282	201236	19516	9213	(12+13)-V1-1						6.90

Asia : 29 [24 , 350]

Sez. G: HE 240 A L=60,0 cm Ln1=60,0 cm Ln2=60,0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-1965	2731	-202	211298	20492	9673	6	10	1.000	1.000	--	0.974	0.335	0.584	0.558

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	1965	2660	68	201236	19516	9213	(12+13)-II-2						6.52
1	Z	1965	1596	113	201236	19516	9213	(12+13)-II-2						9.64

Asia : 30 [23 , 349]

Sez. G: HE 240 A L=60,0 cm Ln1=60,0 cm Ln2=60,0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-1888	2508	-295	211298	20492	9673	6	10	1.000	1.000	—	0.982	0.387	0.589	0.644

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	1888	2462	114	201236	19516	9213	(12+13)-V1-2						6.76
1	Z	1888	1477	190	201236	19516	9213	(12+13)-V1-2						9.46

Asia : 31 [22 , 348]

Sez. G: HE 240 A L=60,0 cm Ln1=60,0 cm Ln2=60,0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1819	2371	-234	211298	20492	9673	6	10	1.000	1.000	--	0.995	0.333	0.597
													0.554

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	1819	2360	78	201236	19516	9213	(12+13)-V1-2						7.22
1	Z	1819	1416	130	201236	19516	9213	(12+13)-V1-2						10.5

Asia : 32 [21 , 347]

Sez. G: HE 240 A L=60,0 cm Ln1=60,0 cm Ln2=60,0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1766	2272	-295	211298	20492	9673	6	10	1.000	1.000	--	0.996	0.370	0.598	0.617

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	1766	2264	109	201236	19516	9213	(12+13)-V1-2						7.32
1	Z	1766	1358	182	201236	19516	9213	(12+13)-V1-2						10.2

Asia : 33 [20 , 346]

Sez. G: HE 240 A L=60,0 cm Ln1=60,0 cm Ln2=60,0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1744	2261	116	211298	20492	9673	6	10	1.000	1.000	--	0.999	0.351	0.600
												0.584	

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	1744	2259	41	201236	19516	9213	(12+13)-V-2						7.76
1	Z	1744	1356	68	201236	19516	9213	(12+13)-V-2						11.7

Asia : 34 [19 , 345]

Sez. G: HE 240 A L=60,0 cm Ln1=60,0 cm Ln2=60,0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2242	4068	-358	211298	20492	9673	6	10	1.000	1.000	--	0.858	0.366	0.515
0.609													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	2242	3490	131	201236	19516	9213	(12+13)-VIII-2						4.90
1	Z	2242	2094	218	201236	19516	9213	(12+13)-VIII-2						7.04

Asia : 35 [18 , 344]

Sez. G: HE 240 A L=60,0 cm Ln1=60,0 cm Ln2=60,0 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619 kg/cmq ft=4300 kg/cmq; **Verficato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-2261	3951	524	211298	20492	9673	6	10	1.000	1.000	--	0.871	0.347	0.523	0.579

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.						SF
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	2261	3443	182	201236	19516	9213	(12+13)-VIII-1						4.82
1	Z	2261	2066	303	201236	19516	9213	(12+13)-VIII-1						6.67

Asta : 36 [17 , 343]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.976	0.328	0.586
-1760	2387	105	211298	20492	9673	6	10	1,000	1,000	--	0.976	0.328	0.586

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	1760	2329	35	201236	19516	9213	(12+13)-V-2	7.59
1	Z	1760	1397	58	201236	19516	9213	(12+13)-V-2	11.5

Asta : 37 [16 , 342]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.979	0.383	0.587
-1741	2336	109	211298	20492	9673	6	10	1,000	1,000	--	0.979	0.383	0.587

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	1741	2286	42	201236	19516	9213	(12+13)-VII-2	7.67
1	Z	1741	1372	70	201236	19516	9213	(12+13)-VII-2	11.6

Asta : 38 [15 , 341]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.977	0.350	0.586
-1740	2350	79	211298	20492	9673	6	10	1,000	1,000	--	0.977	0.350	0.586

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	1740	2295	28	201236	19516	9213	(12+13)-VII-2	7.74
1	Z	1740	1377	46	201236	19516	9213	(12+13)-VII-2	11.9

Asta : 39 [14 , 340]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.965	0.336	0.579
-2221	3409	-388	211298	20492	9673	6	10	1,000	1,000	--	0.965	0.336	0.579

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	2221	3289	130	201236	19516	9213	(12+13)-VIII-2	5.16
1	Z	2221	1974	217	201236	19516	9213	(12+13)-VIII-2	7.37

Asta : 40 [13 , 339]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.867	0.341	0.520
-2188	3847	516	211298	20492	9673	6	10	1,000	1,000	--	0.867	0.341	0.520

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	2188	3337	176	201236	19516	9213	(12+13)-VIII-1	4.98
1	Z	2188	2002	293	201236	19516	9213	(12+13)-VIII-1	6.88

Asta : 41 [12 , 338]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.978	0.350	0.587
-1713	2264	69	211298	20492	9673	6	10	1,000	1,000	--	0.978	0.350	0.587

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	1713	2214	24	201236	19516	9213	(12+13)-VII-2	8.03
1	Z	1713	1328	40	201236	19516	9213	(12+13)-VII-2	12.4

Asta : 42 [11 , 337]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.977	0.378	0.586
-1706	2252	98	211298	20492	9673	6	10	1,000	1,000	--	0.977	0.378	0.586

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	1706	2182	37	201236	19516	9213	(12+13)-VII-2	8.04
1	Z	1706	1309	62	201236	19516	9213	(12+13)-VII-2	12.2

Asta : 43 [10 , 336]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.989	0.524	0.593
-1706	2175	6	211298	20492	9673	6	10	1,000	1,000	--	0.989	0.524	0.593

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	1706	2151	3	201236	19516	9213	(12+13)-III-2	8.40
1	Z	1706	1291	5	201236	19516	9213	(12+13)-III-2	13.3

Asta : 44 [9 , 335]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.977	0.298	0.586
-1789	2370	10	211298	20492	9673	6	10	1,000	1,000	--	0.977	0.298	0.586

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	1789	2315	3	201236	19516	9213	(12+13)-III-2	7.82
1	Z	1789	1389	5	201236	19516	9213	(12+13)-III-2	12.4

Asta : 45 [8 , 334]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.853	0.390	0.512
-2174	4167	-408	211298	20492	9673	6	10	1,000	1,000	--	0.853	0.390	0.512

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m		
1	Y	2174	3555	159	201236	19516	9213	(12+13)-IV-2	4.76
1	Z	2174	2133	265	201236	19516	9213	(12+13)-IV-2	6.72

Asta : 46 [7 , 333]

Sez. G: HE 240 A L=60.0 cm L_{n1}=60.0 cm L_{n2}=60.0 cm Crit.: Acciaio_Pressflessione γ_M=1.05 fy_k/γ_M=2619 kg/cmq
ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyy	kzz
kg	kg* ^m	kg* ^m	kg	kg* ^m	kg* ^m	6	10	1,000	1,000	--	0.849	0.366	0.509
-2163	4111	455	211298	20492	9673	6	10	1,000	1,000	--	0.849	0.366	0.509

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	2163	3490	167	20236	19516	9213	(12+13)-IV-1	4.82
I	Z	2163	2094	278	20236	19516	9213	(12+13)-IV-1	6.75

Asta : 47 [6 , 332]

Sez. G: HE 240 A L=60.0 cm Ln1=60.0 cm Ln2=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq
f=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m				
-2026	2817	162	211298	20492	9673	6	10	1.000	1.000	--	0.973	0.325	0.584
													0.541

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	2026	2741	53	20236	19516	9213	(12+13)-III-1	6.40
I	Z	2026	1645	88	20236	19516	9213	(12+13)-III-1	9.63

Asta : 48 [5 , 331]

Sez. G: HE 240 A L=60.0 cm Ln1=60.0 cm Ln2=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq
f=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m				
-2087	2937	182	211298	20492	9673	6	10	1.000	1.000	--	0.973	0.333	0.584
													0.555

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	2087	2857	60	20236	19516	9213	(12+13)-III-1	6.12
I	Z	2087	1714	101	20236	19516	9213	(12+13)-III-1	9.16

Asta : 49 [4 , 330]

Sez. G: HE 240 A L=60.0 cm Ln1=60.0 cm Ln2=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq
f=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m				
-2107	3035	272	211298	20492	9673	6	10	1.000	1.000	--	0.957	0.387	0.574
													0.646

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	2107	2906	105	20236	19516	9213	(12+13)-I-1	5.85
I	Z	2107	1743	176	20236	19516	9213	(12+13)-I-1	8.41

Asta : 50 [3 , 329]

Sez. G: HE 240 A L=60.0 cm Ln1=60.0 cm Ln2=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq
f=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m				
-2216	3282	199	211298	20492	9673	6	10	1.000	1.000	--	0.960	0.388	0.576
													0.646

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	2216	3150	77	20236	19516	9213	(12+13)-I-1	5.53
I	Z	2216	1890	128	20236	19516	9213	(12+13)-I-1	8.21

Asta : 51 [2 , 328]

Sez. G: HE 240 A L=60.0 cm Ln1=60.0 cm Ln2=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq
f=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m				
-2232	3880	-549	211298	20492	9673	6	10	1.000	1.000	--	0.890	0.379	0.534
													0.632

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	2232	3452	208	20236	19516	9213	(12+13)-IV-2	4.75
I	Z	2232	2071	347	20236	19516	9213	(12+13)-IV-2	6.46

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Asta : 52 [26 , 352]

Sez. G: HE 240 A L=60.0 cm Ln1=60.0 cm Ln2=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq
f=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m				
-1692	3975	-231	211298	20492	9673	6	10	1.000	1.000	--	0.768	0.325	0.461
													0.542

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	1692	3051	75	20236	19516	9213	(12+13)-VI-4	5.78
I	Z	1692	1831	125	20236	19516	9213	(12+13)-VI-4	8.63

Asta : 8000 [0 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq f=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m				
-2545	1905	-217	211298	20492	9673	18	30	0.945	0.923	--	0.863	0.360	0.518
													0.601

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	2545	1644	78	190238	19516	9213	(12+13)-I-1	9.43
I	Z	2545	986	130	185803	19516	9213	(12+13)-I-1	12.8

Asta : 8000 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq f=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m				
-2297	1549	-225	211298	20492	9673	18	30	0.948	0.927	--	0.825	0.540	0.495
													0.900

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	2297	1277	122	190743	19516	9213	(12+13)-I-1	11.0
I	Z	2297	766	203	186492	19516	9213	(12+13)-I-1	13.6

Asta : 8000 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq f=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m				
-540	-2436	424	211298	20492	9673	18	30	0.948	0.927	--	0.836	0.586	0.502
													0.977

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	540	2038	248	190743	19516	9213	8	7.45
I	Z	540	1223	414	186492	19516	9213	8	9.05

Asta : 8000 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq f=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m				
-1288	-2292	433	211298	20492	9673	15	25	0.965	0.950	--	0.905	0.531	0.485
													0.885

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
I	Y	1288	2075	230	194116	19516	9213	3	7.25
I	Z	1288	1245	384	191146	19516	9213	3	8.91

Asta : 8000 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq f=4300 kg/cmq;**Verificato**

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N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χ_{LT}	kyy	kzy	kzz	
kg	kg·m	kg·m	kg	kg·m	kg·m									
-413	-3294	588	211298	20492	9673	15	25	0.967	0.953	—	0.969	0.499	0.582	0.832

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	413	3193	293	194567	19516	9213	8	5.06
1	Z	413	1916	489	191775	19516	9213	8	6.52

Asia : 8000 [0 , 73]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

g/cmq ft=4300 kg/cmq, <i>Verificato</i>													
N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-29	-3279	383	211298	20492	9673	13	22	0.976	0.965	--	1.000	0.485	0.600 0.809

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	29	3279	186	196339	19516	9213	8	5.31
1	Z	29	1967	310	194259	19516	9213	8	7.43

Asia : 8000 [73 , 74]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

g/cmq ft=4300 kg/cmq, <i>Verified</i>													
N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m								
-132	-3190	219	211298	20492	9673	12	20	0.983	0.976	--	0.953	0.441	0.572 0.736

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	132	3041	97	197915	19516	9213	8	5.99
1	Z	132	1825	161	196487	19516	9213	8	8.96

Asia : 8000 [74 , 399]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

g/cmq ft=4300 kg/cmq. <i>Verified</i>														
N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-2258	1986	174	211298	20492	9673	11	19	0.990	0.985	--	0.807	0.263	0.484	0.438

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2258	1603	46	199179	19516	9213	(12+13)-IV-4	10.2
1	Z	2258	962	76	198286	19516	9213	(12+13)-IV-4	14.5

Asia : 8000 [399 , 400]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

g/cm ft=4300 kg/cm; <i>Verificado</i>														
N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-4821	1688	161	211298	20492	9673	11	18	0.993	0.990	--	0.947	0.260	0.568	0.433

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4821	1598	42	199875	19516	9213	(12+13)-IV-4	9.04
1	Z	4821	959	70	199281	19516	9213	(12+13)-IV-4	12.4

Asia : 8000 [400 , 327]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

g/cmq ft=4300 kg/cmq, Verified													
N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4684	1512	-80	211298	20492	9673	11	19	0.990	0.986	--	0.541	0.250	0.325 0.417

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4684	818	20	199297	19516	9213	(12+13)-VIII-4	14.8
1	Z	4684	491	33	198454	19516	9213	(12+13)-VIII-4	19.1

Asia : 8001 [102 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

g/cmq ft=4300 kg/cmq. <i>Verified</i>														
N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz	
kg	kg*m	kg*m	kg	kg*m	kg*m									
-7455	3748	-194	211298	20492	9673	18	30	0.945	0.923	--	0.682	0.337	0.409	0.561

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7455	2557	65	190236	19516	9213	3	5.64
1	Z	7455	1534	109	185800	19516	9213	3	7.66

Asia : 8001 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

g/cmq ft=4300 kg/cmq. <i>Verified</i>														
	N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
	kg	kg*m	kg*m	kg	kg*m	kg*m								
-4113	-1678	-496	211298	20492	9673	18	30	0.948	0.927	--	0.884	0.343	0.530	0.571

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4113	1482	170	190741	19516	9213	(12+13)-I-4	8.62
1	Z	4113	889	283	186489	19516	9213	(12+13)-I-4	10.2

Asia : 8001 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

g/cmq ft=4300 kg/cmq. <i>Verified</i>													
N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5041	-2729	618	211298	20492	9673	18	30	0.948	0.927	--	0.847	0.537	0.508 0.895

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5041	2312	332	190741	19516	9213	8	5.53
1	Z	5041	1387	553	186489	19516	9213	8	6.32

Asia : 8001 [0 , 0]

Sez. G: HE 240 A L=151.4 cm Ln1=151.4 cm Ln2=151.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

g/cmq ft=4300 kg/cmq. <i>Verificato</i>													
N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
4296	-3688	693	211298	20492	9673	15	25	0.965	0.950	--	0.894	0.584	0.536 0.974

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4296	3296	405	194114	19516	9213	8	4.26
1	Z	4296	1978	675	191143	19516	9213	8	5.08

Asia : 8001 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione γM=1.05 fyk/γM=2619

g/cmq ft=4300 kg/cmq. <i>Verified</i>													
N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2654	-3757	687	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.540	0.601
													0.900

Cls	Dir	N	Mvseq	Mzeq	NRk	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2654	3762	371	194565	19516	9213	8	4.05
1	Z	2654	2257	618	191772	19516	9213	8	5.09

Asia : 8001 [0 , 75]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2137	-3733	594	211298	20492	9673	13	22	0.976	0.965	--	0.971	0.472	0.583
													0.786

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2137	3625	280	196336	19516	9213	8					4.40
1	Z	2137	2175	467	194255	19516	9213	8					5.78

Asia : 8001 [75 , 76]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1726	-3440	356	211298	20492	9673	12	20	0.983	0.976	--	0.922	0.455	0.553
													0.758

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1726	3173	162	197912	19516	9213	8					5.29
1	Z	1726	1904	270	196483	19516	9213	8					7.37

Asia : 8001 [76 , 0]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-520	-2900	208	211298	20492	9673	11	19	0.990	0.985	--	0.876	0.404	0.525
													0.673

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	520	2539	84	199176	19516	9213	9					7.05
1	Z	520	1523	140	198282	19516	9213	9					10.4

Asia : 8001 [0 , 0]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4917	1815	-68	211298	20492	9673	11	18	0.993	0.990	--	0.822	0.239	0.493
													0.398

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	4917	1492	16	199872	19516	9213	(12+13)-VIII-1	9.73				
1	Z	4917	895	27	199276	19516	9213	(12+13)-VIII-1	13.6				

Asia : 8001 [0 , 328]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2066	2820	-51	211298	20492	9673	11	19	0.990	0.986	--	0.605	0.375	0.363
													0.626

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2066	1707	19	199294	19516	9213	(12+13)-I-2	10.0				
1	Z	2066	1024	32	198449	19516	9213	(12+13)-I-2	15.1				

Asia : 8002 [103 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6555	4206	-176	211298	20492	9673	18	30	0.945	0.923	--	0.695	0.458	0.417
													0.763

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	6555	2921	81	190233	19516	9213	3					5.18
1	Z	6555	1753	134	185796	19516	9213	3					7.16

Asia : 8002 [0 , 0]

Sez. G: HE 240 A L=177.7 cm Ln1=177.7 cm Ln2=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1253	2285	257	211298	20492	9673	18	30	0.948	0.927	--	0.837	0.240	0.502
													0.400

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1253	1913	62	190737	19516	9213	(12+13)-I-1	8.99				
1	Z	1253	1148	103	186484	19516	9213	(12+13)-I-1	13.0				

Asia : 8002 [0 , 0]

Sez. G: HE 240 A L=177.7 cm Ln1=177.7 cm Ln2=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4090	-2843	602	211298	20492	9673	18	30	0.948	0.927	--	0.839	0.541	0.503
													0.902

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	4090	2285	326	190737	19516	9213	8					5.59
1	Z	4090	1431	543	186484	19516	9213	8					6.49

Asia : 8002 [0 , 0]

Sez. G: HE 240 A L=151.4 cm Ln1=151.4 cm Ln2=151.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3520	-3710	674	211298	20492	9673	15	25	0.965	0.950	--	0.904	0.587	0.542
													0.978

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	3320	3353	396	194110	19516	9213	8					4.31
1	Z	3320	2012	660	191137	19516	9213	8					5.21

Asia : 8002 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2732	-3858	670	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.539	0.601
													0.899

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2732	3862	562	194560	19516	9213	8					3.98
1	Z	2732	2317	603	191766	19516	9213	8					5.04

Asia : 8002 [0 , 71]

Sez. G: HE 240 A L=134.5 cm Ln1=134.5 cm Ln2=134.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2198	-3825	578	211298	20492	9673	13	22	0.976	0.965	--	0.970	0.480	0.582
													0.799

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2198	3709	277	196332	19516	9213	8	4.32
1	Z	2198	2225	462	194248	19516	9213	8	5.70

Asta : 8002 [71 , 72]

Sez. G: HE 240 A L=122.7 cm Ln1=122.7 cm Ln2=122.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1813	-3513	365	211298	20492	9673	12	20	0.983	0.976	--	0.920	0.454	0.552
													0.756

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1813	3232	166	197907	19516	9213	8	5.19
1	Z	1813	1939	276	196475	19516	9213	8	7.22

Asta : 8002 [72 , 397]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-705	-2869	205	211298	20492	9673	11	19	0.990	0.985	--	0.873	0.404	0.524
													0.674

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	705	2505	83	199170	19516	9213	9	7.10
1	Z	705	1503	138	198273	19516	9213	9	10.5

Asta : 8002 [397 , 398]

Sez. G: HE 240 A L=108.2 cm Ln1=108.2 cm Ln2=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-841	-1983	58	211298	20492	9673	11	18	0.993	0.990	--	0.758	0.501	0.455
													0.834

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	841	1503	29	199866	19516	9213	9	11.9
1	Z	841	902	48	199267	19516	9213	9	18.0

Asta : 8002 [398 , 329]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2675	1653	-8	211298	20492	9673	11	19	0.990	0.986	--	0.860	0.240	0.516
													0.399

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2675	1422	2	199288	19516	9213	10	11.6
1	Z	2675	853	3	198441	19516	9213	10	17.4

Asta : 8003 [104 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6912	4125	-144	211298	20492	9673	18	30	0.945	0.923	--	0.695	0.503	0.417
													0.838

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6912	2867	73	190243	19516	9213	3	5.23
1	Z	6912	1720	121	185809	19516	9213	3	7.22

913

Asta : 8003 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5185	-1733	448	211298	20492	9673	18	30	0.948	0.927	--	0.602	0.361	0.601

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5185	1044	162	190747	19516	9213	8	10.2
1	Z	5185	626	269	186498	19516	9213	8	11.2

Asta : 8003 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4107	-2810	596	211298	20492	9673	18	30	0.948	0.927	--	0.602	0.361	0.601

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg*m	kg*m		
1	Y	4107	1691	215	190747	19516	9213	8	7.60
1	Z	4107	1015	358	186498	19516	9213	8	8.86

Asta : 8003 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3367	-3684	668	211298	20492	9673	15	25	0.965	0.950	--	0.902	0.585	0.541
													0.975

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3367	3324	391	194122	19516	9213	8	4.35
1	Z	3367	1994	651	191154	19516	9213	8	5.25

Asta : 8003 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2771	-3839	658	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.538	0.601
													0.896

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2771	3843	354	194573	19516	9213	8	4.01
1	Z	2771	2306	590	191783	19516	9213	8	5.09

Asta : 8003 [0 , 65]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2231	-3808	561	211298	20492	9673	13	22	0.976	0.965	--	0.971	0.482	0.803

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2231	3695	270	196345	19516	9213	8	4.35
1	Z	2231	2217	451	194268	19516	9213	8	5.75

Asta : 8003 [65 , 66]

Sez. G: HE 240 A L=122.5 cm Ln1=122.5 cm Ln2=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

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N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1844	-3506	360	211298	20492	9673	12	20	0.984	0.976	--	0.921	0.456	0.552
0.760													
Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	1844	3228	164	197922	19516	9213				8		5.19
1	Z	1844	1937	274	196497	19516	9213				8		7.23

Asia : 8003 [66 , 391]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-747	-2858	205	211298	20492	9673	11	19	0.990	0.985	--	0.874	0.410	0.524
0.684													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	747	2498	84	199187	19516	9213				9		7.10
1	Z	747	1499	140	198297	19516	9213				9		10.4

Asia : 8003 [391 , 392]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-851	-1979	64	211298	20492	9673	11	18	0.993	0.990	--	0.760	0.495	0.456
0.826													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	851	1504	32	199883	19516	9213				9		11.8
1	Z	851	903	53	199293	19516	9213				9		17.8

Asia : 8003 [392 , 330]

Sez. G: HE 240 A L=112.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2604	1699	7	211298	20492	9673	11	19	0.990	0.986	--	0.848	0.240	0.509
0.399													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	2604	1441	2	199305	19516	9213				10		11.5
1	Z	2604	865	3	198465	19516	9213				10		17.3

Asia : 8004 [105 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4658	4268	-87	211298	20492	9673	18	30	0.945	0.923	--	0.698	0.532	0.419
0.887													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	6658	2981	46	190242	19516	9213				3		5.19
1	Z	6658	1789	77	185808	19516	9213				3		7.36

Asia : 8004 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1637	1940	-294	211298	20492	9673	18	30	0.948	0.927	--	0.818	0.397	0.491
0.661													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	1637	1387	117	190746	19516	9213				(12+13)+2		9.75
1	Z	1637	952	194	186497	19516	9213				(12+13)+2		12.7

Asia : 8004 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4175	-2832	584	211298	20492	9673	18	30	0.948	0.927	--	0.837	0.550	0.502
0.917													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	4175	2369	321	190746	19516	9213				8		5.61
1	Z	4175	1421	535	186497	19516	9213				8		6.52

Asia : 8004 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3387	-3720	654	211298	20492	9673	15	25	0.965	0.950	--	0.901	0.584	0.541
0.973													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	3387	3353	382	194120	19516	9213				8		4.33
1	Z	3387	2012	636	191152	19516	9213				8		5.27

Asia : 8004 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2780	-3881	641	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.536	0.601
0.893													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	2780	3886	343	194571	19516	9213				8		3.99
1	Z	2780	2331	572	191781	19516	9213				8		5.10

Asia : 8004 [0 , 77]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2227	-3850	541	211298	20492	9673	13	22	0.976	0.965	--	0.971	0.483	0.583
0.805													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	2227	3739	261	196344	19516	9213				8		4.32
1	Z	2227	2243	435	194266	19516	9213				8		5.76

Asia : 8004 [77 , 78]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619
kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1837	-3551	351	211298	20492	9673	12	20	0.984	0.976	--	0.920	0.456	0.552
0.761													

Clis	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd				Comb.		SF
kg	kg	kg	kg*m	kg*m	kg	kg	kg*m						
1	Y	1837	3268	160	197921	19516	9213				8		5.15
1	Z	1837	1961	267	196494	19516	9213				8		7.21

Asia : 8004 [78 , 0]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-753	-2871	203	211298	20492	9673	11	19	0.990	0.985	--	0.873	0.404	0.524

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	753	2306	82	199185	19516	9213	9					7.09
1	Z	753	1503	136	198295	19516	9213	9					10.5

Asia : 8004 [0 , 0]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-898	-1983	57	211298	20492	9673	11	18	0.993	0.990	--	0.757	0.513	0.454
													0.854

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	898	1502	29	199881	19516	9213	9					11.8
1	Z	898	901	48	199290	19516	9213	9					17.9

Asia : 8004 [0 , 331]

Sez. G: HE 240 A L=112.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2619	1783	-7	211298	20492	9673	11	19	0.990	0.986	--	0.842	0.240	0.505
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2619	1502	2	199303	19516	9213	10					11.1
1	Z	2619	901	3	198462	19516	9213	10					16.8

Asia : 8005 [106 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6712	4330	-71	211298	20492	9673	18	30	0.945	0.923	--	0.697	0.596	0.418
													0.994

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	6712	3019	42	190239	19516	9213	3					5.14
1	Z	6712	1811	71	185804	19516	9213	3					7.32

Asia : 8005 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1650	1964	-251	211298	20492	9673	18	30	0.948	0.927	--	0.822	0.393	0.493
													0.655

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1650	1613	99	190743	19516	9213	(12+13)+2					9.80
1	Z	1650	968	164	186492	19516	9213	(12+13)+2					13.1

Asia : 8005 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4210	-2859	557	211298	20492	9673	18	30	0.948	0.927	--	0.602	0.361	0.601

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	4210	1721	201	190743	19516	9213	8					7.57
1	Z	4210	1033	335	186492	19516	9213	8					8.94

Asia : 8005 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3467	-3741	624	211298	20492	9673	15	25	0.965	0.950	--	0.903	0.585	0.542
													0.975

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	3467	3377	365	194117	19516	9213	8					4.34
1	Z	3467	2026	609	191147	19516	9213	8					5.32

Asia : 8005 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2868	-3880	614	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.535	0.601
													0.891

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2868	3885	329	194568	19516	9213	8					4.01
1	Z	2868	2331	548	191776	19516	9213	8					5.16

Asia : 8005 [0 , 69]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2316	-3846	516	211298	20492	9673	13	22	0.976	0.965	--	0.969	0.484	0.582
													0.806

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	2316	3727	250	196340	19516	9213	8					4.35
1	Z	2316	2236	416	194260	19516	9213	8					5.82

Asia : 8005 [69 , 70]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1927	-3528	339	211298	20492	9673	12	20	0.984	0.976	--	0.919	0.459	0.551
													0.764

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						SF
1	Y	1927	3241	155	197916	19516	9213	8					5.19
1	Z	1927	1945	259	196488	19516	9213	8					7.27

Asia : 8005 [70 , 395]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1752	-2810	201	211298	20492	9673	11	19	0.990	0.985	--	0.848	0.402	0.509
													0.670

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1752	2384	81	199180	19516	9213	8	7.16
1	Z	1752	1430	135	198287	19516	9213	8	10.3

Asta : 8005 [395 , 396]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	18	0.993	0.990	--	0.759	0.529	0.455
-988	-1951	54	211298	20492	9673	11	18	0.993	0.990	--	0.759	0.529	0.455

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	988	1480	29	199876	19516	9213	9	11.9
1	Z	988	888	48	199282	19516	9213	9	18.0

Asta : 8005 [396 , 332]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	19	0.990	0.986	--	0.842	0.240	0.505
-2640	1803	-6	211298	20492	9673	11	19	0.990	0.986	--	0.842	0.240	0.505

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2640	1518	1	199298	19516	9213	10	11.0
1	Z	2640	911	2	198455	19516	9213	10	16.6

Asta : 8006 [107 , 168]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.945	0.923	--	0.694	0.536	0.416
-6423	4227	-25	211298	20492	9673	18	30	0.945	0.923	--	0.694	0.536	0.416

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6423	2934	13	190241	19516	9213	3	5.39
1	Z	6423	1760	22	185806	19516	9213	3	7.86

Asta : 8006 [168 , 169]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.948	0.927	--	0.602	0.361	0.361
-4446	-1805	474	211298	20492	9673	18	30	0.948	0.927	--	0.602	0.361	0.361

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4446	1087	171	190745	19516	9213	8	10.3
1	Z	4446	652	285	186495	19516	9213	8	11.3

Asta : 8006 [169 , 170]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.948	0.927	--	0.601	0.360	0.361
-2775	-2934	586	211298	20492	9673	18	30	0.948	0.927	--	0.601	0.360	0.361

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2775	1764	211	190745	19516	9213	8	7.82
1	Z	2775	1058	352	186495	19516	9213	8	9.32

919

Asta : 8006 [170 , 171]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	15	25	0.965	0.950	--	0.917	0.583	0.550
-1992	-3663	655	211298	20492	9673	15	25	0.965	0.950	--	0.917	0.583	0.550

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1992	3358	382	194119	19516	9213	8	4.47
1	Z	1992	2015	637	191151	19516	9213	8	5.47

Asta : 8006 [171 , 172]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	15	25	0.967	0.953	--	1.001	0.533	0.600
-2249	-3860	631	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.533	0.600

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2249	3863	336	194570	19516	9213	8	4.07
1	Z	2249	2318	560	191780	19516	9213	8	5.23

Asta : 8006 [172 , 33]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	13	22	0.976	0.965	--	0.955	0.506	0.573
-1691	-3811	520	211298	20492	9673	13	22	0.976	0.965	--	0.955	0.506	0.573

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1691	3639	263	196343	19516	9213	8	4.47
1	Z	1691	2183	438	194264	19516	9213	8	5.95

Asta : 8006 [33 , 34]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	12	20	0.984	0.976	--	0.912	0.459	0.547
-2051	-3448	375	211298	20492	9673	12	20	0.984	0.976	--	0.912	0.459	0.547

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2051	3143	172	197919	19516	9213	8	5.26
1	Z	2051	1886	287	196493	19516	9213	8	7.24

Asta : 8006 [34 , 359]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	19	0.990	0.985	--	0.839	0.432	0.504
-1885	-2685	216	211298	20492	9673	11	19	0.990	0.985	--	0.839	0.432	0.504

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1885	2254	94	199184	19516	9213	8	7.40
1	Z	1885	1352	156	198292	19516	9213	8	10.4

Asta : 8006 [359 , 360]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cm² ft=4300 kg/cm² **Verificato**

920

Clis	Dir	Asia : 8006 [360, 333]										SF		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
-4860	1689	-74	211298	20492	9673	11	18	0.993	0.990	--	0.914	0.239	0.548	0.398
Clis	Dir	Asia : 8006 [360, 333]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	4860	1543	18	199880	19516	9213	(12+13)+VIII-4					9.50	
1	Z	4860	926	30	199288	19516	9213	(12+13)+VIII-4					13.3	

Asia : 8006 [360, 333]

Sez. G: HE 240 A L=112.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	Asia : 8007 [183, 184]										SF		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
-2412	1860	-7	211298	20492	9673	11	19	0.990	0.986	--	0.821	0.244	0.493	0.407

Clis	Dir	Asia : 8007 [183, 184]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	2412	1527	2	199301	19516	9213	10					11.0	
1	Z	2412	916	3	198460	19516	9213	10					16.8	

Asia : 8007 [108, 183]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	Asia : 8007 [183, 184]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
-8036	4319	-35	211298	20492	9673	18	30	0.945	0.923	--	0.700	0.306	0.420	0.510

Clis	Dir	Asia : 8007 [183, 184]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	8036	3023	11	190239	19516	9213	3					5.04	
1	Z	8036	1814	18	185803	19516	9213	3					7.24	

Asia : 8007 [183, 184]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	Asia : 8007 [184, 185]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
-6544	-1636	470	211298	20492	9673	18	30	0.948	0.927	--	0.491	0.437	0.295	0.728

Clis	Dir	Asia : 8007 [184, 185]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	6544	804	205	190743	19516	9213	8					10.2	
1	Z	6544	482	342	186492	19516	9213	8					10.3	

Asia : 8007 [184, 185]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	Asia : 8007 [185, 186]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
-5180	-2661	567	211298	20492	9673	18	30	0.948	0.927	--	0.832	0.574	0.499	0.957

Clis	Dir	Asia : 8007 [185, 186]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	5180	2214	325	190743	19516	9213	8					5.69	
1	Z	5180	1328	542	186492	19516	9213	8					6.46	

Asia : 8007 [185, 186]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	Asia : 8007 [185, 186]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
-4407	-3714	637	211298	20492	9673	15	25	0.965	0.950	--	0.884	0.567	0.530	0.946

Clis	Dir	Asia : 8007 [186, 187]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	4407	3283	361	194116	19516	9213	8					4.34	
1	Z	4407	1970	602	191147	19516	9213	8					5.28	

Asia : 8007 [186, 187]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	Asia : 8007 [187, 39]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
-2637	-3918	592	211298	20492	9673	15	25	0.967	0.953	--	0.964	0.532	0.578	0.887

Clis	Dir	Asia : 8007 [187, 39]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	2637	3775	315	194567	19516	9213	8					4.15	
1	Z	2637	2265	525	191776	19516	9213	8					5.35	

Asia : 8007 [187, 39]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	Asia : 8007 [187, 39]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
-2072	-3904	491	211298	20492	9673	13	22	0.976	0.965	--	1.001	0.483	0.600	0.805

Clis	Dir	Asia : 8007 [187, 39]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	2072	3906	237	196339	19516	9213	8					4.23	
1	Z	2072	2344	396	194259	19516	9213	8					5.76	

Asia : 8007 [139, 40]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	Asia : 8007 [139, 40]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
-1229	-3698	326	211298	20492	9673	12	20	0.983	0.976	--	0.935	0.466	0.561	0.776

Clis	Dir	Asia : 8007 [140, 365]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg*m	kg*m	kg	kg*m	kg*m							
1	Y	1229	3457	152	197916	19516	9213	8					5.00	
1	Z	1229	2074	253	196487	19516	9213	8					7.14	

Asia : 8007 [140, 365]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619 kg/cmq ft=4300 kg/cmq;**Verificato**

Clis	Dir	Asia : 8007 [140, 365]										Comb.		
		N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzz
		kg	kg·m	kg·m	kg	kg·m	kg·m							
		-176	-3123	205	211298	20492	9673	11	19	0.990	0.985	--	0.882	0.436
													0.529	0.727

Asia : 8007 [366 , 334]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1831	2791	-3	211298	20492	9673	11	19	0.990	0.986	--	0.711	0.240	0.427 0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1831	1985	1	199297	19516	9213	(12+13)+2	9.01
1	Z	1831	1191	1	198455	19516	9213	(12+13)+2	14.2

Asia : 8008 [109 , 163]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6537	4031	-55	211298	20492	9673	18	30	0.945	0.923	--	0.694	0.247	0.416 0.412

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6537	2798	14	190244	19516	9213	3	5.58
1	Z	6537	1679	23	185811	19516	9213	3	8.09

Asia : 8008 [163 , 164]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4762	-1662	510	211298	20492	9673	18	30	0.948	0.927	--	0.515	0.432	0.309 0.720

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4762	856	220	190749	19516	9213	8	10.8
1	Z	4762	514	367	186500	19516	9213	8	10.9

Asia : 8008 [164 , 165]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4073	-2744	527	211298	20492	9673	18	30	0.948	0.927	--	0.840	0.596	0.504 0.994

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4073	2305	314	190749	19516	9213	8	5.76
1	Z	4073	1383	524	186500	19516	9213	8	6.69

Asia : 8008 [165 , 166]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3275	-3619	590	211298	20492	9673	15	25	0.965	0.950	--	0.900	0.583	0.540 0.972

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3275	3258	344	194123	19516	9213	8	4.52
1	Z	3275	1955	573	191156	19516	9213	8	5.57

Asia : 8008 [166 , 167]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2665	-3802	576	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.528	0.601 0.880

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2665	3806	304	194574	19516	9213	8	4.14
1	Z	2665	2284	507	191785	19516	9213	8	5.38

Asia : 8008 [167 , 31]

Sez. G: HE 240 A L=134.3 cm Ln1=134.3 cm Ln2=134.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2111	-3774	466	211298	20492	9673	13	22	0.976	0.965	--	0.974	0.491	0.585 0.819

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2111	3678	229	196347	19516	9213	8	4.46
1	Z	2111	2207	381	194271	19516	9213	8	6.05

Asia : 8008 [31 , 32]

Sez. G: HE 240 A L=122.5 cm Ln1=122.5 cm Ln2=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1718	-3512	524	211298	20492	9673	12	20	0.984	0.976	--	0.924	0.461	0.555 0.769

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1718	3246	149	197924	19516	9213	8	5.23
1	Z	1718	1947	249	196500	19516	9213	8	7.38

Asia : 8008 [32 , 357]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1552	-2846	197	211298	20492	9673	11	19	0.990	0.985	--	0.855	0.401	0.513 0.669

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1552	2432	79	199190	19516	9213	8	7.09
1	Z	1552	1459	152	198301	19516	9213	8	10.3

Asia : 8008 [357 , 358]

Sez. G: HE 240 A L=108.0 cm Ln1=108.0 cm Ln2=108.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-810	-2013	51	211298	20492	9673	11	18	0.993	0.990	--	0.765	0.562	0.459 0.936

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	810	1539	28	199886	19516	9213	9	11.6
1	Z	810	924	47	199296	19516	9213	9	17.7

Asia : 8008 [358 , 335]

Sez. G: HE 240 A L=112.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2548	1684	-4	211298	20492	9673	11	19	0.990	0.986	--	0.843	0.240	0.506 0.399

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2548	1420	1	199307	19516	9213	10	11.7
1	Z	2548	852	1	198468	19516	9213	10	17.7

Asta : 8009 [110 , 178]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.945	0.923	--	0.693	0.359	0.416
-4509	4068	90	211298	20492	9673	18	30	0.945	0.923	--	0.693	0.359	0.416
													0.598

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6509	2819	32	190239	19516	9213	3	5.49
1	Z	6509	1692	54	185804	19516	9213	3	7.84

Asta : 8009 [178 , 179]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.948	0.927	--	0.518	0.459	0.311
-4760	-1685	533	211298	20492	9673	18	30	0.948	0.927	--	0.518	0.459	0.311
													0.766

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4760	873	245	190743	19516	9213	8	10.4
1	Z	4760	524	408	186492	19516	9213	8	10.3

Asta : 8009 [179 , 180]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.948	0.927	--	0.841	0.600	0.505
-4078	-2768	541	211298	20492	9673	18	30	0.948	0.927	--	0.841	0.600	0.505
													1.000

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4078	2329	325	190743	19516	9213	8	5.68
1	Z	4078	1398	542	186492	19516	9213	8	6.57

Asta : 8009 [180 , 181]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	15	25	0.965	0.950	--	0.902	0.575	0.541
-3293	-3629	606	211298	20492	9673	15	25	0.965	0.950	--	0.902	0.575	0.541
													0.958

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3293	3274	348	194117	19516	9213	8	4.49
1	Z	3293	1964	581	191147	19516	9213	8	5.53

Asta : 8009 [181 , 182]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	15	25	0.967	0.953	--	1.001	0.525	0.601
-2692	-3793	570	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.525	0.601
													0.876

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2692	3797	299	194568	19516	9213	8	4.15
1	Z	2692	2278	499	191776	19516	9213	8	5.41

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Asta : 8009 [182 , 37]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	13	22	0.976	0.965	--	0.973	0.493	0.584
-2142	-3763	453	211298	20492	9673	13	22	0.976	0.965	--	0.973	0.493	0.584
													0.822

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2142	3661	223	196340	19516	9213	8	4.49
1	Z	2142	2197	372	194260	19516	9213	8	6.10

Asta : 8009 [37 , 38]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	12	20	0.984	0.976	--	0.923	0.462	0.554
-1751	-3487	319	211298	20492	9673	12	20	0.984	0.976	--	0.923	0.462	0.554
													0.770

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1751	3219	147	197916	19516	9213	8	5.27
1	Z	1751	1932	246	196488	19516	9213	8	7.43

Asta : 8009 [38 , 363]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	19	0.990	0.985	--	0.876	0.401	0.526
-709	-2844	195	211298	20492	9673	11	19	0.990	0.985	--	0.876	0.401	0.526
													0.669

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	709	2492	78	199180	19516	9213	9	7.15
1	Z	709	1495	131	198287	19516	9213	9	10.6

Asta : 8009 [363 , 364]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	18	0.993	0.990	--	0.765	0.558	0.459
-856	-1989	51	211298	20492	9673	11	18	0.993	0.990	--	0.765	0.558	0.459
													0.931

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	856	1523	29	199876	19516	9213	9	11.7
1	Z	856	914	48	199282	19516	9213	9	17.8

Asta : 8009 [364 , 336]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	19	0.990	0.986	--	0.843	0.240	0.506
-2533	1692	-3	211298	20492	9673	11	19	0.990	0.986	--	0.843	0.240	0.506
													0.399

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2533	1426	1	199298	19516	9213	10	11.6
1	Z	2533	856	1	198455	19516	9213	10	17.6

Asta : 8010 [111 , 153]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

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N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m
-4915	4130	107	211298	20492	9673	18	30	0.945	0.923	--	0.693	0.344	0.416
SF													
Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	6915	2862	37	190239	19516	9213	3					
1	Z	6915	1717	62	185804	19516	9213	3					

Asia : 8010 [153 , 154]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg	kg*m	kg
-5235	-1700	535	211298	20492	9673	18	30	0.948	0.927	--	0.521	0.471	0.312
0.785													

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	5235	885	252	190744	19516	9213	8					
1	Z	5235	531	420	186493	19516	9213	8					

Asia : 8010 [154 , 155]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg	kg*m	kg
-3956	-2746	553	211298	20492	9673	18	30	0.948	0.927	--	0.836	0.592	0.501
0.986													

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	3956	2294	327	190744	19516	9213	8					
1	Z	3956	1377	545	186493	19516	9213	8					

Asia : 8010 [155 , 156]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg	kg*m	kg
-3173	-3617	594	211298	20492	9673	15	25	0.965	0.950	--	0.901	0.575	0.540
0.958													

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	3173	3258	342	194117	19516	9213	8					
1	Z	3173	1955	569	191148	19516	9213	8					

Asia : 8010 [156 , 157]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg	kg*m	kg
-2564	-3809	559	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.523	0.601
0.872													

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2564	3813	293	194568	19516	9213	8					
1	Z	2564	2288	488	191777	19516	9213	8					

Asia : 8010 [157 , 271]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg	kg*m	kg
-2011	-3782	439	211298	20492	9673	13	22	0.976	0.965	--	0.975	0.496	0.585
0.827													

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2011	3689	218	196340	19516	9213	8					
1	Z	2011	2214	363	194261	19516	9213	8					

Asia : 8010 [27 , 28]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg	kg*m	kg
-1620	-3529	316	211298	20492	9673	12	20	0.984	0.976	--	0.925	0.464	0.555
0.773													

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	1620	3264	147	197917	19516	9213	8					
1	Z	1620	1959	244	196489	19516	9213	8					

Asia : 8010 [28 , 353]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg	kg*m	kg
-1459	-2867	197	211298	20492	9673	11	19	0.990	0.985	--	0.855	0.407	0.513
0.679													

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	1459	2452	80	199181	19516	9213	8					
1	Z	1459	1471	133	198289	19516	9213	8					

Asia : 8010 [353 , 354]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg	kg*m	kg
-716	-2017	54	211298	20492	9673	11	18	0.993	0.990	--	0.763	0.559	0.458
0.932													

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	716	1539	30	199877	19516	9213	9					
1	Z	716	924	50	199284	19516	9213	9					

Asia : 8010 [354 , 337]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg*m	kg*m	kg*m	kg	kg*m	kg
-2400	1776	-2	211298	20492	9673	11	19	0.990	0.986	--	0.833	0.240	0.500
0.399													

Cls	Dir	N	Mvseq	Mzseq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2400	1479	1	199299	19516	9213	10					
1	Z	2400	887	1	198456	19516	9213	10					

Asia : 8011 [112 , 188]

Asia : 8011 [188 , 189]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4722	-1706	569	211298	20492	9673	18	30	0.948	0.927	--	0.537	0.471	0.322
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	4722	917	268	190743	19516	9213	8					
1	Z	4722	550	447	186492	19516	9213	8					

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	4722	917	268	190743	19516	9213	8					
1	Z	4722	550	447	186492	19516	9213	8					

Asia : 8011 [189 , 190]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4049	-2750	575	211298	20492	9673	18	30	0.948	0.927	--	0.846	0.571	0.508
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	4049	2328	328	190743	19516	9213	8					
1	Z	4049	1397	547	186492	19516	9213	8					

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	4049	2328	328	190743	19516	9213	8					
1	Z	4049	1397	547	186492	19516	9213	8					

Asia : 8011 [190 , 191]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3281	-3580	562	211298	20492	9673	15	25	0.965	0.950	--	0.904	0.576	0.543
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	3281	3238	324	194116	19516	9213	8					
1	Z	3281	1943	540	191147	19516	9213	8					

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	3281	3238	324	194116	19516	9213	8					
1	Z	3281	1943	540	191147	19516	9213	8					

Asia : 8011 [191 , 192]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2685	-3732	531	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.520	0.601
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2685	3737	276	194568	19516	9213	8					
1	Z	2685	2242	460	191776	19516	9213	8					

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2685	3737	276	194568	19516	9213	8					
1	Z	2685	2242	460	191776	19516	9213	8					

Asia : 8011 [192 , 41]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2148	-3702	408	211298	20492	9673	13	22	0.976	0.965	--	0.972	0.499	0.583
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2148	3599	204	196340	19516	9213	8					
1	Z	2148	2159	340	194260	19516	9213	8					

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2148	3599	204	196340	19516	9213	8					
1	Z	2148	2159	340	194260	19516	9213	8					

Asia : 8011 [41 , 42]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

kg/cmq	ft=4300 kg/cmq	<i>Verificato</i>
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N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1767	-3424	302	211298	20492	9673	12	20	0.984	0.976	--	0.923	0.465	0.554
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	1767	3162	140	197916	19516	9213	8					
1	Z	1767	1897	234	196488	19516	9213	8					

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	1767	3162	140	197916	19516	9213	8					
1	Z	1767	1897	234	196488	19516	9213	8					

Asia : 8011 [42 , 367]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-747	-2796	191	211298	20492	9673	11	19	0.990	0.985	--	0.878	0.399	0.527
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	747	2454	76	199180	19516	9213	9					
1	Z	747	1472	127	198287	19516	9213	9					

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	747	2454	76	199180	19516	9213	9					
1	Z	747	1472	127	198287	19516	9213	9					

Asia : 8011 [367 , 368]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-903	-1966	47	211298	20492	9673	11	18	0.993	0.990	--	0.772	0.595	0.463
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m							

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4781	973	286	190738	19516	9213	8	9.44
1	Z	4781	584	476	186486	19516	9213	8	9.33

Asta : 8012 [194 , 195]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-2814	-2872	597	211298	20492	9673	18	30	0.948	0.927	--	0.827	0.576	0.496

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2814	2375	344	190738	19516	9213	8	5.75
1	Z	2814	1425	573	186486	19516	9213	8	6.65

Asta : 8012 [195 , 196]

Sez. G: HE 240 A L=151.4 cm Ln1=151.4 cm Ln2=151.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-2005	-3648	601	211298	20492	9673	15	25	0.965	0.950	--	0.911	0.567	0.547

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2005	3324	341	194111	19516	9213	8	4.59
1	Z	2005	1995	568	191139	19516	9213	8	5.74

Asta : 8012 [196 , 197]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-1761	-3807	549	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.519	0.600

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1761	3809	285	194562	19516	9213	8	4.25
1	Z	1761	2285	475	191768	19516	9213	8	5.62

Asta : 8012 [197 , 43]

Sez. G: HE 240 A L=134.5 cm Ln1=134.5 cm Ln2=134.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-1211	-3767	418	211298	20492	9673	13	22	0.976	0.965	--	0.956	0.514	0.574

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1211	3601	215	196333	19516	9213	8	4.67
1	Z	1211	2160	358	194251	19516	9213	8	6.42

Asta : 8012 [43 , 44]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-1835	-3450	329	211298	20492	9673	12	20	0.983	0.976	--	0.906	0.469	0.544

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1835	3127	154	197909	19516	9213	8	5.37
1	Z	1835	1876	257	196477	19516	9213	8	7.50

931

Asta : 8012 [44 , 369]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-1693	-2644	209	211298	20492	9673	11	19	0.990	0.985	--	0.831	0.447	0.499

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1693	2198	93	199172	19516	9213	8	7.62
1	Z	1693	1319	156	198276	19516	9213	8	10.8

Asta : 8012 [369 , 370]

Sez. G: HE 240 A L=108.2 cm Ln1=108.2 cm Ln2=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-4672	1790	85	211298	20492	9673	11	18	0.993	0.990	--	0.887	0.239	0.532

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4672	1587	20	199868	19516	9213	(12+13)-VIII-4	9.35
1	Z	4672	952	34	199270	19516	9213	(12+13)-VIII-4	13.2

Asta : 8012 [370 , 339]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-2407	1704	0	211298	20492	9673	11	19	0.990	0.986	--	0.838	0.577	0.503

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2407	1427	0	199290	19516	9213	10	11.7
1	Z	2407	856	0	198443	19516	9213	10	17.8

Asta : 8013 [114 , 158]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-7421	3682	210	211298	20492	9673	18	30	0.945	0.923	--	0.604	0.361	0.362

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	7421	2222	76	190241	19516	9213	3	6.21
1	Z	7421	1333	127	185806	19516	9213	3	8.19

Asta : 8013 [158 , 159]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-6079	-1673	589	211298	20492	9673	18	30	0.948	0.927	--	0.528	0.502	0.317

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6079	884	296	190745	19516	9213	8	9.15
1	Z	6079	530	493	186495	19516	9213	8	8.83

Asta : 8013 [159 , 160]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

932

Asia : 8014 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3130	-3579	539	211298	20492	9673	15	25	0.965	0.950	--	0.900	0.572	0.540
0.954													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3130	3223	309	194118	19516	9213	8	4.66
	Z	3130	1934	514	191148	19516	9213	8	5.84

Asia : 8014 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2534	-3762	500	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.510	0.601
0.850													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2534	3766	255	194569	19516	9213	8	4.28
	Z	2534	2260	426	191777	19516	9213	8	5.71

Asia : 8014 [0 , 47]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1985	-3735	361	211298	20492	9673	13	22	0.976	0.965	--	0.975	0.512	0.585
0.853													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1985	3643	185	196341	19516	9213	8	4.61
	Z	1985	2186	308	194261	19516	9213	8	6.42

Asia : 8014 [47 , 48]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1600	-3484	290	211298	20492	9673	12	20	0.984	0.976	--	0.926	0.467	0.555
0.779													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1600	3224	136	197917	19516	9213	8	5.32
	Z	1600	1935	226	196490	19516	9213	8	7.59

Asia : 8014 [48 , 373]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-589	-2869	187	211298	20492	9673	11	19	0.990	0.985	--	0.878	0.396	0.527
0.660													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	589	2519	74	199182	19516	9213	9	7.14
	Z	589	1512	124	198289	19516	9213	9	10.7

Asia : 8014 [373 , 374]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3122	-3609	547	211298	20492	9673	15	25	0.965	0.950	--	0.902	0.566	0.541
0.943													

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-737	-2020	51	211298	20492	9673	11	18	0.993	0.990	--	0.768	0.557	0.461
0.928													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	737	1550	28	199878	19516	9213	9	11.6
	Z	737	930	47	199284	19516	9213	9	17.7

Asia : 8014 [374 , 341]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2455	1625	1	211298	20492	9673	11	19	0.990	0.986	--	0.845	0.240	0.507
0.399													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2455	1373	0	199299	19516	9213	10	12.1
	Z	2455	824	1	198457	19516	9213	10	18.3

Asia : 8015 [116 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6946	4073	282	211298	20492	9673	18	30	0.945	0.923	--	0.690	0.396	0.414
0.659													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6946	2812	112	190243	19516	9213	3	5.19
	Z	6946	1687	186	185810	19516	9213	3	6.94

Asia : 8015 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5258	-1729	614	211298	20492	9673	18	30	0.948	0.927	--	0.602	0.361	0.361
0.601													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5258	1042	222	190748	19516	9213	8	9.53
	Z	5258	625	369	186499	19516	9213	8	9.97

Asia : 8015 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3864	-2752	639	211298	20492	9673	18	30	0.948	0.927	--	0.602	0.361	0.361
0.601													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3864	1656	230	190748	19516	9213	8	7.69
	Z	3864	994	384	186499	19516	9213	8	8.82

Asia : 8015 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3122	-3609	547	211298	20492	9673	15	25	0.965	0.950	--	0.902	0.566	0.541
0.943													

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3122	3256	310	194122	19516	9213	8	4.62
1	Z	3122	1953	516	191155	19516	9213	8	5.80

Asta : 8015 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	15	25	0.967	0.953	--	1.001	0.509	0.601
-2527	-3783	493	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.509	0.601

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2527	3787	251	194573	19516	9213	8	4.27
1	Z	2527	2272	419	191784	19516	9213	8	5.71

Asta : 8015 [0 , 57]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	13	22	0.976	0.965	--	0.974	0.515	0.584
-1986	-3756	354	211298	20492	9673	13	22	0.976	0.965	--	0.974	0.515	0.584

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1986	3657	182	196346	19516	9213	8	4.60
1	Z	1986	2194	304	194269	19516	9213	8	6.43

Asta : 8015 [57 , 58]

Sez. G: HE 240 A L=122.5 cm Ln1=122.5 cm Ln2=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	12	20	0.984	0.976	--	0.924	0.468	0.555
-1603	-3489	291	211298	20492	9673	12	20	0.984	0.976	--	0.924	0.468	0.555

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1603	3225	136	197923	19516	9213	8	5.32
1	Z	1603	1935	226	196498	19516	9213	8	7.58

Asta : 8015 [58 , 383]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	19	0.990	0.985	--	0.877	0.395	0.526
-605	-2858	188	211298	20492	9673	11	19	0.990	0.985	--	0.877	0.395	0.526

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	605	2506	74	199188	19516	9213	9	7.17
1	Z	605	1504	124	198299	19516	9213	9	10.7

Asta : 8015 [383 , 384]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	18	0.993	0.990	--	0.766	0.552	0.459
-713	-2000	52	211298	20492	9673	11	18	0.993	0.990	--	0.766	0.552	0.459

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	713	1531	28	199884	19516	9213	9	11.7
1	Z	713	919	47	199294	19516	9213	9	17.9

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Asta : 8015 [384 , 342]

Sez. G: HE 240 A L=12.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	11	19	0.990	0.986	--	0.838	0.240	0.503
-2358	1706	2	211298	20492	9673	11	19	0.990	0.986	--	0.838	0.240	0.503

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2358	1429	0	199306	19516	9213	10	11.7
1	Z	2358	858	1	198466	19516	9213	10	17.9

Asta : 8016 [117 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.945	0.923	--	0.689	0.411	0.684
-6438	3978	303	211298	20492	9673	18	30	0.945	0.923	--	0.689	0.411	0.684

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6438	2740	125	190238	19516	9213	3	5.33
1	Z	6438	1644	208	185803	19516	9213	3	7.07

Asta : 8016 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.948	0.927	--	0.538	0.512	0.854
-4712	-1734	678	211298	20492	9673	18	30	0.948	0.927	--	0.538	0.512	0.854

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4712	933	347	190743	19516	9213	8	9.08
1	Z	4712	560	579	186492	19516	9213	8	8.56

Asta : 8016 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	18	30	0.948	0.927	--	0.602	0.361	0.601
-3999	-2777	664	211298	20492	9673	18	30	0.948	0.927	--	0.602	0.361	0.601

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3999	1671	240	190743	19516	9213	8	7.54
1	Z	3999	1003	399	186492	19516	9213	8	8.61

Asta : 8016 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	15	25	0.965	0.950	--	0.906	0.564	0.940
-3262	-3595	522	211298	20492	9673	15	25	0.965	0.950	--	0.906	0.564	0.940

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3262	3258	294	194116	19516	9213	8	4.64
1	Z	3262	1955	491	191146	19516	9213	8	5.87

Asta : 8016 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

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N	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-2662	-3736	465	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.505
											0.601	0.842
Clis	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd					
								Comb.				
kg	kg	kg	kg*m	kg	kg	kg	kg*m					
1	Y	2662	3741	235	194567	19516	9213					
1	Z	2662	2244	392	191775	19516	9213					

Asia : 8016 [0 , 49]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-2125	-3704	324	211298	20492	9673	13	22	0.976	0.965	--	0.971	0.522
											0.583	0.869

Clis	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd					
								Comb.				
kg	kg	kg	kg*m	kg	kg	kg	kg*m					
1	Y	2125	3597	169	196339	19516	9213					
1	Z	2125	2158	282	194259	19516	9213					

Asia : 8016 [49 , 50]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-1741	-3414	278	211298	20492	9673	12	20	0.983	0.976	--	0.923	0.470
											0.554	0.783

Clis	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd					
								Comb.				
kg	kg	kg	kg*m	kg	kg	kg	kg*m					
1	Y	1741	3150	131	197915	19516	9213					
1	Z	1741	1890	218	196487	19516	9213					

Asia : 8016 [50 , 375]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-725	-2790	184	211298	20492	9673	11	19	0.990	0.985	--	0.877	0.394
											0.526	0.657

Clis	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd					
								Comb.				
kg	kg	kg	kg*m	kg	kg	kg	kg*m					
1	Y	725	2448	72	199179	19516	9213					
1	Z	725	1469	121	198286	19516	9213					

Asia : 8016 [375 , 376]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-889	-1959	53	211298	20492	9673	11	18	0.993	0.990	--	0.771	0.533
											0.463	0.888

Clis	Dir	N	Mvseq	Mzeq	NRd	MvRd	MzRd					
								Comb.				
kg	kg	kg	kg*m	kg	kg	kg	kg*m					
1	Y	889	1511	28	199875	19516	9213					
1	Z	889	906	47	199281	19516	9213					

Asia : 8016 [376 , 343]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-2471	1625	3	211298	20492	9673	11	19	0.990	0.986	--	0.847	0.240
											0.508	0.399

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Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd					
								Comb.				
kg	kg	kg	kg*m	kg	kg	kg	kg*m					
1	Y	2471	1377	1	199297	19516	9213					
1	Z	2471	826	1	198454	19516	9213					

Asia : 8017 [118 , 173]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg	kg	kg	kg*m	kg	kg*m	kg	kg*m	kg
-7350	3799	351	211298	20492	9673	18	30	0.945	0.923	--	0.603	0.361
											0.362	0.602

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd					
								Comb.				
kg	kg	kg	kg*m	kg	kg	kg	kg*m					
1	Y	7350	2293	127	190239	19516	9213					
1	Z	7350	1376	211	185804	19516	9213					

Asia : 8017 [173 , 174]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione γM=1.05 fykγM=2619

kg/cmq ft=4300 kg/cmq;**Verificato**

N	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg	kg*m	kg	kg	kg	kg*m	kg	kg*m	kg	kg*m	kg
-5439	-1790	683	211298	20492	9673	18	30	0.948	0.927	--	0.526	0.531
											0.315	0.885

Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd					
								Comb.				
kg	kg	kg	kg*m	kg	kg	kg	kg*m					

Asia : 8017 [177 , 35]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1017	-3857	329	211298	20492	9673	13	22	0.976	0.965	--	0.958	0.509	0.575
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	1017	3694	168	196340	19516	9213	8					
1	Z	1017	2216	279	194260	19516	9213	8					

Asia : 8017 [35 , 36]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1784	-3541	296	211298	20492	9673	12	20	0.984	0.976	--	0.899	0.476	0.539
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	1784	3182	141	197916	19516	9213	8					
1	Z	1784	1909	235	196489	19516	9213	8					

Asia : 8017 [36 , 36]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-809	-2681	201	211298	20492	9673	11	19	0.990	0.985	--	0.844	0.454	0.507
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	809	2263	91	199181	19516	9213	9					
1	Z	809	1358	152	198288	19516	9213	9					

Asia : 8017 [361 , 362]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4855	1893	108	211298	20492	9673	11	18	0.993	0.990	--	0.888	0.239	0.533
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	4855	1681	26	199877	19516	9213	(12+13)-VIII-4					
1	Z	4855	1008	43	199283	19516	9213	(12+13)-VIII-4					

Asia : 8017 [362 , 344]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2529	1712	6	211298	20492	9673	11	19	0.990	0.986	--	0.850	0.260	0.510
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	2529	1455	2	199298	19516	9213	10					
1	Z	2529	873	3	198456	19516	9213	10					

Asia : 8018 [119 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-7125	4142	379	211298	20492	9673	18	30	0.945	0.923	--	0.692	0.417	0.694
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	7125	2867	158	190242	19516	9213	3					
1	Z	7125	1720	263	185808	19516	9213	3					

Asia : 8018 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-5729	-1723	674	211298	20492	9673	18	30	0.948	0.927	--	0.523	0.545	0.314
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	5729	901	367	190746	19516	9213	8					
1	Z	5729	540	612	186497	19516	9213	8					

Asia : 8018 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4405	-2689	718	211298	20492	9673	18	30	0.948	0.927	--	0.843	0.522	0.506
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	4405	2268	375	190746	19516	9213	8					
1	Z	4405	1361	624	186497	19516	9213	8					

Asia : 8018 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3643	-3518	541	211298	20492	9673	15	25	0.965	0.950	--	0.903	0.533	0.542
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	3643	3176	288	194120	19516	9213	8					
1	Z	3643	1906	481	191152	19516	9213	8					

Asia : 8018 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3067	-3759	440	211298	20492	9673	15	25	0.967	0.953	--	0.973	0.504	0.584
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	3067	3656	222	194572	19516	9213	8					
1	Z	3067	2194	369	191781	19516	9213	8					

Asia : 8018 [0 , 53]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2527	-3738	309	211298	20492	9673	13	22	0.976	0.965	--	1.001	0.491	0.600
Clis	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.					
		kg	kg*m	kg*m	kg	kg*m	kg*m						
1	Y	3067	3656	222	194572	19516	9213	8					

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2527	3741	151	196344	19516	9213	8	4.53
1	Z	2527	2244	252	194266	19516	9213	8	6.43

Asta : 8018 [53 , 54]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-1383	-3481	245	211298	20492	9673	12	20	0.984	0.976	--	0.948	0.492	0.569
													0.820

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1383	3299	120	197921	19516	9213	8	5.29
1	Z	1383	1980	201	196495	19516	9213	8	7.68

Asta : 8018 [54 , 379]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-1202	-3022	190	211298	20492	9673	11	19	0.990	0.985	--	0.881	0.464	0.529
													0.773

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1202	2662	88	199186	19516	9213	8	6.58
1	Z	1202	1597	147	198295	19516	9213	8	9.63

Asta : 8018 [379 , 380]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-4819	1868	-119	211298	20492	9673	11	18	0.993	0.990	--	0.831	0.239	0.498
													0.398

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4819	1552	28	199882	19516	9213	(12+13)-VIII-1	9.37
1	Z	4819	931	47	199290	19516	9213	(12+13)-VIII-1	13.0

Asta : 8018 [380 , 345]

Sez. G: HE 240 A L=112.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-1931	2560	13	211298	20492	9673	11	19	0.990	0.986	--	0.734	0.240	0.440
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1931	1878	5	199503	19516	9213	(12+13)-V-2	9.41
1	Z	1931	1127	5	198463	19516	9213	(12+13)-V-2	14.7

Asta : 8019 [120 , 0]

Sez. G: HE 240 A L=181.5 cm Ln1=181.5 cm Ln2=181.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-4612	4122	399	211298	20492	9673	18	30	0.945	0.923	--	0.696	0.419	0.417
													0.698

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6612	2868	167	190246	19516	9213	3	5.00
1	Z	6612	1721	278	185813	19516	9213	3	6.50

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Asta : 8019 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-4824	-1655	739	211298	20492	9673	18	30	0.948	0.927	--	0.508	0.532	0.886

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4824	841	393	190750	19516	9213	8	9.01
1	Z	4824	504	655	186502	19516	9213	8	8.14

Asta : 8019 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-4108	-2773	749	211298	20492	9673	18	30	0.948	0.927	--	0.836	0.504	0.840

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4108	2319	377	190750	19516	9213	8	5.51
1	Z	4108	1392	629	186502	19516	9213	8	6.19

Asta : 8019 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-3292	-3668	499	211298	20492	9673	15	25	0.965	0.950	--	0.899	0.555	0.540
													0.925

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3292	3298	277	194125	19516	9213	8	4.63
1	Z	3292	1979	462	191159	19516	9213	8	5.93

Asta : 8019 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-2676	-3841	424	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.496	0.601
													0.826

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2676	3846	210	194577	19516	9213	8	4.28
1	Z	2676	2307	351	191788	19516	9213	8	5.87

Asta : 8019 [0 , 59]

Sez. G: HE 240 A L=134.3 cm Ln1=134.3 cm Ln2=134.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg*m	kg	kg*m				
-2110	-3811	276	211298	20492	9673	13	22	0.976	0.965	--	0.973	0.538	0.897

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2110	3710	149	196350	19516	9213	8	4.61
1	Z	2110	2226	248	194274	19516	9213	8	6.59

Asta : 8019 [59 , 60]

Sez. G: HE 240 A L=122.5 cm Ln1=122.5 cm Ln2=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

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N		My		Mz		NRk		MyRk		MzRk		λY		λZ		χY		χZ		χLT		kyz		kzz	
kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-1729	-3534	262	211298	20492	6673	12	20	0.984	0.976	--	0.922	0.474	0.553	0.791											
Cls	Dir		N		Mvseq		NRd		MyRd		MzRd		Comb.		SF										
	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m													
1	Y	1729	3258	124	197927	19516	9213	8	5.29																
1	Z	1729	1955	207	196504	19516	9213	8	7.61																

Asia : 8019 [60 , 385]

Sez. G: HE 240 A L=113.1 cm Ln1=113.1 cm Ln2=113.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

	N		My		Mz		NRk		MyRk		MzRk		λY		λZ		χY		χZ		χLT		kyz		kzz	
	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-675	-2874	180	211298	20492	673	11	19	0.990	0.985	--	0.875	0.392	0.525	0.653												

Cls	Dir	N	Myeq kg	Mzeq kg*m	NfRd	MyRd kg*m	MzRd kg*m	Comb.	SF
1	Y	675	2513	71	199192	19516	9213	9	7.15
1	Z	675	1508	118	198305	19516	9213	9	10.7

Asia : 8019 [385 , 386]

Sez. G: HE 240 A L=108.0 cm Ln1=108.0 cm Ln2=108.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

	N		My		Mz		NRk		MyRk		MzRk		λY		λZ		χY		χZ		χLT		kyz		kzz	
	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-816	-1996	57	211298	20492	673	11	18	0.993	0.990	--	0.761	0.506	0.457	0.843												

Cls	Dir	N	Mvseq kg kg*m	Mvseq kg*m	NRd	MyRd kg*m	MzRd kg*m	Comb.	SF
1	Y	816	1519	29	198889	19516	9213	9	11.8
1	Z	816	911	48	199301	19516	9213	9	17.8

Asia : 8019 [386 , 346]

Sez. G: HE 240 A L=112.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

	N		My		Mz		NRk		MvRk		MzRk		λY		λZ		χY		χZ		χLT		kyz		kzz	
	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-2560	1696	5	211298	20492	673	11	19	0.990	0.986	--	0.847	0.240	0.508	0.399												

Cls	Dir	N		Mvseq		NRd		MyRd		MzRd		Comb.	SF
		kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m				
1	Y	2560	1437	1	199310	19516	9213	10	11.5				
1	Z	2560	862	2	198473	19516	9213	10	17.5				

Asia : 8020 [121 , 198]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

	N		My		Mz		NRk		MyRk		MzRk		λY		λZ		χY		χZ		χLT		kyz		kzz	
	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-7197	4185	471	211298	20492	6673	18	30	0.945	0.923	--	0.697	0.429	0.418	0.714												

Cls	Dir	N	Mvseq		Mzseq		NRd		MyRd		MzRd		Comb.	SF
			kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m				
1	Y	7197	2915	202	190235	19516	9213	3	4.78					
1	Z	7197	1749	336	185799	19516	9213	3	6.07					

Asia : 8020 [198 , 199]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

	N		My		Mz		NRk		MvRk		MzRk		λY		λZ		χY		χZ		χLT		kyz		kzz	
	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-5511	-1757	654	211298	20492	673	18	30	0.948	0.927	--	0.514	0.585	0.308	0.974												

Clis	Dir	N	N	Mveq	Mzseq	NRd	MyRd	MzRd	Comb.	SF
1	Y	5511	902	382	190740	19516	9213	8	8.58	
1	Z	5511	541	637	186488	19516	9213	8	7.91	

Asia : 8020 [199 , 200]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

	N		My		Mz		NRk		MyRk		MzRk		λY		λZ		χY		χZ		χLT		kyz		kzz	
	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m	kg	kg*m
-4146	-2785	684	211298	20492	673	18	30	0.948	0.927	--	0.833	0.519	0.500	0.865												

Cls	Dir	N		Mveq		Mreq		NRd		MyRd		MzRd		Comb.	SF
		kg		kg*m		kg*m		kg		kg*m		kg*m			
1	Y	4146		2321		355		190740		19516		9213		8	5.58
1	Z	4146		1392		592		186488		19516		9213		8	6.34

Asia : 8020 [46 , 371]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-735	-2867	183	211298	20492	9673	11	19	0.990	0.985	--	0.873	0.401	0.524
													0.669

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	735	2304	73	199174	19516	9213	9	7.14
	Z	735	1502	122	198279	19516	9213	9	10.6

Asia : 8020 [371 , 372]

Sez. G: HE 240 A L=108.2 cm Ln1=108.2 cm Ln2=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-859	-1981	59	211298	20492	9673	11	18	0.993	0.990	--	0.758	0.530	0.455
													0.883

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	859	1501	31	199870	19516	9213	9	11.8
	Z	859	901	52	199273	19516	9213	9	17.8

Asia : 8020 [372 , 347]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2539	1765	6	211298	20492	9673	11	19	0.990	0.986	--	0.842	0.240	0.505
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2539	1486	1	199292	19516	9213	10	11.2
	Z	2539	891	2	198447	19516	9213	10	17.0

Asia : 8021 [122 , 0]

Sez. G: HE 240 A L=181.7 cm Ln1=181.7 cm Ln2=181.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6533	4212	464	211298	20492	9673	18	30	0.945	0.923	--	0.698	0.418	0.419
													0.696

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6533	2942	194	190232	19516	9213	3	4.85
	Z	6533	1765	323	185795	19516	9213	3	6.22

Asia : 8021 [0 , 0]

Sez. G: HE 240 A L=171.7 cm Ln1=177.7 cm Ln2=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4790	-1701	762	211298	20492	9673	18	30	0.948	0.927	--	0.503	0.550	0.302
													0.917

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4790	855	419	190736	19516	9213	8	8.74
	Z	4790	513	699	186483	19516	9213	8	7.82

Asia : 8021 [0 , 0]

Sez. G: HE 240 A L=171.7 cm Ln1=177.7 cm Ln2=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4145	-2810	772	211298	20492	9673	18	30	0.948	0.927	--	0.840	0.500	0.504
													0.833

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4145	2361	386	190736	19516	9213	8	5.42
	Z	4145	1417	643	186483	19516	9213	8	6.07

Asia : 8021 [0 , 0]

Sez. G: HE 240 A L=151.4 cm Ln1=151.4 cm Ln2=151.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3371	-3688	500	211298	20492	9673	15	25	0.965	0.950	--	0.902	0.544	0.541
													0.906

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3371	3326	272	194108	19516	9213	8	4.60
	Z	3371	1995	453	191136	19516	9213	8	5.92

Asia : 8021 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2766	-3851	401	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.494	0.601
													0.823

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2766	3856	198	194559	19516	9213	8	4.29
	Z	2766	2314	330	191764	19516	9213	8	5.92

Asia : 8021 [0 , 61]

Sez. G: HE 240 A L=134.5 cm Ln1=134.5 cm Ln2=134.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2213	-3821	258	211298	20492	9673	13	22	0.976	0.965	--	0.972	0.544	0.583
													0.906

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2213	3714	140	196330	19516	9213	8	4.61
	Z	2213	2229	234	194247	19516	9213	8	6.62

Asia : 8021 [61 , 62]

Sez. G: HE 240 A L=122.7 cm Ln1=122.7 cm Ln2=122.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1821	-3531	252	211298	20492	9673	12	20	0.983	0.976	--	0.921	0.480	0.553
													0.799

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1821	3254	121	197905	19516	9213	8	5.29
	Z	1821	1952	201	196473	19516	9213	8	7.62

Asia : 8021 [62 , 387]

Sez. G: HE 240 A L=113.3 cm Ln1=113.3 cm Ln2=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq *Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1650	-2834	180	211298	20492	9673	11	19	0.990	0.985	--	0.850	0.392	0.510
													0.654

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1650	2410	71	199169	19516	9213	8	7.17
1	Z	1650	1446	118	198271	19516	9213	8	10.5

Asta : 80221 [387 , 388]

Sez. G: HE 240 A L=108.2 cm Ln1=108.2 cm Ln2=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-904	-1978	59	211298	20492	9673	11	18	0.993	0.990	--	0.758	0.502	0.455
													0.836

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	904	1499	30	199864	19516	9213	9	11.8
1	Z	904	899	50	199265	19516	9213	9	17.9

Asta : 8021 [388 , 348]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-2601	1767	7	211298	20492	9673	11	19	0.990	0.986	--	0.841	0.240	0.505
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2601	1487	2	199286	19516	9213	10	11.2
1	Z	2601	892	3	198438	19516	9213	10	16.9

Asta : 8022 [123 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-4897	3645	527	211298	20492	9673	18	30	0.945	0.923	--	0.603	0.361	0.362
													0.602

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6897	2199	191	190242	19516	9213	3	5.90
1	Z	6897	1319	318	185808	19516	9213	3	7.18

Asta : 8022 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-5260	-1703	696	211298	20492	9673	18	30	0.948	0.927	--	0.521	0.591	0.313
													0.985

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	5260	887	411	190746	19516	9213	8	8.50
1	Z	5260	532	686	186497	19516	9213	8	7.70

Asta : 8022 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-4149	-2742	744	211298	20492	9673	18	30	0.948	0.927	--	0.839	0.500	0.503
													0.834

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4149	2300	372	190746	19516	9213	8	5.56
1	Z	4149	1380	620	186497	19516	9213	8	6.24

949

Asta : 8022 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-3383	-3614	484	211298	20492	9673	15	25	0.965	0.950	--	0.900	0.546	0.540
													0.909

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3383	3254	264	194120	19516	9213	8	4.70
1	Z	3383	1952	440	191152	19516	9213	8	6.04

Asta : 8022 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Ln1=147.8 cm Ln2=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-2779	-3787	392	211298	20492	9673	15	25	0.967	0.953	--	1.001	0.487	0.601
													0.811

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2779	3792	191	194571	19516	9213	8	4.36
1	Z	2779	2275	318	191781	19516	9213	8	6.04

Asta : 8022 [0 , 51]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-2236	-3758	239	211298	20492	9673	13	22	0.976	0.965	--	0.973	0.552	0.584
													0.920

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2236	3658	132	196344	19516	9213	8	4.69
1	Z	2236	2195	220	194266	19516	9213	8	6.77

Asta : 8022 [51 , 52]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-1844	-3484	244	211298	20492	9673	12	20	0.984	0.976	--	0.923	0.484	0.806

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1844	3217	118	197921	19516	9213	8	5.35
1	Z	1844	1930	197	196495	19516	9213	8	7.71

Asta : 8022 [52 , 377]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m	kg	kg	kg	kg				
-751	-2849	182	211298	20492	9673	11	19	0.990	0.985	--	0.876	0.397	0.526
													0.662

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	751	2496	72	199185	19516	9213	9	7.17
1	Z	751	1498	121	198295	19516	9213	9	10.7

Asta : 8022 [377 , 378]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$

kg/cm² ft=4300 kg/cm²**Verificato**

950

Asia : 8023 [382 , 350]

Sez. G: HE 240 A L=112.3 cm Ln1=112.3 cm Ln2=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2661	1661	8	211298	20492	9673	11	19	0.990	0.986	--	0.853	0.240	0.512
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2661	1417	2	199302	19516	9213	10	11.6
1	Z	2661	850	3	198461	19516	9213	10	17.4

Asia : 8024 [125 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-6459	3561	564	211298	20492	9673	18	30	0.945	0.923	--	0.676	0.388	0.406
													0.647

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	6459	2409	219	190239	19516	9213	3	5.52
1	Z	6459	1445	364	185804	19516	9213	3	6.74

Asia : 8024 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4656	-1911	739	211298	20492	9673	18	30	0.948	0.927	--	0.578	0.591	0.347
													0.985

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4656	1103	437	190743	19516	9213	8	7.79
1	Z	4656	662	728	186493	19516	9213	8	7.25

Asia : 8024 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2825	-2942	753	211298	20492	9673	18	30	0.948	0.927	--	0.839	0.504	0.503
													0.840

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2825	2467	379	190743	19516	9213	8	5.48
1	Z	2825	1480	632	186493	19516	9213	8	6.26

Asia : 8024 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2022	-3679	507	211298	20492	9673	15	25	0.965	0.950	--	0.916	0.525	0.550
													0.876

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2022	3370	266	194117	19516	9213	8	4.72
1	Z	2022	2022	444	191147	19516	9213	8	6.16

Asia : 8024 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1617	-3727	392	211298	20492	9673	15	25	0.967	0.953	--	1.000	0.486	0.600
													0.810

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1617	3727	190	194568	19516	9213	8	4.55
1	Z	1617	2236	317	191776	19516	9213	8	6.35

Asia : 8024 [0 , 63]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1080	-3639	239	211298	20492	9673	13	22	0.976	0.965	--	0.936	0.567	0.561
													0.945

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1080	3405	135	196340	19516	9213	8	5.14
1	Z	1080	2043	226	194260	19516	9213	8	7.42

Asia : 8024 [63 , 64]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-2522	-3244	264	211298	20492	9673	12	20	0.984	0.976	--	0.881	0.498	0.528
													0.830

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	2522	2857	131	197916	19516	9213	8	5.77
1	Z	2522	1714	219	196488	19516	9213	8	8.04

Asia : 8024 [64 , 389]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-1339	-2393	205	211298	20492	9673	11	19	0.990	0.985	--	0.831	0.463	0.499
													0.772

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1339	1989	95	199180	19516	9213	9	8.41
1	Z	1339	1194	158	198288	19516	9213	9	11.8

Asia : 8024 [389 , 390]

Sez. G: HE 240 A L=08.1 cm Ln1=08.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-4948	1872	80	211298	20492	9673	11	18	0.993	0.990	--	0.825	0.239	0.495
													0.398

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	4948	1546	19	199876	19516	9213	(12+13)-VIII-4	9.43
1	Z	4948	927	32	199282	19516	9213	(12+13)-VIII-4	13.2

Asia : 8024 [390 , 351]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/γM=2619

kg/cmq ft=4300 kg/cmq*Verificato*

N	My	Mz	NRk	MvRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m								
-3086	1164	15	211298	20492	9673	11	19	0.990	0.986	--	0.903	0.239	0.542
													0.399

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	3086	1050	4	199298	19516	9213	10	14.4
1	Z	3086	630	6	198455	19516	9213	10	20.6

Asta : 8025 [126 , 0]

Sez. G: HE 240 A L=181.6 cm Ln1=181.6 cm Ln2=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg	kg*m			
-4022	2318	585	211298	20492	9673	18	30	0.945	0.923	--	0.663	0.383	0.398
													0.638

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	4022	1537	224	190238	19516	9213	3	8.05
1	Z	4022	922	373	185803	19516	9213	3	9.14

Asta : 8025 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg	kg*m			
-3315	-1494	811	211298	20492	9673	18	30	0.948	0.927	--	0.631	0.583	0.378
													0.971

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg	kg*m		
1	Y	3315	942	473	190743	19516	9213	8	8.55
1	Z	3315	565	788	186492	19516	9213	8	7.56

Asta : 8025 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Ln1=177.6 cm Ln2=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg	kg*m			
-3280	-2244	817	211298	20492	9673	18	30	0.948	0.927	--	0.873	0.497	0.524
													0.829

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	3280	1958	406	190743	19516	9213	8	6.19
1	Z	3280	1175	677	186492	19516	9213	8	6.61

Asta : 8025 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Ln1=151.3 cm Ln2=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg	kg*m			
-2909	-2872	521	211298	20492	9673	15	25	0.965	0.950	--	0.911	0.516	0.547
													0.860

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	2909	2616	269	194116	19516	9213	8	5.61
1	Z	2909	1570	448	191147	19516	9213	8	6.93

Asta : 8025 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Ln1=147.9 cm Ln2=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg	kg*m			
-2221	-3158	403	211298	20492	9673	15	25	0.967	0.953	--	0.957	0.486	0.574
													0.809

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	2221	3023	196	194567	19516	9213	8	5.33
1	Z	2221	1814	326	191775	19516	9213	8	7.15

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Asta : 8025 [0 , 67]

Sez. G: HE 240 A L=134.4 cm Ln1=134.4 cm Ln2=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz
kg	kg*m	kg	kg	kg*m	kg*m	kg	kg	kg	kg	kg*m			
-1936	-3258	251	211298	20492	9673	13	22	0.976	0.965	--	1.001	0.497	0.600
													0.828

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	1936	3260	125	196339	19516	9213	8	5.25
1	Z	1936	1956	208	194259	19516	9213	8	7.54

Asta : 8025 [67 , 68]

Sez. G: HE 240 A L=122.6 cm Ln1=122.6 cm Ln2=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz
kg	kg	kg	kg	kg*m	kg*m	kg	kg	kg	kg	kg*m			
-205	-3072	204	211298	20492	9673	12	20	0.983	0.976	--	1.000	0.520	0.600
													0.866

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	205	3073	106	197915	19516	9213	8	5.88
1	Z	205	1844	177	196487	19516	9213	8	8.72

Asta : 8025 [68 , 393]

Sez. G: HE 240 A L=113.2 cm Ln1=113.2 cm Ln2=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz
kg	kg	kg	kg	kg*m	kg*m	kg	kg	kg	kg	kg*m			
-123	-2956	183	211298	20492	9673	11	19	0.990	0.985	--	0.928	0.475	0.557
													0.792

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	123	2744	87	199180	19516	9213	8	6.64
1	Z	123	1646	145	198287	19516	9213	8	9.93

Asta : 8025 [393 , 394]

Sez. G: HE 240 A L=108.1 cm Ln1=108.1 cm Ln2=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz
kg	kg	kg	kg	kg*m	kg*m	kg	kg	kg	kg	kg*m			
-4867	1665	-183	211298	20492	9673	11	18	0.993	0.990	--	0.929	0.245	0.408

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	4867	1546	45	199876	19516	9213	(12+13)-VIII-1	9.22
1	Z	4867	928	75	199281	19516	9213	(12+13)-VIII-1	12.5

Asta : 8025 [394 , 352]

Sez. G: HE 240 A L=112.4 cm Ln1=112.4 cm Ln2=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk $\gamma M=2619$ kg/cmq ft=4300 kg/cmq;**Verificato**

N	My	Mz	NRk	MvRk	MzRk	λ Y	λ Z	χ Y	χ Z	χ LT	kyz	kzy	kzz
kg	kg	kg	kg	kg*m	kg*m	kg	kg	kg	kg	kg*m			
-1394	1336	26	211298	20492	9673	11	19	0.990	0.986	--	0.956	0.278	0.463

Cls	Dir	N	Mveq	Mzeq	NRd	MvRd	MzRd	Comb.	SF
		kg	kg	kg*m	kg	kg	kg*m		
1	Y	1394	1277	7	199297	19516	9213	(12+13)-V-2	13.7
1	Z	1394	766	12	198454	19516	9213	(12+13)-V-2	21.0

Verifica Resistenza aste Metalliche

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Scenario di calcolo : Set_NT_SLV_A2_STR/GEO									
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Asta : 1 [1 , 54]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
167	1	-17430	-936	-835	-6	898	-1992		--	--	(12+13)+V11-4

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86632	37865	462	9213	19516	462	45.3	2.87	75.1	2.87

Asta : 1 [54 , 101]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-5420	401	-240	6	-1552	685		--	--	9

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86661	37877	462	9213	19516	462	>100	5.53	80.1	5.53

Asta : 2 [2 , 53]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
0	1	11997	-948	-922	3	2006	-2063		--	--	(12+13)+V1-4

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86884	37975	462	9213	19516	462	41.2	2.59	>100	2.59

Asta : 2 [53 , 102]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
167	1	-2957	290	-1870	-2	-4575	56		--	--	3

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
167	1	201236	86932	37996	462	9213	19516	462	20.3	3.92	>100	3.92

Asta : 3 [3 , 55]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-2759	-930	-637	1	841	-2060		--	--	(12+13)+V1-4

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87056	38050	462	9213	19516	462	59.8	3.57	>100	3.57

Asta : 3 [55 , 103]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
167	1	-4622	288	-2173	-2	-4952	4		--	--	3

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
167	1	201236	86984	38019	462	9213	19516	462	17.5	3.48	>100	3.48

Asta : 4 [4 , 56]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-3419	-920	-635	1	960	-2064		--	--	(12+13)+V1-4

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87051	38048	462	9213	19516	462	59.9	3.45	>100	3.45

Asta : 4 [56 , 104]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
167	1	-6469	229	-2162	-2	-4914	64		--	--	3

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
167	1	201236	86966	38011	462	9213	19516	462	17.6	3.44	>100	3.44

Asta : 5 [5 , 71]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-3195	-900	-671	1	1001	-2048		--	--	(12+13)+V1-4

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87024	38036	462	9213	19516	462	56.7	3.45	>100	3.45

Asta : 5 [71 , 105]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
167	1	-6719	242	-2251	-1	-5027	28		--	--	3

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
167	1	201236	87012	38031	462	9213	19516	462	16.9	3.40	>100	3.40

Asta : 6 [6 , 74]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	Vyr	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*	kg*	kg*			
0	1	-2509	-894	-669	1	958	-2033		--	--	(12+13)+V1-4

X	cls	Nr	Vyr	Vzr	MTrd	MTrz	Mrv	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86993	38022	462	9213	19516	462	56.9	3.54	>100	3.54

Asta : 6 [74 , 106]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
167	1	-6787	216	-2290	-1	-5097	58	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
167	1	201236	86993	38023	19516	9213	462	16.6	3.32	>100	3.32

Asta : 7 [7 , 76]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-18710	-866	-625	-1	834	-1994	--	--	(12+13)+V1-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	87054	38049	19516	9213	462	60.9	2.84	>100	2.84

Asta : 7 [76 , 107]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
167	1	-8673	211	-2232	-0	-4960	90	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
167	1	201236	87082	38061	19516	9213	462	17.1	3.26	>100	3.26

Asta : 8 [8 , 75]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	12894	-842	-921	0	1716	-1954	--	--	(12+13)+V1-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	87096	38068	19516	9213	462	41.3	2.75	>100	2.75

Asta : 8 [75 , 108]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
167	1	-4526	154	-2375	-0	-5222	141	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
167	1	201236	87082	38061	19516	9213	462	16.0	3.27	>100	3.27

Asta : 9 [9 , 72]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-3410	-773	-871	2	1519	-1819	--	--	(12+13)+V111-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	86980	38017	19516	9213	462	43.6	3.42	>100	3.42

959

Asta : 9 [72 , 109]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
167	1	-6567	213	-2140	-1	-4772	7	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
167	1	201236	87025	38037	19516	9213	462	17.8	3.60	>100	3.60

Asta : 10 [10 , 70]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-3390	-740	-871	0	1512	-1771	--	--	(12+13)+V111-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	87075	38058	19516	9213	462	43.7	3.49	>100	3.49

Asta : 10 [70 , 110]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
167	1	-6816	216	-2356	0	-4784	-24	--	--	6

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
167	1	201236	87086	38063	19516	9213	462	16.2	3.55	>100	3.55

Asta : 11 [11 , 69]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-3468	-757	-810	0	1437	-1812	--	--	(12+13)+V1-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	87060	38052	19516	9213	462	46.9	3.48	>100	3.48

Asta : 11 [69 , 111]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
167	1	-6859	185	-2240	-0	-4908	7	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
167	1	201236	87077	38059	19516	9213	462	17.0	3.49	>100	3.49

Asta : 12 [12 , 72]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-3464	-700	-879	1	1588	-1691	--	--	(12+13)+V111-4

960

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87013	38031	19516	9213	462	43.2	3.55	>100	3.55

Asta : 12 [77 , 112]

Sez. G: HE 240 A L=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-6716	175	-2304	0	-4644	10	--	--	6

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	87095	38067	19516	9213	462	16.5	3.67	>100	3.67

Asta : 13 [13 , 78]

Sez. G: HE 240 A L=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	11708	705	-793	0	2173	1699	--	--	(12+13)>V1-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87069	38056	19516	9213	462	48.0	2.83	>100	2.83

Asta : 13 [78 , 113]

Sez. G: HE 240 A L=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-7356	194	-2147	1	-4785	-2	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	87032	38040	19516	9213	462	17.7	3.55	>100	3.55

Asta : 14 [14 , 73]

Sez. G: HE 240 A L=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-17288	734	-761	1	1172	1750	--	--	(12+13)>V1-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87052	38048	19516	9213	462	50.0	2.98	>100	2.98

Asta : 14 [73 , 114]

Sez. G: HE 240 A L=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-5331	211	-2213	0	-4848	-61	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	87068	38055	19516	9213	462	17.2	3.55	>100	3.55

Asta : 15 [15 , 61]

Sez. G: HE 240 A L=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-3120	-667	-866	1	1562	-1611	--	--	(12+13)>H-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87013	38031	19516	9213	462	43.9	3.70	>100	3.70

Asta : 15 [61 , 115]

Sez. G: HE 240 A L=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-6396	190	-2087	1	-4638	-60	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	87047	38046	19516	9213	462	18.2	3.62	>100	3.62

Asta : 16 [16 , 62]

Sez. G: HE 240 A L=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3526	771	-771	-1	1263	1826	--	--	(12+13)>V1-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87052	38048	19516	9213	462	49.3	3.57	>100	3.57

Asta : 16 [62 , 116]

Sez. G: HE 240 A L=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-6778	184	-2207	1	-4857	-71	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	87038	38042	19516	9213	462	17.2	3.45	>100	3.45

Asta : 17 [17 , 63]

Sez. G: HE 240 A L=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2056	793	-436	-1	1148	1866	--	--	(12+13)>V1-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87035	38041	19516	9213	462	87.2	3.68	>100	3.68

Asta : 17 [63 , 117]

Sez. G: HE 240 A L=167,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-6483	157	-2112	1	-4710	-47	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	87003	38027	19516	9213	462	18.0	3.59	>100	3.59

Asta : 18 [18 , 64]

Sez. G: HE 240 A L=240,0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-16449	-667	-970	2	1872	-1575	--	--	(12+13)-V1-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86937	37998	19516	9213	462	39.2	2.87	>100	2.87

Asta : 18 [64 , 118]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-4755	165	-2258	1	-4991	-82	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	87050	38048	19516	9213	462	16.8	3.35	>100	3.35

Asta : 19 [19 , 60]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-18620	839	-637	2	908	1955	--	--	(12+13)-V1-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86929	37995	19516	9213	462	59.7	2.85	>100	2.85

Asta : 19 [60 , 119]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-6388	198	-2239	2	-4953	-138	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	86981	38017	19516	9213	462	17.0	3.33	>100	3.33

Asta : 20 [20 , 57]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2172	639	-1156	-1	2131	1478	--	--	(12+13)-V-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87002	38026	19516	9213	462	32.9	3.57	>100	3.57

Asta : 20 [57 , 120]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-4640	167	-2201	2	-4872	-113	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	86975	38015	19516	9213	462	17.3	3.39	>100	3.39

Asta : 21 [21 , 59]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2052	823	-761	-1	1246	1925	--	--	(12+13)-V111-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87027	38038	19516	9213	462	50.0	3.53	>100	3.53

Asta : 21 [59 , 121]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-6625	200	-2251	2	-5013	-179	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	86944	38001	19516	9213	462	16.9	3.23	>100	3.23

Asta : 22 [22 , 65]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3197	828	-1227	-1	2254	1941	--	--	(12+13)-V111-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87028	38038	19516	9213	462	31.0	2.92	>100	2.92

Asta : 22 [65 , 122]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-6584	152	-2228	2	-4958	-91	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
167	1	201236	86952	38005	19516	9213	462	17.1	3.37	>100	3.37

Asta : 23 [23 , 58]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3358	858	-1191	0	1148	1969	--	--	(12+13)-V111-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87067	38055	19516	9213	462	32.0	3.46	>100	3.46

Asta : 23 [58 , 123]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
167	1	-6201	158	-2120	3	-4772	-139	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
167	1	201236	86906	37984	19516	9213	462	17.9	3.44	>100	3.44

Asia : 24 [24 , 66]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3512	880	-709	-1	1106	1980	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86993	38023	19516	9213	462	53.6	3.46	>100	3.46

Asia : 24 [66 , 124]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
167	1	-6562	95	-2159	3	-4870	-55	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
167	1	201236	86891	37978	19516	9213	462	17.6	3.47	>100	3.47

Asia : 25 [25 , 67]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	11753	884	-1119	2	2026	1976	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86968	38012	19516	9213	462	34.0	2.65	>100	2.65

Asia : 25 [67 , 125]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
167	1	-4570	152	-1830	1	-4313	-148	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
167	1	201236	87004	38027	19516	9213	462	20.8	3.85	>100	3.85

Asia : 26 [26 , 68]

Sez. G: HE 240 A L=240.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-17764	947	-1005	-2	1357	2014	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86926	37993	19516	9213	462	37.8	2.66	>100	2.66

Asia : 26 [68 , 126]

Sez. G: HE 240 A L=167.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
167	1	-8439	-152	-1180	7	-2851	-27	--	--	(12+13)+VI-1

905

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
167	1	201236	86575	37840	19516	9213	462	32.1	5.24	66.9	5.24

Asia : 27 [1 , 327]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1417	606	-4633	6	4167	344	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86619	37859	19516	9213	462	8.17	3.88	73.0	3.88

Asia : 28 [25 , 351]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2149	761	-1873	7	3703	505	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86536	37823	19516	9213	462	20.2	3.92	62.3	3.92

Asia : 29 [24 , 350]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1965	-357	-492	-4	2731	-202	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86789	37934	19516	9213	462	77.1	5.83	>100	5.83

Asia : 30 [23 , 349]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1877	-481	-353	-4	2486	-322	--	--	(12+13)-II-2

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86788	37933	19516	9213	462	>100	5.83	>100	5.83

Asia : 31 [22 , 348]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1819	-422	-249	-4	2371	-234	--	--	(12+13)+VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86783	37931	19516	9213	462	>100	6.41	>100	6.41

Asia : 32 [21 , 347]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1766	-480	-230	-4	2272	-295	--	--	(12+13)+VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86776	37928	19516	9213	462	>100	6.36	>100	6.36

966

Asia : 33 [18 , 346]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1609	-539	-301	-5	2059	-289	--	--	(12+13)+VIII-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86755	37918	19516	9213	462	>100	6.90	>100	6.90

Asia : 34 [19 , 345]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-2166	-795	-2379	-6	3875	-473	--	--	(12+13)+IV-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86622	37860	19516	9213	462	15.9	3.84	73.5	3.84

Asia : 35 [18 , 344]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-2261	888	-2304	7	3951	524	--	--	(12+13)+VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86574	37839	19516	9213	462	16.4	3.70	66.7	3.70

Asia : 36 [17 , 343]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1590	-568	-328	-5	2050	-316	--	--	(12+13)+VIII-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86733	37909	19516	9213	462	>100	6.79	95.8	6.79

Asia : 37 [16 , 342]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1535	-673	-232	-5	1907	-440	--	--	(12+13)+VIII-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86730	37908	19516	9213	462	>100	6.53	95.0	6.53

Asia : 38 [15 , 341]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1537	-594	-315	-5	1981	-321	--	--	(12+13)+VIII-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86719	37903	19516	9213	462	>100	6.94	92.2	6.94

Asia : 39 [14 , 340]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1720	-897	-2475	-7	3982	-524	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86591	37847	19516	9213	462	15.3	3.71	69.0	3.71

Asia : 40 [13 , 339]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-2188	888	-2259	7	3847	516	--	--	(12+13)+VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86589	37846	19516	9213	462	16.8	3.79	68.7	3.79

Asia : 41 [12 , 338]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1479	-587	1187	-5	1800	-320	--	--	(12+13)+VIII-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86700	37894	19516	9213	462	31.9	7.45	87.8	7.45

Asia : 42 [11 , 337]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1537	612	-545	4	1884	403	--	--	(12+13)+VII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86766	37923	19516	9213	462	69.6	6.76	>100	6.76

Asia : 43 [10 , 336]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1517	436	-364	4	1812	243	--	--	(12+13)+VII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86762	37922	19516	9213	462	>100	7.89	>100	7.89

Asia : 44 [9 , 335]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1778	13	-348	1	2351	15	--	--	(12+13)+I-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87057	38050	19516	9213	462	>100	7.64	>100	7.64

Asia : 45 [8 , 334]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/M=2619$ kg/cmq fl=4300 kg/cmq : <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-2116	-772	-2747	-7	4106	-511	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86555	37831	19516	9213	462	13.8	3.62	64.4	3.62

Asia : 46 [7 , 333]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2103	792	-2785	7	4072	477	--	--	(12+13)-VII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86601	37851	19516	9213	462	13.6	3.69	70.3	3.69

Asia : 47 [6 , 332]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2026	292	-519	4	2817	162	--	--	(12+13)-III-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86785	37932	19516	9213	462	73.1	5.81	>100	5.81

Asia : 48 [5 , 331]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2087	323	-534	4	2937	182	--	--	(12+13)-I-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86786	37932	19516	9213	462	71.1	5.54	>100	5.54

Asia : 49 [4 , 330]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2107	410	-376	4	3035	272	--	--	(12+13)-I-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86790	37934	19516	9213	462	>100	5.11	>100	5.11

Asia : 50 [3 , 329]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2216	-190	-844	4	3282	199	--	--	(12+13)-I-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86789	37934	19516	9213	462	44.9	4.98	>100	4.98

Asia : 51 [2 , 328]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2232	-845	-1888	-6	3880	-549	--	--	(12+13)-IV-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86653	37874	19516	9213	462	20.1	3.71	78.5	3.71

969

Asia : 52 [26 , 332]

Sez. G: HE 240 A L=60.0 cm Crit.: Acciaio Pressflessione $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1501	-488	-4471	-6	4150	-269	--	--	(12+13)-VII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86635	37866	19516	9213	462	8.47	4.01	75.6	4.01

Asia : 7001 [1 , 53]

Sez. G: Fi20 L=256.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-4345	--	--	--	--	--	--	--	(12+13)-VI-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	8228	--	--	--	--	--	>100	1.89	>100	1.89

Asia : 7002 [53 , 101]

Sez. G: Fi20 L=189.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
190	1	6136	--	--	--	--	--	--	--	(12+13)-VI-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
190	1	8228	--	--	--	--	--	>100	1.34	>100	1.34

Asia : 7003 [101 , 0]

Sez. G: Fi16 L=371.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
372	1	2354	--	--	--	--	--	--	--	(12+13)-VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
372	1	5266	--	--	--	--	--	>100	2.24	>100	2.24

Asia : 7004 [0 , 0]

Sez. G: Fi16 L=345.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1279	--	--	--	--	--	--	--	(12+13)-VII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	4.12	>100	4.12

Asia : 7005 [0 , 75]

Sez. G: Fi16 L=269.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2305	--	--	--	--	--	--	--	(12+13)-VII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.28	>100	2.28

Asia : 7006 [75 , 399]

Sez. G: Fi16 L=269.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm ² f=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				

970

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
269	1	3059	--	--	--	--	--	--	--	(12+13)÷VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
269	1	5266	--	--	--	--	--	>100	1.72	>100	1.72

Asia : 7007 [399 , 328]

Sez. G: Fil16 L=260.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	660	--	--	--	--	--	--	--	(12+13)÷VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	7.98	>100	7.98

Asia : 7008 [327 , 0]

Sez. G: Fil16 L=260.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-563	--	--	--	--	--	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	9.35	>100	9.35

Asia : 7009 [0 , 73]

Sez. G: Fil16 L=269.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
269	1	-3300	--	--	--	--	--	--	--	(12+13)÷VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
269	1	5266	--	--	--	--	--	>100	1.60	>100	1.60

Asia : 7010 [73 , 0]

Sez. G: Fil16 L=306.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2015	--	--	--	--	--	--	--	(12+13)÷VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.61	>100	2.61

Asia : 7011 [0 , 0]

Sez. G: Fil16 L=345.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	967	--	--	--	--	--	--	--	(12+13)÷IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	5.45	>100	5.45

Asia : 7012 [0 , 102]

Sez. G: Fil16 L=371.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	2423	--	--	--	--	--	--	--	(12+13)÷VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	5266	--	--	--	--	--	>100	2.17	>100	2.17

Asia : 7013 [102 , 54]

Sez. G: F20 L=189.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
189	1	-6444	--	--	--	--	--	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
189	1	8228	--	--	--	--	--	>100	1.28	>100	1.28

Asia : 7014 [54 , 2]

Sez. G: F20 L=256.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	4260	--	--	--	--	--	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	8228	--	--	--	--	--	>100	1.93	>100	1.93

Asia : 7015 [25 , 68]

Sez. G: F20 L=256.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg**m	kg**m	kg**m			
256	1	4234	--	--	--	--	--	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
256	1	8228	--	--	--	--	--	>100	1.94	>100	1.94

Asia : 7016 [68 , 125]

Sez. G: F20 L=189.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-6627	--	--	--	--	--	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	8228	--	--	--	--	--	>100	1.24	>100	1.24

Asia : 7017 [125 , 0]

Sez. G: Fil16 L=371.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
372	1	2545	--	--	--	--	--	--	--	(12+13)÷VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
372	1	5266	--	--	--	--	--	>100	2.07	>100	2.07

Asia : 7018 [0 , 0]

Sez. G: Fil16 L=345.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg ^{*m}	kg ^{*m}	kg ^{*m}			
345	1	997	--	--	--	--	--	--	--	(12+13)÷VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
345	1	5266	--	--	--	--	--	>100	5.28	>100	5.28

Asia : 7019 [0 , 67]

Sez. G: Fi16 L=306.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
306	1	2019	--	--	--	--	--	--	(12+13)+V/III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
306	1	5266	--	--	--	--	--	>100	2.61	>100	2.61

Asia : 7020 [67 , 389]

Sez. G: Fi16 L=268.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-3377	--	--	--	--	--	--	(12+13)+V/III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	1.56	>100	1.56

Asia : 7021 [389 , 352]

Sez. G: Fi16 L=260.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
261	1	-444	--	--	--	--	--	--	(12+13)+V/III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
261	1	5266	--	--	--	--	--	>100	11.9	>100	11.9

Asia : 7022 [351 , 393]

Sez. G: Fi16 L=260.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
260	1	531	--	--	--	--	--	--	(12+13)+V/III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
260	1	5266	--	--	--	--	--	>100	9.91	>100	9.91

Asia : 7023 [393 , 63]

Sez. G: Fi16 L=269.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	3110	--	--	--	--	--	--	(12+13)+V/III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	1.69	>100	1.69

Asia : 7024 [63 , 0]

Sez. G: Fi16 L=305.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
306	1	-2340	--	--	--	--	--	--	(12+13)+V/III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
306	1	5266	--	--	--	--	--	>100	2.25	>100	2.25

Asia : 7025 [0 , 0]

Sez. G: Fi16 L=345.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
345	1	-1340	--	--	--	--	--	--	(12+13)+V/III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
345	1	5266	--	--	--	--	--	>100	3.93	>100	3.93

Asia : 7026 [0 , 126]

Sez. G: Fi16 L=371.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	2337	--	--	--	--	--	--	(12+13)+V/1-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.25	>100	2.25

Asia : 7027 [126 , 67]

Sez. G: Fi20 L=189.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	6476	--	--	--	--	--	--	(12+13)+V/1-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	8228	--	--	--	--	--	>100	1.27	>100	1.27

Asia : 7028 [67 , 26]

Sez. G: Fi20 L=256.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
256	1	-4374	--	--	--	--	--	--	(12+13)+V/1-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
256	1	8228	--	--	--	--	--	>100	1.88	>100	1.88

Asia : 7029 [102 , 0]

Sez. G: Fi16 L=406.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
407	1	1852	--	--	--	--	--	--	(12+13)+V/III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
407	1	5266	--	--	--	--	--	>100	2.84	>100	2.84

Asia : 7030 [104 , 0]

Sez. G: Fi16 L=406.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1579	--	--	--	--	--	--	(12+13)+V/III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	3.34	>100	3.34

Asia : 7031 [328 , 391]

Sez. G: Fi16 L=360.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1377	--	--	--	--	--	--	(12+13)+V/III-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.82	>100	3.82
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7032 [330 , 0]

Sez. G: Fi16 L=359.8 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-1620	--	--	--	--	--	--	--	(12+13)>VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.25	>100	3.25
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7033 [19 , 64]

Sez. G: Fi20 L=255.9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-4248	--	--	--	--	--	--	--	(12+13)>VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.94	>100	1.94
0	1	8228	--	--	--	--	--	--	--	--	--

Asia : 7034 [64 , 119]

Sez. G: Fi20 L=189.1 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
185	1	6818	--	--	--	--	--	--	--	(12+13)>VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.21	>100	1.21
185	1	8228	--	--	--	--	--	--	--	--	--

Asia : 7035 [119 , 174]

Sez. G: Fi16 L=371.5 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
371	1	2830	--	--	--	--	--	--	--	(12+13)>VII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.86	>100	1.86
371	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7036 [174 , 0]

Sez. G: Fi16 L=344.9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-1640	--	--	--	--	--	--	--	(12+13)>VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.21	>100	3.21
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7037 [0 , 35]

Sez. G: Fi16 L=305.9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-2035	--	--	--	--	--	--	--	(12+13)>VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.59	>100	2.59
0	1	5266	--	--	--	--	--	--	--	--	--

975

Asia : 7038 [35 , 379]

Sez. G: Fi16 L=268.5 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
244	1	3592	--	--	--	--	--	--	--	(12+13)>VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.47	>100	1.47
244	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7039 [379 , 344]

Sez. G: Fi16 L=260.9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
261	1	-313	--	--	--	--	--	--	--	(12+13)>VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	16.8	>100	16.8
261	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7040 [345 , 361]

Sez. G: Fi16 L=269.9 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	-338	--	--	--	--	--	--	--	(12+13)>VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	15.6	>100	15.6
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7041 [361 , 53]

Sez. G: Fi16 L=269.0 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
269	1	-3457	--	--	--	--	--	--	--	(12+13)>VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.52	>100	1.52
269	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7042 [53 , 176]

Sez. G: Fi16 L=305.6 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
306	1	-1909	--	--	--	--	--	--	--	(12+13)>VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.76	>100	2.76
306	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7043 [176 , 0]

Sez. G: Fi16 L=345.1 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		
0	1	1310	--	--	--	--	--	--	--	(12+13)>VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	4.02	>100	4.02
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7044 [0 , 118]

Sez. G: Fi16 L=371.4 cm Crit.: Acciaio Tirante $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm η =4300 kg/cm η : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m		

976

X	cls	Nr	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	2644	--	--	--	--	--	--	--	(12+13)>VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	1.99	>100	1.99

Asia : 7045 [118 , 60]

Sez. G: Fi20 L=189.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
189	1	-7033	--	--	--	--	--	--	--	(12+13)>VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
189	1	8228	--	--	--	--	--	>100	1.17	>100	1.17

Asia : 7046 [60 , 18]

Sez. G: Fi20 L=255.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	3990	--	--	--	--	--	--	--	(12+13)>VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	8228	--	--	--	--	--	>100	2.06	>100	2.06

Asia : 7047 [199 , 123]

Sez. G: Fi16 L=406.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	2214	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	2.38	>100	2.38

Asia : 7048 [123 , 0]

Sez. G: Fi16 L=406.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1607	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	3.28	>100	3.28

Asia : 7049 [125 , 0]

Sez. G: Fi16 L=406.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
407	1	1821	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
407	1	5266	--	--	--	--	--	>100	2.89	>100	2.89

Asia : 7050 [0 , 121]

Sez. G: Fi16 L=406.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
407	1	-2044	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
407	1	5266	--	--	--	--	--	>100	2.58	>100	2.58

Asia : 7051 [121 , 0]

Sez. G: Fi16 L=406.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
406	1	2188	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
406	1	5266	--	--	--	--	--	>100	2.41	>100	2.41

Asia : 7052 [379 , 347]

Sez. G: Fi16 L=360.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
360	1	-1344	--	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
360	1	5266	--	--	--	--	--	>100	3.92	>100	3.92

Asia : 7053 [347 , 377]

Sez. G: Fi16 L=359.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-965	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
0	1	5266	--	--	--	--	--	>100	5.46	>100	5.46

Asia : 7054 [377 , 351]

Sez. G: Fi16 L=359.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
360	1	-1172	--	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
360	1	5266	--	--	--	--	--	>100	4.49	>100	4.49

Asia : 7055 [371 , 345]

Sez. G: Fi16 L=350.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
360	1	-1118	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
360	1	5266	--	--	--	--	--	>100	4.71	>100	4.71

Asia : 7056 [389 , 349]

Sez. G: Fi16 L=350.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
360	1	-1564	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*	kg*			
360	1	5266	--	--	--	--	--	>100	3.37	>100	3.37

Asia : 7057 [349 , 371]

Sez. G: Fi16 L=359,1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1046	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	5.03	>100	5.03

Asia : 7058 [199 , 119]

Sez. G: Fi16 L=406,6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
407	1	-2015	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
407	1	5266	--	--	--	--	--	>100	2.61	>100	2.61

Asia : 7059 [108 , 76]

Sez. G: Fi20 L=189,9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
190	1	-7137	--	--	--	--	--	--	(12+13)>VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
190	1	8228	--	--	--	--	--	>100	1.15	>100	1.15

Asia : 7060 [76 , 8]

Sez. G: Fi20 L=256,4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	4097	--	--	--	--	--	--	(12+13)>VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	8228	--	--	--	--	--	>100	2.01	>100	2.01

Asia : 7061 [7 , 75]

Sez. G: Fi20 L=256,4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-4315	--	--	--	--	--	--	(12+13)>VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	8228	--	--	--	--	--	>100	1.91	>100	1.91

Asia : 7062 [75 , 107]

Sez. G: Fi20 L=189,9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
190	1	6818	--	--	--	--	--	--	(12+13)>VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
190	1	8228	--	--	--	--	--	>100	1.21	>100	1.21

Asia : 7063 [107 , 184]

Sez. G: Fi16 L=371,7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
370	1	2820	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
370	1	5266	--	--	--	--	--	>100	1.87	>100	1.87

Asia : 7064 [184 , 171]

Sez. G: Fi16 L=345,8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1650	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	3.19	>100	3.19

Asia : 7065 [171 , 39]

Sez. G: Fi16 L=306,7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-2025	--	--	--	--	--	--	(12+13)>VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.60	>100	2.60

Asia : 7066 [39 , 359]

Sez. G: Fi16 L=270,3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
270	1	3344	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
270	1	5266	--	--	--	--	--	>100	1.57	>100	1.57

Asia : 7067 [359 , 334]

Sez. G: Fi16 L=262,1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	438	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	12.0	>100	12.0

Asia : 7068 [333 , 365]

Sez. G: Fi16 L=262,1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-447	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	11.8	>100	11.8

Asia : 7069 [365 , 33]

Sez. G: Fi16 L=270,1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq fl=4300 kg/cmq γ :Verificato									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
270	1	-3456	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.52	>100	1.52
270	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7070 [33 , 186]

Sez. G: F16 L=306.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-4	
307	1	-2051	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.57	>100	2.57
307	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7071 [186 , 169]

Sez. G: F16 L=345.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-1	
0	1	1478	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	3.56	>100	3.56
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7072 [169 , 108]

Sez. G: F16 L=372.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-1	
372	1	-2626	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.01	>100	2.01
372	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7073 [0 , 107]

Sez. G: F16 L=458.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-1	
458	1	-2566	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.23	>100	2.23
458	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7074 [104 , 169]

Sez. G: F16 L=474 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-1	
458	1	2474	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.13	>100	2.13
458	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7075 [391 , 333]

Sez. G: F16 L=480.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-1	
480	1	-1141	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	4.62	>100	4.62
480	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7076 [359 , 330]

Sez. G: F16 L=479.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-4	
480	1	-1269	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	4.15	>100	4.15
480	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7077 [108 , 154]

Sez. G: F16 L=459.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-1	
459	1	2462	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.14	>100	2.14
459	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7078 [184 , 111]

Sez. G: F16 L=458.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-1	
458	1	-2366	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.23	>100	2.23
458	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7079 [111 , 194]

Sez. G: F16 L=406.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-1	
405	1	2033	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	2.59	>100	2.59
405	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7080 [194 , 114]

Sez. G: F16 L=371.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-4	
0	1	2674	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.97	>100	1.97
0	1	5266	--	--	--	--	--	--	--	--	--

Asia : 7081 [114 , 78]

Sez. G: F20 L=189.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VI-4	
189	1	-6640	--	--	--	--	--	--	--	--	--

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	>100	1.24	>100	1.24
189	1	8228	--	--	--	--	--	--	--	--	--

Asia : 7082 [78 , 14]

Sez. G: F20 L=256.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cm γ ft=4300 kg/cm γ : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m	kg*m	(12+13)+VIII-1	
480	1	5266	--	--	--	--	--	--	--	--	--

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
256	1	-3809	--	--	--	--	--	--	--	(12+13)>VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
256	1	8228	--	--	--	--	--	>100	2.16	>100	2.16

Asia : 7083 [13 , 73]

Sez. G: F120 L=236.2 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3808	--	--	--	--	--	--	--	(12+13)>VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	8228	--	--	--	--	--	>100	2.16	>100	2.16

Asia : 7084 [73 , 113]

Sez. G: F120 L=189.5 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-6676	--	--	--	--	--	--	--	(12+13)>VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	8228	--	--	--	--	--	>100	1.23	>100	1.23

Asia : 7085 [113 , 159]

Sez. G: F116 L=371.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
372	1	2703	--	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
372	1	5266	--	--	--	--	--	>100	1.95	>100	1.95

Asia : 7086 [159 , 196]

Sez. G: F116 L=345.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1387	--	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	3.80	>100	3.80

Asia : 7087 [196 , 29]

Sez. G: F116 L=306.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2070	--	--	--	--	--	--	--	(12+13)>VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.54	>100	2.54

Asia : 7088 [161 , 194]

Sez. G: F116 L=345.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
345	1	-1361	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
345	1	5266	--	--	--	--	--	>100	3.87	>100	3.87

Asia : 7089 [154 , 113]

Sez. G: F116 L=406.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
406	1	-1865	--	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
406	1	5266	--	--	--	--	--	>100	2.82	>100	2.82

Asia : 7090 [161 , 43]

Sez. G: F116 L=306.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2003	--	--	--	--	--	--	--	(12+13)>VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.63	>100	2.63

Asia : 7091 [43 , 355]

Sez. G: F116 L=268.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-3397	--	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	1.55	>100	1.55

Asia : 7092 [355 , 339]

Sez. G: F116 L=260.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
261	1	-338	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
261	1	5266	--	--	--	--	--	>100	15.6	>100	15.6

Asia : 7093 [340 , 369]

Sez. G: F116 L=260.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-354	--	--	--	--	--	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	14.9	>100	14.9

Asia : 7094 [369 , 29]

Sez. G: F116 L=260.1 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/M=2619 \text{ kg/cmq}$ fl=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
269	1	-3375	--	--	--	--	--	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
269	1	5266	--	--	--	--	--	>100	1.56	>100	1.56

Asia : 7095 [114 , 0]

Sez. G: Fil16 L=406.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1869	--	--	--	--	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.82	>100	2.82

Asia : 7096 [0 , 118]

Sez. G: Fil16 L=406.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	2067	--	--	--	--	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	2.55	>100	2.55

Asia : 7097 [174 , 116]

Sez. G: Fil16 L=406.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
406	1	-1951	--	--	--	--	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
406	1	5266	--	--	--	--	--	>100	2.70	>100	2.70

Asia : 7098 [116 , 159]

Sez. G: Fil16 L=406.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
406	1	1978	--	--	--	--	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
406	1	5266	--	--	--	--	--	>100	2.66	>100	2.66

Asia : 7099 [340 , 383]

Sez. G: Fil16 L=360.0 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1232	--	--	--	--	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	4.27	>100	4.27

Asia : 7100 [383 , 344]

Sez. G: Fil16 L=360.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
360	1	-1231	--	--	--	--	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
360	1	5266	--	--	--	--	--	>100	4.28	>100	4.28

Asia : 7101 [361 , 342]

Sez. G: Fil16 L=359.9 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
360	1	-1401	--	--	--	--	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
360	1	5266	--	--	--	--	--	>100	3.76	>100	3.76

Asia : 7102 [342 , 355]

Sez. G: Fil16 L=359.8 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1315	--	--	--	--	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	4.00	>100	4.00

Asia : 7103 [334 , 353]

Sez. G: Fil16 L=480.3 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1056	--	--	--	--	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	4.99	>100	4.99

Asia : 7104 [353 , 339]

Sez. G: Fil16 L=359.7 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
360	1	-1219	--	--	--	--	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
360	1	5266	--	--	--	--	--	>100	4.52	>100	4.52

Asia : 7105 [369 , 337]

Sez. G: Fil16 L=359.4 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
359	1	-1372	--	--	--	--	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
359	1	5266	--	--	--	--	--	>100	3.84	>100	3.84

Asia : 7106 [337 , 365]

Sez. G: Fil16 L=480.6 cm Crit.: Acciaio Tirante $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq : <i>Verificato</i>									
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1245	--	--	--	--	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	5266	--	--	--	--	--	>100	4.23	>100	4.23

Asia : 8000 [101 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_{yk}/\gamma M=2619$ kg/cmq ft=4300 kg/cmq									
: <i>Verificato</i>									

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m			
0	1	-1985	230	-332	4	2606	51	--	(12+13)+II-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86785	37952	19516	9213	462	>100	6.71	>100	6.71

Asta : 8000 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1722	-16	-753	0	1547	-387	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87078	38060	19516	9213	462	50.6	7.70	>100	7.70

Asta : 8000 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-276	-14	-457	7	-2436	424	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86554	37831	19516	9213	462	82.7	5.81	64.3	5.81

Asta : 8000 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
151	1	207	-73	-257	-2	-2963	579	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
151	1	201236	86960	38008	19516	9213	462	>100	4.64	>100	4.64

Asta : 8000 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-413	167	-274	2	-3040	588	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86957	38007	19516	9213	462	>100	4.51	>100	4.51

Asta : 8000 [0 , 73]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-29	136	-13	-5	-3278	383	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86722	37904	19516	9213	462	>100	4.77	92.9	4.77

Asta : 8000 [73 , 74]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

987

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-132	118	200	-2	-3190	219	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86925	37993	19516	9213	462	>100	5.32	>100	5.32

Asta : 8000 [74 , 399]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	369	63	516	-8	-2811	98	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86528	37819	19516	9213	462	73.3	6.39	61.3	6.39

Asta : 8000 [399 , 400]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	4319	-168	976	22	-1864	-182	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	85386	37320	19516	9213	462	38.2	7.31	20.6	7.31

Asta : 8000 [400 , 327]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	2176	-32	2227	-11	2225	-19	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	86251	37698	19516	9213	462	16.9	7.88	41.3	7.88

Asta : 8000 [102 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-7455	118	-1828	0	3748	20	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87072	38057	19516	9213	462	20.8	4.32	>100	4.32

Asta : 8001 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-5891	-281	-987	7	-1765	413	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86539	37824	19516	9213	462	38.3	6.08	62.6	6.08

Asta : 8001 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

988

Asia : 8001 [0 , 0]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-4625	-93	-442	7	-2729	618	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86559	37833	19516	9213	462	85.6	4.35	64.9	4.35

Asia : 8001 [0 , 0]

Sez. G: HE 240 A L=151.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
151	1	-3973	30	-495	-5	-3688	647	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
151	1	201236	86687	37889	19516	9213	462	76.5	3.58	85.1	3.58

Asia : 8001 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
30	1	-2598	116	-259	6	-3623	653	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	201236	86647	37871	19516	9213	462	>100	3.71	77.5	3.71

Asia : 8001 [0 , 75]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2137	235	29	-0	-3733	594	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87085	38063	19516	9213	462	>100	3.75	>100	3.75

Asia : 8001 [75 , 76]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1726	175	367	1	-3440	356	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87055	38050	19516	9213	462	>100	4.47	>100	4.47

Asia : 8001 [76 , 0]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-520	150	658	-5	-2900	208	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86706	37897	19516	9213	462	57.6	5.76	89.3	5.76

Asia : 8001 [0 , 0]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-4917	-112	-874	24	1815	-68	--	--	(12+13)VIII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	85255	37263	19516	9213	462	42.7	8.01	19.1	8.01

Asia : 8001 [0 , 328]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	863	-107	2604	-18	2978	42	--	--	(12+13)IV-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	85734	37472	19516	9213	462	14.4	6.19	25.7	6.19

Asia : 8002 [103 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-6555	58	-1955	3	4206	-71	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86904	37984	19516	9213	462	19.4	3.91	>100	3.91

Asia : 8002 [0 , 0]

Sez. G: HE 240 A L=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-4350	-291	-1053	5	-1712	446	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86723	37904	19516	9213	462	36.0	6.34	93.1	6.34

Asia : 8002 [0 , 0]

Sez. G: HE 240 A L=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-3676	-84	-496	6	-2843	602	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86626	37862	19516	9213	462	76.4	4.36	74.2	4.36

Asia : 8002 [0 , 0]

Sez. G: HE 240 A L=151.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
151	1	-2998	24	-436	-6	-3710	638	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
151	1	201236	86674	37883	19516	9213	462	86.9	3.65	82.4	3.65

Asia : 8002 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
15	1	-2706	114	-257	5	-3721	653	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
15	1	201236	86685	37888	19516	9213	462	>100	3.64	84.7	3.64

Asia : 8002 [0 , 71]

Sez. G: HE 240 A L=134.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2198	215	46	0	-3825	578	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87086	38063	19516	9213	462	>100	3.71	>100	3.71

Asia : 8002 [71 , 72]

Sez. G: HE 240 A L=122.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1813	181	394	1	-3513	365	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87031	38039	19516	9213	462	96.5	4.37	>100	4.37

Asia : 8002 [72 , 397]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1642	149	742	-5	-2809	207	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86732	37909	19516	9213	462	51.1	5.73	95.6	5.73

Asia : 8002 [397 , 398]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-841	22	966	-6	-1983	58	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86635	37866	19516	9213	462	39.2	8.92	75.6	8.92

Asia : 8002 [398 , 329]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	39	48	2202	-11	2932	-26	--	--	(12+13)-1

991

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	86245	37696	19516	9213	462	17.1	6.52	41.1	6.52

Asia : 8003 [104 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6912	33	-1919	3	4125	-85	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86897	37980	19516	9213	462	19.8	3.92	>100	3.92

Asia : 8003 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4824	-262	-1039	4	-1733	448	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86772	37926	19516	9213	462	36.5	6.20	>100	6.20

Asia : 8003 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-3731	-80	-494	6	-2810	596	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86622	37860	19516	9213	462	76.7	4.40	73.4	4.40

Asia : 8003 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-3044	28	-442	-6	-3684	626	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
151	1	201236	86679	37885	19516	9213	462	85.7	3.68	83.4	3.68

Asia : 8003 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
15	1	-2743	115	-261	5	-3696	641	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
15	1	201236	86690	37890	19516	9213	462	>100	3.67	85.6	3.67

Asia : 8003 [0 , 65]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

992

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2231	206	37	1	-3808	561	--	--	8
X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	>100	3.74	>100
0	1	201236	87052	38048	19516	9213	462			

Asia : 8003 [65 , 66]

Sez. G: HE 240 A L=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1844	176	387	1	-3506	360	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	98.3	4.39	>100
0	1	201236	87016	38032	19516	9213	462			

Asia : 8003 [66 , 391]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1671	141	734	-5	-2810	208	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	51.6	5.72	94.7
0	1	201236	86729	37907	19516	9213	462			

Asia : 8003 [391 , 392]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-851	26	953	-6	-1979	64	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	39.7	8.89	78.2
0	1	201236	86651	37873	19516	9213	462			

Asia : 8003 [392 , 330]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	228	51	2076	-11	2702	-23	--	--	(12+13)+1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	18.2	7.04	40.6
112	1	201236	86236	37692	19516	9213	462			

Asia : 8004 [105 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6658	14	-1958	3	4268	-62	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	19.4	3.87	>100
0	1	201236	86906	37984	19516	9213	462			

Asia : 8004 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4466	-237	-1049	4	-1690	454	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	36.2	6.33	>100
178	1	201236	86787	37932	19516	9213	462			

Asia : 8004 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-3762	-70	-504	6	-2832	584	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	75.1	4.40	71.4
178	1	201236	86608	37854	19516	9213	462			

Asia : 8004 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-3064	29	-451	-5	-3720	610	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	84.0	3.68	87.8
151	1	201236	86700	37894	19516	9213	462			

Asia : 8004 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
15	1	-2749	116	-265	5	-3731	624	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	>100	3.67	88.2
15	1	201236	86701	37895	19516	9213	462			

Asia : 8004 [0 , 77]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2227	196	34	1	-3850	541	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	>100	3.74	>100
0	1	201236	87030	38039	19516	9213	462			

Asia : 8004 [77 , 78]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1837	171	395	1	-3551	351	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*	96.3	4.36	>100
0	1	201236	86997	38024	19516	9213	462			

Asia : 8004 [78 , 0]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	-1664	148	755	-5	-2843	204	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
0	1	201236	86731	37908	19516	9213	462	50.2	5.68	95.4		5.68

Asia : 8004 [0 , 0]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	-898	19	967	-6	-1983	57	--	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
0	1	201236	86662	37878	19516	9213	462	39.2	8.91	80.3		8.91

Asia : 8004 [0 , 33]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
112	1	-98	48	2019	-11	2697	-26	--	--	--	(12+13)+1

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
112	1	201236	86241	37694	19516	9213	462	18.7	7.07	40.9		7.07

Asia : 8005 [106 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	-6712	-1	-1989	4	4330	-71	--	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
0	1	201236	86829	37951	19516	9213	462	19.1	3.80	>100		3.80

Asia : 8005 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
178	1	-4541	-233	-1063	4	-1724	463	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
178	1	201236	86810	37943	19516	9213	462	35.7	6.21	>100		6.21

Asia : 8005 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
178	1	-3842	-50	-502	5	-2859	557	--	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
178	1	201236	86708	37898	19516	9213	462	75.4	4.42	89.6		4.42

Asia : 8005 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
151	1	-3147	26	-448	-5	-3741	585	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
151	1	201236	86716	37901	19516	9213	462	84.5	3.69	91.5		3.69

Asia : 8005 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
15	1	-2836	113	-246	4	-3749	598	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
15	1	201236	86758	37920	19516	9213	462	>100	3.69	>100		3.69

Asia : 8005 [0 , 69]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	-2316	185	49	1	-3846	516	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
0	1	201236	87033	38040	19516	9213	462	>100	3.78	>100		3.78

Asia : 8005 [69 , 70]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	-1927	162	404	1	-3528	539	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
0	1	201236	86985	38019	19516	9213	462	94.2	4.40	>100		4.40

Asia : 8005 [70 , 395]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*		
0	1	-1752	146	752	-5	-2810	201	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	MZ	Mv4	Mz4	SF	Mt	SF
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*	kg*	kg*	kg*	kg*
0	1	201236	86718	37903	19516	9213	462	50.4	5.73	92.1		5.73

Asia : 8005 [395 , 396]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm	kg	kg	kg	kg	kg*	kg*	kg*	kg*		

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-988	15	943	-5	-1951	54	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86683	37887	19516	9213	462	40.2	9.03	84.3	9.03

Asta : 8005 [396 , 332]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	22	48	1946	-12	2592	-26	--	--	(12+13)-III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	86221	37685	19516	9213	462	19.4	7.36	39.9	7.36

Asta : 8006 [107 , 168]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6423	4	-1966	1	4227	-18	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87032	38040	19516	9213	462	19.3	3.99	>100	3.99

Asta : 8006 [168 , 169]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4086	-205	-1072	3	-1805	474	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86838	37955	19516	9213	462	35.4	6.09	>100	6.09

Asta : 8006 [169 , 170]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-2400	-53	-558	6	-2934	586	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86633	37865	19516	9213	462	67.9	4.43	75.2	4.43

Asta : 8006 [170 , 171]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-1667	30	-347	-6	-3663	609	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
151	1	201236	86669	37881	19516	9213	462	>100	3.81	81.5	3.81

Asta : 8006 [171 , 172]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2249	120	-241	6	-3735	631	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86652	37873	19516	9213	462	>100	3.69	78.4	3.69

Asta : 8006 [172 , 33]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1691	151	145	2	-5811	520	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86978	38016	19516	9213	462	>100	3.85	>100	3.85

Asta : 8006 [33 , 34]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2051	180	439	3	-3448	375	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86898	37981	19516	9213	462	86.5	4.39	>100	4.39

Asta : 8006 [34 , 359]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1885	133	763	-5	-2685	216	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86726	37906	19516	9213	462	49.7	5.87	94.0	5.87

Asta : 8006 [359 , 360]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4860	108	-476	-28	1689	64	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	84930	37121	19516	9213	462	78.0	8.50	16.3	8.50

Asta : 8006 [360 , 333]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	2381	77	2746	-18	2807	-39	--	--	(12+13)-IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	85699	37457	19516	9213	462	13.6	6.26	25.1	6.26

Asia : 8007 [108 , 183]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-8036	-23	-1977	2	4319	-35	--	--	3
X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86964	38010	19516	9213	462	19.2	3.77	>100

Asia : 8007 [183 , 184]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-6145	-181	-1024	4	-1636	470	--	--	8
X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	201236	86811	37943	19516	9213	462	37.0	6.05	>100

Asia : 8007 [184 , 185]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4765	-36	-484	5	-2661	567	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	201236	86708	37898	19516	9213	462	78.4	4.51	89.7

Asia : 8007 [185 , 186]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-4083	57	-559	-4	-3714	551	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	201236	86769	37925	19516	9213	462	67.9	3.70	>100

Asia : 8007 [186 , 187]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
74	1	-2477	113	-250	5	-3799	509	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
74	1	201236	86749	37916	19516	9213	462	>100	3.81	>100

Asia : 8007 [187 , 39]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2072	177	-80	2	-3891	491	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			

999

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
0	1	201236	86951	38004	19516	9213	462	>100	3.80	>100

Asia : 8007 [39 , 40]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1229	148	310	2	-3698	326	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86961	38009	19516	9213	462	>100	4.33	>100

Asia : 8007 [40 , 365]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1056	126	778	-5	-3096	205	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86698	37893	19516	9213	462	48.7	5.37	87.3

Asia : 8007 [365 , 366]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-398	35	1171	-5	-2235	81	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86755	37919	19516	9213	462	32.4	7.98	>100

Asia : 8007 [366 , 334]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	2404	-102	2705	21	2783	60	--	--	(12+13)*III-4

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	201236	85514	37376	19516	9213	462	13.8	6.21	22.2

Asia : 8008 [109 , 163]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6537	-45	-1885	3	4031	-55	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86835	37954	19516	9213	462	20.1	4.08	>100

Asia : 8008 [163 , 164]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4362	-203	-987	3	-1662	510	--	--	8

1000

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86881	37973	19516	9213	462	38.5	6.16	>100	6.16

Asta.: 8008 [164., 165.]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-3659	-6	-470	4	-2744	527	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86767	37924	19516	9213	462	80.6	4.63	>100	4.63

Asta.: 8008 [165., 166.]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
151	1	-2953	27	-443	-5	-3619	549	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
151	1	201236	86747	37915	19516	9213	462	85.7	3.85	99.6	3.85

Asta.: 8008 [166., 167.]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-2639	117	-285	4	-3633	559	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	201236	86792	37935	19516	9213	462	>100	3.85	>100	3.85

Asta.: 8008 [167., 31.]

Sez. G: HE 240 A L=134.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2111	157	9	2	-3774	466	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86945	38001	19516	9213	462	>100	3.93	>100	3.93

Asta.: 8008 [31., 32.]

Sez. G: HE 240 A L=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1718	152	364	2	-3512	524	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86949	38003	19516	9213	462	>100	4.47	>100	4.47

Asta.: 8008 [32., 352.]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1552	144	728	-5	-2846	197	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86723	37904	19516	9213	462	52.0	5.72	93.2	5.72

Asta.: 8008 [357., 358.]

Sez. G: HE 240 A L=108.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-810	7	953	-5	-2013	51	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86742	37913	19516	9213	462	39.8	8.88	98.2	8.88

Asta.: 8008 [358., 335.]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	-328	5	1691	-1	2198	-3	--	--	(12+13)+II-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	86997	38024	19516	9213	462	22.5	8.73	>100	8.73

Asta.: 8009 [110., 178.]

Sez. G: HE 240 A L=81.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-6509	-50	-1908	1	4068	-1	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87004	38027	19516	9213	462	19.9	4.15	>100	4.15

Asta.: 8009 [178., 179.]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-4357	-177	-993	3	-1685	533	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86901	37982	19516	9213	462	38.3	6.03	>100	6.03

Asta.: 8009 [179., 180.]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-3662	-1	-469	6	-2768	541	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86663	37878	19516	9213	462	80.8	4.57	80.4	4.57

Asta.: 8009 [180., 181.]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-2971	42	-432	-4	-3629	543	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
151	1	201236	86774	37927	19516	9213	462	87.9	3.85	>100	3.85

Asta : 8009 [181 , 182]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
15	1	-2667	120	-271	5	-3642	552	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
15	1	201236	86742	37913	19516	9213	462	>100	3.85	98.4	3.85

Asta : 8009 [182 , 37]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2142	149	19	3	-3763	453	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86894	37979	19516	9213	462	>100	3.96	>100	3.96

Asta : 8009 [37 , 38]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1751	149	368	2	-3487	319	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86933	37996	19516	9213	462	>100	4.50	>100	4.50

Asta : 8009 [38 , 363]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1586	143	723	-5	-2817	196	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86729	37907	19516	9213	462	52.4	5.76	94.7	5.76

Asta : 8009 [363 , 364]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-856	8	937	-4	-1989	51	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86759	37920	19516	9213	462	40.5	8.95	>100	8.95

1003

Asta : 8009 [364 , 336]

Sez. G: HE 240 A L=12.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	-381	6	1577	-1	2069	-4	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	86986	38019	19516	9213	462	24.1	9.23	>100	9.23

Asta : 8010 [111 , 153]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4915	-63	-1937	2	4130	-8	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86954	38006	19516	9213	462	19.6	4.05	>100	4.05

Asta : 8010 [153 , 154]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4832	-164	-998	3	-1700	535	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86902	37983	19516	9213	462	38.1	5.91	>100	5.91

Asta : 8010 [154 , 155]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-3540	12	-486	4	-2746	530	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86762	37922	19516	9213	462	78.0	4.63	>100	4.63

Asta : 8010 [155 , 156]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-2850	41	-439	-4	-3617	532	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
151	1	201236	86763	37922	19516	9213	462	86.3	3.89	>100	3.89

Asta : 8010 [156 , 157]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
30	1	-2509	120	-259	4	-3674	524	--	--	8

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X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	201236	86763	37922	19516	9213	462	>100	3.88	>100	3.88

Asia : 8010 [157 , 27]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2011	141	4	3	-3782	439	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86869	37968	19516	9213	462	>100	3.98	>100	3.98

Asia : 8010 [27 , 28]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1620	146	363	2	-3529	316	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86922	37991	19516	9213	462	>100	4.48	>100	4.48

Asia : 8010 [28 , 353]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1459	139	736	-5	-2867	197	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86722	37904	19516	9213	462	51.5	5.70	92.9	5.70

Asia : 8010 [353 , 354]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-716	8	966	-4	-2017	54	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86789	37933	19516	9213	462	39.3	8.87	>100	8.87

Asia : 8010 [354 , 337]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	-41	6	1604	-12	2091	-4	--	--	(12+13)-III-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	86172	37664	19516	9213	462	23.5	9.28	37.9	9.28

Asia : 8011 [112 , 188]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	-6425	-78	-1873	2	3938	-5	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86915	37988	19516	9213	462	20.3	4.27	>100	4.27

Asia : 8011 [188 , 189]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-4318	-173	-962	2	-1706	569	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86917	37989	19516	9213	462	39.5	5.86	>100	5.86

Asia : 8011 [189 , 190]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-3634	41	-447	4	-2750	502	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86779	37929	19516	9213	462	84.9	4.68	>100	4.68

Asia : 8011 [190 , 191]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
151	1	-2960	37	-411	-4	-3580	506	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
151	1	201236	86818	37946	19516	9213	462	92.3	3.95	>100	3.95

Asia : 8011 [191 , 192]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-2660	119	-260	4	-3592	513	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
15	1	201236	86825	37949	19516	9213	462	>100	3.95	>100	3.95

Asia : 8011 [192 , 41]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:*Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2148	127	23	3	-3702	408	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86874	37971	19516	9213	462	>100	4.09	>100	4.09

Asia : 8011 [41 , 42]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

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Asia : 8012 [194 , 195]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1767	138	361	2	-3424	302	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86928	37994	19516	9213	462	>100	4.61	>100	4.61

Asia : 8011 [42 , 367]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1607	141	701	-5	-2767	191	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86700	37894	19516	9213	462	54.0	5.87	87.8	5.87

Asia : 8011 [367 , 368]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-903	-1	900	-4	-1966	46	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86815	37945	19516	9213	462	42.2	9.07	>100	9.07

Asia : 8011 [368 , 338]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	-230	10	1629	-3	2094	-4	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	86902	37983	19516	9213	462	23.3	9.18	>100	9.18

Asia : 8012 [113 , 193]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-6665	-75	-1909	0	4018	51	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87096	38067	19516	9213	462	19.9	4.09	>100	4.09

Asia : 8012 [193 , 194]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-4374	-146	-1025	2	-1808	579	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86914	37988	19516	9213	462	37.1	5.64	>100	5.64

Asia : 8012 [194 , 195]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-2398	34	-547	5	-2872	536	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86737	37911	19516	9213	462	69.3	4.60	96.9	4.60

Asia : 8012 [195 , 196]

Sez. G: HE 240 A L=151.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
151	1	-1684	54	-376	-4	-3648	519	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
151	1	201236	86792	37935	19516	9213	462	>100	3.98	>100	3.98

Asia : 8012 [196 , 197]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1761	125	-257	5	-3661	549	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86745	37914	19516	9213	462	>100	3.91	99.2	3.91

Asia : 8012 [197 , 43]

Sez. G: HE 240 A L=134.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1211	111	140	4	-3767	418	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86799	37938	19516	9213	462	>100	4.09	>100	4.09

Asia : 8012 [43 , 44]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1835	146	485	3	-3450	329	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86876	37971	19516	9213	462	78.2	4.51	>100	4.51

Asia : 8012 [44 , 369]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: *Verificato*

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1693	117	806	-5	-2644	209	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
0	1	201236	86686	37888	19516	9213	462	47.0	6.00	84.8	6.00

Asia : 8012 [369 , 370]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4672	117	-639	-28	1790	85	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	84967	37137	19516	9213	462	58.1	8.05	16.6	8.05

Asia : 8012 [370 , 339]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	2238	87	2698	-19	2791	-43	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	85614	37420	19516	9213	462	13.9	6.30	23.7	6.30

Asia : 8013 [114 , 158]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-7460	-97	-1911	1	4027	35	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87010	38030	19516	9213	462	19.9	4.05	>100	4.05

Asia : 8013 [158 , 159]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-5671	-137	-961	3	-1673	589	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86893	37979	19516	9213	462	39.5	5.62	>100	5.62

Asia : 8013 [159 , 160]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4373	58	-424	4	-2606	521	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86784	37931	19516	9213	462	89.5	4.72	>100	4.72

Asia : 8013 [160 , 161]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-3719	93	-473	-2	-3529	446	--	--	8

1009

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
151	1	201236	86947	38003	19516	9213	462	80.4	4.04	>100	4.04

Asia : 8013 [161 , 162]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
74	1	-2671	101	-229	3	-3645	410	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
74	1	201236	86877	37972	19516	9213	462	>100	4.09	>100	4.09

Asia : 8013 [162 , 29]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2286	133	-102	4	-3725	390	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86799	37938	19516	9213	462	>100	4.09	>100	4.09

Asia : 8013 [29 , 30]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1177	118	222	2	-3535	285	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86945	38002	19516	9213	462	>100	4.59	>100	4.59

Asia : 8013 [30 , 355]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1006	111	669	-6	-3051	198	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86654	37875	19516	9213	462	56.6	5.47	78.8	5.47

Asia : 8013 [355 , 356]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4817	-115	-239	28	1861	-79	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	84958	37133	19516	9213	462	>100	7.82	16.5	7.82

Asia : 8013 [356 , 340]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

1010

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	2245	-86	2681	19	2743	42	--	--	(12+13)+IV-4
X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	201236	85634	37429	19516	9213	462	14.0	6.40	24.0
0	1	201236	85634	37429	19516	9213	462	14.0	6.40	24.0

Asta : 8014 [115 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6369	-110	-1852	1	3916	34	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	87011	38030	19516	9213	462	20.5	4.24	>100
0	1	201236	87011	38030	19516	9213	462	20.5	4.24	>100

Asta : 8014 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4211	-159	-949	2	-1639	640	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	201236	86958	38007	19516	9213	462	40.0	5.73	>100
0	1	201236	86958	38007	19516	9213	462	40.0	5.73	>100

Asta : 8014 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-3505	93	-464	4	-2716	482	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	201236	86803	37939	19516	9213	462	81.7	4.79	>100
0	1	201236	86803	37939	19516	9213	462	81.7	4.79	>100

Asta : 8014 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-2810	41	-434	-3	-3579	477	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	201236	86861	37965	19516	9213	462	87.4	4.01	>100
0	1	201236	86861	37965	19516	9213	462	87.4	4.01	>100

Asta : 8014 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
15	1	-2506	126	-280	3	-3594	482	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
15	1	201236	86835	37953	19516	9213	462	>100	4.02	>100
0	1	201236	86835	37953	19516	9213	462	>100	4.02	>100

Asta : 8014 [0 , 47]

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Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1985	98	7	4	-3735	361	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86774	37927	19516	9213	462	>100	4.16	>100
0	1	201236	86774	37927	19516	9213	462	>100	4.16	>100

Asta : 8014 [47 , 48]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1600	130	360	2	-3484	290	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86909	37986	19516	9213	462	>100	4.59	>100
0	1	201236	86909	37986	19516	9213	462	>100	4.59	>100

Asta : 8014 [48 , 373]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1443	140	723	-5	-2835	187	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86694	37892	19516	9213	462	52.4	5.79	86.6
0	1	201236	86694	37892	19516	9213	462	52.4	5.79	86.6

Asta : 8014 [373 , 374]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-737	-8	954	-3	-2020	42	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86889	37977	19516	9213	462	39.8	8.95	>100
0	1	201236	86889	37977	19516	9213	462	39.8	8.95	>100

Asta : 8014 [374 , 341]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	186	14	1676	-3	2166	-7	--	--	(12+13)+VII-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	201236	86855	37962	19516	9213	462	22.7	8.88	>100
0	1	201236	86855	37962	19516	9213	462	22.7	8.88	>100

Asta : 8015 [116 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6946	-133	-1934	1	4073	40	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86994	38023	19516	9213	462	19.7	4.04	>100
0	1	201236	86994	38023	19516	9213	462	19.7	4.04	>100

1012

Asia : 8015 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-4882	-113	-992	3	-1729	614		--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m				
178	1	201236	86899	37982	19516	9213	462	38.3	5.57	>100	5.57	

Asia : 8015 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-3482	94	-480	3	-2752	488		--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m				
178	1	201236	86903	37983	19516	9213	462	79.2	4.73	>100	4.73	

Asia : 8015 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m	kg*m			
151	1	-2803	51	-430	-3	-3609	470		--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m	kg*m				
151	1	201236	86835	37953	19516	9213	462	88.2	4.00	>100	4.00	

Asia : 8015 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m	kg*m			
15	1	-2500	126	-271	4	-3623	474		--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m	kg*m				
15	1	201236	86819	37946	19516	9213	462	>100	4.01	>100	4.01	

Asia : 8015 [0 , 57]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1986	93	20	5	-3756	354		--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86733	37909	19516	9213	462	>100	4.15	95.9	4.15	

Asia : 8015 [57 , 58]

Sez. G: HE 240 A L=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	Vyr	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1603	131	372	3	-3489	291		--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86891	37978	19516	9213	462	>100	4.58	>100	4.58	

Asia : 8015 [58 , 383]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m			
0	1	-1447	142	734	-5	-2828	187	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m					
0	1	201236	86704	37896	19516	9213	462	51.6	5.80	88.8	5.80	

Asia : 8015 [383 , 384]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m			
0	1	-713	-9	955	-3	-2000	41	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m					
0	1	201236	86908	37985	19516	9213	462	39.8	9.05	>100	9.05	

Asia : 8015 [384 , 342]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	249	18	1680	-14	2170	-7	--	--	(12+13)-VII-2

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m					
112	1	201236	86022	37598	19516	9213	462	22.4	8.83	32.6	8.83	

Asia : 8016 [117 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m			
0	1	-6438	-133	-1902	1	3978	62	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m					
0	1	201236	87044	38045	19516	9213	462	20.0	4.12	>100	4.12	

Asia : 8016 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m			
178	1	-4298	-141	-975	2	-1734	678	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	MTrd	Mv4	Mz4	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg	kg*m	kg*m					
178	1	201236	86980	38017	19516	9213	462	39.0	5.44	>100	5.44	

Asia : 8016 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m			

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
178	1	-3617	124	-444	4	-2777	467	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86825	37949	19516	9213	462	85.5	4.74	>100	4.74

Asta : 8016 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-2943	51	-404	-3	-3595	444	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
151	1	201236	86901	37982	19516	9213	462	94.0	4.05	>100	4.05

Asta : 8016 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2662	124	-275	3	-3566	465	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86856	37963	19516	9213	462	>100	4.06	>100	4.06

Asta : 8016 [0 , 49]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2125	78	39	5	-3704	324	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86726	37906	19516	9213	462	>100	4.25	94.1	4.25

Asta : 8016 [49 , 50]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1741	123	374	3	-3414	278	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86903	37983	19516	9213	462	>100	4.68	>100	4.68

Asta : 8016 [50 , 375]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1587	138	715	-5	-2753	183	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86683	37887	19516	9213	462	53.0	5.93	84.2	5.93

Asta : 8016 [375 , 376]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-889	-14	910	-2	-1959	39	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86937	37998	19516	9213	462	41.8	9.18	>100	9.18

Asta : 8016 [376 , 343]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	214	16	1702	-4	2211	-8	--	--	(12+13)+VII-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	86815	37945	19516	9213	462	22.3	8.68	>100	8.68

Asta : 8017 [118 , 173]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-7394	-143	-1958	-1	4152	91	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87059	38052	19516	9213	462	19.4	3.86	>100	3.86

Asta : 8017 [173 , 174]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-5023	-113	-1041	1	-1790	683	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86989	38021	19516	9213	462	36.5	5.24	>100	5.24

Asta : 8017 [174 , 175]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-2789	119	-574	4	-2891	495	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86802	37939	19516	9213	462	66.1	4.64	>100	4.64

Asta : 8017 [175 , 176]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²q

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-2065	80	-446	-2	-3769	435	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
151	1	201236	86922	37992	19516	9213	462	85.2	3.99	>100	3.99

Asia : 8017 [176 , 177]

Sez. G: HE 240 A L=147,9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1574	119	-283	4	-3707	461	--	--	8
X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86819	37946	19516	9213	462	>100	4.04	>100 4.04

Asia : 8017 [177 , 35]

Sez. G: HE 240 A L=134,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1017	92	143	6	-3857	329	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86659	37877	19516	9213	462	>100	4.19	79.6 4.19

Asia : 8017 [35 , 36]

Sez. G: HE 240 A L=122,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1784	124	572	3	-3541	296	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86903	37983	19516	9213	462	66.4	4.49	>100 4.49

Asia : 8017 [36 , 36]

Sez. G: HE 240 A L=113,2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1656	105	902	-6	-2645	200	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	86651	37873	19516	9213	462	42.0	6.04	78.3 6.04

Asia : 8017 [36 , 36]

Sez. G: HE 240 A L=108,1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-4855	125	-687	-27	1893	108	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	85061	37178	19516	9213	462	54.1	7.53	17.3 7.53

Asia : 8017 [36 , 344]

Sez. G: HE 240 A L=112,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	2290	90	2766	-20	2894	-44	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			

1017

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
112	1	201236	85544	37389	19516	9213	462	13.5	6.08	22.6 6.08

Asia : 8018 [119 , 0]

Sez. G: HE 240 A L=181,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-7125	-161	-1957	1	4142	87	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	201236	87057	38050	19516	9213	462	19.4	3.89	>100 3.89

Asia : 8018 [0 , 0]

Sez. G: HE 240 A L=177,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-5311	-90	-1003	2	-1723	674	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	201236	86959	38008	19516	9213	462	37.9	5.32	>100 5.32

Asia : 8018 [0 , 0]

Sez. G: HE 240 A L=177,6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-3984	134	-442	3	-2689	480	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	201236	86894	37979	19516	9213	462	86.0	4.77	>100 4.77

Asia : 8018 [0 , 0]

Sez. G: HE 240 A L=151,3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-3325	100	-411	-2	-3518	390	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	201236	86975	38015	19516	9213	462	92.4	4.18	>100 4.18

Asia : 8018 [0 , 0]

Sez. G: HE 240 A L=147,8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
30	1	-3007	119	-281	3	-3581	404	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt
cm		kg	kg	kg	kg*	kg*	kg*			
30	1	201236	86884	37975	19516	9213	462	>100	4.13	>100 4.13

Asia : 8018 [0 , 53]

Sez. G: HE 240 A L=134,4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2527	104	-52	6	-3732	309	--	--	8

1018

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86621	37860	19516	9213	462	>100	4.21	73.4	4.21

Asta : 8018 [53 , 54]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1383	89	212	2	-3481	245	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86938	37998	19516	9213	462	>100	4.72	>100	4.72

Asta : 8018 [54 , 379]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1202	95	633	-6	-3022	190	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86622	37860	19516	9213	462	59.8	5.51	73.4	5.51

Asta : 8018 [379 , 380]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-4819	-138	-267	29	1868	-119	--	--	(12+13)-V/III-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	84903	37109	19516	9213	462	>100	7.54	16.1	7.54

Asta : 8018 [380 , 345]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	1509	-57	2095	14	2873	30	--	--	(12+13)-V/III-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	86073	37620	19516	9213	462	18.0	6.33	34.2	6.33

Asta : 8019 [120 , 0]

Sez. G: HE 240 A L=181.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-6612	-167	-1921	-0	4122	95	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	87067	38055	19516	9213	462	19.8	3.93	>100	3.93

Asta : 8019 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-4416	-120	-995	0	-1655	739	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	87060	38052	19516	9213	462	38.3	5.35	>100	5.35

Asta : 8019 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-3692	170	-489	4	-2773	447	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86832	37952	19516	9213	462	77.6	4.79	>100	4.79

Asta : 8019 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
151	1	-2975	62	-458	-2	-3668	405	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
151	1	201236	86947	38002	19516	9213	462	83.0	4.05	>100	4.05

Asta : 8019 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2676	124	-299	3	-3636	424	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86861	37965	19516	9213	462	>100	4.07	>100	4.07

Asta : 8019 [0 , 59]

Sez. G: HE 240 A L=134.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2110	53	33	6	-3811	276	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86648	37872	19516	9213	462	>100	4.24	77.8	4.24

Asta : 8019 [59 , 60]

Sez. G: HE 240 A L=122.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1729	111	405	3	-3534	262	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86864	37966	19516	9213	462	93.7	4.59	>100	4.59

Asta : 8019 [60 , 385]

Sez. G: HE 240 A L=113.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-1566	136	771	-6	-2842	179	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	86680	37886	19516	9213	462	49.1	5.79	83.7	5.79

Asta : 8019 [385 , 386]

Sez. G: HE 240 A L=108.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-816	-21	983	-1	-1996	35	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	86997	38024	19516	9213	462	38.7	9.08	>100	9.08

Asta : 8019 [386 , 346]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
112	1	-47	22	1599	-5	2191	-11	--	--	(12+13)-V-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
112	1	201236	86732	37908	19516	9213	462	23.7	8.80	95.5	8.80

Asta : 8020 [121 , 198]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-7197	-187	-1937	1	4185	131	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	87055	38050	19516	9213	462	19.6	3.78	>100	3.78

Asta : 8020 [198 , 199]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
178	1	-5116	-26	-1057	3	-1757	654	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
178	1	201236	86835	37953	19516	9213	462	35.9	5.36	>100	5.36

Asta : 8020 [199 , 200]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
178	1	-3742	131	-510	0	-2785	451	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
178	1	201236	87081	38061	19516	9213	462	74.7	4.76	>100	4.76

1021

Asta : 8020 [200 , 0]

Sez. G: HE 240 A L=151.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
151	1	-3050	71	-468	-3	-3690	400	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
151	1	201236	86858	37964	19516	9213	462	81.2	4.04	>100	4.04

Asta : 8020 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-2754	124	-295	3	-3658	420	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	86858	37963	19516	9213	462	>100	4.05	>100	4.05

Asta : 8020 [0 , 45]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-2196	52	41	6	-3828	272	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	86625	37862	19516	9213	462	>100	4.23	75.9	4.23

Asta : 8020 [45 , 46]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-1808	107	411	4	-3540	258	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	86829	37951	19516	9213	462	92.4	4.58	>100	4.58

Asta : 8020 [46 , 371]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-1640	134	777	-5	-2838	181	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
0	1	201236	86693	37892	19516	9213	462	48.8	5.77	86.4	5.77

Asta : 8020 [371 , 372]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	-859	-16	986	-1	-1981	42	--	--	9

1022

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87011	38030	19516	9213	462	38.6	9.07	>100	9.07

Asta : 8020 [372 , 347]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	-139	-59	1613	13	2202	26	--	--	(12+13)>V1-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	86144	37651	19516	9213	462	23.3	8.60	36.7	8.60

Asta : 8021 [122 , 0]

Sez. G: HE 240 A L=181.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6533	-196	-1931	-1	4212	109	--	--	3

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87041	38044	19516	9213	462	19.7	3.84	>100	3.84

Asta : 8021 [0 , 0]

Sez. G: HE 240 A L=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4406	-91	-1048	-1	-1701	762	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	87039	38043	19516	9213	462	36.3	5.21	>100	5.21

Asta : 8021 [0 , 0]

Sez. G: HE 240 A L=177.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-3752	183	-492	3	-2810	447	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86838	37955	19516	9213	462	77.2	4.74	>100	4.74

Asta : 8021 [0 , 0]

Sez. G: HE 240 A L=151.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-3068	77	-454	-2	-3688	383	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
151	1	201236	86939	37999	19516	9213	462	83.7	4.07	>100	4.07

Asta : 8021 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			

1023

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
15	1	-2737	119	-257	4	-3696	383	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
15	1	201236	86831	37952	19516	9213	462	>100	4.09	>100	4.09

Asta : 8021 [0 , 61]

Sez. G: HE 240 A L=134.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2213	45	42	7	-3821	258	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86596	37849	19516	9213	462	>100	4.26	69.7	4.26

Asta : 8021 [61 , 62]

Sez. G: HE 240 A L=122.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1821	103	406	4	-3531	252	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86800	37938	19516	9213	462	93.5	4.60	>100	4.60

Asta : 8021 [62 , 387]

Sez. G: HE 240 A L=113.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1650	137	773	-5	-2834	180	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86693	37891	19516	9213	462	49.0	5.78	86.3	5.78

Asta : 8021 [387 , 388]

Sez. G: HE 240 A L=108.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-904	-22	983	-1	-1978	35	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87025	38037	19516	9213	462	38.7	9.12	>100	9.12

Asta : 8021 [388 , 348]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	-179	-51	1662	12	2285	26	--	--	(12+13)>V1-2

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	86171	37663	19516	9213	462	22.7	8.28	37.8	8.28

Asta : 8022 [123 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

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Asia : 8022 [51 , 52]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²
: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1844	96	386	4	-3484	244	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86781	37930	19516	9213	462	98.2	4.67	>100	4.67

Asia : 8022 [52 , 377]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1667	138	744	-6	-2813	180	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86670	37881	19516	9213	462	50.9	5.82	81.7	5.82

Asia : 8022 [377 , 378]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-913	-22	973	-0	-1991	38	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87064	38054	19516	9213	462	39.1	9.03	>100	9.03

Asia : 8022 [378 , 349]

Sez. G: HE 240 A L=12.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	-52	-59	1758	12	2354	26	--	--	(12+13)-VI-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	86175	37665	19516	9213	462	21.4	8.09	38.0	8.09

Asia : 8023 [124 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6497	-238	-1934	1	4130	103	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87036	38041	19516	9213	462	19.7	3.92	>100	3.92

Asia : 8023 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4416	-39	-1055	-1	-1789	744	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				

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: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6939	-220	-1840	0	3977	127	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87096	38068	19516	9213	462	20.7	3.97	>100	3.97

Asia : 8022 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4884	-17	-1009	1	-1703	696	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	87032	38040	19516	9213	462	37.7	5.35	>100	5.35

Asia : 8022 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-3763	176	-485	1	-2742	432	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86991	38022	19516	9213	462	78.5	4.85	>100	4.85

Asia : 8022 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-3086	72	-454	-2	-3614	374	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
151	1	201236	86909	37986	19516	9213	462	83.7	4.15	>100	4.15

Asia : 8022 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2779	125	-293	3	-3582	392	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86870	37969	19516	9213	462	>100	4.17	>100	4.17

Asia : 8022 [0 , 51]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2236	35	33	7	-3758	239	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86575	37840	19516	9213	462	>100	4.36	66.9	4.36

1025

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
178	1	201236	87052	38049	19516	9213	462	36.1	5.15	>100	5.15

Asia : 8023 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-3799	206	-469	2	-2850	386	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86948	38003	19516	9213	462	81.0	4.84	>100	4.84

Asia : 8023 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
151	1	-3156	58	-418	-1	-3667	342	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
151	1	201236	86991	38022	19516	9213	462	91.0	4.15	>100	4.15

Asia : 8023 [0 , 0]

Sez. G: HE 240 A L=147.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2867	127	-246	2	-3635	358	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86980	38017	19516	9213	462	>100	4.18	>100	4.18

Asia : 8023 [0 , 55]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-2346	15	74	7	-3744	196	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86591	37847	19516	9213	462	>100	4.45	69.0	4.45

Asia : 8023 [55 , 56]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1963	84	406	4	-3417	225	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86789	37933	19516	9213	462	93.4	4.78	>100	4.78

Asia : 8023 [56 , 381]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1790	136	735	-6	-2723	174	--	--	8

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86617	37858	19516	9213	462	51.5	5.98	72.7	5.98

Asia : 8023 [381 , 382]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1025	-36	924	0	-1921	26	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87093	38066	19516	9213	462	41.2	9.40	>100	9.40

Asia : 8023 [382 , 350]

Sez. G: HE 240 A L=112.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	21	-49	1865	12	2516	26	--	--	(12+13)+V1-2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	86199	37675	19516	9213	462	20.2	7.58	39.0	7.58

Asia : 8024 [125 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-6459	-276	-1757	1	3561	63	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	87014	38032	19516	9213	462	21.6	4.52	>100	4.52

Asia : 8024 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-4288	-18	-1001	-3	-1911	739	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86872	37970	19516	9213	462	37.9	5.01	>100	5.01

Asia : 8024 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
178	1	-2446	170	-530	1	-2942	450	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
178	1	201236	86986	38020	19516	9213	462	71.7	4.72	>100	4.72

Asia : 8024 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

: **Verificato**

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
151	1	-1730	104	-368	-2	-3679	349	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
151	1	201236	86937	37998	19516	9213	462	>100	4.25	>100	4.25

Asia : 8024 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1617	126	-149	2	-3673	392	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86911	37987	19516	9213	462	>100	4.19	>100	4.19

Asia : 8024 [0 , 63]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1080	24	282	9	-3639	239	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86453	37786	19516	9213	462	>100	4.59	54.2	4.59

Asia : 8024 [63 , 64]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-2522	91	632	5	-3244	264	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86718	37902	19516	9213	462	60.0	4.82	91.9	4.82

Asia : 8024 [64 , 389]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-1339	103	769	-7	-2393	205	--	--	9

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	86583	37843	19516	9213	462	49.2	6.60	67.9	6.60

Asia : 8024 [389 , 390]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-4948	110	-896	-24	1872	80	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	85260	37265	19516	9213	462	41.6	7.74	19.2	7.74

Asia : 8024 [390 , 351]

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Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
112	1	1267	101	2509	-21	2969	-50	--	--	(12+13)+VI-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
112	1	201236	85465	37355	19516	9213	462	14.9	6.10	21.5	6.10

Asia : 8025 [126 , 0]

Sez. G: HE 240 A L=181.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-337	-332	-1034	16	2557	-127	--	--	(12+13)+VI-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	201236	85893	37542	19516	9213	462	36.3	6.83	29.1	6.83

Asia : 8025 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
178	1	-3076	-35	-692	-6	-1494	811	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
178	1	201236	86659	37877	19516	9213	462	54.7	5.56	79.7	5.56

Asia : 8025 [0 , 0]

Sez. G: HE 240 A L=177.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
71	1	-3175	198	-427	5	-1849	676	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
71	1	201236	86698	37894	19516	9213	462	88.8	5.44	87.4	5.44

Asia : 8025 [0 , 0]

Sez. G: HE 240 A L=151.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
151	1	-2721	120	-338	-1	-2872	339	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
151	1	201236	87017	38033	19516	9213	462	>100	5.06	>100	5.06

Asia : 8025 [0 , 0]

Sez. G: HE 240 A L=147.9 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm²

:**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
30	1	-2181	130	-295	3	-2906	364	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	201236	86852	37961	19516	9213	462	>100	5.02	>100	5.02

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Asta : 8025 [0 , 67]

Sez. G: HE 240 A L=134.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1936	80	-191	11	-3144	251	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86301	37720	19516	9213	462	>100	5.05	43.9	5.05

Asta : 8025 [67 , 68]

Sez. G: HE 240 A L=122.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-205	56	-14	5	-3072	204	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86732	37908	19516	9213	462	>100	5.54	95.5	5.54

Asta : 8025 [68 , 393]

Sez. G: HE 240 A L=113.2 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-123	84	358	-8	-2956	183	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	86511	37812	19516	9213	462	>100	5.82	59.6	5.82

Asta : 8025 [393 , 394]

Sez. G: HE 240 A L=108.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	4350	183	712	-22	-1854	205	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	201236	85404	37328	19516	9213	462	52.4	7.20	20.8	7.20

Asta : 8025 [394 , 352]

Sez. G: HE 240 A L=112.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq

: **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
112	1	3215	-68	2512	17	2188	22	--	--	(12+13)+VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
112	1	201236	85831	37515	19516	9213	462	14.9	7.67	27.7	7.67

Asta : 8028 [101 , 102]

Sez. G: IPE 100 L=89.7 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
78	1	-1293	-139	62	-0	0	71	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				

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X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
78	1	27037	9477	7686	1033	240	27	68.2	2.92	>100	2.92

Asta : 8028 [102 , 103]

Sez. G: IPE 100 L=89.6 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-3242	126	-35	-0	0	58	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9475	7684	1033	240	27	75.1	2.78	>100	2.78

Asta : 8028 [103 , 104]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
89	1	-3013	67	32	-0	0	-37	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9476	7685	1033	240	27	>100	3.74	>100	3.74

Asta : 8028 [104 , 105]

Sez. G: IPE 100 L=89.3 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1387	111	-35	-0	0	50	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9478	7687	1033	240	27	85.5	3.83	>100	3.83

Asta : 8028 [105 , 106]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1260	92	-35	-0	0	42	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9476	7685	1033	240	27	>100	4.54	>100	4.54

Asta : 8028 [106 , 107]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
89	1	-1163	100	35	-0	0	-46	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9475	7685	1033	240	27	94.7	4.27	>100	4.27

Asta : 8028 [107 , 108]

Sez. G: IPE 100 L=90.4 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
90	1	-2627	-57	89	0	0	43	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	27037	9480	7688	1033	240	27	86.5	3.62	>100	3.62

Asta : 8028 [108 , 109]

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Sez. G: IPE 100 L=88.8 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
0	1	-3318	134	-31	-0	0	61	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	27037	9474	7684	1033	240	27	71.0	2.66	>100	2.66

Asia: 8028 [109, 110]

Sez. G: IPE 100 L=89.8 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
90	1	-3075	78	35	-0	0	-37	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
90	1	27037	9476	7685	1033	240	27	>100	3.75	>100	3.75

Asia: 8028 [110, 111]

Sez. G: IPE 100 L=89.7 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
0	1	-2913	68	-29	-0	0	31	--	--	(12+13)-IV-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	27037	9478	7686	1033	240	27	>100	4.22	>100	4.22

Asia: 8028 [111, 112]

Sez. G: IPE 100 L=89.2 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
0	1	-4162	31	-81	-0	0	24	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	27037	9479	7688	1033	240	27	95.4	3.92	>100	3.92

Asia: 8028 [112, 113]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
89	1	-3410	-100	34	0	0	46	--	--	(12+13)-VI-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
89	1	27037	9476	7685	1033	240	27	94.5	3.13	>100	3.13

Asia: 8028 [113, 114]

Sez. G: IPE 100 L=89.6 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
90	1	-3426	-53	84	0	0	40	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
90	1	27037	9480	7688	1033	240	27	91.8	3.39	>100	3.39

Asia: 8028 [114, 115]

Sez. G: IPE 100 L=89.9 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
0	1	-3242	91	-27	-0	0	43	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	27037	9476	7685	1033	240	27	>100	3.35	>100	3.35

Asia: 8028 [115, 116]

Sez. G: IPE 100 L=89.2 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
89	1	-4571	-33	95	-0	0	25	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
89	1	27037	9480	7688	1033	240	27	80.6	3.66	>100	3.66

Asia: 8028 [116, 117]

Sez. G: IPE 100 L=88.8 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
0	1	-3041	-74	-27	0	0	-33	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	27037	9476	7685	1033	240	27	>100	3.97	>100	3.97

Asia: 8028 [117, 118]

Sez. G: IPE 100 L=90.0 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
90	1	-3164	-112	33	0	0	52	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
90	1	27037	9476	7685	1033	240	27	84.5	2.99	>100	2.99

Asia: 8028 [118, 119]

Sez. G: IPE 100 L=88.7 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
89	1	-2823	-59	77	0	0	43	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
89	1	27037	9480	7688	1033	240	27	99.7	3.51	>100	3.51

Asia: 8028 [119, 120]

Sez. G: IPE 100 L=89.9 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
0	1	-2692	78	-30	-0	0	36	--	--	(12+13)-VI-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
0	1	27037	9476	7685	1033	240	27	>100	3.99	>100	3.99

Asia: 8028 [120, 121]

Sez. G: IPE 100 L=89.1 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_y k/\gamma M=2619 \text{ kg/cmq}$ fl=4300 kg/cmq **:Verificato**

X	cls	N	TY	TZ	Mt	Mry	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m		
89	1	-2949	-57	87	-0	0	35	--	--	3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m	kg*m			
89	1	27037	9480	7688	1033	240	27	88.6	3.91	>100	3.91

Asia : 8028 [121 , 122]

Sez. G: IPE 100 L=89.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	-1815	-92	29	0	0	41	--	--	(12+13) > VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
89	1	27037	9478	7686	1033	240	27	>100	4.19	>100	4.19

Asia : 8028 [122 , 123]

Sez. G: IPE 100 L=89.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	-1923	-107	29	0	0	48	--	--	(12+13) > VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	27037	9479	7687	1033	240	27	88.4	3.67	>100	3.67

Asia : 8028 [123 , 124]

Sez. G: IPE 100 L=89.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-3070	-89	-35	0	0	-40	--	--	(12+13) > VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9476	7685	1033	240	27	>100	3.55	>100	3.55

Asia : 8028 [124 , 125]

Sez. G: IPE 100 L=89.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	-3428	-124	29	0	0	56	--	--	(12+13) > VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
90	1	27037	9475	7684	1033	240	27	76.1	2.77	>100	2.77

Asia : 8028 [125 , 126]

Sez. G: IPE 100 L=89.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-1870	81	-36	-0	0	41	--	--	(12+13) > VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9467	7678	1033	240	27	>100	4.17	>100	4.17

Asia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-146	50	-63	0	0	42	--	--	(12+13) > II-2	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9474	7684	1033	240	27	>100	5.48	>100	5.48

Asia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.6 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-351	133	-64	-0	0	73	--	--	(12+13) > II-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9475	7685	1033	240	27	71.1	3.13	>100	3.13

Asia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-996	36	-166	0	0	34	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	46.3	5.60	>100	5.60

Asia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
29	1	-1243	17	-73	-0	-36	19	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
29	1	27037	9480	7689	1033	240	27	>100	6.20	>100	6.20

Asia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.1 cm Crit.: Acciaio_Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
29	1	-1445	14	-73	-0	-36	23	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
29	1	27037	9480	7689	1033	240	27	>100	5.48	>100	5.48

Asia : 8029 [0 , 168]

Sez. G: IPE 100 L=94.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
95	1	-383	123	68	-0	0	-72	--	--	(12+13) > VI-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
95	1	27037	9475	7684	1033	240	27	77.2	3.17	>100	3.17

Asia : 8029 [168 , 183]

Sez. G: IPE 100 L=96.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
87	1	-1780	-31	146	0	-16	30	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
87	1	27037	9480	7688	1033	240	27	52.5	4.81	>100	4.81

Asia : 8029 [183 , 163]

Sez. G: IPE 100 L=94.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-465	129	-66	-0	0	74	--	--	(12+13) > VI-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9476	7685	1033	240	27	73.5	3.08	>100	3.08

Asia : 8029 [153 , 188]

Sez. G: IPE 100 L=95.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
48	1	-2087	4	1	0	-40	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
48	1	27037	9480	7688	1033	240	27	>100	5.26	>100	5.26

Asia : 8029 [188 , 193]

Sez. G: IPE 100 L=95.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	-754	-119	60	0	0	67	--	--	(12+13)>V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	27037	9476	7685	1033	240	27	79.4	3.23	>100	3.23

Asia : 8029 [193 , 158]

Sez. G: IPE 100 L=95.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	-2139	-34	153	0	0	34	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	27037	9480	7688	1033	240	27	50.2	4.51	>100	4.51

Asia : 8029 [158 , 0]

Sez. G: IPE 100 L=95.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-763	-112	-61	0	0	-67	--	--	(12+13)>V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9475	7684	1033	240	27	85.0	3.25	>100	3.25

Asia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
86	1	-2110	-26	124	-0	-13	26	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
86	1	27037	9480	7688	1033	240	27	62.1	4.97	>100	4.97

Asia : 8029 [0 , 0]

Sez. G: IPE 100 L=94.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
66	1	-2023	-11	62	0	-31	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
66	1	27037	9481	7689	1033	240	27	>100	5.51	>100	5.51

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Asia : 8029 [0 , 173]

Sez. G: IPE 100 L=96.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	-757	-125	61	0	0	73	--	--	(12+13)>V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	27037	9476	7685	1033	240	27	75.8	3.01	>100	3.01

Asia : 8029 [173 , 0]

Sez. G: IPE 100 L=94.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	-1874	-41	157	0	0	38	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	27037	9480	7688	1033	240	27	48.9	4.40	>100	4.40

Asia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-668	-118	-64	0	0	-69	--	--	(12+13)>V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9475	7685	1033	240	27	80.5	3.21	>100	3.21

Asia : 8029 [0 , 198]

Sez. G: IPE 100 L=95.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	-1615	-37	160	-0	0	35	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	27037	9480	7688	1033	240	27	48.0	4.84	>100	4.84

Asia : 8029 [198 , 0]

Sez. G: IPE 100 L=95.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	-1380	-41	162	0	0	35	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	27037	9481	7689	1033	240	27	47.5	5.08	>100	5.08

Asia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
77	1	-1200	-26	100	0	-26	25	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
77	1	27037	9480	7688	1033	240	27	76.7	5.70	>100	5.70

Asia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
95	1	-920	-65	166	-0	0	50	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	27037	9480	7688	1033	240	27	46.2	4.11	>100	4.11

Astia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
96	1	-355	-134	66	0	0	74	--	--	(12+13)+VL-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
96	1	27037	9475	7684	1033	240	27	70.6	3.11	>100	3.11

Astia : 8029 [0 , 0]

Sez. G: IPE 100 L=95.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
95	1	-318	-67	171	0	0	43	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
95	1	27037	9470	7680	1033	240	27	45.0	5.20	>100	5.20

Astia : 8029 [163 , 178]

Sez. G: IPE 100 L=95.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
48	1	-1986	-4	1	-0	-42	13	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
48	1	27037	9481	7689	1033	240	27	>100	5.98	>100	5.98

Astia : 8029 [178 , 153]

Sez. G: IPE 100 L=95.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
48	1	-2053	-4	1	-0	-42	18	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
48	1	27037	9481	7689	1033	240	27	>100	5.18	>100	5.18

Astia : 8030 [0 , 0]

Sez. G: IPE 100 L=101.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
102	1	-246	100	68	-0	0	-80	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
102	1	27037	9466	7677	1033	240	27	94.7	2.92	>100	2.92

Astia : 8030 [0 , 0]

Sez. G: IPE 100 L=101.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	366	-60	-68	0	0	-40	--	--	(12+13)+VL-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9481	7689	1033	240	27	>100	5.57	>100	5.57

Astia : 8030 [0 , 0]

Sez. G: IPE 100 L=101.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	-714	86	-69	-0	0	44	--	--	(12+13)+IV-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9480	7688	1033	240	27	>100	4.75	>100	4.75

Astia : 8030 [0 , 0]

Sez. G: IPE 100 L=101.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	980	51	-70	0	0	34	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9478	7686	1033	240	27	>100	5.61	>100	5.61

Astia : 8030 [0 , 0]

Sez. G: IPE 100 L=101.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
81	1	-45	-25	114	0	-31	27	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
81	1	27037	9480	7688	1033	240	27	67.2	6.98	>100	6.98

Astia : 8030 [0 , 169]

Sez. G: IPE 100 L=100.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
101	1	1278	40	72	-0	0	-41	--	--	(12+13)+II-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
101	1	27037	9477	7686	1033	240	27	>100	4.61	>100	4.61

Astia : 8030 [169 , 184]

Sez. G: IPE 100 L=102.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
103	1	705	-179	72	0	0	96	--	--	(12+13)+VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
103	1	27037	9473	7682	1033	240	27	52.8	2.34	>100	2.34

Astia : 8030 [184 , 164]

Sez. G: IPE 100 L=100.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1222	-33	-70	0	0	-28	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9476	7685	1033	240	27	>100	6.15	>100	6.15

Asia : 8030 [164 , 179]

Sez. G: IPE 100 L=101,8 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	730	-30	-69	-0	0	-26	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7688	1033	240	27	>100	7.39	>100	7.39

Asia : 8030 [179 , 154]

Sez. G: IPE 100 L=101,7 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
102	1	1325	-49	67	-0	0	34	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
102	1	27037	9478	7686	1033	240	27	>100	5.19	>100	5.19

Asia : 8030 [154 , 189]

Sez. G: IPE 100 L=101,1 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	1142	76	-66	0	0	42	--	--	(12+13)-VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7687	1033	240	27	>100	4.64	>100	4.64

Asia : 8030 [189 , 194]

Sez. G: IPE 100 L=101,1 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	987	43	65	-0	0	-34	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	27037	9476	7685	1033	240	27	>100	5.64	>100	5.64

Asia : 8030 [194 , 159]

Sez. G: IPE 100 L=101,5 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	862	175	-65	-0	0	93	--	--	(12+13)-VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9473	7682	1033	240	27	54.0	2.38	>100	2.38

Asia : 8030 [159 , 0]

Sez. G: IPE 100 L=101,8 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	1300	-47	-65	0	0	-38	--	--	(12+13)-VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9477	7686	1033	240	27	>100	4.85	>100	4.85

Asia : 8030 [0 , 0]

Sez. G: IPE 100 L=101,3 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
101	1	368	-45	163	0	0	41	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	27037	9481	7689	1033	240	27	47.0	5.46	>100	5.46

Asia : 8030 [0 , 0]

Sez. G: IPE 100 L=100,9 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	985	61	64	0	0	-32	--	--	(12+13)-VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	27037	9478	7687	1033	240	27	>100	5.85	>100	5.85

Asia : 8030 [0 , 174]

Sez. G: IPE 100 L=102,0 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
102	1	821	46	66	-0	0	-37	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
102	1	27037	9475	7684	1033	240	27	>100	5.40	>100	5.40

Asia : 8030 [174 , 0]

Sez. G: IPE 100 L=100,8 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	852	163	-67	-0	0	84	--	--	(12+13)-VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9473	7682	1033	240	27	58.2	2.62	>100	2.62

Asia : 8030 [0 , 0]

Sez. G: IPE 100 L=101,8 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	1173	-58	-70	0	0	-43	--	--	(12+13)-VI-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9478	7686	1033	240	27	>100	4.49	>100	4.49

Asia : 8030 [0 , 199]

Sez. G: IPE 100 L=101,3 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	862	-85	70	-0	0	48	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
101	1	27037	9478	7687	1033	240	27	>100	4.28	>100	4.28

Asia : 8030 [199 , 0]

Sez. G: IPE 100 L=101,3 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-416	-71	-70	0	0	-50	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9478	7687	1033	240	27	>100	4.43	>100	4.43

Asia : 8030 [0 , 0]

Sez. G: IPE 100 L=101,7 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
92	1	-254	-33	148	0	-17	34	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
92	1	27037	9479	7688	1033	240	27	51.9	6.03	>100	6.03

Asia : 8030 [0 , 0]

Sez. G: IPE 100 L=101,4 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
101	1	-733	-53	183	-0	0	44	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
101	1	27037	9480	7688	1033	240	27	42.1	4.72	>100	4.72

Asia : 8030 [0 , 0]

Sez. G: IPE 100 L=101,6 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
102	1	376	63	72	-0	0	-43	--	--	(12+13)+V1-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
102	1	27037	9479	7687	1033	240	27	>100	5.17	>100	5.17

Asia : 8030 [0 , 0]

Sez. G: IPE 100 L=101,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-218	-105	-72	0	0	-82	--	--	(12+13)+V11-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9466	7677	1033	240	27	90.3	2.87	>100	2.87

Asia : 8031 [0 , 0]

Sez. G: IPE 100 L=107,7 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
108	1	-50	-138	118	-0	0	82	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
108	1	27037	9479	7687	1033	240	27	65.4	2.91	>100	2.91

Asia : 8031 [0 , 0]

Sez. G: IPE 100 L=107,7 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-73	-237	-67	0	0	-136	--	--	(12+13)+V11-1	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9480	7688	1033	240	27	40.0	1.75	>100	1.75

Asia : 8031 [0 , 0]

Sez. G: IPE 100 L=107,1 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	130	-142	70	-0	0	79	--	--	(12+13)+V11-1	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	27037	9479	7687	1033	240	27	66.9	2.99	>100	2.99

Asia : 8031 [0 , 0]

Sez. G: IPE 100 L=107,0 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	186	-149	71	0	0	82	--	--	(12+13)+V11-1	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	27037	9478	7686	1033	240	27	63.4	2.88	>100	2.88

Asia : 8031 [0 , 0]

Sez. G: IPE 100 L=107,3 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	545	-144	-71	-0	0	-82	--	--	(12+13)+V11-1	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9479	7688	1033	240	27	65.9	2.75	>100	2.75

Asia : 8031 [0 , 170]

Sez. G: IPE 100 L=106,7 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	720	-226	71	0	0	130	--	--	(12+13)+V11-1	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
107	1	27037	9478	7686	1033	240	27	42.0	1.76	>100	1.76

Asia : 8031 [170 , 185]

Sez. G: IPE 100 L=109,0 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
109	1	579	-123	180	-0	0	85	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
109	1	27037	9480	7689	1033	240	27	42.8	2.67	>100	2.67

Asia : 8031 [185 , 165]

Sez. G: IPE 100 L=106,4 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	346	-226	-69	0	0	-129	--	--	(12+13)+V11-1	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9478	7686	1033	240	27	42.0	1.81	>100	1.81

Asia : 8031 [165 , 180]

Sez. G: IPE 100 L=107,8 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
108	1	393	-135	67	0	0	78	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	27037	9480	7688	1033	240	27	70.1	2.94	>100	2.94

Asia : 8031 [180, 155]

Sez. G: IPE 100 L=107.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	419	-139	-68	-0	0	-77	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7688	1033	240	27	68.2	2.97	>100	2.97

Asia : 8031 [155, 190]

Sez. G: IPE 100 L=107.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	432	-133	-66	0	0	-74	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9478	7687	1033	240	27	71.3	3.09	>100	3.09

Asia : 8031 [190, 195]

Sez. G: IPE 100 L=107.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
107	1	598	211	64	-0	0	-123	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9476	7685	1033	240	27	44.9	1.87	>100	1.87

Asia : 8031 [195, 160]

Sez. G: IPE 100 L=107.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
107	1	824	-116	162	0	0	80	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9481	7689	1033	240	27	47.4	2.75	>100	2.75

Asia : 8031 [160, 0]

Sez. G: IPE 100 L=107.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	693	210	-65	-0	0	121	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9478	7687	1033	240	27	45.2	1.89	>100	1.89

Asia : 8031 [0, 0]

Sez. G: IPE 100 L=107.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
107	1	628	135	64	0	0	-76	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9480	7688	1033	240	27	70.1	2.95	>100	2.95

Asia : 8031 [0, 0]

Sez. G: IPE 100 L=107.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	600	138	-66	0	0	76	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7688	1033	240	27	68.7	2.93	>100	2.93

Asia : 8031 [0, 175]

Sez. G: IPE 100 L=108.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
108	1	541	210	67	-0	0	-121	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	27037	9477	7686	1033	240	27	45.2	1.91	>100	1.91

Asia : 8031 [175, 0]

Sez. G: IPE 100 L=106.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
107	1	675	-103	172	0	0	72	--	--	8

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9480	7688	1033	240	27	44.8	3.06	>100	3.06

Asia : 8031 [0, 0]

Sez. G: IPE 100 L=107.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	639	219	-71	-0	0	127	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9478	7686	1033	240	27	43.4	1.81	>100	1.81

Asia : 8031 [0, 200]

Sez. G: IPE 100 L=107.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
107	1	500	139	72	-0	0	-77	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9479	7687	1033	240	27	68.1	2.95	>100	2.95

Asia : 8031 [200, 0]

Sez. G: IPE 100 L=107.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
107	1	650	138	73	-0	0	-77	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9479	7688	1033	240	27	68.7	2.89	>100	2.89

Asia : 8031 [0 , 0]

Sez. G: IPE 100 L=107.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	340	144	-73	-0	0	79	--	--	(12+13)>VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9480	7688	1033	240	27	66.0	2.91	>100	2.91

Asia : 8031 [0 , 0]

Sez. G: IPE 100 L=107.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-343	144	-72	0	0	81	--	--	(12+13)>VI-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9478	7687	1033	240	27	65.7	2.85	>100	2.85

Asia : 8031 [0 , 0]

Sez. G: IPE 100 L=107.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	-438	233	74	-0	0	-135	--	--	(12+13)>VI-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
108	1	27037	9478	7687	1033	240	27	40.6	1.73	>100	1.73

Asia : 8031 [0 , 0]

Sez. G: IPE 100 L=107.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	74	-115	189	0	0	76	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
107	1	27037	9477	7686	1033	240	27	40.7	3.13	>100	3.13

Asia : 8032 [0 , 0]

Sez. G: IPE 100 L=113.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
114	1	1243	65	66	0	0	-56	--	--	(12+13)>VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
114	1	27037	9465	7676	1033	240	27	>100	3.60	>100	3.60

Asia : 8032 [0 , 0]

Sez. G: IPE 100 L=113.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	1940	-82	-65	-0	0	-54	--	--	(12+13)>VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9473	7682	1033	240	27	>100	3.38	>100	3.38

Asia : 8032 [0 , 0]

Sez. G: IPE 100 L=113.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
113	1	627	-44	172	0	0	41	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27037	9479	7688	1033	240	27	44.8	5.13	>100	5.13

Asia : 8032 [0 , 0]

Sez. G: IPE 100 L=113.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	717	-42	175	0	0	40	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27037	9480	7688	1033	240	27	43.9	5.18	>100	5.18

Asia : 8032 [0 , 0]

Sez. G: IPE 100 L=113.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	807	-43	182	0	0	42	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27037	9479	7688	1033	240	27	42.3	4.91	>100	4.91

Asia : 8032 [0 , 171]

Sez. G: IPE 100 L=112.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	702	88	69	0	0	-58	--	--	(12+13)>VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
113	1	27037	9476	7685	1033	240	27	>100	3.71	>100	3.71

Asia : 8032 [171 , 186]

Sez. G: IPE 100 L=115.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	1072	103	-70	0	0	60	--	--	(12+13)>VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9469	7679	1033	240	27	92.0	3.45	>100	3.45

Asia : 8032 [186 , 166]

Sez. G: IPE 100 L=112.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	1802	-96	-67	-0	0	-62	--	--	(12+13)>VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9476	7685	1033	240	27	98.4	3.07	>100	3.07

Asia : 8032 [166 , 181]

Sez. G: IPE 100 L=113.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
114	1	1081	-38	166	0	0	37	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
114	1	27037	9479	7688	1033	240	27	46.3	5.15	>100	5.15

Asta : 8032 [181 , 156]

Sez. G: IPE 100 L=113.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
114	1	1161	-36	164	0	0	37	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
114	1	27037	9480	7688	1033	240	27	47.0	5.06	>100	5.06

Asta : 8032 [156 , 191]

Sez. G: IPE 100 L=113.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	1242	-38	161	0	0	39	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	27037	9479	7687	1033	240	27	47.8	4.79	>100	4.79

Asta : 8032 [191 , 196]

Sez. G: IPE 100 L=113.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	1214	94	63	0	0	-62	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	27037	9476	7685	1033	240	27	>100	3.29	>100	3.29

Asta : 8032 [196 , 161]

Sez. G: IPE 100 L=113.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	788	-108	63	-0	0	65	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
113	1	27037	9470	7680	1033	240	27	87.8	3.35	>100	3.35

Asta : 8032 [161 , 0]

Sez. G: IPE 100 L=113.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	1492	-83	-64	-0	0	-53	--	--	(12+13)+VIII-1	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9477	7685	1033	240	27	>100	3.60	>100	3.60

Asta : 8032 [0 , 0]

Sez. G: IPE 100 L=113.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
102	1	1084	-33	131	0	-17	31	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
102	1	27037	9480	7688	1033	240	27	58.7	5.45	>100	5.45

1049

Asta : 8032 [0 , 0]

Sez. G: IPE 100 L=113.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
102	1	1160	-33	131	0	-17	32	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
102	1	27037	9479	7688	1033	240	27	58.6	5.19	>100	5.19

Asta : 8032 [0 , 176]

Sez. G: IPE 100 L=114.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
114	1	1209	72	66	0	0	-44	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
114	1	27037	9476	7685	1033	240	27	>100	4.41	>100	4.41

Asta : 8032 [176 , 0]

Sez. G: IPE 100 L=112.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	697	-122	-67	-0	0	-74	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9470	7680	1033	240	27	77.8	2.99	>100	2.99

Asta : 8032 [0 , 0]

Sez. G: IPE 100 L=113.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	1220	-92	-70	-0	0	-62	--	--	(12+13)+VIII-1	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9476	7685	1033	240	27	>100	3.27	>100	3.27

Asta : 8032 [0 , 0]

Sez. G: IPE 100 L=113.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
91	1	794	-28	113	0	-34	26	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
91	1	27037	9480	7689	1033	240	27	68.2	5.93	>100	5.93

Asta : 8032 [0 , 0]

Sez. G: IPE 100 L=112.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
91	1	849	-24	114	0	-34	24	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
91	1	27037	9480	7689	1033	240	27	67.4	6.09	>100	6.09

Asta : 8032 [0 , 0]

Sez. G: IPE 100 L=113.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

1050

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
91	1	892	-25	117	0	-35	25	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
91	1	27037	9480	7688	1033	240	27	65.8	5.83	>100	5.83

Asta : 8032 [0 , 0]

Sez. G: IPE 100 L=113.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
91	1	947	-27	119	0	-35	27	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
91	1	27037	9479	7688	1033	240	27	64.8	5.45	>100	5.45

Asta : 8032 [0 , 0]

Sez. G: IPE 100 L=113.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
114	1	2040	84	73	0	0	-55	--	--	(12+13):VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
114	1	27037	9473	7683	1033	240	27	>100	3.27	>100	3.27

Asta : 8032 [0 , 0]

Sez. G: IPE 100 L=113.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1296	-65	-72	-0	0	-56	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9465	7676	1033	240	27	>100	3.58	>100	3.58

Asta : 8033 [0 , 0]

Sez. G: IPE 100 L=119,7 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
120	1	-27	-100	114	0	0	70	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
120	1	27037	9477	7686	1033	240	27	67.3	3.42	>100	3.42

Asta : 8033 [0 , 0]

Sez. G: IPE 100 L=119,7 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m			
0	1	20	-158	-65	-0	0	-99	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9472	7682	1033	240	27	59.9	2.42	>100	2.42

Asta : 8033 [0 , 0]

Sez. G: IPE 100 L=119,1 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m			
119	1	360	-118	68	-0	0	72	--	--	(12+13):VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9478	7687	1033	240	27	80.2	3.17	>100	3.17

Asta : 8033 [0 , 0]

Sez. G: IPE 100 L=118.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg	kg*m	kg*m			
119	1	496	-120	69	-0	0	72	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9479	7687	1033	240	27	78.8	3.15	>100	3.15

Asta : 8033 [0 , 0]

Sez. G: IPE 100 L=119,5 cm Crit.: Acciaio Flessione $\gamma M=1,05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	610	-114	-69	-0	0	-71	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9477	7686	1033	240	27	83.3	3.15	>100	3.15

Asta : 8033 [0 , 172]

Sez. G: IPE 100 L=118.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
119	1	733	-158	69	-0	0	97	--	--	(12+13)-VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9473	7682	1033	240	27	60.1	2.32	>100	2.32

Asta : 8033 [172 , 187]

Sez. G: IPE 100 L=121.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
121	1	493	-74	174	-0	0	62	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
121	1	27037	9479	7688	1033	240	27	44.2	3.62	>100	3.62

Asta : 8033 [187 , 167]

Sez. G: IPE 100 L=118.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	117	-159	-67	-0	0	-98	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9473	7682	1033	240	27	59.4	2.41	>100	2.41

Asta : 8033 [167 , 182]

Sez. G: IPE 100 L=119.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
120	1	126	-108	65	0	0	67	--	--	(12+13)+VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
120	1	27037	9478	7686	1033	240	27	87.9	3.51	>100	3.51

Asia : 8033 [182 , 157]

Sez. G: IPE 100 L=119,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	134	-114	-66	-0	0	-69	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9478	7687	1033	240	27	83.2	3.43	>100	3.43

Asia : 8033 [157 , 192]

Sez. G: IPE 100 L=119,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	141	-109	-65	-0	0	-67	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9477	7686	1033	240	27	87.2	3.52	>100	3.52

Asia : 8033 [192 , 197]

Sez. G: IPE 100 L=119,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	432	149	63	0	0	-93	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9473	7683	1033	240	27	63.7	2.48	>100	2.48

Asia : 8033 [197 , 162]

Sez. G: IPE 100 L=119,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	662	-67	160	-0	0	57	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9479	7687	1033	240	27	48.0	3.79	>100	3.79

Asia : 8033 [162 , 0]

Sez. G: IPE 100 L=119,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	482	147	-65	0	0	90	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9473	7683	1033	240	27	64.5	2.54	>100	2.54

Asia : 8033 [0 , 0]

Sez. G: IPE 100 L=119,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	453	112	64	0	0	-69	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9478	7687	1033	240	27	84.8	3.29	>100	3.29

Asia : 8033 [0 , 0]

Sez. G: IPE 100 L=119,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

1053

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
0	1	427	113	-65	0	0	69	--	--	(12+13)-VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7687	1033	240	27	83.7	3.28	>100	3.28

Asia : 8033 [0 , 177]

Sez. G: IPE 100 L=120,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
120	1	388	147	67	0	0	-90	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
120	1	27037	9473	7683	1033	240	27	64.3	2.57	>100	2.57

Asia : 8033 [177 , 0]

Sez. G: IPE 100 L=118,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	528	-59	118	-0	0	52	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9479	7688	1033	240	27	65.2	4.26	>100	4.26

Asia : 8033 [0 , 0]

Sez. G: IPE 100 L=119,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	509	156	-72	0	0	97	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9474	7683	1033	240	27	60.8	2.36	>100	2.36

Asia : 8033 [0 , 0]

Sez. G: IPE 100 L=119,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
120	1	441	115	75	-0	0	-71	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
120	1	27037	9478	7686	1033	240	27	82.7	3.22	>100	3.22

Asia : 8033 [0 , 0]

Sez. G: IPE 100 L=119,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	391	120	76	0	0	-72	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
119	1	27037	9480	7688	1033	240	27	79.1	3.18	>100	3.18

Asia : 8033 [0 , 0]

Sez. G: IPE 100 L=119,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	334	118	-75	0	0	71	--	--	(12+13)-VIII-4	

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X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9480	7688	1033	240	27	80.3	3.26	>100	3.26

Asia : 8033 [0 , 0]

Sez. G: IPE 100 L=119,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	249	119	-75	-0	0	73	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9478	7687	1033	240	27	79.5	3.17	>100	3.17

Asia : 8033 [0 , 0]

Sez. G: IPE 100 L=119,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
120	1	105	160	75	0	0	-100	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
120	1	27037	9472	7681	1033	240	27	59.1	2.38	>100	2.38

Asia : 8033 [0 , 0]

Sez. G: IPE 100 L=119,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
119	1	19	65	75	-0	0	-49	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
119	1	27037	9454	7667	1033	240	27	>100	4.92	>100	4.92

Asia : 8034 [73 , 75]

Sez. G: IPE 100 L=125,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	308	-72	110	0	0	59	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	27037	9475	7684	1033	240	27	69.7	3.88	>100	3.88

Asia : 8034 [75 , 71]

Sez. G: IPE 100 L=125,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	187	-68	163	0	0	59	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	27037	9478	7687	1033	240	27	47.1	3.97	>100	3.97

Asia : 8034 [71 , 65]

Sez. G: IPE 100 L=125,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	157	-68	165	0	0	59	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	27037	9479	7687	1033	240	27	46.6	3.98	>100	3.98

Asia : 8034 [65 , 71]

Sez. G: IPE 100 L=124,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	131	-66	168	0	0	58	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	27037	9478	7687	1033	240	27	45.9	4.07	>100	4.07

Asia : 8034 [77 , 69]

Sez. G: IPE 100 L=125,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	109	-65	174	0	0	57	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	27037	9478	7687	1033	240	27	44.2	4.12	>100	4.12

Asia : 8034 [69 , 33]

Sez. G: IPE 100 L=124,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
124	1	89	-61	167	0	0	54	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
124	1	27037	9478	7687	1033	240	27	45.9	4.40	>100	4.40

Asia : 8034 [33 , 39]

Sez. G: IPE 100 L=127,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
128	1	422	-61	168	0	0	56	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
128	1	27037	9480	7689	1033	240	27	45.9	4.02	>100	4.02

Asia : 8034 [39 , 31]

Sez. G: IPE 100 L=124,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
124	1	316	-63	160	0	0	55	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
124	1	27037	9478	7687	1033	240	27	48.1	4.11	>100	4.11

Asia : 8034 [31 , 37]

Sez. G: IPE 100 L=125,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	315	-61	160	0	0	55	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	27037	9478	7687	1033	240	27	48.1	4.18	>100	4.18

Asia : 8034 [37 , 27]

Sez. G: IPE 100 L=125,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
126	1	318	-60	158	0	0	54	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
126	1	27037	9479	7687	1033	240	27	48.7	4.21	>100	4.21

Astia : 8034 [27., 41]

Sez. G: IPE 100 L=125.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
125	1	326	-61	156	0	0	55	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	27037	9479	7687	1033	240	27	49.4	4.17	>100	4.17

Astia : 8034 [41., 43]

Sez. G: IPE 100 L=125.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
125	1	345	-55	107	0	0	50	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	27037	9478	7686	1033	240	27	72.1	4.51	>100	4.51

Astia : 8034 [43., 29]

Sez. G: IPE 100 L=125.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
125	1	514	-64	155	-0	0	57	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	27037	9481	7689	1033	240	27	49.5	3.89	>100	3.89

Astia : 8034 [29., 47]

Sez. G: IPE 100 L=125.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
126	1	317	-56	107	0	0	52	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
126	1	27037	9478	7686	1033	240	27	71.8	4.40	>100	4.40

Astia : 8034 [47., 57]

Sez. G: IPE 100 L=125.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
126	1	350	-57	108	0	0	52	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
126	1	27037	9478	7687	1033	240	27	71.1	4.34	>100	4.34

Astia : 8034 [57., 49]

Sez. G: IPE 100 L=125.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
125	1	388	-58	109	0	0	53	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	27037	9479	7687	1033	240	27	70.3	4.27	>100	4.27

Astia : 8034 [49., 35]

Sez. G: IPE 100 L=126.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
126	1	433	-52	113	0	0	49	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
126	1	27037	9477	7686	1033	240	27	68.0	4.54	>100	4.54

Astia : 8034 [35., 53]

Sez. G: IPE 100 L=124.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
125	1	363	-65	169	-0	0	58	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	27037	9480	7689	1033	240	27	45.6	3.94	>100	3.94

Astia : 8034 [53., 59]

Sez. G: IPE 100 L=125.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
126	1	-1076	65	70	0	0	-41	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
126	1	27037	9471	7681	1033	240	27	>100	4.74	>100	4.74

Astia : 8034 [59., 45]

Sez. G: IPE 100 L=125.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
126	1	76	-53	127	0	0	50	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
126	1	27037	9478	7687	1033	240	27	60.3	4.76	>100	4.76

Astia : 8034 [45., 61]

Sez. G: IPE 100 L=125.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
125	1	131	-52	130	0	0	49	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	27037	9479	7687	1033	240	27	59.3	4.78	>100	4.78

Astia : 8034 [61., 51]

Sez. G: IPE 100 L=125.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
125	1	188	-52	131	0	0	49	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
125	1	27037	9479	7688	1033	240	27	58.7	4.75	>100	4.75

Asia : 8034 [51..55]

Sez. G: IPE 100 L=125.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	247	-50	130	0	0	48	--		9	

X	cls	Nr	Vyr	Vzr	Mry	Mtz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
126	1	27037	9478	7687	1033	240	27	59.2	4.75	>100	4.75

Asia : 8034 [55..63]

Sez. G: IPE 100 L=125.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	1364	66	74	0	0	-42	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
126	1	27037	9472	7682	1033	240	27	>100	4.46	>100	4.46

Asia : 8034 [63..67]

Sez. G: IPE 100 L=125.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	341	-66	187	-0	0	59	--		8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
125	1	27037	9475	7684	1033	240	27	41.2	3.89	>100	3.89

Asia : 8035 [74..76]

Sez. G: IPE 100 L=131.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	-49	-52	107	0	0	49	--	--	9	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9474	7683	1033	240	27	71.8	4.81	>100	4.81

Asia : 8035 [76..72]

Sez. G: IPE 100 L=131.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
132	1	-75	-49	158	0	0	49	--		8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9477	7686	1033	240	27	48.6	4.86	>100	4.86

Asia : 8035 [72..66]

Sez. G: IPE 100 L=131.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
131	1	-104	-49	160	0	0	48	--		8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9479	7687	1033	240	27	48.2	4.86	>100	4.86

Asia : 8035 [66..78]

Sez. G: IPE 100 L=130.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

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X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
131	1	-135	-49	162	0	0	48	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9478	7687	1033	240	27	47.5	4.83	>100	4.83

Asia : 8035 [78..70]

Sez. G: IPE 100 L=131.7 cm Crit.: Acciaio Flessione $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	-156	-48	168	0	0	48	--	--		8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9478	7687	1033	240	27	45.8	4.85	>100	4.85

Asia : 8035 [70..34]

Sez. G: IPE 100 L=130.3 cm Crit.: Acciaio Flessione $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
130	1	-169	-48	162	0	0	47	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
130	1	27037	9479	7687	1033	240	27	47.5	4.93	>100	4.93

Asia : 8035 [34..40]

Sez. G: IPE 100 L=133.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
134	1	-213	-47	162	0	0	48	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
134	1	27037	9478	7687	1033	240	27	47.4	4.81	>100	4.81

Asia : 8035 [40..32]

Sez. G: IPE 100 L=129.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
130	1	-233	-47	155	0	0	47	--			8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm			kg	kg	kg*m	kg*m	kg*m				
130	1	27037	9479	7688	1033	240	27	49.7	4.87	>100	4.87

Asia : 8035 [32..38]

Sez. G: IPE 100 L=131.8 cm Crit.: Acciaio Flessione $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
132	1	-239	-46	155	0	0	47	--	--		8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg* ^m	kg* ^m	kg* ^m				
132	1	27037	9478	7687	1033	240	27	49.6	4.88	>100	4.88

Asia : 8035 [38..28]

Sez. G: IPE 100 L=131.7 cm Crit.: Acciaio Flessione $\gamma_M=1.05$ fyk/ $\gamma_M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
132	1	-242	-46	153	0	0	47	--	--	8	

1060

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9478	7687	1033	240	27	50.1	4.88	>100	4.88

Asia : 8035 [28 , 42]

Sez. G: IPE 100 L=131,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	-246	-46	151	0	0	47	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9479	7687	1033	240	27	50.8	4.89	>100	4.89

Asia : 8035 [42 , 44]

Sez. G: IPE 100 L=131,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	-239	-44	152	0	0	45	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9477	7686	1033	240	27	50.7	5.07	>100	5.07

Asia : 8035 [44 , 30]

Sez. G: IPE 100 L=131,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	-266	-48	151	0	0	48	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9479	7688	1033	240	27	50.8	4.76	>100	4.76

Asia : 8035 [30 , 48]

Sez. G: IPE 100 L=131,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	-270	-44	153	0	0	45	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9478	7687	1033	240	27	50.4	5.04	>100	5.04

Asia : 8035 [48 , 58]

Sez. G: IPE 100 L=131,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	-258	-45	154	0	0	46	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9478	7686	1033	240	27	49.8	4.99	>100	4.99

Asia : 8035 [58 , 50]

Sez. G: IPE 100 L=131,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	-244	-45	156	0	0	46	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9478	7687	1033	240	27	49.2	5.01	>100	5.01

Asia : 8035 [50 , 36]

Sez. G: IPE 100 L=132,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	-277	-66	64	-0	0	44	--	--	(12+13)+V/III-1	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9474	7683	1033	240	27	>100	5.14	>100	5.14

Asia : 8035 [36 , 54]

Sez. G: IPE 100 L=130,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	-243	-47	166	0	0	47	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9480	7688	1033	240	27	46.4	4.85	>100	4.85

Asia : 8035 [54 , 60]

Sez. G: IPE 100 L=131,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	-203	-42	120	0	0	44	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9477	7686	1033	240	27	64.2	5.23	>100	5.23

Asia : 8035 [60 , 46]

Sez. G: IPE 100 L=131,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	-207	-45	183	0	0	45	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
132	1	27037	9478	7686	1033	240	27	42.0	5.17	>100	5.17

Asia : 8035 [46 , 62]

Sez. G: IPE 100 L=131,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	-153	-43	129	0	0	45	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9478	7687	1033	240	27	59.6	5.20	>100	5.20

Asia : 8035 [62 , 52]

Sez. G: IPE 100 L=131,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	-120	-43	130	0	0	45	--	--	9	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
131	1	27037	9479	7687	1033	240	27	59.0	5.24	>100	5.24

Asia : 8035 [52 , 56]

Sez. G: IPE 100 L=131,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
132	1	-85	-43	129	0	0	45	--	--	9

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
132	1	27037	9478	7686	1033	240	27	59.6	5.26	>100	5.26

Asia : 8035 [56 , 64]

Sez. G: IPE 100 L=131.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
131	1	28	65	73	0	0	-43	--	--	(12+13)>VIII-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
131	1	27037	9476	7685	1033	240	27	>100	5.60	>100	5.60

Asia : 8035 [64 , 68]

Sez. G: IPE 100 L=131.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
131	1	-30	-50	184	-0	0	50	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
131	1	27037	9477	7686	1033	240	27	41.8	4.80	>100	4.80

Asia : 8036 [399 , 0]

Sez. G: IPE 100 L=137.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
96	1	-60	-15	65	0	-46	20	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
96	1	27037	9475	7684	1033	240	27	>100	7.57	>100	7.57

Asia : 8036 [0 , 397]

Sez. G: IPE 100 L=137.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1766	-43	-61	-0	0	-30	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9480	7688	1033	240	27	>100	5.23	>100	5.23

Asia : 8036 [397 , 391]

Sez. G: IPE 100 L=137.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1935	-32	-62	-0	0	-22	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7687	1033	240	27	>100	6.05	>100	6.05

Asia : 8036 [391 , 0]

Sez. G: IPE 100 L=136.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
96	1	-377	-14	65	0	-46	20	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
96	1	27037	9479	7687	1033	240	27	>100	7.00	>100	7.00

Asia : 8036 [0 , 395]

Sez. G: IPE 100 L=137.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
96	1	-504	-13	66	0	-48	20	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
96	1	27037	9479	7687	1033	240	27	>100	6.77	>100	6.77

Asia : 8036 [395 , 359]

Sez. G: IPE 100 L=136.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
95	1	-634	-11	65	0	-47	19	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
95	1	27037	9480	7688	1033	240	27	>100	6.69	>100	6.69

Asia : 8036 [359 , 365]

Sez. G: IPE 100 L=140.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
98	1	-517	-14	67	0	-49	20	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
98	1	27037	9477	7686	1033	240	27	>100	6.62	>100	6.62

Asia : 8036 [365 , 357]

Sez. G: IPE 100 L=135.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1311	-40	-62	-0	0	-28	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7687	1033	240	27	>100	6.11	>100	6.11

Asia : 8036 [357 , 363]

Sez. G: IPE 100 L=137.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
0	1	-1488	-32	-62	-0	0	-22	--	--	(12+13)>VIII-1

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7687	1033	240	27	>100	6.78	>100	6.78

Asia : 8036 [363 , 353]

Sez. G: IPE 100 L=137.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² : **Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*	kg*	kg*			
83	1	-675	-11	33	0	-53	18	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
83	1	27037	9479	7687	1033	240	27	>100	6.62	>100	6.62

Asia : 8036 [353 , 367]

Sez. G: IPE 100 L=137,0 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
82	1	-761	-10	33	0	-52	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
82	1	27037	9480	7688	1033	240	27	>100	6.56	>100	6.56

Asia : 8036 [367 , 369]

Sez. G: IPE 100 L=137,5 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
83	1	-903	-9	33	0	-52	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
83	1	27037	9479	7687	1033	240	27	>100	6.38	>100	6.38

Asia : 8036 [369 , 355]

Sez. G: IPE 100 L=137,2 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
96	1	-656	-12	65	0	-45	20	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
96	1	27037	9477	7686	1033	240	27	>100	6.68	>100	6.68

Asia : 8036 [355 , 373]

Sez. G: IPE 100 L=137,5 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
0	1	-1348	-35	-61	0	-25	--	--	--	(12+13)+VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7687	1033	240	27	>100	6.56	>100	6.56

Asia : 8036 [373 , 383]

Sez. G: IPE 100 L=137,6 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
83	1	-579	-9	33	0	-52	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
83	1	27037	9479	7687	1033	240	27	>100	6.89	>100	6.89

Asia : 8036 [383 , 375]

Sez. G: IPE 100 L=137,3 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
82	1	-748	-8	33	0	-52	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
82	1	27037	9479	7688	1033	240	27	>100	6.63	>100	6.63

Asia : 8036 [375 , 361]

Sez. G: IPE 100 L=138,0 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
83	1	-900	-6	33	0	-54	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
83	1	27037	9479	7687	1033	240	27	>100	6.39	>100	6.39

Asia : 8036 [361 , 379]

Sez. G: IPE 100 L=137,4 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
82	1	-589	-10	34	0	-55	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
82	1	27037	9478	7687	1033	240	27	>100	6.72	>100	6.72

Asia : 8036 [379 , 385]

Sez. G: IPE 100 L=137,4 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
0	1	-1360	-34	-70	-0	-24	--	--	--	(12+13)+VIII-1	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9479	7687	1033	240	27	>100	6.68	>100	6.68

Asia : 8036 [385 , 371]

Sez. G: IPE 100 L=137,8 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
83	1	-374	-7	39	0	-62	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
83	1	27037	9479	7687	1033	240	27	>100	6.84	>100	6.84

Asia : 8036 [371 , 387]

Sez. G: IPE 100 L=137,0 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
82	1	-484	-6	41	0	-64	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
82	1	27037	9479	7687	1033	240	27	>100	6.57	>100	6.57

Asia : 8036 [387 , 377]

Sez. G: IPE 100 L=137,3 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
82	1	-643	-6	42	0	-66	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
82	1	27037	9480	7688	1033	240	27	>100	6.27	>100	6.27

Asia : 8036 [377 , 381]

Sez. G: IPE 100 L=137,7 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$: <i>Verificato</i>											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	Comb.		
cm		kg	kg	kg	kg*	kg*					
138	1	-2350	31	75	0	-22	--	--	--	(12+13)+VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
138	1	27037	9479	7687	1033	240	27	>100	5.58	>100	5.58

Asia : 8036 [381 , 389]

Sez. G: IPE 100 L=137,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
137	1	-2159	43	74	0	0	-30	--	--	(12+13)-VIII-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
137	1	27037	9481	7689	1033	240	27	>100	4.92	>100	4.92

Asia : 8036 [389 , 393]

Sez. G: IPE 100 L=137,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
82	1	-536	-8	42	0	-65	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
82	1	27037	9480	7689	1033	240	27	>100	6.42	>100	6.42

Asia : 8037 [400 , 0]

Sez. G: IPE 100 L=143,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	-12	11	-34	0	-58	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9478	7686	1033	240	27	>100	7.61	>100	7.61

Asia : 8037 [0 , 398]

Sez. G: IPE 100 L=143,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
58	1	-49	10	-34	0	-58	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
58	1	27037	9479	7687	1033	240	27	>100	7.53	>100	7.53

Asia : 8037 [398 , 392]

Sez. G: IPE 100 L=143,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	-83	11	-34	0	-58	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9480	7688	1033	240	27	>100	7.44	>100	7.44

Asia : 8037 [392 , 0]

Sez. G: IPE 100 L=142,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	-123	11	-34	0	-58	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9479	7688	1033	240	27	>100	7.39	>100	7.39

Asia : 8037 [0 , 396]

Sez. G: IPE 100 L=144,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
58	1	-149	12	-35	0	-59	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
58	1	27037	9480	7688	1033	240	27	>100	7.23	>100	7.23

Asia : 8037 [396 , 360]

Sez. G: IPE 100 L=142,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	-171	13	-68	0	-51	20	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9481	7689	1033	240	27	>100	7.18	>100	7.18

Asia : 8037 [360 , 366]

Sez. G: IPE 100 L=146,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
59	1	-209	9	-35	0	-61	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
59	1	27037	9477	7685	1033	240	27	>100	7.14	>100	7.14

Asia : 8037 [366 , 358]

Sez. G: IPE 100 L=141,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	-240	15	-67	-0	-50	21	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
42	1	27037	9480	7688	1033	240	27	>100	7.02	>100	7.02

Asia : 8037 [358 , 364]

Sez. G: IPE 100 L=143,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	-250	13	-68	0	-51	20	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9480	7688	1033	240	27	>100	7.04	>100	7.04

Asia : 8037 [364 , 354]

Sez. G: IPE 100 L=143,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	-257	12	-68	0	-50	20	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9479	7687	1033	240	27	>100	7.06	>100	7.06

Asia : 8037 [354 , 368]

Sez. G: IPE 100 L=143,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4		Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
43	1	-263	14	-67	0	-50	20	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9480	7689	1033	240	27	>100	7.00	>100	7.00

Asia : 8037 [368 , 370]

Sez. G: IPE 100 L=143.6 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-261	14	-68	0	-50	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9480	7688	1033	240	27	>100	6.97	>100	6.97

Asia : 8037 [370 , 356]

Sez. G: IPE 100 L=143.1 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
57	1	-284	11	-34	0	-56	18	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9476	7685	1033	240	27	>100	7.15	>100	7.15

Asia : 8037 [356 , 374]

Sez. G: IPE 100 L=143.4 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-299	16	-67	-0	-49	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9481	7689	1033	240	27	>100	6.86	>100	6.86

Asia : 8037 [374 , 384]

Sez. G: IPE 100 L=143.7 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-283	14	-67	0	-50	20	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9479	7687	1033	240	27	>100	6.94	>100	6.94

Asia : 8037 [384 , 376]

Sez. G: IPE 100 L=143.6 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-263	15	-67	0	-50	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9480	7688	1033	240	27	>100	6.90	>100	6.90

Asia : 8037 [376 , 362]

Sez. G: IPE 100 L=144.0 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-239	16	-68	0	-52	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9480	7688	1033	240	27	>100	6.85	>100	6.85

Asia : 8037 [362 , 380]

Sez. G: IPE 100 L=143.0 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
57	1	-244	12	-34	0	-61	18	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
57	1	27037	9476	7685	1033	240	27	>100	6.97	>100	6.97

Asia : 8037 [380 , 386]

Sez. G: IPE 100 L=143.3 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-246	17	-75	0	-57	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9480	7689	1033	240	27	>100	6.55	>100	6.55

Asia : 8037 [386 , 372]

Sez. G: IPE 100 L=143.9 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-211	16	-81	0	-60	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9479	7687	1033	240	27	94.6	6.53	>100	6.53

Asia : 8037 [372 , 388]

Sez. G: IPE 100 L=143.0 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-176	16	-86	0	-62	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9479	7687	1033	240	27	89.4	6.50	>100	6.50

Asia : 8037 [388 , 378]

Sez. G: IPE 100 L=143.3 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-135	17	-90	0	-64	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9480	7688	1033	240	27	85.7	6.44	>100	6.44

Asia : 8037 [378 , 382]

Sez. G: IPE 100 L=143.7 cm Crit.: Acciaio Flessione $\gamma M=1.05 \text{ fyk}/\gamma M=2619 \text{ kg}/\text{cmq}$ ft=4300 kg/cm q : Verificato										
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
43	1	-89	17	-91	0	-64	21	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
43	1	27037	9479	7688	1033	240	27	84.9	6.51	>100	6.51

Asia : 8037 [382 , 390]

Sez. G: IPE 100 L=143,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
43	1	-32	21	-90	-0	-63	22	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
43	1	27037	9479	7687	1033	240	27	85.6	6.42	>100	6.42

Asia : 8037 [390 , 394]

Sez. G: IPE 100 L=143,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
57	1	-13	12	-46	0	-72	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
57	1	27037	9476	7685	1033	240	27	>100	6.87	>100	6.87

Asia : 8038 [327 , 328]

Sez. G: IPE 100 L=149,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	-79	20	-77	0	0	30	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
0	1	27037	9481	7689	1033	240	27	>100	7.69	>100	7.69

Asia : 8038 [328 , 329]

Sez. G: IPE 100 L=149,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	-88	15	-57	0	-22	23	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	27037	9481	7689	1033	240	27	>100	8.24	>100	8.24

Asia : 8038 [329 , 330]

Sez. G: IPE 100 L=149,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	-95	15	-57	-0	-22	23	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	27037	9481	7689	1033	240	27	>100	8.23	>100	8.23

Asia : 8038 [330 , 331]

Sez. G: IPE 100 L=148,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	-129	14	-56	-0	-22	23	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	27037	9481	7689	1033	240	27	>100	8.22	>100	8.22

Asia : 8038 [331 , 332]

Sez. G: IPE 100 L=150,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
30	1	-116	14	-57	-0	-23	23	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	27037	9481	7689	1033	240	27	>100	8.25	>100	8.25

Asia : 8038 [332 , 333]

Sez. G: IPE 100 L=148,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	-80	14	-56	-0	-22	23	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	27037	9480	7688	1033	240	27	>100	8.37	>100	8.37

Asia : 8038 [333 , 334]

Sez. G: IPE 100 L=152,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
31	1	-195	12	-57	0	-23	22	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
31	1	27037	9479	7688	1033	240	27	>100	8.24	>100	8.24

Asia : 8038 [334 , 335]

Sez. G: IPE 100 L=147,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	-216	14	-55	-0	-22	23	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	27037	9479	7688	1033	240	27	>100	8.11	>100	8.11

Asia : 8038 [335 , 336]

Sez. G: IPE 100 L=149,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	-166	13	-56	-0	-22	22	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	27037	9481	7689	1033	240	27	>100	8.33	>100	8.33

Asia : 8038 [336 , 337]

Sez. G: IPE 100 L=149,6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	-127	12	-56	-0	-22	22	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*	kg*	kg*				
30	1	27037	9481	7689	1033	240	27	>100	8.50	>100	8.50

Asia : 8038 [337 , 338]

Sez. G: IPE 100 L=149,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*	kg*	kg*				
48	1	-137	10	-39	-0	-34	20	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
48	1	27037	9480	7688	1033	240	27	>100	8.37	>100	8.37

Asia : 8038 [338 , 339]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
14	1	-120	15	-68	-0	-11	25	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
14	1	27037	9480	7688	1033	240	27	>100	8.41	>100	8.41

Asia : 8038 [339 , 340]

Sez. G: IPE 100 L=149,1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	-211	10	-36	0	-29	20	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	27037	9479	7688	1033	240	27	>100	8.52	>100	8.52

Asia : 8038 [340 , 341]

Sez. G: IPE 100 L=149,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	-210	12	-55	-0	-22	22	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	27037	9480	7688	1033	240	27	>100	8.36	>100	8.36

Asia : 8038 [341 , 342]

Sez. G: IPE 100 L=149,7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	-165	11	-55	-0	-22	21	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	27037	9481	7689	1033	240	27	>100	8.58	>100	8.58

Asia : 8038 [342 , 343]

Sez. G: IPE 100 L=149,5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	-118	11	-56	-0	-22	21	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
30	1	27037	9480	7688	1033	240	27	>100	8.72	>100	8.72

Asia : 8038 [343 , 344]

Sez. G: IPE 100 L=150,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	-77	11	-38	-0	-30	20	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	27037	9480	7688	1033	240	27	>100	8.80	>100	8.80

Asia : 8038 [344 , 345]

Sez. G: IPE 100 L=149,0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	-161	9	-40	0	-30	19	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	27037	9479	7688	1033	240	27	>100	8.68	>100	8.68

Asia : 8038 [345 , 346]

Sez. G: IPE 100 L=149,3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	-206	10	-43	-0	-32	20	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	27037	9480	7688	1033	240	27	>100	8.34	>100	8.34

Asia : 8038 [346 , 347]

Sez. G: IPE 100 L=149,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	-160	9	-46	-0	-34	19	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	27037	9481	7689	1033	240	27	>100	8.42	>100	8.42

Asia : 8038 [347 , 348]

Sez. G: IPE 100 L=148,9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	-158	9	-48	-0	-35	19	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	27037	9481	7689	1033	240	27	>100	8.37	>100	8.37

Asia : 8038 [348 , 349]

Sez. G: IPE 100 L=149,2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	-135	9	-26	-0	-42	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9480	7688	1033	240	27	>100	8.34	>100	8.34

Asia : 8038 [349 , 350]

Sez. G: IPE 100 L=149,8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	-18	8	-26	-0	-43	18	--	--	8	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9480	7689	1033	240	27	>100	8.65	>100	8.65

Asia : 8038 [350 , 351]

Sez. G: IPE 100 L=149,4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm ² ft=4300 kg/cm ² <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
45	1	48	9	-50	-0	-36	19	--	--	8

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
45	1	27037	9478	7687	1033	240	27	>100	8.54	>100	8.54

Asta : 8038 [351 , 352]

Sez. G: IPE 100 L=149.4 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq}$ $\gamma=4300 \text{ kg/cmq}$ Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	21	6	-25	0	-41	17	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
60	1	27037	9478	7687	1033	240	27	>100	8.85	>100	8.85

Asta : 8039 [54 , 53]

Sez. G: IPE 100 L=89.7 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$ · Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	592	-8	5	0	0	36	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9472	7682	1033	240	27	>100	5.85	>100	5.85

Asta : 8039 [53 , 55]

Sez. G: IPE 100 L=89.6 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$; Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	972	-17	5	0	0	21	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9480	7689	1033	240	27	>100	8.02	>100	8.02

Asta : 8039 [55 , 56]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$; Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	238	9	-5	-0	0	22	--	--	8	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9479	7688	1033	240	27	>100	10.1	>100	10.1

Asta : 8039 [56 , 71]

Sez. G: IPE 100 L=89.3 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$; Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	-1283	-3	5	0	0	10	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	27037	9481	7689	1033	240	27	>100	11.1	>100	11.1

Asta : 8039 [71 , 74]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$; Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
80	1	-1916	-1	4	-0	-0	12	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
80	1	27037	9480	7688	1033	240	27	>100	8.27	>100	8.27

Asta : 8039 [74 , 76]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$ · Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	Mv4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	-2501	25	4	-0	0	-16	--			(12+13)-V1-4

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	27037	9475	7684	1033	240	27	>100	6.32	>100	6.32

Asta : 8039 [76 , 75]

Sez. G: IPE 100 L=90.4 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$ <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	-1981	-19	5	0	0	19	--			3

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9479	7687	1033	240	27	>100	6.47	>100	6.47

Asta : 8039 [75 , 72]

Sez. G: IPE 100 L=88.8 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$ <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-1834	20	-5	-0	0	20	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9476	7685	1033	240	27	>100	6.60	>100	6.60

Asta : 8039 [72 , 70]

Sez. G: IPE 100 L=89.8 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$ Verificato											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	-2250	-6	5	-0	0	10	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9480	7689	1033	240	27	>100	8.01	>100	8.01

Asta : 8039 [70 , 69]

Sez. G: IPE 100 L=89.7 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$ <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	-2622	-4	5	0	0	13	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9481	7689	1033	240	27	>100	6.60	>100	6.60

Asta : 8039 [69 , 77]

Sez. G: IPE 100 L=89.2 cm Crit.: Acciaio Flessione $\gamma M=1.05 f_{yk}/\gamma M=2619 \text{ kg/cmq ft}=4300 \text{ kg/cmq}$ <i>Verificato</i>											
X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.	
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	-2912	9	-5	-0	0	14	--	--	3	

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF V.	SF M	SF Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	27037	9478	7687	1033	240	27	>100	6.07	>100	6.07

Asia : 8039 [77 , 78]

Sez. G: IPE 100 L=89.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
89	1	-3074	19	4	0	-13	--	--	>100	(12+13)÷V1-4	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
89	1	27037	9476	7685	1033	240	27	>100	6.01	>100	6.01	6.01

Asia : 8039 [78 , 73]

Sez. G: IPE 100 L=89.6 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
90	1	-2566	-6	5	0	14	--	--	>100	3	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
90	1	27037	9480	7688	1033	240	27	>100	6.53	>100	6.53	6.53

Asia : 8039 [73 , 61]

Sez. G: IPE 100 L=89.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
0	1	-2808	-19	-4	0	-13	--	--	>100	(12+13)÷V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
0	1	27037	9476	7685	1033	240	27	>100	6.35	>100	6.35	6.35

Asia : 8039 [61 , 62]

Sez. G: IPE 100 L=89.2 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
89	1	-2596	-11	5	0	15	--	--	>100	3	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
89	1	27037	9480	7688	1033	240	27	>100	6.33	>100	6.33	6.33

Asia : 8039 [62 , 63]

Sez. G: IPE 100 L=88.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
0	1	-2664	11	-5	0	14	--	--	>100	3	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
0	1	27037	9480	7688	1033	240	27	>100	6.35	>100	6.35	6.35

Asia : 8039 [63 , 64]

Sez. G: IPE 100 L=90.0 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
90	1	-2661	-17	5	0	18	--	--	>100	3	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
90	1	27037	9479	7687	1033	240	27	>100	5.70	>100	5.70	5.70

Asia : 8039 [64 , 60]

Sez. G: IPE 100 L=88.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					

X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
0	1	-1812	57	-4	0	38	--	--	>100	(12+13)÷V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
0	1	27037	9473	7682	1033	240	27	>100	4.46	>100	4.46	4.46

Asia : 8039 [60 , 57]

Sez. G: IPE 100 L=89.9 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
0	1	-2766	-46	-4	0	-31	--	--	>100	(12+13)÷V1-1	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
0	1	27037	9475	7684	1033	240	27	>100	4.33	>100	4.33	4.33

Asia : 8039 [57 , 59]

Sez. G: IPE 100 L=89.1 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
89	1	-1861	-7	5	0	12	--	--	>100	3	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
89	1	27037	9480	7688	1033	240	27	>100	8.35	>100	8.35	8.35

Asia : 8039 [59 , 65]

Sez. G: IPE 100 L=89.4 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
89	1	-1717	-3	5	0	13	--	--	>100	3	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
89	1	27037	9480	7689	1033	240	27	>100	8.56	>100	8.56	8.56

Asia : 8039 [65 , 58]

Sez. G: IPE 100 L=89.8 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
0	1	-753	5	-5	0	18	--	--	>100	8	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
0	1	27037	9479	7688	1033	240	27	>100	9.71	>100	9.71	9.71

Asia : 8039 [58 , 66]

Sez. G: IPE 100 L=89.3 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
89	1	-747	-15	5	0	24	--	--	>100	8	

X	cls	Nr	Vyr	Vzr	Mry	Mtrz	MTrd	SF	V.	SF	Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m					
89	1	27037	9480	7689	1033	240	27	>100	7.71	>100	7.71	7.71

Asia : 8039 [66 , 67]

Sez. G: IPE 100 L=89.7 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk/γM=2619 kg/cmq ft=4300 kg/cmq : Verificato											
X	cls	N	TY	TZ	MY	MZ	My4	Mz4	SF	Mt	Comb.
cm		kg	kg	kg	kg*m	kg*m					
90	1	-2035	45	4	0	-25	--	--	>100	(12+13)÷V1-4	

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
90	1	27037	9471	7681	1033	240	27	>100	5.55	>100	5.55

Asia - 8039 [67 , 68]

Sez. G: IPE 100 L=89.5 cm Crit.: Acciaio Flessione $\gamma M=1.05$ fyk÷M=2619 kg/cmq ft=4300 kg/cmq .*Verificato*

X	cls	N	TY	IZ	MY	MZ	MTrd	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
89	1	550	55	4	0	-3.5	27	--	--	(12÷13)-Vt-1

X	cls	Nr	Vyr	Vzr	Mrv	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
89	1	27037	9472	7682	1033	240	27	>100	5.96	>100	5.96

Verifica spostamenti verticali delle aste in Acciaio secondo NTC 2008

Scenario di calcolo : Set_NT_SLD_A2_STR/GEO

Travata: 8000 (Travata 8000) [101 (Nodo 101) , 327 (Nodo 327)]

L = 1426.8cm Crit.Prog: Acciaio_Pressflessione $\hat{\alpha} = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: *Verificata*

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
849.5	2	5.98	57.07	9.54

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
889.8	2	2.37	47.56	20.1

Travata: 8001 (Travata 8001) [102 (Nodo 102) , 328 (Nodo 328)]

L = 1427.0cm Crit.Prog: Acciaio_Pressflessione $\hat{\alpha} = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: *Verificata*

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
791.8	2	8.25	57.08	6.92

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
836.1	2	3.45	47.57	13.8

Travata: 8002 (Travata 8002) [103 (Nodo 103) , 329 (Nodo 329)]

L = 1427.3cm Crit.Prog: Acciaio_Pressflessione $\hat{\alpha} = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: *Verificata*

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
806.7	2	8.94	57.09	6.39

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
836.3	2	3.71	47.58	12.8

Travata: 8003 (Travata 8003) [104 (Nodo 104) , 330 (Nodo 330)]

L = 1426.3cm Crit.Prog: Acciaio_Pressflessione $\hat{\alpha} = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: *Verificata*

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
806.3	2	8.83	57.05	6.46

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
835.8	2	3.65	47.54	13.0

Travata: 8004 (Travata 8004) [105 (Nodo 105) , 331 (Nodo 331)]

L = 1426.4cm Crit.Prog: Acciaio_Pressflessione $\hat{\alpha} = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: *Verificata*

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
821.1	2	9.04	57.06	6.31

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
835.9	2	3.79	47.55	12.6

Travata: 8005 (Travata 8005) [106 (Nodo 106) , 332 (Nodo 332)]

L = 1426.7cm Crit.Prog: Acciaio_Pressflessione $\hat{\alpha} = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: *Verificata*

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
821.2	2	9.10	57.07	6.27

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
836.0	2	3.80	47.56	12.5

Travata: 8006 (Travata 8006) [107 (Nodo 107) , 333 (Nodo 333)]

L = 1426.5cm Crit.Prog: Acciaio_Pressflessione $\hat{\alpha} = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: *Verificata*

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
806.4	2	8.86	57.06	6.44

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
821.1	2	3.63	47.55	13.1

Travata: 8007 (Travata 8007) [108 (Nodo 108) , 334 (Nodo 334)]

L = 1426.7cm Crit.Prog: Acciaio_Pressflessione $\hat{\alpha} = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: *Verificata*

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
836.0	2	9.24	57.07	6.18

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
849.5	2	3.89	47.56	12.2

Travata: 8008 (Travata 8008) [109 (Nodo 109) , 335 (Nodo 335)]

L = 1426.1cm Crit.Prog: Acciaio_Pressflessione $\hat{\alpha} = 0.0cm$

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: *Verificata*

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
821.0	2	8.59	57.05	6.64

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
835.8	2	3.61	47.54	13.2

Travata: 8009 (Travata 8009) [110 (Nodo 110), 336 (Nodo 336)]

L = 1426.7cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: **Verificata**

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
821.2	2	8.62	57.07	6.62

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
836.0	2	3.60	47.56	13.2

Travata: 8010 (Travata 8010) [111 (Nodo 111), 337 (Nodo 337)]

L = 1426.7cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: **Verificata**

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
821.2	2	8.74	57.07	6.53

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
836.0	2	3.62	47.56	13.1

Travata: 8011 (Travata 8011) [112 (Nodo 112), 338 (Nodo 338)]

L = 1426.7cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: **Verificata**

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
821.2	2	8.36	57.07	6.83

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
836.0	2	3.46	47.56	13.7

Travata: 8012 (Travata 8012) [113 (Nodo 113), 339 (Nodo 339)]

L = 1427.2cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: **Verificata**

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
806.6	2	8.52	57.09	6.70

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
821.4	2	3.49	47.57	13.6

Travata: 8013 (Travata 8013) [114 (Nodo 114), 340 (Nodo 340)]

L = 1426.5cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: **Verificata**

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
835.9	2	8.57	57.06	6.66

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
862.8	2	3.58	47.55	13.3

Travata: 8014 (Travata 8014) [115 (Nodo 115), 341 (Nodo 341)]

L = 1426.6cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: **Verificata**

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
821.2	2	8.38	57.07	6.81

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
836.0	2	3.50	47.55	13.6

Travata: 8015 (Travata 8015) [116 (Nodo 116), 342 (Nodo 342)]

L = 1426.2cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: **Verificata**

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
821.0	2	8.59	57.05	6.64

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
835.8	2	3.56	47.54	13.4

Travata: 8016 (Travata 8016) [117 (Nodo 117), 343 (Nodo 343)]

L = 1426.8cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: **Verificata**

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
821.3	2	8.39	57.07	6.80

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
836.0	2	3.47	47.56	13.7

Travata: 8017 (Travata 8017) [118 (Nodo 118), 344 (Nodo 344)]

L = 1426.7cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: **Verificata**

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
806.4	2	8.82	57.07	6.47

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
821.2	2	3.62	47.56	13.1

Travata: 8018 (Travata 8018) [119 (Nodo 119), 345 (Nodo 345)]

L = 1426.4cm Crit.Prog: Acciaio_Pressflessione δ̄ = 0.0cm

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

Verifica: **Verificata**

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
821.1	2	8.70	57.06	6.56

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
849.3	2	3.63	47.55	13.1

Travata: 8019 (Travata 8019) [120 (Nodo 120), 346 (Nodo 346)]

L = 1426.0cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
820.9	2	8.74	57.04	6.53

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
835.7	2	3.67	47.53	13.0

Travata: 8020 (Travata 8020) [121 (Nodo 121), 347 (Nodo 347)]

L = 1427.1cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
821.4	2	8.93	57.08	6.39

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
836.2	2	3.69	47.57	12.9

Travata: 8021 (Travata 8021) [122 (Nodo 122), 348 (Nodo 348)]

L = 1427.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
821.5	2	8.92	57.10	6.40

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
836.3	2	3.70	47.58	12.9

Travata: 8022 (Travata 8022) [123 (Nodo 123), 349 (Nodo 349)]

L = 1426.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
821.1	2	8.62	57.06	6.62

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
835.9	2	3.48	47.55	13.7

Travata: 8023 (Travata 8023) [124 (Nodo 124), 350 (Nodo 350)]

L = 1426.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
806.3	2	8.68	57.06	6.58

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
821.1	2	3.53	47.55	13.5

Travata: 8024 (Travata 8024) [125 (Nodo 125), 351 (Nodo 351)]

L = 1426.7cm Crit.Prog: Acciaio_Pressflessione $\delta x = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
776.9	2	7.80	57.07	7.32

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
791.7	2	3.03	47.56	15.7

Travata: 8025 (Travata 8025) [126 (Nodo 126), 352 (Nodo 352)]

L = 1426.7cm Crit.Prog: Acciaio_Pressflessione $\delta x = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
862.9	2	5.79	57.07	9.85

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
916.7	2	2.24	47.56	21.2

Travata: 8028 (Travata 8028) [101 (Nodo 101), 126 (Nodo 126)]

L = 2223.3cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
640.6	2	-0.43	88.93	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
523.6	7	0.20	74.11	>100

Travata: 8029 (Travata 8029) [0 (Nodo 0), 0 (Nodo 0)]

L = 2385.4cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
2289.9	8	0.46	95.42	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
1622.0	8	0.41	79.51	>100

Travata: 8030 (Travata 8030) [0 (Nodo 0), 0 (Nodo 0)]

L = 2535.5cm Crit.Prog: Acciaio_Flessione $\delta x = 0.0cm$ Verifica: **Verificata**

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
2332.4	5	1.44	101.42	70.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
1724.2	5	0.92	84.52	92.1

Travata: 8031 (Travata 8031) [0 (Nodo 0) , 0 (Nodo 0)]

L = 2685.6cm Crit.Prog: Acciaio_Flessione δ̑ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
2470.5	5	2.42	107.42	44.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
1826.3	5	1.39	89.52	64.6

Travata: 8032 (Travata 8032) [0 (Nodo 0) , 0 (Nodo 0)]

L = 2835.6cm Crit.Prog: Acciaio_Flessione δ̑ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
2381.6	5	3.00	113.43	37.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
2381.6	5	1.61	94.52	58.7

Travata: 8033 (Travata 8033) [0 (Nodo 0) , 0 (Nodo 0)]

L = 2985.7cm Crit.Prog: Acciaio_Flessione δ̑ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
837.0	5	3.12	119.43	38.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
837.0	5	1.56	99.52	63.9

Travata: 8034 (Travata 8034) [73 (Nodo 73) , 67 (Nodo 67)]

L = 3135.8cm Crit.Prog: Acciaio_Flessione δ̑ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
879.2	5	2.71	125.43	46.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
879.2	5	1.37	104.53	76.5

Travata: 8035 (Travata 8035) [74 (Nodo 74) , 68 (Nodo 68)]

L = 3285.9cm Crit.Prog: Acciaio_Flessione δ̑ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
921.4	5	1.92	131.44	68.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
921.4	5	1.00	109.53	>100

Travata: 8036 (Travata 8036) [399 (Nodo 399) , 393 (Nodo 393)]

L = 3436.0cm Crit.Prog: Acciaio_Flessione δ̑ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
963.6	2	1.03	137.44	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
3243.6	7	-0.63	114.53	>100

Travata: 8037 (Travata 8037) [400 (Nodo 400) , 394 (Nodo 394)]

L = 3586.1cm Crit.Prog: Acciaio_Flessione δ̑ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
3485.7	7	-0.44	143.44	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
3385.3	7	-0.55	119.54	>100

Travata: 8038 (Travata 8038) [327 (Nodo 327) , 352 (Nodo 352)]

L = 3724.2cm Crit.Prog: Acciaio_Flessione δ̑ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
1563.4	7	-0.45	148.97	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
1563.4	7	-0.54	124.14	>100

Travata: 8039 (Travata 8039) [54 (Nodo 54) , 68 (Nodo 68)]

L = 2235.3cm Crit.Prog: Acciaio_Flessione δ̑ = 0.0cm Verifica: *Verificata*

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC 2008)

x	Comb.	δmax	L/250.00	Cs
cm		mm	mm	
661.5	2	-0.60	89.41	>100

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC 2008)

x	Comb.	82	L/300.00	Cs
cm		mm	mm	
134.6	8	-0.26	74.51	>100

Verifica delle travi (Stati limite esercizio)

Scenario di calcolo : Set NT_SILD_A2_STR/GEO

Trave di Fond. : 9009 [1. , 2] Pilastrate [1. , 2]

Sez. R: By= 60.0 cm Bz=100.0 cm Ln=89.7 cm Terreno: Terreno I

Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma f[kg/cmq]=3600$

X	M+	M-	M- kg*m	Afsup cmq	Afinf cmq	σ_{c+} kg/cmq	$\sigma f+$ kg/cmq	σ_{c-} kg/cmq	$\sigma f-$ kg/cmq	Cb+	Cb-	Ver.	CS
0.0	--	--	510	12.06	12.06	--	--	--	-1	47	7	2	Si 76.5
9.0	--	--	1362	12.06	12.06	--	--	--	-2	126	7	2	Si 28.7
44.9	--	--	4127	12.06	12.06	--	--	--	-6	380	6	8	Si 9.46
80.8	--	--	6089	12.06	12.06	--	--	--	-9	561	6	8	Si 6.41
89.7	--	--	6439	12.06	12.06	--	--	--	-10	593	6	8	Si 6.07

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma f[kg/cmq]=3600$

X	M+	M-	M- kg*m	Afsup cmq	Afinf cmq	σ_{c+} kg/cmq	$\sigma f+$ kg/cmq	σ_{c-} kg/cmq	$\sigma f-$ kg/cmq	Cb+	Cb-	Ver.	CS
0.0	--	--	410	12.06	12.06	--	--	--	-1	38	14	14	Si 95.3
9.0	--	--	794	12.06	12.06	--	--	--	-1	73	14	14	Si 49.2
44.9	--	--	1824	12.06	12.06	--	--	--	-3	168	14	14	Si 21.4
80.8	--	--	2113	12.06	12.06	--	--	--	-3	195	14	14	Si 18.5
89.7	--	--	2082	12.06	12.06	--	--	--	-3	192	14	14	Si 18.8

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Mq	Aft	pAft	S _{max} cm	$\sigma f+$ kg/cmq	σ_{c-} kg/cmq	Wd	Wk	Cb	Ver.	CS
cm	kg*m			cmq	cmq	cm	kg/cmq	kg/cmq	mm	mm			
0.0	349	0.1	12.06	30.16	12.06	22.4	32	0.002	0.002	0.002	13(Fr)	Si	>100
0.0	410	0.1	12.06	30.16	12.06	22.4	38	0.002	0.002	0.002	14(Qp)	Si	>100
9.0	794	0.1	12.06	30.16	12.06	22.4	73	0.005	0.005	0.005	14(Qp)	Si	64.5
9.0	794	0.1	12.06	30.16	12.06	22.4	73	0.005	0.005	0.005	9(Fr)	Si	85.1
44.9	1824	0.1	12.06	30.16	12.06	22.4	168	0.011	0.011	0.011	14(Qp)	Si	27.9
44.9	1824	0.1	12.06	30.16	12.06	22.4	168	0.011	0.011	0.011	9(Fr)	Si	37.2
80.8	2113	0.1	12.06	30.16	12.06	22.4	195	0.012	0.012	0.012	14(Qp)	Si	24.1
80.8	2113	0.1	12.06	30.16	12.06	22.4	195	0.012	0.012	0.012	9(Fr)	Si	32.1
89.7	2082	0.1	12.06	30.16	12.06	22.4	192	0.012	0.012	0.012	14(Qp)	Si	24.5
89.7	2082	0.1	12.06	30.16	12.06	22.4	192	0.012	0.012	0.012	9(Fr)	Si	32.6

Trave di Fond. : 9009 | 2.3 | Pilastro | 2.3 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.6 cm Ln= 89.6 cm Terreno: TerrenoI

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma f[kg/cmq]=3600$

X	M+	M-	M- kg*m	Afsup cmq	Afinf cmq	σ_{c+} kg/cmq	$\sigma f+$ kg/cmq	σ_{c-} kg/cmq	$\sigma f-$ kg/cmq	Cb+	Cb-	Ver.	CS
cm	kg*m			cmq	cmq	cm	kg/cmq	kg/cmq	kg/cmq				
0.0	--	--	6723	12.06	12.06	--	--	--	-10	620	6	8	Si 5.81
9.0	--	--	6687	12.06	12.06	--	--	--	-10	616	6	8	Si 5.84
44.8	--	--	6034	12.06	12.06	--	--	--	-9	556	6	8	Si 6.47
80.7	--	--	4619	12.06	12.06	--	--	--	-7	426	6	8	Si 8.46
89.6	--	--	4153	12.06	12.06	--	--	--	-6	383	6	8	Si 9.41

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma f[kg/cmq]=3600$

X	M+	M-	M- kg*m	Afsup cmq	Afinf cmq	σ_{c+} kg/cmq	$\sigma f+$ kg/cmq	σ_{c-} kg/cmq	$\sigma f-$ kg/cmq	Cb+	Cb-	Ver.	CS
cm	kg*m			cmq	cmq	cm	kg/cmq	kg/cmq	kg/cmq				
0.0	--	--	2488	12.06	12.06	--	--	--	-4	229	14	14	Si 15.7
9.0	--	--	2392	12.06	12.06	--	--	--	-4	220	14	14	Si 16.3
44.8	--	--	1644	12.06	12.06	--	--	--	-3	152	14	14	Si 23.8
80.7	--	--	361	12.06	12.06	--	--	--	-1	33	14	14	Si >100
89.6	37	--	--	12.06	12.06	-0	3	--	--	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Mq	Aft	pAft	S _{max} cm	$\sigma f+$ kg/cmq	σ_{c-} kg/cmq	Wd	Wk	Cb	Ver.	CS
cm	kg*m			cmq	cmq	cm	kg/cmq	kg/cmq	mm	mm			
0.0	2488	0.1	12.06	30.16	12.06	22.4	229	0.015	0.015	0.015	9(Fr)	Si	27.3
0.0	2488	0.1	12.06	30.16	12.06	22.4	229	0.015	0.015	0.015	14(Qp)	Si	20.5
9.0	2392	0.1	12.06	30.16	12.06	22.4	220	0.014	0.014	0.014	14(Qp)	Si	21.3
9.0	2392	0.1	12.06	30.16	12.06	22.4	220	0.014	0.014	0.014	9(Fr)	Si	28.4
44.8	1644	0.1	12.06	30.16	12.06	22.4	152	0.010	0.010	0.010	14(Qp)	Si	31.0
44.8	1644	0.1	12.06	30.16	12.06	22.4	152	0.010	0.010	0.010	9(Fr)	Si	41.3
80.7	361	--	--	12.06	12.06	22.4	33	0.002	0.002	0.002	14(Qp)	Si	>100

X	M	Act	Aft	pAft	S _{max}	σf_{med}	Wd	Wk	Cb	Ver.	CS
80.7	319	0.1	12.06	30.16	22.4	29	0.002	0.002	12(Fr)		Si >100
89.6	-37	0.1	12.06	30.16	22.4	3	0.000	0.000	14(Qp)		Si >100
89.6	32	0.1	12.06	30.16	22.4	3	0.000	0.000	11(Fr)		Si >100

Trave di Fond. : 9009 | 3.4 | Pilastro | 3.4 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.0 cm Ln= 89.0 cm Terreno: TerrenoI

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma f[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	$\sigma f+$	σ_{c-}	$\sigma f-$	Cb+	Cb-	Ver.	CS
cm	kg·m	kg·m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	4381	12.06	12.06	--	--	--	-7	404	6	8	Si 8.92
8.9	--	4261	12.06	12.06	--	--	--	-7	393	6	8	Si 9.17
44.5	--	3365	12.06	12.06	--	--	--	-5	310	1	8	Si 11.6
80.1	833	1839	12.06	12.06	-1	77	-3	169	1	8	Si 21.2	
89.0	1373	1362	12.06	12.06	-2	127	-2	126	1	8	Si 28.5	

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma f[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	$\sigma f+$	σ_{c-}	$\sigma f-$	Cb+	Cb-	Ver.	CS
cm	kg·m	kg·m	cmq	cmq	cm/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	--	365	12.06	--	--	-1	34	14	14	Si	>100
8.9	--	--	195	12.06	--	--	-0	18	14	14	Si	>100
44.5	759	--	--	12.06	-1	70	--	--	14	14	Si	51.4
80.1	2119	--	--	12.06	-3	195	--	--	14	14	Si	18.4
89.0	2518	--	--	12.06	-4	232	--	--	14	14	Si	15.5

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Mq	Aft	pAft	S _{max} cm	$\sigma f+$ kg/cmq	σ_{c-} kg/cmq	Wd	Wk	Cb	Ver.	CS
cm	kg*m			cmq	cmq	cm	kg/cmq	kg/cmq	mm	mm			
0.0	326	0.1	12.06	30.16	12.06	22.4	30	0.002	0.002	0.002	12(Fr)	Si	>100
0.0	365	0.1	12.06	30.16	12.06	22.4	34	0.002	0.002	0.002	14(Qp)	Si	>100
8.9	195	0.1	12.06	30.16	12.06	22.4	18	0.001	0.001	0.001	14(Qp)	Si	>100
8.9	144	0.1	12.06	30.16	12.06	22.4	13	0.001	0.001	0.001	12(Fr)	Si	>100
44.5	-759	0.1	12.06	30.16	12.06	22.4	70	0.004	0.004	0.004	14(Qp)	Si	67.1
44.5	79	0.1	12.06	30.16	12.06	22.4	7	0.000	0.000	0.000	13(Fr)	Si	>100
80.1	-2119	0.1	12.06	30.16	12.06	22.4	195	0.012	0.012	0.012	14(Qp)	Si	24.0
80.1	-1195	0.1	12.06	30.16	12.06	22.4	110	0.007	0.007	0.007	13(Fr)	Si	56.8
89.0	-2518	0.1	12.06	30.16	12.06	22.4	232	0.015	0.015	0.015	14(Qp)	Si	20.2
89.0	-1572	0.1	12.06	30.16	12.06	22.4	145	0.009	0.009	0.009	13(Fr)	Si	43.2

Trave di Fond. : 9009 | 4.5 | Pilastro | 4.5 |

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 89.3 cm Ln= 89.3 cm Terreno: TerrenoI

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma f[kg/cmq]=3600$

X	M+	M-	M- kg*m	Afsup cmq	Afinf cmq	σ_{c+} kg/cmq	$\sigma f+$ kg/cmq	σ_{c-} kg/cmq	$\sigma f-$ kg/cmq	Cb+	Cb-	Ver.	CS
cm	kg*m			cmq	cmq	cm	kg/cmq	kg/cmq	kg/cmq				
0.0	1040	1525	12.06	12.06	12.06	-2	96	-2	141	1	8	Si	25.6
8.9	1276	1392	12.06	12.06	12.06	-2	118	-2	128	1	8	Si	28.1
44.6	2525	490	12.06	12.06	12.06	-4	233	-1	45	1	8	Si	15.5
80.3	4249	--	12.06	12.06	12.06	-7	392	--	--	1	8	Si	9.19
89.3	4752	--	12.06	12.06	12.06	-7	438	--	--	1	8	Si	8.22

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma f[kg/cmq]=3600$

X	M+	M-	M- kg*m	Afsup cmq	Afinf cmq	σ_{c+} kg/cmq	$\sigma f+$ kg/cmq	σ_{c-} kg/cmq	$\sigma f-$ kg/cmq	Cb+	Cb-	Ver.	CS
cm	kg*m			cmq	cmq	cm	kg/cmq	kg/cmq	kg/cmq				
0.0	2170	--	12.06	12.06	12.06	-3	200	--	--	14	14	Si	18.0
8.9	2344	--	12.06	12.06	12.06	-4	216	--	--	14	14	Si	16.7
44.6	3262	--	12.06	12.06	12.06	-5	301	--	--	14	14	Si	12.0
80.3	4526	--	12.06	12.06	12.06	-7	417	--	--	14	14	Si	8.63
89.3	4895	--	12.06	12.06	12.06	-8	451	--	--	14	14	Si	7.98

Verifica aperture fessure:Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	offred	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-1295	0.1	12.06	30.16	22.4	119	0.008	0.008	13(Fr)	Si	52.4
0.0	-2170	0.1	12.06	30.16	22.4	200	0.013	0.013	14(Qp)	Si	23.5
8.9	-2344	0.1	12.06	30.16	22.4	216	0.014	0.014	14(Qp)	Si	21.7
8.9	-1451	0.1	12.06	30.16	22.4	134	0.009	0.009	13(Fr)	Si	46.8
44.6	-3262	0.1	12.06	30.16	22.4	301	0.019	0.019	14(Qp)	Si	15.6
44.6	-2295	0.1	12.06	30.16	22.4	211	0.014	0.014	13(Fr)	Si	29.6
80.3	-3456	0.1	12.06	30.16	22.4	417	0.027	0.027	14(Qp)	Si	11.3
80.3	-3487	0.1	12.06	30.16	22.4	321	0.021	0.021	13(Fr)	Si	19.5
89.3	-4895	0.1	12.06	30.16	22.4	451	0.029	0.029	14(Qp)	Si	10.4
89.3	-3838	0.1	12.06	30.16	22.4	354	0.023	0.023	13(Fr)	Si	17.7

Trave di Fond. : 9009 | 5.6 | Pilastrate | 5.6 |

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln=89.0 cm Terreno: Terrenol

Criterio : CLS_TraviFondazione

Combinazione Rara: scalc[kg/cmq]=149 sfal[kg/cmq]=3600

X	M+	M-	Alup	Alinf	σc+	σf+	σc-	σf-	Ch+	Ch-	Ver.	CS
cm	kg *m	kg *m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	4482	--	12.06	12.06	-7	413	--	--	1	8	Si	8.72
8.9	4668	--	12.06	12.06	-7	430	--	--	1	8	Si	8.37
44.5	5695	--	12.06	12.06	-9	525	--	--	1	8	Si	6.86
80.1	7257	--	12.06	12.06	-11	669	--	--	2	7	Si	5.38
89.0	7766	--	12.06	12.06	-12	716	--	--	2	7	Si	5.03

Combinazione OP: scalc[kg/cmq]=112 sfal[kg/cmq]=3600

X	M+	M-	Msup	Afin+	σc+	erf+	σc-	erf-	Ch+	Ch-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	4587	--	12.06	12.06	-7	423	--	--	14	14	Si	8.52
8.9	4720	--	12.06	12.06	-7	435	--	--	14	14	Si	8.27
44.5	5461	--	12.06	12.06	-8	503	--	--	14	14	Si	7.15
80.1	6532	--	12.06	12.06	-10	602	--	--	14	14	Si	5.98
89.0	6851	--	12.06	12.06	-11	631	--	--	14	14	Si	5.70

Verifica aperture fessure:Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	mq	cmq	pAft	S _{max}	defined	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-3601	0.1	12.06	30.16	22.4	332	0.021	0.021	0.021	13(Fr)	Si	18.9
0.0	-4587	0.1	12.06	30.16	22.4	423	0.027	0.027	0.027	14(Qp)	Si	11.1
8.9	-4720	0.1	12.06	30.16	22.4	435	0.028	0.028	0.028	14(Qp)	Si	10.8
8.9	-3721	0.1	12.06	30.16	22.4	343	0.022	0.022	0.022	13(Fr)	Si	18.3
44.5	-5461	0.1	12.06	30.16	22.4	503	0.032	0.032	0.032	14(Qp)	Si	9.33
44.5	-4411	0.1	12.06	30.16	22.4	407	0.026	0.026	0.026	13(Fr)	Si	15.4
80.1	-6532	0.1	12.06	30.16	22.4	602	0.038	0.038	0.038	14(Qp)	Si	7.80
80.1	-5433	0.1	12.06	30.16	22.4	501	0.032	0.032	0.032	13(Fr)	Si	12.5
89.0	-6851	0.1	12.06	30.16	22.4	631	0.040	0.040	0.040	14(Qp)	Si	7.43
89.0	-5741	0.1	12.06	30.16	22.4	529	0.034	0.034	0.034	13(Fr)	Si	11.8

Trave di Fond. : 9009 | 6.7 | Pilastrate | 6.7 |

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln=89.0 cm Terreno: Terrenol

Criterio : CLS_TraviFondazione

Combinazione Rara: scalc[kg/cmq]=149 sfal[kg/cmq]=3600

X	M+	M-	Act	Alinif	oc+	σf+	σc-	kg/cmq	σf-	Ch+	Ch-	Ver.	Cs
cm	kg *m	kg *m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	7502	--	12.06	12.06	-12	691	--	--	--	2	7	Si	5.21
8.9	7593	--	12.06	12.06	-12	700	--	--	--	2	7	Si	5.14
44.5	8344	--	12.06	12.06	-13	769	--	--	--	2	7	Si	4.68
80.1	9715	--	12.06	12.06	-15	895	--	--	--	2	7	Si	4.02
89.0	10155	--	12.06	12.06	-16	936	--	--	--	2	7	Si	3.85

Combinazione OP: scalc[kg/cmq]=112 sfal[kg/cmq]=3600

X	M+	M-	A _{flap}	A _{fin}	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq	cmq</
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Verifica aperture fessure:Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	effined	Wd	Wk	Cb	Ver.	Cs
cm	kg·m	nq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-5552	0.1	12.06	30.16	22.4	510	0.033	0.033	13(Fr)	Si	12.3
0.0	-6573	0.1	12.06	30.16	22.4	606	0.039	0.039	14(Qp)	Si	7.75
8.9	-6656	0.1	12.06	30.16	22.4	613	0.039	0.039	14(Qp)	Si	7.65
8.9	-5608	0.1	12.06	30.16	22.4	517	0.033	0.033	13(Fr)	Si	12.1
44.5	-7196	0.1	12.06	30.16	22.4	663	0.042	0.042	14(Qp)	Si	7.08
44.5	-6117	0.1	12.06	30.16	22.4	564	0.036	0.036	13(Fr)	Si	11.1
80.1	-8066	0.1	12.06	30.16	22.4	743	0.048	0.048	14(Qp)	Si	6.31
80.1	-6960	0.1	12.06	30.16	22.4	641	0.041	0.041	13(Fr)	Si	9.76
89.0	-8335	0.1	12.06	30.16	22.4	768	0.049	0.049	14(Qp)	Si	6.11
89.0	-7222	0.1	12.06	30.16	22.4	666	0.043	0.043	13(Fr)	Si	9.40

Trave di Fond. : 9009 | 7.8 | Pilastrate | 7.8 |

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln=89.2 cm Terreno: Terrenol

Criterio : CLS_TraviFondazione

Combinazione Rara: scalc[kg/cmq]=149 sfal[kg/cmq]=3600

Conformazione Rata. 0.04 kg/cm ² Alin ⁺ /cm ² - 2000																			
X	M+	M-	Act	m	kg*m	cmq	cmq	cmq	cmq	sf+	sf-	Ch+	Ch-	Ver.	Cb-	Cb+	Ver.	Cs	
	cm	kg*m	kg*m	--	12.06	12.06	12.06	-15	920	--	--	2	7	Si	3.91	2	7	Si	
	0.0	9978	--	--	12.06	12.06	12.06	-15	881	--	--	2	7	Si	4.09	2	7	Si	
	8.9	9561	--	--	12.06	12.06	12.06	-13	763	--	--	2	7	Si	4.72	2	7	Si	
	44.6	8280	--	--	12.06	12.06	12.06	-12	703	--	--	2	7	Si	5.12	2	7	Si	
	80.2	7623	--	--	12.06	12.06	12.06	-12	696	--	--	2	7	Si	5.17	2	7	Si	
	89.2	7557	--	--	12.06	12.06	12.06	-12	696	--	--	2	7	Si	5.17	2	7	Si	

Combinazione OP: scalc[kg/cmq]=112 sfal[kg/cmq]=3600

X	M+	M-	Δfup	Δfinf	σc+	σf+	σc-	σf-	Ch+	Ch-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	8120	--	12.06	12.06	-13	748	--	--	14	14	Si	4.81
8.9	7987	--	12.06	12.06	-12	736	--	--	14	14	Si	4.89
44.6	7666	--	12.06	12.06	-12	707	--	--	14	14	Si	5.10
80.2	7684	--	12.06	12.06	-12	708	--	--	14	14	Si	5.08
89.2	7742	--	12.06	12.06	-12	714	--	--	14	14	Si	5.05

Verifica aperture fessure:Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	mq	cmq	pAff	S _{max}	cm	kg/cmq	enfrmed	Wd	Wk	Cb	Ver.	Cs
cm	kg·m		mq	cmq	pAff	S _{max}	cm	kg/cmq	enfrmed	mm	mm			
0.0	-7071	0.1	12.06	30.16	22.4	652	0.042	0.042	0.042	0.042	0.042	13(Fr)	Si	9.61
0.0	-8120	0.1	12.06	30.16	22.4	748	0.048	0.048	0.048	0.048	0.048	14(Qp)	Si	6.27
8.9	-7987	0.1	12.06	30.16	22.4	736	0.047	0.047	0.047	0.047	0.047	14(Qp)	Si	6.38
8.9	-6880	0.1	12.06	30.16	22.4	634	0.041	0.041	0.041	0.041	0.041	13(Fr)	Si	9.87
44.6	-7666	0.1	12.06	30.16	22.4	707	0.045	0.045	0.045	0.045	0.045	14(Qp)	Si	6.64
44.6	-6327	0.1	12.06	30.16	22.4	583	0.037	0.037	0.037	0.037	0.037	13(Fr)	Si	10.7
80.2	-7684	0.1	12.06	30.16	22.4	708	0.045	0.045	0.045	0.045	0.045	14(Qp)	Si	6.63
80.2	-6113	0.1	12.06	30.16	22.4	563	0.036	0.036	0.036	0.036	0.036	13(Fr)	Si	11.1
89.2	-7742	0.1	12.06	30.16	22.4	714	0.046	0.046	0.046	0.046	0.046	14(Qp)	Si	6.58
89.2	-6113	0.1	12.06	30.16	22.4	563	0.036	0.036	0.036	0.036	0.036	13(Fr)	Si	11.1

Trave di Fond. : 9009 | 8.9 | Pilastrate | 8.9 |

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln=88.8 cm Terreno: Terrenol

Criterio : CLS_TraviFondazione

Combinazione Rara: scalc[kg/cmq]=149 sfal[kg/cmq]=3600

Composizione (mm. sec/kg cmq) 147 cm/kg cmq 5000																		
X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	Cs						
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq										

X	M	M+	Act	Aft	Afsup	emined	Wd	Wk	Cb	Ver.	Cs
8.9	-7198		0.1	12.06	30.16	22.4	663	0.042	13(Fr)	Si	9.43
44.6	-8327		0.1	12.06	30.16	22.4	767	0.049	14(Qp)	Si	6.12
44.6	-7031		0.1	12.06	30.16	22.4	648	0.041	13(Fr)	Si	9.66
80.3	-8533		0.1	12.06	30.16	22.4	786	0.050	14(Qp)	Si	5.97
80.3	-7250		0.1	12.06	30.16	22.4	668	0.043	13(Fr)	Si	9.37
89.2	-8646		0.1	12.06	30.16	22.4	797	0.051	14(Qp)	Si	5.89
89.2	-7365		0.1	12.06	30.16	22.4	679	0.043	13(Fr)	Si	9.22

Trave di Fond. : 9009 | 12., 13. | Pilastrate [12., 13.]

Sez. R: By= 60.0 cm Bz= 100.0 cm L=89.0 cm Ln=89.0 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cm^2]=149$ $\sigma_{fal}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σe+	σe-	σf-	Cb+	Cr-	Ver.	CS
cm	kg*m	kg*m	cm	cm	kg/cm	kg/cm	kg/cm				
0.0	10164	--	12.06	12.06	-16	937	--	2	7	Si	3.84
8.9	9981	--	12.06	12.06	-15	920	--	2	7	Si	3.91
44.5	9683	--	12.06	12.06	-15	892	--	2	7	Si	4.03
80.1	10089	--	12.06	12.06	-16	930	--	2	7	Si	3.87
89.0	10300	--	12.06	12.06	-16	949	--	2	7	Si	3.79

Combinazione QP: $\sigma_{cal}[kg/cm^2]=112$ $\sigma_{fal}[kg/cm^2]=3600$

X	M+	M-	Atsup	Afin	σe+	σf+	σe-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cm	cm	kg/cm	kg/cm	kg/cm	kg/cm				
0.0	8611	--	12.06	12.06	-13	794	--	--	14	14	Si	4.54
8.9	8501	--	12.06	12.06	-13	784	--	--	14	14	Si	4.59
44.5	8310	--	12.06	12.06	-13	766	--	--	14	14	Si	4.70
80.1	8518	--	12.06	12.06	-13	785	--	--	14	14	Si	4.59
89.0	8633	--	12.06	12.06	-13	796	--	--	14	14	Si	4.52

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M+	Act	Aft	Afsup	emined	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	cm	cm	cm	kg/cm	kg/cm	kg/cm	kg/cm	kg/cm	kg/cm
0.0	-7394		0.1	12.06	30.16	22.4	681	0.044	13(Fr)	Si	9.19
0.0	-8611		0.1	12.06	30.16	22.4	794	0.051	14(Qp)	Si	5.92
8.9	-8501		0.1	12.06	30.16	22.4	784	0.050	14(Qp)	Si	5.99
8.9	-7290		0.1	12.06	30.16	22.4	672	0.043	13(Fr)	Si	9.32
44.5	-8310		0.1	12.06	30.16	22.4	766	0.049	14(Qp)	Si	6.13
44.5	-7117		0.1	12.06	30.16	22.4	656	0.042	13(Fr)	Si	9.54
80.1	-8518		0.1	12.06	30.16	22.4	785	0.050	14(Qp)	Si	5.98
80.1	-7338		0.1	12.06	30.16	22.4	676	0.043	13(Fr)	Si	9.26
89.0	-8633		0.1	12.06	30.16	22.4	796	0.051	14(Qp)	Si	5.90
89.0	-7454		0.1	12.06	30.16	22.4	687	0.044	13(Fr)	Si	9.11

Trave di Fond. : 9009 | 13., 14. | Pilastrate [13., 14.]

Sez. R: By= 60.0 cm Bz= 100.0 cm L=89.6 cm Ln=89.6 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cm^2]=149$ $\sigma_{fal}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σe+	σe-	σf-	Cb+	Cb-	Ver.	CS
cm	kg* ^m	kg* ^m	cm	cm	kg/cm ²	kg/cm ²	kg/cm ²				
0.0	10480	--	12.06	12.06	-16	966	--	2	7	Si	3.73
9.0	10120	--	12.06	12.06	-16	933	--	2	7	Si	3.86
44.8	9124	--	12.06	12.06	-14	841	--	2	7	Si	4.28
80.6	8841	--	12.06	12.06	-14	815	--	2	7	Si	4.42
89.6	8880	--	12.06	12.06	-14	818	--	2	7	Si	4.40

Combinazione QP: $\sigma_{cal}[kg/cm^2]=112$ $\sigma_{fal}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+ kg/cm ²	σc+ kg/cm ²	σc- kg/cm ²	σf- kg/cm ²	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cm	cm	cm	cm	kg/cm ²	kg/cm ²				
0.0	8629	--	12.06	12.06	-13	795	--	--	14	14	Si	4.53
9.0	8514	--	12.06	12.06	-13	785	--	--	14	14	Si	4.59
44.8	8307	--	12.06	12.06	-13	766	--	--	14	14	Si	4.70
80.6	8509	--	12.06	12.06	-13	784	--	--	14	14	Si	4.59

X	M+	M-	Act	Aft	Afsup	emined	Wd	Wk	Cb	Ver.	Cs
89.6	8623	--	12.06	12.06	12.06	-13	795	--	14	14	Si 4.53

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M+	Act	Aft	Afsup	emined	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	cm	cm	cm	kg/cm	kg/cm	kg/cm	kg/cm	kg/cm	kg/cm
0.0	-7512		0.1	12.06	30.16	22.4	692	0.044	13(Fr)	Si	9.04
0.0	-8629		0.1	12.06	30.16	22.4	795	0.051	14(Qp)	Si	5.90
9.0	-8514		0.1	12.06	30.16	22.4	785	0.050	14(Qp)	Si	5.98
9.0	-7346		0.1	12.06	30.16	22.4	677	0.043	13(Fr)	Si	9.25
44.8	-8307		0.1	12.06	30.16	22.4	766	0.049	14(Qp)	Si	6.13
44.8	-6932		0.1	12.06	30.16	22.4	639	0.041	13(Fr)	Si	9.80
80.6	-8309		0.1	12.06	30.16	22.4	784	0.050	14(Qp)	Si	5.99
80.6	-6918		0.1	12.06	30.16	22.4	638	0.041	13(Fr)	Si	9.82
89.6	-8623		0.1	12.06	30.16	22.4	795	0.051	14(Qp)	Si	5.91
89.6	-6977		0.1	12.06	30.16	22.4	643	0.041	13(Fr)	Si	9.73

Trave di Fond. : 9009 | 14., 15. | Pilastrate [14., 15.]

Sez. R: By= 60.0 cm Bz= 100.0 cm L=89.9 cm Ln=89.9 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cm^2]=149$ $\sigma_{fal}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σc-	σf+	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cm	cm	kg/cm	kg/cm	kg/cm	kg/cm				
0.0	9105	--	12.06	12.06	-14	839	--	--	2	7	Si	4.29
9.0	8898	--	12.06	12.06	-14	820	--	--	2	7	Si	4.39
44.9	8516	--	12.06	12.06	-13	785	--	--	2	7	Si	4.59
80.9	8843	--	12.06	12.06	-14	815	--	--	2	7	Si	4.42
89.9	9034	--	12.06	12.06	-14	833	--	--	2	7	Si	4.32

Combinazione QP: $\sigma_{cal}[kg/cm^2]=112$ $\sigma_{fal}[kg/cm^2]=3600$

X	M+	M-	Afup	Afinf	σc+	σc-	σf+	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cm	cm	kg/cm	kg/cm	kg/cm	kg/cm				
0.0	8639	--	12.06	12.06	-13	796	--	--	14	14	Si	4.52
9.0	8514	--	12.06	12.06	-13	785	--	--	14	14	Si	4.59
44.9	8268	--	12.06	12.06	-13	762	--	--	14	14	Si	4.72
80.9	8428	--	12.06	12.06	-13	777	--	--	14	14	Si	4.63
89.9	8531	--	12.06	12.06	-13	786	--	--	14	14	Si	4.58

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	M+	Act	Aft	Afsup	emined	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	kg*m	cm	cm	cm	kg/cm	kg/cm	kg/cm	kg/cm	kg/cm	kg/cm
0.0	-7058		0.1	12.06	30.16	22.4	650	0.042	13(Fr)	Si	9.62
0.0	-8639		0.1	12.06	30.16	22.4	796	0.051	14(Qp)	Si	5.90
9.0	-8514		0.1	12.06	30.16	22.4	785	0.050	14(Qp)	Si	5.98
9.0	-6938		0.1	12.06	30.16	22.4	639	0.041	13(Fr)	Si	9.79
44.9	-8268		0.1	12.06	30.16	22.4	762	0.049	14(Qp)	Si	6.16
44.9	-6711		0.1	12.06	30.16	22.4	618	0.040	13(Fr)	Si	10.1
80.9	-8428		0.1	12.06	30.16	22.4	777	0.050	14(Qp)	Si	6.04
80.9	-6881		0.1	12.06	30.16	22.4	634	0.041	13(Fr)	Si	9.87
89.9	-8531		0.1	12.06	30.16	22.4	786	0.050	14(Qp)	Si	5.97
89.9	-6986		0.1	12.06	30.16	22.4	644	0.041	13(Fr)	Si	9.72

Trave di Fond. : 9009 | 15., 16. | Pilastrate [15., 16.]

Sez. R: By= 60.0 cm Bz= 100.0 cm L=89.2 cm Ln=89.2 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cm^2]=149$ $\sigma_{fal}[kg/cm^2]=3600$

X	M+	M-	Aftsup	Aftinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg* ³ m	kg* ³ m	cm/kg	cm/kg	kg/cmkg	kg/cmkg	kg/cmkg	kg/cmkg				
0.0	9322	--	12.06	12.06	-14	859	--	--	2	7	Si	4.19
8.9	9123	--	12.06	12.06	-14	841	--	--	2	7	Si	4.28
44.6	8758	--	12.06	12.06	-14	807	--	--	2	7	Si	4.46
80.3	9084	--	12.06	12.06	-14	837	--	--	2	7	Si	4.30

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
44.4	-6802	0.1	12.06	30.16	22.4	627	0.040	0.040	13(Fr)	Si	9.98
79.9	-8641	0.1	12.06	30.16	22.4	796	0.051	0.051	14(Op)	Si	5.89
79.9	-7041	0.1	12.06	30.16	22.4	649	0.041	0.041	13(Fr)	Si	9.65
88.7	-8804	0.1	12.06	30.16	22.4	811	0.052	0.052	14(Op)	Si	5.79
88.7	-7155	0.1	12.06	30.16	22.4	659	0.042	0.042	13(Fr)	Si	9.49

Trave di Fond. : 9009 | 19, 20 | Pilastrate [19, 20]

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln= 89.9 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=149$ $\sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	9771	--	12.06	12.06	-15	901	--	--	2	7	Si	4.00
9.0	9437	--	12.06	12.06	-15	870	--	--	2	7	Si	4.14
44.9	8506	--	12.06	12.06	-13	784	--	--	2	7	Si	4.59
80.9	8217	--	12.06	12.06	-13	757	--	--	2	7	Si	4.75
89.9	8244	--	12.06	12.06	-13	760	--	--	2	7	Si	4.74

Combinazione QP: $\sigma_{ca}[kg/cm^2]=112$ $\sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	8994	--	12.06	12.06	-14	829	--	--	14	14	Si	4.34
9.0	8781	--	12.06	12.06	-14	809	--	--	14	14	Si	4.45
44.9	8150	--	12.06	12.06	-13	751	--	--	14	14	Si	4.79
80.9	7870	--	12.06	12.06	-12	725	--	--	14	14	Si	4.96
89.9	7854	--	12.06	12.06	-12	724	--	--	14	14	Si	4.97

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-7410	0.1	12.06	30.16	22.4	683	0.044	0.044	13(Fr)	Si	9.17
0.0	-8994	0.1	12.06	30.16	22.4	829	0.053	0.053	14(Op)	Si	5.66
9.0	-8781	0.1	12.06	30.16	22.4	809	0.052	0.052	14(Op)	Si	5.80
9.0	-7208	0.1	12.06	30.16	22.4	664	0.042	0.042	13(Fr)	Si	9.42
44.9	-8150	0.1	12.06	30.16	22.4	751	0.048	0.048	14(Op)	Si	6.25
44.9	-6622	0.1	12.06	30.16	22.4	610	0.039	0.039	13(Fr)	Si	10.3
80.9	-7870	0.1	12.06	30.16	22.4	725	0.046	0.046	14(Op)	Si	6.47
80.9	-6386	0.1	12.06	30.16	22.4	589	0.038	0.038	13(Fr)	Si	10.6
89.9	-7854	0.1	12.06	30.16	22.4	724	0.046	0.046	14(Op)	Si	6.49
89.9	-6380	0.1	12.06	30.16	22.4	588	0.038	0.038	13(Fr)	Si	10.6

Trave di Fond. : 9009 | 20, 21 | Pilastrate [20, 21]

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln= 89.1 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=149$ $\sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	8835	--	12.06	12.06	-14	814	--	--	2	7	Si	4.42
8.9	8452	--	12.06	12.06	-13	779	--	--	2	7	Si	4.62
44.6	7303	--	12.06	12.06	-11	673	--	--	2	7	Si	5.35
80.2	6768	--	12.06	12.06	-10	624	--	--	2	7	Si	5.77
89.1	6729	--	12.06	12.06	-10	620	--	--	2	7	Si	5.80

Combinazione QP: $\sigma_{ca}[kg/cm^2]=112$ $\sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	8080	--	12.06	12.06	-12	745	--	--	14	14	Si	4.83
8.9	7832	--	12.06	12.06	-12	722	--	--	14	14	Si	4.99
44.6	7042	--	12.06	12.06	-11	649	--	--	14	14	Si	5.55
80.2	6582	--	12.06	12.06	-10	607	--	--	14	14	Si	5.93
89.1	6518	--	12.06	12.06	-10	601	--	--	14	14	Si	5.99

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-6674	0.1	12.06	30.16	22.4	615	0.039	0.039	13(Fr)	Si	10.2
0.0	-8080	0.1	12.06	30.16	22.4	745	0.048	0.048	14(Op)	Si	6.30
8.9	-7832	0.1	12.06	30.16	22.4	722	0.046	0.046	14(Op)	Si	6.50
8.9	-6440	0.1	12.06	30.16	22.4	594	0.038	0.038	13(Fr)	Si	10.5
44.6	-7042	0.1	12.06	30.16	22.4	649	0.041	0.041	14(Op)	Si	7.23
44.6	-5712	0.1	12.06	30.16	22.4	526	0.034	0.034	13(Fr)	Si	11.9
80.2	-6582	0.1	12.06	30.16	22.4	607	0.039	0.039	14(Op)	Si	7.74
80.2	-5314	0.1	12.06	30.16	22.4	490	0.031	0.031	13(Fr)	Si	12.8
89.1	-6518	0.1	12.06	30.16	22.4	601	0.038	0.038	14(Op)	Si	7.81
89.1	-5266	0.1	12.06	30.16	22.4	485	0.031	0.031	13(Fr)	Si	12.9

Trave di Fond. : 9009 | 21, 22 | Pilastrate [21, 22]

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln= 89.4 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=149$ $\sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	7405	--	12.06	12.06	-11	682	--	--	2	7	Si	5.27
8.9	6956	--	12.06	12.06	-11	641	--	--	2	7	Si	5.62
44.7	5621	--	12.06	12.06	-9	518	--	--	1	8	Si	6.95
80.4	4805	--	12.06	12.06	-7	443	--	--	1	8	Si	8.13
89.4	4672	--	12.06	12.06	-7	431	--	--	1	8	Si	8.36

Combinazione QP: $\sigma_{ca}[kg/cm^2]=112$ $\sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	6804	--	12.06	12.06	-11	627	--	--	14	14	Si	5.74
8.9	6504	--	12.06	12.06	-10	599	--	--	14	14	Si	6.01
44.7	5508	--	12.06	12.06	-9	508	--	--	14	14	Si	7.09
80.4	4839	--	12.06	12.06	-7	446	--	--	14	14	Si	8.07
89.4	4723	--	12.06	12.06	-7	435	--	--	14	14	Si	8.27

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-5615	0.1	12.06	30.16	22.4	518	0.033	0.033	13(Fr)	Si	12.1
0.0	-6804	0.1	12.06	30.16	22.4	627	0.040	0.040	14(Op)	Si	7.49
8.9	-6504	0.1	12.06	30.16	22.4	599	0.038	0.038	14(Op)	Si	7.83
8.9	-5335	0.1	12.06	30.16	22.4	492	0.031	0.031	13(Fr)	Si	12.7
44.7	-5508	0.1	12.06	30.16	22.4	508	0.032	0.032	14(Op)	Si	9.25
44.7	-4422	0.1	12.06	30.16	22.4	408	0.026	0.026	13(Fr)	Si	15.4
80.4	-4839	0.1	12.06	30.16	22.4	446	0.029	0.029	14(Op)	Si	10.5
80.4	-3840	0.1	12.06	30.16	22.4	354	0.023	0.023	13(Fr)	Si	17.7
89.4	-4723	0.1	12.06	30.16	22.4	435	0.028	0.028	14(Op)	Si	10.8
89.4	-3745	0.1	12.06	30.16	22.4	345	0.022	0.022	13(Fr)	Si	18.1

Trave di Fond. : 9009 | 22, 23 | Pilastrate [22, 23]

Sez. R: By= 60.0 cm Bz= 100.0 cm Ln= 89.8 cm Terreno: Terrenol

Criterio : CLS TraviFondazione

Combinazione Rara: $\sigma_{ca}[kg/cm^2]=149$ $\sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	5379	--	12.06	12.06	-8	496	--	--	2	7	Si	7.26
9.0	4921	--	12.06	12.06	-8	454	--	--	1	8	Si	7.94
44.9	3417	--	12.06	12.06	-5	315	--	--	1	8	Si	11.4
80.8	2377	--	12.06	12.06	-4	219	--	--	1	8	Si	16.4
89.8	2190	--	12.06	12.06	-3	202	--	--	1	8	Si	17.8

Combinazione QP: $\sigma_{ca}[kg/cm^2]=112$ $\sigma_{fa}[kg/cm^2]=3600$

X	M+	M-	Δ sup	Afinf	$\sigma\epsilon^+$	$\sigma\epsilon^-$	σf^+	Cb+	Cb-	Ver.	CS
0.0	377	416	12.06	12.06	-1	35	-1	38	1	8	Si 93.9
9.0	--	820	12.06	12.06	--	--	-1	76	6	8	Si 47.6
44.8	--	2310	12.06	12.06	--	--	-4	213	6	5	Si 16.9
80.7	--	3224	12.06	12.06	--	--	-5	297	7	2	Si 12.1
89.7	--	3338	12.06	12.06	--	--	-5	308	7	2	Si 11.7

Combinazione QP: $\sigma_{ca}[\text{kg/cmq}] = 112 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	cm	M ₊ kg*	M _* kg*	A _{sup} cmq	A _{fin} cmq	σ ₊ kg/cmq	σ ₋ kg/cmq	σ _f kg/cmq	Cb+	Cb-	Ver.	CS
	0.0	485	--	12.06	12.06	-1	45	--	14	14	Si	80.6
	9.0	89	--	12.06	12.06	-0	8	--	14	14	Si	>100
	44.8	--	12.16	12.06	12.06	--	-2	11.2	14	14	Si	32.1
	80.7	--	2033	12.06	12.06	--	-3	187	14	14	Si	19.2
	89.7	--	2155	12.06	12.06	--	-3	199	14	14	Si	18.1

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAlt	S _{max}	cmf	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-293	0.1	12.06	30.16	22.4	27	0.002	0.002	13(Fr)	Si	>100
0.0	-485	0.1	12.06	30.16	22.4	45	0.003	0.003	14(Qp)	Si	>100
9.0	-89	0.1	12.06	30.16	22.4	8	0.001	0.001	14(Qp)	Si	>100
0.0	-27	0.1	12.06	30.16	22.4	3	0.000	0.000	11(Fr)	Si	>100
44.8	12.16	0.1	12.06	30.16	22.4	112	0.007	0.007	14(Qp)	Si	41.9
44.8	12.10	0.1	12.06	30.16	22.4	112	0.007	0.007	12(Fr)	Si	56.1
80.7	2033	0.1	12.06	30.16	22.4	187	0.012	0.012	14(Qp)	Si	25.1
80.7	1936	0.1	12.06	30.16	22.4	178	0.011	0.011	13(Fr)	Si	35.1
89.7	2155	0.1	12.06	30.16	22.4	199	0.013	0.013	14(Qp)	Si	23.6
89.7	2032	0.1	12.06	30.16	22.4	187	0.012	0.012	3(Fr)	Si	33.4

Trave di Fond.: 9009 | 25, 26 | Pilastrate | 25, 26 |

Sez. R:	B _V = 60.0 cm	B _Z = 100.0 cm	L = 89.5 cm	L _n = 100.9 cm	Terreno: Terreno I
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Criterio: CLS_TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149$ $\sigma_{fa}[\text{kg/cmq}] = 3600$

X	cm	M+	M _*	M _g	Al _{inf}	σ _e +	σ _e +	σ _e	σ _e	Cb+	Cb-	Ver.	CS
	0.0	--	24.22	12.06	12.06	--	--	4	223	7	2	Si	16.1
	10.1	--	25.49	12.06	12.06	--	--	4	235	7	2	Si	15.3
	50.5	--	23.10	12.06	12.06	--	--	4	213	7	2	Si	16.9
	90.8	--	805	12.06	12.06	--	--	1	74	6	8	Si	48.5
	100.9	--	468	12.06	12.06	--	--	1	43	5	7	Si	83.5

Combinazione QP: $\sigma_{ca}[\text{kg/cm}^2]=112 \sigma_{fa}[\text{kg/cm}^2]=3600$

X	cm	M+	M _*	Δsup	Δfinf	σc+	qf+	σc-	qf-	Cb+	Cb-	Ver.	CS
	0.0	--	1723	12.06	12.06	--	--	-3	159	14	14	Si	22.7
	10.1	--	1774	12.06	12.06	--	--	-3	163	14	14	Si	22.0
	50.5	--	1493	12.06	12.06	--	--	-2	138	14	14	Si	26.2
	90.8	--	336	12.06	12.06	--	--	-1	31	14	14	Si	>100
	100.9	106	--	12.06	12.06	-0	10	--	--	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aff	pAff	S _{max}	defined	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	1541	0.1	12.06	30.16	22.4	142	0.009	0.009	13(Fr)	Si	44.1
0.0	1723	0.1	12.06	30.16	22.4	163	0.010	0.010	14(Qp)	Si	29.6
10.1	1774	0.1	12.06	30.16	22.4	163	0.010	0.010	14(Qp)	Si	28.7
10.1	1606	0.1	12.06	30.16	22.4	148	0.009	0.009	13(Fr)	Si	42.3
50.5	1493	0.1	12.06	30.16	22.4	138	0.009	0.009	14(Qp)	Si	34.1
90.8	1412	0.1	12.06	30.16	22.4	130	0.008	0.008	13(Fr)	Si	48.1
90.8	336	0.1	12.06	30.16	22.4	31	0.002	0.002	14(Qp)	Si	>100
90.8	336	0.1	12.06	30.16	22.4	31	0.002	0.002	9(Fr)	Si	>100
100.9	-106	0.1	12.06	30.16	22.4	10	0.001	0.001	14(Qp)	Si	>100
100.9	7	0.1	12.06	30.16	22.4	1	0.000	0.000	3(Fr)	Si	>100

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X	M+	M _*	A _{flap}	A _{fin}	σ ₊	σ _{fl}	σ _c	σ _f	Cb+	Ch-	Ver.	CS
cm	cm	kg*m	kg*m	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	5047	--	12.06	12.06	-8	465	--	--	14	14	Si	7.74
9.0	4698	--	12.06	12.06	-7	433	--	--	14	14	Si	8.31
44.9	3511	--	12.06	12.06	-5	324	--	--	14	14	Si	11.1
80.8	2662	--	12.06	12.06	-4	245	--	--	14	14	Si	14.7
89.8	2503	--	12.06	12.06	-4	231	--	--	14	14	Si	15.6

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efined	Wd	Wk	Cb	Ver.	Cs
cm	kg·m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-4133	0.1	12.06	30.16	22.4	381	0.024	0.024	13(Fr)	Si	16.4
0.0	-5047	0.1	12.06	30.16	22.4	463	0.030	0.030	14(Qp)	Si	10.1
9.0	-4698	0.1	12.06	30.16	22.4	435	0.028	0.028	14(Qp)	Si	10.8
9.0	-3810	0.1	12.06	30.16	22.4	324	0.022	0.022	13(Fr)	Si	17.8
-3511		0.1	12.06	30.16	22.4	351	0.021	0.021	14(Qp)	Si	14.5
44.9	-2728	0.1	12.06	30.16	22.4	251	0.016	0.016	13(Fr)	Si	24.9
80.8	-2662	0.1	12.06	30.16	22.4	245	0.016	0.016	14(Qp)	Si	19.1
80.8	-1988	0.1	12.06	30.16	22.4	183	0.012	0.012	13(Fr)	Si	34.2
89.8	-2503	0.1	12.06	30.16	22.4	231	0.015	0.015	14(Qp)	Si	20.3
-1857		0.1	12.06	30.16	22.4	171	0.011	0.011	13(Fr)	Si	36.6

Trave di Fond.: 9009 [23, 24] Pilastrate [23, 24]

Bez. R:	$B_V=60.0\text{ cm}$	$B_Z=100.0\text{ cm}$	$L=89.3\text{ cm}$	$L_n=89.3\text{ cm}$	Terreno: Terrenol
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Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149$ $\sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M ⁺ kg·m	M ⁺ kg·m	M ⁺ kg·m	Atsup	Atinf	σe ⁺ kg/cmq	σf ⁺ kg/cmq	σe ⁻ kg/cmq	σf ⁻ kg/cmq	Cb+	Cb-	Ver.	CS
0.0	0.0	2941	--	12.06	12.06	12.06	-5	271	--	--	1	8	Si	13.3
8.9	2463	--	12.06	12.06	-4	227	--	--	--	--	1	8	Si	15.9
44.7	852	650	12.06	12.06	-1	78	--	60	-1	60	1	8	Si	45.9
80.4	--	1257	12.06	12.06	--	--	--	--	-2	116	6	8	Si	31.1
89.3	--	1314	12.06	12.06	--	--	--	--	-2	121	6	8	Si	29.7

Combinazione QP: $\sigma_{ca}[\text{kg/cmq}] = 112 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	cm	kg ^a m	M ^a	Atsup	Atinf	σe ⁺	σf ⁺	σe ⁻	σf ⁻	Cb+	Cb-	Ver.	CS
0.0	2860	---	---	12.06	12.06	-4	264	---	---	14	14	Si	13.7
8.9	2478	---	---	12.06	12.06	-4	228	---	---	14	14	Si	15.8
44.7	1171	---	---	12.06	12.06	-2	108	---	---	14	14	Si	33.4
24.3	---	---	---	12.06	12.06	-0	22	---	---	14	14	Si	>100
89.3	73	---	---	12.06	12.06	-0	7	---	---	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	gfined	Wd	Wk	Cb	Ver.	Cs
cm	kg*in	mq	cmq	cm	cm	kg/cmq	mm	mm			
-2278	0.0	0.1	12.06	30.16	22.4	210	0.013	0.013	13(Fr)	Si	29.8
-2860	0.0	0.1	12.06	30.16	22.4	264	0.017	0.017	14(Qp)	Si	17.8
-2478	8.9	0.1	12.06	30.16	22.4	264	0.015	0.015	14(Qp)	Si	20.6
-1929	8.9	0.1	12.06	30.16	22.4	178	0.011	0.011	13(Fr)	Si	35.2
-1171	44.7	0.1	12.06	30.16	22.4	108	0.007	0.007	14(Qp)	Si	43.5
-757	44.7	0.1	12.06	30.16	22.4	70	0.004	0.004	13(Fr)	Si	89.7
-243	80.4	0.1	12.06	30.16	22.4	22	0.001	0.001	14(Qp)	Si	>100
40	80.4	0.1	12.06	30.16	22.4	4	0.000	0.000	13(Fr)	Si	>100
-73	89.3	0.1	12.06	30.16	22.4	7	0.000	0.000	14(Qp)	Si	>100
89.3	-11	0.1	12.06	30.16	22.4	1	0.000	0.000	11(Fr)	Si	>100

Trave di Fond.: 9009 [24, 25 | Pilastrate [24, 25]

Bez. R:	By= 60.0 cm	Bz= 100.0 cm	L=89.7 cm	Ln=89.7 cm	Terreno: Terrenol
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Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M-	Alsup	Alinf	α^+	σ^+	σ^-	Cb+	Cb-	Ver.	CS
cm	kg [*] m	kg [*] m	cmq	cmq	cmq	kg/cmq	kg/cmq				

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Trave di Fond. : 9010 [1, 2 | Pilastrate [27, 51]

Sez. R:	B _V =60.0 cm	B _Z =100.0 cm	L=149.6 cm	L _n =149.6 cm	Terreno: Terrenol
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Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149$ $\sigma_{fa}[\text{kg/cmq}] = 3600$

X	cm	M+	kg·m	M*	kg·m	Afsup	Afinf	cc+	σf+	cc-	σf-	Cb+	Cb-	Ver.	CS
0.0	0.0	--	--	49	12.06	12.06	12.06	--	--	-0	4	8			>100
15.0	15.0	--	--	214	12.06	12.06	12.06	--	--	-0	20	6	2	Si	>100
74.8	74.8	--	--	528	12.06	12.06	12.06	--	--	-1	49	6	8	Si	74.0
134.7	134.7	--	--	677	12.06	12.06	12.06	--	--	-1	35	6	8	Si	>100
149.6	149.6	--	--	269	12.06	12.06	12.06	--	--	-0	25	6	8	Si	>100

Combinazione QP: $\sigma_{ca}[\text{kg/cmq}] = 112 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M _*	Afsup	Afinf	$\sigma_{\text{+}}$	$\sigma_{\text{+}}^{\text{f}}$	$\sigma_{\text{-}}$	$\sigma_{\text{-}}^{\text{f}}$	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	--	31	12.06	12.06	--	--	-0	3	14	14	Si	>100
15.0	--	123	12.06	12.06	--	--	-0	11	14	14	Si	>100
74.8	--	249	12.06	12.06	--	--	-0	23	14	14	Si	>100
134.7	--	40	12.06	12.06	--	--	-0	4	14	14	Si	>100
149.6	57	--	12.06	12.06	-0	5	--	--	14	14	Si	>100

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	cm	M	kg*	Act	mq	Aft	cmq	paft	cm	S _{max}	formed	kg/cmq	Wd	mm	Wk	mm	Cb	Ver.	Cs
	0.0	30	0.1	12.06	30.16	22.4	3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	13(Fr)	Si	>100
	0.0	31	0.1	12.06	30.16	22.4	3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	14(Qp)	Si	>100
	15.0	12.3	0.1	12.06	30.16	22.4	11	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
	15.0	12.3	0.1	12.06	30.16	22.4	11	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	9(Fr)	Si	>100
	74.8	249	0.1	12.06	30.16	22.4	23	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	14(Qp)	Si	>100
	74.8	249	0.1	12.06	30.16	22.4	23	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	0.001	9(Fr)	Si	>100
	134.7	40	0.1	12.06	30.16	22.4	4	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	14(Qp)	Si	>100
	134.7	30	0.1	12.06	30.16	22.4	3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	12(Fr)	Si	>100
	149.6	-57	0.1	12.06	30.16	22.4	5	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	14(Qp)	Si	>100
	149.6	3	0.1	12.06	30.16	22.4	0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	13(Fr)	Si	>100

Trave di Fond.: 9010 | 2, 3 | Pilastrate [51, 50]

Sez. R:	By= 60.0 cm	Bz= 100.0 cm	L= 149.8 cm	Ln= 149.8 cm	Terreno: Terrenol
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Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149$ $\sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M-	M _{sup}	A _{sup}	A _{inf}	σ ₊	σ ₋	σ ₁	Cb+	Cb-	Ver.	CS
0.0	--	--	281	12.06	12.06	--	--	26	6	8	Si	>100
15.0	--	--	376	12.06	12.06	--	--	35	6	8	Si	>100
74.9	--	--	491	12.06	12.06	--	--	45	6	8	Si	79.6
134.8	449	193	12.06	12.06	12.06	-1	41	18	1	8	Si	87.1
149.8	621	55	12.06	12.06	12.06	-1	57	5	1	8	Si	62.9

Combinazione OP: $\sigma_{ca}[\text{kg/cmq}] = 112 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M _*	A ₅₀₀	A ₁₀₀	σ ₊	σ ₋	σ ₊	σ ₋	Cb+	Cb-	Ver.	CS
	cm	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	25	--	12.06	12.06	-0	2	--	--	14	14	Si	>100
15.0	25	--	12.06	12.06	-0	2	--	--	14	14	Si	>100
74.9	179	--	12.06	12.06	-0	17	--	--	14	14	Si	>100
134.8	558	--	12.06	12.06	-1	51	--	--	14	14	Si	70.0
149.8	685	--	12.06	12.06	-1	63	--	--	14	14	Si	57.1

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	σ _{act}	Wd	Wk	Ch	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-8	0.1	12.06	30.16	22.4	1	0.000	0.000	11(Fr)	Si	>100
0.0	-25	0.1	12.06	30.16	22.4	2	0.000	0.000	14(Qp)	Si	>100
15.0	-25	0.1	12.06	30.16	22.4	2	0.000	0.000	14(Qp)	Si	>100
15.0	-4	0.1	12.06	30.16	22.4	0	0.000	0.000	11(Fr)	Si	>100

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Trave di Fond.: 9010 [3, 4] Pilastrate [50, 49]

Sez. R:	$B_y = 60.0$ cm	$B_z = 100.0$ cm	$L = 149.3$ cm	$L_n = 149.3$ cm	Terreno: Terreno I
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Criterio: CLS_TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M _*	A sup	A inf	σ _v	σ _t	σ _c	kg/cmq	Cb+	Cb-	Ver.	CS
cm	kg * m	kg * m	cmq	cmq	kg / cmq	kg / cmq	kg / cmq	kg / cmq				
0.0	585	61	12.06	-1	-1	54	-0	6	1	8	Si	66.7
14.9	554	142	12.06	12.06	-1	51	-0	13	1	8	Si	70.6
74.7	635	227	12.06	12.06	-1	58	-0	21	1	8	Si	61.5
1045	--	--	12.06	-2	96	--	--	--	1	8	Si	37.4
134.3	1198	--	12.06	12.06	-2	110	--	--	1	8	Si	32.6

Combinazione OP: $\sigma_{ca}[\text{kg/cm}^2]=112 \sigma_{fa}[\text{kg/cm}^2]=3600$

X	cm	M ⁺ kg·m	M ⁻ kg·m	A _{sup} cmq	A _{finf} cmq	σ ₊ kg/cmq	σ ₋ kg/cmq	σ _f kg/cmq	Cb+	Cb-	Ver.	CS
0.0	644	--	12.06	-1	59	--	--	--	14	14	Si	60.6
14.9	647	--	12.06	-1	60	--	--	--	14	14	Si	60.4
74.7	776	--	12.06	12.06	-1	72	--	--	14	14	Si	50.3
109.4	1094	--	12.06	-2	101	--	--	--	14	14	Si	35.7
149.3	1203	--	12.06	-2	111	--	--	--	14	14	Si	32.5

Verifica aperture fessure: $W_{amm} \text{ Freq} [\text{mm}] = 0.400 \text{ Wamm } Qp [\text{mm}] = 0.300$

X	M	Act	Aft	cmq	pAft	S _{max}	cm	grind	kg/cmq	Wd	Wk	Cb	Ver.	Cs
cm	kg·m	mq			cm	cm				mm	mm			
0.0	-471	0.1	12.06	30.16	22.4	43	0.003	0.003	13(Ft)	Si	>100			
0.0	-644	0.1	12.06	30.16	22.4	59	0.004	0.004	14(Qp)	Si	79.1			
14.9	-647	0.1	12.06	30.16	22.4	60	0.004	0.004	14(Qp)	Si	78.7			
14.9	-459	0.1	12.06	30.16	22.4	42	0.003	0.003	13(Ft)	Si	>100			
74.7	-776	0.1	12.06	30.16	22.4	72	0.005	0.005	14(Qp)	Si	65.6			
74.7	-542	0.1	12.06	30.16	22.4	50	0.003	0.003	13(Ft)	Si	>100			
134.4	-1094	0.1	12.06	30.16	22.4	101	0.006	0.006	14(Qp)	Si	46.5			
134.4	-832	0.1	12.06	30.16	22.4	77	0.005	0.005	13(Ft)	Si	81.6			
149.3	-1203	0.1	12.06	30.16	22.4	111	0.007	0.007	14(Qp)	Si	42.3			
149.3	-936	0.1	12.06	30.16	22.4	86	0.006	0.006	13(Ft)	Si	72.6			

Trave di Fond.: 9010 [4, 5 | Pilastrate [49, 48]

Sez. R:	$B_y=60.0\text{ cm}$	$B_z=100.0\text{ cm}$	$L=148.5\text{ cm}$	$L_n=148.5\text{ cm}$	Terreno: Terreno I
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Criterio: CLS_TraviFondazione

Combinazione Rara: $\sigma_{ca}[\text{kg/cmq}] = 149 \sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M _*	A _{sup}	A _{inf}	α ₊	σ ₊	α ₋	σ ₋	Cb+	Cb-	Ver.	CS
cm	kg ⁹ m	kg ⁹ m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1173		12.06	12.06	-2	108	--	--	1	8	Si	33.3
14.8	1118		12.06	12.06	-2	103	--	--	1	8	Si	34.9
74.2	1100	0	12.06	12.06	-2	101	-0	0	1	8	Si	35.5
1408			12.06	12.06	-2	130	--	--	1	8	Si	27.7
133.6			12.06	12.06	-2	142	--	--	1	8	Si	25.4
148.5	1537	--	12.06	12.06	-2	142	--	--	1	8	Si	25.4

Combinazione QP: $\sigma_{ca}[\text{kg/cmq}] = 112 \quad \sigma_{fa}[\text{kg/cmq}] = 3600$

X	M+	M-	A _{sup}	A _{inf}	α ₊	α ₋	σ ₊	σ ₋	Cb+	Cb-	Ver	CS
	kg ⁺ m	kg ⁻ m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1172	--	12.06	12.06	-2	108	--	--	14	14	Si	33.3
14.8	1152	--	12.06	12.06	-2	106	--	--	14	14	Si	33.9
74.2	1186	--	12.06	12.06	-2	109	--	--	14	14	Si	32.9
133.6	1412	--	12.06	12.06	-2	130	--	--	14	14	Si	27.7
148.5	1499	--	12.06	12.06	-2	138	--	--	14	14	Si	26.1

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Verifica aperture fessure: Wamm. Freq[mm]=0.400 Wamm. Qp[mm]=0.300

X	M	Act	Aft	paft	S _{max}	Wd	Wk	Cb	Ver.	Cs
cm	kg*in	mq	cmq	cm	cm	mm	mm			
0.0	-913	0.1	12.06	30.16	22.4	0.005	0.005	13(Fr)	Si	74.4
0.0	-1172	0.1	12.06	30.16	22.4	0.007	0.007	14(Qp)	Si	43.5
14.8	-1152	0.1	12.06	30.16	22.4	0.007	0.007	14(Qp)	Si	44.2
14.8	-883	0.1	12.06	30.16	22.4	0.005	0.005	13(Fr)	Si	76.9
74.2	-1186	0.1	12.06	30.16	22.4	0.007	0.007	14(Qp)	Si	42.9
74.2	-889	0.1	12.06	30.16	22.4	0.005	0.005	13(Fr)	Si	76.4
133.6	-1412	0.1	12.06	30.16	22.4	0.008	0.008	14(Qp)	Si	36.1
133.6	-1101	0.1	12.06	30.16	22.4	0.006	0.006	13(Fr)	Si	61.7
148.5	-1499	0.1	12.06	30.16	22.4	0.009	0.009	14(Qp)	Si	34.0
148.5	-1187	0.1	12.06	30.16	22.4	0.007	0.007	13(Fr)	Si	57.2

Trave di Fond. : 9010 | 5. 6 | Pilastrate [48. 47]

Sez. R: By= 60.0 cm Bz=100.0 cm L=150.1 cm Ln=150.1 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M-		M+		Afsup		Afinf		σ _c ⁺		σ _f ⁺		σ _c ⁻		σ _f ⁻		Cb+		Cb-		Ver.		CS	
	cm	kg ² m	cmq	kg ² m	cmq	kg/cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq
0.0	1523	--	12.06	12.06	-2	140	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
15.0	1442	--	12.06	12.06	-2	133	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
75.0	1328	--	12.06	12.06	-2	122	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
135.0	1562	--	12.06	12.06	-2	144	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
150.1	1675	--	12.06	12.06	-3	154	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

X	Mz	Me	Afsup	Afinf	σc ⁺	σf ⁺	σc ⁻	σf ⁻	Cb ⁺	Cb ⁻	Ver.	Cs
cm	kg*m	kg*μm	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1477	--	12.06	12.06	-2	136	--	--	14	14	Si	26.4
15.0	1435	--	12.06	12.06	-2	132	--	--	14	14	Si	27.2
75.0	1391	--	12.06	12.06	-2	128	--	--	14	14	Si	28.1
135.0	1557	--	12.06	12.06	-2	144	--	--	14	14	Si	25.1
150.1	1632	--	12.06	12.06	-3	150	--	--	14	14	Si	23.9

Verifica aperture fessure: Wamm. Freq[mm]=0.400 Wamm. Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	σ _f ⁺	Wd	Wk	Ch	Ver.	Cs
cm	kg·m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-1172	0.1	12.06	30.16	22.4	108	0.007	0.007	13(Fr)	Si	57.9
0.0	-1477	0.1	12.06	30.16	22.4	136	0.009	0.009	14(Qp)	Si	34.5
15.0	-1435	0.1	12.06	30.16	22.4	132	0.008	0.008	14(Qp)	Si	35.5
15.0	-1123	0.1	12.06	30.16	22.4	104	0.007	0.007	13(Fr)	Si	60.5
75.0	-1391	0.1	12.06	30.16	22.4	128	0.008	0.008	14(Qp)	Si	36.6
75.0	-1062	0.1	12.06	30.16	22.4	98	0.006	0.006	13(Fr)	Si	64.0
135.0	-1557	0.1	12.06	30.16	22.4	144	0.009	0.009	14(Qp)	Si	32.7
135.0	-1222	0.1	12.06	30.16	22.4	113	0.007	0.007	13(Fr)	Si	55.6
150.1	-1632	0.1	12.06	30.16	22.4	150	0.010	0.010	14(Qp)	Si	31.2
150.1	-1297	0.1	12.06	30.16	22.4	120	0.008	0.008	13(Fr)	Si	52.4

Trave di Fond. : 9010 | 6. 7 | Pilastrate [47. 46]

Sez. R: By= 60.0 cm Bz=100.0 cm L=148.1 cm Ln=148.1 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

X	M-		M+		Afsup		Afinf		σ _c ⁺		σ _f ⁺		σ _c ⁻		σ _f ⁻		Cb+	Cb-	Ver.	CS
	cm	kg* m	cmq	kg* m	cmq	kg/cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq								
0.0	1673	--	12.06	12.06	-3	154	--	--	--	--	--	--	--	--	--	--	1	8	Si	23.4
14.8	1577	--	12.06	12.06	-2	145	--	--	--	--	--	--	--	--	--	--	1	8	Si	24.8
74.0	1412	--	12.06	12.06	-2	130	--	--	--	--	--	--	--	--	--	--	1	8	Si	27.7
133.2	1598	--	12.06	12.06	-2	147	--	--	--	--	--	--	--	--	--	--	1	8	Si	24.4
148.1	1700	--	12.06	12.06	-3	157	--	--	--	--	--	--	--	--	--	--	1	8	Si	23.0

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

Combinazione QP: σca[kg/cmq]=112 σfa[kg/cmq]=3600

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X	M+	M-	Afsup	Afinf	σ _c ⁺	σ _f ⁺	σ _c ⁻	σ _f ⁻	Cb+	Cb-	Ver.	CS
	cm	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1617	--	12.06	12.06	-2	149	--	--	14	14	Si	24.2
14.8	1562	--	12.06	12.06	-2	144	--	--	14	14	Si	25.0
74.0	1475	--	12.06	12.06	-2	136	--	--	14	14	Si	26.5
133.2	1604	--	12.06	12.06	-2	148	--	--	14	14	Si	24.4
148.1	1669	--	12.06	12.06	-3	154	--	--	14	14	Si	23.4

Verifica aperture fessure: Wamm. Freq[mm]=0.400 Wamm. Qp[mm]=0.300

X	M		Act	mq	cmq	pAft	cm	S _{max}	cm	kg/cm ²	Wd	Wk	Cb	Ver.	Cs
	cm	kg* ^m													
0.0	-1289	0.1	12.06	30.16	22.4	119	0.008	0.008	13(Fr)	Si	52.7				
0.0	-1617	0.1	12.06	30.16	22.4	149	0.010	0.010	14(Qp)	Si	31.5				
14.8	-1562	0.1	12.06	30.16	22.4	144	0.009	0.009	14(Qp)	Si	32.6				
14.8	-1430	0.1	12.06	30.16	22.4	113	0.007	0.007	13(Fr)	Si	55.2				
74.0	-1475	0.1	12.06	30.16	22.4	136	0.009	0.009	14(Qp)	Si	34.5				
74.0	-1132	0.1	12.06	30.16	22.4	104	0.007	0.007	13(Fr)	Si	60.0				
133.2	-1604	0.1	12.06	30.16	22.4	148	0.009	0.009	14(Qp)	Si	31.8				
133.2	-1259	0.1	12.06	30.16	22.4	116	0.007	0.007	13(Fr)	Si	54.0				
148.1	-1669	0.1	12.06	30.16	22.4	154	0.010	0.010	14(Qp)	Si	30.5				
148.1	-1326	0.1	12.06	30.16	22.4	122	0.008	0.008	13(Fr)	Si	51.2				

Trave di Fond. : 9010 | 7. 8 | Pilastrate [46. 45]

Sez. R: By= 60.0 cm Bz=100.0 cm L=152.6 cm Ln=152.6 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: σca[kg/cmq]=149 σfa[kg/cmq]=3600

Conformazione karstica: 0,04 g/cm ³ - 1,47 g/cm ³ - 2000																						
X	M-	M+	M-	Afsup	cmq	cmq	Afinf	σ ⁺ kg/cmq	σ ⁺ kg/cmq	σ _c kg/cmq	σ _f kg/cmq	Cb+	Cb-	Ver.	CS							
cm	kg·m	kg·m	kg·m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq											
0,0	1705	--	--	12,06	12,06	--	3	157	--	--	--	1	8	Si	22,9							
0,5	1603	--	--	12,06	12,06	--	2	148	--	--	--	--	--	--	--							
15,3	1603	--	--	12,06	12,06	--	2	148	--	--	--	1	8	Si	24,4							
76,3	1430	--	--	12,06	12,06	--	1,32	--	--	--	--	1	8	Si	27,3							
137,3	1638	--	--	12,06	12,06	--	-3	151	--	--	--	1	8	Si	23,8							
152,6	1750	--	--	12,06	12,06	--	-3	161	--	--	--	1	8	Si	22,3							

X	M+	M-	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Cb+	Cb-	Ver.	CS
0.0	1759	--	12.06	12.06	-3	162	--	1	8	Si	22.2
14.8	1645	--	12.06	12.06	-3	152	--	1	8	Si	23.7
73.8	1416	--	12.06	12.06	-2	131	--	1	8	Si	27.6
132.8	1548	--	12.06	12.06	-2	143	--	1	8	Si	25.2
147.5	1637	--	12.06	12.06	-3	151	--	1	8	Si	23.9

Combinazione QP: σ_{cal}[kg/cmq]=112 σ_{fal}[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1620	--	12.06	12.06	-3	149	--	14	14	Si	24.1
14.8	1551	--	12.06	12.06	-2	143	--	14	14	Si	25.2
73.8	1413	--	12.06	12.06	-2	130	--	14	14	Si	27.6
132.8	1499	--	12.06	12.06	-2	138	--	14	14	Si	26.1
147.5	1554	--	12.06	12.06	-2	143	--	14	14	Si	25.1

Verifica aperture fessure: W_{amm} Freq[mm]=0.400 W_{amm} Qp[mm]=0.300

X	M	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	kg/cmq	mm	mm				
0.0	-1322	0.1	12.06	30.16	22.4	122	0.008	0.008	13(Fr)	Si	51.4
0.0	-1620	0.1	12.06	30.16	22.4	149	0.010	0.010	14(Qp)	Si	31.5
14.8	-1551	0.1	12.06	30.16	22.4	143	0.009	0.009	14(Qp)	Si	32.8
14.8	-1250	0.1	12.06	30.16	22.4	115	0.007	0.007	13(Fr)	Si	54.3
73.8	-1413	0.1	12.06	30.16	22.4	130	0.008	0.008	14(Qp)	Si	36.0
73.8	-1105	0.1	12.06	30.16	22.4	102	0.007	0.007	13(Fr)	Si	61.4
132.8	-1499	0.1	12.06	30.16	22.4	138	0.009	0.009	14(Qp)	Si	34.0
132.8	-1193	0.1	12.06	30.16	22.4	110	0.007	0.007	13(Fr)	Si	56.9
147.5	-1554	0.1	12.06	30.16	22.4	143	0.009	0.009	14(Qp)	Si	32.8
147.5	-1250	0.1	12.06	30.16	22.4	115	0.007	0.007	13(Fr)	Si	54.3

Trave di Fond. : 9010 | 9, 10 | Pilastrate [44, 43]

Sez. R: B_y= 60.0 cm B_z=100.0 cm L=149.8 cm L_n=149.8 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: σ_{cal}[kg/cmq]=149 σ_{fal}[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1649	--	12.06	12.06	-3	152	--	1	8	Si	23.7
15.0	1537	--	12.06	12.06	-2	142	--	1	8	Si	25.4
74.9	1322	--	12.06	12.06	-2	122	--	1	8	Si	29.6
134.8	1478	--	12.06	12.06	-2	136	--	1	8	Si	26.4
149.8	1574	--	12.06	12.06	-2	145	--	1	8	Si	24.8

Combinazione QP: σ_{cal}[kg/cmq]=112 σ_{fal}[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1548	--	12.06	12.06	-2	143	--	14	14	Si	25.2
15.0	1482	--	12.06	12.06	-2	137	--	14	14	Si	26.4
74.9	1358	--	12.06	12.06	-2	125	--	14	14	Si	28.8
134.8	1464	--	12.06	12.06	-2	135	--	14	14	Si	26.7
149.8	1526	--	12.06	12.06	-2	141	--	14	14	Si	25.6

Verifica aperture fessure: W_{amm} Freq[mm]=0.400 W_{amm} Qp[mm]=0.300

X	M	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	kg/cmq	mm	mm				
0.0	-1251	0.1	12.06	30.16	22.4	115	0.007	0.007	13(Fr)	Si	54.3
0.0	-1548	0.1	12.06	30.16	22.4	143	0.009	0.009	14(Qp)	Si	32.9
15.0	-1482	0.1	12.06	30.16	22.4	137	0.009	0.009	14(Qp)	Si	34.4
15.0	-1181	0.1	12.06	30.16	22.4	109	0.007	0.007	13(Fr)	Si	57.5
74.9	-1358	0.1	12.06	30.16	22.4	125	0.008	0.008	14(Qp)	Si	37.5
74.9	-1047	0.1	12.06	30.16	22.4	97	0.006	0.006	13(Fr)	Si	64.8
134.8	-1464	0.1	12.06	30.16	22.4	135	0.009	0.009	14(Qp)	Si	34.8
134.8	-1153	0.1	12.06	30.16	22.4	106	0.007	0.007	13(Fr)	Si	58.9
149.8	-1526	0.1	12.06	30.16	22.4	141	0.009	0.009	14(Qp)	Si	33.4
149.8	-1216	0.1	12.06	30.16	22.4	112	0.007	0.007	13(Fr)	Si	55.8

Trave di Fond. : 9010 | 10, 11 | Pilastrate [43, 42]

Sez. R: B_y= 60.0 cm B_z=100.0 cm L=149.6 cm L_n=149.6 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: σ_{cal}[kg/cmq]=149 σ_{fal}[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1586	--	12.06	12.06	-2	146	--	1	8	Si	24.6
15.0	1482	--	12.06	12.06	-2	137	--	1	8	Si	26.4
74.8	1291	--	12.06	12.06	-2	119	--	1	8	Si	30.3
134.7	1465	--	12.06	12.06	-2	135	--	1	8	Si	26.7
149.6	1565	--	12.06	12.06	-2	144	--	1	8	Si	25.0

Combinazione QP: σ_{cal}[kg/cmq]=112 σ_{fal}[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1522	--	12.06	12.06	-2	140	--	14	14	Si	25.7
15.0	1461	--	12.06	12.06	-2	135	--	14	14	Si	26.7
74.8	1355	--	12.06	12.06	-2	125	--	14	14	Si	28.8
134.7	1475	--	12.06	12.06	-2	136	--	14	14	Si	26.5
149.6	1540	--	12.06	12.06	-2	142	--	14	14	Si	25.4

Verifica aperture fessure: W_{amm} Freq[mm]=0.400 W_{amm} Qp[mm]=0.300

X	M	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	kg/cmq	mm	mm				
0.0	-1219	0.1	12.06	30.16	22.4	112	0.007	0.007	13(Fr)	Si	55.7
0.0	-1522	0.1	12.06	30.16	22.4	140	0.009	0.009	14(Qp)	Si	33.5
15.0	-1461	0.1	12.06	30.16	22.4	135	0.009	0.009	14(Qp)	Si	34.9
15.0	-1153	0.1	12.06	30.16	22.4	106	0.007	0.007	13(Fr)	Si	58.9
74.8	-1355	0.1	12.06	30.16	22.4	125	0.008	0.008	14(Qp)	Si	37.6
74.8	-1037	0.1	12.06	30.16	22.4	96	0.006	0.006	13(Fr)	Si	65.5
134.7	-1475	0.1	12.06	30.16	22.4	136	0.009	0.009	14(Qp)	Si	34.5
134.7	-1156	0.1	12.06	30.16	22.4	107	0.007	0.007	13(Fr)	Si	58.8
149.6	-1540	0.1	12.06	30.16	22.4	142	0.009	0.009	14(Qp)	Si	33.1
149.6	-1221	0.1	12.06	30.16	22.4	113	0.007	0.007	13(Fr)	Si	55.6

Trave di Fond. : 9010 | 11, 12 | Pilastrate [42, 41]

Sez. R: B_y= 60.0 cm B_z=100.0 cm L=149.0 cm L_n=149.0 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: σ_{cal}[kg/cmq]=149 σ_{fal}[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1586	--	12.06	12.06	-2	146	--	1	8	Si	24.6
14.9	1478	--	12.06	12.06	-2	136	--	1	8	Si	26.4
74.5	1272	--	12.06	12.06	-2	117	--	1	8	Si	30.7
134.1	1421	--	12.06	12.06	-2	131	--	1	8	Si	27.5
149.0	1514	--	12.06	12.06	-2	140	--	1	8	Si	25.8

Combinazione QP: σ_{cal}[kg/cmq]=112 σ_{fal}[kg/cmq]=3600

X	M+	M-	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Cb+	Cb-	Ver.	CS
cm	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1543	--	12.06	12.06	-2	142	--	14	14	Si	25.3
14.9	1479	--	12.06	12.06	-2	136	--	14	14	Si	26.4
74.5	1361	--	12.06	12.06	-2	125	--	14	14	Si	28.7
134.1	1464	--	12.06	12.06	-2	135	--	14	14	Si	26.7
149.0	1524	--	12.06	12.06	-2	140	--	14	14	Si	25.6

Verifica aperture fessure: W_{amm} Freq[mm]=0.400 W_{amm} Qp[mm]=0.300

X	M	M _{sup}	A _{finf}	A _{finf}	σ _{c+}	σ _{f-}	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	kg/cmq	mm	mm				
0.0	-1230	0.1	12.06	30.16	22.4	113	0.007	0.007	13(Fr)	Si	55.2
0.0	-1543	0.1	12.06	30.16	22.4	142	0.009	0.009	14(Qp)	Si	33.0
14.9	-1479	0.1	12.06	30.16	22.4	136	0.009	0.009	14(Qp)	Si	34.4

X	M	Act	Aft	Afsup	efmed	Wd	Wk	Cb	Ver.	Cs
14.9	-1162	0.1	12.06	30.16	22.4	107	0.007	0.007	13(Fr)	58.4
74.5	-1361	0.1	12.06	30.16	22.4	125	0.008	0.008	14(Op)	37.4
74.5	-1034	0.1	12.06	30.16	22.4	95	0.006	0.006	13(Fr)	65.7
134.1	-1464	0.1	12.06	30.16	22.4	135	0.009	0.009	14(Op)	34.8
134.1	-1135	0.1	12.06	30.16	22.4	105	0.007	0.007	13(Fr)	59.8
149.0	-1524	0.1	12.06	30.16	22.4	140	0.009	0.009	14(Op)	33.4
149.0	-1196	0.1	12.06	30.16	22.4	110	0.007	0.007	13(Fr)	56.8

Trave di Fond. : 9010 | 12, 13 | Pilastrate [41, 40]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.7 cm Ln= 149.7 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: scalkg/cmq]=149 sfalkg/cmq]=3600

X	M+	M-	Act	Aft	Afsup	Afinf	sc+	sc-	sf+	sf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1533	--	12.06	12.06	12.06	-2	141	--	--	--	1	8	Si	25.5
15.0	1429	--	12.06	12.06	12.06	-2	132	--	--	--	1	8	Si	27.3
74.8	1235	--	12.06	12.06	12.06	-2	114	--	--	--	1	8	Si	31.6
134.7	1397	--	12.06	12.06	12.06	-2	129	--	--	--	1	8	Si	28.0
149.7	1493	--	12.06	12.06	12.06	-2	138	--	--	--	1	8	Si	26.2

Combinazione QP: scalkg/cmq]=112 sfalkg/cmq]=3600

X	M+	M-	Act	Aft	Afsup	Afinf	sc+	sc-	sf+	sf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1525	--	12.06	12.06	12.06	-2	141	--	--	--	14	14	Si	25.6
15.0	1463	--	12.06	12.06	12.06	-2	135	--	--	--	14	14	Si	26.7
74.8	1352	--	12.06	12.06	12.06	-2	125	--	--	--	14	14	Si	28.9
134.7	1461	--	12.06	12.06	12.06	-2	135	--	--	--	14	14	Si	26.7
149.7	1523	--	12.06	12.06	12.06	-2	140	--	--	--	14	14	Si	25.7

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qpl[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	defined	Wd	Wk	Cb	Ver.	Cs
cm	kg·m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-1203	0.1	12.06	30.16	22.4	111	0.007	0.007	13(Fr)	Si	56.4
0.0	-1525	0.1	12.06	30.16	22.4	141	0.009	0.009	14(Qp)	Si	33.4
15.0	-1463	0.1	12.06	30.16	22.4	135	0.009	0.009	14(Qp)	Si	34.8
15.0	-1137	0.1	12.06	30.16	22.4	105	0.007	0.007	13(Fr)	Si	59.7
74.8	-1352	0.1	12.06	30.16	22.4	125	0.008	0.008	14(Qp)	Si	37.7
134.7	-1017	0.1	12.06	30.16	22.4	135	0.006	0.006	13(Fr)	Si	66.8
134.7	-1461	0.1	12.06	30.16	22.4	94	0.009	0.009	14(Qp)	Si	34.9
134.7	-1127	0.1	12.06	30.16	22.4	104	0.007	0.007	13(Fr)	Si	60.3
149.7	-1523	0.1	12.06	30.16	22.4	140	0.009	0.009	14(Qp)	Si	33.5
149.7	-1189	0.1	12.06	30.16	22.4	110	0.007	0.007	13(Fr)	Si	57.1

Trave di Fond. : 9010 | 13, 14 | Pilastrate [40, 39]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.1 cm Ln= 149.1 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: scalkg/cmq]=149 sfalkg/cmq]=3600

X	M+	M-	Act	Aft	Afsup	Afinf	sc+	sc-	sf+	sf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1521	--	12.06	12.06	12.06	-2	140	--	--	--	1	8	Si	25.7
14.9	1429	--	12.06	12.06	12.06	-2	132	--	--	--	1	8	Si	27.3
74.5	1279	--	12.06	12.06	12.06	-2	118	--	--	--	1	8	Si	30.5
134.1	1484	--	12.06	12.06	12.06	-2	137	--	--	--	1	8	Si	26.3
149.1	1590	--	12.06	12.06	12.06	-2	147	--	--	--	1	8	Si	24.6

Combinazione QP: scalkg/cmq]=112 sfalkg/cmq]=3600

X	M+	M-	Act	Aft	Afsup	Afinf	sc+	sc-	sf+	sf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1533	--	12.06	12.06	12.06	-2	141	--	--	--	14	14	Si	25.5
14.9	1470	--	12.06	12.06	12.06	-2	136	--	--	--	14	14	Si	26.6
74.5	1356	--	12.06	12.06	12.06	-2	125	--	--	--	14	14	Si	28.8
134.1	1460	--	12.06	12.06	12.06	-2	135	--	--	--	14	14	Si	26.8

X	M+	M-	Afsup	Afinf	sc+	sc-	sf+	sf-	Cb+	Cb-	Ver.	Cs
149.1	1520	--	12.06	12.06	-2	140	--	--	14	14	Si	25.7

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qpl[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-1204	0.1	12.06	30.16	22.4	111	0.007	0.007	13(Fr)	Si	56.4
0.0	-1533	0.1	12.06	30.16	22.4	141	0.009	0.009	14(Qp)	Si	33.2
14.9	-1470	0.1	12.06	30.16	22.4	136	0.009	0.009	14(Qp)	Si	34.6
14.9	-1141	0.1	12.06	30.16	22.4	105	0.007	0.007	13(Fr)	Si	59.5
74.5	-1356	0.1	12.06	30.16	22.4	125	0.008	0.008	14(Qp)	Si	37.6
74.5	-1034	0.1	12.06	30.16	22.4	95	0.006	0.006	13(Fr)	Si	65.7
134.1	-1460	0.1	12.06	30.16	22.4	135	0.009	0.009	14(Qp)	Si	34.9
134.1	-1155	0.1	12.06	30.16	22.4	106	0.007	0.007	13(Fr)	Si	58.8
149.1	-1520	0.1	12.06	30.16	22.4	140	0.009	0.009	14(Qp)	Si	33.5
149.1	-1221	0.1	12.06	30.16	22.4	113	0.007	0.007	13(Fr)	Si	55.6

Trave di Fond. : 9010 | 14, 15 | Pilastrate [39, 38]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.4 cm Ln= 149.4 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: scalkg/cmq]=149 sfalkg/cmq]=3600

X	M+	M-	Act	Aft	Afsup	Afinf	sc+	sc-	sf+	sf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1606	--	12.06	12.06	12.06	-2	148	--	--	--	1	8	Si	24.3
14.9	1499	--	12.06	12.06	12.06	-2	138	--	--	--	1	8	Si	26.1
74.7	1291	--	12.06	12.06	12.06	-2	119	--	--	--	1	8	Si	30.3
134.4	1440	--	12.06	12.06	12.06	-2	133	--	--	--	1	8	Si	27.1
149.4	1533	--	12.06	12.06	12.06	-2	141	--	--	--	1	8	Si	25.5

Combinazione QP: scalkg/cmq]=112 sfalkg/cmq]=3600

X	M+	M-	Act	Aft	Afsup	Afinf	sc+	sc-	sf+	sf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1518	--	12.06	12.06	12.06	-2	140	--	--	--	14	14	Si	25.7
14.9	1454	--	12.06	12.06	12.06	-2	134	--	--	--	14	14	Si	26.9
74.7	1334	--	12.06	12.06	12.06	-2	123	--	--	--	14	14	Si	29.3
134.4	1434	--	12.06	12.06	12.06	-2	132	--	--	--	14	14	Si	27.2
149.4	1493	--	12.06	12.06	12.06	-2	138	--	--	--	14	14	Si	26.2

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qpl[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	efmed	Wd	Wk	Cb	Ver.	Cs
cm	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-1225	0.1	12.06	30.16	22.4	113	0.007	0.007	13(Fr)	Si	55.4
0.0	-1518	0.1	12.06	30.16	22.4	140	0.009	0.009	14(Qp)	Si	33.5
14.9	-1454	0.1	12.06	30.16	22.4	134	0.009	0.009	14(Qp)	Si	35.0
14.9	-1157	0.1	12.06	30.16	22.4	107	0.007	0.007	13(Fr)	Si	58.7
74.7	-1334	0.1	12.06	30.16	22.4	123	0.008	0.008	14(Qp)	Si	38.2
74.7	-1028	0.1	12.06	30.16	22.4	95	0.006	0.006	13(Fr)	Si	66.1
134.4	-1434	0.1	12.06	30.16	22.4	132	0.008	0.008	14(Qp)	Si	35.5
134.4	-1128	0.1	12.06	30.16	22.4	104	0.007	0.007	13(Fr)	Si	60.2
149.4	-1493	0.1	12.06	30.16	22.4	138	0.009	0.009	14(Qp)	Si	34.1
149.4	-1188	0.1	12.06	30.16	22.4	109	0.007	0.007	13(Fr)	Si	57.2

Trave di Fond. : 9010 | 15, 16 | Pilastrate [38, 37]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.7 cm Ln= 149.7 cm Terreno: Terreno1

Criterio : CLS_TraviFondazione

Combinazione Rara: scalkg/cmq]=149 sfalkg/cmq]=3600

X	M+	M-	Act	Aft	Afsup	Afinf	sc+	sc-	sf+	sf-	Cb+	Cb-	Ver.	Cs
cm	kg*m	kg*m	cmq	cmq	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1553	--	12.06	12.06	12.06	-2	143	--	--	--	1	8	Si	25.2
15.0	1449	--	12.06	12.06	12.06	-2	134	--	--	--	1	8	Si	27.0
74.9	1252	--	12.06	12.06	12.06	-2	115	--	--	--	1	8	Si	31.2
134.8	1413	--	12.06	12.06	12.06	-2	130	--	--	--	1	8	Si	27.6
149.7	1509	--	12.06	12.06	12.06	-2	139	--	--	--	1	8	Si	25.9

X	M	Act	Aft	pAft	S _{max}	erfmed	Wd	Wk	Cb	Ver.	Cs
149.0	-1247	0.1	12.06	30.16	22.4	115	0.007	0.007	13(Fr)	Si	54.5

Trave di Fond. : 9010 | 19 , 20 | Pilastrate [34 , 33]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.3 cm Ln= 149.3 cm Terreno: Terrenol

Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{c-}	σ_{f+}	σ_{f-}	Cb+	Cb-	Ver.	CS
	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1636	--	12.06	12.06	-3	151	--	--	1	8	Si	23.9
14.9	1531	--	12.06	12.06	-2	141	--	--	1	8	Si	25.5
74.6	1338	--	12.06	12.06	-2	123	--	--	1	8	Si	29.2
134.4	1507	--	12.06	12.06	-2	139	--	--	1	8	Si	25.9
149.3	1605	--	12.06	12.06	-2	148	--	--	1	8	Si	24.3

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{c-}	σ_{f+}	σ_{f-}	Cb+	Cb-	Ver.	CS
	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1566	--	12.06	12.06	-2	144	--	--	14	14	Si	24.9
14.9	1504	--	12.06	12.06	-2	139	--	--	14	14	Si	26.0
74.6	1396	--	12.06	12.06	-2	129	--	--	14	14	Si	28.0
134.4	1512	--	12.06	12.06	-2	139	--	--	14	14	Si	25.8
149.3	1575	--	12.06	12.06	-2	145	--	--	14	14	Si	24.8

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	erfmed	Wd	Wk	Cb	Ver.	Cs
	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-1257	0.1	12.06	30.16	22.4	116	0.007	0.007	13(Fr)	Si	54.0
0.0	-1566	0.1	12.06	30.16	22.4	144	0.009	0.009	14(Qp)	Si	32.5
14.9	-1504	0.1	12.06	30.16	22.4	139	0.009	0.009	14(Qp)	Si	33.9
14.9	-1191	0.1	12.06	30.16	22.4	110	0.007	0.007	13(Fr)	Si	57.0
74.6	-1396	0.1	12.06	30.16	22.4	129	0.008	0.008	14(Qp)	Si	36.5
134.4	-1071	0.1	12.06	30.16	22.4	99	0.006	0.006	13(Fr)	Si	63.4
149.3	-1512	0.1	12.06	30.16	22.4	139	0.009	0.009	14(Qp)	Si	33.7
134.4	-1184	0.1	12.06	30.16	22.4	109	0.007	0.007	13(Fr)	Si	57.3
149.3	-1575	0.1	12.06	30.16	22.4	145	0.009	0.009	14(Qp)	Si	32.3
149.3	-1249	0.1	12.06	30.16	22.4	115	0.007	0.007	13(Fr)	Si	54.4

Trave di Fond. : 9010 | 20 , 21 | Pilastrate [33 , 32]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.9 cm Ln= 149.9 cm Terreno: Terrenol

Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{c-}	σ_{f+}	σ_{f-}	Cb+	Cb-	Ver.	CS
	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1636	--	12.06	12.06	-3	151	--	--	1	8	Si	23.9
15.0	1531	--	12.06	12.06	-2	141	--	--	1	8	Si	25.5
75.0	1338	--	12.06	12.06	-2	123	--	--	1	8	Si	29.2
134.9	1504	--	12.06	12.06	-2	139	--	--	1	8	Si	26.0
149.9	1600	--	12.06	12.06	-2	147	--	--	1	8	Si	24.4

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{c-}	σ_{f+}	σ_{f-}	Cb+	Cb-	Ver.	CS
	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1582	--	12.06	12.06	-2	146	--	--	14	14	Si	24.7
15.0	1522	--	12.06	12.06	-2	140	--	--	14	14	Si	25.7
75.0	1418	--	12.06	12.06	-2	131	--	--	14	14	Si	27.5
134.9	1533	--	12.06	12.06	-2	141	--	--	14	14	Si	25.5
149.9	1595	--	12.06	12.06	-2	147	--	--	14	14	Si	24.5

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	erfmed	Wd	Wk	Cb	Ver.	Cs
	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-1262	0.1	12.06	30.16	22.4	116	0.007	0.007	13(Fr)	Si	53.8

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X	M	Act	Aft	pAft	S _{max}	erfmed	Wd	Wk	Cb	Ver.	Cs
0.0	-1582	0.1	12.06	30.16	22.4	146	0.009	0.009	14(Qp)	Si	32.2
15.0	-1522	0.1	12.06	30.16	22.4	140	0.009	0.009	14(Qp)	Si	33.5
15.0	-1197	0.1	12.06	30.16	22.4	110	0.007	0.007	13(Fr)	Si	56.7
75.0	-1418	0.1	12.06	30.16	22.4	131	0.008	0.008	14(Qp)	Si	35.9
75.0	-1080	0.1	12.06	30.16	22.4	100	0.006	0.006	13(Fr)	Si	62.9
134.9	-1533	0.1	12.06	30.16	22.4	141	0.009	0.009	14(Qp)	Si	33.2
134.9	-1192	0.1	12.06	30.16	22.4	110	0.007	0.007	13(Fr)	Si	57.0
149.9	-1595	0.1	12.06	30.16	22.4	147	0.009	0.009	14(Qp)	Si	31.9
149.9	-1255	0.1	12.06	30.16	22.4	116	0.007	0.007	13(Fr)	Si	54.1

Trave di Fond. : 9010 | 21 , 22 | Pilastrate [32 , 31]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 148.9 cm Ln= 148.9 cm Terreno: Terrenol

Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{c-}	σ_{f+}	σ_{f-}	Cb+	Cb-	Ver.	CS
	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1638	--	12.06	12.06	-3	151	--	--	1	8	Si	23.9
14.9	1526	--	12.06	12.06	-2	141	--	--	1	8	Si	25.6
74.5	1292	--	12.06	12.06	-2	119	--	--	1	8	Si	30.2
134.0	1398	--	12.06	12.06	-2	129	--	--	1	8	Si	27.9
148.9	1477	--	12.06	12.06	-2	136	--	--	1	8	Si	26.4

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{c-}	σ_{f+}	σ_{f-}	Cb+	Cb-	Ver.	CS
	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1608	--	12.06	12.06	-2	148	--	--	14	14	Si	24.3
14.9	1541	--	12.06	12.06	-2	142	--	--	14	14	Si	25.4
74.5	1398	--	12.06	12.06	-2	129	--	--	14	14	Si	27.9
134.0	1459	--	12.06	12.06	-2	134	--	--	14	14	Si	26.8
148.9	1504	--	12.06	12.06	-2	139	--	--	14	14	Si	26.0

Verifica aperture fessure: Wamm Freq[mm]=0.400 Wamm Qp[mm]=0.300

X	M	Act	Aft	pAft	S _{max}	erfmed	Wd	Wk	Cb	Ver.	Cs
	kg*m	mq	cmq	cm	cm	kg/cmq	mm	mm			
0.0	-1274	0.1	12.06	30.16	22.4	117	0.008	0.008	13(Fr)	Si	53.3
0.0	-1608	0.1	12.06	30.16	22.4	148	0.009	0.009	14(Qp)	Si	31.7
14.9	-1541	0.1	12.06	30.16	22.4	142	0.009	0.009	14(Qp)	Si	33.1
14.9	-1203	0.1	12.06	30.16	22.4	111	0.007	0.007	13(Fr)	Si	56.5
74.5	-1398	0.1	12.06	30.16	22.4	129	0.008	0.008	14(Qp)	Si	36.4
74.5	-1053	0.1	12.06	30.16	22.4	97	0.006	0.006	13(Fr)	Si	64.5
134.0	-1459	0.1	12.06	30.16	22.4	134	0.009	0.009	14(Qp)	Si	34.9
134.0	-1120	0.1	12.06	30.16	22.4	103	0.007	0.007	13(Fr)	Si	60.6
148.9	-1504	0.1	12.06	30.16	22.4	139	0.009	0.009	14(Qp)	Si	33.9
148.9	-1170	0.1	12.06	30.16	22.4	108	0.007	0.007	13(Fr)	Si	58.1

Trave di Fond. : 9010 | 22 , 23 | Pilastrate [31 , 30]

Sez. R: By= 60.0 cm Bz= 100.0 cm L= 149.2 cm Ln= 149.2 cm Terreno: Terrenol

Criterio : CLS_TraviFondazione

Combinazione Rara: $\sigma_{cal}[kg/cmq]=149$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{c-}	σ_{f+}	σ_{f-}	Cb+	Cb-	Ver.	CS
	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1523	--	12.06	12.06	-2	140	--	--	1	8	Si	25.7
14.9	1392	--	12.06	12.06	-2	128	--	--	1	8	Si	28.1
74.6	1074	96	12.06	12.06	-2	99	-0	9	1	8	Si	36.4
134.3	1087	--	12.06	12.06	-2	100	--	--	1	8	Si	35.9
149.2	1141	--	12.06	12.06	-2	105	--	--	1	8	Si	34.2

Combinazione QP: $\sigma_{cal}[kg/cmq]=112$ $\sigma_{fa}[kg/cmq]=3600$

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{c-}	σ_{f+}	σ_{f-}	Cb+	Cb-	Ver.	CS
	kg*m	kg*m	cmq	cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq				
0.0	1526	--	12.06	12.06	-2	141	--	--	14	14	Si	25.6
14.9	1443	--	12.06	12.06	-2	133	--	--	14	14	Si	27.1

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Verifica spostamenti laterali delle colonne in acciaio secondo NTC 2008

Scenario di calcolo : Set_NT_SLD_A2_STR/GEO

Verifica spostamenti orizzontali relativi di piano (§4.2.4.2.2 - NTC 2008)

Interp.	Nodo sup.	Nodo inf.	Comb.	SpostX sup. mm	SpostY sup. mm	SpostX inf. mm	SpostY inf. mm	δ mm	h/300.00 mm	Verifica
2-3	327 (Nodo 327)	1 (Nodo 1)	1	0.34	-0.03	0.00	0.00	0.34	2.00	Si
2-3	328 (Nodo 328)	2 (Nodo 2)	1	0.30	-0.04	0.00	0.00	0.30	2.00	Si
2-3	329 (Nodo 329)	3 (Nodo 3)	1	0.32	-0.04	0.00	0.00	0.33	2.00	Si
2-3	330 (Nodo 330)	4 (Nodo 4)	1	0.32	-0.05	0.00	0.00	0.32	2.00	Si
2-3	331 (Nodo 331)	5 (Nodo 5)	1	0.32	-0.07	0.00	0.00	0.33	2.00	Si
2-3	332 (Nodo 332)	6 (Nodo 6)	1	0.31	-0.08	0.00	0.00	0.32	2.00	Si
2-3	333 (Nodo 333)	7 (Nodo 7)	1	0.30	-0.10	0.00	0.00	0.31	2.00	Si
2-3	334 (Nodo 334)	8 (Nodo 8)	1	0.32	-0.12	0.00	0.00	0.34	2.00	Si
2-3	335 (Nodo 335)	9 (Nodo 9)	1	0.29	-0.13	0.00	0.00	0.32	2.00	Si
2-3	336 (Nodo 336)	10 (Nodo 10)	1	0.28	-0.14	0.00	0.00	0.31	2.00	Si
2-3	337 (Nodo 337)	11 (Nodo 11)	1	0.28	-0.16	0.00	0.00	0.32	2.00	Si
2-3	338 (Nodo 338)	12 (Nodo 12)	1	0.25	-0.17	0.00	0.00	0.30	2.00	Si
2-3	339 (Nodo 339)	13 (Nodo 13)	1	0.23	-0.18	0.00	0.00	0.29	2.00	Si
2-3	340 (Nodo 340)	14 (Nodo 14)	1	0.26	-0.21	0.00	0.00	0.33	2.00	Si
2-3	341 (Nodo 341)	15 (Nodo 15)	1	0.22	-0.21	0.00	0.00	0.31	2.00	Si
2-3	342 (Nodo 342)	16 (Nodo 16)	1	0.22	-0.23	0.00	0.00	0.31	2.00	Si
2-3	343 (Nodo 343)	17 (Nodo 17)	1	0.19	-0.23	0.00	0.00	0.30	2.00	Si
2-3	344 (Nodo 344)	18 (Nodo 18)	1	0.17	-0.23	0.00	0.00	0.29	2.00	Si
2-3	345 (Nodo 345)	19 (Nodo 19)	1	0.20	-0.27	0.00	0.00	0.34	2.00	Si
2-3	346 (Nodo 346)	20 (Nodo 20)	1	0.16	-0.26	0.00	0.00	0.31	2.00	Si
2-3	347 (Nodo 347)	21 (Nodo 21)	1	0.15	-0.28	0.00	0.00	0.31	2.00	Si
2-3	348 (Nodo 348)	22 (Nodo 22)	1	0.13	-0.28	0.00	0.00	0.31	2.00	Si
2-3	349 (Nodo 349)	23 (Nodo 23)	1	0.11	-0.28	0.00	0.00	0.30	2.00	Si
2-3	350 (Nodo 350)	24 (Nodo 24)	1	0.10	-0.27	0.00	0.00	0.29	2.00	Si
2-3	351 (Nodo 351)	25 (Nodo 25)	1	0.06	-0.21	0.00	0.00	0.21	2.00	Si
2-3	352 (Nodo 352)	26 (Nodo 26)	1	0.10	-0.30	0.00	0.00	0.31	2.00	Si

Verifica spostamenti orizzontali in sommità (§4.2.4.2.2 - NTC 2008)

Nodo	Comb.	SpostX mm	SpostY mm	Δ mm	H/500.00 mm	Verifica
327 (Nodo 327)	1	0.34	-0.03	0.34	23.76	Si
328 (Nodo 328)	1	0.30	-0.04	0.30	23.76	Si
329 (Nodo 329)	1	0.32	-0.04	0.33	23.76	Si
330 (Nodo 330)	1	0.32	-0.05	0.32	23.76	Si
331 (Nodo 331)	1	0.32	-0.07	0.33	23.76	Si
332 (Nodo 332)	1	0.31	-0.08	0.32	23.76	Si
333 (Nodo 333)	1	0.30	-0.10	0.31	23.76	Si
334 (Nodo 334)	1	0.32	-0.12	0.34	23.76	Si
335 (Nodo 335)	1	0.29	-0.13	0.32	23.76	Si
336 (Nodo 336)	1	0.28	-0.14	0.31	23.76	Si
337 (Nodo 337)	1	0.28	-0.16	0.32	23.76	Si
338 (Nodo 338)	1	0.25	-0.17	0.30	23.76	Si
339 (Nodo 339)	1	0.23	-0.18	0.29	23.76	Si
340 (Nodo 340)	1	0.26	-0.21	0.33	23.76	Si
341 (Nodo 341)	1	0.22	-0.21	0.31	23.76	Si
342 (Nodo 342)	1	0.22	-0.23	0.31	23.76	Si
343 (Nodo 343)	1	0.19	-0.23	0.30	23.76	Si
344 (Nodo 344)	1	0.17	-0.23	0.29	23.76	Si
345 (Nodo 345)	1	0.20	-0.27	0.34	23.76	Si
346 (Nodo 346)	1	0.16	-0.26	0.31	23.76	Si
347 (Nodo 347)	1	0.15	-0.28	0.31	23.76	Si
348 (Nodo 348)	1	0.13	-0.28	0.30	23.76	Si
349 (Nodo 349)	1	0.11	-0.28	0.31	23.76	Si
350 (Nodo 350)	1	0.10	-0.27	0.29	23.76	Si
351 (Nodo 351)	1	0.06	-0.21	0.21	23.76	Si
352 (Nodo 352)	1	0.10	-0.30	0.31	23.76	Si

COLEGAMENTINODI ACCIAIO secondo NTC 2008

Scenario di calcolo : Set_NT_SLD_A2_STR/GEO

NODO COLONNA-FONDAZIONE

Ove non diversamente specificato le dimensioni usate sono DaN e cm

Simbologia sezione I	
Sezione	Nome della sezione
B	Base delle ali
H	Altezza della sezione
t _{bi} ,t _{bs} ,t _b	Spessore ala inferiore, superiore, spessore anima
Geometria costole	
N°	Indice della costola
X _i ,Y _i	coordinate estremo iniziale
X _f ,Y _f	coordinate estremo finale
L _h ,t	lunghezza, altezza, spessore della costola
Geometria Tirafondi	
N°	Indice del tirafondo
X _y	coordinate centro bullone
Φ(mm)	Diámetro nominale del bullone
classe	classe di resistenza
Ares	Area resistente
L	Lunghezza del tirafondo
R	Eventuale raggio dell'uncino del tirafondo
Φm	Minidiametro del dado,diametro medio della testa) (NTC 4.2.64)
Forze applicate	
Comb.	Nome della combinazione cui corrispondono le forze
N ₁ ,Y ₁ ,T _z	Sforzo normale taglio in direzione Y, taglio in direzione Z, nel riferimento locale della colonna
M ₁ ,M _y ,M _z	Momento torcente, flettente secondo Y, flettente secondo Z, nel riferimento locale della colonna
Verifica piastra di base	
Comb. _{„Pann.}	combinazione indice del pannello della mesh con minimo SF
N°	indice del pannello della mesh
X _y	coordinate del centro del pannello della mesh
σ _{xx} ,σ _{yy} ,τ _{xy}	tensioni del pannello nel riferimento della piastra
σ _{id}	tensione ideale di Von Mises=σ _{xx} ² +σ _{yy} ² -σ _{xx} *σ _{yy} +3*τ _{xy} ²) ^{1/2}
SF	Fattore di sicurezza=σ _{id} /(f _y k/γM0) (cfr. NTC. 4.2.4.1.2)
Verifica a punzonamento piastra di base	
N° _{bull}	indice del tirafondo
X _y	coordinate del tirafondo
F _d	azione assiale nel tirafondo
B _p ,R _d	resistenza al punzonamento della piastra (cfr. formula NTC. 4.2.64)
SF	Fattore di sicurezza al punzonamento =B _p ,R _d /A _{azione}
Verifica calcestruzzo	
Comb.	combinazione delle azioni
N° _{vert}	indice vertice area compressa
X _y	coordinate del vertice
σ	tensione (di compressione) nel vertice
SF	Fattore di sicurezza =f _{cd} /σ
Verifica costole	
N°	indice elemento di costola, parte di costola compresa tra due costole o tra costola e sezione
N° _{cost}	Indice della costola cui appartiene l'elemento
X _i ,Y _i	coordinate estremo iniziale dell'elemento
X _f ,Y _f	coordinate estremo finale dell'elemento
σ ₁ ,τ	tensione normale e tangenziale agente sulla sezione verticale dell'elemento di costola
σ _{id}	tensione ideale di Von Mises=(σ ² +3*τ ²)/ ²
SF	Fattore di sicurezza=σ _{id} /(f _y k/γM0) (cfr. NTC. 4.2.4.1.2)
Verifica saldature orizzontali costole	
Comb	nome della combinazione delle azioni
N°	indice elemento di costola, parte di costola compresa tra due costole o tra costola e sezione
N° _{cost}	Indice della costola cui appartiene l'elemento
X _i ,Y _i	coordinate estremo iniziale dell'elemento
X _f ,Y _f	coordinate estremo finale dell'elemento
L	lunghezza dell'elemento
a/2	semidimensione del cordone di saldatura
σ ₁ ,τ _p ,τ _m	tensione normale,tangenziale parallela ed ortogonale sul cordone
(¹)SF	Fattore di sicurezza

Verifica saldature verticali costole	
Comb	nome della combinazione delle azioni
N° cost	Indice della costola
X,Y	punto nel piano ove è posto il cordone
H	altezza della costola
a	dimensione del cordone di saldatura
σn,τp,τn	tensione normale tangenziale parallela ed ortogonale sul cordone
(1)SF	Fattore di sicurezza
Verifica tirafondi uncino	
Comb	nome della combinazione delle azioni
N°	indice tirafondo
X,Y	coordinate tirafondo
Dbordo	distanza dal bordo del tirafondo
Ft,Fv	azione assiale e tangenziale del tirafondo
(2)Frd,Fvrd	resistenza assiale e tangenziale
(3)SF	fattore di sicurezza
(4)Lid,Lrich	lunghezza ideale effettiva e lunghezza ideale richiesta del tirafondo

(1)SF=valore minimo tra: β1*fyk/(σn^2+τp^2+τn^2)^1/2 e β2*fyk/((σm|+τn|)) (cfr. formule NTC 4.2.78,4.2.79)

(2)cfr. formule NTC 4.2.57-4.2.59 e 4.2.62)

(3)nel caso di sola trazione SF=Frd/Ft, solo taglio SF=Fvrd/Fv, nel caso di taglio e trazione SF=1/(Fv/Fvrd+Ft/Frd/1.4) con la condizione Ft/Frd<1(cfr. formula NTC 4.2.65)

(4)Lid=L+6.4*R la resistenza a sfilamento è Fmax=π*φ*Lid/(1+φ/Dbordo)^0.5, la lunghezza richiesta è Lrich=F/Fmax*Lid, il fattore di sicurezza è il minimo tra quello in(3) e Lid/Lrich

Dimensioni piastra: 420 x 420 x 20mm

Sezione della colonna

Centro anima (21,21),Rotazione 90 (°)

Baricentro (21,21)

Sezione	B(mm)	H(mm)	tb(mm)	tbs(mm)	th(mm)
[HEA]_240	240	230	12	12	7.5

Geometria costole

N°	Xi	Yi	Xf	Yf	I	h1	h2	t
1	0	8.5	42	8.5	42	15	15	1
2	0	33.5	42	33.5	42	15	15	1
3	10.1	0	10.1	8	8	10	15	1
4	10.1	34	10.1	42	8	15	10	1
5	31.9	34	31.9	42	8	15	10	1
6	31.9	0	31.9	8	8	10	15	1

Geometria Tirafondi

N°	X	Y	Φ(mm)	classe	Ares	L	R	Φm(mm)
1	5	4	24	8.8	3.53	50	8	24
2	5	38	24	8.8	3.53	50	8	24
3	37	4	24	8.8	3.53	50	8	24
4	37	37	24	8.8	3.53	50	8	24

Proprietà materiali

Calcestruzzo Rck=300, fcd=141.10

Coefficiente Omog. 15

Aderenza tirafondi-cls τad=26.86

Acciaio piastra classe S355: fyd=fyk/γM=3550/1.05=3380.95

Acciaio costole classe S355: fyd=fyk/γM=3550/1.05=3380.95

Proprietà Saldature

Verifiche condotte secondo le formule:

(σn²+τp²+τn²)^{0.5} <=fyk*β1

|σn|+|τn| <=fyk*β2

Elemento	fyk<40mm	β1	β2	0.85
Piastra	3350	3350	0.7	

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Elemento	fyk<40mm	3350	β1	β2	0.85
Costole	fyk<40mm	3350	3350	0.7	

Caratteristiche applicate alla colonna

Le caratteristiche sono intese positive se dirette secondo gli assi locali della colonna e sono applicate nel baricentro della sezione

Riferimento locale della colonna

	X	Y	Z
Origine	21.0000	21.0000	0.0000
Asse x	0.0000	0.0000	1.0000
Asse y	0.0000	1.0000	0.0000
Asse z	-1.0000	0.0000	0.0000

Comb.	N	Ty	Tz	My(DaN*m)	Mz(DaN*m)
Cond_1	-17395	907	4521	0	-6431

Verifiche piastra

Comb.	Pann.	X	Y	σxx	σyy	τxy	σtd	SF
Cond_1	127	8.83	22.56	-2016.00	-548.54	-29.31	1806.06	1.87

Tensione massima ideale = 1806.06 SF= 1.87 (Cond_1)**Verificato**

Verifica a punzonamento piastra

Comb.	N°bull	X	Y	Fd	Bp,Rd	SF
Cond_1	3	37.00	4.00	7324	36915	5.04

Forza di punz. massima = 7323.50 SF=5.04 (Cond_1) (bull 3)**Verificato**

Verifica calcestruzzo

Comb.	N°vert	X	Y	σ	SF
Cond_1	4	0.00	42.00	115.76	

Tensione cls max = 115.76 SF=1.22 (Cond_1)**Verificato**

Verifiche Costole

Cond	N°Cost.	σ	τ	σtd	SF
Cond_1	26	1586	249	1644	2.06

Calcolo saldature orizzontali

Comb	N°cost	Xi	Yi	Xf	Yf	L	a/2	σn	τp	SF
Cond_1	1	0.00	8.50	10.10	8.50	10.10	0.60	1313.24	169.64	1.88
Cond_1	2	0.00	33.50	10.10	33.50	10.10	0.60	2178.95	260.23	1.13
Cond_1	3	10.10	0.00	10.10	8.00	8.00	0.60	204.12	53.42	11.8
Cond_1	4	10.10	34.00	10.10	42.00	8.00	0.60	973.92	165.52	2.52
Cond_1	5	31.90	34.00	31.90	42.00	8.00	0.60	242.57	72.17	9.82
Cond_1	6	31.90	0.00	31.90	8.00	8.00	0.60	548.57	108.02	4.44

Calcolo saldature verticali

Comb	N°cost	X	Y	H	a	σn	τp	SF
Cond_1	1	31.90	8.25	15.00	1.20	177.62	111.44	11.9
Cond_1	3	10.10	8.00	15.00	1.20	39.62	28.49	50.9
Cond_1	6	31.90	8.00	15.00	1.20	88.16	57.61	23.6
Cond_1	2	31.90	33.75	15.00	1.20	101.93	72.61	19.9
Cond_1	4	10.10	34.00	15.00	1.20	134.62	88.28	15.4
Cond_1	5	31.90	34.00	15.00	1.20	49.16	38.49	39.8

Verifica Tirafondi Uncino

Comb	N°	X	Y	Dbordo	Ft	Fv	FvRd	Lid	Lrich	SF
Cond_1	3	37.00	4.00	4.00	7324	1153	20333	13555	101	93

Coefficiente di sicurezza minimo 1.093184 (Cond_1):**Verificato**

Verifica complessiva

Coefficiente di sicurezza minimo 1.093184 (Tirafondi uncino):**Verificato**

1118

Tensioni sezione ridotta trave

Cond		σ	τ	σ _{id}	SF
		DaN/cm ^q	DaN/cm ^q	DaN/cm ^q	
Cond_1		281	124	354	7.40

COLLEGAMENTO DI CONTINUITA' TRAVE

Ove non diversamente specificato le dimensioni usate sono DaN e cm

Caratteristiche elementi

Sezione asta

Sezione	B(mm)	H(mm)	tbi(mm)	tbs(mm)	th(mm)
[HEA]_240	240	230	12	12	7.5

Asta Acciaio S275: Fyk(>40mm)=2550,Fyk(t<40mm)=2750,γM0=1.05,γM2=1.25

Giunto esterno ali

a = distanza dei bulloni dai bordi, secondo l'asse della trave

a1 = distanza dei bulloni dai bordi, in direzione ortogonale all'asse

Bulloni classe 8.8: Ftb=8000,Fyb=6400,γM2=1.25

Acciaio S355: Fyk(>40mm)=3350,Fyk(t<40mm)=3550,γM0=1.05,γM2=1.25

a(mm)	al(mm)	Aresb(cm ^q)	Ø(mm)	Øfori(mm)
30	40	1.15	14	15

B(cm)	L(cm)	t(mm)	Bulloni
24	40	12	4x(2x4)

Giunto interno ali

B(cm)	L(cm)	t(mm)	Bulloni
11.625	40	15	4x(2x4)

Giunto anima

a = distanza dei bulloni dai bordi, secondo l'asse della trave

a1 = distanza dei bulloni dai bordi, in direzione ortogonale all'asse

Bulloni classe 8.8: Ftb=8000,Fyb=6400,γM2=1.25

Acciaio S355: Fyk(>40mm)=3350,Fyk(t<40mm)=3550,γM0=1.05,γM2=1.25

a(mm)	al(mm)	Aresb(cm ^q)	Ø(mm)	Øfori(mm)
50	30	1.15	14	15

B(cm)	L(cm)	t(mm)	Bulloni
15	40	12	3x(2x2)

Caratteristiche sollecitazione asta

comb		Cond_1	N	Tz	M(DaN*m)
			-8302	-2521	5577

Verifiche: Coefficiente sicurezza minimo 1.9586 Verificato

Sollecitazioni elementi della sezione

Nsup,Msup=sforzo normale e momento ala superiore

Ninf,Minf=sforzo normale e momento ala inferiore

Na,Ma,Ta=sforzo normale e momento e taglio anima

Cond	Nsup DaN	Msup DaN*m	Ninf DaN	Minf DaN*m	Na DaN	Ma DaN*m	Ta DaN
Cond_1	20398	3	-26944	3	-1756	412	2521

Tensioni sezione depurata dai fori

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Cond		σ	τ	σ _{id}	SF
		DaN/cm ^q	DaN/cm ^q	DaN/cm ^q	
Cond_1		-1287	-209	1337	1.96

Verifiche giunto anima

Cond	FtRd	FvRd	Ft	Fv	SF	FbRd	Fb	SF	FbRd	Fb	SF	SFmin
	DaN	DaN	DaN	DaN		DaN	DaN		DaN	DaN		
		Bulloni		Rifoll.Giunto		Rifoll.Giunto		Rifoll.Anima				
Cond_1	6624	4416	0	976	4.53	11424	488	23.4	6020	976	6.17	4.53

Verifiche giunto ali

Cond	FtRd	FvRd	Ft	Fv	SF	FbRd	Fb	SF	FbRd	Fb	SF	SFmin
	DaN	DaN	DaN	DaN		DaN	DaN		DaN	DaN		
		Bulloni		Rifoll.Giunto		Rifoll.Giunto		Rifoll.Ali				
Cond_1	6624	4416	0	-842	5.24	7692	-842	9.14	6486	1275	5.09	5.09

COLLEGAMENTO COLONNA-TRAVE PARETE LATERALE

Le sollecitazioni massime agenti, per cui dev'essere verificato il collegamento, sapendo che la trave è inclinata di circa 19° rispetto all'orizzontale, sono:

N=3.165,80 kg

T_y=1.900,00 kg

T_z=3.794,00 kg

Da cui considerando le componenti, rispettivamente orizzontali e verticali, avremo:

N^v=N sen(α°)=3.165,80 sen(19°)=1.031,00 kg

N^o=N cos(α°)=3.165,80 cos(19°)=2.993,00 kg

La piastra di collegamento avrà spessore sp=15mm, acciaio di tipo S275, dimensioni 240mmx430mm,ed otto bulloni φ14mm di classe 8.8, i cui fori saranno posti a distanze tale da rispettare le norme NTC08:

PIASTRA S275 sp=15 [mm] ⇨ f_{yk} = 275 [N/mm^q] f_{tk} = 430 [N/mm^q]

BULLONI 8.8 φ= 14 [mm] ⇨ f_{yb} = 640 [N/mm^q] f_{tb} = 800 [N/mm^q]

Posizione dei fori

Distanza dal bordo in direzione della forza:

e_{lmin} = 1,2 d₀ = 1,2x15 = 18,00 mm

e_{lmax} = 4t + 40 = 4x15+40= 80,00 mm

e₁ = 35,00 mm

Distanza tra i bulloni in direzione della forza:

p_{lmin} = 2,2 d₀ = 2,2x15 = 33,00 mm

p_{lmax} = min (14t;200) = min (14x15;200) = 140,00 mm

p₁ = 120,00 mm

Distanza dal bordo in direzione ortog. forza:

e_{2min} = 1,2 d₀ = 1,2x15 = 18,00 mm

e_{2max} = 4t + 40 = 4x15+40= 80,00 mm

e₂ = 60,00 mm

p_{2min} = 2,2 d₀ = 2,2x15 = 33,00 mm

p_{2max} = min (14t;200) = min (14x15;200) = 140,00 mm

P₂ = 120,00 mm

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Instabilità della flangia considerata:

$$\frac{P_1}{t} < 9 \sqrt{\frac{235}{f_y}}$$

$$\frac{120}{15} (=8mm) < 9 \sqrt{\frac{235}{275}} (=8,31mm) \quad \text{verificato}$$

Azione sui bulloni

$$T=3.794 + 1.031 = 4.825 \text{ kg}=48,25 \text{ kN}$$

$$N=2.993 \text{ kg} = 29,93 \text{ kN}$$

$$F_{v,Ed} = \frac{T}{n_s \cdot n_b} = \frac{48,25}{2 \cdot 8} = 3,02kN$$

$$F_{v,Rd} = \frac{0,6 \times f_v \times A_{ves}}{\gamma_{M2}} = \frac{0,6 \times 800 \times 115}{1,25} = 44,16kN$$

$$F_{t,Ed} = \frac{N}{n_b} = \frac{29,93}{8} = 3,74kN$$

$$F_{t,Rd} = \frac{0,9 \times f_{tb} \times A_{ves}}{\gamma_{M2}} = \frac{0,6 \times 800 \times 115}{1,25} = 66,24kN$$

$$\frac{F_{v,Ed}}{F_{v,Rd}} + \frac{F_{t,Ed}}{1,4 \cdot F_{t,Rd}} \leq 1$$

$$\frac{3,02}{44,16} + \frac{3,74}{1,4 \cdot 66,24} = 0,068 + 0,040 = 0,11 \leq 1$$

Verifica a rifollamento ala colonna

$$F_{b,Rd} = \frac{k \times \alpha \times f_{tk} \times d \times t}{\gamma_{M2}}$$

$$\alpha = \min \left(\frac{e_1}{3d_0}, \frac{f_{tb}}{f_t}, 1 \right) = \min \left(\frac{35}{3 \cdot 15}, \frac{800}{430}, 1 \right) = \min (0,77; 1,86; 1) = 0,77$$

$$k = \min \left(2,6 - \frac{e_2}{d_0}, 1,7; 2,5 \right) = \min \left(2,6 - \frac{35}{17}, 1,7; 2,6 \right) = 2,6$$

$$F_{b,Rd} = \frac{k \times \alpha \times f_{tk} \times d \times t}{\gamma_{M2}} = \frac{2,6 \cdot 0,77 \cdot 430 \cdot 14 \cdot 12}{1,25} = 115,69kN$$

$$F_{b,Rd} (=115,69kN) \geq F_{v,Ed} (=3,02kN) \quad \text{verificato}$$

Verifica a punzonamento ala colonna

$$B_{p,Rd} = \frac{0,6 \times \pi \times d_m \times t_p \times f_{tk}}{\gamma_{M2}} \geq F_{t,Ed}$$

$$B_{p,Rd} = \frac{0,6 \times \pi \times 14 \times 12 \times 430}{1,25} = 108,88kN > 3,74kN \quad \text{verifica}$$

Verifica saldatura flangia-trave

Dobbiamo prima di tutto fare delle ipotesi di base:

- Le saldature lungo le ali assorbono le Ty e la componente verticale di N
- Le saldature dell'anima assorbono le componenti Ty e Nz

$$a = r - \frac{\sqrt{2}}{2} = 6 - \frac{\sqrt{2}}{2} = 4,24mm \quad \text{cordone d'angolo}$$

$$l_1 = \text{lunghezza dei codoni lungo l'anima} = h - 2 \cdot a - 2 \cdot r = 240 - 2 \times 12 - 2 \times 21 = 174 \text{ mm}$$

$$l_2 = \text{lunghezza dei codoni lungo le ali} = b - a - 2 \cdot r = 240 - 4 - 24 - 2 \times 21 = 192 \text{ mm}$$

$$\tau_y = \frac{T_y}{2 \times l_2 \times a} = \frac{1.900 \times 10}{2 \times 192 \times 4,24} = 11,65 \text{ N/mm}^2$$

$$\tau_z = \frac{T_z}{2 \times l_1 \times a} = \frac{4.825 \times 10}{2 \times 172 \times 4,24} = 33,08 \text{ N/mm}^2$$

$$\sqrt{3(\tau_y^2 + \tau_z^2)} \leq \frac{f_{tk}}{\beta_w \cdot \gamma_{M2}}$$

$$\sqrt{3(11,65^2 + 33,08^2)} = 60,75 \text{ N/mm}^2 \leq 404,70 \text{ N/mm}^2 \quad \text{verifica}$$

COLLEGAMENTO MONTANTE RETICOLARE IPE140

Le sollecitazioni massime agenti, per cui dev'essere verificato il collegamento, sono:

$$N=2.500,00 \text{ kg}$$

$$T_y=100,00 \text{ kg}$$

$$T_z=1.073,00 \text{ kg}$$

La piastra di collegamento avrà spessore sp=10mm, acciaio di tipo S275, dimensioni 170mmx220mm, e quattro bulloni ϕ 14mm di classe 5.6, i cui fori saranno posti a distanze tale da rispettare le norme NTC08:

$$\text{PIASTRA S275} \quad sp=10 \text{ [mm]} \quad \Rightarrow \quad f_{tk} = 275 \text{ [N/mm}^2] \quad f_{tk} = 430 \text{ [N/mm}^2]$$

$$\text{BULLONI 8.8} \quad \phi=14 \text{ [mm]} \quad \Rightarrow \quad f_{yk} = 640 \text{ [N/mm}^2] \quad f_{yb} = 800 \text{ [N/mm}^2]$$

Azione sui bulloni

$$T=3.794 + 1.031 = 4.825 \text{ kg}=48,25 \text{ kN}$$

$$N=2.500 \text{ kg} = 25,00 \text{ kN}$$

$$F_{v,Ed} = \sqrt{T_y^2 + T_z^2} = \sqrt{1^2 + 10,75^2} = 10,80 \text{ kN}$$

$$F_{t,Ed} = 25,00 \text{ kN}$$

$$F_{v,Rd} = \frac{0,6 \times f_{tb} \times A_{res}}{\gamma_{M2}} = \frac{0,6 \times 500 \times 115}{1,25} = 27,60 \text{ kN}$$

$$F_{t,Rd} = \frac{0,9 \times f_{tb} \times A_{res}}{\gamma_{M2}} = \frac{0,6 \times 500 \times 115}{1,25} = 41,40 \text{ kN}$$

$$\frac{F_{v,Ed}}{F_{v,Rd}} + \frac{F_{t,Ed}}{1,4 \cdot F_{t,Rd}} \leq 1$$

$$\frac{10,80}{27,60} + \frac{25,00}{1,4 \cdot 41,40} = 0,391 + 0,431 = 0,822 < 1 \quad \text{verifica}$$

Verifica a rifollamento

$$F_{b,Rd} = \frac{k \times \alpha \times f_{tk} \times d \times t}{\gamma_{M2}}$$

$$\alpha = \min \left(\frac{e_t}{3d_0}, \frac{f_{tb}}{f_t}, 1 \right) = \min \left(\frac{35}{3 \cdot 15}, \frac{800}{430}, 1 \right) = \min(0,77; 1,86; 1) = 0,77$$

$$k = \min \left(2,8 - \frac{e_2}{d_0}, 1,7; 2,5 \right) = \min \left(2,8 - \frac{35}{15}, 1,7; 2,5 \right) = 2,5$$

$$F_{b,Rd} = \frac{k \times \alpha \times f_{tk} \times d \times t}{\gamma_{M2}} = \frac{2,5 \cdot 0,77 \cdot 430 \cdot 14 \cdot 10}{1,25} = 92,70 \text{ kN}$$

$$F_{b,Rd} (=92,70 \text{ kN}) \geq F_{v,Ed} (=10,80 \text{ kN}) \quad \text{verificato}$$

Verifica a punzonamento ala colonna

$$B_{p,Rd} = \frac{0,6 \times \pi \times d_m \times t_p \times f_{tk}}{\gamma_{M2}} \geq F_{t,Ed}$$

$$d_m = d - 0,64952p = 14 - 0,64952 \times 2 = 12,70 \text{ mm}$$

$$B_{p,Rd} = \frac{0,6 \times \pi \times 12,70 \times 10 \times 430}{1,25} = 82,35 \text{ kN} > 25,00 \text{ kN} \quad \text{verifica}$$

Verifica saldatura flangia-trave

Dobbiamo prima di tutto fare delle ipotesi di base:

- Le saldature lungo le ali assorbono le T_y e la componente verticale di N
- Le saldature dell'anima assorbono le componenti T_z

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$$a = r \frac{\sqrt{2}}{2} = 6 \frac{\sqrt{2}}{2} = 4,24 \text{ mm} \quad \text{cordone d'angolo}$$

l₁=lunghezza dei codoni ala superiore = 73 mm

l₂=lunghezza dei codoni ala inferiore = 27 mm

l₃=lunghezza dei codoni lungo l'anima = 100 mm

$$\sigma = \frac{N}{A} = \frac{25 \times 1.000}{2 \left[(2 \times 27 \times 4,24) + (100 \times 4,24) + (73 \times 4,24) \right]} = \frac{25.000}{1924,96} = 13,00 \text{ N/mm}^2$$

$$\tau_z = \frac{T_z}{\sum l_i \cdot a_i} = \frac{10,80 \times 1.000}{2 \times 100 \times 4,24} = 12,75 \text{ N/mm}^2$$

$$\sqrt{\sigma^2 + 3(\tau^2)} \leq \frac{f_{tk}}{\beta_w \cdot \gamma_{M2}}$$

$$\sqrt{13^2 + 3(12,75^2)} = 25,2 \text{ N/mm}^2 \leq 404,70 \text{ N/mm}^2 \quad \text{verifica}$$

ELEMENTI DELLA RETICOLARE

Per calcolare questo collegamento si considera la sollecitazione massima agente sull'elemento 2L 60x30x5 che risulta essere circa N=2,930[kg] =30[kN]

Si considerano:

$$\text{PIASTRA S275} \quad sp=5 \text{ [mm]} \quad \Leftrightarrow \quad f_{yk} = 275 \text{ [N/mmq]} \quad f_{tk} = 430 \text{ [N/mmq]}$$

$$\text{BULLONI 5.6} \quad \phi=14 \text{ [mm]} \quad \Leftrightarrow \quad f_{yk} = 500 \text{ [N/mmq]} \quad f_{tk} = 300 \text{ [N/mmq]}$$

Posizione dei fori

Distanza dal bordo in direzione della forza:

$$e_{\min} = 1,2 d_0 = 1,2 \times 15 = 18,00 \text{ mm}$$

$$e_{\max} = 4t + 40 = 4 \times 5 + 40 = 60,00 \text{ mm}$$

$$e_1 = 25,00 \text{ mm}$$

Distanza tra i bulloni in direzione della forza:

$$p_{\min} = 2,2 d_0 = 2,2 \times 15 = 33,00 \text{ mm}$$

$$p_{\max} = \min(14t; 200) = \min(14 \times 5; 200) = 200,00 \text{ mm}$$

$$p_1 = 50,00 \text{ mm}$$

Distanza dal bordo in direzione ortog. forza:

$$e_{2\min} = 1,2 d_0 = 1,2 \times 15 = 18,00 \text{ mm}$$

$$e_{2\max} = 4t + 40 = 4 \times 5 + 40 = 60 \text{ mm}$$

$$e_2 = 25,00 \text{ mm}$$

Verifica del bullone

$$V = \frac{N}{n_b} = \frac{30}{3} = 10,00 \text{ kN}$$

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$$H_{\max} = \frac{M}{\sum y^2} \cdot y_{\max} = \frac{N \cdot e}{\sum y^2} \cdot y_{\max} = \frac{30 \cdot (60 - 21,5 - 25,00)}{(50^2 + 50^2)} \cdot 50 = 4,05 \text{ kN}$$

$$R = \sqrt{V^2 + H^2}_{\max} = \sqrt{10,00^2 + 4,05^2} = 10,80 \text{ kN}$$

$$F_{v,Rd} = \frac{0,6 \times f_{tb} \times A_{res}}{\gamma_{M2}} = \frac{0,6 \times 500 \times 115}{1,25} = 27,60 \text{ kN}$$

$$F_{v,Rd} (= 60,29 \text{ kN}) \geq F_{v,Ed} (= 40,00 \text{ kN}) \quad \text{verificato}$$

Verifica a rifollamento fazzoletto

$$F_{b,Rd} = \frac{k \times \alpha \times f_{tk} \times d \times t}{\gamma_{M2}}$$

$$\alpha = \min \left(\frac{e_1}{3d_0}, \frac{f_{tb}}{f_t}; 1 \right) = \min \left(\frac{25}{3 \cdot 17}, \frac{500}{430}; 1 \right) = \min (0,55; 1,16; 1) = 0,55$$

$$k = \min \left(2,8 \cdot \frac{e_2}{d_0} - 1,7; 2,5 \right) = \min \left(2,8 \cdot \frac{25}{17} - 1,7; 2,5 \right) = 2,5$$

$$F_{b,Rd} = \frac{k \times \alpha \times f_{tk} \times d \times t}{\gamma_{M2}} = \frac{2,5 \cdot 0,55 \cdot 430 \cdot 14 \cdot 5}{1,25} = 33,11 \text{ kN}$$

$$F_{b,Rd} (= 33,11 \text{ kN}) > F_{v,Ed} (= 10,00 \text{ kN}) \quad \text{verificato}$$

COLLEGAMENTO CORRENTE SUPERIORE

Per calcolare questo collegamento si considera la sollecitazione massima agente sull'elemento corrente inferiore (2L 120x120x10) che risulta essere circa N=42.404 [kg] =424 [kN]

Si considerano:

$$\text{PIASTRA S275} \quad s_p=8 \text{ [mm]} \quad \Rightarrow \quad f_{yk} = 275 \text{ [N/mm}^2\text{]} \quad f_{tk} = 430 \text{ [N/mm}^2\text{]}$$

$$\text{BULLONI 8.8} \quad \phi=16 \text{ [mm]} \quad \Rightarrow \quad f_{yk} = 640 \text{ [N/mm}^2\text{]} \quad f_{tb} = 800 \text{ [N/mm}^2\text{]}$$

Posizione dei fori

Distanza dal bordo in direzione della forza:

$$e_{1\min} = 1,2 d_b = 1,2 \times 17 = 20,40 \text{ mm}$$

$$e_{1\max} = 4t + 40 = 4 \times 8 + 40 = 72 \text{ mm}$$

$$e_1 = 35,00 \text{ mm}$$

Distanza tra i bulloni in direzione della forza:

$$p_{\min} = 2,2 d_b = 2,2 \times 17 = 37,40 \text{ mm}$$

$$p_{\max} = \min (14t; 200) = \min (14 \times 8; 200) = 112,00 \text{ mm}$$

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$$p_1 = 60,00 \text{ mm}$$

Distanza dal bordo in direzione ortog. forza:

$$e_{2\min} = 1,2 d_0 = 1,2 \times 17 = 20,40 \text{ mm}$$

$$e_{2\max} = 4t + 40 = 4 \times 8 + 40 = 75 \text{ mm}$$

$$e_2 = 35,00 \text{ mm}$$

Verifica del bullone

$$V = \frac{N}{n_b} = \frac{424}{3} = 141,35 \text{ kN}$$

$$H_{\max} = \frac{M}{\sum y^2} \cdot y_{\max} = \frac{N \cdot e}{\sum y^2} \cdot y_{\max} = \frac{424 \cdot \left(\frac{120}{2} - 33,10 \right)}{(60^2 + 60^2)} \cdot 60 = 95,05 \text{ kN}$$

$$R = \sqrt{V^2 + H^2}_{\max} = \sqrt{141,35^2 + 95,05^2} = 170,33 \text{ kN}$$

$$F_{v,Ed} = \frac{R}{n_b} = \frac{170,33}{3} = 56,77 \text{ kN}$$

$$F_{v,Rd} = \frac{0,6 \times f_{tb} \times A_{res}}{\gamma_{M2}} = \frac{0,6 \times 800 \times 157}{1,25} = 60,29 \text{ kN}$$

$$F_{v,Rd} (= 60,29 \text{ kN}) \geq F_{v,Ed} (= 56,77 \text{ kN}) \quad \text{verificato}$$

Verifica a rifollamento fazzoletto

$$F_{b,Rd} = \frac{k \times \alpha \times f_{tk} \times d \times t}{\gamma_{M2}}$$

$$\alpha = \min \left(\frac{e_1}{3d_0}, \frac{f_{tb}}{f_t}; 1 \right) = \min \left(\frac{35}{3 \cdot 17}, \frac{800}{430}; 1 \right) = \min (0,686; 1,86; 1) = 0,686$$

$$k = \min \left(2,8 \cdot \frac{e_2}{d_0} - 1,7; 2,5 \right) = \min \left(2,8 \cdot \frac{35}{17} - 1,7; 2,5 \right) = 2,5$$

$$F_{b,Rd} = \frac{k \times \alpha \times f_{tk} \times d \times t}{\gamma_{M2}} = \frac{2,5 \cdot 0,686 \cdot 430 \cdot 16 \cdot 8}{1,25} = 75,51 \text{ kN}$$

$$F_{b,Rd} (= 75,51 \text{ kN}) \geq F_{v,Ed} (= 56,77 \text{ kN}) \quad \text{verificato}$$

Il Progettista

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RELAZIONE DEI MATERIALI DI OPERE DI NUOVA COSTRUZIONE

IPOTESI DI BASE

Il metodo di calcolo per le verifiche risulta essere il "Metodo Semiprobabilistico agli Stati Limite". Per la valutazione della resistenza ultima delle sezioni (sforzo normale e flessione retta/composta) si assumono le seguenti ipotesi di base (punto 4.1.2.1.2.1 del D.M. Infrastrutture del 14/01/2008):

- Conservazione delle sezioni piane;
- Perfetta aderenza tra acciaio e calcestruzzo
- Resistenza a trazione del calcestruzzo nulla (tranne che per le verifiche allo stato limite di esercizio di fessurazione e deformazione);
- Rottura del calcestruzzo determinata dal raggiungimento della sua capacità deformativa ultima a compressione;
- Rottura dell'armatura tesa determinata dal raggiungimento della sua capacità deformativa ultima;

Le tensioni nel calcestruzzo e nell'armatura sono dedotte a partire dalle deformazioni, utilizzando i rispettivi diagrammi tensione-deformazione.

I materiali ed i prodotti per uso strutturale, utilizzati nelle opere in oggetto alla presente relazione, devono rispondere ai requisiti indicati nel seguito.

I materiali e prodotti per uso strutturale devono essere:

- identificati univocamente a cura del produttore, secondo le procedure applicabili;
- qualificati sotto la responsabilità del produttore, secondo le procedure applicabili;
- accettati dal Direttore dei lavori mediante acquisizione e verifica della documentazione di qualificazione, nonché mediante eventuali prove sperimentali di accettazione.

I materiali in genere occorrenti per la costruzione delle opere di cui al presente progetto proverranno da quelle località che l'Appaltatore riterrà di sua convenienza, purché, ad insindacabile giudizio della Direzione dei lavori, siano riconosciuti della migliore qualità e rispondano ai requisiti appresso indicati.

Quando la Direzione dei lavori avrà rifiutata qualche provvista perché ritenuta a suo giudizio insindacabile non idonea ai lavori, l'Appaltatore dovrà sostituirla con altra che risponda ai requisiti voluti, ed i materiali rifiutati dovranno essere immediatamente allontanati dalla sede del lavoro o dai cantieri a cura e spese dell'Appaltatore.

Le prove su materiali e prodotti, a seconda delle specifiche procedure applicabili, come specificato di volta in volta nel seguito, devono generalmente essere effettuate da:

- a) laboratori di prova notificati ai sensi dell'art. 18 della Direttiva n.89/106/CEE;
- b) laboratori di cui all'art.59 del DPR n.380/2001;
- c) altri laboratori, dotati di adeguata competenza ed idonee attrezzature, appositamente abilitati dal Servizio Tecnico Centrale.

Qualora si applichino specifiche tecniche europee armonizzate, ai fini della marcatura CE, le attività di certificazione, ispezione e prova dovranno essere eseguite dai soggetti previsti nel relativo sistema di

attestazione della conformità.

Il richiamo alle specifiche tecniche europee EN armonizzate, di cui alla Dir. 89/106/CEE ed al DPR 246/93, deve intendersi riferito all'ultima versione aggiornata, salvo diversamente specificato. Il richiamo alle specifiche tecniche volontarie EN, UNI e ISO deve intendersi riferito alla data di pubblicazione se indicata, ovvero, laddove non indicata, all'ultima versione aggiornata.

I materiali impiegati per la costruzione sono:

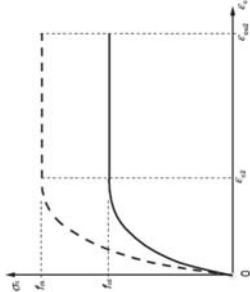
* cemento armato

* acciaio

* carpenteria metallica

DIAGRAMMI DI CALCOLO TENSIONE DEFORMAZIONE CALCESTRUZZO

Per il calcestruzzo e' stato adottato il diagramma di calcolo tensione-deformazione schematizzato con il modello parabola-rettangolo (punto 4.1.2.1.2.2 del D.M. Infrastrutture del 14/01/2008). In particolare, utilizzandosi nel caso in esame una classe di resistenza inferiore a C50/60 si può porre che il vertice alla parabola ha ascissa $\epsilon_{c2} = 0.2\%$, l'estremità del segmento ha ascissa $\epsilon_{cu} = 0.35\%$.



Per sezioni soggette a distribuzioni di tensione di compressione approssimativamente uniformi, si assume per la deformazione ultima a rottura il valore ϵ_{c2} anziché ϵ_{cu} .
Le resistenze di calcolo f_d sono state valutate mediante l'espressione:

$$f_d = \frac{f_k}{\gamma_m}$$

assumendo per il coefficiente γ_m i valori di seguito riportati:

Stati Limite	Acciaio \square_s	Calcestruzzo \square_c
Ultimi	1.15	1.5 per c.a. e c.a. con precompressione parziale
Esercizio	1.00	1.00

Per spessori inferiori a 5 cm il coefficiente la resistenza di calcolo a compressione va ridotta a 0,80 f_{cd} . In particolare, la resistenza di calcolo del calcestruzzo f_{cd} , risulta pari a:

$$f_{cd} = \frac{\alpha_{cc} \times f_k}{\gamma_c}$$

Per strutture o parti strutturali sottoposte a presso-flessione con prevalenza di sforzo normale esposte in ambienti poco o moderatamente aggressivo si adottano le seguenti limitazioni:

- Per combinazione rara: 0.6 f_{ok}
- Per combinazione quasi permanente 0.45 f_{ok}

Per tenere conto della riduzione di resistenza dovuta a carichi di lunga durata, si assume il coefficiente α_{cc} = 0.85.

CARATTERISTICHE RESISTENTI DEL CONGLOMERATO CEMENTIZIO

I parametri relativi ale caratteristiche reistsenti sono riportati di seguito, secondo la notazione in tabella.

Parametro	Descrizione	simbolo	Correlazioni
Resistenza caratteristica cubica a compressione	valore frattile 5% della distribuzione di resistenza determinata su provini cubici confezionati e conservati secondo la norma EN12390-2, e sottoposti a prova di compressione uniassiale dopo 28 giorni, secondo la norma EN12390-3.	R _{ck}	
Resistenza caratteristica cilindrica a compressione	valore frattile 5% della distribuzione di resistenza determinata su provini cilindrici, di diametro 150mm ed altezza 300mm.	f _{ck}	f _{ck} ≐0.83 R _{ck}
Resistenza di calcolo cilindrica a compressione		f _{cd}	f _{ck} /γ _c
Resistenza a trazione	Resistenza media a trazione semplice (assiale)	f _{ctm}	
Resistenza caratteristica		f _{ctk}	f _{ctk} = 0.7 f _{ctm}
Resistenza a trazione per flessione		f _{ctk}	f _{ctk} = 1.2 f _{ctk}
T.A. in esercizio combinazione rara			
T.A. in esercizio combinazione frequente			
T.A. in esercizio combinazione quasi perm.			
Modulo elastico	Viene come funzione della resistenza a rottura media su provino cubico (R _{cm})	E _c	E _c = 22000 · f _{cm} ^{0.3} con f _{cm} =f _{ck} +8 (N/mm ²)
Coefficiente di Poisson	viene adottato un valore maggiore di zero (calcestruzzo fessurato) e minore di 0.2 (non fessurato)	ν _c	0<ν _c ≤0.2
Coefficiente di dilatazione termica	In fase di progettazione viene assunto il valore riportato nella presente tabella	α _c	

Parti in calcestruzzo armato		
Classe calcestruzzo		Clis C25/30
Resistenza cubica R _{ck}	kg/cm ^q	300
Resistenza di calcolo f _{cd}	kg/cm ^q	141
Resistenza a trazione di calcolo f _{ctd}	kg/cm ^q	12
Resistenza cilindrica f _{ck}	kg/cm ^q	249
Resistenza a trazione media f _{ctm}	kg/cm ^q	26
Classe acciaio		Acciaio B450C
Resistenza allo sneramento f _{yk}	kg/cm ^q	>=4500
Resistenza alla rottura f _{tk}	kg/cm ^q	>=5400

Cemento armato

* **LEGANTI:** I leganti impiegati nell'opera in progetto, sono quelli previsti nelle disposizioni vigenti in materia (Legge 26-05-1965 e norme armonizzate della serie EN 197), dotati di attestato di conformità ai sensi delle norme EN 197-1 ed EN 197-2. In presenza di ambienti chimicamente aggressivi si fa riferimento ai cementi previsti dalle norme UNI 9156 (cementi resistenti ai solfati) e UNI 9606 (cementi resistenti al dilavamento della calce).

* **AGGREGATI:** La sabbia deve essere viva, con grani assortiti in grossezza da 0 a 3 mm, non proveniente da rocce in decomposizione, sricchiolante alla mano, pulita, priva di materie organiche, melmose, terrose e di salsedine. La ghiaia deve contenere elementi assortiti, di dimensioni fino a 15 mm, resistenti e non gelivi, non friabili, scevri di sostanze estranee, terra e salsedine. Le ghiaie sporche vanno accuratamente lavate. Anche il pietrisco proveniente da rocce compatte, non gessose né gelive, dovrà essere privo di impurità od elementi in decomposizione.

* **AGGIUNTE**

* **ADDITIVI**

* **ACQUA DI IMPASTO:** L'acqua da utilizzare per gli impasti dovrà essere limpida, priva di sali in percentuale dannosa e non aggressiva.

Leganti

Devono impiegarsi esclusivamente cementi rispondenti ai requisiti di accettazione contenuti nelle disposizioni vigenti in materia. Il tipo, la classe ed il dosaggio del cemento devono essere idonei a soddisfare le esigenze tecniche delle opere.

La dosatura di acqua limpida, dolce priva di sostanze nocive alla compattezza ed alla resistenza dell'impasto dovrà essere di 140 litri/mc di calcestruzzo per un rapporto A/C=0.40.

Se l'impasto dovesse risultare non sufficientemente fluido, sarà allora possibile aumentare l'acqua fino al valore di 160 litri/mc di calcestruzzo.

Aggregati

Gli aggregati utilizzabili, ai fini del confezionamento del calcestruzzo, debbono possedere marcatura CE secondo D.P.R. 246/93 e successivi decreti attuativi.

Gli aggregati debbono essere conformi ai requisiti della normativa UNI EN 12620 e UNI 8520-2 con i relativi riferimenti alla destinazione d'uso del calcestruzzo.

La massa volumica media del granulo in condizioni s.s.a. (saturo a superficie asciutta) deve essere pari o superiore a 2300 kg/m³. A questa prescrizione si potrà derogare solo in casi di comprovata impossibilità di approvvigionamento locale, purché si continuino a rispettare le prescrizioni in termini di resistenza caratteristica a compressione e di durabilità descritti in fase di progetto. Per opere caratterizzate da un elevato rapporto superficie/volume, laddove assume un'importanza predominante la minimizzazione del ritiro igrometrico del calcestruzzo, occorrerà preliminarmente verificare che l'impiego di aggregati di minore massa volumica non determini un incremento del ritiro rispetto ad un analogo conglomerato confezionato con aggregati di massa volumica media maggiore di 2300 Kg/m³.

Per i calcestruzzi con classe di resistenza caratteristica a compressione maggiore di C50/60 preferibilmente dovranno essere utilizzati aggregati di massa volumica maggiore di 2600 kg/m³.

Gli aggregati dovranno rispettare i requisiti minimi imposti dalla norma UNI 8520 parte 2 relativamente al contenuto di sostanze nocive. In particolare:

- il contenuto di solfati solubili in acido (espressi come SO3 da determinarsi con la procedura prevista dalla UNI-EN 1744-1: 1999 punto 12) dovrà risultare inferiore allo 0.2% sulla massa dell'aggregato indipendentemente se l'aggregato è grosso oppure fine (aggregati con classe di contenuto di solfati AS0,2);

- il contenuto totale di zolfo (da determinarsi con UNI-EN 1744-1 punto 11) dovrà risultare inferiore allo 0.1%;

- non dovranno contenere forme di silice amorfa alcali-reattiva o in alternativa dovranno evidenziare espansioni su prismi di malta, valutate con la prova accelerata e/o con la prova a lungo termine in accordo alla metodologia prevista dalla UNI 8520-22, inferiori ai valori massimi riportati nel prospetto 6 della UNI 8520 parte 2.

La granulometria degli aggregati litici per i conglomerati sarà prescritta dalla Direzione dei lavori in base alla destinazione, al dosaggio ed alle condizioni di messa in opera dei calcestruzzi. L'Impresa dovrà garantire la costanza delle caratteristiche della granulometria per ogni lavoro.

Additivi

Gli additivi, ove previsti, per la produzione del calcestruzzo devono possedere la marcatura CE ed essere conformi, in relazione alla particolare categoria di prodotto cui essi appartengono, ai requisiti imposti dai rispettivi prospetti della norma UNI EN 934 (parti 2, 3, 4, 5). Per gli altri additivi che non rientrano nelle classificazioni della norma si dovrà verificarne l'idoneità all'impiego in funzione dell'applicazione e delle proprietà richieste per il calcestruzzo. E' onere del produttore di calcestruzzo verificare preliminarmente i dosaggi ottimali di additivo per conseguire le prestazioni reologiche e meccaniche richieste oltre che per valutare eventuali effetti indesiderati. Per la produzione degli impasti, si consiglia l'impiego costante di additivi fluidificanti/riduttori di acqua o superfluidificanti/riduttori di acqua ad alta efficacia per limitare

il contenuto di acqua di impasto, migliorare la stabilità dimensionale del calcestruzzo e la durabilità dei getti. Nel periodo estivo si consiglia di impiegare specifici additivi capaci di mantenere una prolungata lavorabilità del calcestruzzo in funzione dei tempi di trasporto e di getto.

Per le riprese di getto si potrà far ricorso all'utilizzo di ritardanti di presa e degli adesivi per riprese di getto. Nel periodo invernale al fine di evitare i danni derivanti dalla azione del gelo, in condizioni di maturazione al di sotto dei 5°C, si farà ricorso, oltre che agli additivi superfluidificanti, all'utilizzo di additivi acceleranti di presa e di indurimento privi di cloruri.

Per i getti sottoposti all'azione del gelo e del disgelo, si farà ricorso all'impiego di additivi aeranti come prescritto dalle normative UNI EN 206 e UNI 11104.

Acqua di impasto

Per la produzione del calcestruzzo dovranno essere impiegate le acque potabili e quelle di riciclo conformi alla UNI EN 1008.

Dosatura dei Materiali

La dosatura dei materiali è orientativamente la seguente per m³ d'impasto, salvo la preparazione dei provini:

sabbia	0.4 m³
ghiaia	0.8 m³
acqua	120 litri
cemento tipo 425	3.5 q/m³

2.5 DOSAGGIO DEI MATERIALI IMPIEGATI PER LA COMPOSIZIONE DEL CALCESTRUZZO

2.5.1 INERTI

L'inerte deve essere privo di sostanze dannose ai fini della presa e dell'indurimento, avere una curva granulometrica tale da dare i seguenti valori dei moduli di finezza e di superficie, in funzione della dimensione massima dell'inerte e deve essere suddiviso almeno in tre classi, che verranno separatamente dosate nella confezione degli stessi e avranno la seguente composizione:

sabbia vagliata	granulometria 1.00 mm;
Ghiaietto vagliato	granulometria 10.00 mm;
Ghiaia vagliata	granulometria 25.00 mm;

Non è consentito il misto di fiume. L'acqua per gli impasti deve essere limpida, priva di sali in percentuali dannose e non essere aggressiva.

La dimensione massima dei grani dell'inerte deve essere tale da permettere che il conglomerato possa riempire ogni parte del manufatto, tenendo conto della lavorabilità del conglomerato stesso, della presenza dell'armatura metallica e di eventuali inerti, delle caratteristiche geometriche della carpenteria, delle modalità del getto e dei mezzi d'opera.

La dosatura di acqua liquida, dolce priva di sostanze nocive alla compattezza ed alla resistenza dell'impasto dovrà essere di 140 litri/mc di calcestruzzo per un rapporto A/C=0.40.

Se l'impalcato dovesse risultare non sufficientemente fluido, sarà allora possibile aumentare l'acqua fino al valore di 150 litri/mc di acqua

Se è prevista una classe di esposizione XA, secondo le indicazioni della norma UNI EN 206 e UNI 11104, conseguente ad un'aggressione di tipo solfatico o di dilavamento della calce, sarà necessario utilizzare cementi resistenti ai solfati o alle acque dilavanti in accordo con la UNI 9156 o la UNI 9606.

Per getti di calcestruzzo in sbarramenti di ritenuta di grandi dimensioni si dovranno utilizzare cementi di cui all'art. 1 lettera C della legge 595 del 26 maggio 1965 o, al momento del recepimento nell'ordinamento italiano, cementi a bassissimo calore di idratazione VHL conformi alla norma UNI EN 14216.

Conglomerato cementizio

Al fine di ottenere le prestazioni richieste, si dovranno dare indicazioni in merito alla composizione, ai processi di maturazione ed alle procedure di posa in opera, facendo utile riferimento alla norma UNI ENV 13670-1 ed alle Linee Guida per la messa in opera del calcestruzzo strutturale e per la valutazione delle caratteristiche meccaniche del calcestruzzo pubblicate dal Servizio Tecnico Centrale del Consiglio Superiore dei Lavori Pubblici, nonché dare indicazioni in merito alla composizione della miscela, compresi gli eventuali additivi, tenuto conto anche delle previste classi di esposizione ambientale (di cui, ad esempio, alla norma UNI EN 206-1) e del requisito di durabilità delle opere.

I quantitativi dei diversi materiali da impiegare per la composizione dei conglomerati, secondo le particolari indicazioni che potranno essere imposte dalla Direzione dei lavori o stabilite nell'elenco prezzi, dovranno corrispondere alle seguenti proporzioni:

Classe	Tipo	Quantità Cemento [q.li]	Sabbia [m³]	Ghiaia [m³]	Acqua [lit]
C25/30	Cemento	42.5	0.4	0.8	125

Quando la Direzione dei lavori ritenesse di variare tali proporzioni, l'Appaltatore sarà obbligato ad uniformarsi alle prescrizioni della medesima, salvo le conseguenti variazioni di prezzo in base alle nuove proporzioni previste.

Per il confezionamento del calcestruzzo dovranno essere impiegati aggregati appartenenti a non meno di due classi granulometriche diverse. La percentuale di impiego di ogni singola classe granulometrica verrà stabilita dal produttore con l'obiettivo di conseguire i requisiti di lavorabilità e di resistenza alla segregazione ottimali. La curva granulometrica ottenuta dalla combinazione degli aggregati disponibili, inoltre, sarà quella capace di soddisfare le esigenze di posa in opera richieste dall'impresa (ad esempio, pompabilità), e quelle di resistenza meccanica a compressione e di durabilità richieste per il conglomerato. La dimensione massima dell'aggregato dovrà essere non maggiore di ¼ della sezione minima dell'elemento da realizzare, dell'interfero ridotto di 5 mm, dello spessore del copriferro aumentato del 30%.

L'impasto di materiali, se realizzati in cantiere, dovrà essere fatto a mezzo di macchine impastatrici. I materiali componenti le malte cementizie saranno prima mescolate a secco, fino ad ottenere un miscuglio di tinta uniforme, il quale verrà poi asperso ripetutamente con la minore quantità d'acqua possibile, ma sufficiente, rimescolando continuamente.

La distribuzione granulometrica degli inerti, il cemento e la consistenza degli impasti, saranno determinate in funzione della destinazione d'uso ed al procedimento di posa in opera calcestruzzo. Tutti i calcestruzzi messi in opera dovranno essere costipati mediante vibratore meccanico.

Il produttore del calcestruzzo dovrà adottare tutti gli accorgimenti in termini di ingredienti e di composizione dell'impasto per garantire che il calcestruzzo possieda al momento della consegna del calcestruzzo in cantiere la lavorabilità prescritta.

Qualsiasi altra informazione sarà fornita direttamente dalla Direzione dei lavori.

DIAGRAMMI DI CALCOLO TENSIONE DEFORMAZIONE ACCIAIO

Le armature metalliche saranno costituite da acciaio saldabile e qualificato secondo le procedure di cui ai punti 11.3.1.2 11.3.2 del D.M. 2008;

Tipo acciaio B450C

f_{ly nom} = 450 N/mmq – *Tensione nominale di snervamento*

f_{t nom} = 540 N/mmq – Tensione nominale di rottura

\mathbf{f}_{yk} = 450 N/mmq – Tensione caratteristica di snervamento

f_{tk} = 540 N/mmq – Tensione caratteristica di rottura

τ - Aderenza 2.6 N/mm²

All'atto della posa in opera gli acciai devono presentarsi privi di ossidazione, corrosione, difetti superficiali visibili e pieghe. E' tollerata una ossidazione che scompare totalmente mediante sfregamento con un panno asciutto. Non è ammessa in cantiere alcuna operazione di raddrizzamento.

Acciaio per Cemento Armato

Per l'acciaio si adotta il legame tensioni-deformazioni schematizzato con un legame elastico perfettamente plastico (punto 4.1.2.1.2.3 del D.M. infrastrutture del 14/01/2008).

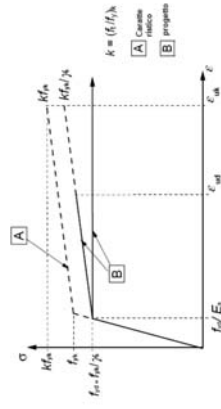
La resistenza di snervamento di calcolo dell'acciaio fs., risulta pari a (punto 4.1.2.1.1.3):

$$f_{yk} = \frac{f_{yk}}{f_{yd}} \gamma_s$$

Il valore della deformazione ultima di calcolo

$\varepsilon_{ud} = 0.9 \varepsilon_{uk}$
in cui si assume che la deformazione uniforme
ultima:

$$\varepsilon_{uk} = (A_{gt})_k = 7.5\%$$



2.3.1 CONGLOMERATO CEMENTIZIO

R_{cd}	[MPa]	30,00	Resistenza Cubica Caratteristica del calcestruzzo
f_{cd}	[MPa]	24,90	Resistenza caratteristica del calcestruzzo
f_{ctd}	[MPa]	14,11	Resistenza di calcolo del calcestruzzo
f_{ctd}	[MPa]	14,11	Resistenza di calcolo a flessione del calcestruzzo (massimo del diagramma parabola rettangolo)
ϵ_{cp}		0,20	Deformazione limite del calcestruzzo in campo elastico
ϵ_{cu}		0,35	Deformazione ultima del calcestruzzo

2.3.2 ACCIAIO PER CALCESTRUZZO

tipo	B450C	
f_{yk}	[MPa]	Resistenza caratteristica dell'acciaio
	450,00	
f_{td}	[MPa]	Resistenza di calcolo dell'acciaio
	391,30	
E_s	[MPa]	Modulo elastico dell'acciaio
	210.000,00	
ϵ_{su}		Deformazione ultima dell'acciaio
	1,00	

Acciai per c.a.

Per opere in calcestruzzo armato si userà acciaio in barre del tipo:

1) B450C (ad adherenza migliorata) avente una tensione caratteristica di snervamento minima garantita di 450.00 N/mm² ed una tensione caratteristica a rottura minima garantita di 540.00 N/mm².

Non saranno poste in opera barre eccessivamente ossidate, corrosive, recanti difetti che ne riducano la resistenza o ricoperte da sostanze che possano ridurre l'aderenza al conglomerato.

L'acciaio da calcestruzzo armato, in ogni sua forma commerciale, deve rispondere alle caratteristiche richieste dalle Norme Tecniche per le Costruzioni, D.M.14/01/2008, che specifica le caratteristiche tecniche che devono essere verificate, i metodi di prova, le condizioni di prova e il sistema per l'attestazione di conformità per gli acciai destinati alle costruzioni in cemento armato che ricadono sotto la Direttiva Prodotti CPD (89/106/CE).

Direttiva Prodotti CPD (89/106/CE).

L'acciaio deve essere qualificato all'origine, deve portare impresso, come prescritto dalle suddette norme, il marchio indelebile che lo renda costantemente riconoscibile e riconducibile inequivocabilmente allo stabilimento di produzione.

Nei riguardi della saldabilità, la composizione chimica deve essere in accordo con quanto specificato nel D.M. 14/01/2008.

Le proprietà meccaniche devono essere in accordo con quanto specificato nelle Norme Tecniche per le Costruzioni (D.M. 14/01/2008):

Proprietà	Valore caratteristico
f_y (N/mm ²)	≥ 450

ft (N/mm²)	≥ 540
ft/fy	≥ 1,15 ≤ 1,35
Agt (%)	≥ 7,5
fy/fy,nom	≤ 1,25

Prova di piega e raddrizzamento In accordo con quanto specificato nel D.M. 14/01/2008, è richiesto il rispetto dei limiti seguenti:

Diametro nominale (Ø) mm	Diametro massimo del mandrino
Ø < 12	4 Ø
12 ≤ Ø ≤ 16	5 Ø
16 < Ø ≤ 25	8 Ø
25 < Ø ≤ 40	10 Ø

Il valore del diametro nominale deve essere concordato all'atto dell'ordine. Le tolleranze devono essere in accordo con il D.M. 14/01/2008:

Diametro nominale (mm)	Da 6 a ≤ 8	Da > 8 a ≤ 50
Tolleranza in % sulla sezione	± 6	± 4,5

I prodotti devono avere una superficie nervata in accordo con il D.M. 14/01/2008. L'indice di aderenza Ir deve essere misurato in accordo a quanto riportato nel paragrafo 11.2.2.10.4 del D.M. 14/01/2008. I prodotti devono aver superato le prove di Beam Test effettuate presso un Laboratorio Ufficiale (Legge 1086).

Diametro nominale mm	Ir
5 ≤ Ø ≤ 6	≥ 0.048
6 < Ø ≤ 8	≥ 0.055
8 < Ø ≤ 12	≥ 0.060
Ø > 12	≥ 0.065

Disposizioni riguardanti gli acciai per c.a.

Non si devono porre in opera armature eccessivamente ossidate, corrosive, recanti difetti superficiali che ne menomino la resistenza o ricoperte da sostanze che possono ridurre sensibilmente l'aderenza.

CARATTERISTICHE MECCANICHE PROFILATI

Si dovranno utilizzare acciai conformi alle norme armonizzate della serie UNI EN 10025 (per i laminati), UNI EN 10219-1 (per i tubi saldati), recanti la Marcatura CE. Nelle calcolazioni statiche sono stati impiegati i seguenti valori:

- modulo elastico: **E = 210000 N/mm²**;
- coefficiente di Poisson: **ν = 0,3**

- modulo di elasticità trasversale: **G = E/[2(1 + ν)] = 80769 N/mm²**
- coefficiente di espansione termica lineare: **α = 12 · 10⁻⁶ per °C⁻¹** (per temperature fino a 100°C)
- densità: **ρ = 7850 kg/m³**

In sede di progettazione, sono stati assunti i dati riportati nella tabella 11.3.X del D.M14.01.2008:

LAMINATO A CALDO CON PROFILI A SEZIONE APERTA (profilati e lamiere)			
Acciaio tipo S 275 per spessori ≤ 40mm			
f _{yk}	[MPa]	275	Resistenza caratteristica di snervamento
f _{tk}	[MPa]	430	Resistenza caratteristica di rottura

LAMINATO A CALDO CON PROFILI A SEZIONE APERTA (piastra di base)			
Acciaio tipo S 275 per spessori 80mm ≤ t ≤ 40mm			
f _{yk}	[MPa]	275	Resistenza caratteristica di snervamento
f _{tk}	[MPa]	410	Resistenza caratteristica di rottura

CARATTERISTICHE MECCANICHE BULLONERIA

I bulloni utilizzati nelle giunzioni devono appartenere alle sotto indicate classi della norma UNI EN ISO 898-1:2001, associate nel modo indicato nella tabella sottostante (D.M:14.01.2008):

vite classe 8.8 - dado 8		
f _{tb}	[MPa]	649
f _{tb}	[MPa]	800
Resistenza caratteristica di snervamento dei bulloni		
Resistenza caratteristica di rottura dei bulloni		

CARATTERISTICHE MECCANICHE SALDATURE E PROCESSO

La saldatura degli acciai dovrà avvenire con uno dei procedimenti all'arco elettrico codificati secondo la norma UNI EN ISO 4063:2001. Sono richieste caratteristiche di duttilità, snervamento, resistenza e tenacità in zona fusa e in zona termica alterata non inferiori a quelle del materiale di base. Nell'esecuzione delle saldature dovranno essere rispettate le norme UNI EN 1011:2005 parti 1 e 2 per gli acciai ferritici e della parte 3 per gli acciai inossidabili. Per la preparazione dei lembi si applicherà, salvo caso particolari, la norma UNI EN ISO 9692-1:2005.

Per l'accertamento delle caratteristiche meccaniche dell'acciaio per carpenteria, il prelievo dei saggi, la posizione nel pezzo da cui essi devono essere prelevati, la preparazione delle provette e le modalità di prova devono rispondere alle prescrizioni delle norme UNI EN ISO 377, UNI 552, EN 10002-1, UNI EN 10045-1.

Il Progettista

SALDATURE	<p>PROCESSO DI SALDATURA secondo ISO EN 15614-1:2008</p> <p>PER S1<20, ECCETTO DIVERSA INDICAZIONE, LE SALDATURE D'ANGOLO AVRANNO ALTEZZA DI GOLA (H) PARI AD ALMENO 0,7 DELLO SPESORE MINIMO DA SALDARE PER SALDATURA SINGOLA E 0,35 PER SALDATURA DOPPIA.</p> <p>CONTROLLI: Al Visivo e dimensionale 100% Et Ultrasonici (UT), Radiografico (RX), Magnetico (MT), Penetranti (PT), Corrosione (CCT), Microscopio elettronico (SEM) secondo le norme tecniche di progetto. Ispettori qualificati secondo le relative certificazioni.</p> <p>RELAZIONE SALDATURE DI CLASSE I: Elementi strutturali RELAZIONE SALDATURE DI CLASSE II: Elementi secondari RELAZIONE SALDATURE DI CLASSE III: Elementi non strutturali (SOTTO GLA INDETTATE MANE)</p> <p><input type="checkbox"/> ANALISI SODIO <input type="checkbox"/> ELETTRONICO TPO 3464LLX UN 3152-74</p>
TOLLERANZE DI LAVORAZIONE	<p>A) FORATURE:</p> <p>Interventi tra file: ± 1 mm ; Intervento fra grigio di file: ± 2 mm Anzi di frangimento ± 1 mm, limitare numero dei file < 5/3 - 3 mm.</p> <p>B) DIMENSIONI LINEARI: Da 7 a 19999 mm (+/- 2); oltre 20000 mm (+/- 3)</p> <p>C) DIMENSIONI ANGOLI ARI: ± 400 /645; 45° : ± ± 500 /645; 120° 800 /645</p>

PROVE SUI MATERIALI DA COSTRUZIONE

La prescrizione del calcestruzzo all'atto del progetto deve essere caratterizzata almeno mediante la classe di resistenza, la classe di consistenza ed il diametro massimo dell'aggregato.

La definizione del calcestruzzo viene effettuata mediante a classe di resistenza, contraddistinta dai valori caratteristici delle resistenze cubica R_{ck} e cilindrica f_{ck} a compressione uniaxiale, misurate su provini normalizzati e cioè rispettivamente su cilindri di diametro 150 mm e di altezza 300 mm e su cubi di spigolo 150 mm. Al fine delle verifiche sperimentali i provini prismatici di base 150×150 mm e di altezza 300 mm sono equiparati ai cilindri di cui sopra.

Per la preparazione, la forma, le dimensioni e la stagionatura dei provini di calcestruzzo vale quanto indicato nelle norme UNI EN 12390-1:2002 e UNI EN 12390-2:2002. Circa il procedimento da seguire per la determinazione della resistenza a compressione dei provini di calcestruzzo vale quanto indicato nelle norme UNI EN 12390-3:2003 e UNI EN 12390-4:2002. Circa il procedimento da seguire per la determinazione della massa volumica vale quanto indicato nella norma UNI EN 12390-7:2002.

Salvo diverse specifiche e/o accordi con il produttore del conglomerato la lavorabilità al momento del getto verrà controllata all'atto del prelievo dei campioni per i controlli d'accettazione della resistenza caratteristica convenzionale a compressione secondo le indicazioni riportate sulle Norme Tecniche sulle Costruzioni. La misura della lavorabilità verrà condotta in accordo alla UNI-EN 206-1 dopo aver proceduto a scaricare dalla betoniera almeno 0,3 mc di calcestruzzo. In accordo con le specifiche di capitolato la misura della lavorabilità potrà essere effettuata mediante differenti metodologie. In particolare la lavorabilità del calcestruzzo può essere definita mediante:

- il valore dell'abbassamento al cono di Abrams (UNI-EN 12350-2) che definisce la classe di consistenza o uno slump di riferimento oggetto di specifica;
- la misura del diametro di spandimento alla tavola a scosse (UNI-EN 12350-5).

ANALISI DEI CARICHI

La valutazione dei carichi e dei sovraccarichi è stata effettuata in accordo con le disposizioni contenute nel **D.M. 14.01.2008 (nuove norme tecniche per le costruzioni)**
I carichi adottati sono i seguenti:

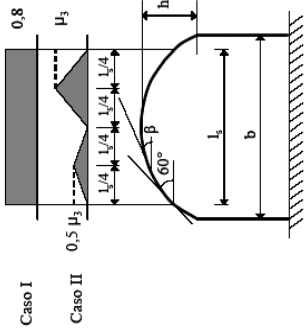
SOVRACCARICO NEVE

Provincia : CATANIA
Zona : 3
Altitudine a_s : 550 m s.l.m.
Esposizione : Normale
Periodo di ritorno : 50 anni
Il carico neve sulle coperture viene valutato con la seguente espressione:
$$q_s = \mu_i \cdot q_{sk} \cdot C_E \cdot C_i \text{ KN/m}^2$$

dove:
 μ_i Coefficiente di forma della copertura
 $C_E = 1.0$ Coefficiente di esposizione
 $C_i = 1.0$ Coefficiente termico
 $q_{sk} = 1.18 \text{ KN/m}^2$ Carico neve al suolo
Nel caso in esame (copertura cilindrica), con $\beta = 42.00^\circ$
 $h = 13.00 \text{ m}$
 $b = 9.00 \text{ m}$
il coefficiente di forma vale:

Caso I
 $0.8 \Rightarrow q_s = 0.94 \text{ KN/m}^2$
in caso di neve non accumulata, oppure, in caso di neve accumulata,
Caso II
 $0.5 \cdot \mu_i = 1.00 \Rightarrow q_s = 1.18 \text{ KN/m}^2$
 $\mu_i = 2.00 \Rightarrow q_s = 2.36 \text{ KN/m}^2$

Cap. 4
ANALISI DEI CARICHI



SOVRACCARICO VENTO

Zona Vento	V _{b,0} (m/s)	a ₀ (m)	K _a (1/s)
4	28	500	0.020

Categoria di esposizione	K	z ₀ (m)	z _{min} (m)
3	0.20	0.10	5

Altitudine: a_s = 550 m s.l.m.
Distanza dalla costa: terra - entro 40 Km

Classe di rugosità terreno:

Altezza manufatto:

Periodo di ritorno:

Velocità di riferimento del vento:

Coefficiente dinamico:

Coefficiente di forma:

Coefficiente di attrito:

Coefficiente di topografia:

Coefficiente di esposizione:

Le azioni del vento si traducono in pressioni (positive) e depressioni (negative) agenti normalmente alla superficie degli elementi che compongono la costruzione. La pressione agente su un singolo elemento è data dall'espressione:

$$p = q_b C_{pe} C_{pi} C_{di} = 1491,04 \text{ Pa}$$

dove,

$$q_b = 1/2 \rho v_b^2$$

è la pressione cinetica di riferimento;

$$\rho = 1,25 \text{ kg/m}^3$$

è la densità dell'aria.

L'azione tangente per unità di superficie parallela alla direzione del vento è:

$$p_r = q_e C_e C_i = 12,43 \text{ Pa}$$

I carichi relativi ai pesi propri vengono valutati in automatico in funzione della geometria degli elementi ed al loro peso specifico i tamponamenti vengono valutati per metro lineare di trave su cui insistono maggiori dettagli ad essi relativi sono riportati nel tabulato di calcolo alla sezione dei carichi relativi alle aste, nodi ed shell.

VALUTAZIONE DELL'AZIONE SISMICA

L'azione sismica è stata valutata in conformità alle indicazioni riportate al capitolo 3.2 del D.M. 14 gennaio 2008 "Norme tecniche per le Costruzioni"

La valutazione degli spettri di risposta per un dato Stato Limite avviene attraverso le seguenti fasi:

- definizione della Vita Nominale e della Classe d'Uso della struttura, in base ai quali si determina il Periodo di Riferimento dell'azione sismica.
- Determinazione attraverso latitudine e longitudine dei parametri sismici di base a_g , F_0 e T_c per lo Stato Limite di interesse; l'individuazione è stata effettuata interpolando tra i 4 punti più vicini al punto di riferimento dell'edificio secondo quanto disposto dall'allegato alle NTC "Pericolosità Sismica", dove:

ag accelerazione orizzontale massima al sito;

Fo valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale.

T*c periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale

- Determinazione dei coefficienti di amplificazione stratigrafica e topografica.

- Calcolo del periodo T_c corrispondente all'inizio del tratto a velocità costante dello Spettro.

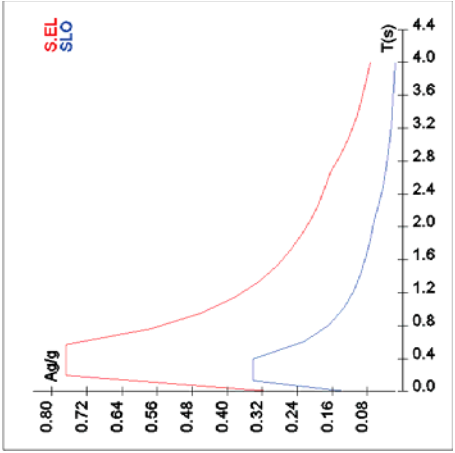
I dati così calcolati sono stati utilizzati per determinare gli Spettri di Progetto nelle verifiche agli Stati Limite considerati, per ogni direzione dell'azione sismica.

Oltre alla determinazione dei parametri sismici del sito si è considerata la tipologia di terreno, la posizione topografica e la tipologia strutturale (classe di duttilità, regolarità, ecc..) che ha condotto alla determinazione dei seguenti spettri di risposta:

Spettri di risposta		
Il calcolo degli spettri e del fattore di struttura sono stati calcolati per la seguente tipologia di terreno e struttura		
Vita della struttura		
Tipo	Porti imp. strategica (>100) >=100 anni	
Vita nominale(anni)	100,0	
Classe d'uso	Classe IV	
Coefficiente d'uso	2,000	
Periodo di riferimento(anni)	200,000	

Stato limite di esercizio - SLO	PVR=81,09%
Stato limite ultimo - SLV	PVR=10,09%
Periodo di ritorno SLO(anni)	TR=120,4
Periodo di ritorno SLV(anni)	TR=1898,2
Parametri del sito	
Comune	Biancavilla - (CT)
Longitudine	14,8652
Latitudine	37,6461
Id reticolo del sito	47419-47197-47196-47418
Valori di riferimento del sito	
Agg(TR=120,4) SLO	0,1103
F0(TR=120,4) SLO	2,5726
T*CTR=120,4) SLO	0,281
Agg(TR=1898,2) SLV	0,2704
F0(TR=1898,2) SLV	2,5180
T*CTR=1898,2) SLV	0,441
Coefficiente Amplificazione Topografica	S=1,000
Categoria terreno B	
stato limite SLV	
	S=1,13
	TB=0,19
	TC=0,57
	TD=2,68
stato limite SLO	
	S=1,20
	TB=0,13
	TC=0,40
	TD=2,04
Spettro Elastico	
Smorzamento viscoso %	q=1 (struttura NON DISSIPATIVA)
	5,0

T	EL [s]	EL [a/g]	TSLO [s]	SLO [a/g]
0,00000	0,30491	0,13236	0,00000	0,13236
0,19040	0,76776	0,13299	0,13299	0,34050
0,57119	0,76776	0,39896	0,39896	0,34050
0,76304	0,57472	0,60424	0,60424	0,22482
0,95489	0,45925	0,80952	0,80952	0,16781
1,14675	0,38242	1,01479	1,01479	0,13387
1,33860	0,32761	1,22007	1,22007	0,11134
1,53045	0,28654	1,42535	1,42535	0,09531
1,72231	0,25462	1,63063	1,63063	0,08331
1,91416	0,22910	1,83591	1,83591	0,07399
2,10602	0,20823	2,04119	2,04119	0,06655
2,29787	0,19084	2,25883	2,25883	0,05435
2,48972	0,17614	2,47648	2,47648	0,04521
2,68158	0,16354	2,69412	2,69412	0,03820
2,90131	0,13970	2,91177	2,91177	0,03270
3,12105	0,12072	3,12942	3,12942	0,02831
3,34079	0,10537	3,34706	3,34706	0,02475
3,56053	0,09276	3,56471	3,56471	0,02182
3,78026	0,08229	3,78235	3,78235	0,01938
4,00000	0,07350	4,00000	4,00000	0,01733



IL PROGETTISTA