EMISSIONE	DATA	MODIFICHE
A	2017.11.10	PRIMA EMISSIONE
B	2018.06.15	EMISSIONE PER VERIFICA

COMUNE DI CATANIA

Completamento del Piano di Risanamento del Rione S. Berillo

Convenzione urbanistica del 16/11/2012 tra Comune di Catania e Istica s.p.a. - C.E.Co.S. s.r.l. - Risanamento San Berillo s.r.l.

OPERE DI URBANIZZAZIONE PRIMARIA - PARCHEGGI PUBBLICI INTERRATI CON SOVRASTANTE E ATTIGUA AREA A VERDE ATTREZZATO Vp1-Vp2

PROGETTO ESECUTIVO

STRUTTURE
Parcheggio interrato - Tabulato di calcolo 1/2

Tav: R16

Scala: --

PROGETTAZIONE STRUTTURALE
Ing. Gabriele Correnti
Piazza della Repubblica, 31
95131 Catania
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ingcorrenti@libero.it

ORDINE DEGLI INGEGNERI PROV. DI CATANIA
DOTT. ING. GABRIELE CORRENTI 1996

San Berillo – Parcheggio Interrato Ottobre 2017_var_r3.dt

En.Ex.Sys. WinStrand
Structural Analisys & Design

Ditta produttrice:	***En.Ex.Sys.*** s.r.l. - Via Tizzano 46/2 - Casalecchio di Reno (Bologna)
Sigla:	WinStrand
Piattaforma software:	Microsoft Windows XP Home, Microsoft Windows XP Home Professional
Documentazione in uso:	Manuale teorico - Manuale d'uso
Campo di applicazione:	Analisi statica e dinamica di strutture in campo elastico lineare.

Elementi finiti implementati

- Truss.
- Beam (Modellazione di Travi e Pilastri).
- Travi su suolo elastico alla Winckler.
- Plinti su suolo elastico alla Winckler.
- Elementi Shear Wall per la modellazione di pareti di taglio.
- Elementi shell (lastra/piastra) equivalenti.
- Elementi Isoparametrici a 8 Nodi Shell (lastra/piastra).

Schemi di Carico

- Carichi nodali concentrati.
- Carichi applicati direttamente agli elementi.
- Carichi Superficiali.

Tipo di Risoluzione

- Analisi statica e/o dinamica in campo lineare con il metodo dell'equilibrio.
- Fattorizzazione LDL^T.
- Analisi Statica:
  -
    - modellazione generale 6 gradi di libertà per nodo.
    - ipotesi di solai infinitamente rigidi nel proprio piano (3 gradi di libertà per nodo + 3 per impalcato).
- Analisi dinamica. (Nel caso di analisi modale gli autovettori ed autovalori possono essere calcolati mediante *subspace iteration* oppure tramite il *metodo dei vettori di Ritz*):
  -
    - Via statica equivalente.
    - Modale con il metodo dello spettro di risposta.

Normativa di riferimento
La normativa italiana cui viene fatto riferimento nelle fasi di calcolo e progettazione è la seguente:

- Circolare del 2 Febbraio 2009, n. 617 *"Istruzioni per l'applicazione delle "Norme tecniche per le costruzioni" di cui al D.M. 14 gennaio 2008"*
- D.M. del 14 Gennaio 2008 *"Approvazione delle nuove norme tecniche per le costruzioni"*
- Legge n. 64 del 2 Febbraio 1974. "*Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche*".
- Legge n. 1086 del 5 Novembre 1971. "*Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso, ed a struttura metallica*".

SOMMARIO - TOMO 1 di 2

Analisi dei carichi

Piastra in c.a.- NTC08									San Berillo - Catania	
									Parcheggio - Analisi dei carichi	
PLATEA PARCHEGGIO						H tot [cm] =		60		
ANALISI DEI CARICHI										
	VALORI CARATTERISTCI									
	Calcestruzzo	0,60	x	2.500	=	1.500	kg/mq	γ_{G1}		
	Permanenti strutt.			G_{1K}	=	1.500	x	1,3	**1.950**	kg/mq
	Peso Iglu' H 80 cm				=	11	kg/mq			
	Consumo calcestruzzo	0,118	x	2.400	=	283	kg/mq			
	Caldana aramata	0,10	x	2.500	=	250	kg/mq			
	Pavimentazione industriale	0,20	x	2.400	=	480	kg/mq	γ_{G2}		
	Permanenti non strutt.			G_{2K}	=	1.024	x	1,5	**1.536**	kg/mq
								γ_Q		
	Carichi variabili			Q_{2K}	=	250	x	1,5	**375**	kg/mq
PLATEA RISERVA IDRICA						H tot [cm] =		60		
ANALISI DEI CARICHI										
	VALORI CARATTERISTCI									
	Calcestruzzo	0,60	x	2.500	=	1.500	kg/mq	γ_{G1}		
	Permanenti strutt.			G_{1K}	=	1.500	x	1,3	**1.950**	kg/mq
	Vespaio areato con igloo				=	250	kg/mq			
	Pavimentazione industriale	0,20	x	2.400	=	480	kg/mq			
	Peso dell'acqua	2,90	x	1.000	=	2.900	kg/mq	γ_{G2}		
	Permanenti non strutt.			G_{2K}	=	3.630	x	1,5	**5.445**	kg/mq
								γ_Q		
	Carichi variabili			Q_{2K}	=	0	x	1,5	**0**	kg/mq
PIASTRA PARCHEGGIO (Liv. -2 e -1)						H tot [cm] =		25		
ANALISI DEI CARICHI										
	VALORI CARATTERISTCI									
	Calcestruzzo	0,25	x	2.500	=	625	kg/mq	γ_{G1}		
	Permanenti strutt.			G_{1K}	=	625	x	1,3	**813**	kg/mq
	Pavimentazione industriale	0,20	x	2.400	=	480	kg/mq			
	Intonaco				=	30	kg/mq			
	Impianti				=	40	kg/mq	γ_{G2}		
	Permanenti non strutt.			G_{2K}	=	550	x	1,5	**825**	kg/mq
								γ_Q		
	Carichi variabili			Q_{2K}	=	250	x	1,5	**375**	kg/mq
PIASTRA PARCHEGGIO CON TERRENO H=1,00 ml (Liv. 0)						H tot [cm] =		50		
ANALISI DEI CARICHI										
	VALORI CARATTERISTCI									
	Calcestruzzo	0,50	x	2.500	=	1.250	kg/mq	γ_{G1}		
	Permanenti strutt.			G_{1K}	=	1.250	x	1,3	**1.625**	kg/mq
	Massetto	0,25	x	2.400	=	600	kg/mq			
	Coibent + Imperm				=	20	kg/mq			
	Terreno Vegetale	1,00	x	1.600	=	1.600	kg/mq			
	Intonaco				=	30	kg/mq	γ_{G2}		
	Permanenti non strutt.			G_{2K}	=	2.250	x	1,5	**3.375**	kg/mq
								γ_Q		
	Carichi variabili			Q_{2K}	=	400	x	1,5	**600**	kg/mq

PIASTRA PARCHEGGIO CON TERRENO H=2,00 ml (Liv. 0)						H tot [cm] =		50		
ANALISI DEI CARICHI										
	VALORI CARATTERISTCI									
	Calcestruzzo	0,50	x	2.500	=	1.250	kg/mq	γ_{G1}		
	Permanenti strutt.			G_{1K}	=	1.250	x	1,3	**1.625**	kg/mq
	Massetto	0,25	x	2.400	=	600	kg/mq			
	Coibent + Imperm				=	20	kg/mq			
	Terreno Vegetale	2,00	x	1.600	=	3.200	kg/mq			
	Intonaco				=	30	kg/mq	γ_{G2}		
	Permanenti non strutt.			G_{2K}	=	3.850	x	1,5	**5.775**	kg/mq
								γ_Q		
	Carichi v ariabili			Q_{2K}	=	400	x	1,5	**600**	kg/mq
PIASTRA PARCHEGGIO CON TERRENO H=3,00 ml (Liv. 0)						H tot [cm] =		50		
ANALISI DEI CARICHI										
	VALORI CARATTERISTCI									
	Calcestruzzo	0,50	x	2.500	=	1.250	kg/mq	γ_{G1}		
	Permanenti strutt.			G_{1K}	=	1.250	x	1,3	**1.625**	kg/mq
	Massetto	0,25	x	2.400	=	600	kg/mq			
	Coibent + Imperm				=	20	kg/mq			
	Terreno Vegetale	3,00	x	1.600	=	4.800	kg/mq			
	Intonaco				=	30	kg/mq	γ_{G2}		
	Permanenti non strutt.			G_{2K}	=	5.450	x	1,5	**8.175**	kg/mq
								γ_Q		
	Carichi v ariabili			Q_{2K}	=	400	x	1,5	**600**	kg/mq
PIASTRA LIVELLO 0 LOC. TEC.						H tot [cm] =		20		
ANALISI DEI CARICHI										
	VALORI CARATTERISTCI									
	Calcestruzzo	0,20	x	2.500	=	500	kg/mq	γ_{G1}		
	Permanenti strutt.			G_{1K}	=	500	x	1,3	**650**	kg/mq
	Massetto	0,10	x	2.400	=	240	kg/mq			
	Pav imento					50	kg/mq			
	Intonaco				=	30	kg/mq	γ_{G2}		
	Permanenti non strutt.			G_{2K}	=	320	x	1,5	**480**	kg/mq
								γ_Q		
	Carichi v ariabili			Q_{2K}	=	400	x	1,5	**600**	kg/mq
PIASTRA COPERTURA LOC. TEC.						H tot [cm] =		20		
ANALISI DEI CARICHI										
	VALORI CARATTERISTCI									
	Calcestruzzo	0,20	x	2.500	=	500	kg/mq	γ_{G1}		
	Permanenti strutt.			G_{1K}	=	500	x	1,3	**650**	kg/mq
	Massetto	0,15	x	2.400	=	360	kg/mq			
	Coibent + Imperm				=	10	kg/mq			
	Pav imento					50	kg/mq			
	Intonaco				=	30	kg/mq	γ_{G2}		
	Permanenti non strutt.			G_{2K}	=	450	x	1,5	**675**	kg/mq
								γ_Q		
	Carichi v ariabili			Q_{2K}	=	100	x	1,5	**150**	kg/mq
SOLETTA RAMPA						H tot [cm] =		25		
ANALISI DEI CARICHI										
	VALORI CARATTERISTCI									
	Calcestruzzo	0,25	x	2.500	=	625	kg/mq	γ_{G1}		
	Permanenti strutt.			G_{1K}	=	625	x	1,3	**813**	kg/mq
	Pav iment. Industr.	0,20	x	2.200	=	440	kg/mq			
	Intonaco				=	30	kg/mq	γ_{G2}		
	Permanenti non strutt.			G_{2K}	=	470	x	1,5	**705**	kg/mq
								γ_Q		
	Carichi v ariabili			Q_{2K}	=	500	x	1,5	**750**	kg/mq

SOLETTA COPERTURA RAMPA						H tot [cm] =		20								
ANALISI DEI CARICHI																
	VALORI CARATTERISTCI															
	Calcestruzzo	0,20	x	2.500	=	500	kg/mq	γ_{G1}								
	Permanenti strutt.			G_{1K}	=	500	x	1,3	**650**	kg/mq						
	Massetto	0,20	x	2.000	=	400	kg/mq									
	Coiben. + Imperm.				=	20	kg/mq									
	Terreno vegetale	0,15	x	1.600	=	240	kg/mq									
	Intonaco				=	30	kg/mq	γ_{G2}								
	Permanenti non strutt.			G_{2K}	=	690	x	1,5	**1.035**	kg/mq						
								γ_Q								
	Carichi variabili			Q_{2K}	=	100	x	1,5	**150**	kg/mq						
GRIGLIATO DI COPERTURA CANALI SHUNT																
ANALISI DEI CARICHI																
	VALORI CARATTERISTCI															
	Trave in acciaio				=	14	kg/mq									
	Orsogrill				=	20	kg/mq	γ_{G1}								
	Permanenti strutt.			G_{1K}	=	34	x	1,3	**44**	kg/mq						
	Permanenti non strutt.			G_{2K}	=		x	1,5	**0**	kg/mq						
								γ_Q								
	Carichi variabili			Q_{2K}	=	500	x	1,5	**750**	kg/mq						
GRIGLIATO IN LEGNO																
ANALISI DEI CARICHI		L'analisi dei carichi si riferisce al metro di sviluppo longitudinale del grigliato														
	LISTELLI VERTICALI				**LISTELLI ORIZZONTALI**											
Base	0,04	m			Base		0,08	m								
Profondità	0,06	m			Profondità		0,08	m								
Lunghezza	5,00	m			Lunghezza		1,00	m								
Passo	0,08	m			Numero		6,0	n/m								
	TRAVI A SBALZO IN ACCIAIO															
Numero travi	2	n														
Listelli verticali	0,04	x	0,06	x	5,00	/	0,08	x	650	/	2	=	49	kg/m		
Listelli orizzontali	0,08	x	0,08	x	1,00	x	6,0	x	650	/	2	=	12	kg/m		
							Permanenti non strutturali:			G_{2k}	**61**	**x**	**1,50**	**=**	**92**	**kg/m**

Calcolo delle spinte del terreno

Setto H=14,25 ml

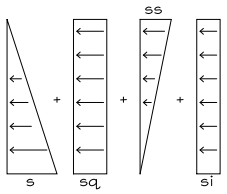
Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	14,70	[ml]	H
	Altezza terreno sul setto	14,70	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,370	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,364	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	35	[°ses]	ϕ_k
	Angolo d'attrito ridotto	29,3	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	19,5	[°ses]	δ
	Peso specifico	2,00	[t/mc]	γ
	Coeff. spinta attiva	0,306	[adim]	Ka
DATI DI CARICO	Sovraccarico	2,00	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	14,70	
Quota di applicazione (dalla testa)	[ml]	7,35	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	66,13	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	80,02	Componente verticale diretta verso l'alto
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	78,71	Componente verticale diretta verso il basso
			Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	13,89	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	9,00	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	5,40	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-14,70		a quota	-14,70
Pressione P_A	[t/m]	9,00	Spinta uniforme equivalente a S_A	[t/mq]	4,50
Pressione dovuta al sisma Ps	[t/m]	1,89	Spinta uniforme equivalente a Ss	[t/mq]	0,94
Pressione dovuta al sovraccarico Pq	[t/m]	0,61	Spinta uniforme equivalente a Sq	[t/mq]	0,61
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,37	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,37
Pressione in assenza di sisma	[t/m]	9,61	Spinta in assenza di sisma	[t/mq]	5,44
Pressione in presenza di sisma	[t/m]	11,25	Spinta in presenza di sisma	[t/mq]	5,81

SCHEMA DI CARICO



Calcolo delle spinte del terreno

Setto H=14,25 ml

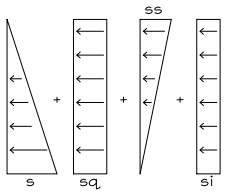
Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	14,25	[ml]	H
	Altezza terreno sul setto	14,25	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,370	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,364	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	35	[°ses]	ϕ_k
	Angolo d'attrito ridotto	29,3	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	19,5	[°ses]	δ
	Peso specifico	2,00	[t/mc]	γ
	Coeff. spinta attiva	0,306	[adim]	Ka
DATI DI CARICO	Sovraccarico	2,00	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	14,25	
Quota di applicazione (dalla testa)	[ml]	7,13	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	62,14	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	75,19	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	73,96	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	13,05	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	8,72	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	5,23	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-14,25		a quota	-14,25
Pressione P_A	[t/m]	8,72	Spinta uniforme equivalente a S_A	[t/mq]	4,36
Pressione dovuta al sisma Ps	[t/m]	1,83	Spinta uniforme equivalente a Ss	[t/mq]	0,92
Pressione dovuta al sovraccarico Pq	[t/m]	0,61	Spinta uniforme equivalente a Sq	[t/mq]	0,61
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,37	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,37
Pressione in assenza di sisma	[t/m]	9,33	Spinta in assenza di sisma	[t/mq]	5,28
Pressione in presenza di sisma	[t/m]	10,92	Spinta in presenza di sisma	[t/mq]	5,64

SCHEMA DI CARICO



Calcolo delle spinte del terreno

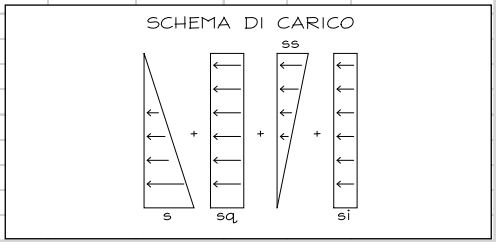
Setto H=14,25 ml - folla compatta

Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	14,25	[ml]	H
	Altezza terreno sul setto	14,25	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,370	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,364	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	35	[°ses]	ϕ_k
	Angolo d'attrito ridotto	29,3	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	19,5	[°ses]	δ
	Peso specifico	2,00	[t/mc]	γ
	Coeff. spinta attiva	0,306	[adim]	Ka
DATI DI CARICO	Sovraccarico	0,50	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	14,25	
Quota di applicazione (dalla testa)	[ml]	7,13	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	62,14	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	75,19	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	73,96	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	13,05	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	2,18	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	1,31	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-14,25		a quota	-14,25
Pressione P_A	[t/m]	8,72	Spinta uniforme equivalente a S_A	[t/mq]	4,36
Pressione dovuta al sisma Ps	[t/m]	1,83	Spinta uniforme equivalente a Ss	[t/mq]	0,92
Pressione dovuta al sovraccarico Pq	[t/m]	0,15	Spinta uniforme equivalente a Sq	[t/mq]	0,15
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,09	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,09
Pressione in assenza di sisma	[t/m]	8,87	Spinta in assenza di sisma	[t/mq]	5,28
Pressione in presenza di sisma	[t/m]	10,65	Spinta in presenza di sisma	[t/mq]	5,37



Calcolo delle spinte del terreno

Setto H=13,50 ml

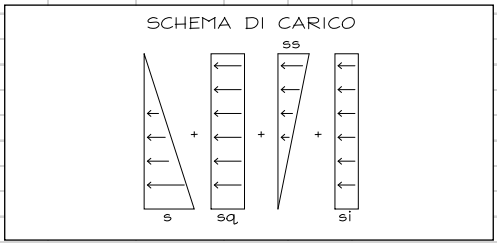
Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	13,50	[ml]	H
	Altezza terreno sul setto	13,50	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,370	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,364	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	35	[°ses]	ϕ_k
	Angolo d'attrito ridotto	29,3	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	19,5	[°ses]	δ
	Peso specifico	2,00	[t/mc]	γ
	Coeff. spinta attiva	0,306	[adim]	Ka
DATI DI CARICO	Sovraccarico	2,00	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	13,50	
Quota di applicazione (dalla testa)	[ml]	6,75	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	55,77	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	67,48	Componente verticale diretta verso l'alto
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	66,38	Componente verticale diretta verso il basso
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	11,71	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	8,26	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	4,96	

Si considera tra le due la spinta maggiore

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-13,50		a quota	-13,50
Pressione P_A	[t/m]	8,26	Spinta uniforme equivalente a S_A	[t/mq]	4,13
Pressione dovuta al sisma Ps	[t/m]	1,74	Spinta uniforme equivalente a Ss	[t/mq]	0,87
Pressione dovuta al sovraccarico Pq	[t/m]	0,61	Spinta uniforme equivalente a Sq	[t/mq]	0,61
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,37	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,37
Pressione in assenza di sisma	[t/m]	8,87	Spinta in assenza di sisma	[t/mq]	5,00
Pressione in presenza di sisma	[t/m]	10,37	Spinta in presenza di sisma	[t/mq]	5,37



Calcolo delle spinte del terreno

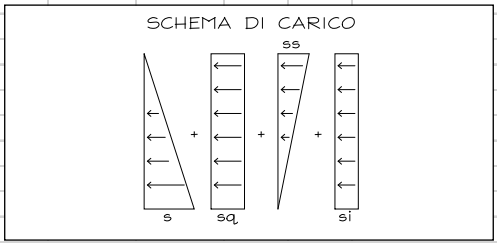
Setto H=13,50 ml - folla compatta

Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	13,50	[ml]	H
	Altezza terreno sul setto	13,50	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,370	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,364	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	35	[°ses]	ϕ_k
	Angolo d'attrito ridotto	29,3	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	19,5	[°ses]	δ
	Peso specifico	2,00	[t/mc]	γ
	Coeff. spinta attiva	0,306	[adim]	Ka
DATI DI CARICO	Sovraccarico	0,50	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	13,50	
Quota di applicazione (dalla testa)	[ml]	6,75	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	55,77	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	67,48	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	66,38	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	11,71	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	2,07	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	1,24	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-13,50		a quota	-13,50
Pressione P_A	[t/m]	8,26	Spinta uniforme equivalente a S_A	[t/mq]	4,13
Pressione dovuta al sisma Ps	[t/m]	1,74	Spinta uniforme equivalente a Ss	[t/mq]	0,87
Pressione dovuta al sovraccarico Pq	[t/m]	0,15	Spinta uniforme equivalente a Sq	[t/mq]	0,15
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,09	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,09
Pressione in assenza di sisma	[t/m]	8,42	Spinta in assenza di sisma	[t/mq]	5,00
Pressione in presenza di sisma	[t/m]	10,09	Spinta in presenza di sisma	[t/mq]	5,09



Calcolo delle spinte del terreno

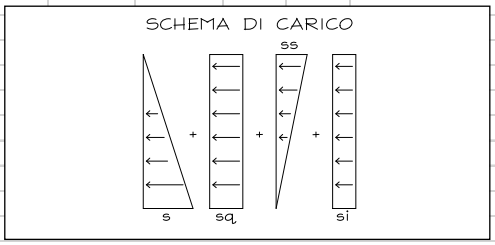
Setto H=12,40 ml

Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	12,40	[ml]	H
	Altezza terreno sul setto	12,40	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,370	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,364	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	35	[°ses]	ϕ_k
	Angolo d'attrito ridotto	29,3	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	19,5	[°ses]	δ
	Peso specifico	2,00	[t/mc]	γ
	Coeff. spinta attiva	0,306	[adim]	Ka
DATI DI CARICO	Sovraccarico	2,00	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	12,40	
Quota di applicazione (dalla testa)	[ml]	6,20	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	47,05	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	56,94	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	56,00	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	9,88	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	7,59	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	4,55	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-12,40		a quota	-12,40
Pressione P_A	[t/m]	7,59	Spinta uniforme equivalente a S_A	[t/mq]	3,79
Pressione dovuta al sisma Ps	[t/m]	1,59	Spinta uniforme equivalente a Ss	[t/mq]	0,80
Pressione dovuta al sovraccarico Pq	[t/m]	0,61	Spinta uniforme equivalente a Sq	[t/mq]	0,61
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,37	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,37
Pressione in assenza di sisma	[t/m]	8,20	Spinta in assenza di sisma	[t/mq]	4,59
Pressione in presenza di sisma	[t/m]	9,55	Spinta in presenza di sisma	[t/mq]	4,96



Calcolo delle spinte del terreno

Setto H=12,40 ml - folla compatta

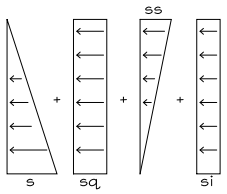
Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	12,40	[ml]	H
	Altezza terreno sul setto	12,40	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,370	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,364	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	35	[°ses]	ϕ_k
	Angolo d'attrito ridotto	29,3	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	19,5	[°ses]	δ
	Peso specifico	2,00	[t/mc]	γ
	Coeff. spinta attiva	0,306	[adim]	Ka
DATI DI CARICO	Sovraccarico	0,50	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	12,40	
Quota di applicazione (dalla testa)	[ml]	6,20	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	47,05	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	56,94	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	56,00	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	9,88	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	1,90	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	1,14	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-12,40		a quota	-12,40
Pressione P_A	[t/m]	7,59	Spinta uniforme equivalente a S_A	[t/mq]	3,79
Pressione dovuta al sisma Ps	[t/m]	1,59	Spinta uniforme equivalente a Ss	[t/mq]	0,80
Pressione dovuta al sovraccarico Pq	[t/m]	0,15	Spinta uniforme equivalente a Sq	[t/mq]	0,15
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,09	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,09
Pressione in assenza di sisma	[t/m]	7,74	Spinta in assenza di sisma	[t/mq]	4,59
Pressione in presenza di sisma	[t/m]	9,27	Spinta in presenza di sisma	[t/mq]	4,68

SCHEMA DI CARICO



Calcolo delle spinte del terreno

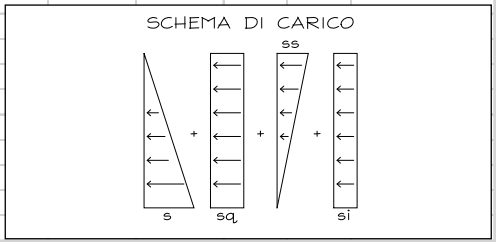
Setto H=11,65 ml - folla compatta

Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	11,65	[ml]	H
	Altezza terreno sul setto	11,65	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,370	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,364	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	35	[°ses]	ϕ_k
	Angolo d'attrito ridotto	29,3	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	19,5	[°ses]	δ
	Peso specifico	2,00	[t/mc]	γ
	Coeff. spinta attiva	0,306	[adim]	Ka
DATI DI CARICO	Sovraccarico	0,50	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	11,65	
Quota di applicazione (dalla testa)	[ml]	5,83	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	41,53	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	50,26	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	49,43	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	8,72	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	1,78	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	1,07	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-11,65		a quota	-11,65
Pressione P_A	[t/m]	7,13	Spinta uniforme equivalente a S_A	[t/mq]	3,57
Pressione dovuta al sisma Ps	[t/m]	1,50	Spinta uniforme equivalente a Ss	[t/mq]	0,75
Pressione dovuta al sovraccarico Pq	[t/m]	0,15	Spinta uniforme equivalente a Sq	[t/mq]	0,15
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,09	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,09
Pressione in assenza di sisma	[t/m]	7,28	Spinta in assenza di sisma	[t/mq]	4,31
Pressione in presenza di sisma	[t/m]	8,72	Spinta in presenza di sisma	[t/mq]	4,41



Calcolo delle spinte del terreno

Setto H=3,50 ml

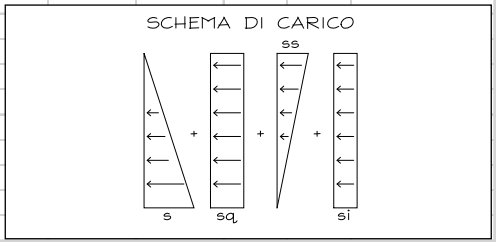
Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	3,50	[ml]	H
	Altezza terreno sul setto	3,50	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,300		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,435	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,428	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	30	[°ses]	ϕ_k
	Angolo d'attrito ridotto	24,8	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	16,5	[°ses]	δ
	Peso specifico	1,60	[t/mc]	γ
	Coeff. spinta attiva	0,364	[adim]	Ka
DATI DI CARICO	Sovraccarico	0,50	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	3,50	
Quota di applicazione (dalla testa)	[ml]	1,75	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	3,56	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	4,26	Componente verticale diretta verso l'alto
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	4,20	Componente verticale diretta verso il basso
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	0,70	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	0,64	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	0,19	

Si considera tra le due la spinta maggiore

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-3,50		a quota	-3,50
Pressione P_A	[t/m]	2,04	Spinta uniforme equivalente a S_A	[t/mq]	1,02
Pressione dovuta al sisma Ps	[t/m]	0,40	Spinta uniforme equivalente a Ss	[t/mq]	0,20
Pressione dovuta al sovraccarico Pq	[t/m]	0,18	Spinta uniforme equivalente a Sq	[t/mq]	0,18
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,05	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,05
Pressione in assenza di sisma	[t/m]	2,22	Spinta in assenza di sisma	[t/mq]	1,22
Pressione in presenza di sisma	[t/m]	2,49	Spinta in presenza di sisma	[t/mq]	1,27



Calcolo delle spinte del terreno

Setto H=3,20 ml

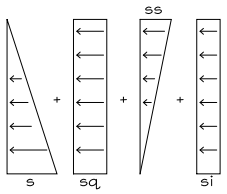
Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	3,20	[ml]	H
	Altezza terreno sul setto	3,20	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,300		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,435	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,428	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	30	[°ses]	ϕ_k
	Angolo d'attrito ridotto	24,8	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	16,5	[°ses]	δ
	Peso specifico	1,60	[t/mc]	γ
	Coeff. spinta attiva	0,364	[adim]	Ka
DATI DI CARICO	Sovraccarico	0,50	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	3,20	
Quota di applicazione (dalla testa)	[ml]	1,60	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	2,98	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	3,56	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	3,51	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	0,58	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	0,58	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	0,17	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-3,20		a quota	-3,20
Pressione P_A	[t/m]	1,86	Spinta uniforme equivalente a S_A	[t/mq]	0,93
Pressione dovuta al sisma Ps	[t/m]	0,36	Spinta uniforme equivalente a Ss	[t/mq]	0,18
Pressione dovuta al sovraccarico Pq	[t/m]	0,18	Spinta uniforme equivalente a Sq	[t/mq]	0,18
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,05	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,05
Pressione in assenza di sisma	[t/m]	2,04	Spinta in assenza di sisma	[t/mq]	1,11
Pressione in presenza di sisma	[t/m]	2,28	Spinta in presenza di sisma	[t/mq]	1,17

SCHEMA DI CARICO



Calcolo delle spinte del terreno

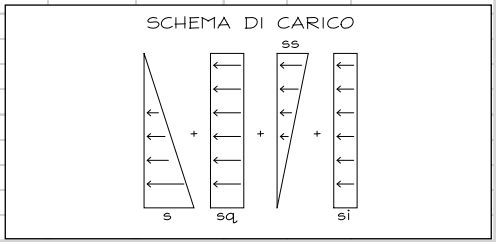
Setto H=2,80 ml

Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	2,80	[ml]	H
	Altezza terreno sul setto	2,80	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,435	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,428	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	30	[°ses]	ϕ_k
	Angolo d'attrito ridotto	24,8	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	16,5	[°ses]	δ
	Peso specifico	1,60	[t/mc]	γ
	Coeff. spinta attiva	0,364	[adim]	Ka
DATI DI CARICO	Sovraccarico	0,50	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	2,80	
Quota di applicazione (dalla testa)	[ml]	1,40	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	2,28	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	2,73	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	2,69	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	0,45	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	0,51	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	0,31	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-2,80		a quota	-2,80
Pressione P_A	[t/m]	1,63	Spinta uniforme equivalente a S_A	[t/mq]	0,81
Pressione dovuta al sisma Ps	[t/m]	0,32	Spinta uniforme equivalente a Ss	[t/mq]	0,16
Pressione dovuta al sovraccarico Pq	[t/m]	0,18	Spinta uniforme equivalente a Sq	[t/mq]	0,18
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,11	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,11
Pressione in assenza di sisma	[t/m]	1,81	Spinta in assenza di sisma	[t/mq]	0,97
Pressione in presenza di sisma	[t/m]	2,06	Spinta in presenza di sisma	[t/mq]	1,08



Calcolo delle spinte del terreno

Setto H=2,40 ml

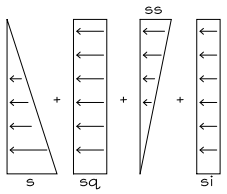
Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	2,40	[ml]	H
	Altezza terreno sul setto	2,40	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,435	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,428	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	30	[°ses]	ϕ_k
	Angolo d'attrito ridotto	24,8	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	16,5	[°ses]	δ
	Peso specifico	1,60	[t/mc]	γ
	Coeff. spinta attiva	0,364	[adim]	Ka
DATI DI CARICO	Sovraccarico	0,50	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	2,40	
Quota di applicazione (dalla testa)	[ml]	1,20	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	1,68	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	2,00	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	1,97	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	0,33	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	0,44	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	0,26	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-2,40		a quota	-2,40
Pressione P_A	[t/m]	1,40	Spinta uniforme equivalente a S_A	[t/mq]	0,70
Pressione dovuta al sisma Ps	[t/m]	0,27	Spinta uniforme equivalente a Ss	[t/mq]	0,14
Pressione dovuta al sovraccarico Pq	[t/m]	0,18	Spinta uniforme equivalente a Sq	[t/mq]	0,18
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,11	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,11
Pressione in assenza di sisma	[t/m]	1,58	Spinta in assenza di sisma	[t/mq]	0,83
Pressione in presenza di sisma	[t/m]	1,78	Spinta in presenza di sisma	[t/mq]	0,94

SCHEMA DI CARICO



Calcolo delle spinte del terreno

Setto H=2,00 ml

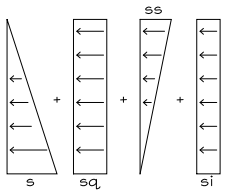
Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	2,00	[ml]	H
	Altezza terreno sul setto	2,00	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,600		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,435	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,428	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	30	[°ses]	ϕ_k
	Angolo d'attrito ridotto	24,8	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	16,5	[°ses]	δ
	Peso specifico	1,60	[t/mc]	γ
	Coeff. spinta attiva	0,364	[adim]	Ka
DATI DI CARICO	Sovraccarico	0,50	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	2,00	
Quota di applicazione (dalla testa)	[ml]	1,00	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	1,16	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	1,39	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	1,37	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	0,23	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	0,36	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	0,22	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-2,00		a quota	-2,00
Pressione P_A	[t/m]	1,16	Spinta uniforme equivalente a S_A	[t/mq]	0,58
Pressione dovuta al sisma Ps	[t/m]	0,23	Spinta uniforme equivalente a Ss	[t/mq]	0,11
Pressione dovuta al sovraccarico Pq	[t/m]	0,18	Spinta uniforme equivalente a Sq	[t/mq]	0,18
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,11	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,11
Pressione in assenza di sisma	[t/m]	1,35	Spinta in assenza di sisma	[t/mq]	0,70
Pressione in presenza di sisma	[t/m]	1,50	Spinta in presenza di sisma	[t/mq]	0,80

SCHEMA DI CARICO



Calcolo delle spinte del terreno

Setto H=1,20 ml

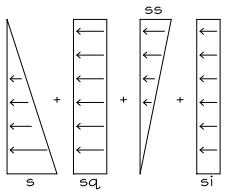
Di seguito vengono calcolate le spinte del terreno sulle pareti della struttura.

DATI GEOMETRICI	Altezza totale	1,20	[ml]	H
	Altezza terreno sul setto	1,20	[ml]	Ht
	Larghezza elemento	1,00	[ml]	B
DATI SISMICI	Categoria Terreno	**B**		
	Accelerazione al suolo	0,247		ag/g
	Coeff. Topografico	1,000	[adim]	S_T
	Coeff. Stratigrafico	1,157	[adim]	S_S
	Coeff. di Amplificazione	1,157	[adim]	S
	Coeff. di combinazione	0,300		ψ_2
	Coeff. di riduzione acc. max	0,31	[adim]	βm
	Acceelerazione massima	0,286		a_{max}
	Coeff. sismico orizzontale	0,089		k_h
	Coeff. sismico verticale	0,044		k_v
	Inclinazione risultante forza peso e d'inerzia	5,31	[°ses]	ϑ Rivolta verso l'alto
	Inclinazione risultante forza peso e d'inerzia	4,86	[°ses]	ϑ Rivolta verso il basso
	Coeff. spinta attiva in sisma	0,435	[adim]	K_{AE} Comp. vert. diretta verso l'alto
	Coeff. spinta attiva in sisma	0,428	[adim]	K_{AE} Comp. vert. diretta verso il basso
DATI GEOTECNICI	Coeff. Parziale	1,25	[adim]	γ_ϕ
	Angolo di pendio	0	[°ses]	β
	Angolo paramento interno rispetto all'orizzontale	90	[°ses]	ψ
	Angolo d'attrito	30	[°ses]	ϕ_k
	Angolo d'attrito ridotto	24,8	[°ses]	ϕ'_k
	Angolo d'attrito paratia-terreno	16,5	[°ses]	δ
	Peso specifico	1,60	[t/mc]	γ
	Coeff. spinta attiva	0,364	[adim]	Ka
DATI DI CARICO	Sovraccarico	0,50	[t/mq]	q

PROFONDITA' (dalla testa) H	[ml]	1,20	
Quota di applicazione (dalla testa)	[ml]	0,60	
S_A: sp.attiva **B x 0,5 x γ x Ht^2 x ka**	[t]	0,42	
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	0,50	Componente verticale diretta verso l'alto — Si considera tra le due la spinta maggiore
S_{AE}: Spinta in sisma **B x 0,5 x γ x Ht^2 x K_{AE}**	[t]	0,49	Componente verticale diretta verso il basso — Si considera tra le due la spinta maggiore
ss: incremento di spinta in sisma **S_{AE} - S_A**	[t]	0,08	
sq: spinta sovracc. **B x q x Ht x Ka**	[t]	0,22	
sq_S: spinta sovracc. in sisma **B x q x ψ_2 x Ht x Ka**	[t]	0,07	

Pressione esercitata dal terreno fondo scavo			Spinta a mq		
	Da quota	0,00		Da quota	0,00
	a quota	-1,20		a quota	-1,20
Pressione P_A	[t/m]	0,70	Spinta uniforme equivalente a S_A	[t/mq]	0,35
Pressione dovuta al sisma Ps	[t/m]	0,14	Spinta uniforme equivalente a Ss	[t/mq]	0,07
Pressione dovuta al sovraccarico Pq	[t/m]	0,18	Spinta uniforme equivalente a Sq	[t/mq]	0,18
Pressione dovuta al sovracc. a Pq_S in sisma	[t/m]	0,05	Spinta uniforme equivalente a Sq_S in sisma	[t/mq]	0,05
Pressione in assenza di sisma	[t/m]	0,88	Spinta in assenza di sisma	[t/mq]	0,42
Pressione in presenza di sisma	[t/m]	0,89	Spinta in presenza di sisma	[t/mq]	0,47

SCHEMA DI CARICO



Verifiche elementi secondari

Soletta in c.a. - NTC08										PARCHEGGIO	
DATI SEZIONE									Soletta Rampa carrabile		
	H tot [cm] =	25		Larghezza trave [cm] =			40	Lb			
MATERIALI											
	CALCESTRUZZO	**C32/40**				Rck	=	400	kg/cmq		
		f_{ck}	=	0,83	x	400	=	332	kg/cmq		
		f_{cm}	=	332	+	80	=	412	kg/cmq		
		f_{ctm}	=				=	17	kg/cmq		
	(γ_c=1,5 - α_{cc}=0,85)	f_{cd}	=	332	/	1,76	=	188	kg/cmq		
		E_{cm}	=				=	336.428	kg/cmq		
	ACCIAIO	**B450C**									
		f_{yk}	=	4.300	kg/cmq						
	(γ_S=1,15)	f_{yd}	=	4.300	/	1,15	=	3.739	kg/cmq		
ANALISI DEI CARICHI											
	VALORI CARATTERISTCI										
	Calcestruzzo	0,25	x	2.500	=	625	kg/mq	γ_{G1}			
	Permanenti strutt.			**G_{1K}**	=	625	x	1,3	**813**	kg/mq	
	Paviment. Industr.	0,20	x	2.200	=	440	kg/mq				
	Intonaco				=	30	kg/mq	γ_{G2}			
	Permanenti non strutt.			**G_{2K}**	=	470	x	1,5	**705**	kg/mq	
								γ_Q			
	Carichi variabili			**G_{2K}**	=	500	x	1,5	**750**	kg/mq	
	VALORI DI CALCOLO	**Gd**	=	**813**	+	**705**	=	**1.518**	kg/mq		
		Qd	=				=	**750**	kg/mq		
					Carico Totale Qt		=	**2.268**	kg/mq		
DATI GEOMETRICI											
	Luce di calcolo	Lc	=	4,35	ml		(in asse travi)				
	Larghezza di calcolo	b	=	1,00	ml						
	Copriferro	c	=	3,0	cm						
	Altezza utile della sezione	d	=	22,0	cm						
DATI DI CARICO											
	Carico lineare q:	Qt x b	=	2.268	kg/ml						
CARATTERISTICHE DI SOLLECITAZIONE				Camp	Bordo						
	Coefficiente Km			10	12						
	Md = (q x Lc^2) / Km		=	4.291	3.576	kgm					
	Vsd = (q x (Lc-Lb)) / 2		=		4.478	kg					
VERIFICHE SLV		Campata							Bordo		
	Armatura minima	7,5	cmq		Asmin1 = Md / (0,9 x d x fyd)			7,5	cmq		
		ϕ	n	Area	Asmin2 = 0,3% H x b			ϕ	n	Area	
	Armatura in progetto	16	3	6,0				16	3	6,0	
		16	2	4,0				16	2	4,0	
		Totale As =		10,1	>	7,5	7,5	<	Totale As =	10,1	
MOMENTI RESISTENTI		M_{rs}							M_d	K	
	Acciaio	7.443	kgm	Mrs = 0,9 x d x fyd x As				>	4.291	1,7	Camp
		7.443	kgm	Mrs = 0,9 x d x fyd x As				>	3.576	2,1	Bordo
	Calcestruzzo	b		Mrc	=	(d / r)^2 / b				K	
	Sezione piena	100	cm	12.100	kgm			>	4.291	2,8	
TAGLIO				V_{Rd1}		K	ρ_l	v_{min}	V_{Rd1}		V_{R2}
	Sezione piena	100	cm	10.852	kg	1,95	0,005	0,326	10.852	>	7.166
				V_{sd}			V_{Rd1}		K		
				4.478	kg	<	10.852		2,4		
VERIFICHE SLE - Deformazione								f [cm]	f [cm]	Lc / f	Min
	Permanenti strutturali	625	x	1,0	=	625	kg/ml	0,07	0,12	3.733	250
	Permanenti non strutt.	470	x	1,0	=	470	kg/ml	0,05			
	Variabili	500	x	1,0	=	500	kg/ml	0,05	0,05	8.174	300
	Controllo verifiche:		Acciaio:	Verificato							
			Calcestruzzo:	Verificato							
			Taglio:	Verificato							
			Deformazione:	Verificato							

Soletta in c.a. - NTC08										PARCHEGGIO	
DATI SEZIONE									Soletta Copertura Rampa		
	H tot [cm] =	20		Larghezza trave [cm] =			40	Lb			
MATERIALI											
	CALCESTRUZZO	**C32/40**				Rck	=	400	kg/cmq		
		f_{ck}	=	0,83	x	400	=	332	kg/cmq		
		f_{cm}	=	332	+	80	=	412	kg/cmq		
		f_{ctm}	=				=	17	kg/cmq		
	(γ_c=1,5 - α_{cc}=0,85)	f_{cd}	=	332	/	1,76	=	188	kg/cmq		
		E_{cm}	=				=	336.428	kg/cmq		
	ACCIAIO	**B450C**									
		f_{yk}	=	4.300	kg/cmq						
	(γ_s=1,15)	f_{yd}	=	4.300	/	1,15	=	3.739	kg/cmq		
ANALISI DEI CARICHI											
	VALORI CARATTERISTCI										
	Calcestruzzo	0,20	x	2.500	=	500	kg/mq	γ_{G1}			
	Permanenti strutt.			G_{1K}	=	500	x	1,3	**650**	kg/mq	
	Massetto	0,20	x	2.000	=	400	kg/mq				
	Coiben. + Imperm.				=	20	kg/mq				
	Terreno vegetale	0,15	x	1.600	=	240	kg/mq				
	Intonaco				=	30	kg/mq	γ_{G2}			
	Permanenti non strutt.			G_{2K}	=	690	x	1,5	**1.035**	kg/mq	
								γ_Q			
	Carichi variabili			G_{2K}	=	100	x	1,5	**150**	kg/mq	
	VALORI DI CALCOLO	**Gd**	=	**650**	+	**1.035**	=	**1.685**	kg/mq		
		Qd	=				=	**150**	kg/mq		
					Carico Totale Qt		=	**1.835**	kg/mq		
DATI GEOMETRICI											
	Luce di calcolo	Lc	=	4,35	ml		(in asse travi)				
	Larghezza di calcolo	b	=	1,00	ml						
	Copriferro	c	=	4,0	cm						
	Altezza utile della sezione	d	=	16,0	cm						
DATI DI CARICO											
	Carico lineare q:	Qt x b	=	1.835	kg/ml						
CARATTERISTICHE DI SOLLECITAZIONE				Camp	Bordo						
	Coefficiente Km			10	12						
	Md = (q x Lc^2) / Km		=	3.472	2.894	kgm					
	Vsd = (q x (Lc-Lb)) / 2		=		3.624	kg					
VERIFICHE SLV		Campata							Bordo		
	Armatura minima	6,4	cmq		Asmin1 = Md / (0,9 x d x fyd)			6,0	cmq		
		ϕ	n	Area	Asmin2 = 0,3% H x b			ϕ	n	Area	
	Armatura in progetto	14	3	4,6				14	3	4,6	
		14	2	3,1				14	2	3,1	
		Totale As =		7,7	>	6,4	6,0	<	Totale As =	7,7	
MOMENTI RESISTENTI		M_{rs}							M_d	K	
	Acciaio	4.144	kgm	Mrs = 0,9 x d x fyd x As				>	3.472	1,2	Camp
		4.144	kgm	Mrs = 0,9 x d x fyd x As				>	2.894	1,4	Bordo
	Calcestruzzo	b		Mrc	=	(d / r)^2 / b				K	
	Sezione piena	100	cm	6.400	kgm			>	3.472	1,8	
TAGLIO				V_{Rd1}		K	ρ_1	v_{min}	V_{Rd1}		V_{R2}
	Sezione piena	100	cm	8.220	kg	2,00	0,005	0,337	8.220	>	5.399
				V_{sd}			V_{Rd1}		K		
				3.624	kg	<	8.220		2,3		
VERIFICHE SLE - Deformazione								f [cm]	f [cm]	Lc / f	Min
	Permanenti strutturali	500	x	1,0	=	500	kg/ml	0,10	0,25	1.759	250
	Permanenti non strutt.	690	x	1,0	=	690	kg/ml	0,14			
	Variabili	100	x	1,0	=	100	kg/ml	0,02	0,02	20.926	300
	Controllo verifiche:		Acciaio:	Verificato							
			Calcestruzzo:	Verificato							
			Taglio:	Verificato							
			Deformazione:	Verificato							

Gradino a sbalzo in c.a. - NTC08											PARCHEGGIO
DATI SEZIONE											Sbalzo Gradino Ln 155
	Alzata [cm] =	16,75			Pedata [cm] =		30				
	Spessore soletta [cm] =	15									
	H tot [cm] =	15,0		Larghezza trave [cm] =			30	Lb			
MATERIALI											
	CALCESTRUZZO	**C32/40**				Rck	=	400	kg/cmq		
		f_{ck}	=	0,83	x	400	=	332	kg/cmq		
		f_{cm}	=	332	+	80	=	412	kg/cmq		
		f_{ctm}	=				=	17	kg/cmq		
	(γ_c=1,5 - α_{cc}=0,85)	f_{cd}	=	332	/	1,76	=	188	kg/cmq		
		E_{cm}	=				=	336.428	kg/cmq		
	ACCIAIO	**B450C**									
		f_{yk}	=	4.300	kg/cmq						
	(γ_s=1,15)	f_{yd}	=	4.300	/	1,15	=	3.739	kg/cmq		
ANALISI DEI CARICHI											
	VALORI CARATTERISTCI										
	Calcestruzzo soletta	0,15	x	2.500	=	375	kg/mq				
	Calcestruzzo gradino	0,08	x	2.500	=	209	kg/mq	γ_{G1}			
	Permanenti strutt.			**G_{1K}**	=	584	x	1,3	**760**	kg/mq	
	Grado e sottogrado				=	100	kg/mq				
	Intonaco				=	30	kg/mq				
	Incidenza parapetto				=	50	kg/mq	γ_{G2}			
	Permanenti non strutt.			**G_{2K}**	=	180	x	1,5	**270**	kg/mq	
								γ_Q			
	Carichi variabili			**G_{2K}**	=	400	x	1,5	**600**	kg/mq	
	VALORI DI CALCOLO	**Gd**	=	**760**	+	**270**	=	**1.030**	kg/mq		
		Qd	=				=	**600**	kg/mq		
					Carico Totale Qt		=	**1.630**	kg/mq		
DATI GEOMETRICI											
	Luce di calcolo	Lc	=	1,55	ml						
	Larghezza di calcolo	b	=	0,30	ml						
	Copriferro	c	=	3,0	cm						
	Altezza utile della sezione	d	=	12,0	cm						
DATI DI CARICO											
	Carico lineare q:	Qt x b	=	489	kg/ml						
CARATTERISTICHE DI SOLLECITAZIONE				Incastro							
	Coefficiente Km			2							
	Md = 1,4 x (q x Lc^2) / Km		=	822	kgm						
	Vsd = 1,4 x (q x Lc)		=	1.061	kg						
VERIFICHE SLV									Incastro		
	Armatura minima	Asmin1 = Md / (0,9 x d x fyd)					Asmin =	2,0	cmq		
		Asmin2 = 0,3% H x b						ϕ	n	Area	
	Armatura in progetto							12	1	1,1	
								12	1	1,1	
							2,0	<	Totale As =	2,3	
MOMENTI RESISTENTI		M_{rs}							M_d	K	
	Acciaio	913	kgm	Mrs = 0,9 x d x fyd x As				>	822	1,1	Incastro
	Calcestruzzo	b		Mrc	=	(d / r)^2 / b				K	
	Sezione piena	30	cm	1.080	kgm			>	822	1,3	
TAGLIO				V_{Rd1}		K	ρ_1	v_{min}	V_{Rd1}		V_{R2}
	Sezione piena	30	cm	2.022	kg	2,00	0,006	0,337	2.022	>	1.215
				V_{sd}			V_{Rd1}		K		
				1.061	kg	<	2.022		1,9		
	Controllo verifiche:		Acciaio:	Verificato							
			Calcestruzzo:	Verificato							
			Taglio:	Verificato							

Soletta in c.a. - NTC08										PARCHEGGIO	
DATI SEZIONE									Soletta Pianerottolo Scala		
	H tot [cm] =	15		Larghezza trave [cm] =			30	Lb			
MATERIALI											
	CALCESTRUZZO	**C32/40**				Rck	=	400	kg/cmq		
		f_{ck}	=	0,83	x	400	=	332	kg/cmq		
		f_{cm}	=	332	+	80	=	412	kg/cmq		
		f_{ctm}	=				=	17	kg/cmq		
	(γ_c=1,5 - α_{cc}=0,85)	f_{cd}	=	332	/	1,76	=	188	kg/cmq		
		E_{cm}	=				=	336.428	kg/cmq		
	ACCIAIO	**B450C**									
		f_{yk}	=	4.300	kg/cmq						
	(γ_s=1,15)	f_{yd}	=	4.300	/	1,15	=	3.739	kg/cmq		
ANALISI DEI CARICHI											
	VALORI CARATTERISTCI										
	Calcestruzzo	0,15	x	2.500	=	375	kg/mq	γ_{G1}			
	Permanenti strutt.			G_{1K}	=	375	x	1,3	**488**	kg/mq	
	Massetto	0,10	x	2.000	=	200	kg/mq				
	Pavimento				=	60	kg/mq				
	Intonaco				=	30	kg/mq				
	Incidenza parapetti				=	50	kg/mq	γ_{G2}			
	Permanenti non strutt.			G_{2K}	=	340	x	1,5	**510**	kg/mq	
								γ_Q			
	Carichi variabili			G_{2K}	=	400	x	1,5	**600**	kg/mq	
	VALORI DI CALCOLO	**Gd**	=	**488**	+	**510**	=	**998**	kg/mq		
		Qd	=				=	**600**	kg/mq		
					Carico Totale Qt		=	**1.598**	kg/mq		
DATI GEOMETRICI											
	Luce di calcolo	Lc	=	3,60	ml		(in asse travi)				
	Larghezza di calcolo	b	=	1,00	ml						
	Copriferro	c	=	3,0	cm						
	Altezza utile della sezione	d	=	12,0	cm						
DATI DI CARICO											
	Carico lineare q:	Qt x b	=	1.598	kg/ml						
CARATTERISTICHE DI SOLLECITAZIONE				Camp	Bordo						
	Coefficiente Km			10	12						
	Md = (q x Lc^2) / Km		=	2.070	1.725	kgm					
	Vsd = (q x (Lc-Lb)) / 2		=		2.636	kg					
VERIFICHE SLV		Campata							Bordo		
	Armatura minima	5,1	cmq		Asmin1 = Md / (0,9 x d x fyd)			4,5	cmq		
		ϕ	n	Area	Asmin2 = 0,3% H x b			ϕ	n	Area	
	Armatura in progetto	14	2	3,1				14	2	3,1	
		14	2	3,1				14	2	3,1	
		Totale As =		6,2	>	5,1	4,5	<	Totale As =	6,2	
MOMENTI RESISTENTI		M_{rs}							M_d	K	
	Acciaio	2.487	kgm	Mrs = 0,9 x d x fyd x As				>	2.070	1,2	Camp
		2.487	kgm	Mrs = 0,9 x d x fyd x As				>	1.725	1,4	Bordo
	Calcestruzzo	b		Mrc	=	(d / r)^2 / b				K	
	Sezione piena	100	cm	3.600	kgm			>	2.070	1,7	
TAGLIO				V_{Rd1}		K	ρ_1	v_{min}	V_{Rd1}		V_{R2}
	Sezione piena	100	cm	6.299	kg	2,00	0,005	0,337	6.299	>	4.049
				V_{sd}			V_{Rd1}		K		
				2.636	kg	<	6.299		2,4		
VERIFICHE SLE - Deformazione								f [cm]	f [cm]	Lc / f	Min
	Permanenti strutturali	375	x	1,0	=	375	kg/ml	0,09	0,17	2.178	250
	Permanenti non strutt.	340	x	1,0	=	340	kg/ml	0,08			
	Variabili	400	x	1,0	=	400	kg/ml	0,09	0,09	3.894	300
	Controllo verifiche:		Acciaio:	Verificato							
			Calcestruzzo:	Verificato							
			Taglio:	Verificato							
			Deformazione:	Verificato							

Soletta Scala in c.a. - NTC08											PARCHEGGIO
DATI SEZIONE								Soletta Scala Tipo - Rampa lunga			
	H tot [cm] =	25		Larghezza trave [cm] =			30	Lb			
MATERIALI											
	CALCESTRUZZO	**C32/40**				Rck	=	400	kg/cmq		
		f_{ck}	=	0,83	x	400	=	332	kg/cmq		
		f_{cm}	=	332	+	80	=	412	kg/cmq		
		f_{ctm}	=				=	17	kg/cmq		
	(γ_c=1,5 - α_{cc}=0,85)	f_{cd}	=	332	/	1,76	=	188	kg/cmq		
		E_{cm}	=				=	336.428	kg/cmq		
	ACCIAIO	**B450C**									
		f_{yk}	=	4.300	kg/cmq						
	(γ_s=1,15)	f_{yd}	=	4.300	/	1,15	=	3.739	kg/cmq		
ANALISI DEI CARICHI											
	VALORI CARATTERISTCI										
	Calcestruzzo soletta	0,25	x	2.500	=	625	kg/mq	γ_{G1}			
	Permanenti strutt.			**G_{1K}**	=	625	x	1,3	**813**	kg/mq	
	Calcestruzzo gradino	0,08	x	2.500	=	201	kg/mq				
	Grado e sottogrado				=	100	kg/mq				
	Pavimento					60	kg/mq				
	Intonaco				=	30	kg/mq				
	Incidenza parapetto				=	50	kg/mq	γ_{G2}			
	Permanenti non strutt.			**G_{2K}**	=	441	x	1,5	**662**	kg/mq	
								γ_Q			
	Carichi variabili			**G_{2K}**	=	400	x	1,5	**600**	kg/mq	
	VALORI DI CALCOLO	**Gd**	=	**813**	+	**662**	=	**1.474**	kg/mq		
		Qd	=				=	**600**	kg/mq		
					Carico Totale Qt		=	**2.074**	kg/mq		
DATI GEOMETRICI											
	Lunghezza pianerottolo 1	Lc	=	0,95	ml		Alzata	=	0,161	ml	
	Lunghezza rampa	Lc	=	4,20	ml		Pedata	=	0,30	ml	
	Lunghezza pianerottolo 2	Lc	=	0,95	ml		Inclinazione	=	28	°se	
	Luce di calcolo	Lc	=	6,67	ml						
	Larghezza di calcolo	b	=	0,85	ml						
	Copriferro	c	=	3,0	cm						
	Altezza utile della sezione	d	=	22,0	cm						
DATI DI CARICO											
	Carico lineare q:	Qt x b	=	1.763	kg/ml						
CARATTERISTICHE DI SOLLECITAZIONE				Camp	Bordo						
	Coefficiente Km			10	12						
	Md = (q x Lc^2) / Km		=	7.836	6.530	kgm					
	Vsd = (q x (Lc-Lb)) / 2		=		5.613	kg					
VERIFICHE SLV		Campata							Bordo		
	Armatura minima	10,6	cmq		Asmin1 = Md / (0,9 x d x fyd)			8,8	cmq		
		ϕ	n	Area	Asmin2 = 0,3% H x b			ϕ	n	Area	
	Armatura in progetto	16	3	6,0				16	3	6,0	
		16	3	6,0				16	3	6,0	
		Totale As =		12,1	>	10,6	8,8	<	Totale As =	12,1	
MOMENTI RESISTENTI		M_{rs}							M_d	K	
	Acciaio	8.931	kgm	Mrs = 0,9 x d x fyd x As				>	7.836	1,1	Camp
		8.931	kgm	Mrs = 0,9 x d x fyd x As				>	6.530	1,4	Bordo
	Calcestruzzo	b		Mrc	=	(d / r)^2 / b					
	Sezione piena	85	cm	10.285	kgm			>	7.836	1,3	
TAGLIO				V_{Rd1}		K	ρ_1	v_{min}	V_{Rd1}		V_{R2}
	Sezione piena	85	cm	10.348	kg	1,95	0,006	0,326	10.348	>	6.091
				V_{sd}			V_{Rd1}		K		
				5.613	kg	<	10.348		1,8		
	Controllo verifiche:		Acciaio:	Verificato							
			Calcestruzzo:	Verificato							
			Taglio:	Verificato							

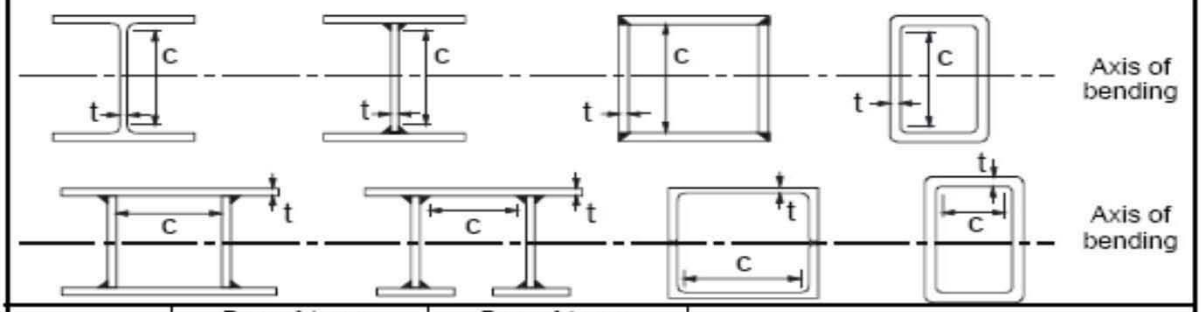
Soletta Scala in c.a. - NTC08											PARCHEGGIO
DATI SEZIONE								Soletta Scala Servizi - Rampa corta			
	H tot [cm] =	20		Larghezza trave [cm] =			30	Lb			
MATERIALI											
	CALCESTRUZZO	**C32/40**				Rck	=	400	kg/cmq		
		f_{ck}	=	0,83	x	400	=	332	kg/cmq		
		f_{cm}	=	332	+	80	=	412	kg/cmq		
		f_{ctm}	=				=	17	kg/cmq		
	(γ_c=1,5 - α_{cc}=0,85)	f_{cd}	=	332	/	1,76	=	188	kg/cmq		
		E_{cm}	=				=	336.428	kg/cmq		
	ACCIAIO	**B450C**									
		f_{yk}	=	4.300	kg/cmq						
	(γ_s=1,15)	f_{yd}	=	4.300	/	1,15	=	3.739	kg/cmq		
ANALISI DEI CARICHI											
	VALORI CARATTERISTCI										
	Calcestruzzo soletta	0,20	x	2.500	=	500	kg/mq	γ_{G1}			
	Permanenti strutt.			**G_{1K}**	=	500	x	1,3	**650**	kg/mq	
	Calcestruzzo gradino	0,08	x	2.500	=	201	kg/mq				
	Grado e sottogrado				=	100	kg/mq				
	Pavimento					60	kg/mq				
	Intonaco				=	30	kg/mq				
	Incidenza parapetto				=	50	kg/mq	γ_{G2}			
	Permanenti non strutt.			**G_{2K}**	=	441	x	1,5	**662**	kg/mq	
								γ_Q			
	Carichi variabili			**G_{2K}**	=	400	x	1,5	**600**	kg/mq	
	VALORI DI CALCOLO	**Gd**	=	**650**	+	**662**	=	**1.312**	kg/mq		
		Qd	=				=	**600**	kg/mq		
					Carico Totale Qt		=	**1.912**	kg/mq		
DATI GEOMETRICI											
	Lunghezza pianerottolo 1	Lc	=	0,95	ml		Alzata	=	0,161	ml	
	Lunghezza rampa	Lc	=	2,40	ml		Pedata	=	0,30	ml	
	Lunghezza pianerottolo 2	Lc	=	1,05	ml		Inclinazione	=	28	°se	
	Luce di calcolo	Lc	=	4,72	ml						
	Larghezza di calcolo	b	=	0,85	ml						
	Copriferro	c	=	3,0	cm						
	Altezza utile della sezione	d	=	17,0	cm						
DATI DI CARICO											
	Carico lineare q:	Qt x b	=	1.625	kg/ml						
CARATTERISTICHE DI SOLLECITAZIONE				Camp	Bordo						
	Coefficiente Km			10	12						
	Md = (q x Lc^2) / Km		=	3.626	3.022	kgm					
	Vsd = (q x (Lc-Lb)) / 2		=		3.595	kg					
VERIFICHE SLV		Campata							Bordo		
	Armatura minima	6,3	cmq		Asmin1 = Md / (0,9 x d x fyd)			5,3	cmq		
		ϕ	n	Area	Asmin2 = 0,3% H x b			ϕ	n	Area	
	Armatura in progetto	16	2	4,0				16	2	4,0	
		16	2	4,0				16	2	4,0	
		Totale As =		8,0	>	6,3	5,3	<	Totale As =	8,0	
MOMENTI RESISTENTI		M_{rs}							M_d	K	
	Acciaio	4.601	kgm	Mrs = 0,9 x d x fyd x As				>	3.626	1,3	Camp
		4.601	kgm	Mrs = 0,9 x d x fyd x As				>	3.022	1,5	Bordo
	Calcestruzzo	b		Mrc	=	(d / r)^2 / b					
	Sezione piena	85	cm	6.141	kgm			>	3.626	1,7	
TAGLIO				V_{Rd1}		K	ρ_1	v_{min}	V_{Rd1}		V_{R2}
	Sezione piena	85	cm	7.793	kg	2,00	0,006	0,337	7.793	>	4.876
				V_{sd}			V_{Rd1}		K		
				3.595	kg	<	7.793		2,2		
	Controllo verifiche:		Acciaio:	Verificato							
		Calcestruzzo:		Verificato							
			Taglio:	Verificato							

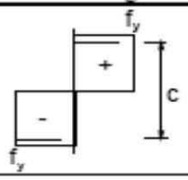
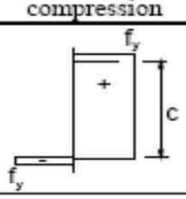
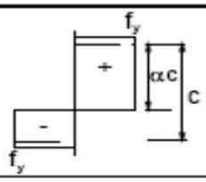
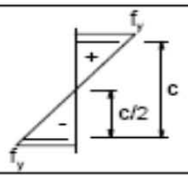
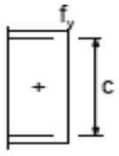
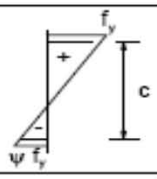
CLASSIFICAZIONE DELLE SEZIONI IN ACCIAIO - NTC08			
PROFILI AD H			
IPE 120			
Altezza della sezione trasversale	h	120,00	[mm]
Larghezza della sezione trasversale	b	64,00	[mm]
Spessore dell'anima	t_w	4,40	[mm]
Spessore delle ali	t_f	6,30	[mm]
Raggio di raccordo	r	7,00	[mm]
Eventuale spessore della saldatura delle ali con l'anima	s	0,00	[mm]
CARATTERISTICHE MECCANICHE			
Altezza tra le ali	h_i	107,40	[mm]
Altezza della porzione saldabile	d	93,40	[mm]
Area della sezione trasversale	A	13,2	[cm²]
Area della sezione resistente al taglio agente lungo z	A_{vz}	6,31	[cm²]
Area della sezione resistente al taglio agente lungo y	A_{vy}	8,06	[cm²]
Momento d'inerzia attorno all'asse forte	I_{yy}	318	[cm⁴]
Momento d'inerzia attorno all'asse debole	I_{zz}	28	[cm⁴]
Raggio d'inerzia attorno all'asse forte	i_{yy}	4,90	[cm]
Raggio d'inerzia attorno all'asse debole	i_{zz}	1,45	[cm]
Modulo di resistenza elastico attorno all'asse forte	$W_{el,yy}$	53,0	[cm³]
Modulo di resistenza elastico attorno all'asse debole	$W_{el,zz}$	8,6	[cm³]
Modulo di resistenza plastico attorno all'asse forte	$W_{pl,yy}$	60,7	[cm³]
Modulo di resistenza plastico attorno all'asse debole	$W_{pl,zz}$	13,6	[cm³]
Momento d'inerzia torsionale	I_t	1,7	[cm⁴]
Costante di warping	I_w	890	[cm⁶]
CLASSIFICAZIONE DELLA SEZIONE			
Valore di snervamento dell'acciaio	f_y	275	[MPa]
Coefficiente ε	ε	0,92	[-]
Classificazione dell'anima			
Altezza dell'anima depurata dei raccordi o delle saldature	c	93,40	[mm]
Spessore dell'anima	t_w	4,40	[mm]
Rapporto tra altezza e spessore	c/t_w	21,23	[-]
Classificazione dell'anima per flessione	**CLASSE 1**		
Classificazione dell'anima per compressione	**CLASSE 1**		
Classificazione delle ali			
Semi larghezza delle ali depurata dei raccordi o delle saldature	c	22,8	[mm]
Spessore delle ali	t_f	6,30	[mm]
Rapporto tra semi larghezza e spessore	c/t_f	3,62	[-]
Classificazione delle ali per flessione	**CLASSE 1**		

CLASSIFICAZIONE DELLE SEZIONI IN ACCIAIO - NTC08			
PROFILI AD H			
IPE 140			
Altezza della sezione trasversale	h	140,00	[mm]
Larghezza della sezione trasversale	b	73,00	[mm]
Spessore dell'anima	t_w	4,70	[mm]
Spessore delle ali	t_f	6,90	[mm]
Raggio di raccordo	r	7,00	[mm]
Eventuale spessore della saldatura delle ali con l'anima	s	0,00	[mm]
CARATTERISTICHE MECCANICHE			
Altezza tra le ali	h_i	126,20	[mm]
Altezza della porzione saldabile	d	112,20	[mm]
Area della sezione trasversale	A	16,4	[cm^2]
Area della sezione resistente al taglio agente lungo z	A_{vz}	7,64	[cm^2]
Area della sezione resistente al taglio agente lungo y	A_{vy}	10,07	[cm^2]
Momento d'inerzia attorno all'asse forte	I_{yy}	541	[cm^4]
Momento d'inerzia attorno all'asse debole	I_{zz}	45	[cm^4]
Raggio d'inerzia attorno all'asse forte	i_{yy}	5,74	[cm]
Raggio d'inerzia attorno all'asse debole	i_{zz}	1,65	[cm]
Modulo di resistenza elastico attorno all'asse forte	$W_{el,yy}$	77,3	[cm^3]
Modulo di resistenza elastico attorno all'asse debole	$W_{el,zz}$	12,3	[cm^3]
Modulo di resistenza plastico attorno all'asse forte	$W_{pl,yy}$	88,3	[cm^3]
Modulo di resistenza plastico attorno all'asse debole	$W_{pl,zz}$	19,2	[cm^3]
Momento d'inerzia torsionale	I_t	2,4	[cm^4]
Costante di warping	I_w	1981	[cm^6]
CLASSIFICAZIONE DELLA SEZIONE			
Valore di snervamento dell'acciaio	f_y	275	[MPa]
Coefficiente ε	ε	0,92	[-]
Classificazione dell'anima			
Altezza dell'anima depurata dei raccordi o delle saldature	c	112,20	[mm]
Spessore dell'anima	t_w	4,70	[mm]
Rapporto tra altezza e spessore	c/t_w	23,87	[-]
Classificazione dell'anima per flessione	**CLASSE 1**		
Classificazione dell'anima per compressione	**CLASSE 1**		
Classificazione delle ali			
Semi larghezza delle ali depurata dei raccordi o delle saldature	c	27,15	[mm]
Spessore delle ali	t_f	6,90	[mm]
Rapporto tra semi larghezza e spessore	c/t_f	3,93	[-]
Classificazione delle ali per flessione	**CLASSE 1**		

Table 5.2 (sheet 1 of 3): Maximum width-to-thickness ratios for compression parts

Internal compression parts



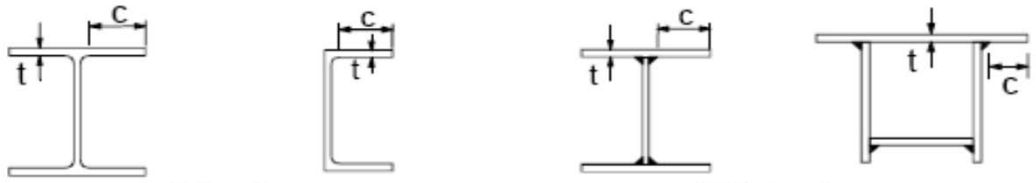
Class	Part subject to bending	Part subject to compression	Part subject to bending and compression
Stress distribution in parts (compression positive)			
1	$c/t \le 72\varepsilon$	$c/t \le 33\varepsilon$	when $\alpha > 0{,}5$: $c/t \le \frac{396\varepsilon}{13\alpha - 1}$ when $\alpha \le 0{,}5$: $c/t \le \frac{36\varepsilon}{\alpha}$
2	$c/t \le 83\varepsilon$	$c/t \le 38\varepsilon$	when $\alpha > 0{,}5$: $c/t \le \frac{456\varepsilon}{13\alpha - 1}$ when $\alpha \le 0{,}5$: $c/t \le \frac{41{,}5\varepsilon}{\alpha}$
Stress distribution in parts (compression positive)			
3	$c/t \le 124\varepsilon$	$c/t \le 42\varepsilon$	when $\psi > -1$: $c/t \le \frac{42\varepsilon}{0{,}67 + 0{,}33\psi}$ when $\psi \le -1$ *): $c/t \le 62\varepsilon(1-\psi)\sqrt{(-\psi)}$

$\varepsilon = \sqrt{235/f_y}$	f_y	235	275	355	420	460
	ε	1,00	0,92	0,81	0,75	0,71

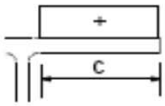
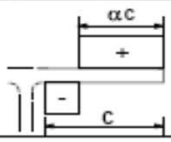
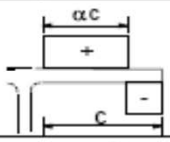
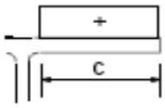
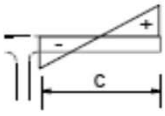
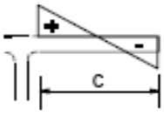
*) $\psi \le -1$ applies where either the compression stress $\sigma \le f_y$ or the tensile strain $\varepsilon_y > f_y/E$

Table 5.2 (sheet 2 of 3): Maximum width-to-thickness ratios for compression parts

Outstand flanges



Rolled sections — Welded sections

Class	Part subject to compression	Part subject to bending and compression	
		Tip in compression	Tip in tension
Stress distribution in parts (compression positive)			
1	$c/t \le 9\varepsilon$	$c/t \le \frac{9\varepsilon}{\alpha}$	$c/t \le \frac{9\varepsilon}{\alpha\sqrt{\alpha}}$
2	$c/t \le 10\varepsilon$	$c/t \le \frac{10\varepsilon}{\alpha}$	$c/t \le \frac{10\varepsilon}{\alpha\sqrt{\alpha}}$
Stress distribution in parts (compression positive)			
3	$c/t \le 14\varepsilon$	$c/t \le 21\varepsilon\sqrt{k_\sigma}$ For k_σ see EN 1993-1-5	

$\varepsilon = \sqrt{235/f_y}$	f_y	235	275	355	420	460
	ε	1,00	0,92	0,81	0,75	0,71

TRAVE IN ACCIAIO - NTC08										
TRAVE Ln =	**2,75**	**ml**								
MATERIALI										
ACCIAIO			S275	(Tab. 11.3.IX)						
Modulo di elasticità	E	=	2.100.000	kg/cmq						
Tensione snerv . car.	f_{yk}	=	2.750	kg/cmq						
Tensione rottura car.	f_{tk}	=	4.300	kg/cmq						
Peso specifico	ρ_k	=	7.850	kg/mc						
Classificazione della sezione			**Classe 1**							
Coeff. di sicurezza	γ_{M0}	=	1,05							
ANALISI DEI CARICHI										
Peso proprio trav e				=	11	kg/mq				
Orsogrill				=	20	kg/mq	γ_{G1}		G_1	
	Permanenti strutturali:			G_{1k}	**31**	**x**	**1,30**	**=**	**40**	**kg/mq**
						kg/mq	γ_{G2}		G_2	
	Permanenti non strutturali:			G_{2k}	**0**	**x**	**1,50**	**=**	**0**	**kg/mq**
							γ_Q		Q_1	
			Variabili:	Q_{1k}	**500**	**x**	**1,50**	**=**	**750**	**kg/mq**
DATI GEOMETRICI										
Luce netta in pianta	Ln	=	2,75	ml						
Inclinazione	α	=	0	°s						
Luce di calcolo	Lc	=	**2,89**	ml						
Interasse	Int	=	**1,20**	ml						
PROFILATO	IPE140									
Area sezione	A	=	16,4	cm^2						
Area di taglio	Av	=	6,6	cm^2						
Modulo di resistenza	W	=	77,3	cm^3						
Modulo di resistenza plastico	Wpl	=	88,3	cm^3						
Momento di inerzia	J	=	541	cm^4						
DATI DI CARICO										
SLU - Carico lineare q:	Q_{SLU} x Int	=	948	kg/ml		$(G_1 + G_2 + Q_1)$ x Int				
SLE - Carico lineare q:	Q_{SLE} x Int	=	637	kg/ml		$(G_{1k} + G_{2k} + Q_{1k})$ x Int				
CARATTERISTICHE DI SOLLECITAZIONE										
SLU - $M_{ED} = (q \times Lc^2) / 12$		=	659	kgm						
SLU - $V_{ED} = (q \times Lc) / 2$		=	1.369	kg						
VERIFICHE SLU - SECONDO PUNTO 4.2.4.1.2 NTC 2008										
FLESSIONE										
Momento Resisstente	$M_{C,Rd}$	=	2.313	kgm	$M_{C,Rd} = M_{Pl,Rd} = (W_{pl.} \times f_{yk}) / \gamma_{M0}$					
$M_{ED} / M_{C,Rd} \leq 1$		=	**0,28**	<	1	**Verificato**				
TAGLIO										
Taglio Resistente	$V_{C,Rd}$	=	9.950	kg	$V_{C,Rd} = (A_v \times f_{yk}) / (\sqrt{3} \times \gamma_{M0})$					
$V_{ED} / V_{C,Rd} \leq 1$		=	**0,14**	<	1	**Verificato**				
VERIFICHE SLE										
DEFORMAZIONE										
Freccia massima = Lc /	250	=	1,16	cm	Carichi permanenti e v ariabili SLE Freq.					
Freccia massima = Lc /	350	=	0,83	cm	Carichi v ariabili SLE Rare					
Freccia (Appoggio)			Perm.		Var.		Totale			
$U = 5/384 \times q \times Lc^4 / (E \times J)$		=	0,03	+	0,33	=	0,36	cm		
Carichi Perm. + Var.	U / Lc	=	9.829		863		**793**	**>**	**250**	
Carichi Var.	U / Lc	=			0,48	=	0,48	cm		
							604	**>**	**350**	

TRAVE IN ACCIAIO - NTC08										
TRAVE Ln =	**3,35**	**ml**								
MATERIALI										
ACCIAIO			S275	(Tab. 11.3.IX)						
Modulo di elasticità	E	=	2.100.000	kg/cmq						
Tensione snerv . car.	f_{yk}	=	2.750	kg/cmq						
Tensione rottura car.	f_{tk}	=	4.300	kg/cmq						
Peso specifico	ρ_k	=	7.850	kg/mc						
Classificazione della sezione			**Classe 1**							
Coeff. di sicurezza	γ_{M0}	=	1,05							
ANALISI DEI CARICHI										
Peso proprio trav e				=	13	kg/mq				
Orsogrill				=	20	kg/mq	γ_{G1}		G_1	
	Permanenti strutturali:			G_{1k}	**33**	**x**	**1,30**	**=**	**43**	**kg/mq**
						kg/mq	γ_{G2}		G_2	
	Permanenti non strutturali:			G_{2k}	**0**	**x**	**1,50**	**=**	**0**	**kg/mq**
							γ_Q		Q_1	
			Variabili:	Q_{1k}	**500**	**x**	**1,50**	**=**	**750**	**kg/mq**
DATI GEOMETRICI										
Luce netta in pianta	Ln	=	3,35	ml						
Inclinazione	α	=	0	°s						
Luce di calcolo	Lc	=	**3,52**	ml						
Interasse	Int	=	**1,00**	ml						
PROFILATO	IPE140									
Area sezione	A	=	16,4	cm^2						
Area di taglio	Av	=	6,6	cm^2						
Modulo di resistenza	W	=	77,3	cm^3						
Modulo di resistenza plastico	Wpl	=	88,3	cm^3						
Momento di inerzia	J	=	541	cm^4						
DATI DI CARICO										
SLU - Carico lineare q:	Q_{SLU} x Int	=	793	kg/ml		$(G_1 + G_2 + Q_1)$ x Int				
SLE - Carico lineare q:	Q_{SLE} x Int	=	533	kg/ml		$(G_{1k} + G_{2k} + Q_{1k})$ x Int				
CARATTERISTICHE DI SOLLECITAZIONE										
SLU - $M_{ED} = (q \times Lc^2) / 12$		=	817	kgm						
SLU - $V_{ED} = (q \times Lc) / 2$		=	1.394	kg						
VERIFICHE SLU - SECONDO PUNTO 4.2.4.1.2 NTC 2008										
FLESSIONE										
Momento Resisstente	$M_{C,Rd}$	=	2.313	kgm	$M_{C,Rd} = M_{Pl,Rd} = (W_{pl.} \times f_{yk}) / \gamma_{M0}$					
$M_{ED} / M_{C,Rd} \leq 1$		=	**0,35**	<	1	**Verificato**				
TAGLIO										
Taglio Resistente	$V_{C,Rd}$	=	9.950	kg	$V_{C,Rd} = (A_v \times f_{yk}) / (\sqrt{3} \times \gamma_{M0})$					
$V_{ED} / V_{C,Rd} \leq 1$		=	**0,14**	<	1	**Verificato**				
VERIFICHE SLE										
DEFORMAZIONE										
Freccia massima = Lc /	250	=	1,41	cm	Carichi permanenti e v ariabili SLE Freq.					
Freccia massima = Lc /	350	=	1,01	cm	Carichi v ariabili SLE Rare					
Freccia (Appoggio)			Perm.		Var.		Totale			
$U = 5/384 \times q \times Lc^4 / (E \times J)$		=	0,06	+	0,61	=	0,67	cm		
Carichi Perm. + Var.	U / Lc	=	6.098		573		**524**	**>**	**250**	
Carichi Var.	U / Lc	=			0,88	=	0,88	cm		
							401	**>**	**350**	

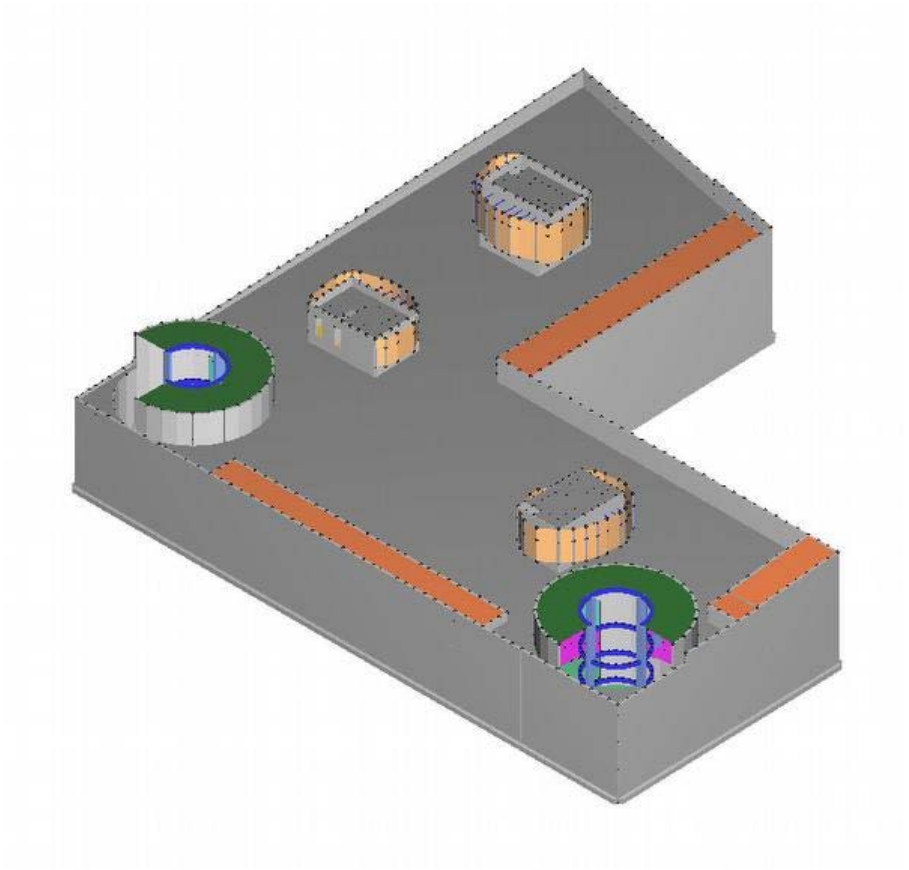
SBALZO IN ACCIAIO - NTC08										
SBALZO Lc =	**2,20**	**ml**								
MATERIALI										
ACCIAIO			S275	(Tab. 11.3.IX)						
Modulo di elasticità	E	=	2.100.000	kg/cmq						
Tensione snerv . car.	f_{yk}	=	2.750	kg/cmq						
Tensione rottura car.	f_{tk}	=	4.300	kg/cmq						
Peso specifico	ρ_k	=	7.850	kg/mc						
Coeff. di sicurezza	γ_{M0}	=	1,05							
ANALISI DEI CARICHI										
Peso proprio				=	15	kg				
	Permanenti strutturali:			**G_{1k}**	**15**	**x**	**1,30**	**=**	**20**	**kg/m**
	Permanenti non strutturali:			**G_{2k}**	**61**	**x**	**1,50**	**=**	**92**	**kg/m**
							γ_Q		**Q_1**	**kg/m**
			Variabili:	**Q_{1k}**	**50**	**x**	**1,50**	**=**	**75**	**kg/m**
DATI GEOMETRICI										
Luce di calcolo	Lc	=	2,20	ml						
Interasse	Int	=	1,50	ml						
PROFILATO	IPE120									
Area sezione	A	=	13,2	cm^2						
Area di taglio	Av	=	6,3	cm^2						
Modulo di resistenza	W	=	53,0	cm^3						
Modulo di resistenza plasti	Wpl	=	60,8	cm^3						
Momento di inerzia	J	=	318	cm^4						
DATI DI CARICO										
SLU - in punta N:	Q_{SLU} x Int	=	280	kg/ml		$(G_1 + G_2 + Q_1)$ x Int				
SLE - in punta N:	Q_{SLE} x Int	=	190	kg/ml		$(G_{1k} + G_{2k} + Q_{1k})$ x Int				
CARATTERISTICHE DI SOLLECITAZIONE										
SLU - M_{ED} = 1,4 x N x Lc		=	862	kgm						
SLU - V_{ED} = 1,4 x N		=	392	kg						
VERIFICHE SLU - SECONDO PUNTO 4.2.4.1.2 NTC 2008										
FLESSIONE										
Momento Resisstente	$M_{C,Rd}$	=	1.592	kgm	$M_{C,Rd} = M_{Pl,Rd} = (W_{pl} \times f_{yk}) / \gamma_{M0}$					
$M_{ED} / M_{C,Rd} \leq 1$		=	**0,54**	<	1	**Verificato**				
TAGLIO										
Taglio Resistente	$V_{C,Rd}$	=	9.541	kg	$V_{C,Rd} = (A_v \times f_{yk}) / (\sqrt{3} \times \gamma_{M0})$					
$V_{ED} / V_{C,Rd} \leq 1$		=	**0,04**	<	1	**Verificato**				
VERIFICHE SLE										
DEFORMAZIONE										
Freccia massima = Lc /	200	=	3,16	cm	Carichi permanenti e v ariabili SLE Freq.					
Freccia massima = Lc /	300	=	2,10	cm	Carichi v ariabili SLE Rare					
Freccia			Perm.		Var.		Totale			
$U = 1/3 \times N \times Lc^3 / (E \times J)$		=	0,61	+	0,28	=	0,89	cm		
Carichi Perm. + Var.	U / Lc	=	361		788		**248**	**>**	**200**	
Carichi Var.	U / Lc	=			0,40	=	0,40	cm		
							552	**>**	**300**	

SBALZO IN ACCIAIO - NTC08										
SBALZO Lc =	**3,00**	**ml**								
MATERIALI										
ACCIAIO			S275	(Tab. 11.3.IX)						
Modulo di elasticità	E	=	2.100.000	kg/cmq						
Tensione snerv . car.	f_{yk}	=	2.750	kg/cmq						
Tensione rottura car.	f_{tk}	=	4.300	kg/cmq						
Peso specifico	ρ_k	=	7.850	kg/mc						
Coeff. di sicurezza	γ_{M0}	=	1,05							
ANALISI DEI CARICHI										
Peso proprio				=	26	kg				
	Permanenti strutturali:			**G_{1k}**	**26**	**x**	**1,30**	**=**	**33**	**kg/m**
	Permanenti non strutturali:			**G_{2k}**	**61**	**x**	**1,50**	**=**	**92**	**kg/m**
							γ_Q		**Q_1**	**kg/m**
			Variabili:	**Q_{1k}**	**50**	**x**	**1,50**	**=**	**75**	**kg/m**
DATI GEOMETRICI										
Luce di calcolo	Lc	=	3,00	ml						
Interasse	Int	=	1,50	ml						
PROFILATO	IPE140									
Area sezione	A	=	16,4	cm^2						
Area di taglio	Av	=	6,6	cm^2						
Modulo di resistenza	W	=	77,3	cm^3						
Modulo di resistenza plasti	Wpl	=	88,3	cm^3						
Momento di inerzia	J	=	541	cm^4						
DATI DI CARICO										
SLU - in punta N:	Q_{SLU} x Int	=	300	kg/ml		$(G_1 + G_2 + Q_1)$ x Int				
SLE - in punta N:	Q_{SLE} x Int	=	205	kg/ml		$(G_{1k} + G_{2k} + Q_{1k})$ x Int				
CARATTERISTICHE DI SOLLECITAZIONE										
SLU - M_{ED} = 1,4 x N x Lc		=	1.262	kgm						
SLU - V_{ED} = 1,4 x N		=	421	kg						
VERIFICHE SLU - SECONDO PUNTO 4.2.4.1.2 NTC 2008										
FLESSIONE										
Momento Resisstente	$M_{C,Rd}$	=	2.313	kgm	$M_{C,Rd} = M_{Pl,Rd} = (W_{pl.} X f_{yk}) / \gamma_{M0}$					
$M_{ED} / M_{C,Rd} \leq 1$		=	**0,55**	<	1	**Verificato**				
TAGLIO										
Taglio Resistente	$V_{C,Rd}$	=	9.950	kg	$V_{C,Rd} = (A_v X f_{yk}) / (\sqrt{3} x \gamma_{M0})$					
$V_{ED} / V_{C,Rd} \leq 1$		=	**0,04**	<	1	**Verificato**				
VERIFICHE SLE										
DEFORMAZIONE										
Freccia massima = Lc /	200	=	3,29	cm	Carichi permanenti e v ariabili SLE Freq.					
Freccia massima = Lc /	300	=	2,19	cm	Carichi v ariabili SLE Rare					
Freccia			Perm.		Var.		Totale			
$U = 1/3 x N x Lc^3 / (E x J)$		=	1,03	+	0,42	=	1,45	cm		
Carichi Perm. + Var.	U / Lc	=	290		721		**207**	**>**	**200**	
Carichi Var.	U / Lc	=			0,59	=	0,59	cm		
							505	**>**	**300**	

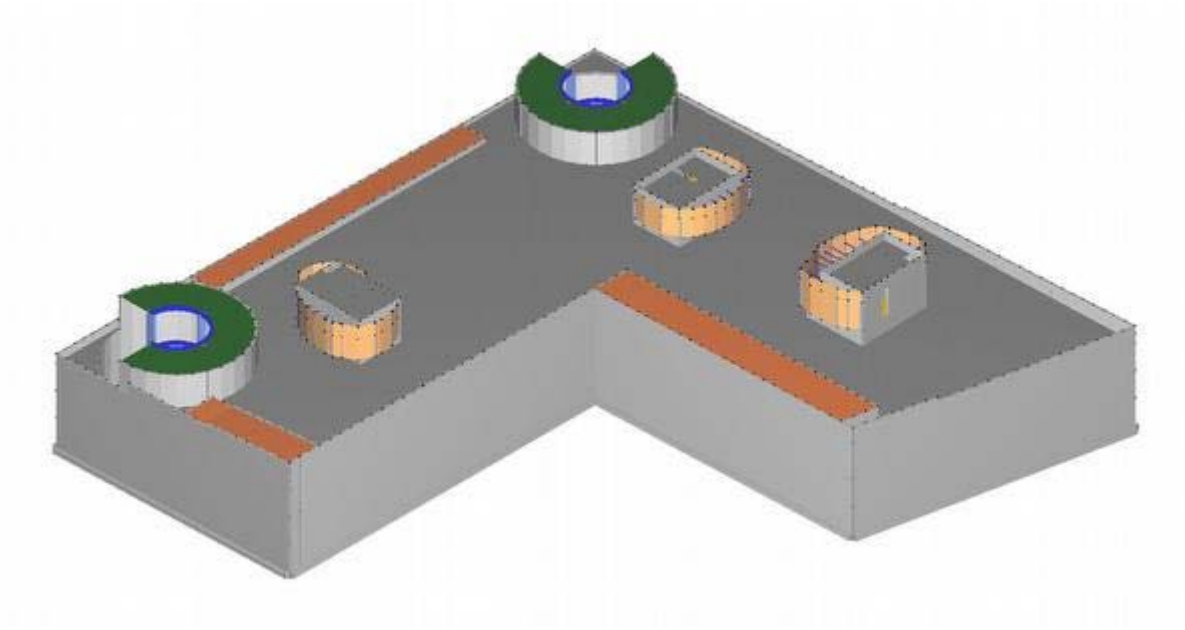
Tabulato di calcolo

Dati relativi ai nodi della struttura

Convenzioni adottate
La terna di riferimento generale è destrorsa.
I nodi vengono numerati, con riferimento a una sezione orizzontale, da sinistra a destra, dal basso verso l'alto e per quote crescenti.
L'impalcato di appartenenza di un nodo è definito, in generale, dalla prima delle tre cifre che ne definiscono il numero, possono tuttavia presentarsi casi in cui si hanno più di 100 nodi per solaio nel qual caso il solaio di appartenenza è specificato dall'ultimo valore stampato nella riga dei dati relativi al nodo.
La maschera dei vincoli è costituita dai valori 0 e 1. Il valore 1 indica che per il nodo in riferimento il grado di libertà correlativo è soppresso mentre il valore 0 indica che è libero.
Nel caso di edifici civili multipiano l'asse *z* generale coincide con l'asse verticale rivolto verso l'alto.



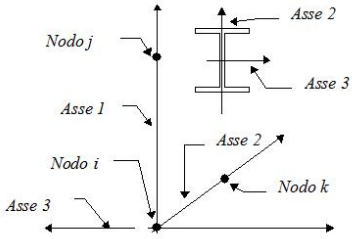
Mesh solida della struttura – Vista 1



Mesh solida della struttura – Vista 2

Elementi tipo pilastro

Convenzioni adottate
Ogni elemento tipo pilastro viene identificato da:
Il nodo iniziale **i**;
Il nodo finale **j**;
Il nodo **k** che definisce l'orientamento nello spazio della terna riferimento locale dell'elemento.
La terna di riferimento locale del pilastro risulta quindi essere cosi disposta:



Sistema di riferimento locale
Vengono riportati i valori di efficacia dei vincoli flessionali alle estremità dell'elemento (variabili fra lo **0%** e il **100%**), nei due piani **1-2** e **1-3** del pilastro in corrispondenza dei nodi, dando quindi la possibilità di considerare aste non perfettamente incastrate alle estremità (coefficienti **Vi12 - Vj12 - Vi13 - Vj13**).
In generale, se non diversamente disposto, l'asse 2 coincide, per i pilastri, con l'asse **y** globale e pertanto la disposizione della sezione coincide con quella che si avrebbe in una vista in pianta.

Caratteristiche dei Materiali:

Tipo	Modulo Elastico [kg/cm^2]	ν	alfa [1/°C]	Peso Specifico [kg/m^3]	Commento
1	314760.000	0.120	0.000012	2500.0	C25/30
2	336428.000	0.120	0.000012	2500.0	C32/40
3	2100000.000	0.330	0.000010	7850.0	S275JR

Sezioni Impiegate:

Sezione	Materiale	Tipo di Sezione	Parametri Dimensionali Commenti
1	2	Rett.	B= 40 H= 100 [cm]
2	2	Rett.	B= 100 H= 40 [cm]
3	2	Rett.	B= 30 H= 100 [cm]
4	2	Rett.	B= 30 H= 40 [cm]

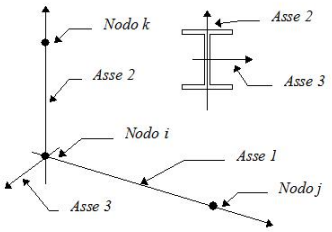
Sezione	Materiale	Tipo di Sezione	Parametri Dimensionali Commenti
5	2	Rett.	B= 30 H= 30 [cm]
6	2	Rett.	B= 40 H= 30 [cm]
7	3	IPE 120	Montante

Caratteristiche Inerziali:

Sezione	Materiale	Area [cm^2]	Jt [cm^4]	J2 [cm^4]	J3 [cm^4]	J23 [cm^4]	Xx	Xy
1	2	4000.00	1661314	3333333	533333	0	1.2	1.2
2	2	4000.00	1661314	533333	3333333	0	1.2	1.2
3	2	3000.00	789387	2500000	225000	0	1.2	1.2
4	2	1200.00	186385	160000	90000	0	1.2	1.2
5	2	900.00	113866	67500	67500	0	1.2	1.2
6	2	1200.00	186385	90000	160000	0	1.2	1.2
7	3	13.23	2	318	28	0	2.5	1.6

Elementi tipo trave

Convenzioni adottate
Ogni elemento tipo trave viene identificato da:
Il nodo iniziale **i**;
Il nodo finale **j**;
Il nodo **k** che definisce l'orientamento nello spazio della terna riferimento locale dell'elemento.
La terna di riferimento locale della trave risulta essere così disposta:



Vengono riportati i valori di efficacia dei vincoli alle estremità dello elemento (variabili fra 0 e 100%), nei due piani **1-2** e **1-3** della trave in corrispondenza dei nodi, dando quindi la possibilità di considerare aste non perfettamente incastrate (coefficienti **Vi12, Vj12, Vi13, Vj13**).

Caratteristiche dei Materiali:

Tipo	Modulo Elastico [kg/cm^2]	ν	alfa [1/°C]	Peso Specifico [kg/m^3]	Commento
1	314760.000	0.120	0.000012	2500.0	C25/30
2	336428.000	0.120	0.000012	2500.0	C32/40
3	2100000.000	0.330	0.000010	7850.0	S275JR

Sezioni Impiegate:

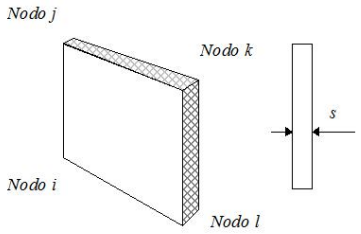
Sezione	Materiale	Tipo di Sezione	Parametri Dimensionali Commenti
1	2	Rett.	B= 40 H= 40 [cm]
2	2	Rett.	B= 40 H= 40 [cm]
3	2	Rett.	B= 30 H= 60 [cm]
4	2	Rett.	B= 40 H= 60 [cm]
5	2	Rett.	B= 40 H= 50 [cm]
6	2	Rett.	B= 30 H= 40 [cm]
7	2	Rett.	B= 30 H= 80 [cm]
8	3	IPE 120	
9	3	IPE 140	

Caratteristiche Inerziali:

Sezione	Materiale	Area [cm²]	Jt [cm^4]	J2 [cm^4]	J3 [cm^4]	J23 [cm^4]	Xx	Xy
1	2	1600.00	359874	213333	213333	0	1.2	1.2
2	2	1600.00	359874	213333	213333	0	1.2	1.2
3	2	1800.00	370716	540000	135000	0	1.2	1.2
4	2	2400.00	722134	720000	320000	0	1.2	1.2
5	2	2000.00	526803	416667	266667	0	1.2	1.2
6	2	1200.00	186385	160000	90000	0	1.2	1.2
7	2	2400.00	578360	1280000	180000	-0	1.2	1.2
8	3	13.23	2	318	28	0	2.5	1.6
9	3	16.44	2.45	542	45	0	2.5	1.6

Elementi setto

Convenzioni adottate
L'elemento setto viene identificato mediante i quattro nodi (**i, j, k, l**) di bordo.



Numerazione dei nodi cui fa capo l'elemento

Caratteristiche dei Materiali:

Tipo	Modulo Elastico [kg/cm²]	ν	alfa [1/°C]	Peso Specifico [kg/m³]	Commento
1	314760.000	0.120	0.000012	2500.0	C25/30
2	336428.000	0.120	0.000012	2500.0	C32/40
3	2100000.000	0.330	0.000010	7850.0	S275JR

Caratteristiche dei Terreni di Fondazione:

Tipo	Costante di Sottofondo [kg/cm³]	Commento
1	4.0	Lave

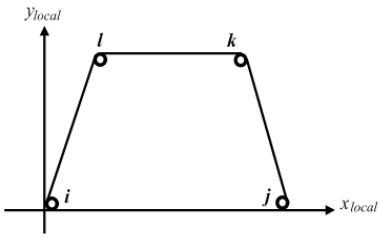
Sezioni Impiegate:

Sezione	Materiale	Tipo di Sezione	Parametri Dimensionali Commenti
1	2	Muro fondazione	B= 120 H= 60 s= 30 [cm] Terreno numero 1 Lave
2	2	Muro	s= 30 [cm]
3	2	Muro	s= 30 [cm]
4	2	Muro	s= 30 [cm] Cordolo
5	2	Muro	s= 30 [cm] Corpo scala
6	2	Muro	s= 30 [cm] Riserva idrica
7	2	Muro	s= 30 [cm]
8	2	Muro	s= 40 [cm] Riserva Idrica 2
9	2	Muro	s= 40 [cm] Locale Tecnico
10	2	Muro	s= 30 [cm] Locale Tecnico
11	2	Muro	s= 15 [cm] Locale Tecnico

Elementi a 4 nodi

Convenzioni adottate
L'elemento a 4 nodi è individuato tramite il numero dei quattro nodi di vertice dello stesso.

Gli assi del sistema di riferimento locale risultano così disposti:



L'asse $\mathbf{x}_{locale}$ ha direzione parallela alla retta congiungente i nodi **i** e **j**, è passante per i medesimi nodi ed ha verso positivo da **i** a **j**.
L'asse $\mathbf{y}_{locale}$ è ortogonale all'asse $\mathbf{x}_{locale}$, passa per il nodo **i** ed ha verso positivo dalla parte del nodo **l**.
L'asse $\mathbf{z}_{locale}$ è ottenuto per prodotto vettoriale fra $\mathbf{x}_{locale}$ e $\mathbf{y}_{locale}$.

Caratteristiche dei Materiali:

Tipo	Modulo Elastico [kg/cm²]	ν	alfa [1/°C]	Peso Specifico [kg/m³]	Commento
1	314760.000	0.120	0.000012	2500.0	C25/30
2	336428.000	0.120	0.000012	2500.0	C32/40
3	2100000.000	0.330	0.000010	7850.0	S275JR

Caratteristiche dei Terreni di Fondazione:

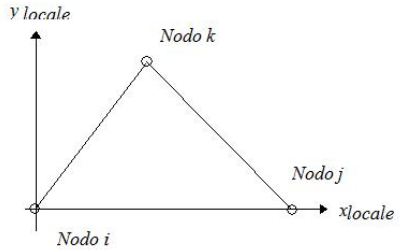
Tipo	Costante di Sottofondo [kg/cm³]	Commento
1	4.0	Lave

Sezioni Impiegate:

Sezione	Materiale	Tipo di Sezione	Parametri Dimensionali Commenti
1	1	Mesh platea	s= 60 [cm] Terreno numero 1 Lave
2	2	Mesh isotropa	s= 25 [cm] Livello -2
3	2	Mesh isotropa	s= 25 [cm] Livello -1
4	2	Mesh isotropa	s= 50 [cm] Livello Copertura
5	2	Mesh isotropa	s= 20 [cm] Livello Copertura Loc Tec
6	2	Mesh isotropa	s= 20 [cm] Livello Copertura Rampe
7	2	Mesh isotropa	s= 25 [cm] Copertura Inclinata
8	2	Mesh isotropa	s= 30 [cm] Riserva Idrica
9	2	Mesh isotropa	s= 25 [cm] Livello -2 - Corpi Scala
10	2	Mesh isotropa	s= 25 [cm] Livello -1 - Corpi Scala
11	2	Mesh isotropa	s= 20 [cm] Livello Copertura - Corpi Scala
12	2	Mesh isotropa	s= 30 [cm]
13	1	Mesh platea	s= 30 [cm] Terreno numero 1 Lave
14	2	Mesh isotropa	s= 25 [cm]

Elementi triangolari

Convenzioni adottate
L'elemento trinangolare è individuato tramite il numero dei nodi di vertice dello stesso.
Gli assi del sistema di riferimento locale risultano così disposti:



L'asse $\mathbf{x}_{locale}$ ha direzione parallela alla retta congiungente i nodi **i** e **j**, è passante per i medesimi nodi ed ha verso positivo da **i** a **j**.
L'asse $\mathbf{y}_{locale}$ è ortogonale all'asse $\mathbf{x}_{locale}$, passa per il nodo **i** ed ha verso positivo dalla parte del nodo **k**.
L'asse $\mathbf{z}_{locale}$ è ottenuto per prodotto vettoriale fra $\mathbf{x}_{locale}$ e $\mathbf{y}_{locale}$.

Caratteristiche dei Materiali:

Tipo	Modulo Elastico [kg/cm²]	ν	alfa [1/°C]	Peso Specifico [kg/m³]	Commento
1	314760.000	0.120	0.000012	2500.0	C25/30
2	336428.000	0.120	0.000012	2500.0	C32/40
3	2100000.000	0.330	0.000010	7850.0	S275JR

Caratteristiche dei Terreni di Fondazione:

Tipo	Costante di Sottofondo [kg/cm³]	Commento
1	4.0	Lave

Sezioni Impiegate:

Sezione	Materiale	Tipo di Sezione	Parametri Dimensionali Commenti
1	1	Mesh platea	s= 60 [cm] Terreno numero 1 Lave
2	2	Mesh isotropa	s= 25 [cm] Livello -2
3	2	Mesh isotropa	s= 25 [cm] Livello -1
4	2	Mesh isotropa	s= 50 [cm] Livello Copertura
5	2	Mesh isotropa	s= 20 [cm] Livello Copertura Loc Tec
6	2	Mesh isotropa	s= 20 [cm] Livello Copertura Rampe
7	2	Mesh isotropa	s= 25 [cm] Copertura Inclinata
8	2	Mesh isotropa	s= 30 [cm] Riserva Idrica
9	2	Mesh isotropa	s= 25 [cm] Livello -2 - Corpi Scala
10	2	Mesh isotropa	s= 25 [cm] Livello -1 - Corpi Scala
11	2	Mesh isotropa	s= 20 [cm] Livello Copertura - Corpi Scala
12	2	Mesh isotropa	s= 30 [cm]
13	1	Mesh platea	s= 30 [cm] Terreno numero 1 Lave
14	2	Mesh isotropa	s= 25 [cm]

Condizioni e combinazioni di carico

Convenzioni adottate
Nel seguito vengono riportate il numero di condizioni di carico statiche e dinamiche che sollecitano la struttura. Si noti che:
Per quanto riguarda le condizioni di carico dinamiche, il programma assimila ogni direzione di ingresso del sisma, definita dal progettista, ad una condizione di carico. Pertanto qualora agiscano sulla struttura *n* condizioni di carico statiche e il progettista abbia supposto che la struttura venga sollecitata da un sisma entrante in *m* direzioni, la struttura stessa viene considerata del programma come soggetta ad *n* + *m* condizioni di carico.
Le combinazioni di carico, definite dal progettista, combinano fra loro le *n* + *m* condizioni di carico ognuna partecipante alla combinazione *i-esima* secondo i fattori di partecipazione nel seguito riportati. N.B.: se la condizione *j-esima* ha fattore di partecipazione unitario, allora partecipa per intero alla combinazione *i-esima*.
Le prime *n* condizioni sono sempre statiche mentre sono di origine dinamica le (eventuali) condizioni da *n+1* a *n+m*.

Condizioni di carico definite:

Condizione	
1	Permanente strutturale
2	Permanente non strutturale
3	Variabile Parcheggi
4	Variabile amb. susc. di affollamento
5	Variabile Copertura non praticabile
6	Spinta delle terre in X+
7	Spinta delle terre in X-
8	Spinta delle terre in Y+
9	Spinta delle terre in Y-
10	Peso + Spinta dell'acqua
11	Spinta dovuta al sovraccarico in X+
12	Spinta dovuta al sovraccarico in X-
13	Spinta dovuta al sovraccarico in Y+
14	Spinta dovuta al sovraccarico in Y-

Condizione	
15	Incremento sismico della spinta in X+
16	Incremento sismico della spinta in X-
17	Incremento sismico della spinta in Y+
18	Incremento sismico della spinta in Y-
19	Mezzi d'opera

Combinazioni agli Stati Limite Ultimi

Combinazione di carico numero	
1	STR 1
2	STR 2
3	STR 3
4	GEO 1
5	GEO 2
6	GEO 3
7	SLV_ SISMA X+ / 30% Y+
8	SLV_ SISMA X+ / 30% Y-
9	SLV_ SISMA X- / 30% Y+
10	SLV_ SISMA X- / 30% Y-
11	SLV_ SISMA Y+ / 30% X+
12	SLV_ SISMA Y+ / 30% X-
13	SLV_ SISMA Y- / 30% X+
14	SLV_ SISMA Y- / 30% X-

Comb.\Cond	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
1	1.3	1.5	1.5	1.5	0.75	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5					
2	1.3	1.5	1.05	1.05	1.5	1.5	1.5	1.5	1.5	1.5	1.05	1.05	1.05	1.05					
3	1.3	1.5	1.5			1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5					1.5
4	1	1.3	1.3	1.3	0.65	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3					
5	1	1.3	0.91	0.91	1.3	1.3	1.3	1.3	1.3	1.3	0.91	0.91	0.91	0.91					
6	1	1.3	1.3			1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3	1.3					1.3
7	1	1	0.6	0.6		1		0.3		1.2	0.6		0.18		1		0.3		
8	1	1	0.6	0.6		1			0.3	1.2	0.6			0.18	1			0.3	
9	1	1	0.6	0.6			1	0.3		1.2		0.6	0.18			1	0.3		
10	1	1	0.6	0.6			1		0.3	1.2		0.6		0.18		1		0.3	
11	1	1	0.6	0.6		0.3		1		1.2	0.18		0.6		0.3		1		
12	1	1	0.6	0.6			0.3	1		1.2		0.18	0.6			0.3	1		
13	1	1	0.6	0.6		0.3			1	1.2	0.18			0.6	0.3			1	
14	1	1	0.6	0.6			0.3		1	1.2		0.18		0.6		0.3		1	

Combinazioni RARE Stati Limite di Esercizio

Combinazione di carico numero	
15	Rare 1
16	Rare 2
17	Rare 3

Comb.\Cond	1	2	3	4	5	6	7	8	9	10	11	12	13	14	19
15	1	1	1	1	0.5	1	1	1	1	1	1	1	1	1	
16	1	1	0.7	0.7	1	1	1	1	1	1	0.7	0.7	0.7	0.7	
17	1	1	1			1	1	1	1	1	1	1	1	1	1

Combinazioni FREQUENTI Stati Limite di Esercizio

Combinazione di carico numero	
18	Freq. 1
19	Freq. 2
20	Freq. 3

Comb.\Cond	1	2	3	4	5	6	7	8	9	10	11	12	13	14	19
18	1	1	0.7	0.7		1	1	1	1	1	0.7	0.7	0.7	0.7	
19	1	1	0.6	0.6	0.2	1	1	1	1	1	0.6	0.6	0.6	0.6	
20	1	1	0.7			1	1	1	1	1	0.7	0.7	0.7	0.7	1

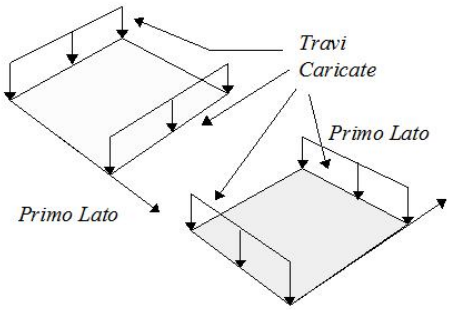
Combinazioni QUASI PERMANENTI Stati Limite di Esercizio

Combinazione di carico numero	
21	Quasi Perm. 1
22	Quasi Perm. 2

Comb.\Cond	1	2	3	4	6	7	8	9	10	11	12	13	14	19
21	1	1	0.6	0.6	1	1	1	1	1	0.6	0.6	0.6	0.6	
22	1	1	0.6		1	1	1	1	1	0.6	0.6	0.6	0.6	1

Dati relativi alle aree di carico

Convenzioni adottate
Nel seguito sono riportate le *aree di carico* definite nel progetto.
Un'*area di carico* è definita da una superfice contornata da travi di bordo ed i carichi superficiali su essa agenti vengono riportati dal programma sulle travi perimetrali in ragione dell'area di influenza relativa ad ogni trave e della direzione di orditura della superficie.
È importante rilevare che **la direzione di orditura viene assunta dal programma con riferimento al primo lato della superficie di carico e non con riferimento all'asse *x* globale della struttura**.



Esempio: *direzione* di orditura 0 gradi.
In particolare ricordiamo che le *aree di carico* fungono esclusivamente da supporto per il calcolo dei carichi di tipo superficiale in quanto i carichi definiti tramite tali *aree di carico* in effetti vengono trasferiti (sotto forma di carichi lineari o carichi nodali concentrati nei nodi) sulle travi perimetrali che contornano l'area di carico stessa.
A seguire vengono riportati per ogni tipologia definita i carichi agenti nelle varie condizioni di carico. La dizione:

Globale indica che il carico è definito nel sistema di riferimento globale della struttura.
Globale Proiettato indica che il carico è definito nel sistema di riferimento globale della struttura ma il valore viene computato in proiezione.
Locale indica che il carico è definito nel sistema di riferimento locale della superficie di carico.

Area di Carico Numero	Commento
3	Frangisole
4	Soletta Copertura Rampa
5	Grigliato LocaleTecnico
6	Grigliato Canali Shunt

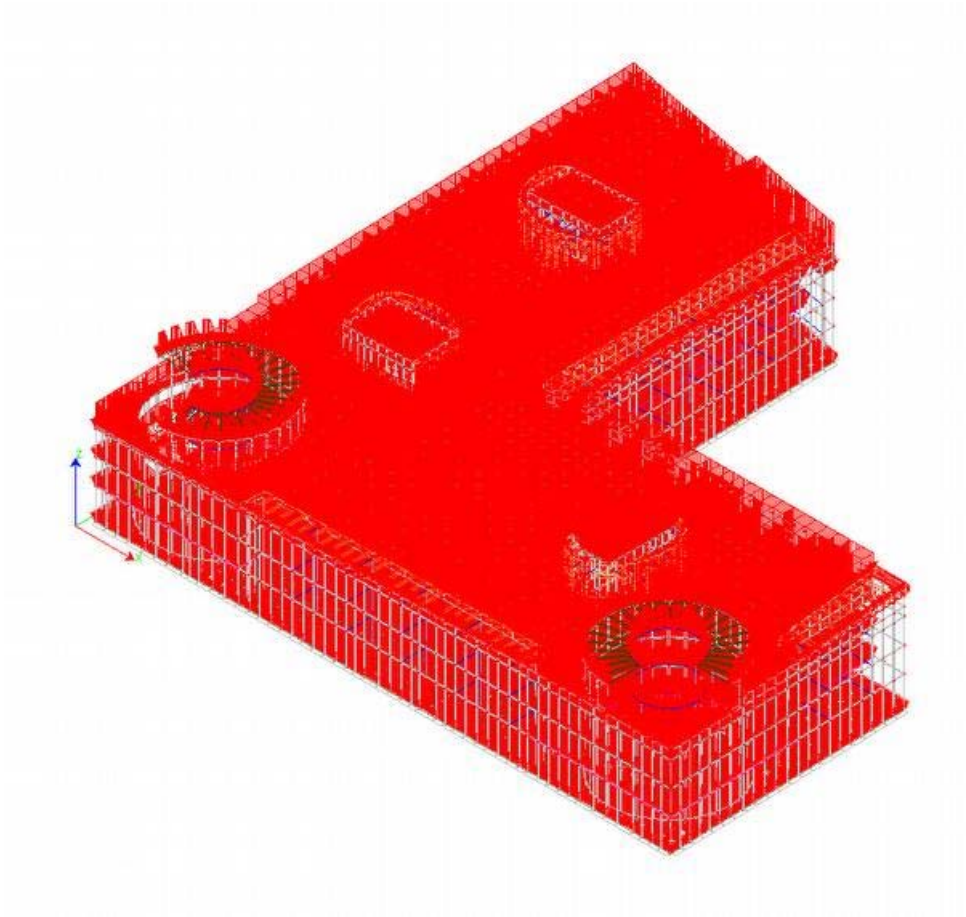
Tipo	Alfa	Condizione	Carico Trasmesso	Riferimento	qx [kg/m²] Qx [kg]	qy [kg/m²] Qy [kg]	qz [kg/m²] Qz [kg]
3	0.00	2	Alle Travi	Globale	0.0	0.0	20.0
					-0.0	-0.0	7044.8
4	0.00	2	Alle Travi	Globale	0.0	0.0	1190.0
					0.0	-0.0	314564.4
4	0.00	5	Alle Travi	Globale	0.0	0.0	100.0
					0.0	0.0	26434.0

Tipo	Alfa	Condizione	Carico Trasmesso	Riferimento	qx [kg/m²] Qx [kg]	qy [kg/m²] Qy [kg]	qz [kg/m²] Qz [kg]
5	0.00	2	Alle Travi	Globale	0.0	0.0	34.0
					0.0	0.0	280.0
5	0.00	3	Alle Travi	Globale	0.0	0.0	500.0
					0.0	0.0	4118.3
6	0.00	2	Alle Travi	Globale	0.0	0.0	34.0
					-0.0	-0.0	12652.8
6	0.00	4	Alle Travi	Globale	0.0	0.0	500.0
					-0.0	-0.0	186071.2

Carichi applicati agli elementi

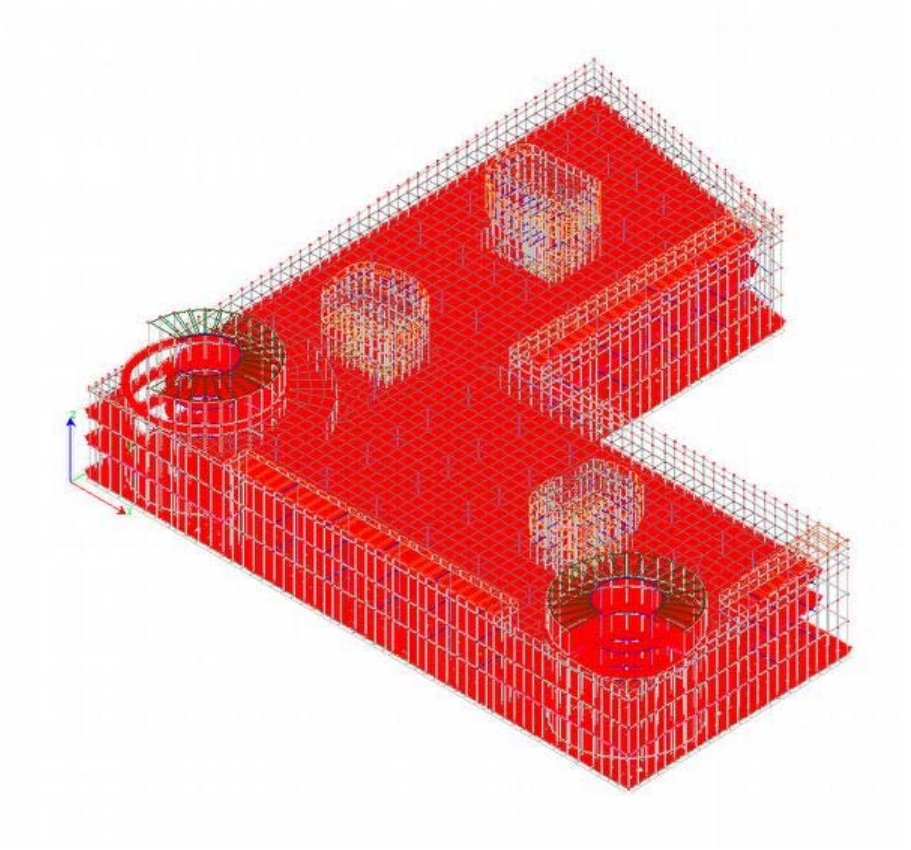
Convenzioni adottate
I carichi applicati vengono raccolti nella tabella riportata alla fine del paragrafo e si intendono applicati nel sistema di riferimento locale dell'elemento.
Per la lettura della tabella si definiscono:

NodoI, NodoJ I nodi iniziale/finale dell'asta o lato dell'elemento cui afferisce il carico
L La distanza fra i suddetti nodi.
qxi, ..., qzj Le componenti di un carico distribuito costante o variabile lineramente iniziali (indice i) e finale (indice j).
xi, xj Le distanze, misurate a partire dal NodoI, dei punti di applicazione dei carichi qxi..qzj relativi a carichi distribuiti applicati su porzioni di un'asta.
Px, ..., Pz xApp Le componenti di un Carico Concentrato applicato a distanza xApp dal NodoI.
Mx, ..., Mz xApp Le componenti di una Coppia Concentrata applicata a distanza xApp dal NodoI.
Var Termica Assiale, ..., Var Termica Farfalla 13 Le variazioni termiche (Assiali ed a Farfalla) misurate in gradi Celsius.
mxi, ..., mzj Le componenti di coppie distribuite costanti o variabili lineramente iniziali (indice i) e finale (indice j).
qS_x, qS_y, qS_z carichi, per unità di superficie, applicati su elementi superficiali o facce di elementi solidi
Peso Proprio Il valore del carico derivante dal peso proprio dell'elemento

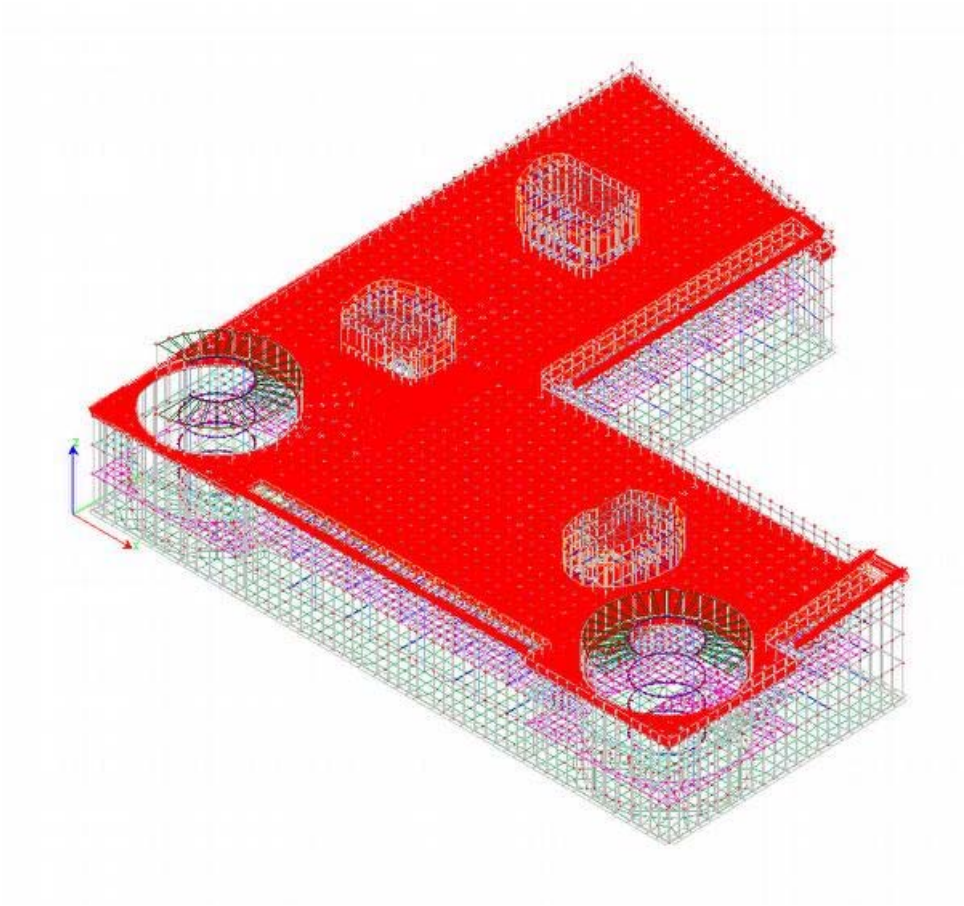


Distribuzione carichi permanenti non strutturali

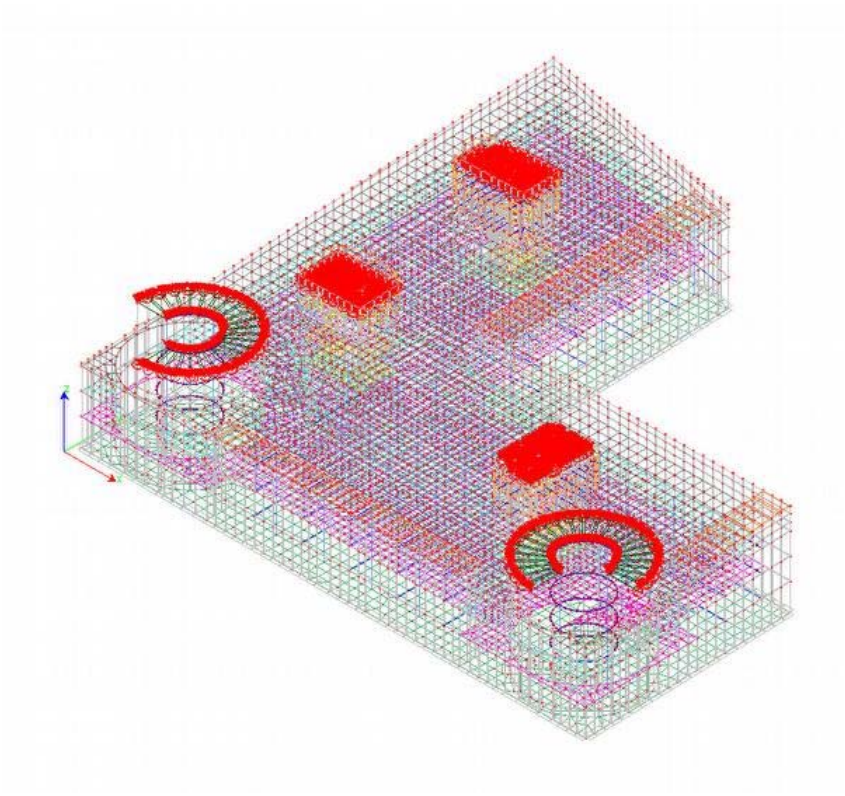
Platea zona parcheggio (Livello -3):	1.024 kg/mq;
Platea zona Riserva Idrica (Livello -3):	3.693 kg/mq;
Piastre Livello -2 e -1:	550 kg/mq;
Piastra Livello 0:	2.250 kg/mq (con presenza di terreno vegetale H=1,00 ml);
Piastra Livello 0:	3.850 kg/mq (con presenza di terreno vegetale H=2,00 ml);
Piastra Livello 0:	5.450 kg/mq (con presenza di terreno vegetale H=3,00 ml);
Piastra Livello 0 zona Locali Tecnici (Corpi scala):	320 kg/mq;
Piastre copertura Locali Tecnici (Corpi scala):	450 kg/mq;
Grigliato zone areazione e loc. tec.:	34 kg/mq;
Soletta rampa:	1.095 kg/mq;
Soletta copertita rampa:	1.190 kg/mq.



Variabile Parcheggi



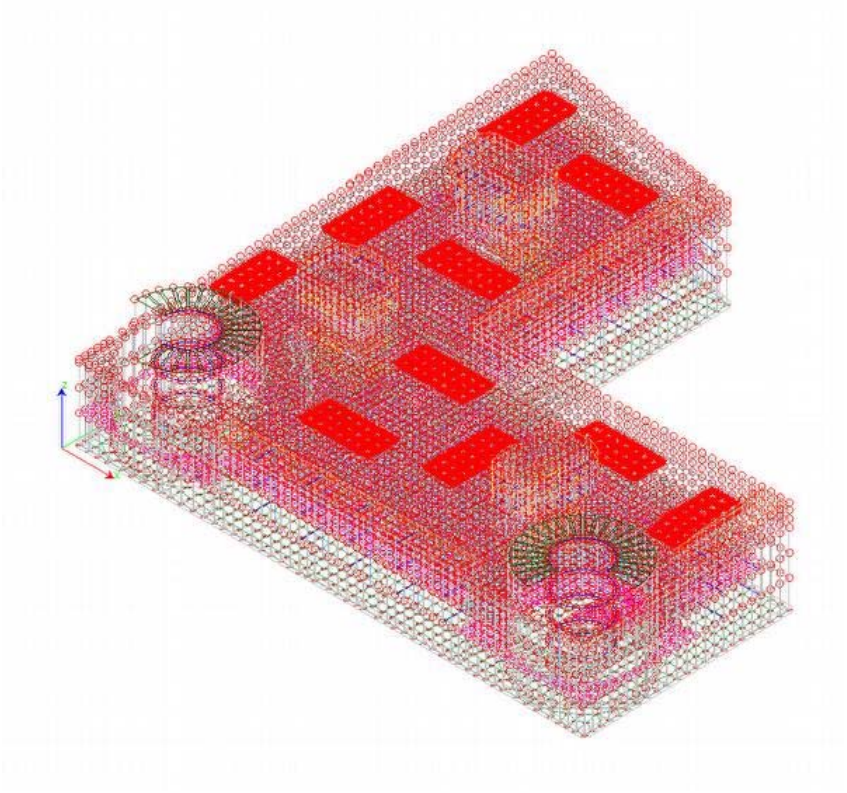
Variabile ambienti suscettibili di affollamento



Variabile coperture non praticabili

Distribuzione dei carichi variabili

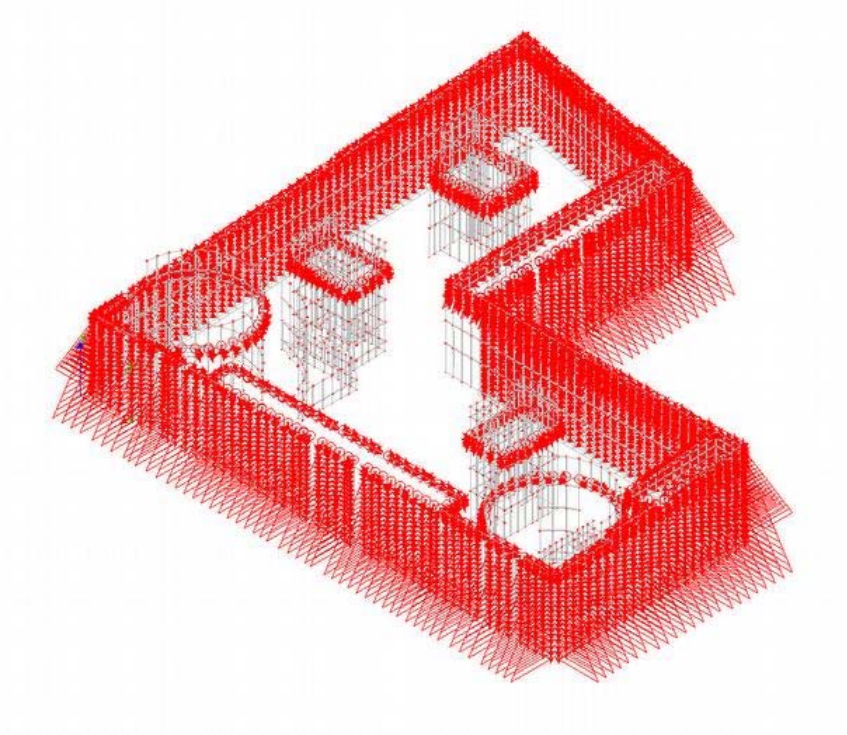
Platea e Piastre Livelli -2 e -1:	250 kg/mq
Piastra Livello 0 e Scale:	400 kg/mq
Piastre e Solette non praticabili:	100 kg/mq



Distribuzione carichi mezzi d'opera sul Livello 0

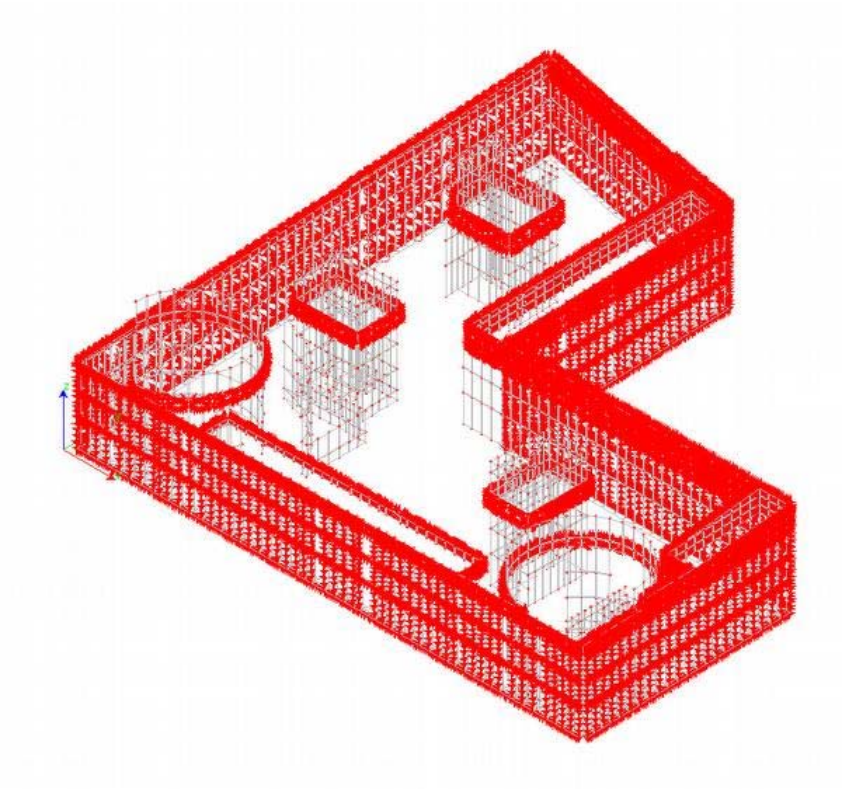
Piastra Livello 0 (Mezzi d'opera): 1.000 kg/mq

Superficie di carico 10,0 m x 4,0 m x 1.000 kg/mq = 40.000 kg



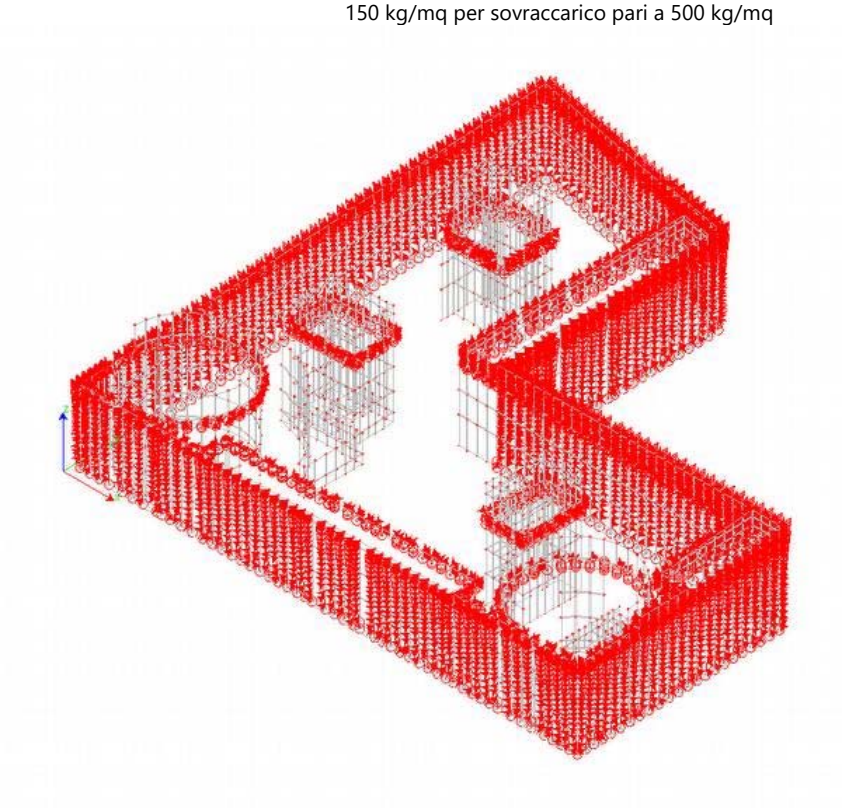
Distribuzione Spinta delle terre

Spinta delle terre: da 0 a 9.000 kg/mq



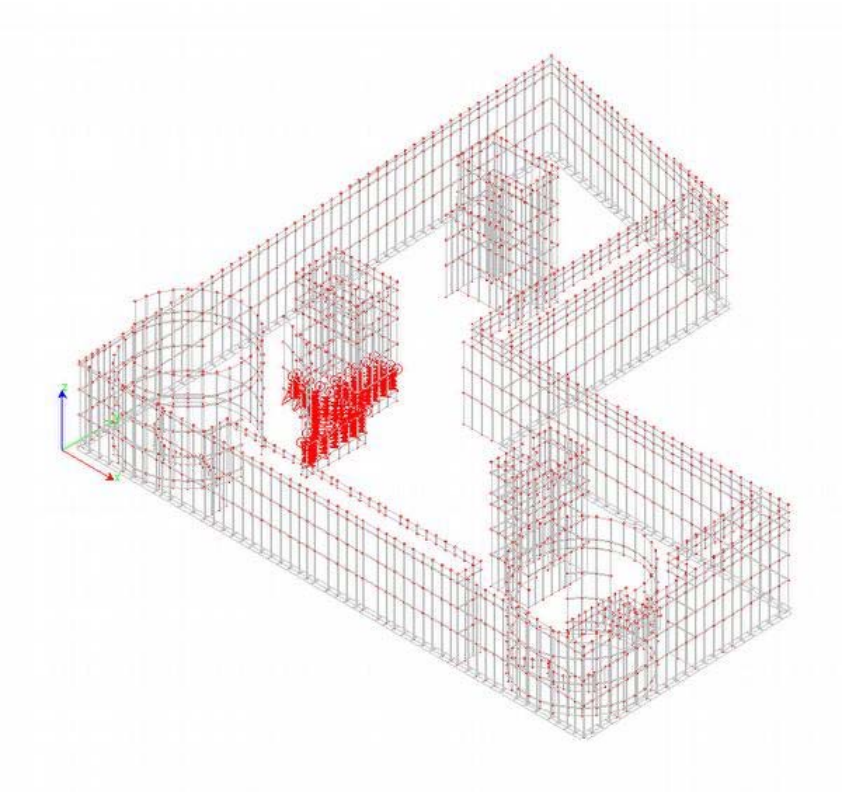
Distribuzione Spinta delle terre dovuta al sovraccarico

Spinta delle terre dovuta al sovraccarico: 610 kg/mq per sovraccarico pari a 2.000 kg/mq
150 kg/mq per sovraccarico pari a 500 kg/mq



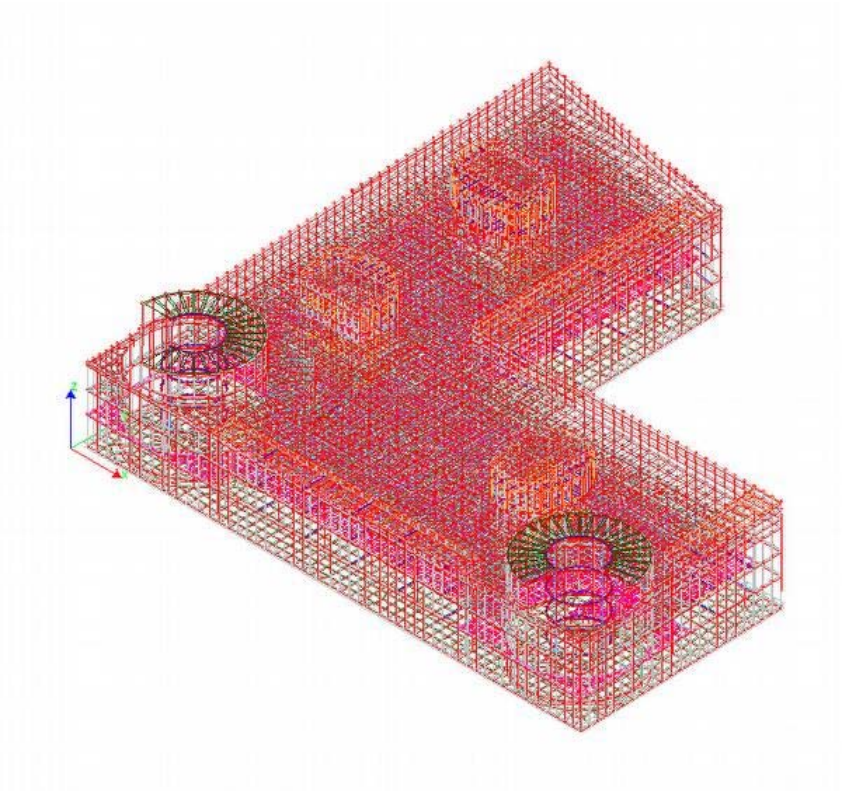
Distribuzione incremento di Spinta delle terre dovuta al sisma

Incremento di spinta delle terre : da 1.890 a 0 kg/mq

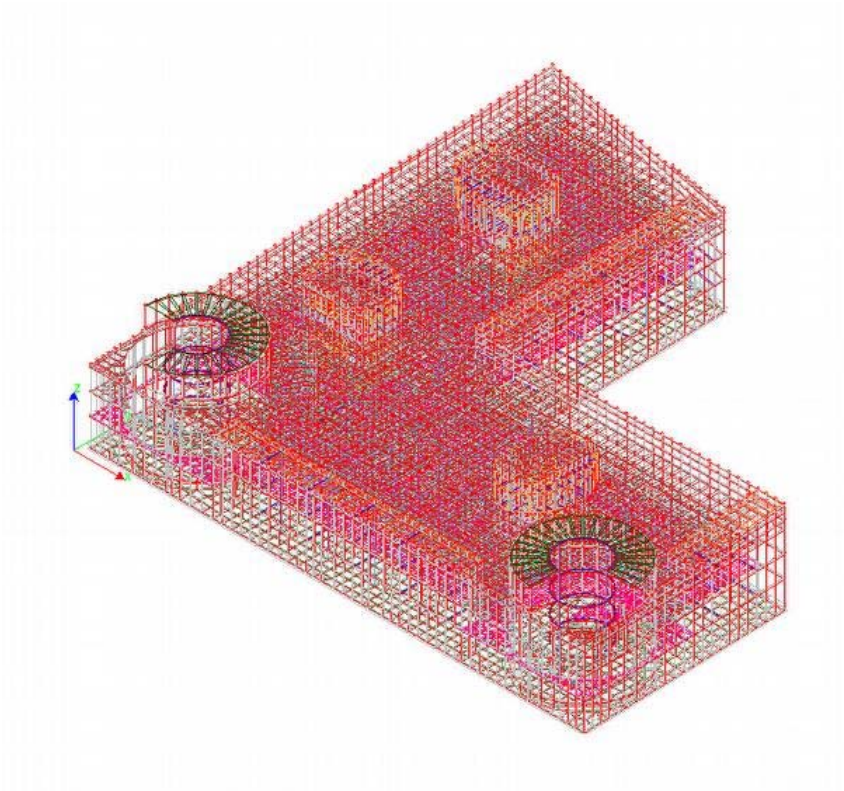


Distribuzione Peso e Spinta dell'acqua

Peso dell'acqua : γxh= 1.000 x 2,90 = 2.900 kg/mq
Spinta dell'acqua : da 0 kg/mq a 2.900 kg/mq



Deformata sisma X+ (0+/90+)



Deformata sisma Y+ (90+/0+)

Spostamenti differenziali massimi

Livello -3 / Livello -2

Massimi Interpiano

Δ x Stilata 66 .. 166

- H = 4.35 [m]
- Combinazione 9
- Δ = -0.08 [cm]
- H / Δ = 5377.3

Δ y Stilata 47A .. 147A

- H = 4.35 [m]
- Combinazione 13
- Δ = -0.12 [cm]
- H / Δ = 3715.3

Δ xy Stilata 48 .. 148

- H = 4.35 [m]
- Combinazione 14
- Δ = 0.12 [cm]
- H / Δ = 3617.7

Dettaglio

Stilata Nodi	H [m]	Totali								
		Δ x			Δ y			Δ xy		
		Δ [cm]	Comb	H/ Δ	Δ [cm]	Comb	H/ Δ	Δ [cm]	Comb	H/ Δ
1 .. 101	4.35	0.01	11	30784.3	0.02	11	22404.8	0.02	11	18115.0
3 .. 103	4.35	-0.05	14	9599.0	0.07	12	6612.9	0.07	11	6279.1
4 .. 104	4.35	-0.05	14	9149.0	0.08	12	5568.3	0.08	11	5461.4
5 .. 105	4.35	-0.04	14	9806.7	0.08	12	5202.0	0.08	12	5187.6

7 .. 107	4.35	-0.04	14	11066.8	0.09	12	5048.7	0.09	14	4965.7
8 .. 108	4.35	-0.03	14	13689.5	-0.09	13	4986.3	0.09	14	4744.2
9 .. 109	4.35	-0.01	9	34525.2	0.02	12	22364.4	0.02	12	19290.3
10 .. 110	4.35	0.02	7	21649.5	0.04	11	10235.7	0.05	11	9283.0
11 .. 111	4.35	0.03	11	17167.9	0.02	11	23749.7	0.03	11	13913.4
12 .. 112	4.35	-0.04	14	11389.2	0.04	11	11376.1	0.05	14	8103.3
13 .. 113	4.35	-0.04	14	10636.2	0.05	12	8746.4	0.06	14	7111.2
14 .. 114	4.35	-0.04	14	10345.4	0.06	12	7094.3	0.07	14	5962.6
15 .. 115	4.35	-0.04	14	10792.3	-0.07	13	5920.7	0.08	14	5287.0
16 .. 116	4.35	-0.04	14	11767.0	-0.08	13	5414.2	0.09	14	5004.5
17 .. 117	4.35	-0.03	14	12695.8	-0.09	13	5091.2	0.09	14	4792.8
18 .. 118	4.35	-0.02	9	23943.6	0.02	12	19395.8	0.03	12	15672.1
19 .. 119	4.35	-0.02	9	23225.0	0.04	12	10049.6	0.05	12	9435.7
20 .. 120	4.35	0.03	11	14747.7	0.04	7	11136.3	0.05	11	8914.6
21 .. 121	4.35	-0.04	14	11915.1	-0.05	13	9494.4	0.06	14	7491.7
22 .. 122	4.35	-0.04	14	11922.7	-0.06	13	7026.3	0.07	14	6163.6
23 .. 123	4.35	-0.04	14	12243.1	-0.08	13	5792.4	0.08	14	5339.9
24 .. 124	4.35	-0.03	14	12920.8	-0.08	13	5408.4	0.09	14	5090.0
25 .. 125	4.35	-0.02	9	17651.2	0.05	12	9616.5	0.05	12	8709.4
26 .. 126	4.35	0.03	7	12773.2	-0.02	14	23402.7	0.04	7	11986.1
27 .. 127	4.35	-0.03	10	12722.1	-0.05	13	9505.2	0.06	14	7858.0
28 .. 128	4.35	-0.03	10	12674.5	-0.06	13	6837.4	0.07	14	6197.6
29 .. 129	4.35	-0.03	10	12582.7	-0.08	13	5560.1	0.08	14	5241.3
30 .. 130	4.35	-0.04	10	12409.3	-0.08	13	5222.1	0.09	14	4987.5
31 .. 131	4.35	-0.04	10	11438.3	-0.09	13	4669.3	0.10	14	4556.1
32 .. 132	4.35	-0.04	10	11837.7	-0.10	13	4368.3	0.10	13	4342.6
34 .. 134	4.35	0.04	7	11423.4	-0.02	14	23072.9	0.04	7	10864.0
35 .. 135	4.35	-0.03	10	12915.6	-0.05	13	9479.3	0.05	14	8290.2
36 .. 136	4.35	-0.03	10	12755.5	-0.07	13	6621.5	0.07	14	6203.3
37 .. 137	4.35	-0.03	10	12556.7	-0.08	13	5244.4	0.09	14	5059.6
38 .. 138	4.35	-0.04	10	11955.4	-0.09	13	4888.1	0.09	14	4737.3
39 .. 139	4.35	-0.04	10	10487.4	-0.10	13	4321.1	0.10	14	4232.1
40 .. 140	4.35	-0.04	10	9881.9	-0.10	13	4232.5	0.10	14	4163.2
41 .. 141	4.35	-0.06	10	6827.1	-0.10	13	4164.3	0.11	14	4058.3
42 .. 142	4.35	-0.03	10	13287.0	-0.04	13	9702.6	0.05	14	9213.6
43 .. 143	4.35	-0.03	10	13519.8	-0.07	13	6437.3	0.07	14	6292.2
44 .. 144	4.35	-0.03	10	13257.7	-0.09	13	4752.6	0.09	14	4732.2
45 .. 145	4.35	-0.03	10	12623.7	-0.10	13	4344.4	0.10	14	4317.9
46 .. 146	4.35	-0.04	10	11775.6	-0.11	13	4075.0	0.11	14	4049.7
47 .. 147	4.35	-0.04	10	10615.1	-0.11	13	3795.5	0.12	14	3770.6
48 .. 148	4.35	-0.06	10	6942.5	-0.12	14	3727.4	0.12	14	3617.7
49 .. 149	4.35	0.05	7	9281.9	-0.02	14	21595.8	0.05	7	8955.8
52 .. 152	4.35	0.05	7	7952.1	-0.02	14	20288.9	0.06	7	7755.9
53 .. 153	4.35	0.05	7	8914.7	-0.03	14	16186.4	0.05	7	8636.6
54 .. 154	4.35	-0.05	10	9485.5	-0.03	14	13949.4	0.05	10	9158.7
55 .. 155	4.35	-0.05	10	9124.2	-0.04	14	11892.7	0.05	10	8765.1
56 .. 156	4.35	-0.05	10	8383.1	-0.04	14	10525.1	0.05	10	8142.5
57 .. 157	4.35	-0.07	10	6281.6	-0.04	13	10052.9	0.07	9	6184.6
58 .. 158	4.35	0.06	8	7634.3	-0.02	14	18889.5	0.06	7	7529.7
59 .. 159	4.35	0.05	8	8417.7	-0.03	14	16347.0	0.05	7	8273.1
60 .. 160	4.35	-0.05	9	8620.8	-0.03	14	13647.9	0.05	10	8562.5
61 .. 161	4.35	-0.05	9	8031.3	-0.04	14	11232.1	0.05	10	7924.5
62 .. 162	4.35	-0.06	9	7154.5	-0.04	14	9875.7	0.06	10	7047.6
63 .. 163	4.35	-0.08	9	5490.9	-0.04	14	9692.2	0.08	10	5456.9
64 .. 164	4.35	0.05	8	8037.3	-0.03	14	16286.0	0.05	7	7945.3

65 .. 165	4.35	-0.06	9	7168.3	-0.05	14	8722.8	0.06	10	6991.2
66 .. 166	4.35	-0.08	9	5377.3	-0.05	14	8530.6	0.08	10	5287.4
67 .. 167	4.35	0.05	8	8212.2	-0.03	14	13444.9	0.05	7	8110.7
68 .. 168	4.35	-0.05	9	9215.7	-0.04	14	10672.7	0.05	10	9071.1
69 .. 169	4.35	-0.05	9	8822.8	-0.05	14	8901.2	0.05	14	8286.7
70 .. 170	4.35	-0.05	9	8287.5	-0.05	14	7998.3	0.06	14	7522.3
71 .. 171	4.35	-0.06	9	7400.8	-0.06	14	7127.2	0.06	14	6778.3
72 .. 172	4.35	-0.08	9	5638.8	-0.06	14	6984.2	0.08	10	5391.2
73 .. 173	4.35	0.05	8	9034.7	-0.04	13	11133.1	0.05	8	8942.5
74 .. 174	4.35	-0.04	9	9858.5	-0.05	14	8405.0	0.05	14	8013.1
75 .. 175	4.35	-0.05	9	9609.1	-0.06	14	7411.1	0.06	14	7125.9
76 .. 176	4.35	-0.05	9	9034.5	-0.06	14	6737.4	0.07	14	6481.9
77 .. 177	4.35	-0.05	9	8869.0	-0.08	14	5676.5	0.08	14	5502.8
78 .. 178	4.35	-0.06	9	7311.6	-0.08	14	5446.4	0.08	14	5265.8
79 .. 179	4.35	-0.04	9	10547.4	-0.04	13	9798.4	0.05	14	9494.0
87 .. 187	4.35	-0.03	10	12626.7	-0.03	14	13626.7	0.04	14	10243.2
47A .. 147A	4.35	-0.05	10	9551.7	-0.12	13	3715.3	0.12	14	3671.1
60A .. 160A	4.35	-0.05	9	8463.5	-0.03	14	13633.1	0.05	9	8427.0

Dalla tabella si evince che in condizioni sismiche non si sono rilevati spostamenti di interpiano superiori a 2/3 di 0.005 H (in quanto costruzione in classe d'uso III) e pi precisamente lo spostamento di interpiano massimo risulta essere pari a 0,12 cm < 2/3 x 0,005 x 435 = 1,43 cm.

Livello -2 / Livello -1

Massimi Interpiano

Δ x Stilata 158 .. 258
- H = 3.45 [m]
- Combinazione 9
- Δ = -0.04 [cm]
- H / Δ = 8150.2

Δ y Stilata 132 .. 232
- H = 3.45 [m]
- Combinazione 13
- Δ = -0.08 [cm]
- H / Δ = 4555.9

Δ xy Stilata 132 .. 232
- H = 3.45 [m]
- Combinazione 14
- Δ = 0.08 [cm]
- H / Δ = 4449.4

Dettaglio

Stilata Nodi	H [m]	Totali								
		Δ x			Δ y			Δ xy		
		Δ [cm]	Comb	H/ Δ	Δ [cm]	Comb	H/ Δ	Δ [cm]	Comb	H/ Δ
179 .. 279	3.45	-0.03	9	11520.3	-0.01	14	25998.7	0.03	9	11461.0
160A .. 260A	3.45	-0.04	9	8862.7	-0.02	14	14515.4	0.04	9	8821.1
147A .. 247A	3.45	-0.03	10	11359.6	0.06	12	5605.5	0.06	12	5572.7
187 .. 287	3.45	-0.03	10	12426.6	-0.03	14	11410.0	0.04	14	9565.8
140 .. 240	3.45	-0.03	10	10391.9	-0.07	13	4954.3	0.07	14	4797.2
139 .. 239	3.45	-0.03	10	10608.6	-0.07	13	5056.8	0.07	14	4934.0
132 .. 232	3.45	-0.04	10	9734.3	-0.08	13	4555.9	0.08	14	4449.4
131 .. 231	3.45	-0.03	10	10168.2	-0.07	13	4739.1	0.07	14	4619.3
178 .. 278	3.45	-0.03	9	12224.2	0.04	11	9755.7	0.04	12	9372.7

177 .. 277	3.45	-0.03	9	12256.2	0.03	11	10233.7	0.03	9	9858.7
176 .. 276	3.45	-0.03	9	11195.5	0.03	11	13589.2	0.03	9	10424.2
175 .. 275	3.45	-0.03	9	11116.0	0.02	11	17658.1	0.03	9	10811.1
174 .. 274	3.45	-0.03	9	10691.6	0.02	11	22653.8	0.03	9	10574.1
173 .. 273	3.45	-0.03	9	10030.0	-0.02	13	22442.7	0.03	9	9970.6
172 .. 272	3.45	0.03	8	11146.4	0.03	11	11616.8	0.04	7	9640.9
171 .. 271	3.45	-0.03	9	10875.3	0.03	11	12331.0	0.03	9	10122.0
170 .. 270	3.45	-0.03	9	10092.2	0.02	11	14984.1	0.04	9	9777.8
169 .. 269	3.45	-0.03	9	10143.6	-0.02	14	17788.8	0.03	9	9969.8
168 .. 268	3.45	-0.04	9	9755.5	-0.02	14	19075.2	0.04	9	9675.2
167 .. 267	3.45	-0.04	9	8848.1	-0.02	14	20443.1	0.04	9	8803.8
166 .. 266	3.45	0.03	8	10333.9	0.03	11	13170.2	0.04	7	9826.4
165 .. 265	3.45	-0.04	9	9433.5	0.03	11	13674.4	0.04	9	9152.8
164 .. 264	3.45	-0.04	9	8583.2	-0.02	14	19478.5	0.04	9	8558.3
163 .. 263	3.45	0.03	8	10711.7	0.03	11	13104.6	0.03	9	10406.4
162 .. 262	3.45	-0.04	9	9762.9	0.03	11	13518.6	0.04	9	9433.1
161 .. 261	3.45	-0.04	9	9026.0	-0.03	14	13445.0	0.04	9	8918.5
160 .. 260	3.45	-0.04	9	8969.2	-0.02	14	14509.6	0.04	9	8928.1
159 .. 259	3.45	-0.04	9	8774.2	-0.02	14	16395.5	0.04	9	8758.3
158 .. 258	3.45	-0.04	9	8150.2	-0.02	14	19816.4	0.04	9	8143.4
157 .. 257	3.45	-0.03	10	11726.4	0.03	12	11388.7	0.03	9	10738.0
156 .. 256	3.45	-0.03	10	10889.2	-0.03	14	12362.9	0.03	9	10389.8
155 .. 255	3.45	-0.03	10	9916.0	-0.03	14	13182.0	0.04	10	9658.2
154 .. 254	3.45	-0.04	10	9739.4	-0.02	14	14744.3	0.04	10	9482.2
153 .. 253	3.45	-0.04	10	9313.9	-0.02	14	16624.3	0.04	10	9103.7
152 .. 252	3.45	-0.04	10	8397.3	-0.02	14	20996.2	0.04	10	8271.7
149 .. 249	3.45	-0.04	10	9759.2	-0.01	14	23098.7	0.04	10	9588.0
148 .. 248	3.45	-0.03	10	12350.7	-0.06	13	5311.4	0.07	14	5126.0
147 .. 247	3.45	-0.03	10	11577.1	0.06	12	5465.2	0.06	12	5439.4
146 .. 246	3.45	-0.03	10	12538.9	0.06	12	5578.3	0.06	12	5560.6
145 .. 245	3.45	-0.03	10	13624.3	0.06	12	5785.7	0.06	12	5774.0
144 .. 244	3.45	-0.02	10	13940.3	0.06	12	6133.2	0.06	12	6122.5
143 .. 243	3.45	-0.03	10	13413.3	0.04	12	7794.3	0.04	11	7692.4
142 .. 242	3.45	-0.03	10	12034.1	0.04	11	9455.4	0.04	11	9233.2
141 .. 241	3.45	-0.03	10	11099.4	-0.07	14	5148.3	0.07	14	4730.6
138 .. 238	3.45	-0.03	10	13104.6	-0.06	13	6154.9	0.06	14	5989.4
137 .. 237	3.45	-0.03	10	13400.0	0.05	12	7046.9	0.05	12	7046.9
136 .. 236	3.45	-0.03	10	13114.6	0.04	12	8282.0	0.04	14	7965.6
135 .. 235	3.45	-0.03	10	12449.2	-0.04	14	9628.5	0.04	14	8358.2
134 .. 234	3.45	-0.03	10	11136.3	0.02	11	22014.6	0.03	10	10957.6
130 .. 230	3.45	-0.03	10	12745.9	-0.06	13	5939.9	0.06	14	5627.6
129 .. 229	3.45	-0.03	10	13081.2	-0.05	13	6995.7	0.05	14	6491.4
128 .. 228	3.45	-0.03	10	12993.4	-0.04	13	8181.1	0.05	14	7318.4
127 .. 227	3.45	-0.03	10	12595.1	-0.04	13	9282.8	0.04	14	7852.7
126 .. 226	3.45	-0.03	10	10838.9	0.02	11	21895.6	0.03	10	10728.4
125 .. 225	3.45	-0.02	9	15550.9	0.02	12	15366.0	0.03	12	11223.2
124 .. 224	3.45	-0.03	10	12900.8	-0.06	13	5739.6	0.06	14	5360.6
123 .. 223	3.45	-0.03	10	12884.1	-0.05	13	6613.2	0.06	14	6027.4
122 .. 222	3.45	-0.03	10	12872.8	-0.04	13	7777.2	0.05	14	6803.3
121 .. 221	3.45	-0.03	10	12694.9	-0.04	13	9248.6	0.05	14	7551.4
120 .. 220	3.45	0.03	11	13466.0	0.02	11	16363.8	0.03	11	10397.9
119 .. 219	3.45	-0.03	9	12067.5	0.02	12	15545.1	0.04	12	9764.0
118 .. 218	3.45	-0.01	9	26349.9	0.03	12	11349.4	0.03	12	10580.6
117 .. 217	3.45	-0.03	14	11611.2	-0.07	13	5069.5	0.07	14	4726.4
116 .. 216	3.45	-0.03	14	11362.6	-0.06	13	5416.9	0.07	14	4981.2

115 .. 215	3.45	-0.03	14	11010.2	-0.06	13	6144.3	0.06	14	5474.1
114 .. 214	3.45	-0.03	14	10925.5	-0.05	13	7206.4	0.06	14	6111.5
113 .. 213	3.45	-0.03	14	11017.1	-0.04	13	8896.7	0.05	14	6959.4
112 .. 212	3.45	-0.03	14	11100.1	0.03	11	10794.3	0.04	14	8233.9
111 .. 211	3.45	0.02	11	21789.7	0.03	11	12683.8	0.03	11	10961.9
110 .. 210	3.45	0.03	11	10964.4	0.02	11	16869.3	0.04	11	9193.2
109 .. 209	3.45	-0.01	9	∞	0.04	12	8850.5	0.04	12	8655.4
108 .. 208	3.45	-0.03	14	12799.8	-0.07	13	5049.6	0.07	14	4776.5
107 .. 207	3.45	-0.03	14	10401.8	-0.07	13	5228.9	0.07	14	4764.9
105 .. 205	3.45	-0.04	14	9841.3	-0.06	13	5829.5	0.07	14	5114.6
104 .. 204	3.45	-0.04	14	9694.6	-0.05	13	6820.5	0.06	14	5657.9
103 .. 203	3.45	-0.04	14	9632.6	-0.04	13	8555.3	0.05	14	6420.8
101 .. 201	3.45	0.01	11	26109.3	0.04	11	9397.7	0.04	11	8842.4

Dalla tabella si evince che in condizioni sismiche non si sono rilevati spostamenti di interpiano superiori a 2/3 di 0.005 H (in quanto costruzione in classe d'uso III) e pi precisamente lo spostamento di interpiano massimo risulta essere pari a 0,08 cm < 2/3 x 0,005 x 345 = 1,14 cm.

Livello -1 / Livello 0

Massimi Interpiano

Δ x Stilata 211 .. 311
- H = 3.45 [m]
- Combinazione 11
- Δ = 0.04 [cm]
- H / Δ = 8808.5

Δ y Stilata 246 .. 346
- H = 3.45 [m]
- Combinazione 13
- Δ = -0.05 [cm]
- H / Δ = 6476.1

Δ xy Stilata 211 .. 311
- H = 3.45 [m]
- Combinazione 11
- Δ = 0.06 [cm]
- H / Δ = 6083.8

Dettaglio

Stilata Nodi	H [m]	Totali								
		Δ x			Δ y			Δ xy		
		Δ [cm]	Comb	H/ Δ	Δ [cm]	Comb	H/ Δ	Δ [cm]	Comb	H/ Δ
201 .. 301	3.45	0.02	11	17644.9	0.02	7	14722.3	0.03	11	11322.4
203 .. 303	3.45	-0.02	14	15695.9	-0.02	13	21127.8	0.03	14	12678.7
204 .. 304	3.45	-0.02	14	14730.6	-0.02	13	16008.9	0.03	14	11017.5
205 .. 305	3.45	-0.02	14	13933.9	-0.03	13	12081.6	0.04	14	9292.1
207 .. 307	3.45	-0.02	14	14891.7	-0.04	13	9301.6	0.04	14	8020.4
209 .. 309	3.45	-0.02	9	21068.3	0.03	12	13220.3	0.03	12	11371.8
210 .. 310	3.45	0.02	11	21601.2	0.02	11	14630.6	0.03	11	12113.6
211 .. 311	3.45	0.04	11	8808.5	0.04	11	8412.6	0.06	11	6083.8
212 .. 312	3.45	-0.02	14	18535.9	0.02	11	13982.5	0.03	11	11471.5
213 .. 313	3.45	-0.02	14	17958.3	-0.02	13	16888.7	0.03	14	12386.9
214 .. 314	3.45	-0.02	14	16890.5	-0.03	13	13441.9	0.03	14	10712.5
215 .. 315	3.45	-0.02	14	16278.7	-0.03	13	10526.7	0.04	14	9021.6
216 .. 316	3.45	-0.02	14	16602.2	-0.04	13	8287.8	0.05	14	7554.6

217 .. 317	3.45	-0.02	10	16701.3	-0.04	13	7931.2	0.05	14	7359.7
218 .. 318	3.45	-0.04	9	9359.2	0.04	12	8047.2	0.06	12	6173.2
219 .. 319	3.45	-0.01	9	27794.7	0.03	12	13441.6	0.03	12	12254.3
220 .. 320	3.45	0.04	11	9450.4	0.04	11	8183.4	0.06	11	6186.3
221 .. 321	3.45	0.02	7	18427.4	-0.02	13	14143.5	0.03	14	12129.5
222 .. 322	3.45	-0.02	10	18646.1	-0.03	13	11414.9	0.03	14	10112.4
223 .. 323	3.45	-0.02	10	17930.8	-0.04	13	9200.1	0.04	14	8469.4
224 .. 324	3.45	-0.02	10	16587.4	-0.05	13	7313.9	0.05	14	6913.7
225 .. 325	3.45	-0.03	9	10254.6	0.04	12	7956.0	0.05	12	6352.4
226 .. 326	3.45	0.02	7	16190.0	0.02	11	19858.6	0.03	11	13012.4
227 .. 327	3.45	0.02	7	19141.9	-0.02	13	14132.8	0.03	14	12357.5
228 .. 328	3.45	-0.02	10	18028.4	-0.03	13	11161.6	0.03	14	10168.1
229 .. 329	3.45	-0.02	10	17631.0	-0.04	13	8982.9	0.04	14	8465.0
230 .. 330	3.45	-0.02	10	17660.0	-0.05	13	7262.9	0.05	14	7000.9
234 .. 334	3.45	0.02	7	15492.9	0.02	11	21396.9	0.03	7	13423.5
235 .. 335	3.45	-0.02	10	17737.7	-0.02	13	13988.5	0.03	14	12320.5
236 .. 336	3.45	-0.02	10	17032.7	-0.03	13	10999.4	0.03	14	10179.2
237 .. 337	3.45	-0.02	10	17011.0	-0.04	13	8806.9	0.04	14	8428.7
238 .. 338	3.45	-0.02	10	16734.1	-0.05	13	7438.9	0.05	14	7170.6
242 .. 342	3.45	-0.02	10	15436.2	-0.03	14	11664.7	0.03	14	10582.4
243 .. 343	3.45	-0.02	10	15575.7	-0.04	13	9109.6	0.04	14	8703.4
244 .. 344	3.45	-0.02	10	16750.9	-0.05	13	7413.8	0.05	14	7309.6
245 .. 345	3.45	-0.02	10	16725.5	-0.05	13	6680.4	0.05	14	6577.7
246 .. 346	3.45	-0.02	10	16412.9	-0.05	13	6476.1	0.05	14	6291.2
247 .. 347	3.45	-0.02	10	16387.2	-0.05	14	6830.6	0.05	14	6520.9
249 .. 349	3.45	0.02	7	14581.3	0.01	11	23424.2	0.03	7	13221.8
252 .. 352	3.45	0.02	7	14489.4	0.01	11	26876.8	0.03	7	13630.3
253 .. 353	3.45	0.02	7	16681.4	0.02	11	21173.6	0.02	7	15046.3
254 .. 354	3.45	0.02	7	16145.0	0.02	11	19537.2	0.02	7	14523.5
255 .. 355	3.45	0.02	7	16066.5	-0.02	14	18009.6	0.02	7	14652.1
256 .. 356	3.45	-0.02	10	18396.6	-0.02	14	14279.2	0.03	14	13328.7
257 .. 357	3.45	-0.01	10	24953.4	-0.03	14	11773.0	0.03	14	11130.5
258 .. 358	3.45	0.02	8	15509.6	-0.01	14	25973.0	0.02	7	15327.9
259 .. 359	3.45	0.02	8	16509.0	-0.02	14	21415.2	0.02	7	16122.4
260 .. 360	3.45	0.02	8	15711.5	-0.02	14	19421.4	0.02	7	15031.6
261 .. 361	3.45	0.02	8	15147.0	-0.02	14	16626.8	0.02	7	14622.9
262 .. 362	3.45	0.02	8	18096.0	-0.02	14	14602.4	0.02	14	14253.2
263 .. 363	3.45	0.02	7	22387.7	-0.03	14	13610.6	0.03	14	12985.6
264 .. 364	3.45	0.02	8	15374.1	-0.02	13	22871.4	0.02	8	15031.8
265 .. 365	3.45	0.02	8	15013.0	-0.02	14	15427.7	0.02	8	14397.3
266 .. 366	3.45	0.02	8	18655.5	-0.02	14	14295.3	0.03	14	13727.1
267 .. 367	3.45	0.02	8	14767.8	-0.02	13	20880.2	0.03	13	13487.8
268 .. 368	3.45	-0.02	9	14068.0	-0.02	13	19832.5	0.02	9	14058.9
269 .. 369	3.45	-0.03	9	13799.7	-0.02	14	19276.3	0.03	9	13755.8
270 .. 370	3.45	0.02	8	14728.0	-0.02	14	17527.7	0.02	8	13984.7
271 .. 371	3.45	-0.02	9	14242.0	-0.02	14	16467.5	0.03	10	13462.0
272 .. 372	3.45	-0.02	9	17163.7	-0.02	14	15984.8	0.02	14	15247.1
273 .. 373	3.45	0.02	8	16837.0	-0.02	13	19223.7	0.03	13	13093.0
274 .. 374	3.45	-0.02	9	14278.3	-0.02	13	17933.1	0.02	9	14174.6
275 .. 375	3.45	-0.03	9	13613.8	-0.02	13	16972.1	0.03	9	13187.9
276 .. 376	3.45	-0.03	9	13286.8	-0.02	14	15406.8	0.03	10	12055.4
277 .. 377	3.45	-0.03	9	11277.8	-0.02	14	14985.3	0.03	10	10081.6
278 .. 378	3.45	-0.03	9	12601.8	-0.01	10	27505.4	0.03	9	12203.2
231 .. 331	3.45	-0.03	10	12946.3	-0.04	13	8059.2	0.05	14	7409.8
232 .. 332	3.45	-0.03	10	11674.3	0.04	12	8430.0	0.05	14	7510.9

239 .. 339	3.45	-0.02	10	15169.3	-0.04	13	7967.5	0.05	14	7476.3
240 .. 340	3.45	-0.02	10	15547.4	-0.04	14	8365.7	0.04	14	7783.0
287 .. 387	3.45	0.02	7	15067.6	-0.02	14	16559.8	0.03	11	13557.1
247A .. 347A	3.45	-0.02	10	18339.9	-0.05	14	7620.3	0.05	14	7283.9
260A .. 360A	3.45	0.02	8	14965.6	-0.02	14	19205.2	0.02	7	14702.8
279 .. 379	3.45	-0.02	9	16719.9	-0.02	13	19069.5	0.02	13	14728.1

Dalla tabella si evince che in condizioni sismiche non si sono rilevati spostamenti di interpiano superiori a 2/3 di 0.005 H (in quanto costruzione in classe d'uso III) e pi precisamente lo spostamento di interpiano massimo risulta essere pari a 0,06 cm < 2/3 x 0,005 x 345 = 1,14 cm.

Livello 0 / Livello Copertura scale e rampe

Massimi Interpiano

Δ x Stilata 301 .. 401

- H = 4.30 [m]
- Combinazione 11
- Δ = 0.27 [cm]
- H / Δ = 1585.7

Δ y Stilata 319 .. 419

- H = 4.30 [m]
- Combinazione 12
- Δ = 0.28 [cm]
- H / Δ = 1532.6

Δ xy Stilata 319 .. 419

- H = 4.30 [m]
- Combinazione 12
- Δ = 0.28 [cm]
- H / Δ = 1517.6

Dettaglio

Stilata Nodi	H [m]	Totali								
		Δ x			Δ y			Δ xy		
		Δ [cm]	Comb	H/ Δ	Δ [cm]	Comb	H/ Δ	Δ [cm]	Comb	H/ Δ
301 .. 401	4.30	0.27	11	1585.7	-0.03	14	12420.2	0.27	11	1579.1
309 .. 409	4.30	-0.27	9	1621.2	-0.04	13	12066.1	0.27	9	1615.0
310 .. 410	4.30	-0.05	14	8283.1	0.28	7	1548.1	0.28	7	1535.4
311 .. 411	4.30	0.09	11	4764.8	0.07	11	6179.8	0.11	11	3773.4
318 .. 418	4.30	-0.09	9	4947.1	0.07	12	5966.2	0.11	12	3834.2
319 .. 419	4.30	0.05	13	8607.3	0.28	12	1532.6	0.28	12	1517.6
320 .. 420	4.30	0.06	11	6805.3	0.09	11	4608.3	0.11	11	3815.8
325 .. 425	4.30	-0.06	9	7197.1	0.10	12	4514.1	0.11	12	3842.1
383 .. 483	4.27	0.02	7	19056.3	-0.06	13	7014.1	0.06	13	7014.0
384 .. 484	3.67	0.03	8	12337.2	-0.02	14	21991.0	0.03	8	12304.0

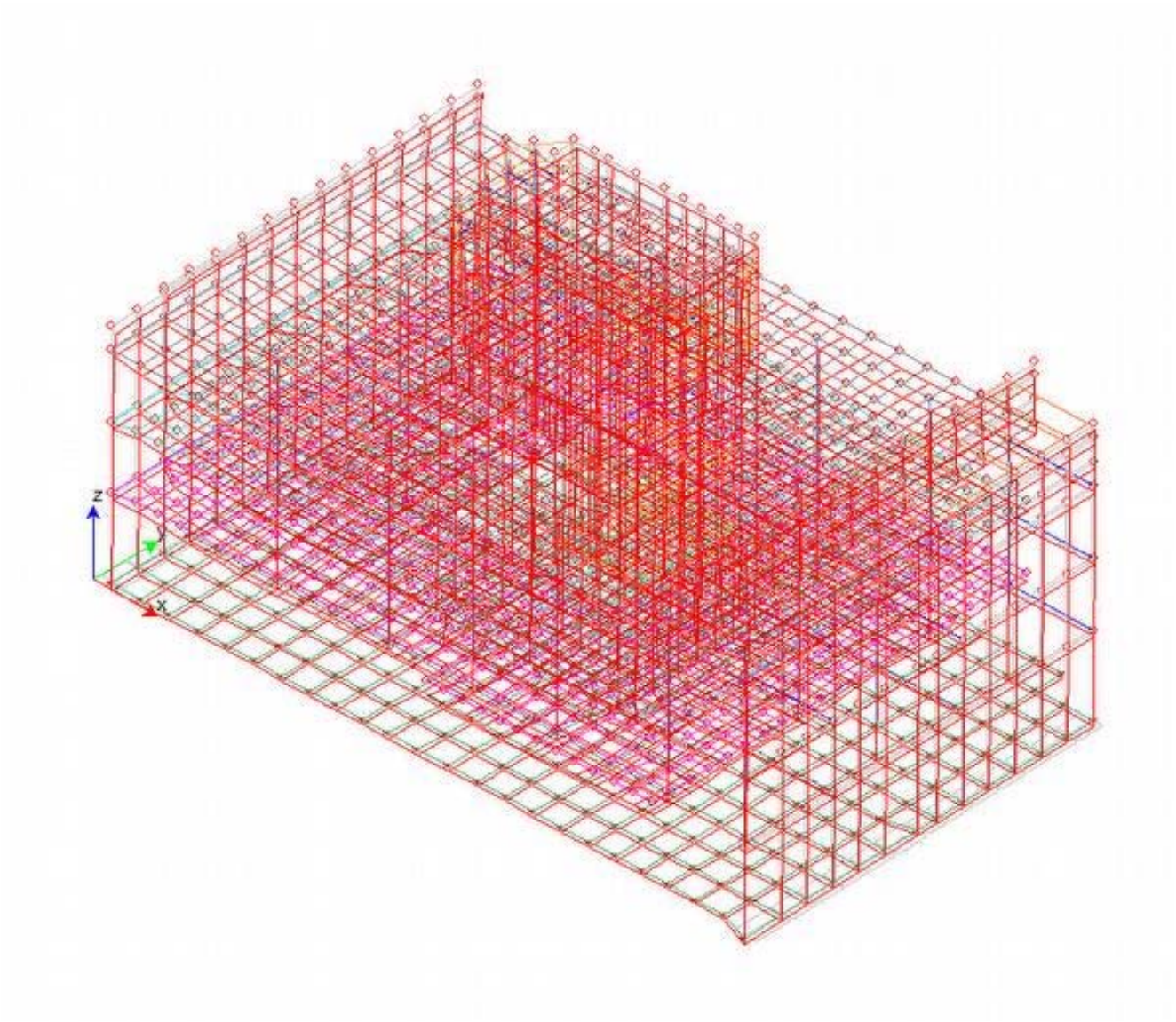
Dalla tabella si evince che in condizioni sismiche non si sono rilevati spostamenti di interpiano superiori a 2/3 di 0.005 H (in quanto costruzione in classe d'uso III) e pi precisamente lo spostamento di interpiano massimo risulta essere pari a 0,28 cm < 2/3 x 0,005 x 430 = 1,42 cm.

In definitiva dalle tabelle precedenti si evince che in condizioni sismiche non si sono rilevati spostamenti di interpiano superiori a 2/3 x 0.005 H.

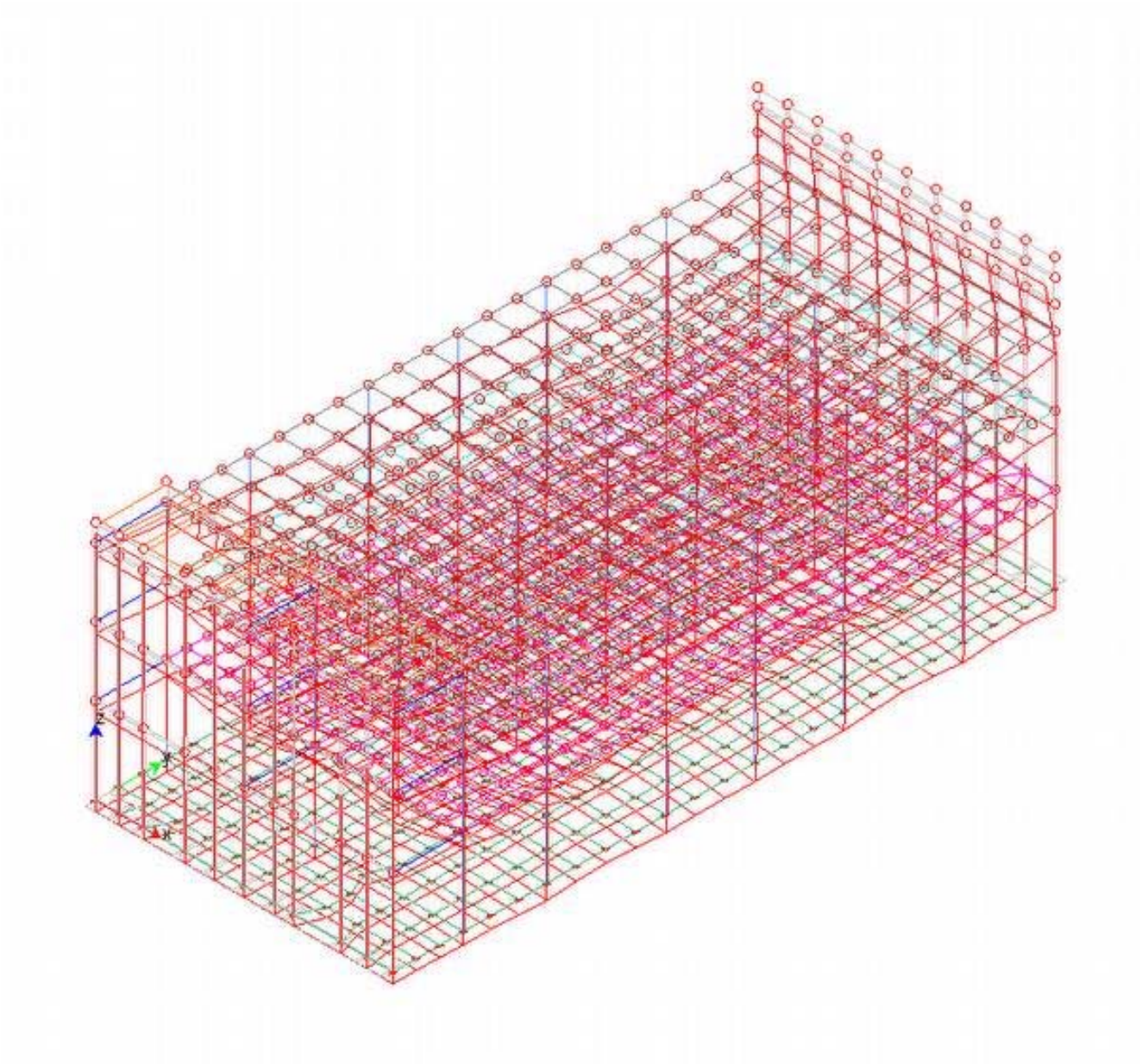
Tensioni sul terreno

- 1,97 kg/cmq in assenza di sisma SLV GEO – Combinazione geotecnica 2 – Approccio 1 (Tab. 6.2.1 del DM 14.01.08) (A2+M2+R2) (v.6.4.2.1)
- 1,64 kg/cmq in presenza di sisma SLV GEO – Combinazione geotecnica 2 – Approccio 1 (Tab. 6.2.1 del DM 14.01.08) (A2+M2+R2) (v.6.4.2.1)

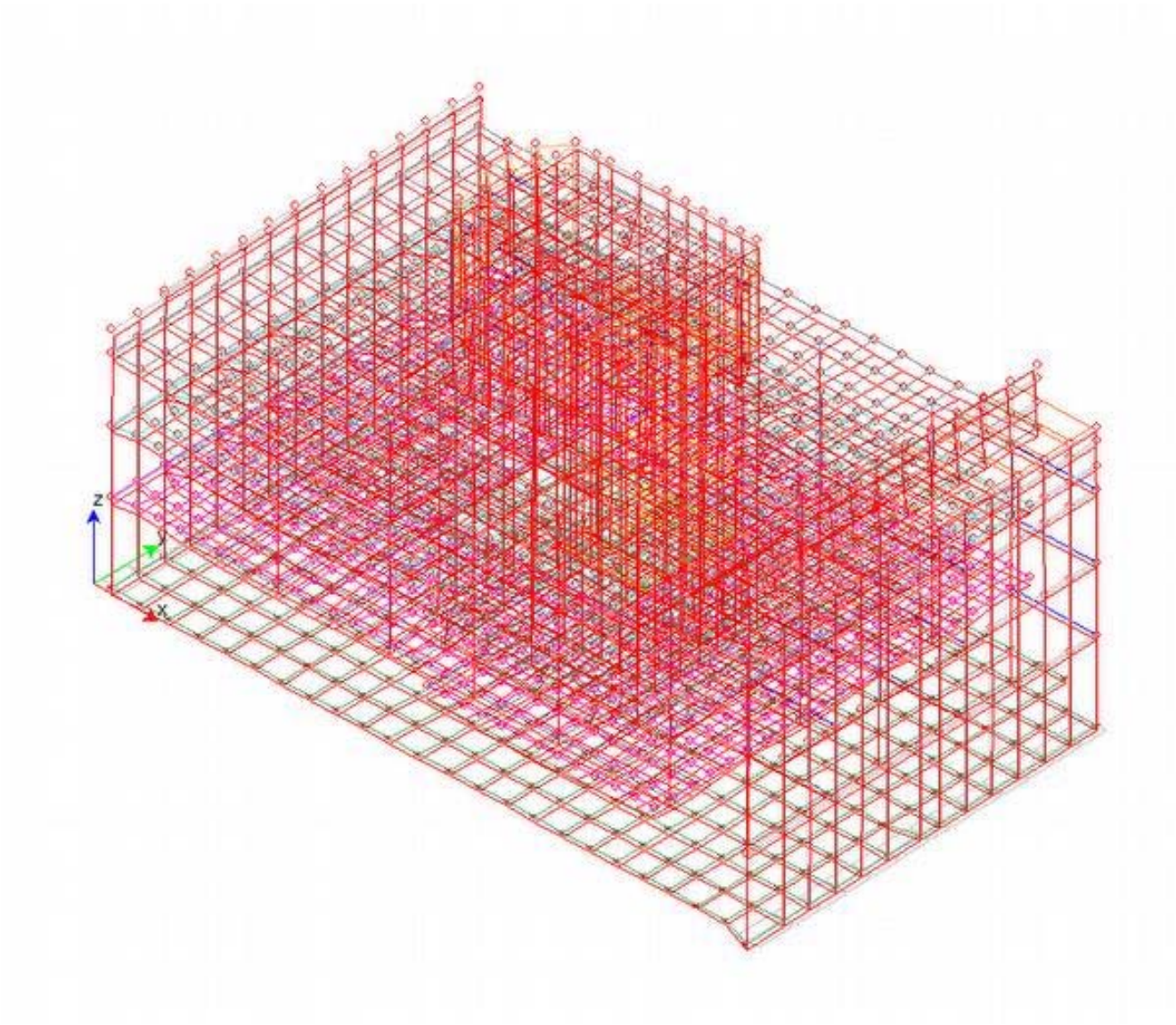
Grafici sintetici dei risultati di calcolo



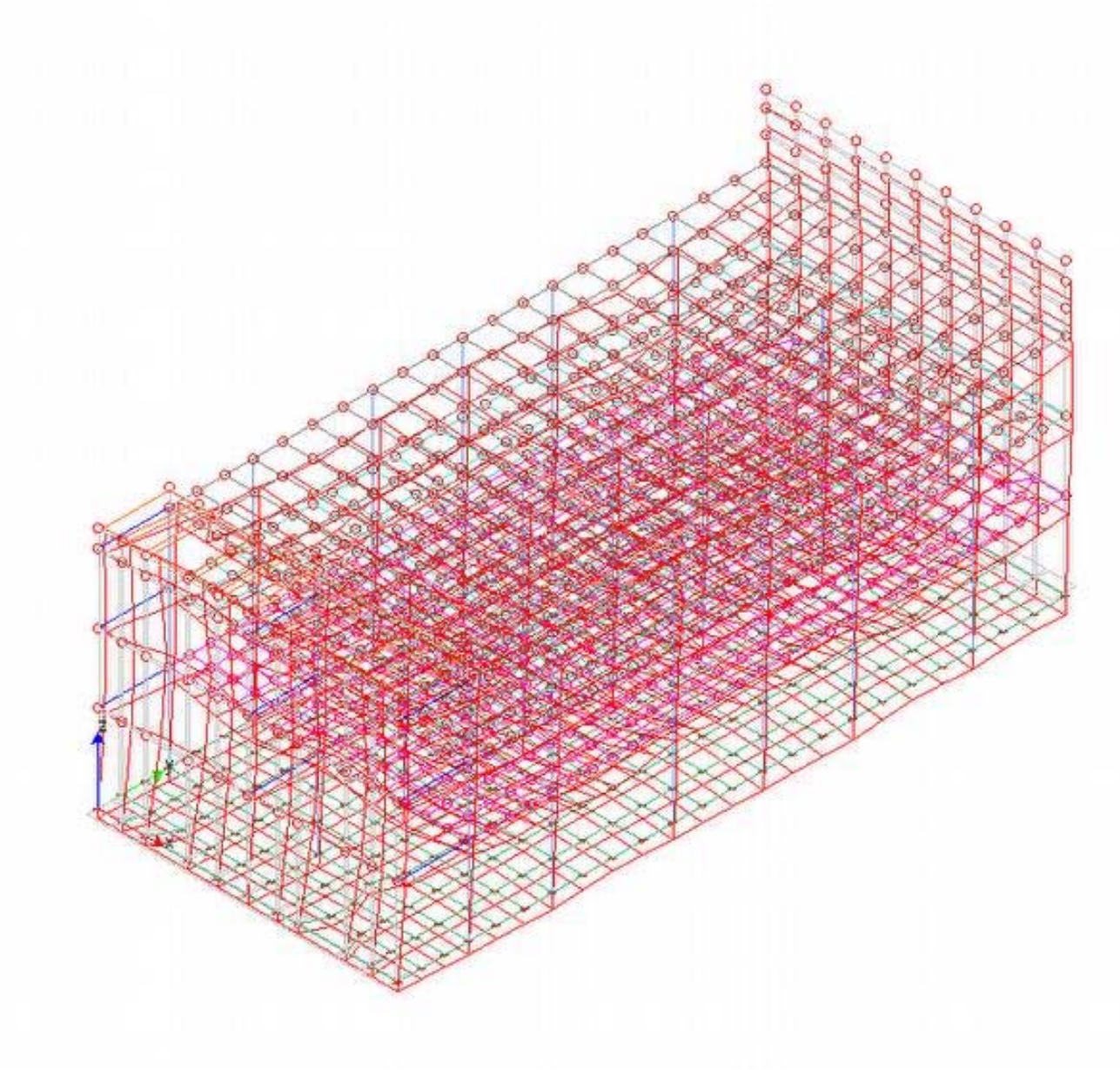
Stralcio 1 – Deformata per Sisma X+



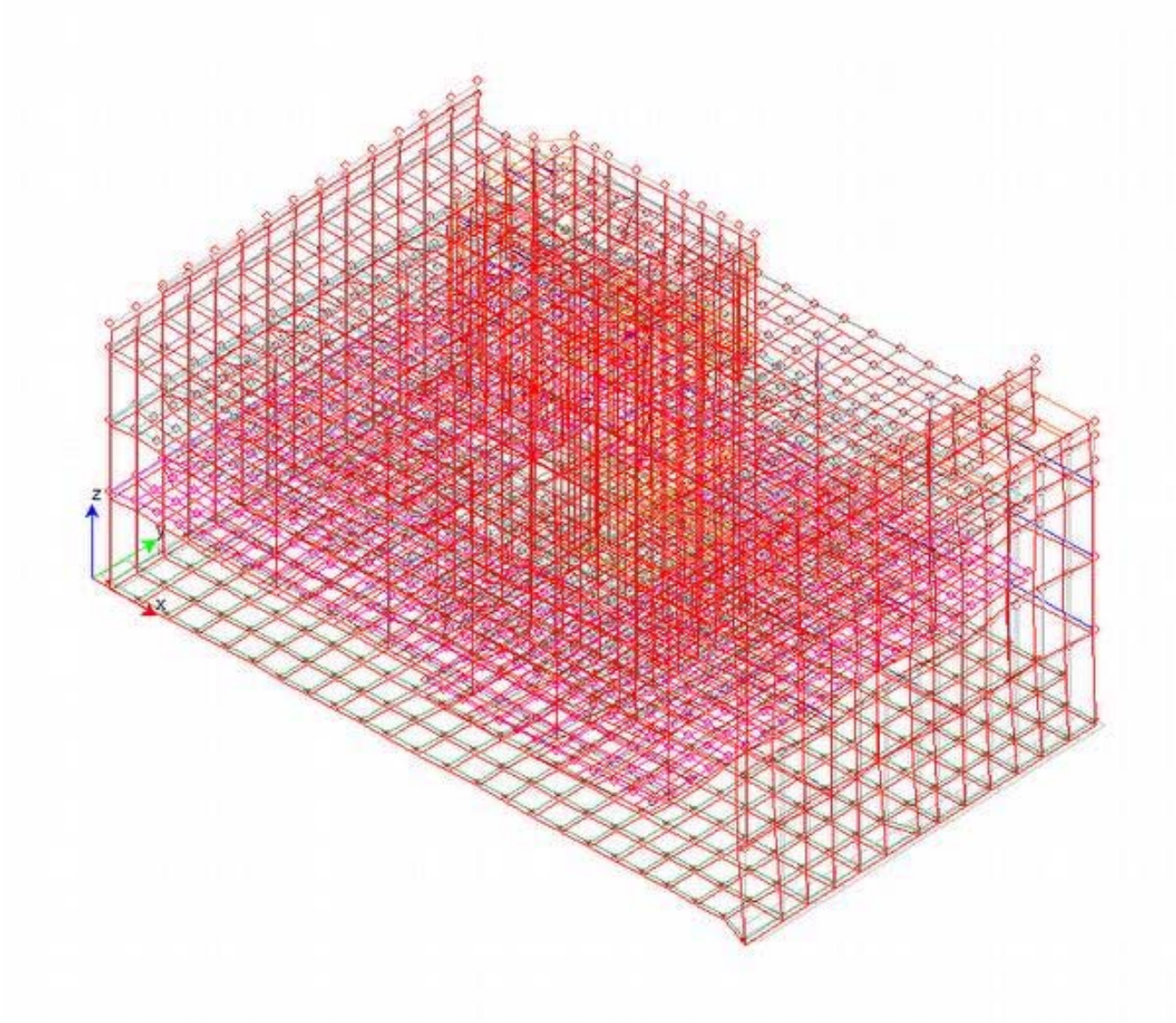
Stralcio 2 – Deformata per Sisma X+



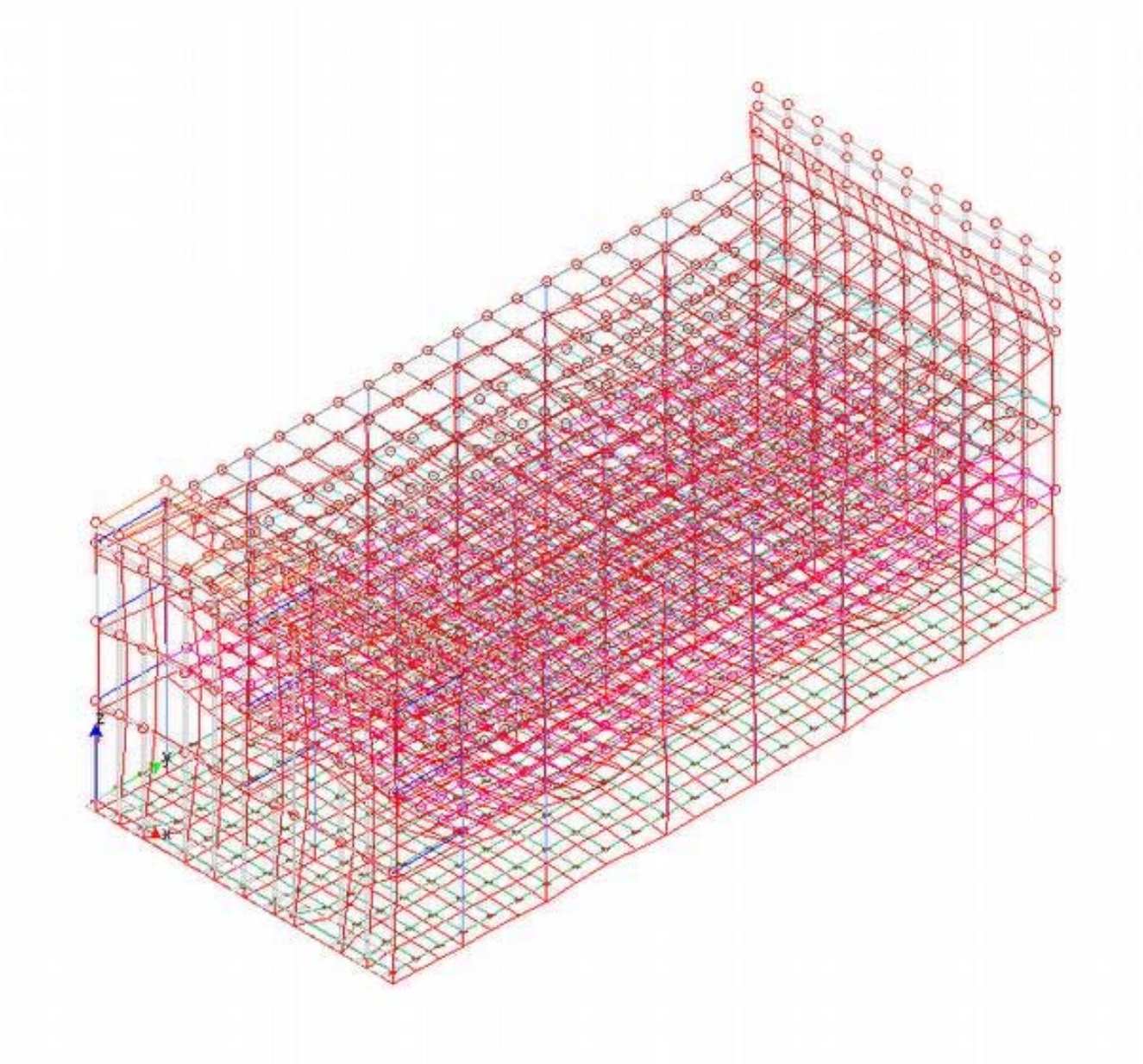
Stralcio 1 – Deformata per Sisma Y+



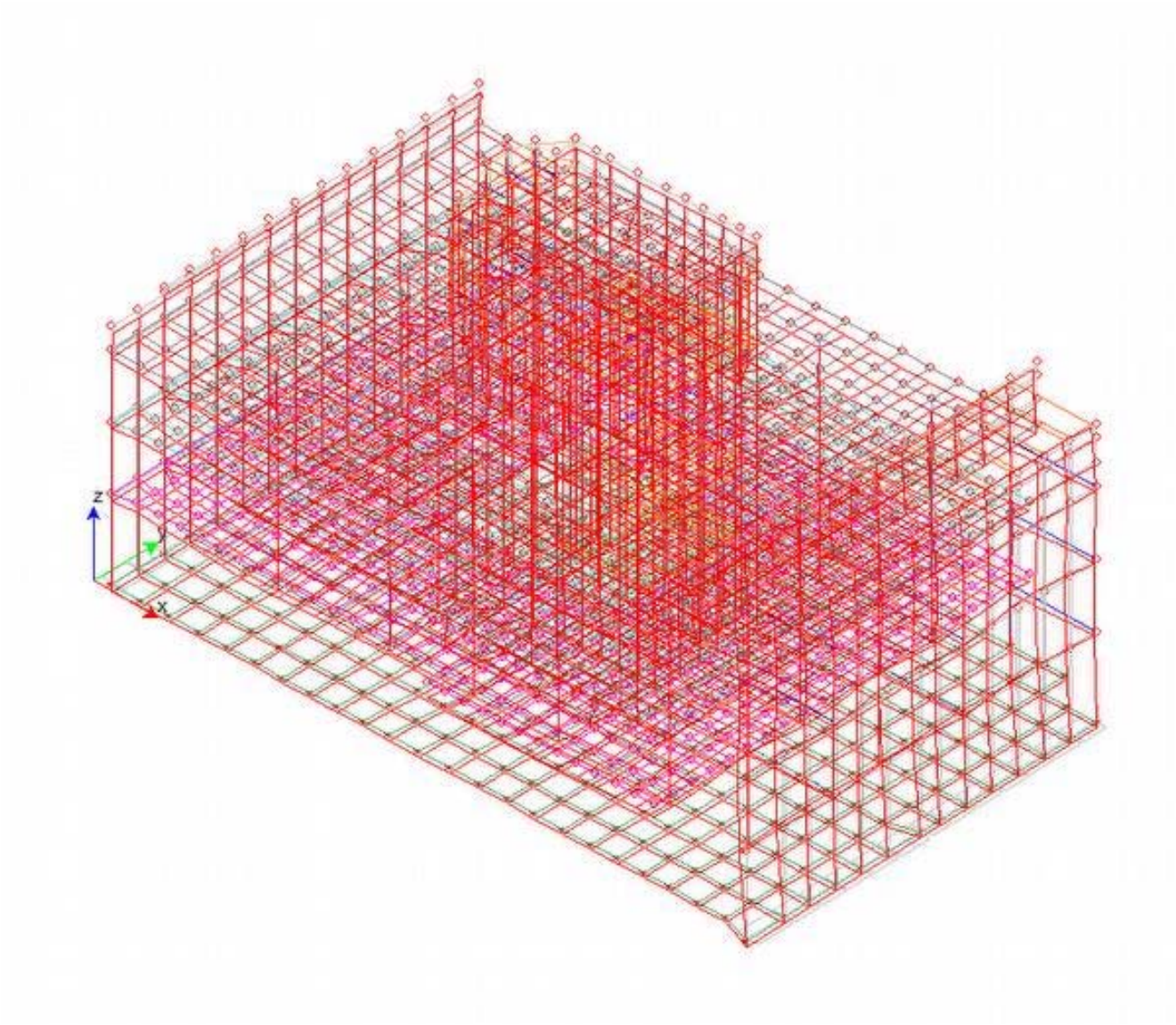
Stralcio 2 – Deformata per Sisma Y+



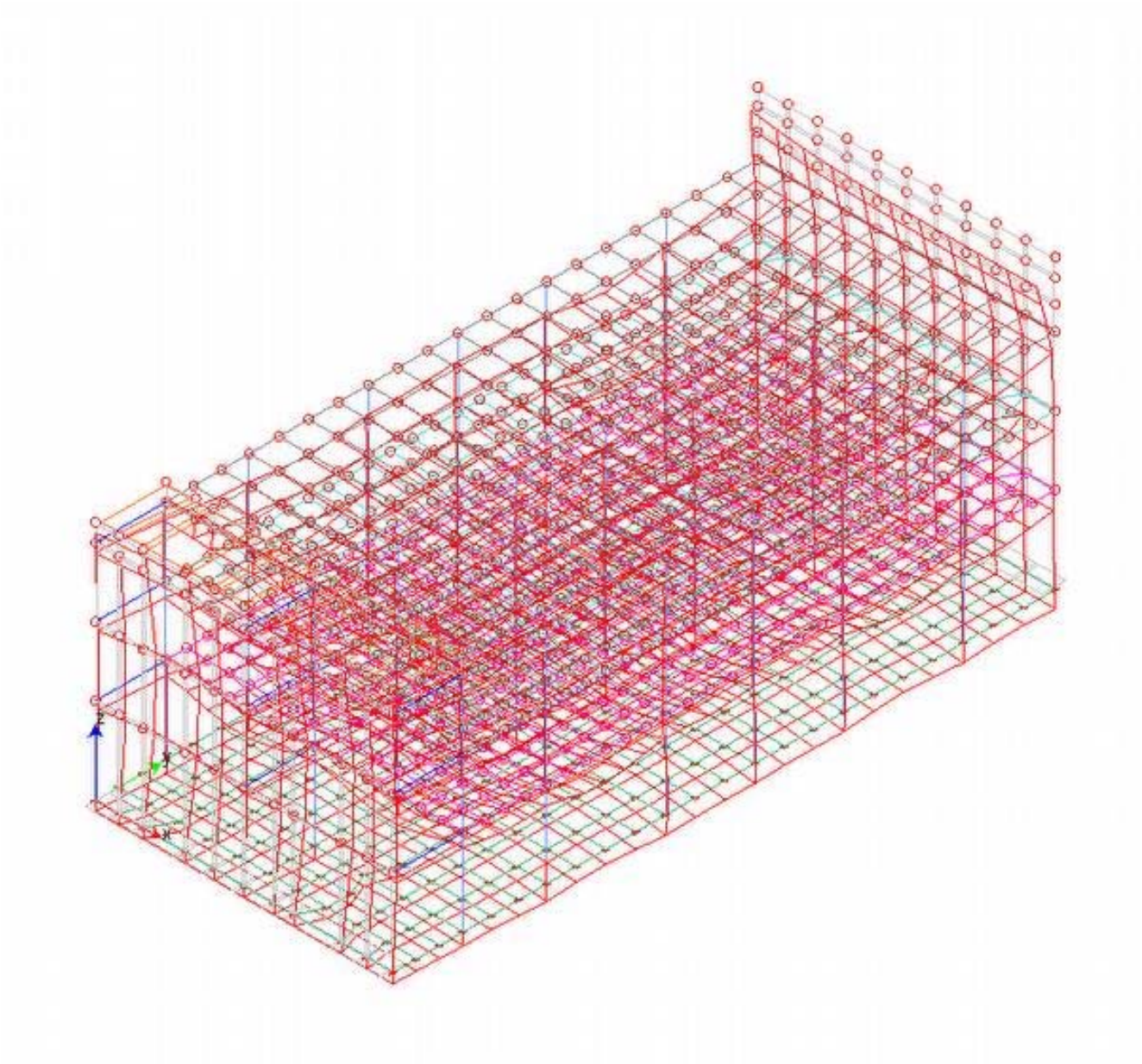
Stralcio 1 – Deformata per Combinazione Rara 1



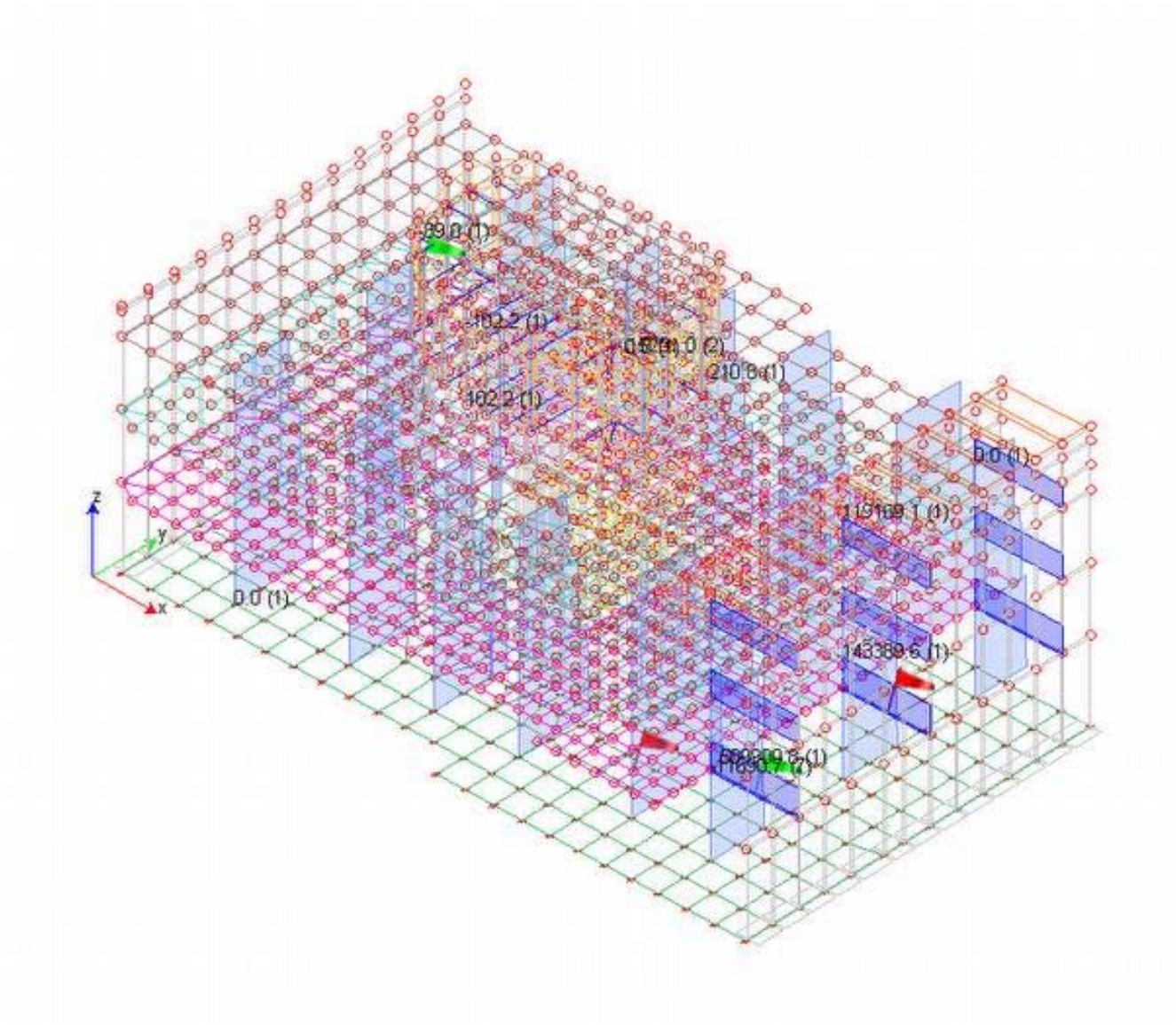
Stralcio 2 – Deformata per Combinazione Rara 1



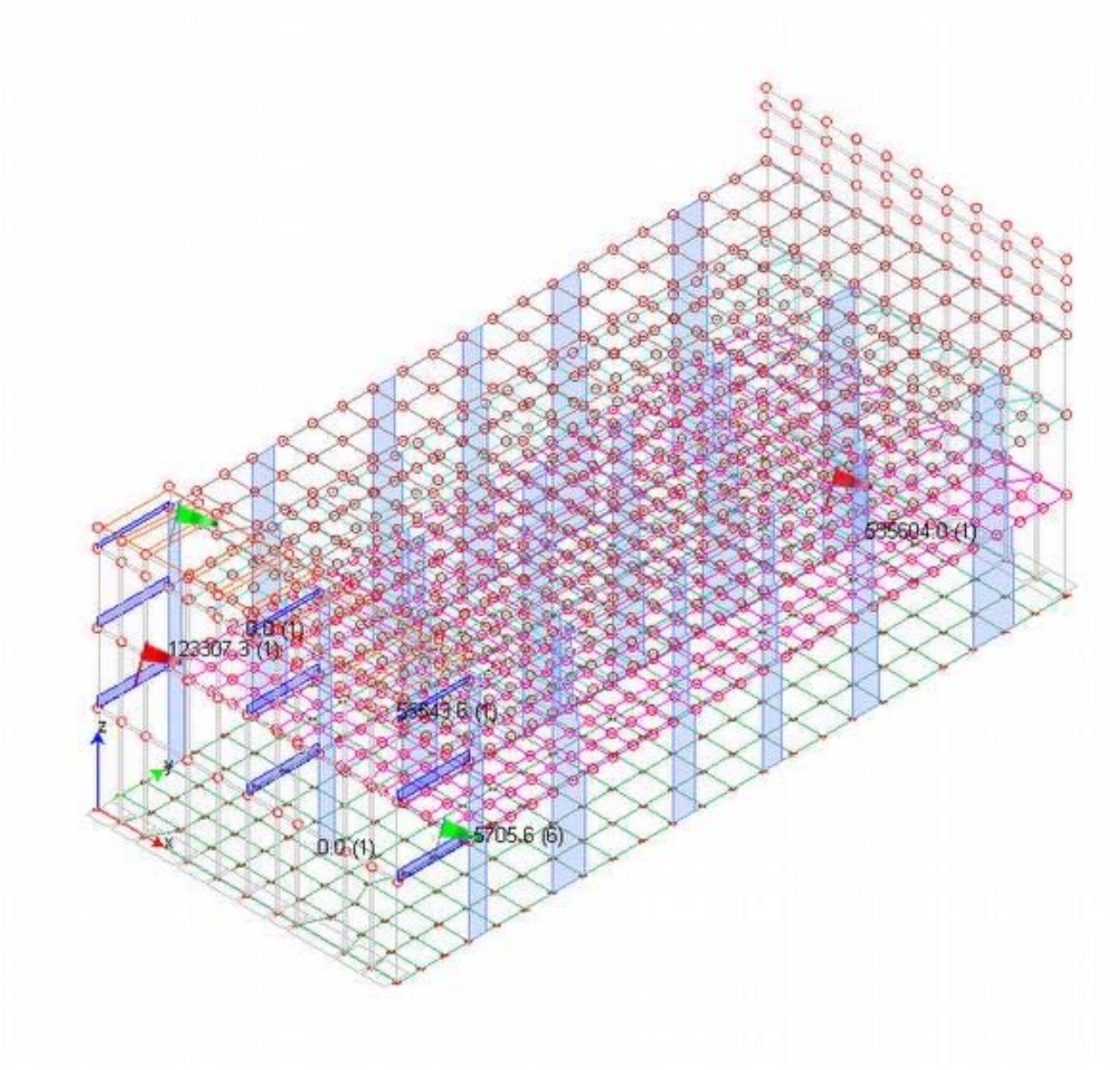
Stralcio 1 – Deformata per Combinazione Rara 2



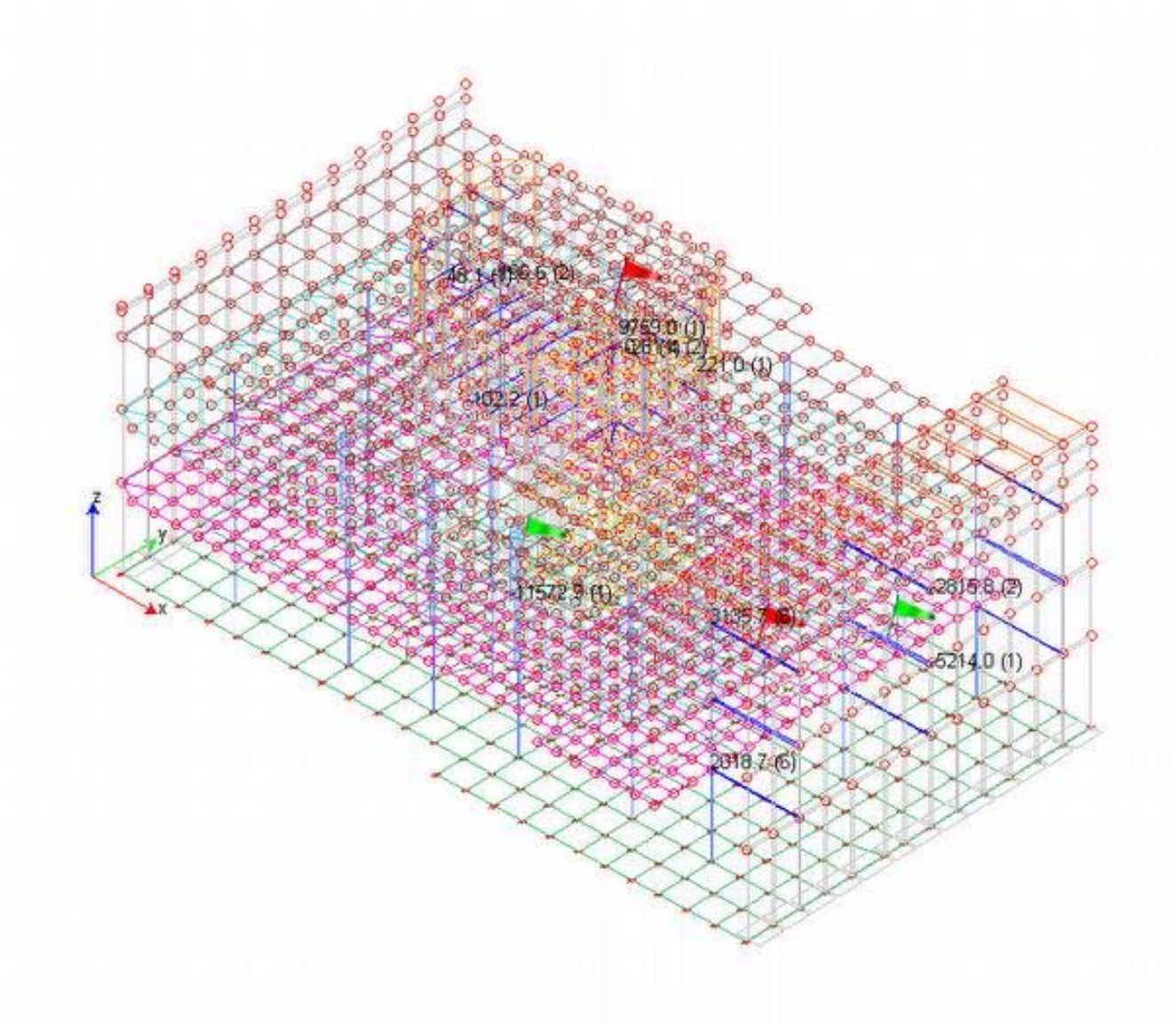
Stralcio 2 – Deformata per Combinazione Rara 2



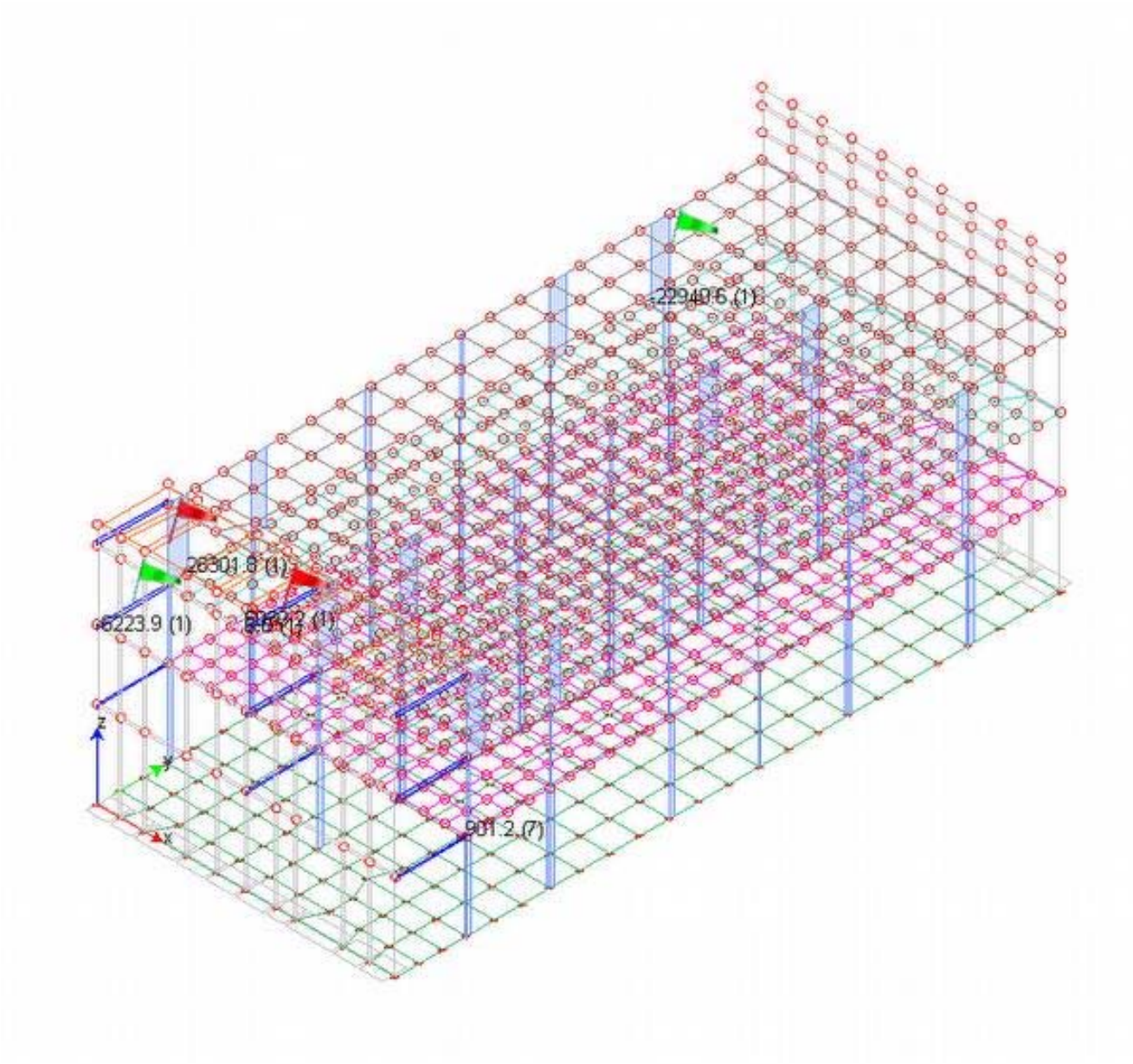
Stralcio 1 - Inviluppo dello Sforzo Normale N



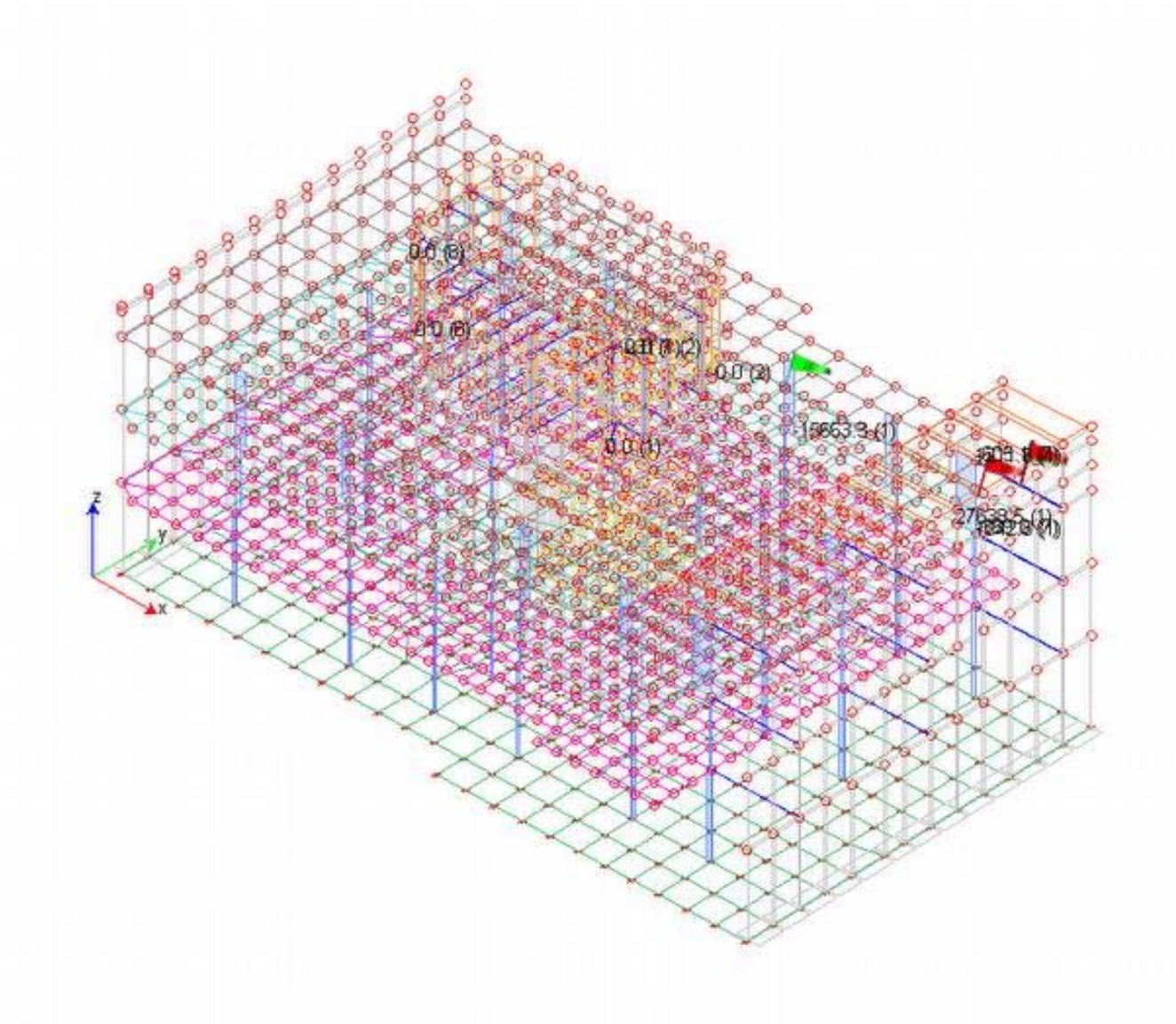
Stralcio 2 - Inviluppo dello Sforzo Normale N



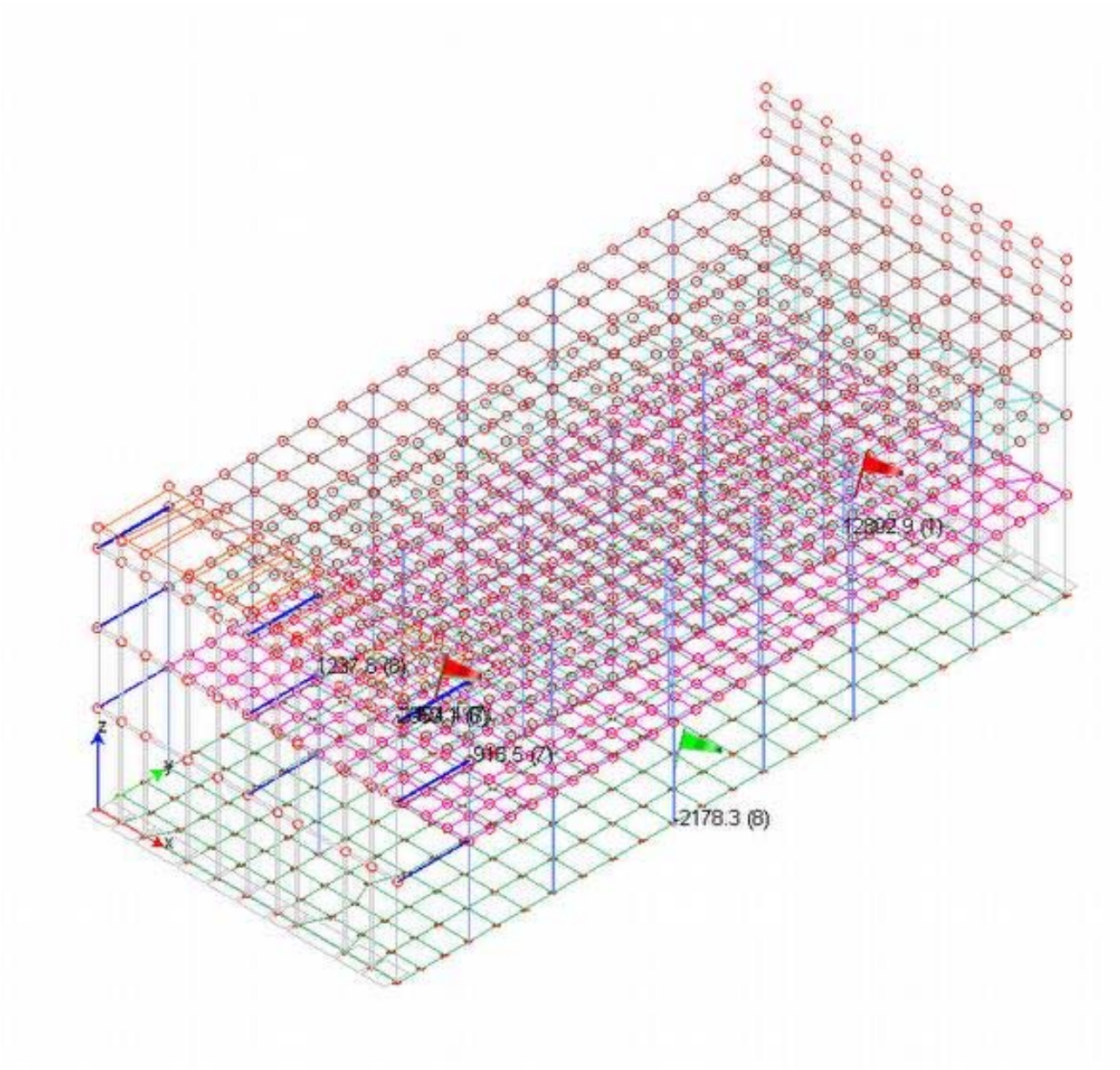
Stralcio 1 - Inviluppo del Taglio T_{12}



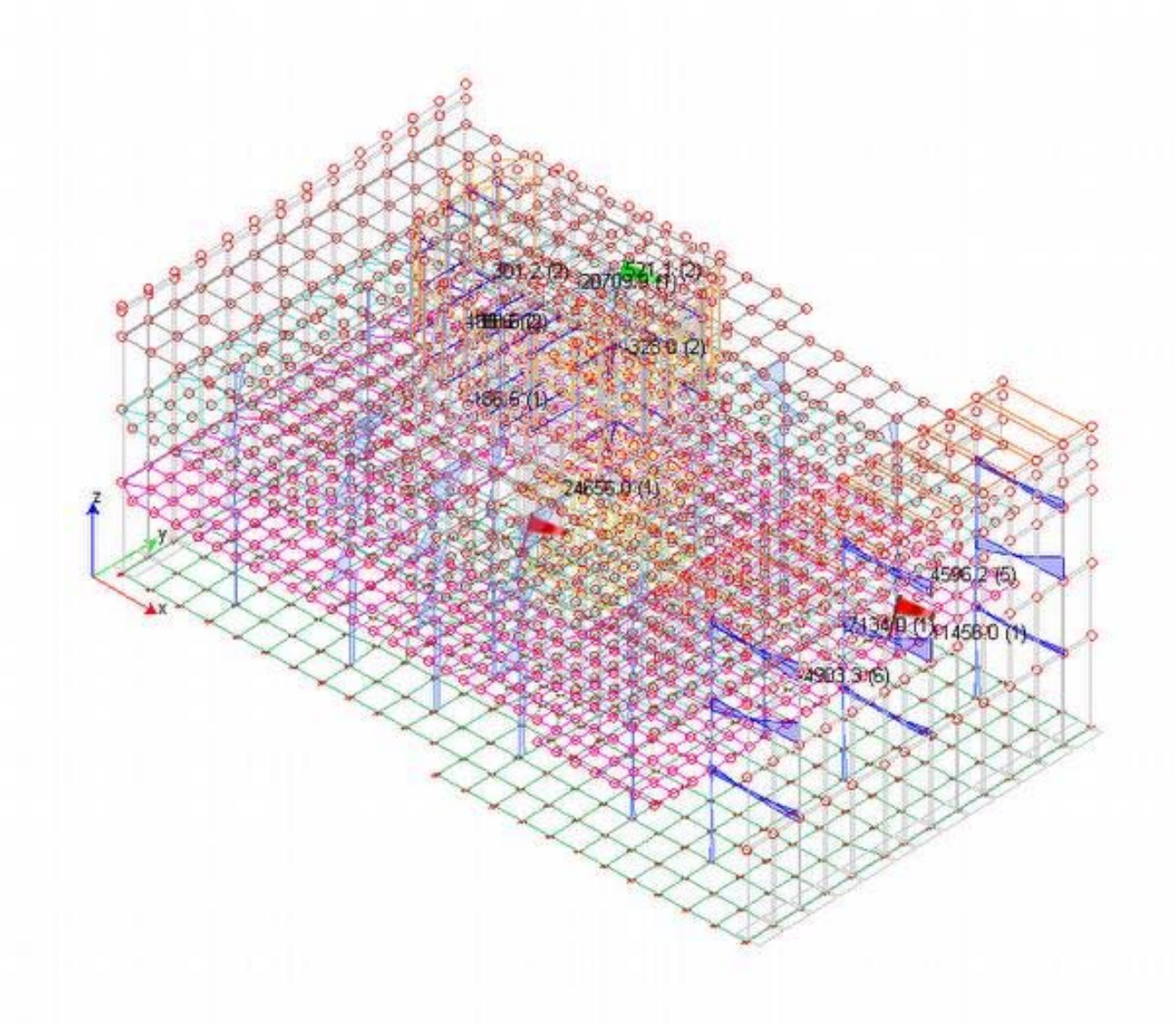
Stralcio 2 - Inviluppo del Taglio T_{12}



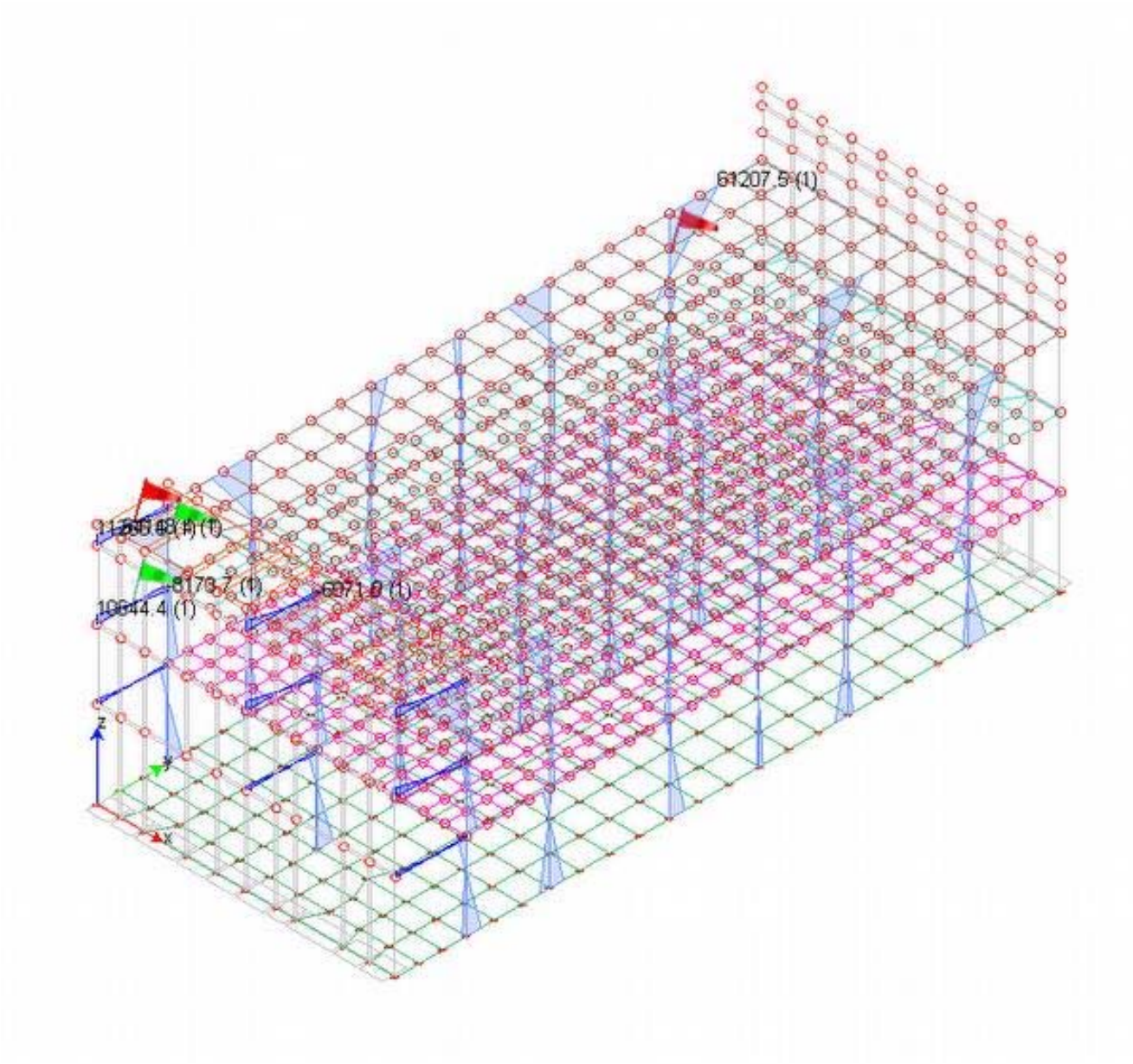
Stralcio 1 - Inviluppo del Taglio T_{13}



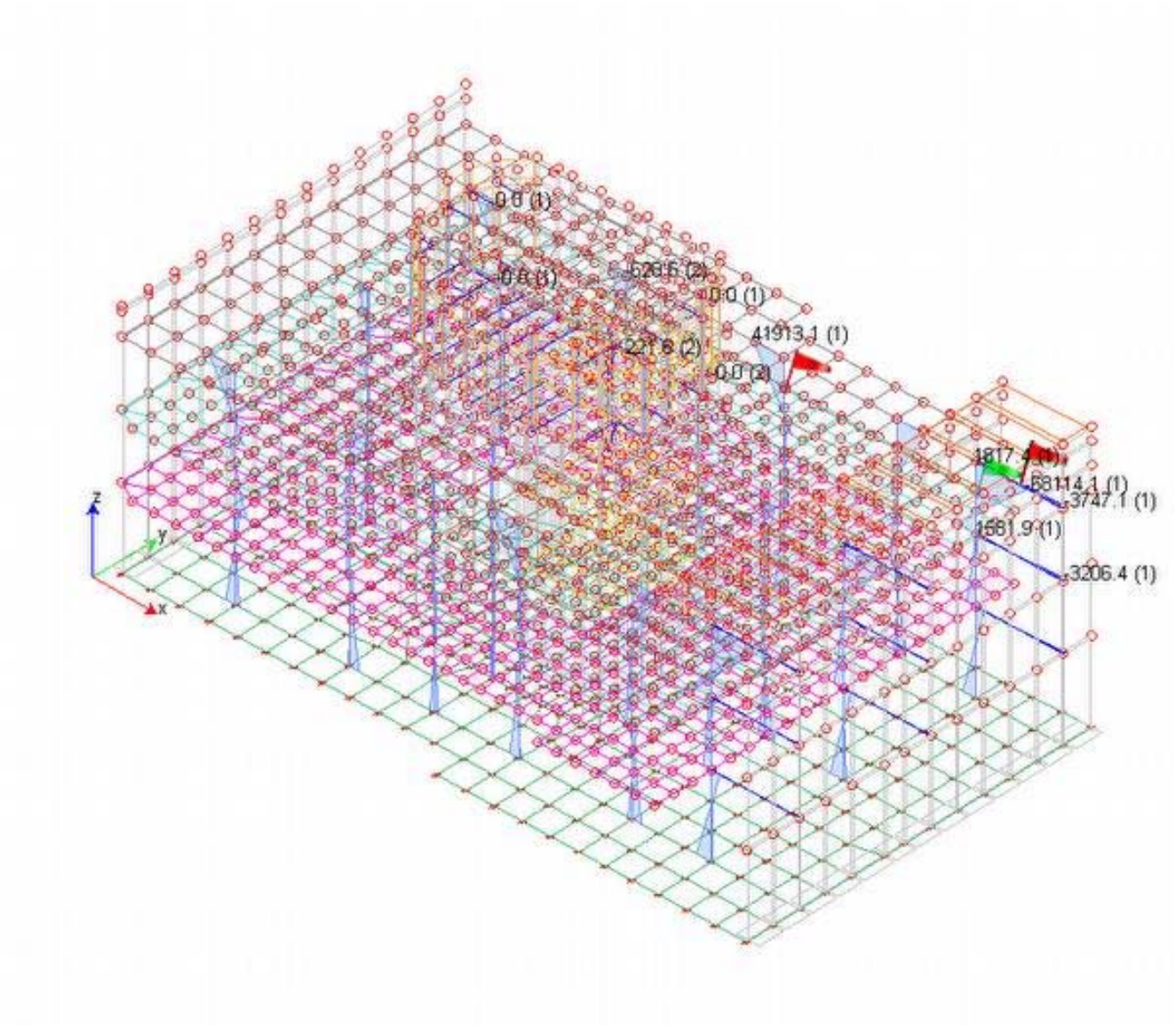
Stralcio 2 - Inviluppo del Taglio T_{13}



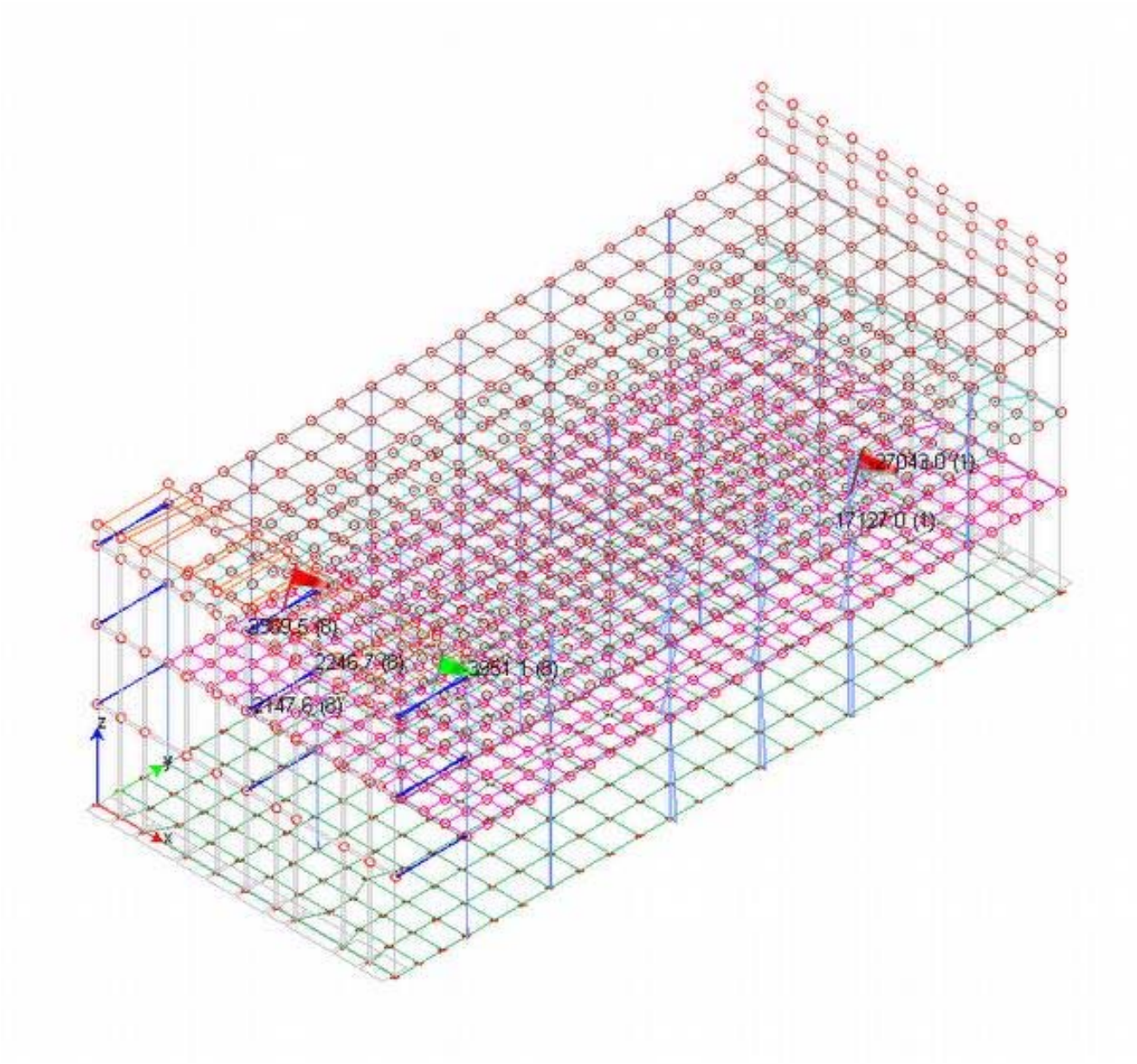
Stralcio 1 - Inviluppo del Momento M_{12}



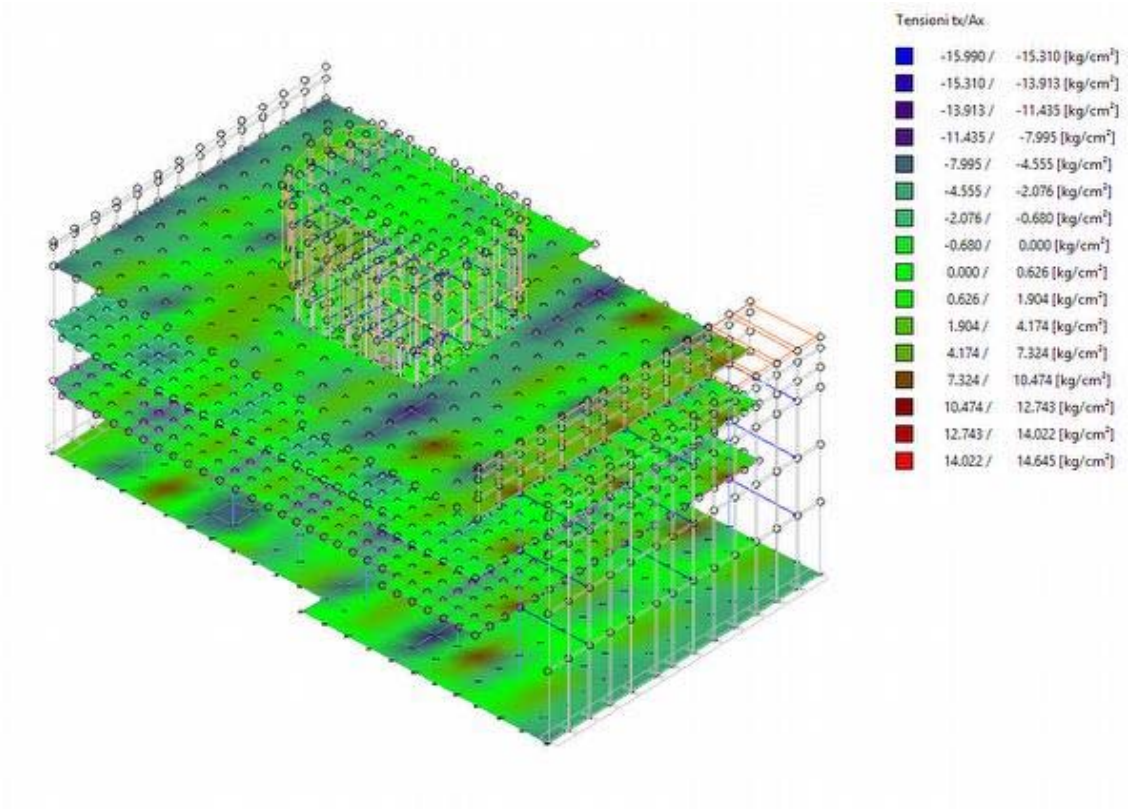
Stralcio 2 - Inviluppo del Momento M_{12}



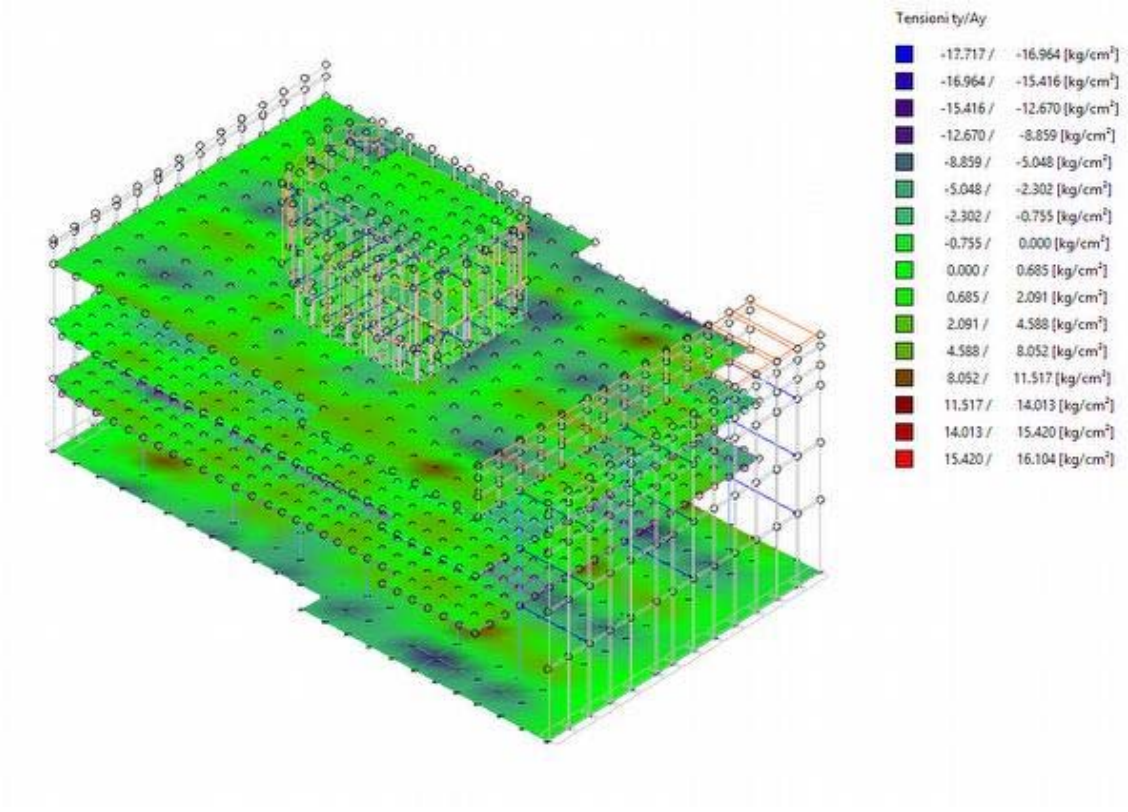
Stralcio 1 - Inviluppo del Momento M_{13}



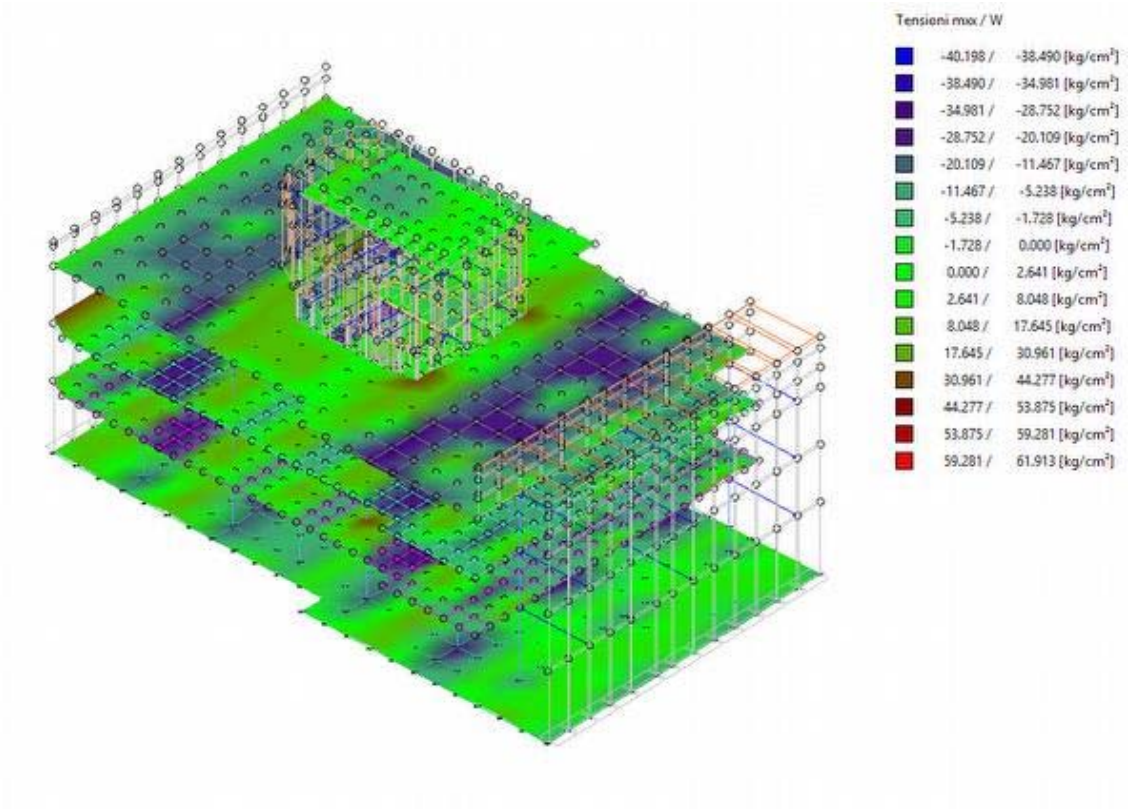
Stralcio 2 - Inviluppo del Momento M_{13}



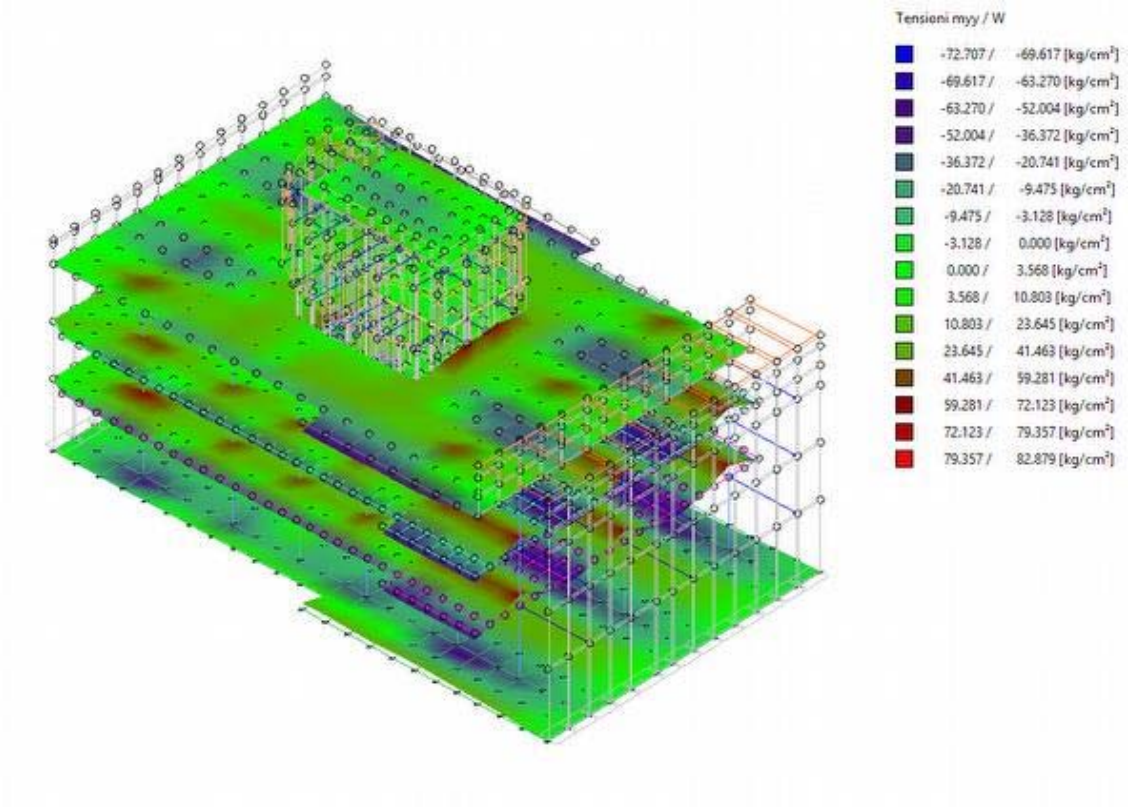
Stralcio 1 - Inviluppo delle tensioni sulle piastre in c.a. dovute al Taglio Tx



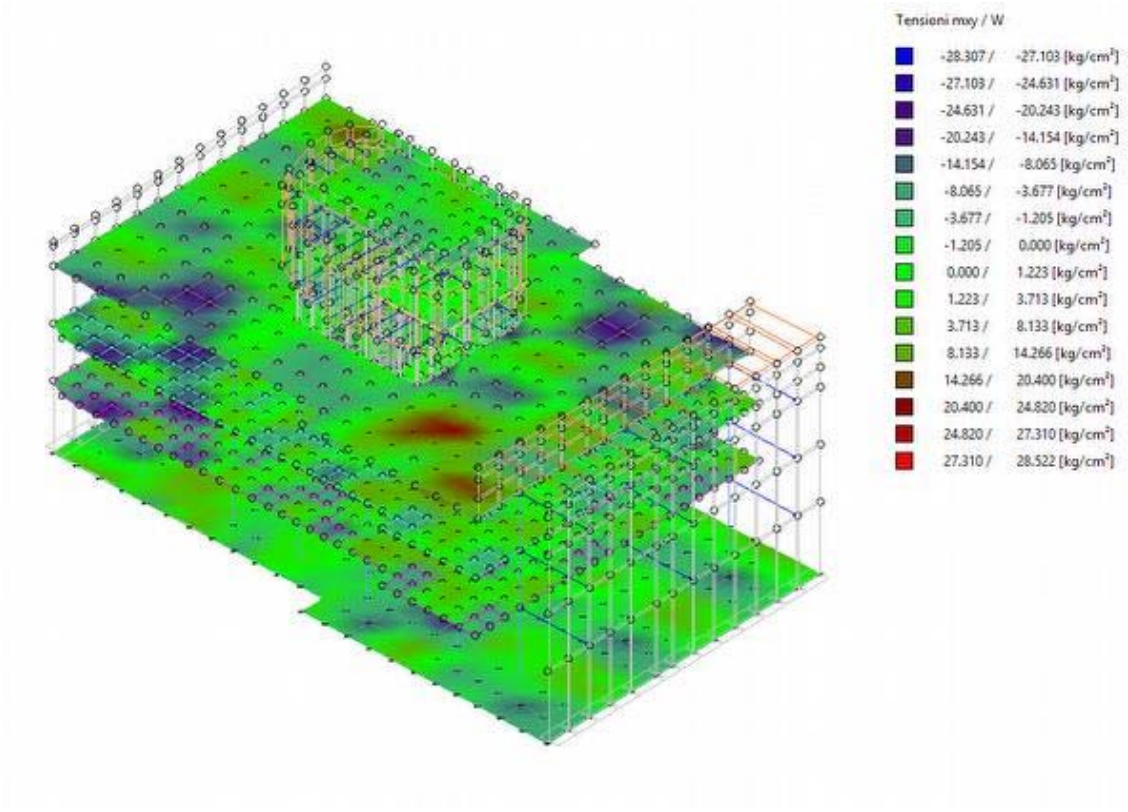
Stralcio 1 - Inviluppo delle tensioni sulle piastre in c.a. dovute al Taglio Ty



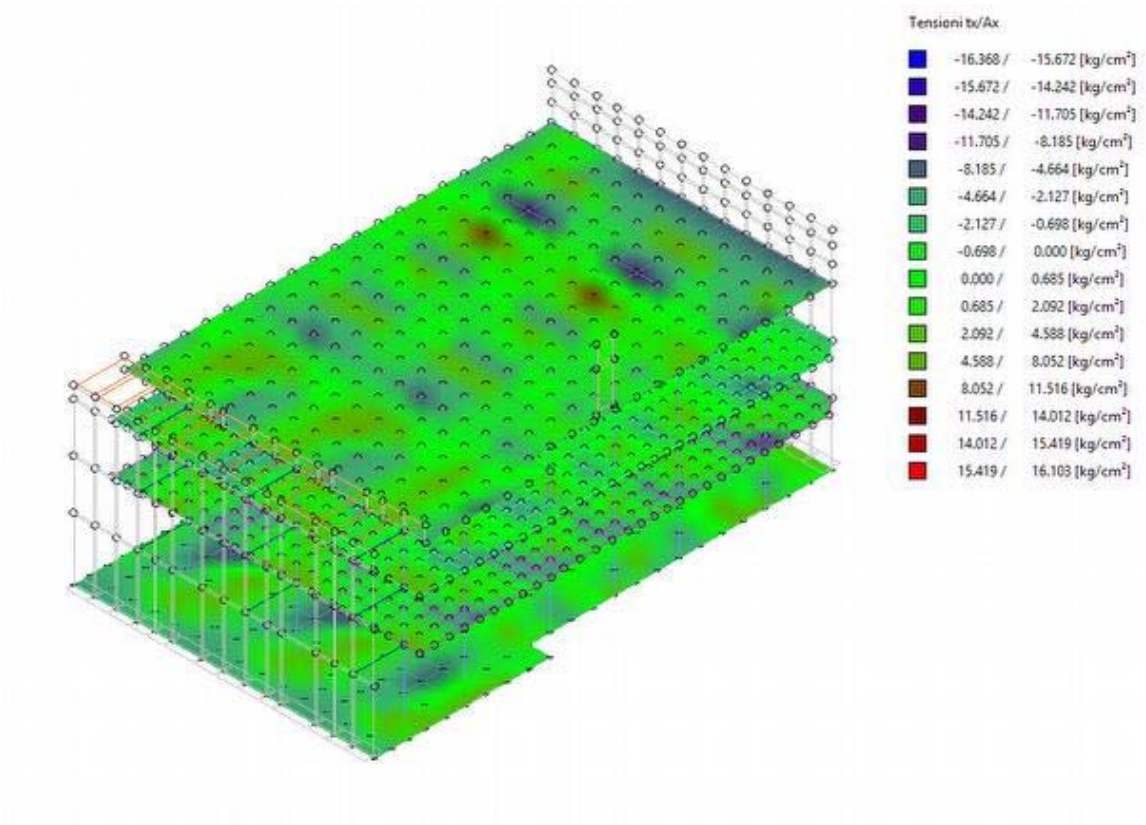
Stralcio 1 - Inviluppo delle tensioni sulle piastre in c.a. dovute ai Momenti Mxx



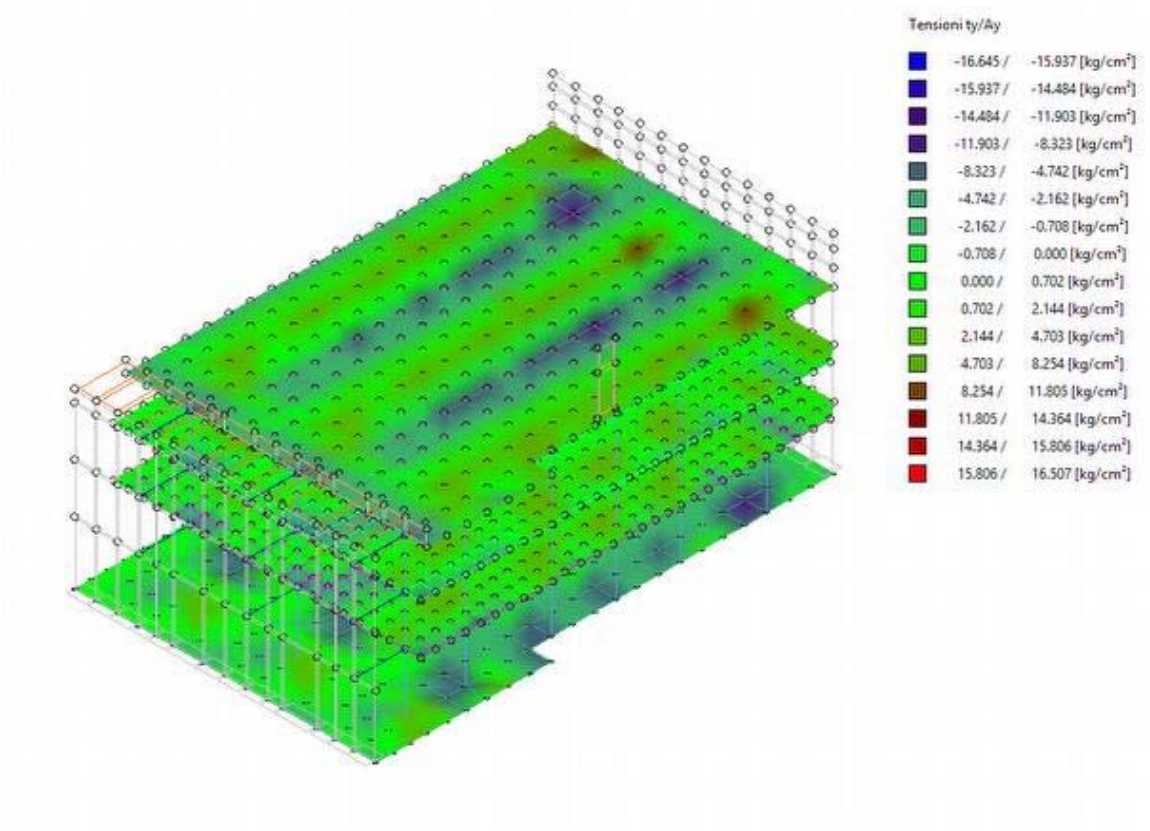
Stralcio 1 - Inviluppo delle tensioni sulle piastre in c.a. dovute ai Momenti Myy



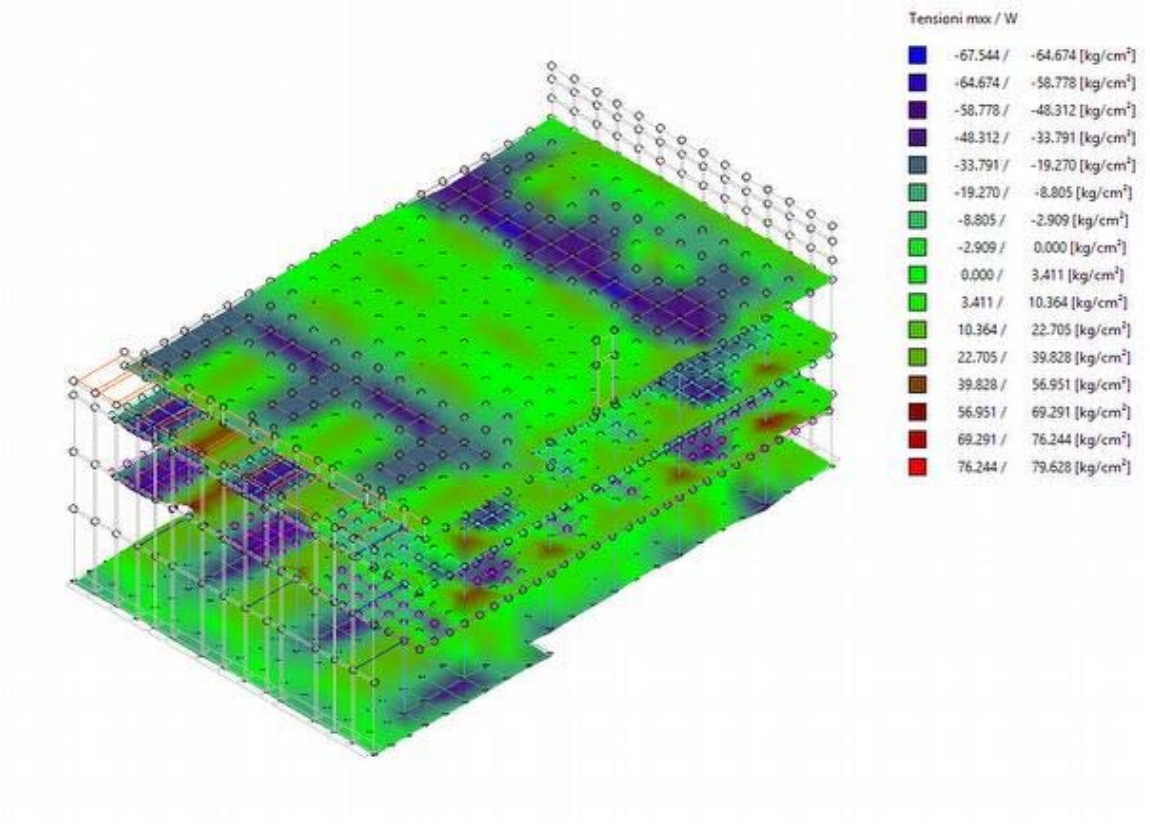
Stralcio 1 - Inviluppo delle tensioni sulle piastre in c.a. dovute ai Momenti Mxy



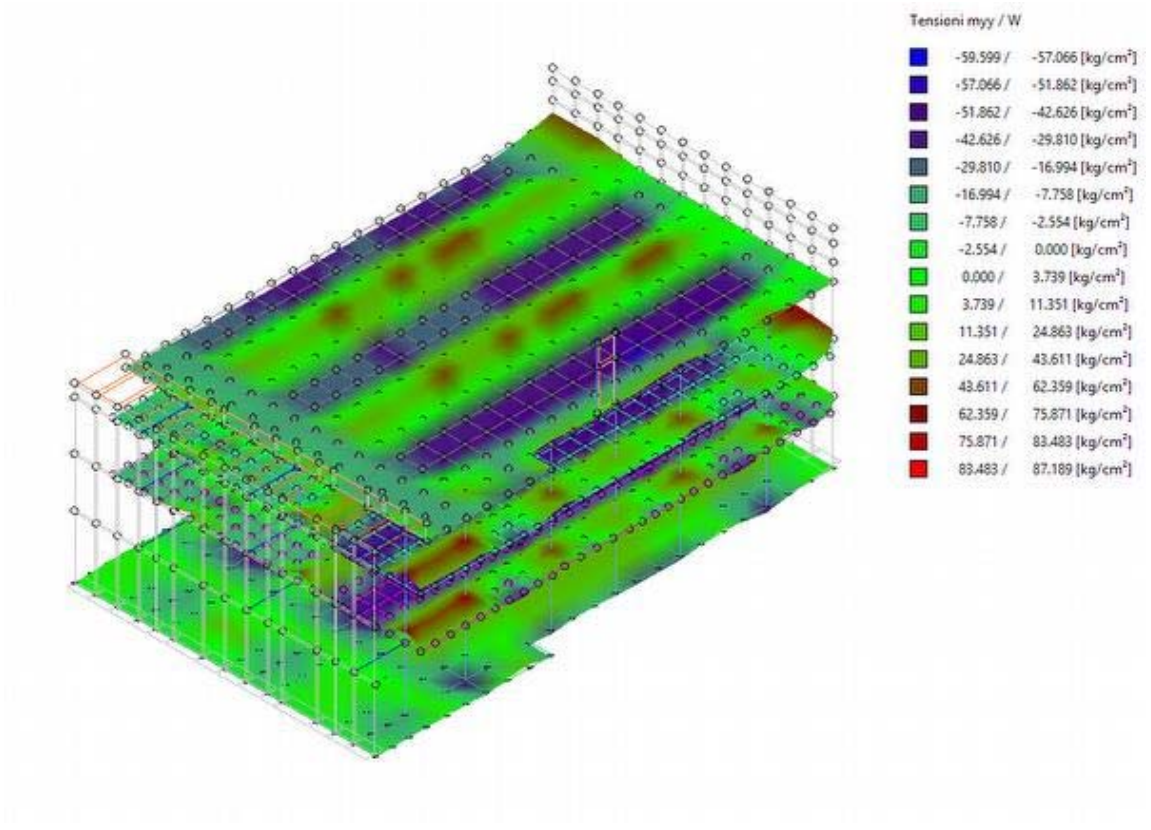
Stralcio 2 - Inviluppo delle tensioni sulle piastre in c.a. dovute al Taglio Tx



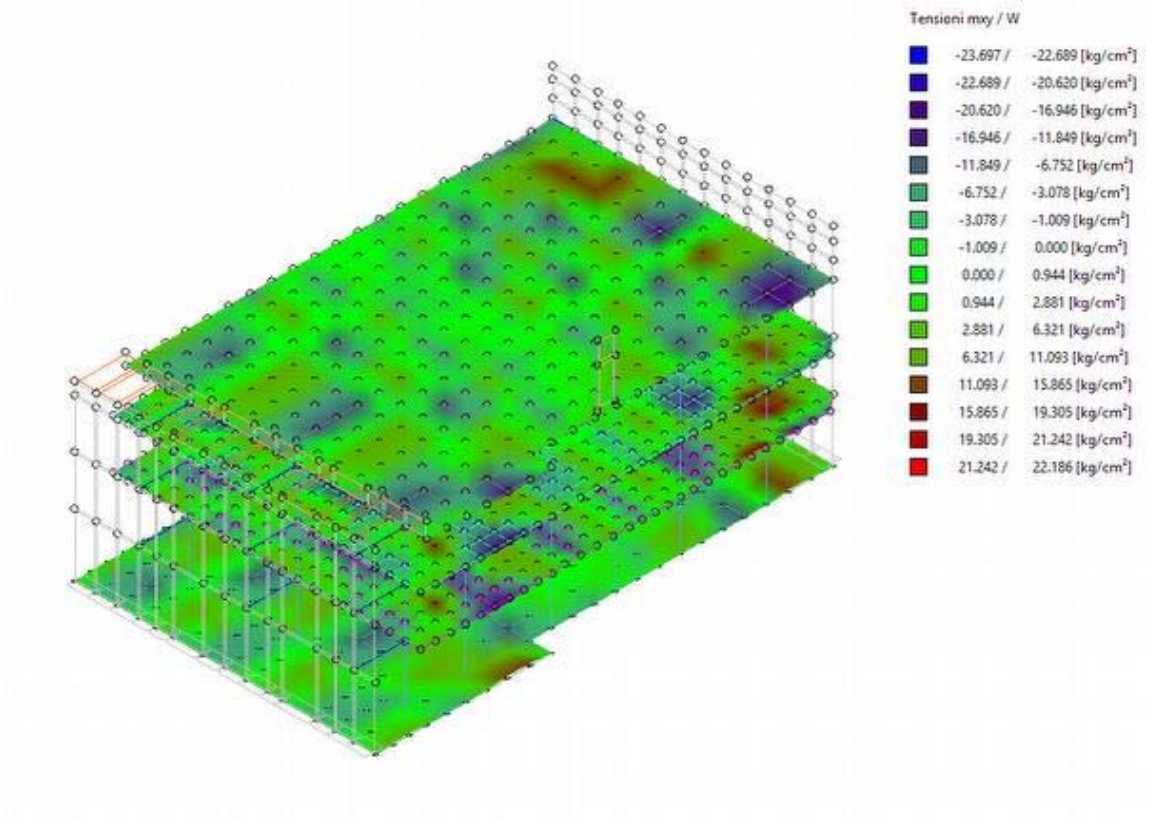
Stralcio 2 - Inviluppo delle tensioni sulle piastre in c.a. dovute al Taglio Ty



Stralcio 2 - Inviluppo delle tensioni sulle piastre in c.a. dovute ai Momenti Mxx



Stralcio 2 - Inviluppo delle tensioni sulle piastre in c.a. dovute ai Momenti Myy



Stralcio 2 - Inviluppo delle tensioni sulle piastre in c.a. dovute ai Momenti Mxy

Verifiche travi

Modalità di verifica
Le travi vengono progettate-verificate a flessione retta e taglio nel piano longitudinale della trave sulla base dell'inviluppo delle sollecitazioni.
Viene comunque sempre predisposta l'armatura minima mentre gli sforzi di taglio vengono integralmente assorbiti dalle staffe.
Le operazioni di progetto-verifica vengono condotte, per ogni asta, in tre diverse sezioni e precisamente in corrispondenza dei fili esterni dei pilastri e della sezione in campata nella quale viene riscontrato il massimo momento positivo (negativo).
I momenti si intendono postivi se tendono le fibre di intradosso (inferiori).
Per quanto concerne il progetto e la verifica delle travi a taglio esse vengono condotte nel modo seguente:
Si controlla se la trave necessita o meno di armatura aggiuntiva a taglio:
Se non occorre armatura aggiuntiva a taglio si procede a disporre la staffatura minima di regolamento e la progettazione ha termine.
Se occorre armatura aggiuntiva a taglio la staffatura viene progettata andando a suddividere la trave, a seconda del caso, in uno, tre o cinque conci:
due tronchi in prossimità degli appoggi di lunghezza pari all'altezza della sezione;
due altri (eventuali) tronchi dall'ascissa precedente a quella in cui il taglio può essere assorbito con la sola staffatura minima da regolamento
un restante (eventuale) concio di chiusura centrale.
In ogni caso l'armatura a taglio si intende simmetrica rispetto alla mezzeria della trave e viene progettata considerando, rispetto alla mezzeria, la zona della trave più sollecitata.
Per quanto concerne le verifiche a taglio esse vengono condotte suddividendo la trave in cinque conci:
due tronchi in prossimità degli appoggi di lunghezza pari all'altezza della sezione; due altri (eventuali) tronchi dall'ascissa precedente a quella in cui il taglio può essere assorbito con la sola staffatura minima da regolamento; il restante (eventuale) concio di chiusura centrale.
L'armatura a taglio si intende simmetrica rispetto alla mezzeria della trave e viene progettata considerando, rispetto alla mezzeria, la zona della trave più sollecitata.
Simbologia utilizzata:
Af Es. Area di ferro all'estradosso
Af In. Area di ferro all'intradosso
Sigb.Es. Tensione del calcestruzzo estradosso
Sigb. In. Tensione del calcestruzzo intradosso
Sigf. Es. Tensione dell'acciaio estradosso
Sigf. In. Tensione dell'acciaio intradosso

Sezioni Impiegate: Trave
Sezioni Nuove

Sez. Num.	Info	Dimensioni	Criterio	Calcestruzzo	γ_M	F.C.	f_{ck} [kg/cm²]	f_{cd} [kg/cm²]	σ_{RARE} [kg/cm²]	σ_{FREQ} [kg/cm²]	σ_{QP} [kg/cm²]	Acciaio	γ_M	F.C.	f_{yk} [kg/cm²]	f_{yd} [kg/cm²]	σ_{yRARE} [kg/cm²]	σ_{yFREQ} [kg/cm²]	σ_{yQP} [kg/cm²]	Cop. Es [cm]	Cop. In [cm]	cotg θ_I	cotg θ
1	Rett.	B 40 [cm] H 40 [cm]	Vertrav	C32/40	1.50	1.00	320.000	181.300	192.000	320.000	144.000	B 450 C	1.15	1.00	4500.000	3913.000	3600.000	4500.000	4500.000	4.00	4.00	2.50	2.50
2	Rett.	B 40 [cm] H 40 [cm]	Vertrav	C32/40	1.50	1.00	320.000	181.300	192.000	320.000	144.000	B 450 C	1.15	1.00	4500.000	3913.000	3600.000	4500.000	4500.000	5.50	5.50	2.50	2.50
3	Rett.	B 30 [cm] H 60 [cm]	Vertrav	C32/40	1.50	1.00	320.000	181.300	192.000	320.000	144.000	B 450 C	1.15	1.00	4500.000	3913.000	3600.000	4500.000	4500.000	4.00	4.00	2.50	2.50
4	Rett.	B 40 [cm] H 60 [cm]	Vertrav	C32/40	1.50	1.00	320.000	181.300	192.000	320.000	144.000	B 450 C	1.15	1.00	4500.000	3913.000	3600.000	4500.000	4500.000	4.00	4.00	2.50	2.50
5	Rett.	B 40 [cm] H 50 [cm]	Vertrav	C32/40	1.50	1.00	320.000	181.300	192.000	320.000	144.000	B 450 C	1.15	1.00	4500.000	3913.000	3600.000	4500.000	4500.000	4.00	4.00	2.50	2.50
6	Rett.	B 30 [cm] H 40 [cm]	Vertrav	C32/40	1.50	1.00	320.000	181.300	192.000	320.000	144.000	B 450 C	1.15	1.00	4500.000	3913.000	3600.000	4500.000	4500.000	5.50	5.50	2.50	2.50
7	Rett.	B 30 [cm] H 80 [cm]	Vertrav	C32/40	1.50	1.00	320.000	181.300	192.000	320.000	144.000	B 450 C	1.15	1.00	4500.000	3913.000	3600.000	4500.000	4500.000	3.50	3.50	1.00	2.50

Verifica a fessurazione diretta (calcolo ampiezza delle fessure)

Elemento	Comb. Rare mm	Comb. Frequenti mm	Comb. Quasi Permanenti mm
Trave	No	0.400	0.300
Trave di Fondazione	No	0.400	0.300

Fattore di sovraresistenza Travi $\gamma_{R,d\ (Nuovo)}$=1.00
Fattore di sovraresistenza delle azioni sulle Fondazioni $\gamma_{R,d\ (Nuovo)}$=1.10

Verifiche Travate :
Travata: *Travata 0 Nodi 378 10463*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
378	0.13	8.04	8.04			528.24	13228.33	0.13	-1034.40	-13228.33	0.13					
				SLE Rare		0.00			-488.54			3.95	0.00	31.45	152.87	
				SLE Freq.		0.00			-429.49			3.47	0.00	27.65	134.39	0.0141
				SLE Q.P.		0.00			-409.74			3.32	0.00	26.38	128.21	0.0134
Camp.	2.33	8.04	8.04	650.00	881.59	174.21	13228.33	0.13	-881.59	-13228.33	0.13					
				SLE Rare		0.00			-678.14			5.49	0.00	43.66	212.20	
				SLE Freq.		0.00			-678.14			5.49	0.00	43.66	212.20	0.0222
				SLE Q.P.		0.00			-678.14			5.49	0.00	43.66	212.20	0.0222
10463	4.53	8.04	8.04			2036.62	13228.33	0.13	-65.37	-13228.33	0.13					
				SLE Rare		1359.89			0.00			0.00	11.00	425.52	87.55	
				SLE Freq.		1293.88			0.00			0.00	10.47	404.87	83.30	0.0087
				SLE Q.P.		1271.83			0.00			0.00	10.29	397.97	81.88	0.0086

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 378 10463 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	1031.88	8701.28	50188.84	61680.39	1321.87	6941.10	4173.10	ø 10 2br. 10.0'
0.63	4.03	3.41	1699.14	8701.28	50188.84	41120.26	1321.87	6941.10	4173.10	ø 10 2br. 15.0'
4.03	4.53	0.50	2024.14	8701.28	50188.84	61680.39	1321.87	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 116 Nodi 11540 11547 11549 11555 11557 11559 11565 11567 11569*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
11540	0.13	12.57	12.57			12138.57	14241.09	0.24	-23.95	-14241.09	0.24					
				SLE Rare		8187.57			-16.22			0.19	93.87	2355.73	539.43	
				SLE Freq.		7725.56			-15.33			0.18	88.57	2222.80	508.99	0.0517
				SLE Q.P.		7610.40			-15.11			0.17	87.25	2189.67	501.40	0.0509
Camp.	0.43	12.57	12.57	4997.74	167.99	12138.57	14241.09	0.24	-157.92	-14241.09	0.24					
				SLE Rare		4914.59			-106.97			1.23	56.34	1414.03	323.79	
				SLE Freq.		4637.65			-101.12			1.16	53.17	1334.35	305.55	0.0310
				SLE Q.P.		4568.74			-99.65			1.14	52.38	1314.52	301.01	0.0306
11547	0.73	12.57	12.57			8579.70	14241.09	0.24	0.00	-14241.09	0.24					
				SLE Rare		1954.76			0.00			0.00	22.41	562.42	128.79	
				SLE Freq.		1845.76			0.00			0.00	21.16	531.06	121.61	0.0123
				SLE Q.P.		1818.82			0.00			0.00	20.85	523.31	119.83	0.0122
Trave Sez. 2 Rett. 40x40 [cm]																
11547	0.00	12.57	12.57			2306.60	14241.09	0.24	-2092.91	-14241.09	0.24					
				SLE Rare		1556.81			0.00			0.00	17.85	447.92	102.57	
				SLE Freq.		1470.37			0.00			0.00	16.86	423.05	96.87	0.0098
				SLE Q.P.		1449.06			0.00			0.00	16.61	416.92	95.47	0.0097
Camp.	0.37	12.57	12.57	4996.07	172.52	2306.60	14241.09	0.24	-5460.83	-14241.09	0.24					
				SLE Rare		0.00			-1296.35			14.86	0.00	85.41	372.99	
				SLE Freq.		0.00			-1221.81			14.01	0.00	80.50	351.54	0.0357
				SLE Q.P.		0.00			-1203.55			13.80	0.00	79.29	346.29	0.0352

11549	0.74	12.57	12.57			0.00	14241.09	0.24	-5460.83	-14241.09	0.24					
				SLE Rare		0.00			-3682.09			42.21	0.00	242.59	1059.41	
				SLE Freq.		0.00			-3472.13			39.81	0.00	228.76	999.00	0.1015
				SLE Q.P.		0.00			-3419.89			39.21	0.00	225.32	983.97	0.0999
Trave Sez. 2 Rett. 40x40 [cm]																
11549	0.00	12.57	12.57			0.00	14241.09	0.24	-8388.16	-14241.09	0.24					
				SLE Rare		0.00			-4012.49			46.00	0.00	264.36	1154.48	
				SLE Freq.		0.00			-3783.86			43.38	0.00	249.30	1088.69	0.1106
				SLE Q.P.		0.00			-3726.97			42.73	0.00	245.55	1072.33	0.1089
Camp.	0.36	12.57	12.57	4996.58	164.01	0.00	14241.09	0.24	-9893.42	-14241.09	0.24					
				SLE Rare		0.00			-5564.29			63.79	0.00	366.60	1600.96	
				SLE Freq.		0.00			-5248.34			60.17	0.00	345.78	1510.05	0.1805
				SLE Q.P.		0.00			-5169.51			59.27	0.00	340.59	1487.37	0.1767
11555	0.72	12.57	12.57			0.00	14241.09	0.24	-9893.42	-14241.09	0.24					
				SLE Rare		0.00			-6671.71			76.49	0.00	439.56	1919.59	
				SLE Freq.		0.00			-6292.75			72.14	0.00	414.59	1810.55	0.2314
				SLE Q.P.		0.00			-6198.05			71.06	0.00	408.35	1783.30	0.2268
Trave Sez. 2 Rett. 40x40 [cm]																
11555	0.00	12.57	12.57			0.00	14241.09	0.24	-10599.28	-14241.09	0.24					
				SLE Rare		0.00			-6815.15			78.13	0.00	449.01	1960.86	
				SLE Freq.		0.00			-6428.15			73.69	0.00	423.51	1849.51	0.2380
				SLE Q.P.		0.00			-6331.46			72.59	0.00	417.14	1821.69	0.2333
Camp.	0.37	12.57	12.57	4996.72	170.45	0.00	14241.09	0.24	-10608.80	-14241.09	0.24					
				SLE Rare		0.00			-7144.98			81.91	0.00	470.74	2055.76	
				SLE Freq.		0.00			-6739.95			77.27	0.00	444.05	1939.22	0.2532
				SLE Q.P.		0.00			-6638.63			76.11	0.00	437.38	1910.07	0.2482
11557	0.74	12.57	12.57			0.00	14241.09	0.24	-10608.80	-14241.09	0.24					
				SLE Rare		0.00			-7012.99			80.40	0.00	462.04	2017.78	
				SLE Freq.		0.00			-6615.19			75.84	0.00	435.83	1903.33	0.2471
				SLE Q.P.		0.00			-6515.63			74.70	0.00	429.28	1874.68	0.2422
Trave Sez. 2 Rett. 40x40 [cm]																
11557	0.00	12.57	12.57			0.00	14241.09	0.24	-10216.82	-14241.09	0.24					
				SLE Rare		0.00			-6890.18			78.99	0.00	453.95	1982.44	
				SLE Freq.		0.00			-6499.44			74.51	0.00	428.21	1870.02	0.2414
				SLE Q.P.		0.00			-6401.68			73.39	0.00	421.77	1841.89	0.2367
Camp.	0.37	12.57	12.57	4999.67	170.55	0.00	14241.09	0.24	-10216.82	-14241.09	0.24					
				SLE Rare		0.00			-5964.16			68.38	0.00	392.94	1716.01	
				SLE Freq.		0.00			-5626.51			64.50	0.00	370.70	1618.86	0.1989
				SLE Q.P.		0.00			-5542.04			63.54	0.00	365.13	1594.56	0.1948
11559	0.74	12.57	12.57			0.00	14241.09	0.24	-8927.73	-14241.09	0.24					
				SLE Rare		0.00			-4576.06			52.46	0.00	301.49	1316.63	
				SLE Freq.		0.00			-4316.76			49.49	0.00	284.41	1242.02	0.1351
				SLE Q.P.		0.00			-4251.90			48.75	0.00	280.13	1223.36	0.1320
Trave Sez. 2 Rett. 40x40 [cm]																
11559	0.00	12.57	12.57			0.00	14241.09	0.24	-6261.24	-14241.09	0.24					
				SLE Rare		0.00			-4222.53			48.41	0.00	278.20	1214.91	
				SLE Freq.		0.00			-3983.38			45.67	0.00	262.44	1146.10	0.1189
				SLE Q.P.		0.00			-3923.60			44.98	0.00	258.50	1128.90	0.1160
Camp.	0.36	13.03	12.57	4994.48	163.94	730.44	14699.60	0.24	-6261.24	-14240.66	0.24					
				SLE Rare		0.00			-2086.87			23.82	0.00	136.20	600.69	
				SLE Freq.		0.00			-1969.29			22.48	0.00	128.53	566.84	0.0576
				SLE Q.P.		0.00			-1939.93			22.14	0.00	126.61	558.39	0.0567
11565	0.72	15.86	12.57			730.44	17497.15	0.26	-3339.80	-14238.39	0.24					
				SLE Rare		492.98			0.00			0.00	5.20	113.59	33.81	
				SLE Freq.		464.69			0.00			0.00	4.90	107.07	31.87	0.0027

				SLE Q.P.		458.24			0.00			0.00	4.84	105.59	31.43	0.0027
Trave Sez. 2 Rett. 40x40 [cm]																
11565	0.00	16.77	12.57			6688.88	18388.04	0.27	0.00	-14237.77	0.24					
				SLE Rare		894.27			0.00			0.00	9.26	195.42	61.76	
				SLE Freq.		843.14			0.00			0.00	8.73	184.25	58.23	0.0048
				SLE Q.P.		830.92			0.00			0.00	8.60	181.58	57.38	0.0047
Camp.	0.37	19.69	12.57	4999.35	172.63	12255.46	21233.54	0.30	-172.63	-14236.05	0.24					
				SLE Rare		4346.14			-116.93			1.26	42.72	815.23	304.76	
				SLE Freq.		4098.82			-110.54			1.19	40.29	768.84	287.41	0.0211
				SLE Q.P.		4037.67			-108.94			1.17	39.69	757.37	283.13	0.0208
11567	0.74	22.60	12.57			12255.46	24040.54	0.32	0.00	-14234.67	0.24					
				SLE Rare		8265.74			0.00			0.00	77.85	1359.50	584.59	
				SLE Freq.		7796.64			0.00			0.00	73.44	1282.35	551.42	0.0371
				SLE Q.P.		7680.18			0.00			0.00	72.34	1263.19	543.18	0.0365
Trave Sez. 2 Rett. 40x40 [cm]																
11567	0.00	23.51	12.57			19947.44	24903.62	0.33	0.00	-14234.29	0.24					
				SLE Rare		8512.89			0.00			0.00	79.25	1348.77	603.15	
				SLE Freq.		8029.70			0.00			0.00	74.75	1272.22	568.92	0.0373
				SLE Q.P.		7909.62			0.00			0.00	73.63	1253.19	560.41	0.0367
Camp.	0.30	25.13	12.57	4996.28	167.94	24438.07	26433.75	0.35	-157.88	-14233.66	0.24					
				SLE Rare		12340.72			-106.94			1.11	112.67	1835.21	876.51	
				SLE Freq.		11640.14			-101.09			1.05	106.27	1731.02	826.75	0.0527
				SLE Q.P.		11465.81			-99.63			1.03	104.68	1705.10	814.37	0.0514
11569	0.61	25.13	12.57			24438.07	26433.75	0.35	-23.94	-14233.66	0.24					
				SLE Rare		16481.61			-16.21			0.17	150.47	2451.01	1170.62	
				SLE Freq.		15546.50			-15.33			0.16	141.94	2311.95	1104.21	0.0818
				SLE Q.P.		15313.65			-15.11			0.16	139.81	2277.32	1087.67	0.0800

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 11540 11547 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	16711.12	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11547 11549 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	12306.51	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11549 11555 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7251.09	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11555 11557 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	2242.24	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11557 11559 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	6491.14	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11559 11565 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	11457.45	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11565 11567 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	16562.29	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11567 11569 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	20941.92	8810.34	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 117 Nodi 11526 11528 11529 11532 11533 11534*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
11526	0.12	12.57	12.57			12102.91	14241.09	0.24	-23.94	-14241.09	0.24					
				SLE Rare		8161.85			-16.21			0.19	93.57	2348.33	537.74	
				SLE Freq.		7699.55			-15.33			0.18	88.27	2215.31	507.28	0.0515
				SLE Q.P.		7585.84			-15.11			0.17	86.97	2182.60	499.78	0.0508
Camp.	0.43	12.57	12.57	4996.28	167.94	12102.91	14241.09	0.24	-157.88	-14241.09	0.24					
				SLE Rare		4894.57			-106.94			1.23	56.11	1408.27	322.47	

				SLE Freq.		4617.27			-101.09			1.16	52.93	1328.48	304.20	0.0309
				SLE Q.P.		4549.58			-99.63			1.14	52.16	1309.00	299.74	0.0304
11528	0.73	12.57	12.57			8549.92	14241.09	0.24	0.00	-14241.09	0.24					
				SLE Rare		1940.33			0.00			0.00	22.24	558.27	127.84	
				SLE Freq.		1830.92			0.00			0.00	20.99	526.79	120.63	0.0123
				SLE Q.P.		1804.96			0.00			0.00	20.69	519.32	118.92	0.0121
Trave Sez. 2 Rett. 40x40 [cm]																
11528	0.00	12.57	12.57			2280.01	14241.09	0.24	-2118.55	-14241.09	0.24					
				SLE Rare		1537.53			0.00			0.00	17.63	442.38	101.30	
				SLE Freq.		1450.76			0.00			0.00	16.63	417.41	95.58	0.0097
				SLE Q.P.		1430.58			0.00			0.00	16.40	411.61	94.25	0.0096
Camp.	0.37	12.57	12.57	4999.34	172.63	2280.01	14241.09	0.24	-5485.18	-14241.09	0.24					
				SLE Rare		0.00			-1314.68			15.07	0.00	86.62	378.26	
				SLE Freq.		0.00			-1240.16			14.22	0.00	81.71	356.82	0.0362
				SLE Q.P.		0.00			-1221.18			14.00	0.00	80.46	351.36	0.0357
11529	0.74	12.57	12.57			0.00	14241.09	0.24	-5485.18	-14241.09	0.24					
				SLE Rare		0.00			-3699.16			42.41	0.00	243.72	1064.33	
				SLE Freq.		0.00			-3488.94			40.00	0.00	229.87	1003.84	0.1019
				SLE Q.P.		0.00			-3436.07			39.39	0.00	226.38	988.63	0.1004
Trave Sez. 2 Rett. 40x40 [cm]																
11529	0.00	12.57	12.57			0.00	14241.09	0.24	-8398.26	-14241.09	0.24					
				SLE Rare		0.00			-4033.35			46.24	0.00	265.73	1160.48	
				SLE Freq.		0.00			-3804.38			43.61	0.00	250.65	1094.60	0.1112
				SLE Q.P.		0.00			-3746.85			42.96	0.00	246.86	1078.05	0.1095
Camp.	0.36	12.57	12.57	4994.49	163.94	0.00	14241.09	0.24	-9886.67	-14241.09	0.24					
				SLE Rare		0.00			-5572.51			63.89	0.00	367.14	1603.33	
				SLE Freq.		0.00			-5256.66			60.26	0.00	346.33	1512.45	0.1809
				SLE Q.P.		0.00			-5177.44			59.36	0.00	341.11	1489.66	0.1771
11532	0.72	12.57	12.57			0.00	14241.09	0.24	-9886.67	-14241.09	0.24					
				SLE Rare		0.00			-6667.49			76.44	0.00	439.28	1918.37	
				SLE Freq.		0.00			-6289.04			72.10	0.00	414.35	1809.48	0.2312
				SLE Q.P.		0.00			-6194.20			71.01	0.00	408.10	1782.20	0.2266
Trave Sez. 2 Rett. 40x40 [cm]																
11532	0.00	12.57	12.57			0.00	14241.09	0.24	-10594.36	-14241.09	0.24					
				SLE Rare		0.00			-6814.67			78.13	0.00	448.98	1960.72	
				SLE Freq.		0.00			-6428.09			73.69	0.00	423.51	1849.49	0.2380
				SLE Q.P.		0.00			-6331.27			72.58	0.00	417.13	1821.64	0.2332
Camp.	0.37	12.57	12.57	4999.67	170.55	0.00	14241.09	0.24	-10603.40	-14241.09	0.24					
				SLE Rare		0.00			-7141.87			81.88	0.00	470.53	2054.86	
				SLE Freq.		0.00			-6737.06			77.24	0.00	443.86	1938.39	0.2530
				SLE Q.P.		0.00			-6635.72			76.07	0.00	437.19	1909.23	0.2481
11533	0.74	12.57	12.57			0.00	14241.09	0.24	-10603.40	-14241.09	0.24					
				SLE Rare		0.00			-7006.99			80.33	0.00	461.65	2016.05	
				SLE Freq.		0.00			-6609.23			75.77	0.00	435.44	1901.61	0.2468
				SLE Q.P.		0.00			-6509.93			74.63	0.00	428.90	1873.04	0.2419
Trave Sez. 2 Rett. 40x40 [cm]																
11533	0.00	12.57	12.57			0.00	14241.09	0.24	-10213.63	-14241.09	0.24					
				SLE Rare		0.00			-6887.86			78.96	0.00	453.80	1981.78	
				SLE Freq.		0.00			-6497.08			74.48	0.00	428.05	1869.34	0.2413
				SLE Q.P.		0.00			-6399.50			73.37	0.00	421.62	1841.27	0.2366
Camp.	0.34	12.57	12.57	4996.72	170.45	0.00	14241.09	0.24	-10213.63	-14241.09	0.24					
				SLE Rare		0.00			-6036.02			69.20	0.00	397.68	1736.69	
				SLE Freq.		0.00			-5693.78			65.28	0.00	375.13	1638.22	0.2022
				SLE Q.P.		0.00			-5608.61			64.30	0.00	369.52	1613.71	0.1981
11534	0.69	12.57	12.57			0.00	14241.09	0.24	-9142.00	-14241.09	0.24					

			SLE Rare	0.00			-4783.00			54.83	0.00	315.12	1376.17	
			SLE Freq.	0.00			-4511.25			51.72	0.00	297.22	1297.98	0.1446
			SLE Q.P.	0.00			-4443.97			50.95	0.00	292.79	1278.62	0.1413

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	Staffe
Trave 11526 11528 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	16684.32	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11528 11529 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	12304.70	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11529 11532 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7199.86	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11532 11533 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	2233.55	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11533 11534 Sez. 2 Rett. 40x40 [cm]							
0.00	0.69	0.69	6250.06	8810.34	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 120 Nodi 11534 11537 11538 11541 11548 11550 11556 11558 11560 11566 11568 11569*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
11534	0.05	12.57	12.57			0.00	14241.09	0.24	-5855.40	-14241.09	0.24					
				SLE Rare		0.00			-3948.30			45.26	0.00	260.13	1136.01	
				SLE Freq.		0.00			-3724.06			42.69	0.00	245.36	1071.49	0.1088
				SLE Q.P.		0.00			-3668.69			42.06	0.00	241.71	1055.56	0.1072
Camp.	0.39	12.57	12.57	4996.58	164.01	771.54	14241.09	0.24	-5855.40	-14241.09	0.24					
				SLE Rare		0.00			-1905.71			21.85	0.00	125.56	548.31	
				SLE Freq.		0.00			-1797.38			20.61	0.00	118.42	517.14	0.0525
				SLE Q.P.		0.00			-1771.25			20.31	0.00	116.70	509.63	0.0518
11537	0.72	14.80	12.57			771.54	16453.38	0.26	-3318.42	-14239.17	0.24					
				SLE Rare		521.84			0.00			0.00	5.64	128.43	35.44	
				SLE Freq.		493.21			0.00			0.00	5.33	121.39	33.49	0.0030
				SLE Q.P.		485.95			0.00			0.00	5.25	119.60	33.00	0.0030
Trave Sez. 2 Rett. 40x40 [cm]																
11537	0.00	15.71	12.57			6725.07	17347.14	0.26	0.00	-14238.50	0.24					
				SLE Rare		918.75			0.00			0.00	9.73	213.66	62.93	
				SLE Freq.		867.36			0.00			0.00	9.18	201.71	59.41	0.0051
				SLE Q.P.		854.35			0.00			0.00	9.05	198.68	58.52	0.0050
Camp.	0.37	18.63	12.57	4996.08	172.52	12292.52	20204.08	0.29	-172.52	-14236.63	0.24					
				SLE Rare		4371.88			-116.86			1.27	43.74	864.40	305.17	
				SLE Freq.		4124.58			-110.47			1.20	41.26	815.50	287.91	0.0220
				SLE Q.P.		4062.57			-108.87			1.18	40.64	803.24	283.58	0.0216
11538	0.74	21.54	12.57			12292.52	23026.31	0.31	0.00	-14235.14	0.24					
				SLE Rare		8292.44			0.00			0.00	79.25	1427.58	584.99	
				SLE Freq.		7823.67			0.00			0.00	74.77	1346.88	551.92	0.0383
				SLE Q.P.		7706.26			0.00			0.00	73.65	1326.67	543.63	0.0377
Trave Sez. 2 Rett. 40x40 [cm]																
11538	0.00	22.45	12.57			19986.35	23894.98	0.32	0.00	-14234.73	0.24					
				SLE Rare		8533.80			0.00			0.00	80.54	1412.65	603.35	
				SLE Freq.		8051.01			0.00			0.00	75.99	1332.73	569.22	0.0384
				SLE Q.P.		7930.05			0.00			0.00	74.85	1312.71	560.66	0.0378
Camp.	0.30	24.76	12.57	4997.74	167.99	24482.83	26080.65	0.35	-157.92	-14233.80	0.24					
				SLE Rare		12367.22			-106.97			1.11	113.40	1865.66	877.96	
				SLE Freq.		11666.98			-101.12			1.05	106.98	1760.03	828.25	0.0532
				SLE Q.P.		11491.64			-99.65			1.03	105.37	1733.57	815.80	0.0518
11541	0.61	25.13	12.57			24482.83	26433.75	0.35	-23.95	-14233.66	0.24					
				SLE Rare		16513.78			-16.22			0.17	150.77	2455.79	1172.91	

				SLE Freq.		15578.97			-15.33			0.16	142.23	2316.77	1106.51	0.0820
				SLE Q.P.		15344.95			-15.11			0.16	140.10	2281.97	1089.89	0.0803
Trave Sez. 2 Rett. 40x40 [cm]																
11541	0.13	25.13	12.57			19949.43	26433.75	0.35	-23.94	-14233.66	0.24					
				SLE Rare		13455.79			-16.21			0.17	122.85	2001.03	955.71	
				SLE Freq.		12694.68			-15.33			0.16	115.90	1887.85	901.65	0.0605
				SLE Q.P.		12504.33			-15.11			0.16	114.16	1859.54	888.13	0.0591
Camp.	0.43	24.34	12.57	4996.28	167.94	19949.43	25684.37	0.34	-157.88	-14233.96	0.24					
				SLE Rare		9747.18			-106.94			1.11	89.82	1494.54	691.54	
				SLE Freq.		9195.82			-101.09			1.05	84.74	1410.00	652.43	0.0418
				SLE Q.P.		9057.92			-99.63			1.04	83.47	1388.86	642.64	0.0412
11548	0.73	22.03	12.57			15922.97	23492.64	0.32	0.00	-14234.92	0.24					
				SLE Rare		6351.61			0.00			0.00	60.29	1070.50	448.63	
				SLE Freq.		5992.89			0.00			0.00	56.89	1010.04	423.29	0.0289
				SLE Q.P.		5903.15			0.00			0.00	56.03	994.91	416.95	0.0285
Trave Sez. 2 Rett. 40x40 [cm]																
11548	0.00	21.12	12.57			9181.15	22621.89	0.31	0.00	-14235.34	0.24					
				SLE Rare		6193.51			0.00			0.00	59.55	1086.43	436.40	
				SLE Freq.		5843.85			0.00			0.00	56.19	1025.09	411.77	0.0289
				SLE Q.P.		5756.38			0.00			0.00	55.35	1009.75	405.60	0.0285
Camp.	0.37	18.21	12.57	4999.35	172.63	9181.15	19794.02	0.28	-181.99	-14236.88	0.24					
				SLE Rare		2802.08			-116.93			1.27	28.24	566.20	195.18	
				SLE Freq.		2643.94			-110.54			1.20	26.65	534.25	184.17	0.0143
				SLE Q.P.		2604.36			-108.94			1.19	26.25	526.25	181.41	0.0141
11550	0.74	15.29	12.57			4363.22	16932.89	0.26	-181.99	-14238.80	0.24					
				SLE Rare		0.00			-121.62			1.36	0.00	7.59	35.08	
				SLE Freq.		0.00			-113.82			1.27	0.00	7.10	32.83	0.0033
				SLE Q.P.		0.00			-112.96			1.26	0.00	7.05	32.58	0.0033
Trave Sez. 2 Rett. 40x40 [cm]																
11550	0.00	15.42	12.57			0.00	17065.64	0.26	-3822.53	-14238.70	0.24					
				SLE Rare		0.00			-383.52			4.28	0.00	23.87	110.62	
				SLE Freq.		0.00			-360.82			4.03	0.00	22.45	104.08	0.0106
				SLE Q.P.		0.00			-356.26			3.98	0.00	22.17	102.76	0.0105
Camp.	0.36	12.57	12.57	4994.48	163.94	0.00	14241.09	0.24	-6034.54	-14241.09	0.24					
				SLE Rare		0.00			-2448.42			28.07	0.00	161.31	704.46	
				SLE Freq.		0.00			-2309.36			26.48	0.00	152.15	664.45	0.0675
				SLE Q.P.		0.00			-2275.45			26.09	0.00	149.92	654.69	0.0665
11556	0.72	12.57	12.57			0.00	14241.09	0.24	-6034.54	-14241.09	0.24					
				SLE Rare		0.00			-4069.13			46.65	0.00	268.09	1170.77	
				SLE Freq.		0.00			-3838.00			44.00	0.00	252.86	1104.27	0.1121
				SLE Q.P.		0.00			-3780.81			43.34	0.00	249.09	1087.82	0.1105
Trave Sez. 2 Rett. 40x40 [cm]																
11556	0.00	12.57	12.57			0.00	14241.09	0.24	-7641.76	-14241.09	0.24					
				SLE Rare		0.00			-4260.08			48.84	0.00	280.67	1225.71	
				SLE Freq.		0.00			-4018.10			46.06	0.00	264.73	1156.09	0.1206
				SLE Q.P.		0.00			-3958.20			45.38	0.00	260.78	1138.85	0.1177
Camp.	0.37	12.57	12.57	4999.67	170.55	0.00	14241.09	0.24	-8191.74	-14241.09	0.24					
				SLE Rare		0.00			-5123.23			58.73	0.00	337.54	1474.06	
				SLE Freq.		0.00			-4832.97			55.41	0.00	318.41	1390.54	0.1603
				SLE Q.P.		0.00			-4760.73			54.58	0.00	313.66	1369.76	0.1568
11558	0.74	12.57	12.57			0.00	14241.09	0.24	-8191.74	-14241.09	0.24					
				SLE Rare		0.00			-5524.29			63.33	0.00	363.96	1589.45	
				SLE Freq.		0.00			-5211.03			59.74	0.00	343.32	1499.32	0.1787
				SLE Q.P.		0.00			-5132.77			58.84	0.00	338.17	1476.80	0.1749
Trave Sez. 2 Rett. 40x40 [cm]																

11558	0.00	12.57	12.57			0.00	14241.09	0.24	-8190.09	-14241.09	0.24					
				SLE Rare		0.00			-5523.20			63.32	0.00	363.89	1589.14	
				SLE Freq.		0.00			-5209.98			59.73	0.00	343.25	1499.02	0.1786
				SLE Q.P.		0.00			-5131.72			58.83	0.00	338.10	1476.50	0.1748
Camp.	0.37	12.57	12.57	4996.72	170.45	0.00	14241.09	0.24	-8190.09	-14241.09	0.24					
				SLE Rare		0.00			-5130.23			58.81	0.00	338.00	1476.07	
				SLE Freq.		0.00			-4839.86			55.49	0.00	318.87	1392.53	0.1606
				SLE Q.P.		0.00			-4767.24			54.65	0.00	314.08	1371.63	0.1571
11560	0.74	12.57	12.57			0.00	14241.09	0.24	-7651.23	-14241.09	0.24					
				SLE Rare		0.00			-4275.45			49.02	0.00	281.68	1230.13	
				SLE Freq.		0.00			-4033.18			46.24	0.00	265.72	1160.43	0.1213
				SLE Q.P.		0.00			-3972.59			45.54	0.00	261.73	1142.99	0.1184
Trave Sez. 2 Rett. 40x40 [cm]																
11560	0.00	12.57	12.57			0.00	14241.09	0.24	-6052.86	-14241.09	0.24					
				SLE Rare		0.00			-4081.92			46.80	0.00	268.93	1174.45	
				SLE Freq.		0.00			-3850.60			44.14	0.00	253.69	1107.90	0.1125
				SLE Q.P.		0.00			-3792.74			43.48	0.00	249.88	1091.25	0.1108
Camp.	0.36	12.57	12.57	4996.58	164.01	0.00	14241.09	0.24	-6052.86	-14241.09	0.24					
				SLE Rare		0.00			-2459.54			28.20	0.00	162.04	707.66	
				SLE Freq.		0.00			-2320.74			26.61	0.00	152.90	667.72	0.0678
				SLE Q.P.		0.00			-2286.00			26.21	0.00	150.61	657.73	0.0668
11566	0.72	14.45	12.57			0.00	16101.47	0.25	-3838.17	-14239.45	0.24					
				SLE Rare		0.00			-392.80			4.42	0.00	24.92	113.20	
				SLE Freq.		0.00			-370.81			4.18	0.00	23.52	106.87	0.0109
				SLE Q.P.		0.00			-365.26			4.11	0.00	23.17	105.27	0.0107
Trave Sez. 2 Rett. 40x40 [cm]																
11566	0.00	14.21	12.57			4340.23	15872.47	0.25	-190.05	-14239.64	0.24					
				SLE Rare		0.00			-128.08			1.45	0.00	8.16	36.91	
				SLE Freq.		0.00			-121.08			1.37	0.00	7.72	34.89	0.0035
				SLE Q.P.		0.00			-119.27			1.35	0.00	7.60	34.37	0.0035
Camp.	0.37	15.67	12.57	4996.07	172.52	9144.10	17311.09	0.26	-190.05	-14238.52	0.24					
				SLE Rare		2785.82			-116.86			1.30	29.52	649.29	190.76	
				SLE Freq.		2627.15			-110.47			1.23	27.84	612.31	179.89	0.0155
				SLE Q.P.		2588.74			-108.87			1.21	27.43	603.36	177.26	0.0152
11568	0.74	17.13	12.57			9144.10	18743.45	0.27	0.00	-14237.54	0.24					
				SLE Rare		6167.15			0.00			0.00	63.41	1320.51	426.93	
				SLE Freq.		5817.24			0.00			0.00	59.81	1245.59	402.70	0.0325
				SLE Q.P.		5731.29			0.00			0.00	58.93	1227.19	396.75	0.0320
Trave Sez. 2 Rett. 40x40 [cm]																
11568	0.00	17.59	12.57			15885.26	19187.31	0.28	0.00	-14237.25	0.24					
				SLE Rare		6329.00			0.00			0.00	64.51	1321.86	439.35	
				SLE Freq.		5969.95			0.00			0.00	60.85	1246.87	414.43	0.0329
				SLE Q.P.		5881.64			0.00			0.00	59.95	1228.42	408.30	0.0324
Camp.	0.30	18.74	12.57	4997.75	167.99	19908.30	20312.02	0.29	-157.92	-14236.57	0.24					
				SLE Rare		9721.10			-106.97			1.16	97.06	1911.21	678.91	
				SLE Freq.		9169.35			-101.12			1.10	91.55	1802.73	640.38	0.0487
				SLE Q.P.		9033.08			-99.65			1.08	90.19	1775.94	630.86	0.0479
11569	0.61	18.85	12.57			19908.30	20420.77	0.29	-23.95	-14236.51	0.24					
				SLE Rare		13426.34			-16.22			0.18	133.80	2624.77	938.17	
				SLE Freq.		12664.76			-15.33			0.17	126.21	2475.89	884.95	0.0670
				SLE Q.P.		12476.25			-15.11			0.16	124.33	2439.04	871.78	0.0660

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	Staffe
Trave 11534 11537 Sez. 2 Rett. 40x40 [cm]							
0.05	0.72	0.67	11508.68	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11537 11538 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	16564.11	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11538 11541 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	20968.72	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11541 11548 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	18834.16	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11548 11550 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	14454.53	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11550 11556 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	9349.69	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11556 11558 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	4383.38	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11558 11560 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	4350.01	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11560 11566 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	9358.85	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11566 11568 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	14414.28	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11568 11569 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	18818.89	8810.34	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 121 Nodi 11527 11593 11594 11595 11596 11597 11598 11599 11544*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
11527	0.12	12.57	12.57			12027.71	14241.09	0.24	-23.95	-14241.09	0.24					
				SLE Rare		8110.74			-16.22			0.19	92.98	2333.62	534.37	
				SLE Freq.		7651.12			-15.33			0.18	87.72	2201.38	504.09	0.0512
				SLE Q.P.		7538.13			-15.11			0.17	86.42	2168.87	496.64	0.0504
Camp.	0.43	12.57	12.57	4997.75	167.99	12027.71	14241.09	0.24	-157.92	-14241.09	0.24					
				SLE Rare		4854.60			-106.97			1.23	55.65	1396.77	319.84	
				SLE Freq.		4579.38			-101.12			1.16	52.50	1317.58	301.71	0.0306
				SLE Q.P.		4512.24			-99.66			1.14	51.73	1298.26	297.28	0.0302
11593	0.73	12.57	12.57			8486.60	14241.09	0.24	0.00	-14241.09	0.24					
				SLE Rare		1911.60			0.00			0.00	21.92	550.01	125.94	
				SLE Freq.		1803.66			0.00			0.00	20.68	518.95	118.83	0.0121
				SLE Q.P.		1778.08			0.00			0.00	20.38	511.59	117.15	0.0119
Trave Sez. 2 Rett. 40x40 [cm]																
11593	0.00	12.57	12.57			2240.67	14241.09	0.24	-2127.43	-14241.09	0.24					
				SLE Rare		1510.52			0.00			0.00	17.32	434.61	99.52	
				SLE Freq.		1425.05			0.00			0.00	16.34	410.02	93.89	0.0095
				SLE Q.P.		1405.22			0.00			0.00	16.11	404.31	92.58	0.0094
Camp.	0.37	12.57	12.57	4996.11	172.52	2240.67	14241.09	0.24	-5466.61	-14241.09	0.24					
				SLE Rare		0.00			-1322.04			15.16	0.00	87.10	380.38	
				SLE Freq.		0.00			-1247.35			14.30	0.00	82.18	358.89	0.0364
				SLE Q.P.		0.00			-1228.33			14.08	0.00	80.93	353.42	0.0359
11594	0.74	12.57	12.57			0.00	14241.09	0.24	-5466.61	-14241.09	0.24					
				SLE Rare		0.00			-3687.18			42.27	0.00	242.93	1060.88	
				SLE Freq.		0.00			-3477.89			39.87	0.00	229.14	1000.66	0.1016
				SLE Q.P.		0.00			-3425.25			39.27	0.00	225.67	985.51	0.1001
Trave Sez. 2 Rett. 40x40 [cm]																
11594	0.00	12.57	12.57			0.00	14241.09	0.24	-8365.64	-14241.09	0.24					

				SLE Rare		0.00			-4019.48			46.08	0.00	264.82	1156.49	
				SLE Freq.		0.00			-3791.60			43.47	0.00	249.81	1090.92	0.1108
				SLE Q.P.		0.00			-3734.35			42.81	0.00	246.03	1074.45	0.1091
Camp.	0.36	12.57	12.57	4974.77	163.30	0.00	14241.09	0.24	-9846.88	-14241.09	0.24					
				SLE Rare		0.00			-5551.51			63.64	0.00	365.76	1597.28	
				SLE Freq.		0.00			-5237.09			60.04	0.00	345.04	1506.82	0.1800
				SLE Q.P.		0.00			-5158.23			59.14	0.00	339.84	1484.13	0.1761
11595	0.72	12.57	12.57			0.00	14241.09	0.24	-9846.88	-14241.09	0.24					
				SLE Rare		0.00			-6641.07			76.14	0.00	437.54	1910.77	
				SLE Freq.		0.00			-6264.30			71.82	0.00	412.72	1802.37	0.2300
				SLE Q.P.		0.00			-6169.89			70.73	0.00	406.50	1775.20	0.2254
Trave Sez. 2 Rett. 40x40 [cm]																
11595	0.00	12.57	12.57			0.00	14241.09	0.24	-10516.08	-14241.09	0.24					
				SLE Rare		0.00			-6787.02			77.81	0.00	447.16	1952.76	
				SLE Freq.		0.00			-6402.26			73.40	0.00	421.81	1842.06	0.2367
				SLE Q.P.		0.00			-6305.89			72.29	0.00	415.46	1814.33	0.2320
Camp.	0.37	12.57	12.57	4928.18	168.11	0.00	14241.09	0.24	-10521.35	-14241.09	0.24					
				SLE Rare		0.00			-7090.66			81.29	0.00	467.16	2040.13	
				SLE Freq.		0.00			-6689.02			76.69	0.00	440.70	1924.57	0.2507
				SLE Q.P.		0.00			-6588.49			75.53	0.00	434.08	1895.64	0.2458
11596	0.74	12.57	12.57			0.00	14241.09	0.24	-10521.35	-14241.09	0.24					
				SLE Rare		0.00			-6938.72			79.55	0.00	457.15	1996.41	
				SLE Freq.		0.00			-6545.08			75.04	0.00	431.22	1883.15	0.2437
				SLE Q.P.		0.00			-6446.86			73.91	0.00	424.74	1854.89	0.2389
Trave Sez. 2 Rett. 40x40 [cm]																
11596	0.00	12.57	12.57			0.00	14241.09	0.24	-10112.33	-14241.09	0.24					
				SLE Rare		0.00			-6820.20			78.19	0.00	449.34	1962.31	
				SLE Freq.		0.00			-6433.55			73.76	0.00	423.87	1851.07	0.2382
				SLE Q.P.		0.00			-6337.03			72.65	0.00	417.51	1823.29	0.2335
Camp.	0.37	12.57	12.57	4999.81	170.56	0.00	14241.09	0.24	-10112.33	-14241.09	0.24					
				SLE Rare		0.00			-5905.17			67.70	0.00	389.06	1699.04	
				SLE Freq.		0.00			-5570.47			63.86	0.00	367.00	1602.74	0.1962
				SLE Q.P.		0.00			-5487.24			62.91	0.00	361.52	1578.79	0.1921
11597	0.74	12.57	12.57			0.00	14241.09	0.24	-8839.67	-14241.09	0.24					
				SLE Rare		0.00			-4528.06			51.91	0.00	298.33	1302.81	
				SLE Freq.		0.00			-4270.56			48.96	0.00	281.36	1228.73	0.1329
				SLE Q.P.		0.00			-4206.94			48.23	0.00	277.17	1210.42	0.1298
Trave Sez. 2 Rett. 40x40 [cm]																
11597	0.00	12.57	12.57			0.00	14241.09	0.24	-6201.21	-14241.09	0.24					
				SLE Rare		0.00			-4181.33			47.94	0.00	275.48	1203.06	
				SLE Freq.		0.00			-3943.80			45.21	0.00	259.83	1134.71	0.1170
				SLE Q.P.		0.00			-3885.10			44.54	0.00	255.97	1117.82	0.1141
Camp.	0.36	12.58	12.57	4994.58	163.95	756.59	14250.04	0.24	-6201.21	-14241.08	0.24					
				SLE Rare		0.00			-2056.43			23.57	0.00	135.46	591.68	
				SLE Freq.		0.00			-1939.35			22.23	0.00	127.75	557.99	0.0567
				SLE Q.P.		0.00			-1911.07			21.91	0.00	125.89	549.86	0.0558
11598	0.72	15.41	12.57			756.59	17050.75	0.26	-3295.52	-14238.71	0.24					
				SLE Rare		512.66			0.00			0.00	5.46	121.44	35.02	
				SLE Freq.		485.00			0.00			0.00	5.17	114.89	33.13	0.0029
				SLE Q.P.		477.97			0.00			0.00	5.09	113.22	32.65	0.0028
Trave Sez. 2 Rett. 40x40 [cm]																
11598	0.00	16.32	12.57			6686.08	17942.91	0.27	0.00	-14238.07	0.24					
				SLE Rare		906.45			0.00			0.00	9.47	203.33	62.39	
				SLE Freq.		856.15			0.00			0.00	8.95	192.05	58.93	0.0049
				SLE Q.P.		843.41			0.00			0.00	8.82	189.19	58.05	0.0048

Camp.	0.37	19.23	12.57	4999.39	172.64	12236.11	20793.47	0.29	-172.64	-14236.30	0.24					
				SLE Rare		4347.31			-116.93			1.26	43.05	833.74	304.28	
				SLE Freq.		4101.97			-110.54			1.19	40.62	786.69	287.11	0.0214
				SLE Q.P.		4040.43			-108.94			1.18	40.01	774.89	282.80	0.0211
11599	0.74	22.15	12.57			12236.11	23607.17	0.32	0.00	-14234.86	0.24					
				SLE Rare		8255.90			0.00			0.00	78.24	1384.30	583.30	
				SLE Freq.		7789.93			0.00			0.00	73.82	1306.17	550.38	0.0375
				SLE Q.P.		7673.20			0.00			0.00	72.72	1286.60	542.13	0.0369
Trave Sez. 2 Rett. 40x40 [cm]																
11599	0.00	23.06	12.57			19898.29	24472.71	0.33	0.00	-14234.47	0.24					
				SLE Rare		8494.87			0.00			0.00	79.54	1371.06	601.36	
				SLE Freq.		8014.94			0.00			0.00	75.05	1293.60	567.39	0.0377
				SLE Q.P.		7894.69			0.00			0.00	73.92	1274.19	558.88	0.0371
Camp.	0.30	25.13	12.57	4996.29	167.94	24378.63	26433.75	0.35	-157.88	-14233.66	0.24					
				SLE Rare		12313.68			-106.94			1.11	112.42	1831.19	874.59	
				SLE Freq.		11617.30			-101.09			1.05	106.06	1727.63	825.13	0.0525
				SLE Q.P.		11442.90			-99.63			1.03	104.47	1701.69	812.74	0.0512
11544	0.61	25.13	12.57			24378.63	26433.75	0.35	-23.94	-14233.66	0.24					
				SLE Rare		16445.54			-16.21			0.17	150.14	2445.64	1168.06	
				SLE Freq.		15515.58			-15.33			0.16	141.65	2307.35	1102.01	0.0815
				SLE Q.P.		15282.76			-15.11			0.16	139.53	2272.72	1085.47	0.0798

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 11527 11593 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	16630.24	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11593 11594 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	12225.61	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11594 11595 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7170.15	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11595 11596 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	2122.82	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11596 11597 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	6444.38	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11597 11598 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	11410.78	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11598 11599 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	16515.67	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11599 11544 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	20895.24	8810.34	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 126 Nodi 11544 11600 11602 11604 11606 11608 11610 11612 11570 11613 11611 11609*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
11544	0.12	21.99	12.57			19913.26	23454.77	0.32	-23.95	-14234.94	0.24					
				SLE Rare		13433.36			-16.22			0.17	127.58	2267.92	948.73	
				SLE Freq.		12674.39			-15.33			0.16	120.37	2139.79	895.13	0.0632
				SLE Q.P.		12484.54			-15.11			0.16	118.57	2107.74	881.72	0.0616
Camp.	0.43	21.99	12.57	4997.69	167.98	19913.26	23454.77	0.32	-157.92	-14234.94	0.24					
				SLE Rare		9725.84			-106.97			1.13	92.37	1641.99	686.89	
				SLE Freq.		9176.47			-101.12			1.07	87.15	1549.24	648.09	0.0443
				SLE Q.P.		9039.03			-99.65			1.05	85.85	1526.04	638.38	0.0437
11600	0.73	20.43	12.57			15888.21	21957.51	0.30	0.00	-14235.67	0.24					
				SLE Rare		6331.46			0.00			0.00	61.51	1146.22	445.17	
				SLE Freq.		5974.56			0.00			0.00	58.04	1081.61	420.07	0.0301
				SLE Q.P.		5885.24			0.00			0.00	57.17	1065.44	413.79	0.0297

Trave Sez. 2 Rett. 40x40 [cm]																
11600	0.00	19.75	12.57			9147.49	21299.37	0.30	0.00	-14236.02	0.24					
				SLE Rare		6172.44			0.00			0.00	60.60	1154.02	432.93	
				SLE Freq.		5824.71			0.00			0.00	57.19	1089.00	408.54	0.0300
				SLE Q.P.		5737.70			0.00			0.00	56.33	1072.73	402.44	0.0295
Camp.	0.37	17.57	12.57	4996.16	172.52	9147.49	19168.89	0.28	-193.35	-14237.26	0.24					
				SLE Rare		2788.34			-116.86			1.28	28.43	582.96	193.54	
				SLE Freq.		2631.56			-110.47			1.21	26.83	550.18	182.66	0.0145
				SLE Q.P.		2592.30			-108.87			1.19	26.43	541.97	179.93	0.0143
11602	0.74	15.38	12.57			4340.43	17020.95	0.26	-193.35	-14238.74	0.24					
				SLE Rare		0.00			-128.32			1.43	0.00	7.99	37.01	
				SLE Freq.		0.00			-119.72			1.34	0.00	7.46	34.53	0.0035
				SLE Q.P.		0.00			-118.75			1.33	0.00	7.40	34.25	0.0035
Trave Sez. 2 Rett. 40x40 [cm]																
11602	0.00	15.92	12.57			0.00	17555.31	0.26	-3841.32	-14238.35	0.24					
				SLE Rare		0.00			-390.52			4.34	0.00	24.07	112.69	
				SLE Freq.		0.00			-366.97			4.08	0.00	22.62	105.89	0.0108
				SLE Q.P.		0.00			-362.30			4.03	0.00	22.33	104.55	0.0106
Camp.	0.36	12.58	12.57	4996.69	164.02	0.00	14251.66	0.24	-6059.02	-14241.08	0.24					
				SLE Rare		0.00			-2459.96			28.20	0.00	162.04	707.79	
				SLE Freq.		0.00			-2319.88			26.59	0.00	152.81	667.48	0.0678
				SLE Q.P.		0.00			-2285.79			26.20	0.00	150.56	657.67	0.0668
11604	0.72	12.57	12.57			0.00	14241.09	0.24	-6059.02	-14241.09	0.24					
				SLE Rare		0.00			-4085.02			46.83	0.00	269.14	1175.34	
				SLE Freq.		0.00			-3852.71			44.17	0.00	253.83	1108.50	0.1126
				SLE Q.P.		0.00			-3795.27			43.51	0.00	250.05	1091.98	0.1109
Trave Sez. 2 Rett. 40x40 [cm]																
11604	0.00	12.57	12.57			0.00	14241.09	0.24	-7656.91	-14241.09	0.24					
				SLE Rare		0.00			-4275.85			49.02	0.00	281.71	1230.25	
				SLE Freq.		0.00			-4032.68			46.23	0.00	265.69	1160.28	0.1213
				SLE Q.P.		0.00			-3972.52			45.54	0.00	261.73	1142.98	0.1184
Camp.	0.37	12.57	12.57	4996.58	170.45	0.00	14241.09	0.24	-8198.96	-14241.09	0.24					
				SLE Rare		0.00			-5133.40			58.85	0.00	338.21	1476.98	
				SLE Freq.		0.00			-4842.40			55.51	0.00	319.04	1393.26	0.1607
				SLE Q.P.		0.00			-4770.00			54.68	0.00	314.27	1372.43	0.1572
11606	0.74	12.57	12.57			0.00	14241.09	0.24	-8198.96	-14241.09	0.24					
				SLE Rare		0.00			-5529.14			63.39	0.00	364.28	1590.85	
				SLE Freq.		0.00			-5215.58			59.79	0.00	343.62	1500.63	0.1789
				SLE Q.P.		0.00			-5137.24			58.90	0.00	338.46	1478.09	0.1751
Trave Sez. 2 Rett. 40x40 [cm]																
11606	0.00	12.57	12.57			0.00	14241.09	0.24	-8196.59	-14241.09	0.24					
				SLE Rare		0.00			-5527.54			63.37	0.00	364.18	1590.39	
				SLE Freq.		0.00			-5214.04			59.78	0.00	343.52	1500.19	0.1788
				SLE Q.P.		0.00			-5135.71			58.88	0.00	338.36	1477.65	0.1750
Camp.	0.37	12.57	12.57	4999.63	170.55	0.00	14241.09	0.24	-8196.59	-14241.09	0.24					
				SLE Rare		0.00			-5129.26			58.80	0.00	337.94	1475.79	
				SLE Freq.		0.00			-4839.06			55.48	0.00	318.82	1392.30	0.1606
				SLE Q.P.		0.00			-4766.48			54.64	0.00	314.03	1371.41	0.1570
11608	0.74	12.57	12.57			0.00	14241.09	0.24	-7649.83	-14241.09	0.24					
				SLE Rare		0.00			-4268.91			48.94	0.00	281.25	1228.25	
				SLE Freq.		0.00			-4027.27			46.17	0.00	265.33	1158.73	0.1210
				SLE Q.P.		0.00			-3966.82			45.48	0.00	261.35	1141.34	0.1181
Trave Sez. 2 Rett. 40x40 [cm]																
11608	0.00	12.57	12.57			0.00	14241.09	0.24	-6041.63	-14241.09	0.24					
				SLE Rare		0.00			-4074.90			46.72	0.00	268.47	1172.43	

				SLE Freq.		0.00			-3844.22			44.07	0.00	253.27	1106.06	0.1123
				SLE Q.P.		0.00			-3786.50			43.41	0.00	249.47	1089.45	0.1106
Camp.	0.36	12.57	12.57	4994.53	163.95	0.00	14241.09	0.24	-6041.63	-14241.09	0.24					
				SLE Rare		0.00			-2456.93			28.17	0.00	161.87	706.91	
				SLE Freq.		0.00			-2318.60			26.58	0.00	152.76	667.11	0.0677
				SLE Q.P.		0.00			-2283.96			26.18	0.00	150.48	657.14	0.0667
11610	0.72	13.75	12.57			0.00	15411.93	0.25	-3832.73	-14240.03	0.24					
				SLE Rare		0.00			-394.77			4.47	0.00	25.39	113.70	
				SLE Freq.		0.00			-373.08			4.23	0.00	24.00	107.46	0.0109
				SLE Q.P.		0.00			-367.59			4.17	0.00	23.65	105.88	0.0108
Trave Sez. 2 Rett. 40x40 [cm]																
11610	0.00	14.22	12.57			4350.51	15882.59	0.25	-191.13	-14239.63	0.24					
				SLE Rare		0.00			-129.71			1.46	0.00	8.26	37.37	
				SLE Freq.		0.00			-122.99			1.39	0.00	7.84	35.44	0.0036
				SLE Q.P.		0.00			-121.24			1.37	0.00	7.73	34.94	0.0036
Camp.	0.37	17.14	12.57	4999.44	172.64	9165.19	18753.47	0.27	-191.13	-14237.53	0.24					
				SLE Rare		2791.19			-116.93			1.29	28.69	597.31	193.23	
				SLE Freq.		2631.67			-110.54			1.22	27.05	563.17	182.19	0.0147
				SLE Q.P.		2593.19			-108.94			1.20	26.66	554.94	179.53	0.0145
11612	0.74	20.06	12.57			9165.19	21594.64	0.30	0.00	-14235.86	0.24					
				SLE Rare		6179.81			0.00			0.00	60.38	1138.67	433.94	
				SLE Freq.		5828.49			0.00			0.00	56.95	1073.94	409.27	0.0297
				SLE Q.P.		5742.36			0.00			0.00	56.11	1058.07	403.22	0.0293
Trave Sez. 2 Rett. 40x40 [cm]																
11612	0.00	20.97	12.57			15909.01	22470.33	0.31	0.00	-14235.41	0.24					
				SLE Rare		6341.81			0.00			0.00	61.12	1120.38	446.65	
				SLE Freq.		5981.40			0.00			0.00	57.64	1056.71	421.26	0.0297
				SLE Q.P.		5892.90			0.00			0.00	56.79	1041.08	415.03	0.0293
Camp.	0.30	23.27	12.57	4996.27	167.94	19933.50	24676.51	0.33	-157.88	-14234.38	0.24					
				SLE Rare		9735.10			-106.94			1.12	90.90	1557.48	689.45	
				SLE Freq.		9181.82			-101.09			1.06	85.74	1468.96	650.26	0.0429
				SLE Q.P.		9045.34			-99.63			1.04	84.46	1447.13	640.60	0.0423
11570	0.61	25.13	12.57			19933.50	26433.75	0.35	-23.94	-14233.66	0.24					
				SLE Rare		13441.44			-16.21			0.17	122.72	1998.90	954.69	
				SLE Freq.		12678.17			-15.33			0.16	115.75	1885.39	900.48	0.0604
				SLE Q.P.		12489.44			-15.11			0.16	114.03	1857.32	887.07	0.0590
Trave Sez. 2 Rett. 40x40 [cm]																
11570	0.12	25.13	12.57			24444.76	26433.75	0.35	-23.95	-14233.66	0.24					
				SLE Rare		16484.40			-16.22			0.17	150.50	2451.42	1170.82	
				SLE Freq.		15548.33			-15.33			0.16	141.95	2312.22	1104.34	0.0818
				SLE Q.P.		15315.65			-15.11			0.16	139.83	2277.62	1087.81	0.0800
Camp.	0.43	25.13	12.57	4997.71	167.99	24444.76	26433.75	0.35	-157.92	-14233.66	0.24					
				SLE Rare		12342.43			-106.97			1.11	112.68	1835.46	876.63	
				SLE Freq.		11641.05			-101.12			1.05	106.28	1731.16	826.82	0.0527
				SLE Q.P.		11466.89			-99.65			1.03	104.69	1705.26	814.45	0.0514
11613	0.73	23.52	12.57			19952.66	24908.26	0.33	0.00	-14234.29	0.24					
				SLE Rare		8513.59			0.00			0.00	79.25	1348.62	603.21	
				SLE Freq.		8029.79			0.00			0.00	74.75	1271.98	568.93	0.0373
				SLE Q.P.		7909.85			0.00			0.00	73.63	1252.98	560.43	0.0367
Trave Sez. 2 Rett. 40x40 [cm]																
11613	0.00	22.61	12.57			12258.63	24045.20	0.32	0.00	-14234.66	0.24					
				SLE Rare		8266.42			0.00			0.00	77.86	1359.34	584.65	
				SLE Freq.		7796.61			0.00			0.00	73.43	1282.08	551.42	0.0371
				SLE Q.P.		7680.32			0.00			0.00	72.34	1262.96	543.20	0.0365
Camp.	0.37	19.69	12.57	4996.27	172.53	12258.63	21238.29	0.30	-172.53	-14236.05	0.24					

				SLE Rare		4351.52			-116.86			1.26	42.77	816.05	305.14	
				SLE Freq.		4103.32			-110.47			1.19	40.33	769.50	287.74	0.0212
				SLE Q.P.		4042.23			-108.87			1.17	39.73	758.05	283.45	0.0208
11611	0.74	16.77	12.57			6698.42	18392.84	0.27	0.00	-14237.77	0.24					
				SLE Rare		904.05			0.00			0.00	9.36	197.51	62.43	
				SLE Freq.		851.90			0.00			0.00	8.82	186.11	58.83	0.0048
				SLE Q.P.		839.64			0.00			0.00	8.69	183.43	57.99	0.0048
Trave Sez. 2 Rett. 40x40 [cm]																
11611	0.00	15.87	12.57			746.36	17501.97	0.26	-3335.69	-14238.38	0.24					
				SLE Rare		502.56			0.00			0.00	5.30	115.77	34.47	
				SLE Freq.		473.20			0.00			0.00	4.99	109.00	32.46	0.0028
				SLE Q.P.		466.72			0.00			0.00	4.92	107.51	32.01	0.0027
Camp.	0.34	13.26	12.57	4996.53	164.01	746.36	14929.08	0.24	-5866.84	-14240.45	0.24					
				SLE Rare		0.00			-1919.85			21.86	0.00	124.72	552.72	
				SLE Freq.		0.00			-1812.12			20.64	0.00	117.72	521.71	0.0530
				SLE Q.P.		0.00			-1785.20			20.33	0.00	115.97	513.96	0.0522
11609	0.67	12.57	12.57			0.00	14241.09	0.24	-5866.84	-14241.09	0.24					
				SLE Rare		0.00			-3957.30			45.37	0.00	260.72	1138.60	
				SLE Freq.		0.00			-3733.55			42.80	0.00	245.98	1074.22	0.1091
				SLE Q.P.		0.00			-3677.60			42.16	0.00	242.29	1058.12	0.1075

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 11544 11600 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	18827.92	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11600 11602 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	14423.34	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11602 11604 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	9367.87	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11604 11606 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	4359.03	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11606 11608 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	4374.18	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11608 11610 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	9340.52	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11610 11612 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	14445.39	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11612 11570 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	18824.99	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11570 11613 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	20948.44	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11613 11611 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	16543.85	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11611 11609 Sez. 2 Rett. 40x40 [cm]							
0.00	0.67	0.67	11488.30	8810.34	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 14 Nodi 104 2793*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 1 Rett. 40x40 [cm]																
104	0.13	4.54	5.68			0.00	6105.08	0.14	-3145.03	-7386.30	0.14					
				SLE Rare		0.00			-1502.92			22.41	0.00	99.89	812.02	
				SLE Freq.		0.00			-1404.26			20.93	0.00	93.33	758.72	0.0849
				SLE Q.P.		0.00			-1370.45			20.43	0.00	91.09	740.45	0.0828
Camp.	1.77	6.03	6.03	520.00	409.58	812.55	7803.06	0.15	-1292.37	-7803.06	0.15					
				SLE Rare		0.00			-556.12			7.92	0.00	47.56	301.59	
				SLE Freq.		0.00			-541.65			7.72	0.00	46.32	293.74	0.0319

				SLE Q.P.		0.00			-536.91			7.65	0.00	45.91	291.17	0.0316
2793	3.42	6.03	6.03			4031.28	7803.06	0.15	-436.60	-7803.06	0.15					
				SLE Rare		1497.94			0.00			0.00	21.34	812.34	128.10	
				SLE Freq.		1431.43			0.00			0.00	20.40	776.27	122.41	0.0133
				SLE Q.P.		1408.18			0.00			0.00	20.06	763.66	120.42	0.0131

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 104 2793 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	1674.64	6895.68	38935.73	63800.94	151.92	5004.46	2398.29	ø 10 2br. 7.5'
0.52	3.03	2.50	2674.64	7037.02	38935.73	38280.56	151.92	5004.46	2832.32	ø 10 2br. 12.5'
3.03	3.42	0.40	2834.64	7037.02	38935.73	63800.94	151.92	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 15 Nodi 105 2798*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
105	0.13	4.54	5.68			0.00	6105.08	0.14	-3457.18	-7386.30	0.14					
				SLE Rare		0.00			-1671.32			24.92	0.00	111.08	903.01	
				SLE Freq.		0.00			-1570.77			23.42	0.00	104.40	848.68	0.0949
				SLE Q.P.		0.00			-1536.36			22.90	0.00	102.11	830.09	0.0929
Camp.	1.77	6.03	6.03	520.00	409.58	921.43	7803.06	0.15	-1320.08	-7803.06	0.15					
				SLE Rare		0.00			-530.50			7.56	0.00	45.37	287.69	
				SLE Freq.		0.00			-515.69			7.35	0.00	44.10	279.66	0.0303
				SLE Q.P.		0.00			-510.76			7.28	0.00	43.68	276.99	0.0300
2798	3.42	6.03	6.03			4395.23	7803.06	0.15	-402.38	-7803.06	0.15					
				SLE Rare		1725.10			0.00			0.00	24.58	935.52	147.52	
				SLE Freq.		1657.18			0.00			0.00	23.61	898.70	141.72	0.0154
				SLE Q.P.		1633.50			0.00			0.00	23.28	885.85	139.69	0.0151

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 105 2798 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	1879.52	6895.68	38935.73	63800.94	170.18	5004.46	2398.29	ø 10 2br. 7.5'
0.52	3.03	2.50	2879.52	7037.02	38935.73	38280.56	170.18	5004.46	2832.32	ø 10 2br. 12.5'
3.03	3.42	0.40	3039.52	7037.02	38935.73	63800.94	170.18	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 155 Nodi 3921 3984 4057*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 7 Rett. 30x80 [cm]																
3921	0.13	8.04	8.04			10483.69	22578.91	0.08	-1.79	-22578.91	0.08					
				SLE Rare		7498.37			-1.38			0.01	29.92	1356.71	320.67	
				SLE Freq.		7229.84			-1.38			0.01	28.85	1308.13	309.18	0.0278
				SLE Q.P.		7149.67			-1.38			0.01	28.53	1293.62	305.75	0.0275
Camp.	0.48	8.04	8.04	780.00	34.41	10483.69	22578.91	0.08	-32.86	-22578.91	0.08					
				SLE Rare		5668.50			-25.27			0.10	22.62	1025.62	242.41	
				SLE Freq.		5466.57			-25.27			0.10	21.81	989.09	233.78	0.0210
				SLE Q.P.		5405.89			-25.27			0.10	21.57	978.11	231.18	0.0208
3984	0.84	8.04	8.04			10483.69	22578.91	0.08	0.00	-22578.91	0.08					
				SLE Rare		3915.38			0.00			0.00	15.62	708.43	167.44	
				SLE Freq.		3780.04			0.00			0.00	15.08	683.94	161.65	0.0145
				SLE Q.P.		3738.87			0.00			0.00	14.92	676.49	159.89	0.0144
Trave Sez. 7 Rett. 30x80 [cm]																
3984	0.00	8.04	8.04			963.33	22578.91	0.08	-5880.26	-22578.91	0.08					
				SLE Rare		0.00			-402.89			1.61	0.00	17.23	72.90	
				SLE Freq.		0.00			-380.05			1.52	0.00	16.25	68.76	0.0062

				SLE Q.P.		0.00			-375.73			1.50	0.00	16.07	67.98	0.0061
Camp.	0.49	8.04	8.04	780.00	59.03	963.33	22578.91	0.08	-6434.19	-22578.91	0.08					
				SLE Rare		0.00			-2108.87			8.41	0.00	90.19	381.57	
				SLE Freq.		0.00			-2031.18			8.10	0.00	86.86	367.51	0.0330
				SLE Q.P.		0.00			-2012.57			8.03	0.00	86.07	364.14	0.0327
4057	0.98	8.04	8.04			811.49	22578.91	0.08	-6434.19	-22578.91	0.08					
				SLE Rare		0.00			-3672.23			14.65	0.00	157.04	664.43	
				SLE Freq.		0.00			-3539.69			14.12	0.00	151.37	640.45	0.0576
				SLE Q.P.		0.00			-3506.79			13.99	0.00	149.97	634.50	0.0570

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 3921 3984 Sez. 7 Rett. 30x80 [cm]										
0.13	0.84	0.72	7192.30	9231.02	91905.48	33235.49	1687.50	11601.62	6485.85	ø 10 2br. 12.5'
Trave 3984 4057 Sez. 7 Rett. 30x80 [cm]										
0.00	0.98	0.98	5377.27	9231.02	91905.48	33235.49	1355.65	11601.62	6485.85	ø 10 2br. 12.5'

Travata: *Travata 17 Nodi 107 2803*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
107	0.13	4.12	5.68			343.49	5628.58	0.13	-3082.86	-7381.72	0.14					
				SLE Rare		0.00			-1253.50			18.80	0.00	76.63	676.99	
				SLE Freq.		0.00			-1167.61			17.51	0.00	71.38	630.61	0.0705
				SLE Q.P.		0.00			-1137.82			17.07	0.00	69.55	614.51	0.0687
Camp.	1.77	6.03	6.03	520.00	409.58	765.88	7803.06	0.15	-1234.80	-7803.06	0.15					
				SLE Rare		0.00			-582.71			8.30	0.00	49.83	316.01	
				SLE Freq.		0.00			-565.58			8.06	0.00	48.37	306.72	0.0333
				SLE Q.P.		0.00			-559.87			7.98	0.00	47.88	303.62	0.0329
2803	3.42	6.03	6.03			3918.67	7803.06	0.15	-773.25	-7803.06	0.15					
				SLE Rare		1192.17			0.00			0.00	16.99	646.52	101.95	
				SLE Freq.		1143.87			0.00			0.00	16.30	620.33	97.82	0.0106
				SLE Q.P.		1126.40			0.00			0.00	16.05	610.85	96.33	0.0104

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 107 2803 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	1621.68	6895.68	38935.73	63800.94	165.83	5004.46	2299.93	ø 10 2br. 7.5'
0.52	3.03	2.50	2621.68	7037.02	38935.73	38280.56	165.83	5004.46	2832.32	ø 10 2br. 12.5'
3.03	3.42	0.40	2781.68	7037.02	38935.73	63800.94	165.83	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 2 Nodi 141 3962*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
141	0.13	6.03	6.03			4489.49	7803.06	0.15	0.00	-7803.06	0.15					
				SLE Rare		3259.08			0.00			0.00	46.44	1767.41	278.70	
				SLE Freq.		3148.58			0.00			0.00	44.86	1707.48	269.25	0.0292
				SLE Q.P.		3112.30			0.00			0.00	44.35	1687.81	266.15	0.0289
Camp.	2.13	6.03	6.03	520.00	587.03	454.71	7803.06	0.15	-1210.48	-7803.06	0.15					
				SLE Rare		0.00			-451.56			6.43	0.00	38.62	244.88	
				SLE Freq.		0.00			-451.56			6.43	0.00	38.62	244.88	0.0266
				SLE Q.P.		0.00			-451.56			6.43	0.00	38.62	244.88	0.0266
3962	4.13	6.03	6.03			0.00	7803.06	0.15	-3329.63	-7803.06	0.15					
				SLE Rare		0.00			-2337.62			33.31	0.00	199.90	1267.70	
				SLE Freq.		0.00			-2226.78			31.73	0.00	190.43	1207.59	0.1310
				SLE Q.P.		0.00			-2190.54			31.21	0.00	187.33	1187.94	0.1288

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 141 3962 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	2994.78	7037.02	38935.73	63800.94	215.33	5004.46	2832.32	ø 10 2br. 7.5'
0.52	3.72	3.20	2786.78	7037.02	38935.73	38280.56	215.33	5004.46	2832.32	ø 10 2br. 12.5'
3.72	4.13	0.40	1122.78	7037.02	38935.73	63800.94	215.33	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 20 Nodi 203 5846*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
203	0.13	6.03	8.04			0.00	7812.95	0.15	-6930.18	-10079.37	0.16					
				SLE Rare		0.00			-4605.19			58.75	0.00	410.56	1894.42	
				SLE Freq.		0.00			-4360.13			55.63	0.00	388.71	1793.61	0.1748
				SLE Q.P.		0.00			-4277.44			54.57	0.00	381.34	1759.60	0.1695
Camp.	1.77	6.03	6.03	520.00	409.58	2419.32	7803.06	0.15	-1527.88	-7803.06	0.15					
				SLE Rare		252.64			-315.06			4.49	3.60	137.01	170.86	
				SLE Freq.		233.13			-315.06			4.49	3.32	126.43	170.86	0.0185
				SLE Q.P.		226.66			-315.06			4.49	3.23	122.92	170.86	0.0185
5846	3.42	8.04	6.03			9151.01	10079.37	0.16	0.00	-7812.94	0.15					
				SLE Rare		6201.28			0.00			0.00	79.12	2551.00	552.85	
				SLE Freq.		5917.21			0.00			0.00	75.49	2434.14	527.53	0.0448
				SLE Q.P.		5821.59			0.00			0.00	74.27	2394.81	519.00	0.0441

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 203 5846 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	4223.09	7745.24	38935.73	63800.94	101.69	5004.46	3304.37	ø 10 2br. 7.5'
0.52	3.03	2.50	5523.09	7037.02	38935.73	38280.56	101.69	5004.46	2832.32	ø 10 2br. 12.5'
3.03	3.42	0.40	5731.09	7037.02	38935.73	63800.94	101.69	5004.46	3304.37	ø 10 2br. 7.5'

Travata: *Travata 21 Nodi 204 5851*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
204	0.13	6.03	8.04			0.00	7812.95	0.15	-7621.21	-10079.37	0.16					
				SLE Rare		0.00			-5072.16			64.71	0.00	452.19	2086.52	
				SLE Freq.		0.00			-4808.50			61.35	0.00	428.68	1978.06	0.2037
				SLE Q.P.		0.00			-4719.87			60.22	0.00	420.78	1941.59	0.1980
Camp.	1.77	6.03	6.03	520.00	409.58	2607.38	7803.06	0.15	-1686.32	-7803.06	0.15					
				SLE Rare		262.20			-315.06			4.49	3.74	142.19	170.86	
				SLE Freq.		242.20			-315.06			4.49	3.45	131.34	170.86	0.0185
				SLE Q.P.		235.55			-315.06			4.49	3.36	127.74	170.86	0.0185
5851	3.42	8.04	6.03			9871.66	10079.37	0.16	0.00	-7812.94	0.15					
				SLE Rare		6687.38			0.00			0.00	85.32	2750.96	596.19	
				SLE Freq.		6383.72			0.00			0.00	81.44	2626.04	569.11	0.0483
				SLE Q.P.		6281.79			0.00			0.00	80.14	2584.12	560.03	0.0476

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 204 5851 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	4650.87	7745.24	38935.73	63800.94	107.66	5004.46	3304.37	ø 10 2br. 7.5'
0.52	3.03	2.50	5950.87	7037.02	38935.73	38280.56	107.66	5004.46	2832.32	ø 10 2br. 12.5'
3.03	3.42	0.40	6158.87	7037.02	38935.73	63800.94	107.66	5004.46	3304.37	ø 10 2br. 7.5'

Travata: *Travata 214 Nodi 363 10154*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
363	0.13	8.04	8.04			3991.77	13228.33	0.13	-502.55	-13228.33	0.13					

				SLE Rare		866.20			0.00			0.00	7.01	271.05	55.76	
				SLE Freq.		642.93			0.00			0.00	5.20	201.18	41.39	0.0043
				SLE Q.P.		568.50			0.00			0.00	4.60	177.89	36.60	0.0038
Camp.	2.33	8.04	8.04	650.00	883.62	1033.36	13228.33	0.13	-2644.24	-13228.33	0.13					
				SLE Rare		0.00			-708.11			5.73	0.00	45.59	221.58	
				SLE Freq.		0.00			-679.70			5.50	0.00	43.76	212.69	0.0223
				SLE Q.P.		0.00			-679.70			5.50	0.00	43.76	212.69	0.0223
10154	4.54	8.04	8.04			3839.05	13228.33	0.13	-4895.17	-13228.33	0.13					
				SLE Rare		1289.49			0.00			0.00	10.43	403.49	83.01	
				SLE Freq.		1481.79			0.00			0.00	11.99	463.67	95.39	0.0100
				SLE Q.P.		1482.15			0.00			0.00	11.99	463.78	95.42	0.0100

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 363 10154 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	3116.90	8701.28	50188.84	61680.39	134.60	6941.10	4173.10	ø 10 2br. 10.0'
0.63	4.04	3.41	2866.90	8701.28	50188.84	41120.26	134.60	6941.10	4173.10	ø 10 2br. 15.0'
4.04	4.54	0.50	2083.16	8701.28	50188.84	61680.39	134.60	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 215 Nodi 372 10369*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
372	0.13	8.04	8.04			2069.35	13228.33	0.13	-1046.54	-13228.33	0.13					
				SLE Rare		14.98			-424.51			3.43	0.12	27.33	132.83	
				SLE Freq.		0.00			-439.70			3.56	0.00	28.31	137.59	0.0144
				SLE Q.P.		0.00			-440.00			3.56	0.00	28.33	137.68	0.0144
Camp.	2.30	8.04	8.04	650.00	856.55	1078.56	13228.33	0.13	-1507.81	-13228.33	0.13					
				SLE Rare		0.00			-658.89			5.33	0.00	42.42	206.17	
				SLE Freq.		0.00			-658.89			5.33	0.00	42.42	206.17	0.0216
				SLE Q.P.		0.00			-658.89			5.33	0.00	42.42	206.17	0.0216
10369	4.47	8.04	8.04			3638.44	13228.33	0.13	-1943.72	-13228.33	0.13					
				SLE Rare		2428.88			0.00			0.00	19.65	760.02	156.37	
				SLE Freq.		2553.74			0.00			0.00	20.66	799.09	164.40	0.0172
				SLE Q.P.		2554.03			0.00			0.00	20.66	799.19	164.42	0.0172

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 372 10369 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	2002.73	8701.28	50188.84	61680.39	149.28	6941.10	4173.10	ø 10 2br. 10.0'
0.63	3.97	3.34	2140.18	8701.28	50188.84	41120.26	149.28	6941.10	4173.10	ø 10 2br. 15.0'
3.97	4.47	0.50	2465.18	8701.28	50188.84	61680.39	149.28	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 216 Nodi 366 10259*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
366	0.13	8.04	8.04			2322.69	13228.33	0.13	-1961.82	-13228.33	0.13					
				SLE Rare		0.00			-1084.51			8.77	0.00	69.82	339.36	
				SLE Freq.		0.00			-1111.07			8.99	0.00	71.53	347.67	0.0365
				SLE Q.P.		0.00			-1111.66			8.99	0.00	71.57	347.85	0.0365
Camp.	2.32	8.04	8.04	650.00	873.94	1122.33	13228.33	0.13	-2351.13	-13228.33	0.13					
				SLE Rare		0.00			-802.04			6.49	0.00	51.63	250.97	
				SLE Freq.		0.00			-672.26			5.44	0.00	43.28	210.36	0.0221
				SLE Q.P.		0.00			-672.26			5.44	0.00	43.28	210.36	0.0221
10259	4.51	8.04	8.04			4457.58	13228.33	0.13	-3401.83	-13228.33	0.13					
				SLE Rare		2522.10			0.00			0.00	20.41	789.19	162.37	
				SLE Freq.		2691.23			0.00			0.00	21.77	842.12	173.25	0.0182

			SLE Q.P.	2691.71			0.00			0.00	21.78	842.27	173.29	0.0182

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 366 10259 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	2401.58	8701.28	50188.84	61680.39	66.40	6941.10	4173.10	ø 10 2br. 10.0'
0.63	4.01	3.39	2409.59	8701.28	50188.84	41120.26	66.40	6941.10	4173.10	ø 10 2br. 15.0'
4.01	4.51	0.50	2734.59	8701.28	50188.84	61680.39	66.40	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 217 Nodi 357 10050*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
357	0.13	8.04	8.04			5496.06	13228.33	0.13	0.00	-13228.33	0.13					
				SLE Rare		2972.21			0.00			0.00	24.05	930.04	191.34	
				SLE Freq.		2766.00			0.00			0.00	22.38	865.51	178.07	0.0187
				SLE Q.P.		2697.26			0.00			0.00	21.82	844.00	173.64	0.0182
Camp.	2.35	8.04	8.04	650.00	896.52	853.20	13228.33	0.13	-2557.93	-13228.33	0.13					
				SLE Rare		0.00			-689.63			5.58	0.00	44.40	215.79	
				SLE Freq.		0.00			-689.63			5.58	0.00	44.40	215.79	0.0226
				SLE Q.P.		0.00			-689.63			5.58	0.00	44.40	215.79	0.0226
10050	4.57	8.04	8.04			1863.49	13228.33	0.13	-5673.82	-13228.33	0.13					
				SLE Rare		0.00			-1442.18			11.67	0.00	92.84	451.28	
				SLE Freq.		0.00			-879.60			7.12	0.00	56.63	275.24	0.0289
				SLE Q.P.		0.00			-692.07			5.60	0.00	44.55	216.56	0.0227

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 357 10050 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	3623.31	8701.28	50188.84	61680.39	296.75	6941.10	4173.10	ø 10 2br. 10.0'
0.63	4.07	3.45	3373.31	8701.28	50188.84	41120.26	296.75	6941.10	4173.10	ø 10 2br. 15.0'
4.07	4.57	0.50	1649.47	8701.28	50188.84	61680.39	296.75	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 218 Nodi 266 8267*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
266	0.13	4.54	7.57			0.00	6122.58	0.14	-6776.84	-9538.68	0.16					
				SLE Rare		0.00			-4444.89			59.37	0.00	309.33	1822.33	
				SLE Freq.		0.00			-4208.93			56.22	0.00	292.91	1725.59	0.1663
				SLE Q.P.		0.00			-4130.25			55.16	0.00	287.44	1693.33	0.1632
Camp.	2.32	6.03	6.03	520.00	699.15	2429.48	7803.06	0.15	-886.45	-7803.06	0.15					
				SLE Rare		475.96			-537.81			7.66	6.78	258.12	291.65	
				SLE Freq.		407.68			-537.81			7.66	5.81	221.09	291.65	0.0316
				SLE Q.P.		384.92			-537.81			7.66	5.48	208.75	291.65	0.0316
8267	4.51	10.05	6.03			10811.11	12344.55	0.18	0.00	-7819.74	0.15					
				SLE Rare		7326.67			0.00			0.00	86.26	2433.98	661.66	
				SLE Freq.		6954.15			0.00			0.00	81.87	2310.23	628.02	0.0453
				SLE Q.P.		6829.96			0.00			0.00	80.41	2268.97	616.80	0.0445

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 266 8267 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	3075.16	7589.68	38935.73	63800.94	66.70	5004.46	2842.47	ø 10 2br. 7.5'
0.52	4.11	3.59	4940.99	7037.02	38935.73	38280.56	66.70	5004.46	2832.32	ø 10 2br. 12.5'
4.11	4.51	0.40	5148.99	7037.02	38935.73	63800.94	66.70	5004.46	3776.43	ø 10 2br. 7.5'

Travata: *Travata 219 Nodi 272 8474*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm

Trave Sez. 1 Rett. 40x40 [cm]																
272	0.13	4.54	7.57			0.00	6122.58	0.14	-6584.99	-9538.68	0.16					
				SLE Rare		0.00			-4323.21			57.74	0.00	300.87	1772.45	
				SLE Freq.		0.00			-4095.00			54.69	0.00	284.98	1678.88	0.1618
				SLE Q.P.		0.00			-4018.91			53.68	0.00	279.69	1647.69	0.1588
Camp.	2.30	6.03	6.03	520.00	685.24	2281.60	7803.06	0.15	-886.35	-7803.06	0.15					
				SLE Rare		407.46			-527.11			7.51	5.81	220.97	285.85	
				SLE Freq.		349.13			-527.11			7.51	4.97	189.33	285.85	0.0310
				SLE Q.P.		329.69			-527.11			7.51	4.70	178.79	285.85	0.0310
8474	4.47	10.05	6.03			10357.00	12344.55	0.18	0.00	-7819.74	0.15					
				SLE Rare		7027.41			0.00			0.00	82.73	2334.56	634.64	
				SLE Freq.		6682.54			0.00			0.00	78.67	2219.99	603.49	0.0435
				SLE Q.P.		6567.56			0.00			0.00	77.32	2181.80	593.11	0.0428

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**T_{Ed} [kgm]**	**T_{Rcd} [kgm]**	**T_{Rsd} [kgm]**	**Staffe**
Trave 272 8474 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	2981.24	7589.68	38935.73	63800.94	73.15	5004.46	2842.47	ø 10 2br. 7.5'
0.52	4.07	3.54	4822.95	7037.02	38935.73	38280.56	73.15	5004.46	2832.32	ø 10 2br. 12.5'
4.07	4.47	0.40	5030.95	7037.02	38935.73	63800.94	73.15	5004.46	3776.43	ø 10 2br. 7.5'

Travata: *Travata 22 Nodi 205 5856*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 1 Rett. 40x40 [cm]																
205	0.13	6.03	8.04			0.00	7812.95	0.15	-7616.73	-10079.37	0.16					
				SLE Rare		0.00			-5073.16			64.72	0.00	452.28	2086.93	
				SLE Freq.		0.00			-4808.26			61.34	0.00	428.66	1977.96	0.2037
				SLE Q.P.		0.00			-4719.21			60.21	0.00	420.72	1941.32	0.1980
Camp.	1.77	6.03	6.03	520.00	409.58	2569.04	7803.06	0.15	-1707.78	-7803.06	0.15					
				SLE Rare		242.35			-315.06			4.49	3.45	131.42	170.86	
				SLE Freq.		220.99			-315.06			4.49	3.15	119.84	170.86	0.0185
				SLE Q.P.		213.89			-315.06			4.49	3.05	116.00	170.86	0.0185
5856	3.42	8.04	6.03			9807.38	10079.37	0.16	0.00	-7812.94	0.15					
				SLE Rare		6648.66			0.00			0.00	84.82	2735.03	592.74	
				SLE Freq.		6341.05			0.00			0.00	80.90	2608.49	565.31	0.0480
				SLE Q.P.		6237.82			0.00			0.00	79.58	2566.03	556.11	0.0472

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**T_{Ed} [kgm]**	**T_{Rcd} [kgm]**	**T_{Rsd} [kgm]**	**Staffe**
Trave 205 5856 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	4630.03	7745.24	38935.73	63800.94	149.37	5004.46	3304.37	ø 10 2br. 7.5'
0.52	3.03	2.50	5930.03	7037.02	38935.73	38280.56	149.37	5004.46	2832.32	ø 10 2br. 12.5'
3.03	3.42	0.40	6138.03	7037.02	38935.73	63800.94	149.37	5004.46	3304.37	ø 10 2br. 7.5'

Travata: *Travata 220 Nodi 278 8651*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 1 Rett. 40x40 [cm]																
278	0.13	6.03	6.03			0.00	7803.06	0.15	-2815.88	-7803.06	0.15					
				SLE Rare		0.00			-1818.67			25.91	0.00	155.53	986.27	
				SLE Freq.		0.00			-1731.24			24.67	0.00	148.05	938.86	0.1018
				SLE Q.P.		0.00			-1702.05			24.25	0.00	145.55	923.03	0.1001
Camp.	2.33	6.03	6.03	520.00	705.27	967.57	7803.06	0.15	-705.27	-7803.06	0.15					
				SLE Rare		58.85			-542.51			7.73	0.84	46.39	294.21	
				SLE Freq.		41.90			-542.51			7.73	0.60	46.39	294.21	0.0319
				SLE Q.P.		36.25			-542.51			7.73	0.52	46.39	294.21	0.0319
8651	4.53	6.03	6.03			5641.88	7803.06	0.15	0.00	-7803.06	0.15					

			SLE Rare	3884.09			0.00			0.00	55.34	2106.35	332.15	
			SLE Freq.	3762.78			0.00			0.00	53.62	2040.57	321.78	0.0349
			SLE Q.P.	3722.27			0.00			0.00	53.04	2018.60	318.31	0.0345

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 278 8651 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	980.38	7037.02	38935.73	63800.94	194.54	5004.46	2832.32	ø 10 2br. 7.5'
0.52	4.13	3.61	2856.74	7037.02	38935.73	38280.56	194.54	5004.46	2832.32	ø 10 2br. 12.5'
4.13	4.53	0.40	3064.74	7037.02	38935.73	63800.94	194.54	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 221 Nodi 257 7877*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
257	0.12	4.54	5.68			0.00	6105.08	0.14	-4161.14	-7386.30	0.14					
				SLE Rare		0.00			-2696.02			40.19	0.00	179.19	1456.65	
				SLE Freq.		0.00			-2542.73			37.91	0.00	169.00	1373.83	0.1537
				SLE Q.P.		0.00			-2491.61			37.14	0.00	165.60	1346.21	0.1506
Camp.	2.35	6.03	6.03	520.00	717.84	1884.18	7803.06	0.15	-717.84	-7803.06	0.15					
				SLE Rare		443.24			-552.19			7.87	6.32	240.37	299.45	
				SLE Freq.		384.27			-552.19			7.87	5.48	208.39	299.45	0.0325
				SLE Q.P.		364.62			-552.19			7.87	5.20	197.73	299.45	0.0325
7877	4.57	8.04	6.03			8175.99	10079.37	0.16	0.00	-7812.94	0.15					
				SLE Rare		5566.95			0.00			0.00	71.02	2290.06	496.30	
				SLE Freq.		5295.72			0.00			0.00	67.56	2178.48	472.12	0.0401
				SLE Q.P.		5205.28			0.00			0.00	66.41	2141.28	464.06	0.0394

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 257 7877 Sez. 1 Rett. 40x40 [cm]										
0.12	0.52	0.40	1823.62	6895.68	38935.73	63800.94	124.55	5004.46	2398.29	ø 10 2br. 7.5'
0.52	4.17	3.65	3721.49	7037.02	38935.73	38280.56	124.55	5004.46	2832.32	ø 10 2br. 12.5'
4.17	4.57	0.40	3929.49	7037.02	38935.73	63800.94	124.55	5004.46	3304.37	ø 10 2br. 7.5'

Travata: *Travata 222 Nodi 263 8079*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
263	0.13	4.54	5.68			0.00	6105.08	0.14	-5992.34	-7386.30	0.14					
				SLE Rare		0.00			-3919.27			58.43	0.00	260.49	2117.57	
				SLE Freq.		0.00			-3703.62			55.21	0.00	246.16	2001.06	0.2239
				SLE Q.P.		0.00			-3631.67			54.14	0.00	241.38	1962.18	0.2195
Camp.	2.33	6.03	6.03	520.00	706.89	2266.86	7803.06	0.15	-851.22	-7803.06	0.15					
				SLE Rare		468.67			-543.76			7.75	6.68	254.16	294.89	
				SLE Freq.		398.48			-543.76			7.75	5.68	216.09	294.89	0.0320
				SLE Q.P.		375.08			-543.76			7.75	5.34	203.41	294.89	0.0320
8079	4.54	10.05	6.03			10035.66	12344.55	0.18	0.00	-7819.74	0.15					
				SLE Rare		6809.08			0.00			0.00	80.16	2262.03	614.92	
				SLE Freq.		6453.04			0.00			0.00	75.97	2143.75	582.76	0.0420
				SLE Q.P.		6334.30			0.00			0.00	74.57	2104.30	572.04	0.0412

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 263 8079 Sez. 1 Rett. 40x40 [cm]										
0.13	0.53	0.40	2691.81	6895.68	38935.73	63800.94	77.51	5004.46	2398.29	ø 10 2br. 7.5'
0.53	4.14	3.61	4570.96	7037.02	38935.73	38280.56	77.51	5004.46	2832.32	ø 10 2br. 12.5'
4.14	4.54	0.40	4778.96	7037.02	38935.73	63800.94	77.51	5004.46	3776.43	ø 10 2br. 7.5'

Travata: *Travata 24 Nodi 207 5861*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
207	0.13	6.03	8.04			0.00	7812.95	0.15	-7188.46	-10079.37	0.16					
				SLE Rare		0.00			-4781.72			61.01	0.00	426.30	1967.04	
				SLE Freq.		0.00			-4529.50			57.79	0.00	403.81	1863.29	0.1857
				SLE Q.P.		0.00			-4444.45			56.70	0.00	396.23	1828.30	0.1803
Camp.	1.77	6.03	6.03	520.00	409.58	2532.96	7803.06	0.15	-1560.83	-7803.06	0.15					
				SLE Rare		280.17			-315.06			4.49	3.99	151.94	170.86	
				SLE Freq.		256.29			-315.06			4.49	3.65	138.99	170.86	0.0185
				SLE Q.P.		248.37			-315.06			4.49	3.54	134.69	170.86	0.0185
5861	3.42	8.04	6.03			9489.97	10079.37	0.16	0.00	-7812.94	0.15					
				SLE Rare		6432.89			0.00			0.00	82.07	2646.27	573.50	
				SLE Freq.		6132.91			0.00			0.00	78.24	2522.87	546.76	0.0464
				SLE Q.P.		6032.00			0.00			0.00	76.96	2481.36	537.76	0.0457

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 207 5861 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	4404.07	7745.24	38935.73	63800.94	158.96	5004.46	3304.37	ø 10 2br. 7.5'
0.52	3.03	2.50	5704.07	7037.02	38935.73	38280.56	158.96	5004.46	2832.32	ø 10 2br. 12.5'
3.03	3.42	0.40	5912.07	7037.02	38935.73	63800.94	158.96	5004.46	3304.37	ø 10 2br. 7.5'

Travata: *Travata 27 Nodi 8904 303*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
8904	0.13	8.04	8.04			9663.47	13228.33	0.13	0.00	-13228.33	0.13					
				SLE Rare		6423.71			0.00			0.00	51.97	2010.05	413.54	
				SLE Freq.		6051.95			0.00			0.00	48.97	1893.72	389.61	0.0408
				SLE Q.P.		5926.31			0.00			0.00	47.95	1854.41	381.52	0.0400
Camp.	1.77	8.04	8.04	650.00	511.98	3936.97	13228.33	0.13	-567.34	-13228.33	0.13					
				SLE Rare		1052.27			-393.83			3.19	8.51	329.27	123.23	
				SLE Freq.		1015.64			-393.83			3.19	8.22	317.81	123.23	0.0129
				SLE Q.P.		1003.36			-393.83			3.19	8.12	313.96	123.23	0.0129
303	3.42	8.04	8.04			51.77	13228.33	0.13	-4698.10	-13228.33	0.13					
				SLE Rare		0.00			-2955.64			23.91	0.00	190.28	924.85	
				SLE Freq.		0.00			-2657.14			21.50	0.00	171.06	831.45	0.0872
				SLE Q.P.		0.00			-2556.08			20.68	0.00	164.55	799.83	0.0839

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 8904 303 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	5424.49	8701.28	50188.84	61680.39	81.26	6941.10	4173.10	ø 10 2br. 10.0'
0.63	2.92	2.30	5099.49	8701.28	50188.84	41120.26	81.26	6941.10	4173.10	ø 10 2br. 15.0'
2.92	3.42	0.50	3604.49	8701.28	50188.84	61680.39	81.26	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 277 Nodi 163 5021*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
163	0.13	6.03	6.03			2167.16	7803.06	0.15	-1392.08	-7803.06	0.15					
				SLE Rare		926.19			0.00			0.00	13.20	502.28	79.20	
				SLE Freq.		867.18			0.00			0.00	12.36	470.27	74.16	0.0080
				SLE Q.P.		847.50			0.00			0.00	12.08	459.60	72.48	0.0079
Camp.	2.33	6.03	6.03	520.00	706.89	0.00	7803.06	0.15	-1758.59	-7803.06	0.15					
				SLE Rare		0.00			-1118.18			15.93	0.00	95.62	606.39	

				SLE Freq.		0.00			-1078.22			15.36	0.00	92.21	584.73	0.0634
				SLE Q.P.		0.00			-1065.93			15.19	0.00	91.15	578.06	0.0627
5021	4.54	6.03	6.03			2339.90	7803.06	0.15	-2828.81	-7803.06	0.15					
				SLE Rare		0.00			-1186.93			16.91	0.00	101.50	643.67	
				SLE Freq.		0.00			-1054.34			15.02	0.00	90.16	571.77	0.0620
				SLE Q.P.		0.00			-1010.15			14.39	0.00	86.38	547.81	0.0594

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 163 5021 Sez. 1 Rett. 40x40 [cm]										
0.13	0.53	0.40	2014.66	7037.02	38935.73	63800.94	90.17	5004.46	2832.32	ø 10 2br. 7.5'
0.53	4.14	3.61	1854.66	7037.02	38935.73	38280.56	90.17	5004.46	2832.32	ø 10 2br. 12.5'
4.14	4.54	0.40	1727.38	7037.02	38935.73	63800.94	90.17	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 278 Nodi 166 5209*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
166	0.13	6.03	6.03			1376.69	7803.06	0.15	-1521.95	-7803.06	0.15					
				SLE Rare		433.06			0.00			0.00	6.17	234.85	37.03	
				SLE Freq.		397.42			0.00			0.00	5.66	215.52	33.99	0.0037
				SLE Q.P.		385.54			0.00			0.00	5.49	209.08	32.97	0.0036
Camp.	2.32	6.03	6.03	520.00	699.15	0.00	7803.06	0.15	-1534.34	-7803.06	0.15					
				SLE Rare		0.00			-1063.63			15.16	0.00	90.96	576.81	
				SLE Freq.		0.00			-1030.47			14.68	0.00	88.12	558.83	0.0606
				SLE Q.P.		0.00			-1019.43			14.53	0.00	87.18	552.84	0.0600
5209	4.51	6.03	6.03			2484.59	7803.06	0.15	-1906.13	-7803.06	0.15					
				SLE Rare		0.00			-609.34			8.68	0.00	52.11	330.45	
				SLE Freq.		0.00			-507.07			7.23	0.00	43.36	274.99	0.0298
				SLE Q.P.		0.00			-472.98			6.74	0.00	40.45	256.50	0.0278

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 166 5209 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	1620.22	7037.02	38935.73	63800.94	84.33	5004.46	2832.32	ø 10 2br. 7.5'
0.52	4.11	3.59	1630.67	7037.02	38935.73	38280.56	84.33	5004.46	2832.32	ø 10 2br. 12.5'
4.11	4.51	0.40	1790.67	7037.02	38935.73	63800.94	84.33	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 279 Nodi 172 5416*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
172	0.13	6.03	6.03			750.65	7803.06	0.15	-1091.80	-7803.06	0.15					
				SLE Rare		254.07			0.00			0.00	3.62	137.78	21.73	
				SLE Freq.		238.53			0.00			0.00	3.40	129.36	20.40	0.0022
				SLE Q.P.		233.35			0.00			0.00	3.32	126.55	19.96	0.0022
Camp.	2.30	6.03	6.03	520.00	685.24	0.00	7803.06	0.15	-1397.72	-7803.06	0.15					
				SLE Rare		0.00			-1009.96			14.39	0.00	86.37	547.71	
				SLE Freq.		0.00			-981.39			13.98	0.00	83.92	532.21	0.0577
				SLE Q.P.		0.00			-971.86			13.85	0.00	83.11	527.05	0.0572
5416	4.47	6.03	6.03			1952.56	7803.06	0.15	-1184.52	-7803.06	0.15					
				SLE Rare		0.00			-352.10			5.02	0.00	30.11	190.94	
				SLE Freq.		0.00			-280.36			3.99	0.00	23.98	152.04	0.0165
				SLE Q.P.		0.00			-256.45			3.65	0.00	21.93	139.07	0.0151

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 172 5416 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	1279.04	7037.02	38935.73	63800.94	91.17	5004.46	2832.32	ø 10 2br. 7.5'
0.52	4.07	3.54	1399.42	7037.02	38935.73	38280.56	91.17	5004.46	2832.32	ø 10 2br. 12.5'
4.07	4.47	0.40	1559.42	7037.02	38935.73	63800.94	91.17	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 28 Nodi 8909 304*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
8909	0.13	8.04	8.04			10519.07	13228.33	0.13	0.00	-13228.33	0.13					
				SLE Rare		6998.52			0.00			0.00	56.62	2189.92	450.55	
				SLE Freq.		6614.24			0.00			0.00	53.52	2069.67	425.81	0.0446
				SLE Q.P.		6484.93			0.00			0.00	52.47	2029.21	417.48	0.0438
Camp.	1.77	8.04	8.04	650.00	511.98	4204.78	13228.33	0.13	-836.72	-13228.33	0.13					
				SLE Rare		1052.59			-393.83			3.19	8.52	329.37	123.23	
				SLE Freq.		1018.88			-393.83			3.19	8.24	318.82	123.23	0.0129
				SLE Q.P.		1007.59			-393.83			3.19	8.15	315.29	123.23	0.0129
304	3.42	8.04	8.04			0.00	13228.33	0.13	-5555.28	-13228.33	0.13					
				SLE Rare		0.00			-3529.81			28.56	0.00	227.24	1104.52	
				SLE Freq.		0.00			-3212.95			26.00	0.00	206.84	1005.37	0.1054
				SLE Q.P.		0.00			-3106.23			25.13	0.00	199.97	971.97	0.1019

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 8909 304 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	5943.52	8701.28	50188.84	61680.39	43.96	6941.10	4173.10	ø 10 2br. 10.0'
0.63	2.92	2.30	5618.52	8701.28	50188.84	41120.26	43.96	6941.10	4173.10	ø 10 2br. 15.0'
2.92	3.42	0.50	4123.52	8701.28	50188.84	61680.39	43.96	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 280 Nodi 178 5593*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
178	0.13	6.03	6.03			1104.25	7803.06	0.15	-482.84	-7803.06	0.15					
				SLE Rare		651.13			0.00			0.00	9.28	353.11	55.68	
				SLE Freq.		643.79			0.00			0.00	9.17	349.13	55.05	0.0060
				SLE Q.P.		641.37			0.00			0.00	9.14	347.82	54.85	0.0059
Camp.	2.33	6.03	6.03	520.00	705.27	0.00	7803.06	0.15	-1172.81	-7803.06	0.15					
				SLE Rare		0.00			-828.16			11.80	0.00	70.82	449.12	
				SLE Freq.		0.00			-811.73			11.57	0.00	69.42	440.20	0.0477
				SLE Q.P.		0.00			-806.25			11.49	0.00	68.95	437.23	0.0474
5593	4.53	6.03	6.03			1321.14	7803.06	0.15	-1056.45	-7803.06	0.15					
				SLE Rare		0.00			-302.65			4.31	0.00	25.88	164.13	
				SLE Freq.		0.00			-258.80			3.69	0.00	22.13	140.35	0.0152
				SLE Q.P.		0.00			-244.20			3.48	0.00	20.88	132.43	0.0144

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 178 5593 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	1429.98	7037.02	38935.73	63800.94	237.22	5004.46	2832.32	ø 10 2br. 7.5'
0.52	4.13	3.61	1221.98	7037.02	38935.73	38280.56	237.22	5004.46	2832.32	ø 10 2br. 12.5'
4.13	4.53	0.40	1251.47	7037.02	38935.73	63800.94	237.22	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 281 Nodi 157 4819*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
157	0.12	6.03	6.03			3010.82	7803.06	0.15	-535.50	-7803.06	0.15					
				SLE Rare		1918.45			0.00			0.00	27.34	1040.38	164.06	
				SLE Freq.		1842.97			0.00			0.00	26.26	999.45	157.60	0.0171
				SLE Q.P.		1817.81			0.00			0.00	25.90	985.80	155.45	0.0169
Camp.	2.35	6.03	6.03	520.00	717.84	0.00	7803.06	0.15	-2152.04	-7803.06	0.15					
				SLE Rare		0.00			-1188.29			16.93	0.00	101.62	644.41	
				SLE Freq.		0.00			-1148.50			16.36	0.00	98.22	622.83	0.0675
				SLE Q.P.		0.00			-1135.23			16.18	0.00	97.08	615.64	0.0668
4819	4.57	6.03	6.03			1196.29	7803.06	0.15	-3747.08	-7803.06	0.15					
				SLE Rare		0.00			-2284.46			32.55	0.00	195.36	1238.87	
				SLE Freq.		0.00			-2139.11			30.48	0.00	182.93	1160.04	0.1258
				SLE Q.P.		0.00			-2090.65			29.79	0.00	178.78	1133.77	0.1230

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 157 4819 Sez. 1 Rett. 40x40 [cm]										
0.12	0.52	0.40	2489.71	7037.02	38935.73	63800.94	198.17	5004.46	2832.32	ø 10 2br. 7.5'
0.52	4.17	3.65	2281.71	7037.02	38935.73	38280.56	198.17	5004.46	2832.32	ø 10 2br. 12.5'
4.17	4.57	0.40	1237.32	7037.02	38935.73	63800.94	198.17	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 29 Nodi 8914 305*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
8914	0.13	8.04	8.04			10493.20	13228.33	0.13	0.00	-13228.33	0.13					
				SLE Rare		6987.36			0.00			0.00	56.53	2186.42	449.83	
				SLE Freq.		6624.07			0.00			0.00	53.59	2072.75	426.44	0.0447
				SLE Q.P.		6501.72			0.00			0.00	52.61	2034.46	418.57	0.0439
Camp.	1.77	8.04	8.04	650.00	511.98	4172.75	13228.33	0.13	-874.38	-13228.33	0.13					
				SLE Rare		1029.47			-393.83			3.19	8.33	322.13	123.23	
				SLE Freq.		1001.87			-393.83			3.19	8.11	313.50	123.23	0.0129
				SLE Q.P.		992.61			-393.83			3.19	8.03	310.60	123.23	0.0129
305	3.42	8.04	8.04			0.00	13228.33	0.13	-5599.11	-13228.33	0.13					
				SLE Rare		0.00			-3564.88			28.84	0.00	229.50	1115.49	
				SLE Freq.		0.00			-3256.82			26.35	0.00	209.67	1019.10	0.1069
				SLE Q.P.		0.00			-3152.98			25.51	0.00	202.98	986.60	0.1034

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 8914 305 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	5948.96	8701.28	50188.84	61680.39	43.75	6941.10	4173.10	ø 10 2br. 10.0'
0.63	2.92	2.30	5623.96	8701.28	50188.84	41120.26	43.75	6941.10	4173.10	ø 10 2br. 15.0'
2.92	3.42	0.50	4128.96	8701.28	50188.84	61680.39	43.75	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 3 Nodi 148 4373*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
148	0.13	6.03	6.03			3730.23	7803.06	0.15	0.00	-7803.06	0.15					
				SLE Rare		2721.67			0.00			0.00	38.78	1475.97	232.75	
				SLE Freq.		2648.67			0.00			0.00	37.74	1436.38	226.50	0.0246
				SLE Q.P.		2624.76			0.00			0.00	37.40	1423.42	224.46	0.0243
Camp.	2.13	6.03	6.03	520.00	587.03	192.00	7803.06	0.15	-1462.07	-7803.06	0.15					
				SLE Rare		0.00			-612.72			8.73	0.00	52.40	332.28	

				SLE Freq.		0.00			-602.62			8.59	0.00	51.53	326.80	0.0354
				SLE Q.P.		0.00			-599.32			8.54	0.00	51.25	325.02	0.0352
4373	4.13	6.03	6.03			0.00	7803.06	0.15	-3244.53	-7803.06	0.15					
				SLE Rare		0.00			-2279.16			32.48	0.00	194.90	1235.99	
				SLE Freq.		0.00			-2183.72			31.12	0.00	186.74	1184.24	0.1284
				SLE Q.P.		0.00			-2152.49			30.67	0.00	184.07	1167.30	0.1266

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 148 4373 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	2783.69	7037.02	38935.73	63800.94	298.86	5004.46	2832.32	ø 10 2br. 7.5'
0.52	3.72	3.20	2575.69	7037.02	38935.73	38280.56	298.86	5004.46	2832.32	ø 10 2br. 12.5'
3.72	4.13	0.40	911.69	7037.02	38935.73	63800.94	298.86	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 301 Nodi 333 9432*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
333	0.13	8.04	8.04			1235.51	13228.33	0.13	-288.21	-13228.33	0.13					
				SLE Rare		156.89			0.00			0.00	1.27	49.09	10.10	
				SLE Freq.		174.75			0.00			0.00	1.41	54.68	11.25	0.0012
				SLE Q.P.		185.12			0.00			0.00	1.50	57.93	11.92	0.0012
Camp.	2.13	8.04	8.04	650.00	733.79	224.95	13228.33	0.13	-733.79	-13228.33	0.13					
				SLE Rare		0.00			-564.45			4.57	0.00	36.34	176.62	
				SLE Freq.		0.00			-564.45			4.57	0.00	36.34	176.62	0.0185
				SLE Q.P.		0.00			-564.45			4.57	0.00	36.34	176.62	0.0185
9432	4.13	8.04	8.04			191.40	13228.33	0.13	-128.26	-13228.33	0.13					
				SLE Rare		128.92			0.00			0.00	1.04	40.34	8.30	
				SLE Freq.		131.77			0.00			0.00	1.07	41.23	8.48	0.0009
				SLE Q.P.		131.92			0.00			0.00	1.07	41.28	8.49	0.0009

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 333 9432 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	1599.17	8701.28	50188.84	61680.39	963.56	6941.10	4173.10	ø 10 2br. 10.0'
0.63	3.63	3.00	2113.75	8701.28	50188.84	41120.26	963.56	6941.10	4173.10	ø 10 2br. 15.0'
3.63	4.13	0.50	404.70	8701.28	50188.84	61680.39	963.56	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 304 Nodi 351 9938*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
351	0.13	8.04	8.04			858.35	13228.33	0.13	0.00	-13228.33	0.13					
				SLE Rare		589.91			0.00			0.00	4.77	184.59	37.98	
				SLE Freq.		591.88			0.00			0.00	4.79	185.21	38.10	0.0040
				SLE Q.P.		591.80			0.00			0.00	4.79	185.18	38.10	0.0040
Camp.	2.36	8.04	8.04	650.00	905.14	642.01	13228.33	0.13	-905.04	-13228.33	0.13					
				SLE Rare		364.25			-696.18			5.63	2.95	113.98	217.84	
				SLE Freq.		351.55			-696.18			5.63	2.84	110.00	217.84	0.0228
				SLE Q.P.		347.34			-696.18			5.63	2.81	108.69	217.84	0.0228
9938	4.60	8.04	8.04			494.24	13228.33	0.13	0.00	-13228.33	0.13					
				SLE Rare		284.35			0.00			0.00	2.30	88.98	18.31	
				SLE Freq.		277.13			0.00			0.00	2.24	86.72	17.84	0.0019
				SLE Q.P.		274.74			0.00			0.00	2.22	85.97	17.69	0.0019

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 351 9938 Sez. 5 Rett. 40x50 [cm]										
0.12	0.62	0.50	678.01	8701.28	50188.84	61680.39	1877.58	6941.10	4173.10	ø 10 2br. 10.0'
0.62	4.10	3.47	640.89	8701.28	50188.84	41120.26	1877.58	6941.10	4173.10	ø 10 2br. 15.0'
4.10	4.60	0.50	715.06	8701.28	50188.84	61680.39	1877.58	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 31 Nodi 8919 307*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
8919	0.13	8.04	8.04			9750.93	13228.33	0.13	0.00	-13228.33	0.13					
				SLE Rare		6485.60			0.00			0.00	52.47	2029.42	417.53	
				SLE Freq.		6174.14			0.00			0.00	49.95	1931.96	397.48	0.0417
				SLE Q.P.		6068.42			0.00			0.00	49.10	1898.88	390.67	0.0410
Camp.	1.77	8.04	8.04	650.00	511.98	3791.77	13228.33	0.13	-925.18	-13228.33	0.13					
				SLE Rare		883.57			-393.83			3.19	7.15	276.48	123.23	
				SLE Freq.		869.50			-393.83			3.19	7.04	272.08	123.23	0.0129
				SLE Q.P.		864.78			-393.83			3.19	7.00	270.60	123.23	0.0129
307	3.42	8.04	8.04			0.00	13228.33	0.13	-5288.61	-13228.33	0.13					
				SLE Rare		0.00			-3354.93			27.14	0.00	215.98	1049.80	
				SLE Freq.		0.00			-3071.63			24.85	0.00	197.74	961.15	0.1008
				SLE Q.P.		0.00			-2975.35			24.07	0.00	191.55	931.02	0.0976

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 8919 307 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	5629.94	8701.28	50188.84	61680.39	97.52	6941.10	4173.10	ø 10 2br. 10.0'
0.63	2.92	2.30	5304.94	8701.28	50188.84	41120.26	97.52	6941.10	4173.10	ø 10 2br. 15.0'
2.92	3.42	0.50	3809.94	8701.28	50188.84	61680.39	97.52	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 334 Nodi 101 2978 2980 2992 3032 3038 3088 3122 111*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
101	0.12	15.62	6.49			15030.18	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10158.30			-17.25			0.26	115.63	2364.60	543.19	
				SLE Freq.		9221.24			-15.68			0.23	104.97	2146.48	493.08	0.0400
				SLE Q.P.		8908.88			-15.16			0.22	101.41	2073.77	476.38	0.0387
Camp.	0.43	14.24	9.42	5320.00	178.82	15030.18	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7246.03			-113.75			1.44	82.12	1846.07	521.57	
				SLE Freq.		6574.94			-103.42			1.31	74.52	1675.10	473.27	0.0374
				SLE Q.P.		6351.25			-99.98			1.26	71.98	1618.11	457.17	0.0362
2978	0.73	13.08	9.42			11864.06	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4666.77			0.00			0.00	54.46	1288.39	331.07	
				SLE Freq.		4231.42			0.00			0.00	49.38	1168.20	300.18	0.0253
				SLE Q.P.		4086.31			0.00			0.00	47.69	1128.13	289.89	0.0245
Trave Sez. 2 Rett. 40x40 [cm]																
2978	0.00	12.63	9.42			6664.46	14307.31	0.24	0.00	-11116.93	0.22					
				SLE Rare		4499.08			0.00			0.00	53.16	1284.49	316.97	
				SLE Freq.		4077.96			0.00			0.00	48.18	1164.26	287.30	0.0249
				SLE Q.P.		3937.58			0.00			0.00	46.53	1124.18	277.41	0.0241
Camp.	0.37	11.17	9.42	5320.00	183.71	6664.46	12854.87	0.23	-593.13	-11113.99	0.22					
				SLE Rare		1800.02			-124.31			1.61	22.23	577.59	123.26	
				SLE Freq.		1625.83			-113.02			1.47	20.08	521.70	111.33	0.0107
				SLE Q.P.		1567.77			-109.26			1.42	19.37	503.07	107.36	0.0103
2980	0.74	9.71	9.42			2835.67	11397.24	0.22	-593.13	-11110.44	0.22					
				SLE Rare		0.00			-408.90			5.37	0.00	26.38	154.31	

				SLE Freq.		0.00			-379.77			4.99	0.00	24.50	143.31	0.0161
				SLE Q.P.		0.00			-369.75			4.86	0.00	23.86	139.53	0.0157
Trave Sez. 2 Rett. 40x40 [cm]																
2980	0.00	9.42	9.42			0.00	11109.65	0.22	-3550.92	-11109.65	0.22					
				SLE Rare		0.00			-642.49			8.46	0.00	41.73	242.37	
				SLE Freq.		0.00			-592.57			7.81	0.00	38.48	223.54	0.0251
				SLE Q.P.		0.00			-575.63			7.58	0.00	37.38	217.15	0.0244
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5169.04	-11109.65	0.22					
				SLE Rare		0.00			-2308.96			30.42	0.00	149.95	871.04	
				SLE Freq.		0.00			-2106.11			27.74	0.00	136.78	794.51	0.0894
				SLE Q.P.		0.00			-2038.26			26.85	0.00	132.37	768.92	0.0865
2992	0.72	9.42	9.42			0.00	11109.65	0.22	-5169.04	-11109.65	0.22					
				SLE Rare		0.00			-3502.75			46.14	0.00	227.48	1321.39	
				SLE Freq.		0.00			-3189.90			42.02	0.00	207.16	1203.37	0.1353
				SLE Q.P.		0.00			-3085.46			40.65	0.00	200.38	1163.97	0.1309
Trave Sez. 2 Rett. 40x40 [cm]																
2992	0.00	9.42	9.42			0.00	11109.65	0.22	-6532.42	-11109.65	0.22					
				SLE Rare		0.00			-3669.95			48.35	0.00	238.34	1384.46	
				SLE Freq.		0.00			-3342.11			44.03	0.00	217.05	1260.79	0.1418
				SLE Q.P.		0.00			-3232.70			42.59	0.00	209.94	1219.51	0.1372
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6853.37	-11109.65	0.22					
				SLE Rare		0.00			-4400.39			57.97	0.00	285.77	1660.02	
				SLE Freq.		0.00			-4004.61			52.75	0.00	260.07	1510.71	0.1739
				SLE Q.P.		0.00			-3872.62			51.02	0.00	251.50	1460.92	0.1646
3032	0.74	9.42	9.42			0.00	11109.65	0.22	-6853.37	-11109.65	0.22					
				SLE Rare		0.00			-4639.61			61.12	0.00	301.31	1750.26	
				SLE Freq.		0.00			-4220.50			55.60	0.00	274.09	1592.15	0.1892
				SLE Q.P.		0.00			-4080.82			53.76	0.00	265.02	1539.46	0.1793
Trave Sez. 2 Rett. 40x40 [cm]																
3032	0.00	9.42	9.42			0.00	11109.65	0.22	-6859.11	-11109.65	0.22					
				SLE Rare		0.00			-4643.43			61.17	0.00	301.56	1751.70	
				SLE Freq.		0.00			-4224.02			55.64	0.00	274.32	1593.48	0.1894
				SLE Q.P.		0.00			-4084.26			53.80	0.00	265.24	1540.76	0.1796
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6859.11	-11109.65	0.22					
				SLE Rare		0.00			-4391.43			57.85	0.00	285.19	1656.64	
				SLE Freq.		0.00			-3993.59			52.61	0.00	259.36	1506.55	0.1731
				SLE Q.P.		0.00			-3860.98			50.86	0.00	250.74	1456.53	0.1638
3038	0.74	9.42	9.42			0.00	11109.65	0.22	-6524.43	-11109.65	0.22					
				SLE Rare		0.00			-3649.74			48.08	0.00	237.03	1376.84	
				SLE Freq.		0.00			-3317.51			43.70	0.00	215.45	1251.51	0.1408
				SLE Q.P.		0.00			-3206.77			42.24	0.00	208.26	1209.73	0.1361
Trave Sez. 2 Rett. 40x40 [cm]																
3038	0.00	9.42	9.42			0.00	11109.65	0.22	-5160.49	-11109.65	0.22					
				SLE Rare		0.00			-3490.90			45.99	0.00	226.71	1316.92	
				SLE Freq.		0.00			-3173.15			41.80	0.00	206.07	1197.05	0.1346
				SLE Q.P.		0.00			-3067.24			40.41	0.00	199.20	1157.09	0.1301
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5160.49	-11109.65	0.22					
				SLE Rare		0.00			-2286.07			30.12	0.00	148.46	862.41	
				SLE Freq.		0.00			-2076.04			27.35	0.00	134.82	783.17	0.0881
				SLE Q.P.		0.00			-2006.02			26.43	0.00	130.28	756.76	0.0851
3088	0.72	9.42	9.42			0.00	11109.65	0.22	-3531.29	-11109.65	0.22					
				SLE Rare		0.00			-608.57			8.02	0.00	39.52	229.58	
				SLE Freq.		0.00			-549.18			7.23	0.00	35.67	207.17	0.0233
				SLE Q.P.		0.00			-529.38			6.97	0.00	34.38	199.71	0.0225
Trave Sez. 2 Rett. 40x40 [cm]																

3088	0.00	9.71	9.42			2864.49	11397.24	0.22	-573.00	-11110.44	0.22					
				SLE Rare		0.00			-383.63			5.04	0.00	24.75	144.77	
				SLE Freq.		0.00			-344.80			4.53	0.00	22.25	130.11	0.0146
				SLE Q.P.		0.00			-331.85			4.36	0.00	21.41	125.23	0.0141
Camp.	0.37	11.17	9.42	5320.00	183.71	6704.97	12854.87	0.23	-573.00	-11113.99	0.22					
				SLE Rare		1833.89			-124.31			1.61	22.65	588.46	125.58	
				SLE Freq.		1672.76			-113.02			1.47	20.66	536.76	114.55	0.0110
				SLE Q.P.		1618.60			-109.26			1.42	19.99	519.38	110.84	0.0107
3122	0.74	12.63	9.42			6704.97	14307.31	0.24	0.00	-11116.93	0.22					
				SLE Rare		4544.27			0.00			0.00	53.69	1297.39	320.16	
				SLE Freq.		4138.55			0.00			0.00	48.90	1181.56	291.57	0.0253
				SLE Q.P.		4002.78			0.00			0.00	47.30	1142.80	282.01	0.0245
Trave Sez. 2 Rett. 40x40 [cm]																
3122	0.00	13.08	9.42			11903.19	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4701.41			0.00			0.00	54.86	1297.95	333.52	
				SLE Freq.		4281.09			0.00			0.00	49.96	1181.91	303.71	0.0256
				SLE Q.P.		4140.47			0.00			0.00	48.32	1143.09	293.73	0.0248
Camp.	0.30	14.24	9.42	5320.00	178.82	15076.55	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7289.93			-113.75			1.44	82.62	1857.25	524.73	
				SLE Freq.		6635.80			-103.42			1.31	75.21	1690.60	477.65	0.0378
				SLE Q.P.		6417.18			-99.98			1.26	72.73	1634.90	461.91	0.0365
111	0.61	15.62	6.49			15076.55	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10211.46			-17.25			0.26	116.24	2376.98	546.04	
				SLE Freq.		9293.28			-15.68			0.23	105.79	2163.25	496.94	0.0403
				SLE Q.P.		8986.57			-15.16			0.22	102.30	2091.85	480.54	0.0390

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 101 2978 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	14963.21	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 2978 2980 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11726.80	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 2980 2992 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7772.42	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 2992 3032 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3916.99	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3032 3038 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3949.90	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3038 3088 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7805.34	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3088 3122 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11759.72	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3122 111 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14996.13	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 335 Nodi 111 3176 3216 3266 3273 3307 3314 3321 120*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
111	0.13	15.62	6.49			15094.24	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10207.21			-17.25			0.26	116.19	2375.99	545.81	
				SLE Freq.		9273.07			-15.68			0.23	105.56	2158.54	495.86	0.0402
				SLE Q.P.		8961.69			-15.16			0.22	102.01	2086.06	479.21	0.0389
Camp.	0.43	14.24	9.42	5320.00	178.82	15094.24	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7287.37			-113.76			1.44	82.59	1856.60	524.55	
				SLE Freq.		6618.85			-103.42			1.31	75.02	1686.28	476.43	0.0377
				SLE Q.P.		6396.01			-99.98			1.26	72.49	1629.51	460.39	0.0364

3176	0.73	13.08	9.42			11920.84	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4700.55			0.00			0.00	54.85	1297.71	333.46	
				SLE Freq.		4267.39			0.00			0.00	49.80	1178.13	302.73	0.0255
				SLE Q.P.		4123.01			0.00			0.00	48.11	1138.27	292.49	0.0247
Trave Sez. 2 Rett. 40x40 [cm]																
3176	0.00	12.63	9.42			6712.13	14307.30	0.24	0.00	-11116.93	0.22					
				SLE Rare		4535.64			0.00			0.00	53.59	1294.93	319.55	
				SLE Freq.		4116.98			0.00			0.00	48.65	1175.40	290.05	0.0252
				SLE Q.P.		3977.43			0.00			0.00	47.00	1135.56	280.22	0.0243
Camp.	0.37	11.17	9.42	5320.00	183.71	6712.13	12854.87	0.23	-562.85	-11113.99	0.22					
				SLE Rare		1827.34			-124.31			1.61	22.57	586.36	125.13	
				SLE Freq.		1655.18			-113.02			1.47	20.45	531.11	113.34	0.0109
				SLE Q.P.		1597.79			-109.26			1.42	19.74	512.70	109.41	0.0105
3216	0.74	9.71	9.42			2871.63	11397.24	0.22	-562.85	-11110.44	0.22					
				SLE Rare		0.00			-386.05			5.07	0.00	24.91	145.68	
				SLE Freq.		0.00			-356.02			4.68	0.00	22.97	134.35	0.0151
				SLE Q.P.		0.00			-345.91			4.54	0.00	22.32	130.54	0.0147
Trave Sez. 2 Rett. 40x40 [cm]																
3216	0.00	9.42	9.42			0.00	11109.65	0.22	-3533.33	-11109.65	0.22					
				SLE Rare		0.00			-617.78			8.14	0.00	40.12	233.05	
				SLE Freq.		0.00			-566.88			7.47	0.00	36.82	213.85	0.0241
				SLE Q.P.		0.00			-549.82			7.24	0.00	35.71	207.42	0.0233
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5164.69	-11109.65	0.22					
				SLE Rare		0.00			-2294.78			30.23	0.00	149.03	865.69	
				SLE Freq.		0.00			-2091.10			27.55	0.00	135.80	788.85	0.0887
				SLE Q.P.		0.00			-2023.15			26.65	0.00	131.39	763.22	0.0858
3266	0.72	9.42	9.42			0.00	11109.65	0.22	-5164.69	-11109.65	0.22					
				SLE Rare		0.00			-3499.10			46.09	0.00	227.24	1320.01	
				SLE Freq.		0.00			-3185.58			41.96	0.00	206.88	1201.73	0.1352
				SLE Q.P.		0.00			-3081.04			40.59	0.00	200.09	1162.30	0.1307
Trave Sez. 2 Rett. 40x40 [cm]																
3266	0.00	9.42	9.42			0.00	11109.65	0.22	-6541.30	-11109.65	0.22					
				SLE Rare		0.00			-3664.87			48.28	0.00	238.01	1382.54	
				SLE Freq.		0.00			-3336.29			43.95	0.00	216.67	1258.59	0.1416
				SLE Q.P.		0.00			-3226.74			42.51	0.00	209.55	1217.27	0.1369
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6876.04	-11109.65	0.22					
				SLE Rare		0.00			-4406.04			58.04	0.00	286.14	1662.15	
				SLE Freq.		0.00			-4009.67			52.82	0.00	260.40	1512.62	0.1743
				SLE Q.P.		0.00			-3877.57			51.08	0.00	251.82	1462.78	0.1649
3273	0.74	9.42	9.42			0.00	11109.65	0.22	-6876.04	-11109.65	0.22					
				SLE Rare		0.00			-4655.99			61.33	0.00	302.37	1756.44	
				SLE Freq.		0.00			-4236.45			55.81	0.00	275.13	1598.17	0.1903
				SLE Q.P.		0.00			-4096.66			53.97	0.00	266.05	1545.44	0.1804
Trave Sez. 2 Rett. 40x40 [cm]																
3273	0.00	9.42	9.42			0.00	11109.65	0.22	-6879.54	-11109.65	0.22					
				SLE Rare		0.00			-4658.24			61.36	0.00	302.52	1757.29	
				SLE Freq.		0.00			-4238.36			55.83	0.00	275.25	1598.89	0.1905
				SLE Q.P.		0.00			-4098.46			53.99	0.00	266.17	1546.12	0.1806
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6879.54	-11109.65	0.22					
				SLE Rare		0.00			-4416.97			58.19	0.00	286.85	1666.27	
				SLE Freq.		0.00			-4018.54			52.94	0.00	260.98	1515.97	0.1749
				SLE Q.P.		0.00			-3885.83			51.19	0.00	252.36	1465.90	0.1655
3307	0.74	9.42	9.42			0.00	11109.65	0.22	-6558.64	-11109.65	0.22					
				SLE Rare		0.00			-3684.48			48.54	0.00	239.28	1389.94	
				SLE Freq.		0.00			-3352.12			44.16	0.00	217.70	1264.56	0.1422

				SLE Q.P.		0.00			-3241.47			42.70	0.00	210.51	1222.82	0.1375
Trave Sez. 2 Rett. 40x40 [cm]																
3307	0.00	9.42	9.42			0.00	11109.65	0.22	-5203.98	-11109.65	0.22					
				SLE Rare		0.00			-3523.00			46.41	0.00	228.79	1329.02	
				SLE Freq.		0.00			-3205.05			42.22	0.00	208.15	1209.08	0.1360
				SLE Q.P.		0.00			-3099.21			40.83	0.00	201.27	1169.15	0.1315
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5203.98	-11109.65	0.22					
				SLE Rare		0.00			-2327.19			30.66	0.00	151.14	877.92	
				SLE Freq.		0.00			-2117.41			27.89	0.00	137.51	798.78	0.0898
				SLE Q.P.		0.00			-2047.66			26.97	0.00	132.98	772.46	0.0869
3314	0.72	9.42	9.42			0.00	11109.65	0.22	-3585.92	-11109.65	0.22					
				SLE Rare		0.00			-658.71			8.68	0.00	42.78	248.49	
				SLE Freq.		0.00			-600.03			7.90	0.00	38.97	226.36	0.0255
				SLE Q.P.		0.00			-580.67			7.65	0.00	37.71	219.05	0.0246
Trave Sez. 2 Rett. 40x40 [cm]																
3314	0.00	9.71	9.42			2783.30	11397.24	0.22	-635.00	-11110.44	0.22					
				SLE Rare		0.00			-429.81			5.65	0.00	27.73	162.19	
				SLE Freq.		0.00			-391.62			5.15	0.00	25.27	147.78	0.0166
				SLE Q.P.		0.00			-379.09			4.98	0.00	24.46	143.06	0.0161
Camp.	0.37	11.17	9.42	5320.00	183.71	6609.84	12854.87	0.23	-635.00	-11113.99	0.22					
				SLE Rare		1774.29			-124.31			1.61	21.92	569.34	121.50	
				SLE Freq.		1612.30			-113.02			1.47	19.92	517.36	110.41	0.0106
				SLE Q.P.		1558.30			-109.26			1.42	19.25	500.03	106.71	0.0103
3321	0.74	12.63	9.42			6609.84	14307.31	0.24	0.00	-11116.93	0.22					
				SLE Rare		4473.89			0.00			0.00	52.86	1277.30	315.20	
				SLE Freq.		4067.17			0.00			0.00	48.06	1161.18	286.54	0.0249
				SLE Q.P.		3931.59			0.00			0.00	46.46	1122.47	276.99	0.0240
Trave Sez. 2 Rett. 40x40 [cm]																
3321	0.00	13.08	9.42			11801.75	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4637.56			0.00			0.00	54.12	1280.32	328.99	
				SLE Freq.		4216.39			0.00			0.00	49.20	1164.05	299.12	0.0252
				SLE Q.P.		4076.00			0.00			0.00	47.57	1125.29	289.16	0.0244
Camp.	0.30	14.24	9.42	5320.00	178.82	14966.47	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7217.26			-113.75			1.44	81.80	1838.74	519.50	
				SLE Freq.		6562.16			-103.42			1.31	74.37	1671.84	472.35	0.0374
				SLE Q.P.		6343.80			-99.98			1.26	71.90	1616.21	456.63	0.0361
120	0.61	15.62	6.49			14966.47	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10129.97			-17.25			0.26	115.31	2358.01	541.68	
				SLE Freq.		9210.70			-15.68			0.23	104.85	2144.02	492.52	0.0400
				SLE Q.P.		8904.27			-15.16			0.22	101.36	2072.70	476.14	0.0386

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 111 3176 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	14996.29	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3176 3216 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11759.88	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3216 3266 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7805.51	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3266 3273 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3950.07	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3273 3307 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3910.65	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3307 3314 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7766.09	8004.72	37247.76	36621.00	ø 10 2br. 12.5'

Trave 3314 3321 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11720.47	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3321 120 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14956.88	7069.46	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 336 Nodi 120 3320 3313 3306 3272 3265 3215 3175 110*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
120	0.13	15.62	6.49			15254.21	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10323.94			-17.25			0.26	117.52	2403.16	552.05	
				SLE Freq.		9383.90			-15.68			0.23	106.82	2184.34	501.78	0.0407
				SLE Q.P.		9070.56			-15.16			0.22	103.25	2111.40	485.03	0.0394
Camp.	0.43	14.24	9.42	5320.00	178.82	15254.21	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7388.57			-113.75			1.44	83.74	1882.38	531.83	
				SLE Freq.		6714.92			-103.42			1.31	76.10	1710.76	483.34	0.0382
				SLE Q.P.		6490.37			-99.98			1.26	73.56	1653.55	467.18	0.0369
3320	0.73	13.08	9.42			12065.28	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4786.22			0.00			0.00	55.85	1321.36	339.54	
				SLE Freq.		4348.71			0.00			0.00	50.75	1200.58	308.50	0.0260
				SLE Q.P.		4202.87			0.00			0.00	49.05	1160.31	298.16	0.0252
Trave Sez. 2 Rett. 40x40 [cm]																
3320	0.00	12.63	9.42			6845.05	14307.30	0.24	0.00	-11116.93	0.22					
				SLE Rare		4632.27			0.00			0.00	54.73	1322.52	326.36	
				SLE Freq.		4208.38			0.00			0.00	49.73	1201.50	296.49	0.0257
				SLE Q.P.		4067.09			0.00			0.00	48.06	1161.16	286.54	0.0249
Camp.	0.37	11.17	9.42	5320.00	183.71	6845.05	12854.87	0.23	-482.12	-11113.99	0.22					
				SLE Rare		1905.00			-124.31			1.61	23.53	611.28	130.45	
				SLE Freq.		1728.54			-113.02			1.47	21.35	554.65	118.37	0.0114
				SLE Q.P.		1669.72			-109.26			1.42	20.63	535.78	114.34	0.0110
3313	0.74	9.71	9.42			2979.48	11397.24	0.22	-482.12	-11110.44	0.22					
				SLE Rare		0.00			-327.21			4.30	0.00	21.11	123.48	
				SLE Freq.		0.00			-300.39			3.95	0.00	19.38	113.36	0.0128
				SLE Q.P.		0.00			-291.53			3.83	0.00	18.81	110.01	0.0124
Trave Sez. 2 Rett. 40x40 [cm]																
3313	0.00	9.42	9.42			0.00	11109.65	0.22	-3469.67	-11109.65	0.22					
				SLE Rare		0.00			-551.89			7.27	0.00	35.84	208.20	
				SLE Freq.		0.00			-504.86			6.65	0.00	32.79	190.45	0.0214
				SLE Q.P.		0.00			-489.25			6.44	0.00	31.77	184.56	0.0208
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5124.87	-11109.65	0.22					
				SLE Rare		0.00			-2247.46			29.61	0.00	145.96	847.84	
				SLE Freq.		0.00			-2046.72			26.96	0.00	132.92	772.11	0.0868
				SLE Q.P.		0.00			-1979.86			26.08	0.00	128.58	746.89	0.0840
3306	0.72	9.42	9.42			0.00	11109.65	0.22	-5124.87	-11109.65	0.22					
				SLE Rare		0.00			-3470.35			45.72	0.00	225.38	1309.16	
				SLE Freq.		0.00			-3158.84			41.61	0.00	205.14	1191.65	0.1340
				SLE Q.P.		0.00			-3055.05			40.24	0.00	198.40	1152.49	0.1296
Trave Sez. 2 Rett. 40x40 [cm]																
3306	0.00	9.42	9.42			0.00	11109.65	0.22	-6520.34	-11109.65	0.22					
				SLE Rare		0.00			-3630.39			47.82	0.00	235.77	1369.54	
				SLE Freq.		0.00			-3304.42			43.53	0.00	214.60	1246.57	0.1402
				SLE Q.P.		0.00			-3195.78			42.10	0.00	207.54	1205.59	0.1356
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6879.91	-11109.65	0.22					
				SLE Rare		0.00			-4390.49			57.84	0.00	285.13	1656.28	
				SLE Freq.		0.00			-3995.79			52.64	0.00	259.50	1507.38	0.1733
				SLE Q.P.		0.00			-3864.23			50.90	0.00	250.96	1457.75	0.1640

3272	0.74	9.42	9.42			0.00	11109.65	0.22	-6879.91	-11109.65	0.22					
				SLE Rare		0.00			-4659.37			61.38	0.00	302.59	1757.71	
				SLE Freq.		0.00			-4240.56			55.86	0.00	275.40	1599.72	0.1906
				SLE Q.P.		0.00			-4100.96			54.02	0.00	266.33	1547.06	0.1807
Trave Sez. 2 Rett. 40x40 [cm]																
3272	0.00	9.42	9.42			0.00	11109.65	0.22	-6876.09	-11109.65	0.22					
				SLE Rare		0.00			-4656.76			61.34	0.00	302.42	1756.73	
				SLE Freq.		0.00			-4238.11			55.83	0.00	275.24	1598.80	0.1904
				SLE Q.P.		0.00			-4098.54			53.99	0.00	266.17	1546.14	0.1806
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6876.09	-11109.65	0.22					
				SLE Rare		0.00			-4434.42			58.42	0.00	287.98	1672.85	
				SLE Freq.		0.00			-4036.28			53.17	0.00	262.13	1522.66	0.1762
				SLE Q.P.		0.00			-3903.53			51.42	0.00	253.51	1472.58	0.1668
3265	0.74	9.42	9.42			0.00	11109.65	0.22	-6579.99	-11109.65	0.22					
				SLE Rare		0.00			-3720.86			49.02	0.00	241.64	1403.67	
				SLE Freq.		0.00			-3387.85			44.63	0.00	220.02	1278.04	0.1437
				SLE Q.P.		0.00			-3276.80			43.17	0.00	212.81	1236.15	0.1390
Trave Sez. 2 Rett. 40x40 [cm]																
3265	0.00	9.42	9.42			0.00	11109.65	0.22	-5244.17	-11109.65	0.22					
				SLE Rare		0.00			-3553.58			46.81	0.00	230.78	1340.56	
				SLE Freq.		0.00			-3235.49			42.62	0.00	210.12	1220.57	0.1373
				SLE Q.P.		0.00			-3129.40			41.22	0.00	203.23	1180.54	0.1328
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5244.17	-11109.65	0.22					
				SLE Rare		0.00			-2376.34			31.30	0.00	154.33	896.46	
				SLE Freq.		0.00			-2165.50			28.53	0.00	140.63	816.92	0.0919
				SLE Q.P.		0.00			-2095.14			27.60	0.00	136.06	790.38	0.0889
3215	0.72	9.42	9.42			0.00	11109.65	0.22	-3649.93	-11109.65	0.22					
				SLE Rare		0.00			-726.43			9.57	0.00	47.18	274.04	
				SLE Freq.		0.00			-665.76			8.77	0.00	43.24	251.15	0.0282
				SLE Q.P.		0.00			-645.45			8.50	0.00	41.92	243.49	0.0274
Trave Sez. 2 Rett. 40x40 [cm]																
3215	0.00	9.71	9.42			2676.18	11397.24	0.22	-716.07	-11110.44	0.22					
				SLE Rare		0.00			-490.34			6.44	0.00	31.64	185.04	
				SLE Freq.		0.00			-450.68			5.92	0.00	29.08	170.07	0.0191
				SLE Q.P.		0.00			-437.36			5.75	0.00	28.22	165.04	0.0186
Camp.	0.37	11.17	9.42	5320.00	183.71	6477.65	12854.87	0.23	-716.07	-11113.99	0.22					
				SLE Rare		1695.66			-124.31			1.61	20.95	544.11	116.12	
				SLE Freq.		1536.04			-113.02			1.47	18.97	492.89	105.19	0.0101
				SLE Q.P.		1482.84			-109.26			1.42	18.32	475.81	101.54	0.0098
3175	0.74	12.63	9.42			6477.65	14307.30	0.24	0.00	-11116.93	0.22					
				SLE Rare		4376.27			0.00			0.00	51.71	1249.43	308.32	
				SLE Freq.		3972.87			0.00			0.00	46.94	1134.26	279.90	0.0243
				SLE Q.P.		3838.40			0.00			0.00	45.35	1095.87	270.43	0.0235
Trave Sez. 2 Rett. 40x40 [cm]																
3175	0.00	13.08	9.42			11657.95	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4551.04			0.00			0.00	53.11	1256.43	322.86	
				SLE Freq.		4132.55			0.00			0.00	48.23	1140.90	293.17	0.0247
				SLE Q.P.		3993.06			0.00			0.00	46.60	1102.39	283.27	0.0239
Camp.	0.30	14.24	9.42	5320.00	178.82	14807.14	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7115.20			-113.76			1.44	80.64	1812.74	512.16	
				SLE Freq.		6463.56			-103.42			1.31	73.26	1646.72	465.25	0.0368
				SLE Q.P.		6246.35			-99.98			1.26	70.79	1591.38	449.62	0.0356
110	0.61	15.62	6.49			14807.14	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10012.38			-17.25			0.26	113.97	2330.64	535.39	
				SLE Freq.		9097.34			-15.68			0.23	103.56	2117.64	486.46	0.0395

			SLE Q.P.	8792.33			-15.16			0.22	100.08	2046.64	470.15	0.0381

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	Staffe
Trave 120 3320 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	15067.11	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3320 3313 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11830.70	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3313 3306 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7876.32	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3306 3272 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	4020.88	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3272 3265 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3840.09	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3265 3215 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7695.53	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3215 3175 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11649.90	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3175 110 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14886.32	7069.46	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 339 Nodi 201 6038 6040 6052 6092 6098 6148 6182 211*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
201	0.12	15.62	6.49			15026.92	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10162.13			-17.25			0.26	115.68	2365.49	543.40	
				SLE Freq.		9234.57			-15.68			0.23	105.12	2149.58	493.80	0.0401
				SLE Q.P.		8925.38			-15.16			0.22	101.60	2077.61	477.26	0.0387
Camp.	0.43	14.24	9.42	5320.00	178.82	15026.92	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7256.57			-113.75			1.44	82.24	1848.75	522.33	
				SLE Freq.		6593.94			-103.42			1.31	74.73	1679.94	474.64	0.0375
				SLE Q.P.		6373.07			-99.98			1.26	72.23	1623.66	458.74	0.0363
6038	0.73	13.08	9.42			11868.64	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4684.03			0.00			0.00	54.66	1293.15	332.29	
				SLE Freq.		4256.09			0.00			0.00	49.67	1175.01	301.93	0.0255
				SLE Q.P.		4113.44			0.00			0.00	48.00	1135.62	291.81	0.0246
Trave Sez. 2 Rett. 40x40 [cm]																
6038	0.00	12.63	9.42			6680.92	14307.31	0.24	0.00	-11116.93	0.22					
				SLE Rare		4515.31			0.00			0.00	53.35	1289.13	318.12	
				SLE Freq.		4102.02			0.00			0.00	48.47	1171.13	289.00	0.0251
				SLE Q.P.		3964.26			0.00			0.00	46.84	1131.80	279.29	0.0242
Camp.	0.37	11.17	9.42	5320.00	183.71	6680.92	12854.87	0.23	-542.79	-11113.99	0.22					
				SLE Rare		1824.45			-124.31			1.61	22.54	585.43	124.94	
				SLE Freq.		1656.82			-113.02			1.47	20.47	531.64	113.46	0.0109
				SLE Q.P.		1600.94			-109.26			1.42	19.78	513.71	109.63	0.0105
6040	0.74	9.71	9.42			2864.76	11397.24	0.22	-542.79	-11110.44	0.22					
				SLE Rare		0.00			-371.29			4.88	0.00	23.95	140.11	
				SLE Freq.		0.00			-339.34			4.46	0.00	21.89	128.06	0.0144
				SLE Q.P.		0.00			-327.96			4.31	0.00	21.16	123.76	0.0139
Trave Sez. 2 Rett. 40x40 [cm]																
6040	0.00	9.42	9.42			0.00	11109.65	0.22	-3490.46	-11109.65	0.22					
				SLE Rare		0.00			-606.69			7.99	0.00	39.40	228.87	
				SLE Freq.		0.00			-553.79			7.30	0.00	35.96	208.91	0.0235
				SLE Q.P.		0.00			-535.44			7.05	0.00	34.77	201.99	0.0227
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5097.38	-11109.65	0.22					
				SLE Rare		0.00			-2265.71			29.85	0.00	147.14	854.72	

				SLE Freq.		0.00			-2061.08			27.15	0.00	133.85	777.53	0.0875
				SLE Q.P.		0.00			-1992.17			26.24	0.00	129.38	751.53	0.0845
6052	0.72	9.42	9.42			0.00	11109.65	0.22	-5097.38	-11109.65	0.22					
				SLE Rare		0.00			-3452.05			45.47	0.00	224.19	1302.26	
				SLE Freq.		0.00			-3138.63			41.35	0.00	203.83	1184.02	0.1332
				SLE Q.P.		0.00			-3033.46			39.96	0.00	197.00	1144.35	0.1287
Trave Sez. 2 Rett. 40x40 [cm]																
6052	0.00	9.42	9.42			0.00	11109.65	0.22	-6453.44	-11109.65	0.22					
				SLE Rare		0.00			-3622.89			47.73	0.00	235.28	1366.71	
				SLE Freq.		0.00			-3294.36			43.40	0.00	213.95	1242.77	0.1398
				SLE Q.P.		0.00			-3184.22			41.95	0.00	206.79	1201.22	0.1351
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6764.11	-11109.65	0.22					
				SLE Rare		0.00			-4345.86			57.25	0.00	282.23	1639.44	
				SLE Freq.		0.00			-3950.50			52.04	0.00	256.56	1490.30	0.1701
				SLE Q.P.		0.00			-3818.12			50.30	0.00	247.96	1440.36	0.1620
6092	0.74	9.42	9.42			0.00	11109.65	0.22	-6764.11	-11109.65	0.22					
				SLE Rare		0.00			-4578.46			60.31	0.00	297.34	1727.19	
				SLE Freq.		0.00			-4160.03			54.80	0.00	270.16	1569.34	0.1849
				SLE Q.P.		0.00			-4020.29			52.96	0.00	261.09	1516.63	0.1750
Trave Sez. 2 Rett. 40x40 [cm]																
6092	0.00	9.42	9.42			0.00	11109.65	0.22	-6777.45	-11109.65	0.22					
				SLE Rare		0.00			-4587.52			60.43	0.00	297.93	1730.61	
				SLE Freq.		0.00			-4168.93			54.92	0.00	270.74	1572.70	0.1855
				SLE Q.P.		0.00			-4029.13			53.08	0.00	261.66	1519.96	0.1757
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6777.45	-11109.65	0.22					
				SLE Rare		0.00			-4328.89			57.03	0.00	281.13	1633.04	
				SLE Freq.		0.00			-3932.01			51.80	0.00	255.36	1483.32	0.1688
				SLE Q.P.		0.00			-3799.72			50.05	0.00	246.77	1433.42	0.1612
6098	0.74	9.42	9.42			0.00	11109.65	0.22	-6432.49	-11109.65	0.22					
				SLE Rare		0.00			-3579.05			47.15	0.00	232.43	1350.17	
				SLE Freq.		0.00			-3249.05			42.80	0.00	211.00	1225.68	0.1379
				SLE Q.P.		0.00			-3139.05			41.35	0.00	203.86	1184.18	0.1332
Trave Sez. 2 Rett. 40x40 [cm]																
6098	0.00	9.42	9.42			0.00	11109.65	0.22	-5066.55	-11109.65	0.22					
				SLE Rare		0.00			-3428.19			45.16	0.00	222.64	1293.26	
				SLE Freq.		0.00			-3112.70			41.00	0.00	202.15	1174.24	0.1321
				SLE Q.P.		0.00			-3007.53			39.62	0.00	195.32	1134.57	0.1276
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5066.55	-11109.65	0.22					
				SLE Rare		0.00			-2215.37			29.18	0.00	143.87	835.73	
				SLE Freq.		0.00			-2008.83			26.46	0.00	130.46	757.82	0.0852
				SLE Q.P.		0.00			-1939.99			25.56	0.00	125.99	731.85	0.0823
6148	0.72	9.42	9.42			0.00	11109.65	0.22	-3425.38	-11109.65	0.22					
				SLE Rare		0.00			-529.86			6.98	0.00	34.41	199.89	
				SLE Freq.		0.00			-475.22			6.26	0.00	30.86	179.27	0.0202
				SLE Q.P.		0.00			-457.01			6.02	0.00	29.68	172.40	0.0194
Trave Sez. 2 Rett. 40x40 [cm]																
6148	0.00	9.71	9.42			2981.53	11397.24	0.22	-468.07	-11110.44	0.22					
				SLE Rare		0.00			-314.94			4.14	0.00	20.32	118.85	
				SLE Freq.		0.00			-280.76			3.69	0.00	18.11	105.95	0.0119
				SLE Q.P.		0.00			-269.37			3.54	0.00	17.38	101.65	0.0114
Camp.	0.37	11.17	9.42	5320.00	183.71	6833.84	12854.87	0.23	-468.07	-11113.99	0.22					
				SLE Rare		1909.68			-124.31			1.61	23.59	612.78	130.77	
				SLE Freq.		1741.44			-113.02			1.47	21.51	558.80	119.25	0.0115
				SLE Q.P.		1685.67			-109.26			1.42	20.82	540.90	115.43	0.0111
6182	0.74	12.63	9.42			6833.84	14307.31	0.24	0.00	-11116.93	0.22					

				SLE Rare		4627.70			0.00			0.00	54.68	1321.21	326.03	
				SLE Freq.		4213.64			0.00			0.00	49.79	1203.00	296.86	0.0258
				SLE Q.P.		4075.91			0.00			0.00	48.16	1163.68	287.16	0.0249
Trave Sez. 2 Rett. 40x40 [cm]																
6182	0.00	13.08	9.42			12023.63	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4770.50			0.00			0.00	55.67	1317.02	338.43	
				SLE Freq.		4342.58			0.00			0.00	50.68	1198.88	308.07	0.0260
				SLE Q.P.		4200.11			0.00			0.00	49.01	1159.55	297.96	0.0251
Camp.	0.30	14.24	9.42	5320.00	178.82	15204.33	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7365.27			-113.75			1.44	83.48	1876.45	530.16	
				SLE Freq.		6702.53			-103.42			1.31	75.96	1707.60	482.45	0.0382
				SLE Q.P.		6481.77			-99.98			1.26	73.46	1651.36	466.56	0.0369
211	0.61	15.62	6.49			15204.33	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10293.07			-17.25			0.26	117.17	2395.97	550.40	
				SLE Freq.		9365.24			-15.68			0.23	106.61	2180.00	500.79	0.0406
				SLE Q.P.		9056.12			-15.16			0.22	103.09	2108.04	484.26	0.0393

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 201 6038 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	14927.64	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6038 6040 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11691.23	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6040 6052 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7736.85	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6052 6092 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3881.42	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6092 6098 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3983.19	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6098 6148 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7838.63	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6148 6182 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11793.01	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6182 211 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	15029.42	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 344 Nodi 211 6236 6276 6326 6333 6367 6374 6381 220*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
211	0.13	15.62	6.49			15114.25	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10226.37			-17.25			0.26	116.41	2380.45	546.83	
				SLE Freq.		9298.38			-15.68			0.23	105.85	2164.44	497.21	0.0403
				SLE Q.P.		8989.32			-15.16			0.22	102.33	2092.49	480.68	0.0390
Camp.	0.43	14.24	9.42	5320.00	178.82	15114.25	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7306.92			-113.76			1.44	82.81	1861.58	525.96	
				SLE Freq.		6643.96			-103.42			1.31	75.30	1692.68	478.24	0.0378
				SLE Q.P.		6423.24			-99.98			1.26	72.80	1636.45	462.35	0.0366
6236	0.73	13.08	9.42			11941.76	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4720.48			0.00			0.00	55.09	1303.21	334.88	
				SLE Freq.		4292.31			0.00			0.00	50.09	1185.01	304.50	0.0257
				SLE Q.P.		4149.84			0.00			0.00	48.43	1145.67	294.40	0.0248
Trave Sez. 2 Rett. 40x40 [cm]																
6236	0.00	12.63	9.42			6744.63	14307.30	0.24	0.00	-11116.93	0.22					
				SLE Rare		4562.58			0.00			0.00	53.91	1302.62	321.45	
				SLE Freq.		4148.82			0.00			0.00	49.02	1184.50	292.30	0.0254
				SLE Q.P.		4011.19			0.00			0.00	47.40	1145.20	282.60	0.0245

Camp.	0.37	11.17	9.42	5320.00	183.71	6744.63	12854.87	0.23	-525.54	-11113.99	0.22					
				SLE Rare		1854.76			-124.31			1.61	22.91	595.16	127.01	
				SLE Freq.		1686.78			-113.02			1.47	20.84	541.25	115.51	0.0111
				SLE Q.P.		1631.06			-109.26			1.42	20.15	523.38	111.69	0.0107
6276	0.74	9.71	9.42			2905.59	11397.24	0.22	-525.54	-11110.44	0.22					
				SLE Rare		0.00			-357.00			4.69	0.00	23.03	134.72	
				SLE Freq.		0.00			-323.64			4.25	0.00	20.88	122.13	0.0137
				SLE Q.P.		0.00			-312.52			4.11	0.00	20.16	117.93	0.0133
Trave Sez. 2 Rett. 40x40 [cm]																
6276	0.00	9.42	9.42			0.00	11109.65	0.22	-3485.98	-11109.65	0.22					
				SLE Rare		0.00			-583.37			7.68	0.00	37.89	220.07	
				SLE Freq.		0.00			-529.35			6.97	0.00	34.38	199.69	0.0225
				SLE Q.P.		0.00			-511.35			6.74	0.00	33.21	192.90	0.0217
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5115.39	-11109.65	0.22					
				SLE Rare		0.00			-2259.51			29.77	0.00	146.74	852.38	
				SLE Freq.		0.00			-2053.49			27.05	0.00	133.36	774.66	0.0871
				SLE Q.P.		0.00			-1984.81			26.15	0.00	128.90	748.76	0.0842
6326	0.72	9.42	9.42			0.00	11109.65	0.22	-5115.39	-11109.65	0.22					
				SLE Rare		0.00			-3462.97			45.62	0.00	224.90	1306.38	
				SLE Freq.		0.00			-3147.95			41.47	0.00	204.44	1187.54	0.1336
				SLE Q.P.		0.00			-3042.86			40.08	0.00	197.61	1147.90	0.1291
Trave Sez. 2 Rett. 40x40 [cm]																
6326	0.00	9.42	9.42			0.00	11109.65	0.22	-6483.26	-11109.65	0.22					
				SLE Rare		0.00			-3624.37			47.74	0.00	235.38	1367.27	
				SLE Freq.		0.00			-3294.59			43.40	0.00	213.96	1242.86	0.1398
				SLE Q.P.		0.00			-3184.60			41.95	0.00	206.82	1201.37	0.1351
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6816.24	-11109.65	0.22					
				SLE Rare		0.00			-4364.67			57.50	0.00	283.45	1646.54	
				SLE Freq.		0.00			-3968.18			52.27	0.00	257.71	1496.97	0.1713
				SLE Q.P.		0.00			-3835.82			50.53	0.00	249.11	1447.04	0.1628
6333	0.74	9.42	9.42			0.00	11109.65	0.22	-6816.24	-11109.65	0.22					
				SLE Rare		0.00			-4613.92			60.78	0.00	299.64	1740.57	
				SLE Freq.		0.00			-4195.17			55.26	0.00	272.45	1582.60	0.1874
				SLE Q.P.		0.00			-4055.33			53.42	0.00	263.37	1529.84	0.1775
Trave Sez. 2 Rett. 40x40 [cm]																
6333	0.00	9.42	9.42			0.00	11109.65	0.22	-6815.63	-11109.65	0.22					
				SLE Rare		0.00			-4613.51			60.77	0.00	299.62	1740.41	
				SLE Freq.		0.00			-4194.75			55.26	0.00	272.42	1582.44	0.1874
				SLE Q.P.		0.00			-4054.91			53.42	0.00	263.34	1529.68	0.1775
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6815.63	-11109.65	0.22					
				SLE Rare		0.00			-4371.75			57.59	0.00	283.91	1649.21	
				SLE Freq.		0.00			-3975.14			52.37	0.00	258.16	1499.59	0.1718
				SLE Q.P.		0.00			-3842.69			50.62	0.00	249.56	1449.63	0.1630
6367	0.74	9.42	9.42			0.00	11109.65	0.22	-6493.27	-11109.65	0.22					
				SLE Rare		0.00			-3638.78			47.93	0.00	236.31	1372.70	
				SLE Freq.		0.00			-3308.92			43.59	0.00	214.89	1248.27	0.1404
				SLE Q.P.		0.00			-3198.74			42.14	0.00	207.74	1206.70	0.1357
Trave Sez. 2 Rett. 40x40 [cm]																
6367	0.00	9.42	9.42			0.00	11109.65	0.22	-5135.24	-11109.65	0.22					
				SLE Rare		0.00			-3476.28			45.79	0.00	225.76	1311.40	
				SLE Freq.		0.00			-3161.12			41.64	0.00	205.29	1192.51	0.1341
				SLE Q.P.		0.00			-3055.85			40.26	0.00	198.46	1152.80	0.1297
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5135.24	-11109.65	0.22					
				SLE Rare		0.00			-2280.00			30.04	0.00	148.07	860.11	
				SLE Freq.		0.00			-2073.69			27.32	0.00	134.67	782.28	0.0880

				SLE Q.P.		0.00			-2004.70			26.41	0.00	130.19	756.26	0.0851
6374	0.72	9.42	9.42			0.00	11109.65	0.22	-3515.76	-11109.65	0.22					
				SLE Rare		0.00			-611.04			8.05	0.00	39.68	230.51	
				SLE Freq.		0.00			-556.51			7.33	0.00	36.14	209.94	0.0236
				SLE Q.P.		0.00			-538.12			7.09	0.00	34.95	203.00	0.0228
Trave Sez. 2 Rett. 40x40 [cm]																
6374	0.00	9.71	9.42			2855.93	11397.24	0.22	-564.16	-11110.44	0.22					
				SLE Rare		0.00			-382.91			5.03	0.00	24.70	144.50	
				SLE Freq.		0.00			-349.00			4.59	0.00	22.52	131.70	0.0148
				SLE Q.P.		0.00			-337.52			4.43	0.00	21.78	127.37	0.0143
Camp.	0.37	11.17	9.42	5320.00	183.71	6684.50	12854.87	0.23	-564.16	-11113.99	0.22					
				SLE Rare		1821.76			-124.31			1.61	22.50	584.57	124.75	
				SLE Freq.		1655.38			-113.02			1.47	20.45	531.18	113.36	0.0109
				SLE Q.P.		1599.92			-109.26			1.42	19.76	513.38	109.56	0.0105
6381	0.74	12.63	9.42			6684.50	14307.31	0.24	0.00	-11116.93	0.22					
				SLE Rare		4522.23			0.00			0.00	53.43	1291.10	318.60	
				SLE Freq.		4110.31			0.00			0.00	48.57	1173.50	289.58	0.0251
				SLE Q.P.		3973.00			0.00			0.00	46.94	1134.30	279.91	0.0243
Trave Sez. 2 Rett. 40x40 [cm]																
6381	0.00	13.08	9.42			11874.99	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4683.36			0.00			0.00	54.65	1292.96	332.24	
				SLE Freq.		4256.91			0.00			0.00	49.68	1175.23	301.99	0.0255
				SLE Q.P.		4114.77			0.00			0.00	48.02	1135.99	291.91	0.0246
Camp.	0.30	14.24	9.42	5320.00	178.82	15040.97	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7263.76			-113.75			1.44	82.33	1850.58	522.85	
				SLE Freq.		6602.73			-103.42			1.31	74.83	1682.17	475.27	0.0376
				SLE Q.P.		6382.38			-99.98			1.26	72.34	1626.04	459.41	0.0363
220	0.61	15.62	6.49			15040.97	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10177.17			-17.25			0.26	115.85	2369.00	544.20	
				SLE Freq.		9251.31			-15.68			0.23	105.31	2153.48	494.69	0.0401
				SLE Q.P.		8942.69			-15.16			0.22	101.80	2081.64	478.19	0.0388

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 211 6236 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	14992.09	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6236 6276 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11755.67	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6276 6326 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7801.30	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6326 6333 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3945.86	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6333 6367 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3916.36	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6367 6374 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7771.80	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6374 6381 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11726.18	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6381 220 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14962.59	7069.46	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 345 Nodi 220 6380 6373 6366 6332 6325 6275 6235 210*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
220	0.13	15.62	6.49			15167.67	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10264.07			-17.25			0.26	116.84	2389.22	548.85	

				SLE Freq.		9331.75			-15.68			0.23	106.22	2172.20	498.99	0.0405
				SLE Q.P.		9020.98			-15.16			0.22	102.69	2099.86	482.38	0.0391
Camp.	0.43	14.24	9.42	5320.00	178.82	15167.67	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7341.40			-113.75			1.44	83.21	1870.36	528.44	
				SLE Freq.		6674.59			-103.42			1.31	75.65	1700.48	480.44	0.0380
				SLE Q.P.		6452.32			-99.98			1.26	73.13	1643.85	464.44	0.0367
6380	0.73	13.08	9.42			11991.93	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4751.75			0.00			0.00	55.45	1311.85	337.10	
				SLE Freq.		4320.19			0.00			0.00	50.42	1192.70	306.48	0.0259
				SLE Q.P.		4176.34			0.00			0.00	48.74	1152.99	296.28	0.0250
Trave Sez. 2 Rett. 40x40 [cm]																
6380	0.00	12.63	9.42			6805.94	14307.30	0.24	0.00	-11116.93	0.22					
				SLE Rare		4605.36			0.00			0.00	54.42	1314.84	324.46	
				SLE Freq.		4187.84			0.00			0.00	49.48	1195.64	295.05	0.0256
				SLE Q.P.		4048.67			0.00			0.00	47.84	1155.90	285.24	0.0248
Camp.	0.37	11.17	9.42	5320.00	183.71	6805.94	12854.87	0.23	-473.84	-11113.99	0.22					
				SLE Rare		1893.60			-124.31			1.61	23.39	607.62	129.67	
				SLE Freq.		1722.44			-113.02			1.47	21.28	552.70	117.95	0.0113
				SLE Q.P.		1665.38			-109.26			1.42	20.57	534.39	114.04	0.0110
6373	0.74	9.71	9.42			2961.66	11397.24	0.22	-473.84	-11110.44	0.22					
				SLE Rare		0.00			-321.20			4.22	0.00	20.72	121.21	
				SLE Freq.		0.00			-291.82			3.83	0.00	18.83	110.12	0.0124
				SLE Q.P.		0.00			-281.67			3.70	0.00	18.17	106.29	0.0120
Trave Sez. 2 Rett. 40x40 [cm]																
6373	0.00	9.42	9.42			0.00	11109.65	0.22	-3426.62	-11109.65	0.22					
				SLE Rare		0.00			-538.12			7.09	0.00	34.95	203.00	
				SLE Freq.		0.00			-488.66			6.44	0.00	31.74	184.34	0.0207
				SLE Q.P.		0.00			-471.71			6.21	0.00	30.63	177.95	0.0200
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5061.53	-11109.65	0.22					
				SLE Rare		0.00			-2218.42			29.22	0.00	144.07	836.88	
				SLE Freq.		0.00			-2016.27			26.56	0.00	130.94	760.62	0.0856
				SLE Q.P.		0.00			-1948.44			25.67	0.00	126.54	735.03	0.0827
6366	0.72	9.42	9.42			0.00	11109.65	0.22	-5061.53	-11109.65	0.22					
				SLE Rare		0.00			-3426.10			45.13	0.00	222.50	1292.47	
				SLE Freq.		0.00			-3114.13			41.02	0.00	202.24	1174.78	0.1321
				SLE Q.P.		0.00			-3009.73			39.65	0.00	195.46	1135.40	0.1277
Trave Sez. 2 Rett. 40x40 [cm]																
6366	0.00	9.42	9.42			0.00	11109.65	0.22	-6423.54	-11109.65	0.22					
				SLE Rare		0.00			-3579.22			47.15	0.00	232.45	1350.24	
				SLE Freq.		0.00			-3252.76			42.85	0.00	211.24	1227.08	0.1380
				SLE Q.P.		0.00			-3143.50			41.41	0.00	204.15	1185.86	0.1334
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6761.97	-11109.65	0.22					
				SLE Rare		0.00			-4323.82			56.96	0.00	280.80	1631.13	
				SLE Freq.		0.00			-3929.60			51.77	0.00	255.20	1482.41	0.1686
				SLE Q.P.		0.00			-3797.79			50.03	0.00	246.64	1432.69	0.1611
6332	0.74	9.42	9.42			0.00	11109.65	0.22	-6761.97	-11109.65	0.22					
				SLE Rare		0.00			-4577.20			60.30	0.00	297.26	1726.71	
				SLE Freq.		0.00			-4159.84			54.80	0.00	270.15	1569.27	0.1849
				SLE Q.P.		0.00			-4020.36			52.96	0.00	261.09	1516.65	0.1750
Trave Sez. 2 Rett. 40x40 [cm]																
6332	0.00	9.42	9.42			0.00	11109.65	0.22	-6752.08	-11109.65	0.22					
				SLE Rare		0.00			-4570.49			60.21	0.00	296.82	1724.18	
				SLE Freq.		0.00			-4153.23			54.71	0.00	269.72	1566.78	0.1844
				SLE Q.P.		0.00			-4013.78			52.87	0.00	260.67	1514.17	0.1746
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6752.08	-11109.65	0.22					

				SLE Rare		0.00			-4332.65			57.08	0.00	281.38	1634.46	
				SLE Freq.		0.00			-3936.87			51.86	0.00	255.67	1485.15	0.1691
				SLE Q.P.		0.00			-3804.61			50.12	0.00	247.08	1435.26	0.1614
6325	0.74	9.42	9.42			0.00	11109.65	0.22	-6434.89	-11109.65	0.22					
				SLE Rare		0.00			-3603.58			47.47	0.00	234.03	1359.43	
				SLE Freq.		0.00			-3273.91			43.13	0.00	212.62	1235.06	0.1389
				SLE Q.P.		0.00			-3163.72			41.68	0.00	205.46	1193.49	0.1342
Trave Sez. 2 Rett. 40x40 [cm]																
6325	0.00	9.42	9.42			0.00	11109.65	0.22	-5075.14	-11109.65	0.22					
				SLE Rare		0.00			-3436.02			45.26	0.00	223.15	1296.21	
				SLE Freq.		0.00			-3121.12			41.12	0.00	202.69	1177.42	0.1324
				SLE Q.P.		0.00			-3015.87			39.73	0.00	195.86	1137.71	0.1280
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5075.14	-11109.65	0.22					
				SLE Rare		0.00			-2243.58			29.56	0.00	145.70	846.37	
				SLE Freq.		0.00			-2036.87			26.83	0.00	132.28	768.39	0.0864
				SLE Q.P.		0.00			-1967.72			25.92	0.00	127.79	742.31	0.0835
6275	0.72	9.42	9.42			0.00	11109.65	0.22	-3460.62	-11109.65	0.22					
				SLE Rare		0.00			-578.45			7.62	0.00	37.57	218.22	
				SLE Freq.		0.00			-522.87			6.89	0.00	33.96	197.25	0.0222
				SLE Q.P.		0.00			-504.13			6.64	0.00	32.74	190.18	0.0214
Trave Sez. 2 Rett. 40x40 [cm]																
6275	0.00	9.71	9.42			2904.39	11397.24	0.22	-509.78	-11110.44	0.22					
				SLE Rare		0.00			-346.92			4.56	0.00	22.38	130.92	
				SLE Freq.		0.00			-312.06			4.10	0.00	20.13	117.76	0.0132
				SLE Q.P.		0.00			-300.24			3.94	0.00	19.37	113.30	0.0127
Camp.	0.37	11.17	9.42	5320.00	183.71	6727.32	12854.87	0.23	-509.78	-11113.99	0.22					
				SLE Rare		1853.69			-124.31			1.61	22.90	594.81	126.94	
				SLE Freq.		1687.47			-113.02			1.47	20.84	541.48	115.55	0.0111
				SLE Q.P.		1632.64			-109.26			1.42	20.17	523.88	111.80	0.0107
6235	0.74	12.63	9.42			6727.32	14307.30	0.24	0.00	-11116.93	0.22					
				SLE Rare		4549.94			0.00			0.00	53.76	1299.02	320.56	
				SLE Freq.		4138.73			0.00			0.00	48.90	1181.61	291.59	0.0253
				SLE Q.P.		4002.28			0.00			0.00	47.29	1142.66	281.97	0.0245
Trave Sez. 2 Rett. 40x40 [cm]																
6235	0.00	13.08	9.42			11915.50	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4713.76			0.00			0.00	55.01	1301.36	334.40	
				SLE Freq.		4287.78			0.00			0.00	50.04	1183.76	304.18	0.0257
				SLE Q.P.		4146.42			0.00			0.00	48.39	1144.73	294.15	0.0248
Camp.	0.30	14.24	9.42	5320.00	178.82	15078.00	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7290.72			-113.76			1.44	82.63	1857.45	524.79	
				SLE Freq.		6630.61			-103.42			1.31	75.15	1689.28	477.27	0.0377
				SLE Q.P.		6411.24			-99.98			1.26	72.66	1633.39	461.48	0.0365
210	0.61	15.62	6.49			15078.00	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10200.70			-17.25			0.26	116.12	2374.47	545.46	
				SLE Freq.		9276.21			-15.68			0.23	105.59	2159.27	496.02	0.0402
				SLE Q.P.		8968.79			-15.16			0.22	102.09	2087.71	479.59	0.0389

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 220 6380 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	15006.84	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6380 6373 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11770.43	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6373 6366 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7816.05	8004.72	37247.76	36621.00	ø 10 2br. 12.5'

Trave 6366 6332 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3960.61	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6332 6325 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3900.53	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6325 6275 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7755.97	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6275 6235 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11710.34	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6235 210 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14946.76	7069.46	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 346 Nodi 210 6181 6147 6097 6091 6051 6039 6037 201*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
210	0.13	15.62	9.42			15000.21	17258.31	0.27	-25.49	-11121.61	0.22					
				SLE Rare		10152.77			-17.25			0.22	111.55	2368.90	740.40	
				SLE Freq.		9232.19			-15.68			0.20	101.43	2154.11	673.26	0.0497
				SLE Q.P.		8924.75			-15.16			0.19	98.05	2082.38	650.84	0.0481
Camp.	0.43	14.24	9.42	5320.00	178.82	15000.21	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7233.64			-113.75			1.44	81.98	1842.91	520.68	
				SLE Freq.		6577.63			-103.42			1.31	74.55	1675.78	473.46	0.0374
				SLE Q.P.		6358.38			-99.98			1.26	72.06	1619.92	457.68	0.0362
6181	0.73	13.08	9.42			11828.49	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4647.53			0.00			0.00	54.24	1283.07	329.70	
				SLE Freq.		4225.83			0.00			0.00	49.31	1166.65	299.79	0.0253
				SLE Q.P.		4084.70			0.00			0.00	47.67	1127.69	289.77	0.0245
Trave Sez. 2 Rett. 40x40 [cm]																
6181	0.00	12.63	9.42			6619.57	14307.31	0.24	0.00	-11116.93	0.22					
				SLE Rare		4481.00			0.00			0.00	52.95	1279.33	315.70	
				SLE Freq.		4074.28			0.00			0.00	48.14	1163.21	287.04	0.0249
				SLE Q.P.		3938.06			0.00			0.00	46.53	1124.32	277.45	0.0241
Camp.	0.37	11.17	9.42	5320.00	183.71	6619.57	12854.87	0.23	-646.27	-11113.99	0.22					
				SLE Rare		1773.57			-124.31			1.61	21.91	569.10	121.45	
				SLE Freq.		1612.05			-113.02			1.47	19.91	517.28	110.39	0.0106
				SLE Q.P.		1557.57			-109.26			1.42	19.24	499.79	106.66	0.0103
6147	0.74	9.71	9.42			2781.74	11397.24	0.22	-646.27	-11110.44	0.22					
				SLE Rare		0.00			-436.62			5.74	0.00	28.17	164.77	
				SLE Freq.		0.00			-399.31			5.25	0.00	25.76	150.69	0.0170
				SLE Q.P.		0.00			-386.92			5.08	0.00	24.96	146.01	0.0164
Trave Sez. 2 Rett. 40x40 [cm]																
6147	0.00	9.42	9.42			0.00	11109.65	0.22	-3613.33	-11109.65	0.22					
				SLE Rare		0.00			-667.83			8.80	0.00	43.37	251.93	
				SLE Freq.		0.00			-609.71			8.03	0.00	39.60	230.01	0.0259
				SLE Q.P.		0.00			-590.39			7.78	0.00	38.34	222.72	0.0251
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5242.12	-11109.65	0.22					
				SLE Rare		0.00			-2343.96			30.88	0.00	152.22	884.24	
				SLE Freq.		0.00			-2133.89			28.11	0.00	138.58	804.99	0.0905
				SLE Q.P.		0.00			-2064.12			27.19	0.00	134.05	778.67	0.0876
6097	0.72	9.42	9.42			0.00	11109.65	0.22	-5242.12	-11109.65	0.22					
				SLE Rare		0.00			-3547.42			46.73	0.00	230.38	1338.24	
				SLE Freq.		0.00			-3228.33			42.53	0.00	209.66	1217.86	0.1370
				SLE Q.P.		0.00			-3122.42			41.13	0.00	202.78	1177.91	0.1325
Trave Sez. 2 Rett. 40x40 [cm]																
6097	0.00	9.42	9.42			0.00	11109.65	0.22	-6612.15	-11109.65	0.22					
				SLE Rare		0.00			-3710.71			48.88	0.00	240.98	1399.84	

				SLE Freq.		0.00			-3376.87			44.48	0.00	219.30	1273.90	0.1433
				SLE Q.P.		0.00			-3266.05			43.02	0.00	212.11	1232.09	0.1386
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6944.21	-11109.65	0.22					
				SLE Rare		0.00			-4451.00			58.63	0.00	289.06	1679.11	
				SLE Freq.		0.00			-4050.22			53.35	0.00	263.03	1527.92	0.1771
				SLE Q.P.		0.00			-3917.29			51.60	0.00	254.40	1477.77	0.1677
6091	0.74	9.42	9.42			0.00	11109.65	0.22	-6944.21	-11109.65	0.22					
				SLE Rare		0.00			-4700.08			61.92	0.00	305.24	1773.07	
				SLE Freq.		0.00			-4277.31			56.35	0.00	277.78	1613.59	0.1932
				SLE Q.P.		0.00			-4137.08			54.50	0.00	268.67	1560.68	0.1833
Trave Sez. 2 Rett. 40x40 [cm]																
6091	0.00	9.42	9.42			0.00	11109.65	0.22	-6941.59	-11109.65	0.22					
				SLE Rare		0.00			-4698.27			61.89	0.00	305.12	1772.39	
				SLE Freq.		0.00			-4275.60			56.32	0.00	277.67	1612.94	0.1931
				SLE Q.P.		0.00			-4135.39			54.48	0.00	268.56	1560.05	0.1832
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6941.59	-11109.65	0.22					
				SLE Rare		0.00			-4456.13			58.70	0.00	289.39	1681.04	
				SLE Freq.		0.00			-4056.16			53.43	0.00	263.42	1530.16	0.1776
				SLE Q.P.		0.00			-3923.52			51.69	0.00	254.81	1480.12	0.1682
6051	0.74	9.42	9.42			0.00	11109.65	0.22	-6618.02	-11109.65	0.22					
				SLE Rare		0.00			-3722.76			49.04	0.00	241.77	1404.39	
				SLE Freq.		0.00			-3390.13			44.66	0.00	220.17	1278.90	0.1438
				SLE Q.P.		0.00			-3279.93			43.21	0.00	213.01	1237.33	0.1392
Trave Sez. 2 Rett. 40x40 [cm]																
6051	0.00	9.42	9.42			0.00	11109.65	0.22	-5251.64	-11109.65	0.22					
				SLE Rare		0.00			-3555.49			46.84	0.00	230.90	1341.28	
				SLE Freq.		0.00			-3237.78			42.65	0.00	210.27	1221.43	0.1374
				SLE Q.P.		0.00			-3132.52			41.27	0.00	203.44	1181.72	0.1329
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5251.64	-11109.65	0.22					
				SLE Rare		0.00			-2358.82			31.07	0.00	153.19	889.85	
				SLE Freq.		0.00			-2150.52			28.33	0.00	139.66	811.27	0.0912
				SLE Q.P.		0.00			-2081.72			27.42	0.00	135.19	785.31	0.0883
6039	0.72	9.42	9.42			0.00	11109.65	0.22	-3631.01	-11109.65	0.22					
				SLE Rare		0.00			-689.48			9.08	0.00	44.78	260.10	
				SLE Freq.		0.00			-633.51			8.35	0.00	41.14	238.99	0.0269
				SLE Q.P.		0.00			-615.48			8.11	0.00	39.97	232.19	0.0261
Trave Sez. 2 Rett. 40x40 [cm]																
6039	0.00	9.71	9.42			2758.82	11397.24	0.22	-667.32	-11110.44	0.22					
				SLE Rare		0.00			-454.01			5.97	0.00	29.29	171.33	
				SLE Freq.		0.00			-418.96			5.50	0.00	27.03	158.10	0.0178
				SLE Q.P.		0.00			-407.85			5.36	0.00	26.31	153.91	0.0173
Camp.	0.37	11.17	9.42	5320.00	183.71	6588.90	12854.87	0.23	-667.32	-11113.99	0.22					
				SLE Rare		1754.19			-124.31			1.61	21.67	562.89	120.12	
				SLE Freq.		1585.62			-113.02			1.47	19.59	508.79	108.58	0.0104
				SLE Q.P.		1529.43			-109.26			1.42	18.89	490.76	104.73	0.0101
6037	0.74	12.63	9.42			6588.90	14307.30	0.24	0.00	-11116.93	0.22					
				SLE Rare		4455.25			0.00			0.00	52.64	1271.98	313.88	
				SLE Freq.		4040.48			0.00			0.00	47.74	1153.56	284.66	0.0247
				SLE Q.P.		3902.23			0.00			0.00	46.11	1114.09	274.92	0.0239
Trave Sez. 2 Rett. 40x40 [cm]																
6037	0.00	13.08	9.42			11796.34	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4626.87			0.00			0.00	53.99	1277.37	328.24	
				SLE Freq.		4197.59			0.00			0.00	48.98	1158.85	297.78	0.0251
				SLE Q.P.		4054.49			0.00			0.00	47.32	1119.35	287.63	0.0243
Camp.	0.30	14.24	9.42	5320.00	178.82	14963.26	15899.04	0.26	-168.10	-11119.63	0.22					

				SLE Rare		7207.76			-113.75			1.44	81.69	1836.32	518.82	
				SLE Freq.		6543.36			-103.42			1.31	74.16	1667.05	470.99	0.0373
				SLE Q.P.		6321.89			-99.98			1.26	71.65	1610.62	455.05	0.0360
201	0.61	15.62	9.42			14963.26	17258.31	0.27	-25.49	-11121.61	0.22					
				SLE Rare		10121.67			-17.25			0.22	111.20	2361.65	738.13	
				SLE Freq.		9191.89			-15.68			0.20	100.99	2144.71	670.32	0.0495
				SLE Q.P.		8881.97			-15.16			0.19	97.58	2072.39	647.72	0.0479

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	Staffe
Trave 210 6181 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	14988.66	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6181 6147 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11752.24	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6147 6097 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7797.87	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6097 6091 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3942.43	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6091 6051 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3920.64	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6051 6039 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7776.08	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6039 6037 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11730.45	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 6037 201 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14966.87	8004.72	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 347 Nodi 301 9044 9047 9055 9057 9090 9098 9124 311*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
301	0.12	18.71	6.49			14392.07	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		9736.88			-17.25			0.25	104.79	1910.07	529.28	
				SLE Freq.		8808.24			-15.68			0.23	94.80	1727.90	478.80	0.0342
				SLE Q.P.		8498.69			-15.16			0.22	91.47	1667.17	461.97	0.0330
Camp.	0.43	16.64	9.42	5320.00	178.82	14392.07	18263.85	0.28	-168.10	-11122.91	0.22					
				SLE Rare		6887.03			-113.75			1.41	74.11	1512.65	505.99	
				SLE Freq.		6223.40			-103.42			1.28	66.96	1366.89	457.23	0.0323
				SLE Q.P.		6002.19			-99.98			1.24	64.58	1318.30	440.98	0.0311
9044	0.73	14.91	9.42			11293.83	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4370.21			0.00			0.00	48.76	1065.32	316.75	
				SLE Freq.		3941.33			0.00			0.00	43.97	960.78	285.66	0.0218
				SLE Q.P.		3798.38			0.00			0.00	42.38	925.93	275.30	0.0210
Trave Sez. 2 Rett. 40x40 [cm]																
9044	0.00	14.23	9.42			6217.85	15895.24	0.26	0.00	-11119.63	0.22					
				SLE Rare		4205.67			0.00			0.00	47.67	1071.75	302.71	
				SLE Freq.		3791.53			0.00			0.00	42.98	966.22	272.91	0.0216
				SLE Q.P.		3653.49			0.00			0.00	41.41	931.04	262.97	0.0208
Camp.	0.37	12.04	9.42	5320.00	183.71	6217.85	13724.82	0.24	-812.47	-11115.81	0.22					
				SLE Rare		1582.89			-124.31			1.60	19.02	472.81	110.39	
				SLE Freq.		1414.50			-113.02			1.46	17.00	422.51	98.65	0.0089
				SLE Q.P.		1358.37			-109.26			1.41	16.33	405.74	94.73	0.0085
9047	0.74	9.86	9.42			2498.54	11540.97	0.22	-812.47	-11110.82	0.22					
				SLE Rare		0.00			-550.98			7.23	0.00	35.43	207.96	
				SLE Freq.		0.00			-512.18			6.72	0.00	32.94	193.31	0.0218
				SLE Q.P.		0.00			-501.22			6.58	0.00	32.23	189.18	0.0213
Trave Sez. 2 Rett. 40x40 [cm]																

9047	0.00	9.42	9.42			0.00	11109.65	0.22	-3630.68	-11109.65	0.22					
				SLE Rare		0.00			-772.99			10.18	0.00	50.20	291.60	
				SLE Freq.		0.00			-713.63			9.40	0.00	46.35	269.21	0.0303
				SLE Q.P.		0.00			-695.69			9.16	0.00	45.18	262.44	0.0295
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5142.43	-11109.65	0.22					
				SLE Rare		0.00			-2363.20			31.13	0.00	153.47	891.50	
				SLE Freq.		0.00			-2154.69			28.38	0.00	139.93	812.84	0.0914
				SLE Q.P.		0.00			-2086.11			27.48	0.00	135.48	786.97	0.0885
9055	0.72	9.42	9.42			0.00	11109.65	0.22	-5142.43	-11109.65	0.22					
				SLE Rare		0.00			-3480.74			45.85	0.00	226.05	1313.09	
				SLE Freq.		0.00			-3166.00			41.71	0.00	205.61	1194.35	0.1343
				SLE Q.P.		0.00			-3061.11			40.32	0.00	198.80	1154.78	0.1299
Trave Sez. 2 Rett. 40x40 [cm]																
9055	0.00	9.42	9.42			0.00	11109.65	0.22	-6365.85	-11109.65	0.22					
				SLE Rare		0.00			-3633.55			47.87	0.00	235.97	1370.73	
				SLE Freq.		0.00			-3304.28			43.53	0.00	214.59	1246.51	0.1402
				SLE Q.P.		0.00			-3194.36			42.08	0.00	207.45	1205.05	0.1355
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6590.51	-11109.65	0.22					
				SLE Rare		0.00			-4288.79			56.50	0.00	278.53	1617.92	
				SLE Freq.		0.00			-3892.89			51.28	0.00	252.82	1468.56	0.1660
				SLE Q.P.		0.00			-3760.68			49.54	0.00	244.23	1418.69	0.1596
9057	0.74	9.42	9.42			0.00	11109.65	0.22	-6590.51	-11109.65	0.22					
				SLE Rare		0.00			-4453.73			58.67	0.00	289.24	1680.14	
				SLE Freq.		0.00			-4034.90			53.15	0.00	262.04	1522.14	0.1761
				SLE Q.P.		0.00			-3895.27			51.31	0.00	252.97	1469.46	0.1662
Trave Sez. 2 Rett. 40x40 [cm]																
9057	0.00	9.42	9.42			0.00	11109.65	0.22	-6572.80	-11109.65	0.22					
				SLE Rare		0.00			-4448.35			58.60	0.00	288.89	1678.11	
				SLE Freq.		0.00			-4029.25			53.08	0.00	261.67	1520.01	0.1757
				SLE Q.P.		0.00			-3889.50			51.24	0.00	252.60	1467.29	0.1658
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6572.80	-11109.65	0.22					
				SLE Rare		0.00			-4122.07			54.30	0.00	267.70	1555.02	
				SLE Freq.		0.00			-3725.04			49.07	0.00	241.92	1405.24	0.1581
				SLE Q.P.		0.00			-3592.69			47.33	0.00	233.32	1355.32	0.1524
9090	0.74	9.42	9.42			0.00	11109.65	0.22	-6132.22	-11109.65	0.22					
				SLE Rare		0.00			-3304.57			43.53	0.00	214.61	1246.62	
				SLE Freq.		0.00			-2974.33			39.18	0.00	193.16	1122.04	0.1262
				SLE Q.P.		0.00			-2864.25			37.73	0.00	186.01	1080.52	0.1215
Trave Sez. 2 Rett. 40x40 [cm]																
9090	0.00	9.42	9.42			0.00	11109.65	0.22	-4650.07	-11109.65	0.22					
				SLE Rare		0.00			-3146.78			41.45	0.00	204.36	1187.10	
				SLE Freq.		0.00			-2830.91			37.29	0.00	183.85	1067.94	0.1201
				SLE Q.P.		0.00			-2725.62			35.91	0.00	177.01	1028.22	0.1156
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-4650.07	-11109.65	0.22					
				SLE Rare		0.00			-1867.58			24.60	0.00	121.29	704.53	
				SLE Freq.		0.00			-1660.58			21.88	0.00	107.84	626.44	0.0705
				SLE Q.P.		0.00			-1591.58			20.97	0.00	103.36	600.41	0.0675
9098	0.72	9.42	9.42			0.00	11109.65	0.22	-2917.13	-11109.65	0.22					
				SLE Rare		0.00			-115.71			1.52	0.00	7.51	43.65	
				SLE Freq.		0.00			-60.52			0.80	0.00	3.93	22.83	0.0026
				SLE Q.P.		0.00			-42.12			0.55	0.00	2.74	15.89	0.0018
Trave Sez. 2 Rett. 40x40 [cm]																
9098	0.00	9.86	9.42			3719.51	11540.97	0.22	0.00	-11110.82	0.22					
				SLE Rare		163.67			0.00			0.00	2.12	59.17	10.80	
				SLE Freq.		147.77			0.00			0.00	1.91	53.42	9.75	0.0010

				SLE Q.P.		140.94			0.00			0.00	1.82	50.95	9.30	0.0010
Camp.	0.37	12.04	9.42	5320.00	183.71	7672.24	13724.81	0.24	-183.71	-11115.81	0.22					
				SLE Rare		2403.70			-124.31			1.60	28.89	717.99	167.64	
				SLE Freq.		2217.57			-113.02			1.46	26.65	662.39	154.66	0.0140
				SLE Q.P.		2162.15			-109.26			1.41	25.99	645.83	150.79	0.0136
9124	0.74	14.23	9.42			7672.24	15895.24	0.26	0.00	-11119.63	0.22					
				SLE Rare		5192.29			0.00			0.00	58.85	1323.18	373.73	
				SLE Freq.		4757.70			0.00			0.00	53.93	1212.43	342.45	0.0271
				SLE Q.P.		4620.39			0.00			0.00	52.37	1177.44	332.56	0.0263
Trave Sez. 2 Rett. 40x40 [cm]																
9124	0.00	14.91	9.42			12932.12	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		5308.30			0.00			0.00	59.22	1294.00	384.74	
				SLE Freq.		4860.88			0.00			0.00	54.23	1184.93	352.31	0.0269
				SLE Q.P.		4718.85			0.00			0.00	52.65	1150.31	342.02	0.0261
Camp.	0.30	16.64	9.42	5320.00	178.82	16175.08	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7960.83			-113.75			1.41	85.66	1748.49	584.88	
				SLE Freq.		7276.42			-103.42			1.28	78.30	1598.17	534.60	0.0378
				SLE Q.P.		7056.17			-99.98			1.24	75.93	1549.80	518.42	0.0366
311	0.61	18.71	6.49			16175.08	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10946.37			-17.25			0.25	117.81	2147.33	595.02	
				SLE Freq.		9994.74			-15.68			0.23	107.57	1960.65	543.29	0.0388
				SLE Q.P.		9686.17			-15.16			0.22	104.25	1900.12	526.52	0.0376

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 301 9044 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	14654.98	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9044 9047 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11418.57	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9047 9055 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7464.19	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9055 9057 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3608.75	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9057 9090 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	4265.91	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9090 9098 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	8121.35	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9098 9124 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	12075.73	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9124 311 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	15312.14	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 349 Nodi 311 9162 9164 9202 9204 9206 9217 9245 320*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
311	0.13	18.71	9.42			15116.83	20274.91	0.30	-25.49	-11125.18	0.22					
				SLE Rare		10230.09			-17.25			0.21	106.06	2010.33	759.80	
				SLE Freq.		9303.99			-15.68			0.19	96.46	1828.34	691.02	0.0450
				SLE Q.P.		8995.53			-15.16			0.19	93.26	1767.73	668.11	0.0435
Camp.	0.43	16.64	9.42	5320.00	178.82	15116.83	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7311.47			-113.76			1.41	78.67	1605.87	537.17	
				SLE Freq.		6650.22			-103.42			1.28	71.56	1460.64	488.59	0.0345
				SLE Q.P.		6430.03			-99.98			1.24	69.19	1412.27	472.41	0.0334
9162	0.73	14.91	9.42			11945.35	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4725.88			0.00			0.00	52.73	1152.02	342.53	
				SLE Freq.		4299.21			0.00			0.00	47.97	1048.02	311.60	0.0238

				SLE Q.P.		4157.22			0.00			0.00	46.38	1013.40	301.31	0.0230
Trave Sez. 2 Rett. 40x40 [cm]																
9162	0.00	14.23	9.42			6753.40	15895.23	0.26	0.00	-11119.63	0.22					
				SLE Rare		4570.45			0.00			0.00	51.80	1164.71	328.97	
				SLE Freq.		4158.16			0.00			0.00	47.13	1059.64	299.29	0.0237
				SLE Q.P.		4020.98			0.00			0.00	45.58	1024.69	289.42	0.0229
Camp.	0.37	12.04	9.42	5320.00	183.71	6753.40	13724.82	0.24	-515.13	-11115.81	0.22					
				SLE Rare		1863.65			-124.31			1.60	22.40	556.67	129.97	
				SLE Freq.		1696.90			-113.02			1.46	20.39	506.86	118.34	0.0107
				SLE Q.P.		1641.57			-109.26			1.41	19.73	490.34	114.48	0.0103
9164	0.74	9.86	9.42			2915.99	11540.97	0.22	-515.13	-11110.82	0.22					
				SLE Rare		0.00			-348.27			4.57	0.00	22.40	131.45	
				SLE Freq.		0.00			-313.51			4.11	0.00	20.16	118.33	0.0133
				SLE Q.P.		0.00			-301.92			3.96	0.00	19.42	113.95	0.0128
Trave Sez. 2 Rett. 40x40 [cm]																
9164	0.00	9.42	9.42			0.00	11109.65	0.22	-3471.01	-11109.65	0.22					
				SLE Rare		0.00			-572.73			7.54	0.00	37.19	216.06	
				SLE Freq.		0.00			-517.37			6.82	0.00	33.60	195.18	0.0220
				SLE Q.P.		0.00			-498.92			6.57	0.00	32.40	188.21	0.0212
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5098.80	-11109.65	0.22					
				SLE Rare		0.00			-2247.82			29.61	0.00	145.98	847.97	
				SLE Freq.		0.00			-2040.70			26.88	0.00	132.53	769.84	0.0866
				SLE Q.P.		0.00			-1971.66			25.97	0.00	128.05	743.79	0.0837
9202	0.72	9.42	9.42			0.00	11109.65	0.22	-5098.80	-11109.65	0.22					
				SLE Rare		0.00			-3450.22			45.45	0.00	224.07	1301.57	
				SLE Freq.		0.00			-3134.28			41.29	0.00	203.55	1182.38	0.1330
				SLE Q.P.		0.00			-3028.96			39.90	0.00	196.71	1142.65	0.1285
Trave Sez. 2 Rett. 40x40 [cm]																
9202	0.00	9.42	9.42			0.00	11109.65	0.22	-6462.49	-11109.65	0.22					
				SLE Rare		0.00			-3610.04			47.56	0.00	234.45	1361.86	
				SLE Freq.		0.00			-3279.47			43.20	0.00	212.98	1237.16	0.1392
				SLE Q.P.		0.00			-3169.29			41.75	0.00	205.82	1195.59	0.1345
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6793.50	-11109.65	0.22					
				SLE Rare		0.00			-4349.26			57.29	0.00	282.45	1640.73	
				SLE Freq.		0.00			-3951.95			52.06	0.00	256.65	1490.84	0.1702
				SLE Q.P.		0.00			-3819.51			50.32	0.00	248.05	1440.88	0.1621
9204	0.74	9.42	9.42			0.00	11109.65	0.22	-6793.50	-11109.65	0.22					
				SLE Rare		0.00			-4597.26			60.56	0.00	298.56	1734.28	
				SLE Freq.		0.00			-4177.85			55.04	0.00	271.32	1576.06	0.1862
				SLE Q.P.		0.00			-4038.03			53.19	0.00	262.24	1523.32	0.1763
Trave Sez. 2 Rett. 40x40 [cm]																
9204	0.00	9.42	9.42			0.00	11109.65	0.22	-6791.57	-11109.65	0.22					
				SLE Rare		0.00			-4595.97			60.54	0.00	298.48	1733.80	
				SLE Freq.		0.00			-4176.66			55.02	0.00	271.24	1575.61	0.1861
				SLE Q.P.		0.00			-4036.87			53.18	0.00	262.17	1522.88	0.1762
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6791.57	-11109.65	0.22					
				SLE Rare		0.00			-4352.75			57.34	0.00	282.68	1642.04	
				SLE Freq.		0.00			-3956.26			52.12	0.00	256.93	1492.47	0.1705
				SLE Q.P.		0.00			-3823.94			50.37	0.00	248.34	1442.55	0.1623
9206	0.74	9.42	9.42			0.00	11109.65	0.22	-6466.95	-11109.65	0.22					
				SLE Rare		0.00			-3618.42			47.67	0.00	234.99	1365.02	
				SLE Freq.		0.00			-3289.27			43.33	0.00	213.62	1240.85	0.1396
				SLE Q.P.		0.00			-3179.28			41.88	0.00	206.47	1199.36	0.1349
Trave Sez. 2 Rett. 40x40 [cm]																
9206	0.00	9.42	9.42			0.00	11109.65	0.22	-5106.24	-11109.65	0.22					

				SLE Rare		0.00			-3455.75			45.52	0.00	224.43	1303.66	
				SLE Freq.		0.00			-3141.40			41.38	0.00	204.01	1185.07	0.1333
				SLE Q.P.		0.00			-3036.35			40.00	0.00	197.19	1145.44	0.1288
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5106.24	-11109.65	0.22					
				SLE Rare		0.00			-2258.48			29.75	0.00	146.67	851.99	
				SLE Freq.		0.00			-2053.20			27.05	0.00	133.34	774.55	0.0871
				SLE Q.P.		0.00			-1984.51			26.14	0.00	128.88	748.64	0.0842
9217	0.72	9.42	9.42			0.00	11109.65	0.22	-3485.22	-11109.65	0.22					
				SLE Rare		0.00			-588.53			7.75	0.00	38.22	222.02	
				SLE Freq.		0.00			-535.25			7.05	0.00	34.76	201.92	0.0227
				SLE Q.P.		0.00			-517.24			6.81	0.00	33.59	195.12	0.0219
Trave Sez. 2 Rett. 40x40 [cm]																
9217	0.00	9.86	9.42			2888.60	11540.97	0.22	-532.63	-11110.82	0.22					
				SLE Rare		0.00			-361.02			4.74	0.00	23.22	136.26	
				SLE Freq.		0.00			-328.43			4.31	0.00	21.12	123.96	0.0139
				SLE Q.P.		0.00			-317.33			4.16	0.00	20.41	119.77	0.0135
Camp.	0.37	12.04	9.42	5320.00	183.71	6718.89	13724.82	0.24	-532.63	-11115.81	0.22					
				SLE Rare		1844.25			-124.31			1.60	22.16	550.88	128.62	
				SLE Freq.		1676.51			-113.02			1.46	20.15	500.77	116.92	0.0105
				SLE Q.P.		1620.60			-109.26			1.41	19.48	484.07	113.02	0.0102
9245	0.74	14.23	9.42			6718.89	15895.24	0.26	0.00	-11119.63	0.22					
				SLE Rare		4545.80			0.00			0.00	51.53	1158.43	327.20	
				SLE Freq.		4132.27			0.00			0.00	46.84	1053.05	297.43	0.0235
				SLE Q.P.		3994.42			0.00			0.00	45.28	1017.92	287.51	0.0227
Trave Sez. 2 Rett. 40x40 [cm]																
9245	0.00	14.91	9.42			11909.25	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4705.45			0.00			0.00	52.50	1147.04	341.05	
				SLE Freq.		4277.35			0.00			0.00	47.72	1042.69	310.02	0.0237
				SLE Q.P.		4134.66			0.00			0.00	46.13	1007.90	299.67	0.0229
Camp.	0.30	16.64	9.42	5320.00	178.82	15076.29	18263.85	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7286.74			-113.75			1.41	78.41	1600.44	535.36	
				SLE Freq.		6623.85			-103.42			1.28	71.27	1454.84	486.65	0.0344
				SLE Q.P.		6402.88			-99.98			1.24	68.90	1406.31	470.42	0.0332
320	0.61	18.71	9.42			15076.29	20274.91	0.30	-25.49	-11125.18	0.22					
				SLE Rare		10201.04			-17.25			0.21	105.75	2004.62	757.64	
				SLE Freq.		9273.11			-15.68			0.19	96.13	1822.27	688.72	0.0449
				SLE Q.P.		8963.79			-15.16			0.19	92.93	1761.49	665.75	0.0434

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 311 9162 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	14987.51	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9162 9164 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11751.10	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9164 9202 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7796.73	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9202 9204 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3941.29	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9204 9206 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3921.20	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9206 9217 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7776.64	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9217 9245 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11731.01	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9245 320 Sez. 2 Rett. 40x40 [cm]							

0.00	0.61	0.61	14967.43	8004.72	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 350 Nodi 320 9244 9216 9205 9203 9201 9163 9161 310*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
320	0.13	18.71	6.49			16110.85	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10899.82			-17.25			0.25	117.31	2138.20	592.49	
				SLE Freq.		9947.75			-15.68			0.23	107.06	1951.43	540.74	0.0386
				SLE Q.P.		9638.33			-15.16			0.22	103.73	1890.73	523.92	0.0374
Camp.	0.43	16.64	9.42	5320.00	178.82	16110.85	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7921.13			-113.75			1.41	85.23	1739.77	581.96	
				SLE Freq.		7236.26			-103.42			1.28	77.86	1589.35	531.65	0.0375
				SLE Q.P.		7015.23			-99.98			1.24	75.48	1540.81	515.41	0.0364
9244	0.73	14.91	9.42			12874.81	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		5275.45			0.00			0.00	58.86	1285.99	382.36	
				SLE Freq.		4827.55			0.00			0.00	53.86	1176.81	349.89	0.0267
				SLE Q.P.		4684.82			0.00			0.00	52.27	1142.02	339.55	0.0259
Trave Sez. 2 Rett. 40x40 [cm]																
9244	0.00	14.23	9.42			7619.17	15895.23	0.26	0.00	-11119.63	0.22					
				SLE Rare		5153.89			0.00			0.00	58.42	1313.39	370.96	
				SLE Freq.		4718.98			0.00			0.00	53.49	1202.56	339.66	0.0269
				SLE Q.P.		4580.99			0.00			0.00	51.92	1167.40	329.73	0.0261
Camp.	0.37	12.04	9.42	5320.00	183.71	7619.17	13724.82	0.24	-183.71	-11115.81	0.22					
				SLE Rare		2373.67			-124.31			1.60	28.53	709.02	165.54	
				SLE Freq.		2187.20			-113.02			1.46	26.29	653.32	152.54	0.0138
				SLE Q.P.		2131.20			-109.26			1.41	25.61	636.59	148.63	0.0134
9216	0.74	9.86	9.42			3677.63	11540.97	0.22	0.00	-11110.82	0.22					
				SLE Rare		140.78			0.00			0.00	1.82	50.89	9.29	
				SLE Freq.		124.54			0.00			0.00	1.61	45.02	8.22	0.0009
				SLE Q.P.		118.43			0.00			0.00	1.53	42.81	7.81	0.0008
Trave Sez. 2 Rett. 40x40 [cm]																
9216	0.00	9.42	9.42			0.00	11109.65	0.22	-2936.56	-11109.65	0.22					
				SLE Rare		0.00			-137.79			1.82	0.00	8.95	51.98	
				SLE Freq.		0.00			-85.46			1.13	0.00	5.55	32.24	0.0036
				SLE Q.P.		0.00			-67.63			0.89	0.00	4.39	25.51	0.0029
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-4660.23	-11109.65	0.22					
				SLE Rare		0.00			-1882.45			24.80	0.00	122.25	710.14	
				SLE Freq.		0.00			-1677.66			22.10	0.00	108.95	632.89	0.0712
				SLE Q.P.		0.00			-1609.11			21.20	0.00	104.50	607.03	0.0683
9205	0.72	9.42	9.42			0.00	11109.65	0.22	-4660.23	-11109.65	0.22					
				SLE Rare		0.00			-3154.43			41.55	0.00	204.86	1189.98	
				SLE Freq.		0.00			-2840.12			37.41	0.00	184.45	1071.42	0.1205
				SLE Q.P.		0.00			-2735.16			36.03	0.00	177.63	1031.82	0.1161
Trave Sez. 2 Rett. 40x40 [cm]																
9205	0.00	9.42	9.42			0.00	11109.65	0.22	-6136.74	-11109.65	0.22					
				SLE Rare		0.00			-3315.67			43.68	0.00	215.33	1250.81	
				SLE Freq.		0.00			-2986.86			39.35	0.00	193.98	1126.77	0.1267
				SLE Q.P.		0.00			-2877.06			37.90	0.00	186.85	1085.35	0.1221
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6567.65	-11109.65	0.22					
				SLE Rare		0.00			-4125.81			54.35	0.00	267.94	1556.43	
				SLE Freq.		0.00			-3729.56			49.13	0.00	242.21	1406.95	0.1582
				SLE Q.P.		0.00			-3597.36			47.39	0.00	233.62	1357.08	0.1526
9203	0.74	9.42	9.42			0.00	11109.65	0.22	-6567.65	-11109.65	0.22					
				SLE Rare		0.00			-4444.73			58.55	0.00	288.65	1676.74	
				SLE Freq.		0.00			-4025.65			53.03	0.00	261.44	1518.65	0.1754

				SLE Q.P.		0.00			-3885.94			51.19	0.00	252.36	1465.94	0.1655
Trave Sez. 2 Rett. 40x40 [cm]																
9203	0.00	9.42	9.42			0.00	11109.65	0.22	-6588.13	-11109.65	0.22					
				SLE Rare		0.00			-4453.26			58.66	0.00	289.21	1679.96	
				SLE Freq.		0.00			-4034.35			53.15	0.00	262.00	1521.93	0.1760
				SLE Q.P.		0.00			-3894.70			51.31	0.00	252.93	1469.25	0.1662
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6588.13	-11109.65	0.22					
				SLE Rare		0.00			-4280.96			56.39	0.00	278.02	1614.96	
				SLE Freq.		0.00			-3884.01			51.17	0.00	252.24	1465.22	0.1654
				SLE Q.P.		0.00			-3751.70			49.42	0.00	243.65	1415.30	0.1592
9201	0.74	9.42	9.42			0.00	11109.65	0.22	-6355.67	-11109.65	0.22					
				SLE Rare		0.00			-3617.45			47.65	0.00	234.93	1364.66	
				SLE Freq.		0.00			-3287.10			43.30	0.00	213.47	1240.04	0.1395
				SLE Q.P.		0.00			-3176.99			41.85	0.00	206.32	1198.50	0.1348
Trave Sez. 2 Rett. 40x40 [cm]																
9201	0.00	9.42	9.42			0.00	11109.65	0.22	-5124.83	-11109.65	0.22					
				SLE Rare		0.00			-3467.84			45.68	0.00	225.21	1308.22	
				SLE Freq.		0.00			-3152.40			41.53	0.00	204.73	1189.22	0.1338
				SLE Q.P.		0.00			-3047.25			40.14	0.00	197.90	1149.55	0.1293
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5124.83	-11109.65	0.22					
				SLE Rare		0.00			-2341.66			30.85	0.00	152.07	883.37	
				SLE Freq.		0.00			-2132.94			28.10	0.00	138.52	804.64	0.0905
				SLE Q.P.		0.00			-2064.03			27.19	0.00	134.04	778.64	0.0876
9163	0.72	9.42	9.42			0.00	11109.65	0.22	-3601.76	-11109.65	0.22					
				SLE Rare		0.00			-743.28			9.79	0.00	48.27	280.40	
				SLE Freq.		0.00			-683.74			9.01	0.00	44.40	257.94	0.0290
				SLE Q.P.		0.00			-665.37			8.77	0.00	43.21	251.00	0.0282
Trave Sez. 2 Rett. 40x40 [cm]																
9163	0.00	9.86	9.42			2538.96	11540.98	0.22	-777.54	-11110.82	0.22					
				SLE Rare		0.00			-525.56			6.90	0.00	33.80	198.36	
				SLE Freq.		0.00			-486.41			6.38	0.00	31.28	183.59	0.0207
				SLE Q.P.		0.00			-474.98			6.23	0.00	30.54	179.27	0.0202
Camp.	0.37	12.04	9.42	5320.00	183.71	6268.04	13724.82	0.24	-777.54	-11115.81	0.22					
				SLE Rare		1612.24			-124.31			1.60	19.38	481.58	112.44	
				SLE Freq.		1447.34			-113.02			1.46	17.39	432.32	100.94	0.0091
				SLE Q.P.		1391.95			-109.26			1.41	16.73	415.77	97.08	0.0088
9161	0.74	14.23	9.42			6268.04	15895.23	0.26	0.00	-11119.63	0.22					
				SLE Rare		4242.42			0.00			0.00	48.09	1081.12	305.36	
				SLE Freq.		3832.44			0.00			0.00	43.44	976.64	275.85	0.0218
				SLE Q.P.		3695.26			0.00			0.00	41.88	941.68	265.98	0.0210
Trave Sez. 2 Rett. 40x40 [cm]																
9161	0.00	14.91	9.42			11346.73	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4401.36			0.00			0.00	49.11	1072.92	319.01	
				SLE Freq.		3976.55			0.00			0.00	44.37	969.36	288.22	0.0220
				SLE Q.P.		3834.45			0.00			0.00	42.78	934.72	277.92	0.0212
Camp.	0.30	16.64	9.42	5320.00	178.82	14451.04	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		6924.25			-113.76			1.41	74.51	1520.82	508.72	
				SLE Freq.		6265.22			-103.42			1.28	67.41	1376.08	460.30	0.0325
				SLE Q.P.		6044.97			-99.98			1.24	65.04	1327.70	444.12	0.0314
310	0.61	18.71	6.49			14451.04	20249.27	0.32	-25.49	-8214.46	0.21					
				SLE Rare		9780.15			-17.25			0.25	105.26	1918.56	531.63	
				SLE Freq.		8856.66			-15.68			0.23	95.32	1737.39	481.43	0.0344
				SLE Q.P.		8548.18			-15.16			0.22	92.00	1676.88	464.66	0.0332

Da	**A**	**Dx**	**V_{Ed}**	**$V_{Rd,c}$**	**V_{Rcd}**	**V_{Rd}**	**Staffe**

[m]	[m]	[m]	[kg]	[kg]	[kg]	[kg]	
Trave 320 9244 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	15280.69	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9244 9216 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	12044.28	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9216 9205 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	8089.90	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9205 9203 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	4234.46	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9203 9201 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3636.31	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9201 9163 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7491.75	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9163 9161 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11446.12	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9161 310 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14682.54	7069.46	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 351 Nodi 310 9123 9097 9089 9056 9054 9046 9043 301*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
310	0.13	18.71	6.49			15377.80	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10407.60			-17.25			0.25	112.01	2041.64	565.74	
				SLE Freq.		9477.97			-15.68			0.23	102.01	1859.28	515.20	0.0368
				SLE Q.P.		9170.68			-15.16			0.22	98.70	1799.00	498.50	0.0356
Camp.	0.43	16.64	9.42	5320.00	178.82	15377.80	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7486.88			-113.75			1.41	80.56	1644.40	550.06	
				SLE Freq.		6821.95			-103.42			1.28	73.41	1498.35	501.21	0.0354
				SLE Q.P.		6602.90			-99.98			1.24	71.05	1450.24	485.11	0.0343
9123	0.73	14.91	9.42			12204.33	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4899.17			0.00			0.00	54.66	1194.27	355.09	
				SLE Freq.		4468.70			0.00			0.00	49.86	1089.33	323.89	0.0247
				SLE Q.P.		4327.80			0.00			0.00	48.28	1054.98	313.67	0.0240
Trave Sez. 2 Rett. 40x40 [cm]																
9123	0.00	14.23	9.42			7046.06	15895.24	0.26	0.00	-11119.63	0.22					
				SLE Rare		4768.93			0.00			0.00	54.05	1215.29	343.26	
				SLE Freq.		4352.22			0.00			0.00	49.33	1109.10	313.26	0.0248
				SLE Q.P.		4216.28			0.00			0.00	47.79	1074.46	303.48	0.0240
Camp.	0.37	12.04	9.42	5320.00	183.71	7046.06	13724.82	0.24	-241.89	-11115.81	0.22					
				SLE Rare		2059.54			-124.31			1.60	24.75	615.19	143.63	
				SLE Freq.		1888.20			-113.02			1.46	22.69	564.01	131.69	0.0119
				SLE Q.P.		1834.06			-109.26			1.41	22.04	547.83	127.91	0.0115
9097	0.74	9.86	9.42			3205.40	11540.97	0.22	-241.89	-11110.82	0.22					
				SLE Rare		0.00			-163.40			2.14	0.00	10.51	61.67	
				SLE Freq.		0.00			-125.06			1.64	0.00	8.04	47.20	0.0053
				SLE Q.P.		0.00			-112.28			1.47	0.00	7.22	42.38	0.0048
Trave Sez. 2 Rett. 40x40 [cm]																
9097	0.00	9.42	9.42			0.00	11109.65	0.22	-3178.53	-11109.65	0.22					
				SLE Rare		0.00			-372.63			4.91	0.00	24.20	140.57	
				SLE Freq.		0.00			-313.42			4.13	0.00	20.35	118.24	0.0133
				SLE Q.P.		0.00			-293.69			3.87	0.00	19.07	110.79	0.0125
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-4809.13	-11109.65	0.22					
				SLE Rare		0.00			-2050.06			27.01	0.00	133.14	773.37	
				SLE Freq.		0.00			-1839.33			24.23	0.00	119.45	693.87	0.0780
				SLE Q.P.		0.00			-1769.08			23.30	0.00	114.89	667.37	0.0751

9089	0.72	9.42	9.42			0.00	11109.65	0.22	-4809.13	-11109.65	0.22					
				SLE Rare		0.00			-3254.81			42.88	0.00	211.38	1227.85	
				SLE Freq.		0.00			-2935.49			38.67	0.00	190.64	1107.39	0.1246
				SLE Q.P.		0.00			-2829.05			37.27	0.00	183.73	1067.24	0.1200
Trave Sez. 2 Rett. 40x40 [cm]																
9089	0.00	9.42	9.42			0.00	11109.65	0.22	-6163.42	-11109.65	0.22					
				SLE Rare		0.00			-3406.04			44.87	0.00	221.20	1284.90	
				SLE Freq.		0.00			-3071.94			40.47	0.00	199.50	1158.87	0.1303
				SLE Q.P.		0.00			-2960.58			39.00	0.00	192.27	1116.86	0.1256
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6497.37	-11109.65	0.22					
				SLE Rare		0.00			-4147.65			54.64	0.00	269.36	1564.67	
				SLE Freq.		0.00			-3747.05			49.36	0.00	243.34	1413.55	0.1590
				SLE Q.P.		0.00			-3613.51			47.60	0.00	234.67	1363.17	0.1533
9056	0.74	9.42	9.42			0.00	11109.65	0.22	-6497.37	-11109.65	0.22					
				SLE Rare		0.00			-4398.03			57.94	0.00	285.62	1659.13	
				SLE Freq.		0.00			-3975.84			52.37	0.00	258.20	1499.86	0.1719
				SLE Q.P.		0.00			-3834.97			50.52	0.00	249.05	1446.71	0.1627
Trave Sez. 2 Rett. 40x40 [cm]																
9056	0.00	9.42	9.42			0.00	11109.65	0.22	-6494.61	-11109.65	0.22					
				SLE Rare		0.00			-4396.13			57.91	0.00	285.50	1658.41	
				SLE Freq.		0.00			-3973.99			52.35	0.00	258.08	1499.16	0.1718
				SLE Q.P.		0.00			-3833.15			50.50	0.00	248.94	1446.03	0.1626
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6494.61	-11109.65	0.22					
				SLE Rare		0.00			-4155.30			54.74	0.00	269.86	1567.56	
				SLE Freq.		0.00			-3756.33			49.48	0.00	243.95	1417.05	0.1594
				SLE Q.P.		0.00			-3623.00			47.73	0.00	235.29	1366.75	0.1537
9054	0.74	9.42	9.42			0.00	11109.65	0.22	-6172.93	-11109.65	0.22					
				SLE Rare		0.00			-3423.25			45.10	0.00	222.32	1291.40	
				SLE Freq.		0.00			-3092.07			40.73	0.00	200.81	1166.46	0.1312
				SLE Q.P.		0.00			-2981.13			39.27	0.00	193.60	1124.61	0.1265
Trave Sez. 2 Rett. 40x40 [cm]																
9054	0.00	9.42	9.42			0.00	11109.65	0.22	-4826.02	-11109.65	0.22					
				SLE Rare		0.00			-3267.72			43.05	0.00	212.22	1232.72	
				SLE Freq.		0.00			-2951.38			38.88	0.00	191.67	1113.39	0.1252
				SLE Q.P.		0.00			-2845.42			37.48	0.00	184.79	1073.41	0.1207
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-4826.02	-11109.65	0.22					
				SLE Rare		0.00			-2072.34			27.30	0.00	134.58	781.78	
				SLE Freq.		0.00			-1865.86			24.58	0.00	121.17	703.88	0.0792
				SLE Q.P.		0.00			-1796.31			23.66	0.00	116.66	677.64	0.0762
9046	0.72	9.42	9.42			0.00	11109.65	0.22	-3207.19	-11109.65	0.22					
				SLE Rare		0.00			-404.29			5.33	0.00	26.26	152.51	
				SLE Freq.		0.00			-350.59			4.62	0.00	22.77	132.26	0.0149
				SLE Q.P.		0.00			-331.76			4.37	0.00	21.55	125.15	0.0141
Trave Sez. 2 Rett. 40x40 [cm]																
9046	0.00	9.86	9.42			3147.61	11540.97	0.22	-277.28	-11110.82	0.22					
				SLE Rare		0.00			-190.24			2.50	0.00	12.23	71.80	
				SLE Freq.		0.00			-157.32			2.06	0.00	10.12	59.38	0.0067
				SLE Q.P.		0.00			-145.47			1.91	0.00	9.35	54.90	0.0062
Camp.	0.37	12.04	9.42	5320.00	183.71	6974.01	13724.81	0.24	-277.28	-11115.81	0.22					
				SLE Rare		2017.26			-124.31			1.60	24.24	602.55	140.69	
				SLE Freq.		1845.52			-113.02			1.46	22.18	551.26	128.71	0.0116
				SLE Q.P.		1790.15			-109.26			1.41	21.51	534.72	124.85	0.0113
9043	0.74	14.23	9.42			6974.01	15895.23	0.26	0.00	-11119.63	0.22					
				SLE Rare		4715.76			0.00			0.00	53.45	1201.74	339.43	
				SLE Freq.		4298.63			0.00			0.00	48.72	1095.44	309.40	0.0245

				SLE Q.P.		4161.24			0.00			0.00	47.17	1060.43	299.52	0.0237
Trave Sez. 2 Rett. 40x40 [cm]																
9043	0.00	14.91	9.42			12126.92	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4853.24			0.00			0.00	54.15	1183.07	351.76	
				SLE Freq.		4422.13			0.00			0.00	49.34	1077.98	320.51	0.0245
				SLE Q.P.		4279.81			0.00			0.00	47.75	1043.29	310.20	0.0237
Camp.	0.30	16.64	9.42	5320.00	178.82	15291.56	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7432.04			-113.75			1.41	79.97	1632.35	546.03	
				SLE Freq.		6766.46			-103.42			1.28	72.81	1486.17	497.13	0.0351
				SLE Q.P.		6545.81			-99.98			1.24	70.43	1437.70	480.92	0.0340
301	0.61	18.71	6.49			15291.56	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10343.86			-17.25			0.25	111.32	2029.14	562.27	
				SLE Freq.		9413.56			-15.68			0.23	101.31	1846.64	511.70	0.0365
				SLE Q.P.		9104.49			-15.16			0.22	97.99	1786.01	494.90	0.0353

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 310 9123 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	14996.62	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9123 9097 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11760.20	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9097 9089 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7805.82	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9089 9056 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3950.39	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9056 9054 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3912.83	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9054 9046 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7768.27	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9046 9043 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11722.65	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 9043 301 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14959.06	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 357 Nodi 110 3121 3087 3037 3031 2991 2979 2977 101*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
110	0.13	15.62	6.49			15155.18	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10259.86			-17.25			0.26	116.79	2388.24	548.62	
				SLE Freq.		9332.80			-15.68			0.23	106.24	2172.45	499.05	0.0405
				SLE Q.P.		9023.53			-15.16			0.22	102.72	2100.46	482.51	0.0392
Camp.	0.43	14.24	9.42	5320.00	178.82	15155.18	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7332.61			-113.75			1.44	83.11	1868.12	527.81	
				SLE Freq.		6670.64			-103.42			1.31	75.60	1699.48	480.16	0.0380
				SLE Q.P.		6449.73			-99.98			1.26	73.10	1643.19	464.26	0.0367
3121	0.73	13.08	9.42			11975.03	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4738.37			0.00			0.00	55.30	1308.15	336.15	
				SLE Freq.		4311.25			0.00			0.00	50.31	1190.23	305.85	0.0258
				SLE Q.P.		4168.62			0.00			0.00	48.65	1150.86	295.73	0.0250
Trave Sez. 2 Rett. 40x40 [cm]																
3121	0.00	12.63	9.42			6752.84	14307.31	0.24	0.00	-11116.93	0.22					
				SLE Rare		4572.97			0.00			0.00	54.03	1305.59	322.18	
				SLE Freq.		4160.89			0.00			0.00	49.16	1187.94	293.15	0.0254
				SLE Q.P.		4023.23			0.00			0.00	47.54	1148.64	283.45	0.0246
Camp.	0.37	11.17	9.42	5320.00	183.71	6752.84	12854.87	0.23	-542.73	-11113.99	0.22					
				SLE Rare		1855.60			-124.31			1.61	22.92	595.43	127.07	

				SLE Freq.		1689.38			-113.02			1.47	20.87	542.09	115.69	0.0111
				SLE Q.P.		1633.66			-109.26			1.42	20.18	524.21	111.87	0.0108
3087	0.74	9.71	9.42			2901.41	11397.24	0.22	-542.73	-11110.44	0.22					
				SLE Rare		0.00			-365.36			4.80	0.00	23.57	137.88	
				SLE Freq.		0.00			-331.19			4.35	0.00	21.37	124.98	0.0141
				SLE Q.P.		0.00			-319.80			4.20	0.00	20.63	120.68	0.0136
Trave Sez. 2 Rett. 40x40 [cm]																
3087	0.00	9.42	9.42			0.00	11109.65	0.22	-3526.69	-11109.65	0.22					
				SLE Rare		0.00			-598.58			7.89	0.00	38.87	225.81	
				SLE Freq.		0.00			-543.35			7.16	0.00	35.29	204.97	0.0231
				SLE Q.P.		0.00			-524.94			6.92	0.00	34.09	198.03	0.0223
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5168.00	-11109.65	0.22					
				SLE Rare		0.00			-2283.83			30.09	0.00	148.32	861.56	
				SLE Freq.		0.00			-2076.63			27.36	0.00	134.86	783.39	0.0881
				SLE Q.P.		0.00			-2007.57			26.45	0.00	130.38	757.34	0.0852
3037	0.72	9.42	9.42			0.00	11109.65	0.22	-5168.00	-11109.65	0.22					
				SLE Rare		0.00			-3496.69			46.06	0.00	227.09	1319.10	
				SLE Freq.		0.00			-3180.17			41.89	0.00	206.53	1199.70	0.1349
				SLE Q.P.		0.00			-3074.76			40.50	0.00	199.68	1159.93	0.1305
Trave Sez. 2 Rett. 40x40 [cm]																
3037	0.00	9.42	9.42			0.00	11109.65	0.22	-6559.45	-11109.65	0.22					
				SLE Rare		0.00			-3664.46			48.27	0.00	237.98	1382.39	
				SLE Freq.		0.00			-3332.82			43.90	0.00	216.44	1257.28	0.1414
				SLE Q.P.		0.00			-3222.37			42.45	0.00	209.27	1215.62	0.1367
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6904.94	-11109.65	0.22					
				SLE Rare		0.00			-4414.62			58.15	0.00	286.70	1665.38	
				SLE Freq.		0.00			-4015.45			52.90	0.00	260.78	1514.80	0.1747
				SLE Q.P.		0.00			-3882.68			51.15	0.00	252.15	1464.71	0.1653
3031	0.74	9.42	9.42			0.00	11109.65	0.22	-6904.94	-11109.65	0.22					
				SLE Rare		0.00			-4673.57			61.57	0.00	303.52	1763.07	
				SLE Freq.		0.00			-4251.70			56.01	0.00	276.12	1603.92	0.1914
				SLE Q.P.		0.00			-4111.45			54.16	0.00	267.01	1551.01	0.1815
Trave Sez. 2 Rett. 40x40 [cm]																
3031	0.00	9.42	9.42			0.00	11109.65	0.22	-6910.59	-11109.65	0.22					
				SLE Rare		0.00			-4677.42			61.62	0.00	303.77	1764.52	
				SLE Freq.		0.00			-4255.22			56.06	0.00	276.35	1605.25	0.1916
				SLE Q.P.		0.00			-4114.86			54.21	0.00	267.23	1552.30	0.1817
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6910.59	-11109.65	0.22					
				SLE Rare		0.00			-4445.14			58.56	0.00	288.68	1676.90	
				SLE Freq.		0.00			-4045.02			53.29	0.00	262.70	1525.95	0.1768
				SLE Q.P.		0.00			-3912.02			51.53	0.00	254.06	1475.78	0.1674
2991	0.74	9.42	9.42			0.00	11109.65	0.22	-6600.45	-11109.65	0.22					
				SLE Rare		0.00			-3721.65			49.03	0.00	241.70	1403.96	
				SLE Freq.		0.00			-3388.21			44.63	0.00	220.04	1278.18	0.1438
				SLE Q.P.		0.00			-3277.44			43.17	0.00	212.85	1236.39	0.1391
Trave Sez. 2 Rett. 40x40 [cm]																
2991	0.00	9.42	9.42			0.00	11109.65	0.22	-5258.26	-11109.65	0.22					
				SLE Rare		0.00			-3560.72			46.91	0.00	231.24	1343.26	
				SLE Freq.		0.00			-3241.78			42.70	0.00	210.53	1222.94	0.1376
				SLE Q.P.		0.00			-3135.83			41.31	0.00	203.65	1182.97	0.1331
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5258.26	-11109.65	0.22					
				SLE Rare		0.00			-2373.74			31.27	0.00	154.16	895.48	
				SLE Freq.		0.00			-2163.57			28.50	0.00	140.51	816.19	0.0918
				SLE Q.P.		0.00			-2093.88			27.58	0.00	135.98	789.90	0.0888
2979	0.72	9.42	9.42			0.00	11109.65	0.22	-3650.51	-11109.65	0.22					

				SLE Rare		0.00			-714.08			9.41	0.00	46.37	269.38	
				SLE Freq.		0.00			-655.61			8.64	0.00	42.58	247.32	0.0278
				SLE Q.P.		0.00			-636.49			8.38	0.00	41.34	240.11	0.0270
Trave Sez. 2 Rett. 40x40 [cm]																
2979	0.00	9.71	9.42			2700.11	11397.24	0.22	-709.67	-11110.44	0.22					
				SLE Rare		0.00			-484.01			6.36	0.00	31.23	182.65	
				SLE Freq.		0.00			-446.13			5.86	0.00	28.78	168.35	0.0189
				SLE Q.P.		0.00			-433.85			5.70	0.00	27.99	163.72	0.0184
Camp.	0.37	11.17	9.42	5320.00	183.71	6516.57	12854.87	0.23	-709.67	-11113.99	0.22					
				SLE Rare		1713.26			-124.31			1.61	21.16	549.75	117.32	
				SLE Freq.		1548.85			-113.02			1.47	19.13	497.00	106.06	0.0102
				SLE Q.P.		1494.04			-109.26			1.42	18.46	479.41	102.31	0.0098
2977	0.74	12.63	9.42			6516.57	14307.30	0.24	0.00	-11116.93	0.22					
				SLE Rare		4404.37			0.00			0.00	52.04	1257.45	310.30	
				SLE Freq.		3994.38			0.00			0.00	47.20	1140.40	281.42	0.0244
				SLE Q.P.		3857.72			0.00			0.00	45.58	1101.38	271.79	0.0236
Trave Sez. 2 Rett. 40x40 [cm]																
2977	0.00	13.08	9.42			11702.93	14757.60	0.25	0.00	-11117.74	0.22					
				SLE Rare		4571.87			0.00			0.00	53.35	1262.19	324.33	
				SLE Freq.		4147.47			0.00			0.00	48.40	1145.02	294.23	0.0248
				SLE Q.P.		4006.00			0.00			0.00	46.75	1105.96	284.19	0.0240
Camp.	0.30	14.24	9.42	5320.00	178.82	14861.41	15899.04	0.26	-168.10	-11119.63	0.22					
				SLE Rare		7144.63			-113.75			1.44	80.98	1820.23	514.27	
				SLE Freq.		6485.60			-103.42			1.31	73.51	1652.33	466.84	0.0369
				SLE Q.P.		6265.93			-99.98			1.26	71.02	1596.37	451.03	0.0357
101	0.61	15.62	6.49			14861.41	17260.20	0.28	-25.49	-8203.77	0.21					
				SLE Rare		10050.39			-17.25			0.26	114.41	2339.49	537.42	
				SLE Freq.		9126.50			-15.68			0.23	103.89	2124.43	488.02	0.0396
				SLE Q.P.		8818.54			-15.16			0.22	100.38	2052.74	471.55	0.0383

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 110 3121 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	15026.95	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3121 3087 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11790.54	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3087 3037 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7836.16	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3037 3031 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3980.72	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 3031 2991 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3882.28	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 2991 2979 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7737.72	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 2979 2977 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11692.10	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 2977 101 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14928.51	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 358 Nodi 109 5802 5804 5806 5808 5810 5812 5814 119*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
109	0.13	18.71	6.49			14839.43	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10032.17			-17.25			0.25	107.97	1967.99	545.33	
				SLE Freq.		9106.92			-15.68			0.23	98.01	1786.49	495.03	0.0353
				SLE Q.P.		8798.51			-15.16			0.22	94.69	1725.99	478.27	0.0341

Camp.	0.43	16.64	9.42	5320.00	178.82	14839.43	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7128.17			-113.76			1.41	76.70	1565.61	523.71	
				SLE Freq.		6467.97			-103.42			1.28	69.60	1420.61	475.20	0.0336
				SLE Q.P.		6247.91			-99.98			1.24	67.23	1372.27	459.03	0.0324
5802	0.73	14.91	9.42			11682.41	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4557.19			0.00			0.00	50.84	1110.90	330.30	
				SLE Freq.		4131.79			0.00			0.00	46.10	1007.21	299.47	0.0229
				SLE Q.P.		3990.00			0.00			0.00	44.52	972.64	289.19	0.0221
Trave Sez. 2 Rett. 40x40 [cm]																
5802	0.00	14.23	9.42			6496.51	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4388.00			0.00			0.00	49.74	1118.22	315.84	
				SLE Freq.		3976.99			0.00			0.00	45.08	1013.48	286.25	0.0226
				SLE Q.P.		3839.98			0.00			0.00	43.53	978.56	276.39	0.0219
Camp.	0.37	12.04	9.42	5320.00	183.71	6496.51	13724.80	0.24	-726.35	-11115.81	0.22					
				SLE Rare		1699.07			-124.31			1.60	20.42	507.51	118.50	
				SLE Freq.		1533.86			-113.02			1.46	18.43	458.16	106.97	0.0096
				SLE Q.P.		1478.79			-109.26			1.41	17.77	441.72	103.13	0.0093
5804	0.74	9.86	9.42			2682.50	11540.96	0.22	-726.35	-11110.82	0.22					
				SLE Rare		0.00			-497.18			6.52	0.00	31.97	187.65	
				SLE Freq.		0.00			-459.59			6.03	0.00	29.55	173.46	0.0195
				SLE Q.P.		0.00			-447.37			5.87	0.00	28.77	168.85	0.0190
Trave Sez. 2 Rett. 40x40 [cm]																
5804	0.00	9.42	9.42			0.00	11109.65	0.22	-3665.52	-11109.65	0.22					
				SLE Rare		0.00			-728.33			9.59	0.00	47.30	274.76	
				SLE Freq.		0.00			-670.14			8.83	0.00	43.52	252.80	0.0284
				SLE Q.P.		0.00			-651.08			8.58	0.00	42.28	245.61	0.0276
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5270.55	-11109.65	0.22					
				SLE Rare		0.00			-2385.58			31.43	0.00	154.93	899.94	
				SLE Freq.		0.00			-2175.53			28.66	0.00	141.29	820.70	0.0923
				SLE Q.P.		0.00			-2105.86			27.74	0.00	136.76	794.42	0.0894
5806	0.72	9.42	9.42			0.00	11109.65	0.22	-5270.55	-11109.65	0.22					
				SLE Rare		0.00			-3570.14			47.03	0.00	231.86	1346.81	
				SLE Freq.		0.00			-3251.18			42.83	0.00	211.14	1226.48	0.1379
				SLE Q.P.		0.00			-3145.21			41.43	0.00	204.26	1186.51	0.1335
Trave Sez. 2 Rett. 40x40 [cm]																
5806	0.00	9.42	9.42			0.00	11109.65	0.22	-6610.58	-11109.65	0.22					
				SLE Rare		0.00			-3731.77			49.16	0.00	242.35	1407.78	
				SLE Freq.		0.00			-3398.29			44.77	0.00	220.70	1281.98	0.1442
				SLE Q.P.		0.00			-3287.49			43.31	0.00	213.50	1240.18	0.1395
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6917.90	-11109.65	0.22					
				SLE Rare		0.00			-4452.80			58.66	0.00	289.18	1679.79	
				SLE Freq.		0.00			-4052.48			53.38	0.00	263.18	1528.77	0.1773
				SLE Q.P.		0.00			-3919.42			51.63	0.00	254.54	1478.57	0.1679
5808	0.74	9.42	9.42			0.00	11109.65	0.22	-6917.90	-11109.65	0.22					
				SLE Rare		0.00			-4682.62			61.69	0.00	304.10	1766.48	
				SLE Freq.		0.00			-4260.07			56.12	0.00	276.66	1607.08	0.1920
				SLE Q.P.		0.00			-4119.61			54.27	0.00	267.54	1554.09	0.1821
Trave Sez. 2 Rett. 40x40 [cm]																
5808	0.00	9.42	9.42			0.00	11109.65	0.22	-6912.78	-11109.65	0.22					
				SLE Rare		0.00			-4679.15			61.64	0.00	303.88	1765.17	
				SLE Freq.		0.00			-4256.92			56.08	0.00	276.46	1605.89	0.1918
				SLE Q.P.		0.00			-4116.56			54.23	0.00	267.34	1552.94	0.1818
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6912.78	-11109.65	0.22					
				SLE Rare		0.00			-4417.74			58.20	0.00	286.90	1666.56	
				SLE Freq.		0.00			-4018.22			52.93	0.00	260.96	1515.84	0.1749

				SLE Q.P.		0.00			-3885.27			51.18	0.00	252.32	1465.69	0.1655
5810	0.74	9.42	9.42			0.00	11109.65	0.22	-6564.47	-11109.65	0.22					
				SLE Rare		0.00			-3665.31			48.28	0.00	238.04	1382.71	
				SLE Freq.		0.00			-3333.20			43.91	0.00	216.47	1257.43	0.1414
				SLE Q.P.		0.00			-3222.50			42.45	0.00	209.28	1215.66	0.1367
Trave Sez. 2 Rett. 40x40 [cm]																
5810	0.00	9.42	9.42			0.00	11109.65	0.22	-5170.53	-11109.65	0.22					
				SLE Rare		0.00			-3497.80			46.08	0.00	227.16	1319.52	
				SLE Freq.		0.00			-3180.82			41.90	0.00	206.57	1199.94	0.1350
				SLE Q.P.		0.00			-3075.15			40.51	0.00	199.71	1160.08	0.1305
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5170.53	-11109.65	0.22					
				SLE Rare		0.00			-2283.11			30.08	0.00	148.27	861.29	
				SLE Freq.		0.00			-2074.94			27.33	0.00	134.75	782.76	0.0880
				SLE Q.P.		0.00			-2005.55			26.42	0.00	130.25	756.58	0.0851
5812	0.72	9.42	9.42			0.00	11109.65	0.22	-3527.35	-11109.65	0.22					
				SLE Rare		0.00			-595.73			7.85	0.00	38.69	224.74	
				SLE Freq.		0.00			-539.32			7.10	0.00	35.02	203.45	0.0229
				SLE Q.P.		0.00			-520.51			6.86	0.00	33.80	196.36	0.0221
Trave Sez. 2 Rett. 40x40 [cm]																
5812	0.00	9.86	9.42			2907.73	11540.97	0.22	-541.05	-11110.82	0.22					
				SLE Rare		0.00			-362.79			4.76	0.00	23.33	136.93	
				SLE Freq.		0.00			-327.47			4.30	0.00	21.06	123.60	0.0139
				SLE Q.P.		0.00			-315.70			4.14	0.00	20.30	119.15	0.0134
Camp.	0.37	12.04	9.42	5320.00	183.71	6762.03	13724.81	0.24	-541.05	-11115.81	0.22					
				SLE Rare		1861.65			-124.31			1.60	22.37	556.08	129.83	
				SLE Freq.		1696.50			-113.02			1.46	20.39	506.75	118.32	0.0107
				SLE Q.P.		1641.08			-109.26			1.41	19.72	490.19	114.45	0.0103
5814	0.74	14.23	9.42			6762.03	15895.24	0.26	0.00	-11119.63	0.22					
				SLE Rare		4581.49			0.00			0.00	51.93	1167.52	329.76	
				SLE Freq.		4170.64			0.00			0.00	47.27	1062.83	300.19	0.0237
				SLE Q.P.		4033.31			0.00			0.00	45.72	1027.83	290.31	0.0230
Trave Sez. 2 Rett. 40x40 [cm]																
5814	0.00	14.91	9.42			11986.69	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4746.31			0.00			0.00	52.95	1157.01	344.01	
				SLE Freq.		4320.34			0.00			0.00	48.20	1053.17	313.13	0.0239
				SLE Q.P.		4178.02			0.00			0.00	46.61	1018.47	302.82	0.0231
Camp.	0.30	16.64	9.42	5320.00	178.82	15168.62	18263.85	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7342.57			-113.75			1.41	79.01	1612.70	539.46	
				SLE Freq.		6681.88			-103.42			1.28	71.90	1467.59	490.92	0.0347
				SLE Q.P.		6461.32			-99.98			1.24	69.52	1419.15	474.71	0.0335
119	0.61	18.71	6.49			15168.62	20249.27	0.32	-25.49	-8214.46	0.21					
				SLE Rare		10271.85			-17.25			0.25	110.55	2015.01	558.36	
				SLE Freq.		9346.20			-15.68			0.23	100.59	1833.43	508.04	0.0363
				SLE Q.P.		9037.29			-15.16			0.22	97.26	1772.83	491.25	0.0351

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 109 5802 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	14921.65	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5802 5804 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11685.21	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5804 5806 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7730.85	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5806 5808 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3875.41	8004.72	37247.76	36621.00	ø 10 2br. 12.5'

Trave 5808 5810 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3988.78	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5810 5812 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7844.21	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5812 5814 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11798.59	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5814 119 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	15035.00	7069.46	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 383 Nodi 119 5816 5818 5820 5822 5824 5826 5828 125*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
119	0.13	18.71	6.49			14830.57	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10032.20			-17.25			0.25	107.97	1968.00	545.33	
				SLE Freq.		9117.71			-15.68			0.23	98.13	1788.60	495.62	0.0354
				SLE Q.P.		8812.88			-15.16			0.22	94.85	1728.81	479.05	0.0342
Camp.	0.43	16.64	9.42	5320.00	178.82	14830.57	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7133.07			-113.76			1.41	76.75	1566.69	524.07	
				SLE Freq.		6481.84			-103.42			1.28	69.75	1423.65	476.22	0.0336
				SLE Q.P.		6264.76			-99.98			1.24	67.41	1375.97	460.27	0.0325
5816	0.73	14.91	9.42			11679.79	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4566.96			0.00			0.00	50.95	1113.29	331.01	
				SLE Freq.		4148.74			0.00			0.00	46.29	1011.34	300.70	0.0230
				SLE Q.P.		4009.33			0.00			0.00	44.73	977.35	290.59	0.0222
Trave Sez. 2 Rett. 40x40 [cm]																
5816	0.00	14.23	9.42			6497.30	15895.23	0.26	0.00	-11119.63	0.22					
				SLE Rare		4392.77			0.00			0.00	49.79	1119.43	316.18	
				SLE Freq.		3989.62			0.00			0.00	45.22	1016.70	287.16	0.0227
				SLE Q.P.		3855.24			0.00			0.00	43.70	982.45	277.49	0.0220
Camp.	0.37	12.04	9.42	5320.00	183.71	6497.30	13724.81	0.24	-700.59	-11115.81	0.22					
				SLE Rare		1709.78			-124.31			1.60	20.55	510.71	119.24	
				SLE Freq.		1550.24			-113.02			1.46	18.63	463.06	108.12	0.0098
				SLE Q.P.		1497.06			-109.26			1.41	17.99	447.17	104.41	0.0094
5818	0.74	9.86	9.42			2693.30	11540.97	0.22	-700.59	-11110.82	0.22					
				SLE Rare		0.00			-477.84			6.27	0.00	30.73	180.35	
				SLE Freq.		0.00			-438.37			5.75	0.00	28.19	165.46	0.0186
				SLE Q.P.		0.00			-425.17			5.58	0.00	27.34	160.47	0.0181
Trave Sez. 2 Rett. 40x40 [cm]																
5818	0.00	9.42	9.42			0.00	11109.65	0.22	-3637.76	-11109.65	0.22					
				SLE Rare		0.00			-713.91			9.40	0.00	46.36	269.32	
				SLE Freq.		0.00			-653.44			8.61	0.00	42.44	246.51	0.0277
				SLE Q.P.		0.00			-633.25			8.34	0.00	41.13	238.89	0.0269
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5234.79	-11109.65	0.22					
				SLE Rare		0.00			-2366.43			31.17	0.00	153.68	892.72	
				SLE Freq.		0.00			-2155.92			28.40	0.00	140.01	813.30	0.0915
				SLE Q.P.		0.00			-2085.70			27.48	0.00	135.45	786.82	0.0885
5820	0.72	9.42	9.42			0.00	11109.65	0.22	-5234.79	-11109.65	0.22					
				SLE Rare		0.00			-3546.27			46.72	0.00	230.31	1337.80	
				SLE Freq.		0.00			-3228.65			42.53	0.00	209.68	1217.98	0.1370
				SLE Q.P.		0.00			-3122.73			41.14	0.00	202.80	1178.03	0.1325
Trave Sez. 2 Rett. 40x40 [cm]																
5820	0.00	9.42	9.42			0.00	11109.65	0.22	-6574.42	-11109.65	0.22					
				SLE Rare		0.00			-3713.93			48.92	0.00	241.19	1401.05	
				SLE Freq.		0.00			-3381.37			44.54	0.00	219.60	1275.60	0.1435
				SLE Q.P.		0.00			-3270.49			43.08	0.00	212.40	1233.77	0.1388

Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6873.40	-11109.65	0.22					
				SLE Rare		0.00			-4430.15			58.36	0.00	287.71	1671.24	
				SLE Freq.		0.00			-4032.60			53.12	0.00	261.89	1521.27	0.1759
				SLE Q.P.		0.00			-3900.04			51.38	0.00	253.28	1471.26	0.1665
5822	0.74	9.42	9.42			0.00	11109.65	0.22	-6873.40	-11109.65	0.22					
				SLE Rare		0.00			-4655.14			61.32	0.00	302.32	1756.12	
				SLE Freq.		0.00			-4237.22			55.82	0.00	275.18	1598.46	0.1904
				SLE Q.P.		0.00			-4097.87			53.98	0.00	266.13	1545.89	0.1805
Trave Sez. 2 Rett. 40x40 [cm]																
5822	0.00	9.42	9.42			0.00	11109.65	0.22	-6878.02	-11109.65	0.22					
				SLE Rare		0.00			-4658.26			61.36	0.00	302.52	1757.30	
				SLE Freq.		0.00			-4240.16			55.86	0.00	275.37	1599.57	0.1906
				SLE Q.P.		0.00			-4100.76			54.02	0.00	266.32	1546.98	0.1807
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6878.02	-11109.65	0.22					
				SLE Rare		0.00			-4392.04			57.86	0.00	285.23	1656.86	
				SLE Freq.		0.00			-3998.18			52.67	0.00	259.65	1508.28	0.1735
				SLE Q.P.		0.00			-3866.86			50.94	0.00	251.13	1458.74	0.1642
5824	0.74	9.42	9.42			0.00	11109.65	0.22	-6521.37	-11109.65	0.22					
				SLE Rare		0.00			-3634.60			47.88	0.00	236.04	1371.12	
				SLE Freq.		0.00			-3309.60			43.60	0.00	214.94	1248.52	0.1404
				SLE Q.P.		0.00			-3201.23			42.17	0.00	207.90	1207.64	0.1358
Trave Sez. 2 Rett. 40x40 [cm]																
5824	0.00	9.42	9.42			0.00	11109.65	0.22	-5129.88	-11109.65	0.22					
				SLE Rare		0.00			-3475.03			45.78	0.00	225.68	1310.93	
				SLE Freq.		0.00			-3164.43			41.69	0.00	205.51	1193.76	0.1343
				SLE Q.P.		0.00			-3060.88			40.32	0.00	198.78	1154.70	0.1299
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5129.88	-11109.65	0.22					
				SLE Rare		0.00			-2254.75			29.70	0.00	146.43	850.59	
				SLE Freq.		0.00			-2055.06			27.07	0.00	133.46	775.26	0.0872
				SLE Q.P.		0.00			-1988.47			26.19	0.00	129.14	750.14	0.0844
5826	0.72	9.42	9.42			0.00	11109.65	0.22	-3477.50	-11109.65	0.22					
				SLE Rare		0.00			-561.79			7.40	0.00	36.48	211.93	
				SLE Freq.		0.00			-515.94			6.80	0.00	33.51	194.63	0.0219
				SLE Q.P.		0.00			-500.62			6.59	0.00	32.51	188.86	0.0212
Trave Sez. 2 Rett. 40x40 [cm]																
5826	0.00	9.86	9.42			2967.43	11540.95	0.22	-493.58	-11110.82	0.22					
				SLE Rare		0.00			-337.29			4.43	0.00	21.69	127.30	
				SLE Freq.		0.00			-311.55			4.09	0.00	20.03	117.59	0.0132
				SLE Q.P.		0.00			-302.96			3.98	0.00	19.48	114.35	0.0129
Camp.	0.37	12.04	9.42	5320.00	183.71	6830.45	13724.79	0.24	-493.58	-11115.81	0.22					
				SLE Rare		1893.99			-124.31			1.60	22.76	565.74	132.09	
				SLE Freq.		1716.09			-113.02			1.46	20.62	512.60	119.68	0.0108
				SLE Q.P.		1656.79			-109.26			1.41	19.91	494.88	115.55	0.0104
5828	0.74	14.23	9.42			6830.45	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4618.88			0.00			0.00	52.35	1177.05	332.46	
				SLE Freq.		4193.38			0.00			0.00	47.53	1068.62	301.83	0.0239
				SLE Q.P.		4051.54			0.00			0.00	45.92	1032.48	291.62	0.0231
Trave Sez. 2 Rett. 40x40 [cm]																
5828	0.00	14.91	9.42			12047.82	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4773.00			0.00			0.00	53.25	1163.51	345.94	
				SLE Freq.		4334.05			0.00			0.00	48.35	1056.51	314.13	0.0240
				SLE Q.P.		4187.73			0.00			0.00	46.72	1020.84	303.52	0.0232
Camp.	0.30	16.64	9.42	5320.00	178.82	15235.23	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7373.42			-113.76			1.41	79.34	1619.48	541.72	
				SLE Freq.		6698.18			-103.42			1.28	72.07	1471.17	492.11	0.0348

				SLE Q.P.		6473.10			-99.98			1.24	69.65	1421.74	475.58	0.0336
125	0.61	18.71	6.49			15235.23	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10306.86			-17.25			0.25	110.93	2021.88	560.26	
				SLE Freq.		9365.09			-15.68			0.23	100.79	1837.13	509.07	0.0363
				SLE Q.P.		9051.17			-15.16			0.22	97.41	1775.55	492.00	0.0351

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	Staffe
Trave 119 5816 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	14894.32	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5816 5818 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11657.90	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5818 5820 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7703.53	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5820 5822 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3848.10	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5822 5824 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	4013.40	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5824 5826 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7868.84	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5826 5828 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11823.21	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5828 125 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	15059.64	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 384 Nodi 125 5827 5825 5823 5821 5819 5817 5815 118*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
125	0.12	18.71	6.49			14986.68	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10143.30			-17.25			0.25	109.17	1989.79	551.37	
				SLE Freq.		9224.44			-15.68			0.23	99.28	1809.54	501.42	0.0358
				SLE Q.P.		8917.96			-15.16			0.22	95.98	1749.42	484.76	0.0346
Camp.	0.43	16.64	9.42	5320.00	178.82	14986.68	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7229.02			-113.76			1.41	77.79	1587.76	531.12	
				SLE Freq.		6574.36			-103.42			1.28	70.74	1443.97	483.02	0.0341
				SLE Q.P.		6355.95			-99.98			1.24	68.39	1396.00	466.97	0.0330
5827	0.73	14.91	9.42			11820.17	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4647.91			0.00			0.00	51.86	1133.02	336.87	
				SLE Freq.		4227.04			0.00			0.00	47.16	1030.43	306.37	0.0234
				SLE Q.P.		4086.69			0.00			0.00	45.59	996.21	296.20	0.0226
Trave Sez. 2 Rett. 40x40 [cm]																
5827	0.00	14.23	9.42			6626.98	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4485.23			0.00			0.00	50.84	1143.00	322.84	
				SLE Freq.		4078.74			0.00			0.00	46.23	1039.41	293.58	0.0232
				SLE Q.P.		3943.25			0.00			0.00	44.70	1004.88	283.83	0.0225
Camp.	0.37	12.04	9.42	5320.00	183.71	6626.98	13724.80	0.24	-621.81	-11115.81	0.22					
				SLE Rare		1783.93			-124.31			1.60	21.44	532.86	124.41	
				SLE Freq.		1622.13			-113.02			1.46	19.50	484.53	113.13	0.0102
				SLE Q.P.		1568.20			-109.26			1.41	18.85	468.42	109.37	0.0099
5825	0.74	9.86	9.42			2797.92	11540.96	0.22	-621.81	-11110.82	0.22					
				SLE Rare		0.00			-420.99			5.52	0.00	27.07	158.89	
				SLE Freq.		0.00			-382.83			5.02	0.00	24.62	144.49	0.0163
				SLE Q.P.		0.00			-370.25			4.86	0.00	23.81	139.74	0.0157
Trave Sez. 2 Rett. 40x40 [cm]																
5825	0.00	9.42	9.42			0.00	11109.65	0.22	-3574.91	-11109.65	0.22					
				SLE Rare		0.00			-649.32			8.55	0.00	42.17	244.95	

				SLE Freq.		0.00			-590.70			7.78	0.00	38.36	222.84	0.0251
				SLE Q.P.		0.00			-571.30			7.53	0.00	37.10	215.52	0.0242
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5195.64	-11109.65	0.22					
				SLE Rare		0.00			-2319.67			30.56	0.00	150.65	875.08	
				SLE Freq.		0.00			-2109.94			27.79	0.00	137.03	795.96	0.0895
				SLE Q.P.		0.00			-2040.15			26.88	0.00	132.49	769.63	0.0866
5823	0.72	9.42	9.42			0.00	11109.65	0.22	-5195.64	-11109.65	0.22					
				SLE Rare		0.00			-3517.33			46.33	0.00	228.43	1326.89	
				SLE Freq.		0.00			-3199.43			42.15	0.00	207.78	1206.96	0.1358
				SLE Q.P.		0.00			-3093.58			40.75	0.00	200.91	1167.03	0.1313
Trave Sez. 2 Rett. 40x40 [cm]																
5823	0.00	9.42	9.42			0.00	11109.65	0.22	-6552.87	-11109.65	0.22					
				SLE Rare		0.00			-3678.50			48.46	0.00	238.89	1387.69	
				SLE Freq.		0.00			-3346.22			44.08	0.00	217.31	1262.34	0.1420
				SLE Q.P.		0.00			-3235.56			42.62	0.00	210.13	1220.59	0.1373
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6876.54	-11109.65	0.22					
				SLE Rare		0.00			-4412.88			58.13	0.00	286.59	1664.73	
				SLE Freq.		0.00			-4014.53			52.88	0.00	260.72	1514.45	0.1746
				SLE Q.P.		0.00			-3881.82			51.14	0.00	252.10	1464.39	0.1652
5821	0.74	9.42	9.42			0.00	11109.65	0.22	-6876.54	-11109.65	0.22					
				SLE Rare		0.00			-4656.05			61.34	0.00	302.38	1756.46	
				SLE Freq.		0.00			-4236.24			55.81	0.00	275.11	1598.09	0.1903
				SLE Q.P.		0.00			-4096.36			53.96	0.00	266.03	1545.32	0.1804
Trave Sez. 2 Rett. 40x40 [cm]																
5821	0.00	9.42	9.42			0.00	11109.65	0.22	-6872.77	-11109.65	0.22					
				SLE Rare		0.00			-4653.66			61.30	0.00	302.22	1755.56	
				SLE Freq.		0.00			-4234.21			55.78	0.00	274.98	1597.33	0.1902
				SLE Q.P.		0.00			-4094.45			53.94	0.00	265.91	1544.60	0.1803
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6872.77	-11109.65	0.22					
				SLE Rare		0.00			-4405.61			58.04	0.00	286.11	1661.98	
				SLE Freq.		0.00			-4009.32			52.82	0.00	260.38	1512.49	0.1743
				SLE Q.P.		0.00			-3877.26			51.08	0.00	251.80	1462.67	0.1649
5819	0.74	9.42	9.42			0.00	11109.65	0.22	-6540.81	-11109.65	0.22					
				SLE Rare		0.00			-3666.33			48.30	0.00	238.10	1383.10	
				SLE Freq.		0.00			-3337.83			43.97	0.00	216.77	1259.17	0.1416
				SLE Q.P.		0.00			-3228.34			42.53	0.00	209.66	1217.87	0.1370
Trave Sez. 2 Rett. 40x40 [cm]																
5819	0.00	9.42	9.42			0.00	11109.65	0.22	-5167.00	-11109.65	0.22					
				SLE Rare		0.00			-3500.42			46.11	0.00	227.33	1320.51	
				SLE Freq.		0.00			-3186.99			41.98	0.00	206.97	1202.27	0.1352
				SLE Q.P.		0.00			-3082.52			40.61	0.00	200.19	1162.86	0.1308
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5167.00	-11109.65	0.22					
				SLE Rare		0.00			-2297.97			30.27	0.00	149.24	866.89	
				SLE Freq.		0.00			-2094.38			27.59	0.00	136.02	790.09	0.0889
				SLE Q.P.		0.00			-2026.51			26.70	0.00	131.61	764.49	0.0860
5817	0.72	9.42	9.42			0.00	11109.65	0.22	-3538.32	-11109.65	0.22					
				SLE Rare		0.00			-622.84			8.20	0.00	40.45	234.96	
				SLE Freq.		0.00			-572.02			7.54	0.00	37.15	215.79	0.0243
				SLE Q.P.		0.00			-555.06			7.31	0.00	36.05	209.39	0.0236
Trave Sez. 2 Rett. 40x40 [cm]																
5817	0.00	9.86	9.42			2862.28	11540.97	0.22	-570.48	-11110.82	0.22					
				SLE Rare		0.00			-390.86			5.13	0.00	25.14	147.52	
				SLE Freq.		0.00			-360.94			4.74	0.00	23.21	136.23	0.0153
				SLE Q.P.		0.00			-350.93			4.60	0.00	22.57	132.45	0.0149
Camp.	0.37	12.04	9.42	5320.00	183.71	6700.25	13724.81	0.24	-570.48	-11115.81	0.22					

				SLE Rare		1821.52			-124.31			1.60	21.89	544.09	127.03	
				SLE Freq.		1649.03			-113.02			1.46	19.82	492.57	115.01	0.0104
				SLE Q.P.		1591.54			-109.26			1.41	19.13	475.39	111.00	0.0100
5815	0.74	14.23	9.42			6700.25	15895.23	0.26	0.00	-11119.63	0.22					
				SLE Rare		4528.10			0.00			0.00	51.32	1153.92	325.92	
				SLE Freq.		4109.09			0.00			0.00	46.58	1047.14	295.76	0.0234
				SLE Q.P.		3969.41			0.00			0.00	44.99	1011.55	285.71	0.0226
Trave Sez. 2 Rett. 40x40 [cm]																
5815	0.00	14.91	9.42			11907.05	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4693.52			0.00			0.00	52.37	1144.14	340.18	
				SLE Freq.		4260.00			0.00			0.00	47.53	1038.46	308.76	0.0236
				SLE Q.P.		4115.49			0.00			0.00	45.92	1003.23	298.29	0.0228
Camp.	0.30	16.64	9.42	5320.00	178.82	15078.88	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7278.94			-113.76			1.41	78.32	1598.73	534.78	
				SLE Freq.		6610.02			-103.42			1.28	71.12	1451.81	485.64	0.0343
				SLE Q.P.		6387.05			-99.98			1.24	68.73	1402.83	469.26	0.0331
118	0.61	18.71	6.49			15078.88	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10197.37			-17.25			0.25	109.75	2000.40	554.31	
				SLE Freq.		9262.80			-15.68			0.23	99.69	1817.07	503.51	0.0359
				SLE Q.P.		8951.28			-15.16			0.22	96.34	1755.96	486.57	0.0347

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 125 5827 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	14964.76	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5827 5825 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11728.33	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5825 5823 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7773.95	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5823 5821 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3918.52	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5821 5819 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3942.87	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5819 5817 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7798.30	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5817 5815 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11752.67	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5815 118 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14989.09	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 385 Nodi 118 5813 5811 5809 5807 5805 5803 5801 109*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
118	0.13	18.71	6.49			15071.49	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10208.92			-17.25			0.25	109.87	2002.66	554.94	
				SLE Freq.		9291.61			-15.68			0.23	100.00	1822.72	505.07	0.0360
				SLE Q.P.		8985.08			-15.16			0.22	96.70	1762.59	488.41	0.0349
Camp.	0.43	16.64	9.42	5320.00	178.82	15071.49	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7287.65			-113.75			1.41	78.42	1600.64	535.42	
				SLE Freq.		6634.29			-103.42			1.28	71.39	1457.14	487.42	0.0344
				SLE Q.P.		6415.81			-99.98			1.24	69.03	1409.15	471.37	0.0333
5813	0.73	14.91	9.42			11898.51	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4699.41			0.00			0.00	52.43	1145.57	340.61	
				SLE Freq.		4279.73			0.00			0.00	47.75	1043.27	310.19	0.0237
				SLE Q.P.		4139.23			0.00			0.00	46.18	1009.02	300.01	0.0229
Trave Sez. 2 Rett. 40x40 [cm]																

5813	0.00	14.23	9.42			6701.38	15895.24	0.26	0.00	-11119.63	0.22					
				SLE Rare		4542.62			0.00			0.00	51.49	1157.62	326.97	
				SLE Freq.		4137.52			0.00			0.00	46.90	1054.39	297.81	0.0236
				SLE Q.P.		4001.87			0.00			0.00	45.36	1019.82	288.04	0.0228
Camp.	0.37	12.04	9.42	5320.00	183.71	6701.38	13724.81	0.24	-575.48	-11115.81	0.22					
				SLE Rare		1832.57			-124.31			1.60	22.02	547.39	127.81	
				SLE Freq.		1671.92			-113.02			1.46	20.09	499.40	116.60	0.0105
				SLE Q.P.		1617.84			-109.26			1.41	19.44	483.25	112.83	0.0102
5811	0.74	9.86	9.42			2861.51	11540.97	0.22	-575.48	-11110.82	0.22					
				SLE Rare		0.00			-384.73			5.05	0.00	24.74	145.21	
				SLE Freq.		0.00			-345.48			4.53	0.00	22.22	130.39	0.0147
				SLE Q.P.		0.00			-332.39			4.36	0.00	21.38	125.45	0.0141
Trave Sez. 2 Rett. 40x40 [cm]																
5811	0.00	9.42	9.42			0.00	11109.65	0.22	-3532.58	-11109.65	0.22					
				SLE Rare		0.00			-609.30			8.03	0.00	39.57	229.85	
				SLE Freq.		0.00			-549.51			7.24	0.00	35.69	207.30	0.0233
				SLE Q.P.		0.00			-529.59			6.98	0.00	34.39	199.78	0.0225
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5161.17	-11109.65	0.22					
				SLE Rare		0.00			-2286.46			30.12	0.00	148.49	862.55	
				SLE Freq.		0.00			-2076.19			27.35	0.00	134.83	783.23	0.0881
				SLE Q.P.		0.00			-2006.10			26.43	0.00	130.28	756.79	0.0851
5809	0.72	9.42	9.42			0.00	11109.65	0.22	-5161.17	-11109.65	0.22					
				SLE Rare		0.00			-3490.95			45.99	0.00	226.71	1316.94	
				SLE Freq.		0.00			-3173.13			41.80	0.00	206.07	1197.04	0.1346
				SLE Q.P.		0.00			-3067.19			40.40	0.00	199.19	1157.07	0.1301
Trave Sez. 2 Rett. 40x40 [cm]																
5809	0.00	9.42	9.42			0.00	11109.65	0.22	-6523.73	-11109.65	0.22					
				SLE Rare		0.00			-3649.38			48.07	0.00	237.00	1376.70	
				SLE Freq.		0.00			-3317.12			43.70	0.00	215.42	1251.36	0.1407
				SLE Q.P.		0.00			-3206.37			42.24	0.00	208.23	1209.58	0.1360
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6857.80	-11109.65	0.22					
				SLE Rare		0.00			-4390.72			57.84	0.00	285.15	1656.37	
				SLE Freq.		0.00			-3993.02			52.60	0.00	259.32	1506.34	0.1731
				SLE Q.P.		0.00			-3860.46			50.85	0.00	250.71	1456.33	0.1638
5807	0.74	9.42	9.42			0.00	11109.65	0.22	-6857.80	-11109.65	0.22					
				SLE Rare		0.00			-4642.32			61.15	0.00	301.49	1751.28	
				SLE Freq.		0.00			-4223.24			55.63	0.00	274.27	1593.19	0.1894
				SLE Q.P.		0.00			-4083.57			53.79	0.00	265.20	1540.50	0.1795
Trave Sez. 2 Rett. 40x40 [cm]																
5807	0.00	9.42	9.42			0.00	11109.65	0.22	-6851.55	-11109.65	0.22					
				SLE Rare		0.00			-4638.13			61.10	0.00	301.21	1749.70	
				SLE Freq.		0.00			-4219.40			55.58	0.00	274.02	1591.74	0.1891
				SLE Q.P.		0.00			-4079.82			53.74	0.00	264.96	1539.08	0.1792
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6851.55	-11109.65	0.22					
				SLE Rare		0.00			-4398.58			57.94	0.00	285.66	1659.33	
				SLE Freq.		0.00			-4003.32			52.74	0.00	259.99	1510.22	0.1738
				SLE Q.P.		0.00			-3871.47			51.00	0.00	251.43	1460.48	0.1645
5805	0.74	9.42	9.42			0.00	11109.65	0.22	-6529.99	-11109.65	0.22					
				SLE Rare		0.00			-3667.82			48.32	0.00	238.20	1383.66	
				SLE Freq.		0.00			-3340.64			44.01	0.00	216.95	1260.23	0.1417
				SLE Q.P.		0.00			-3231.39			42.57	0.00	209.86	1219.02	0.1371
Trave Sez. 2 Rett. 40x40 [cm]																
5805	0.00	9.42	9.42			0.00	11109.65	0.22	-5165.49	-11109.65	0.22					
				SLE Rare		0.00			-3500.30			46.11	0.00	227.32	1320.46	
				SLE Freq.		0.00			-3188.14			42.00	0.00	207.05	1202.70	0.1353

				SLE Q.P.		0.00			-3083.87			40.62	0.00	200.28	1163.37	0.1309
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5165.49	-11109.65	0.22					
				SLE Rare		0.00			-2306.19			30.38	0.00	149.77	869.99	
				SLE Freq.		0.00			-2104.16			27.72	0.00	136.65	793.78	0.0893
				SLE Q.P.		0.00			-2036.52			26.83	0.00	132.26	768.26	0.0864
5803	0.72	9.42	9.42			0.00	11109.65	0.22	-3546.78	-11109.65	0.22					
				SLE Rare		0.00			-639.40			8.42	0.00	41.52	241.21	
				SLE Freq.		0.00			-590.45			7.78	0.00	38.35	222.74	0.0251
				SLE Q.P.		0.00			-573.74			7.56	0.00	37.26	216.44	0.0243
Trave Sez. 2 Rett. 40x40 [cm]																
5803	0.00	9.86	9.42			2841.43	11540.96	0.22	-588.06	-11110.82	0.22					
				SLE Rare		0.00			-405.62			5.32	0.00	26.08	153.09	
				SLE Freq.		0.00			-377.45			4.95	0.00	24.27	142.46	0.0160
				SLE Q.P.		0.00			-367.65			4.82	0.00	23.64	138.76	0.0156
Camp.	0.37	12.04	9.42	5320.00	183.71	6670.83	13724.80	0.24	-588.06	-11115.81	0.22					
				SLE Rare		1803.63			-124.31			1.60	21.68	538.75	125.79	
				SLE Freq.		1628.30			-113.02			1.46	19.57	486.37	113.56	0.0102
				SLE Q.P.		1569.86			-109.26			1.41	18.87	468.92	109.48	0.0099
5801	0.74	14.23	9.42			6670.83	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4503.03			0.00			0.00	51.04	1147.53	324.12	
				SLE Freq.		4080.60			0.00			0.00	46.25	1039.88	293.71	0.0232
				SLE Q.P.		3939.79			0.00			0.00	44.66	1004.00	283.58	0.0224
Trave Sez. 2 Rett. 40x40 [cm]																
5801	0.00	14.91	9.42			11871.20	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4670.79			0.00			0.00	52.11	1138.60	338.53	
				SLE Freq.		4234.19			0.00			0.00	47.24	1032.17	306.89	0.0234
				SLE Q.P.		4088.66			0.00			0.00	45.62	996.69	296.34	0.0226
Camp.	0.30	16.64	9.42	5320.00	178.82	15037.76	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7250.34			-113.76			1.41	78.01	1592.45	532.68	
				SLE Freq.		6577.88			-103.42			1.28	70.78	1444.75	483.28	0.0341
				SLE Q.P.		6353.72			-99.98			1.24	68.37	1395.51	466.81	0.0330
109	0.61	18.71	6.49			15037.76	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10162.91			-17.25			0.25	109.38	1993.64	552.44	
				SLE Freq.		9224.33			-15.68			0.23	99.28	1809.52	501.42	0.0358
				SLE Q.P.		8911.47			-15.16			0.22	95.91	1748.15	484.41	0.0346

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 118 5813 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	14994.39	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5813 5811 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11757.98	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5811 5809 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7803.60	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5809 5807 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3948.17	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5807 5805 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3918.76	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5805 5803 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7774.20	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5803 5801 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11728.57	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 5801 109 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14965.00	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 386 Nodi 209 8816 8818 8820 8822 8824 8826 8828 219*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
209	0.13	18.71	6.49			14943.98	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10105.47			-17.25			0.25	108.76	1982.37	549.31	
				SLE Freq.		9174.44			-15.68			0.23	98.74	1799.73	498.70	0.0356
				SLE Q.P.		8864.09			-15.16			0.22	95.40	1738.85	481.83	0.0344
Camp.	0.43	16.64	9.42	5320.00	178.82	14943.98	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7193.54			-113.76			1.41	77.40	1579.97	528.51	
				SLE Freq.		6528.03			-103.42			1.28	70.24	1433.80	479.61	0.0339
				SLE Q.P.		6306.20			-99.98			1.24	67.86	1385.08	463.32	0.0327
8816	0.73	14.91	9.42			11778.74	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4614.64			0.00			0.00	51.49	1124.91	334.46	
				SLE Freq.		4184.40			0.00			0.00	46.68	1020.03	303.28	0.0232
				SLE Q.P.		4040.99			0.00			0.00	45.08	985.07	292.89	0.0224
Trave Sez. 2 Rett. 40x40 [cm]																
8816	0.00	14.23	9.42			6572.77	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4441.71			0.00			0.00	50.35	1131.91	319.70	
				SLE Freq.		4025.90			0.00			0.00	45.63	1025.94	289.77	0.0229
				SLE Q.P.		3887.30			0.00			0.00	44.06	990.62	279.80	0.0221
Camp.	0.37	12.04	9.42	5320.00	183.71	6572.77	13724.80	0.24	-678.86	-11115.81	0.22					
				SLE Rare		1743.11			-124.31			1.60	20.95	520.67	121.57	
				SLE Freq.		1573.67			-113.02			1.46	18.91	470.06	109.75	0.0099
				SLE Q.P.		1517.19			-109.26			1.41	18.23	453.19	105.81	0.0095
8818	0.74	9.86	9.42			2745.50	11540.96	0.22	-678.86	-11110.82	0.22					
				SLE Rare		0.00			-463.50			6.08	0.00	29.81	174.94	
				SLE Freq.		0.00			-428.94			5.63	0.00	27.58	161.89	0.0182
				SLE Q.P.		0.00			-417.93			5.48	0.00	26.88	157.74	0.0177
Trave Sez. 2 Rett. 40x40 [cm]																
8818	0.00	9.42	9.42			0.00	11109.65	0.22	-3640.20	-11109.65	0.22					
				SLE Rare		0.00			-699.82			9.22	0.00	45.45	264.00	
				SLE Freq.		0.00			-644.38			8.49	0.00	41.85	243.09	0.0273
				SLE Q.P.		0.00			-626.46			8.25	0.00	40.68	236.33	0.0266
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5257.86	-11109.65	0.22					
				SLE Rare		0.00			-2366.55			31.18	0.00	153.69	892.76	
				SLE Freq.		0.00			-2158.65			28.44	0.00	140.19	814.33	0.0916
				SLE Q.P.		0.00			-2089.93			27.53	0.00	135.73	788.41	0.0887
8820	0.72	9.42	9.42			0.00	11109.65	0.22	-5257.86	-11109.65	0.22					
				SLE Rare		0.00			-3560.60			46.90	0.00	231.24	1343.21	
				SLE Freq.		0.00			-3243.17			42.72	0.00	210.62	1223.46	0.1376
				SLE Q.P.		0.00			-3137.97			41.34	0.00	203.79	1183.78	0.1331
Trave Sez. 2 Rett. 40x40 [cm]																
8820	0.00	9.42	9.42			0.00	11109.65	0.22	-6621.60	-11109.65	0.22					
				SLE Rare		0.00			-3728.49			49.12	0.00	242.14	1406.55	
				SLE Freq.		0.00			-3396.16			44.74	0.00	220.56	1281.18	0.1441
				SLE Q.P.		0.00			-3286.02			43.29	0.00	213.40	1239.63	0.1394
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6942.08	-11109.65	0.22					
				SLE Rare		0.00			-4459.19			58.74	0.00	289.59	1682.20	
				SLE Freq.		0.00			-4059.40			53.48	0.00	263.63	1531.38	0.1778
				SLE Q.P.		0.00			-3926.80			51.73	0.00	255.02	1481.36	0.1684
8822	0.74	9.42	9.42			0.00	11109.65	0.22	-6942.08	-11109.65	0.22					
				SLE Rare		0.00			-4698.68			61.90	0.00	305.15	1772.54	
				SLE Freq.		0.00			-4276.04			56.33	0.00	277.70	1613.11	0.1931
				SLE Q.P.		0.00			-4135.85			54.48	0.00	268.59	1560.22	0.1832

Trave Sez. 2 Rett. 40x40 [cm]																
8822	0.00	9.42	9.42			0.00	11109.65	0.22	-6945.30	-11109.65	0.22					
				SLE Rare		0.00			-4700.95			61.93	0.00	305.29	1773.40	
				SLE Freq.		0.00			-4278.24			56.36	0.00	277.84	1613.94	0.1933
				SLE Q.P.		0.00			-4138.03			54.51	0.00	268.74	1561.04	0.1834
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6945.30	-11109.65	0.22					
				SLE Rare		0.00			-4449.21			58.61	0.00	288.95	1678.43	
				SLE Freq.		0.00			-4048.48			53.33	0.00	262.92	1527.26	0.1770
				SLE Q.P.		0.00			-3915.51			51.58	0.00	254.29	1477.10	0.1676
8824	0.74	9.42	9.42			0.00	11109.65	0.22	-6610.15	-11109.65	0.22					
				SLE Rare		0.00			-3706.25			48.82	0.00	240.70	1398.16	
				SLE Freq.		0.00			-3372.52			44.43	0.00	219.02	1272.26	0.1431
				SLE Q.P.		0.00			-3261.60			42.97	0.00	211.82	1230.42	0.1384
Trave Sez. 2 Rett. 40x40 [cm]																
8824	0.00	9.42	9.42			0.00	11109.65	0.22	-5237.41	-11109.65	0.22					
				SLE Rare		0.00			-3543.53			46.68	0.00	230.13	1336.77	
				SLE Freq.		0.00			-3224.53			42.48	0.00	209.41	1216.43	0.1368
				SLE Q.P.		0.00			-3118.53			41.08	0.00	202.53	1176.44	0.1323
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5237.41	-11109.65	0.22					
				SLE Rare		0.00			-2337.46			30.79	0.00	151.80	881.79	
				SLE Freq.		0.00			-2127.53			28.03	0.00	138.17	802.59	0.0903
				SLE Q.P.		0.00			-2057.61			27.11	0.00	133.63	776.22	0.0873
8826	0.72	9.42	9.42			0.00	11109.65	0.22	-3605.67	-11109.65	0.22					
				SLE Rare		0.00			-659.33			8.69	0.00	42.82	248.73	
				SLE Freq.		0.00			-600.79			7.91	0.00	39.02	226.64	0.0255
				SLE Q.P.		0.00			-581.27			7.66	0.00	37.75	219.28	0.0247
Trave Sez. 2 Rett. 40x40 [cm]																
8826	0.00	9.86	9.42			2795.28	11540.97	0.22	-637.08	-11110.82	0.22					
				SLE Rare		0.00			-428.89			5.63	0.00	27.58	161.88	
				SLE Freq.		0.00			-391.14			5.13	0.00	25.15	147.63	0.0166
				SLE Q.P.		0.00			-378.56			4.97	0.00	24.34	142.88	0.0161
Camp.	0.37	12.04	9.42	5320.00	183.71	6636.24	13724.81	0.24	-637.08	-11115.81	0.22					
				SLE Rare		1784.59			-124.31			1.60	21.45	533.06	124.46	
				SLE Freq.		1623.61			-113.02			1.46	19.51	484.97	113.23	0.0102
				SLE Q.P.		1569.22			-109.26			1.41	18.86	468.73	109.44	0.0099
8828	0.74	14.23	9.42			6636.24	15895.24	0.26	0.00	-11119.63	0.22					
				SLE Rare		4494.71			0.00			0.00	50.95	1145.41	323.52	
				SLE Freq.		4088.65			0.00			0.00	46.34	1041.93	294.29	0.0233
				SLE Q.P.		3952.54			0.00			0.00	44.80	1007.24	284.49	0.0225
Trave Sez. 2 Rett. 40x40 [cm]																
8828	0.00	14.91	9.42			11847.00	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4659.96			0.00			0.00	51.99	1135.95	337.75	
				SLE Freq.		4238.88			0.00			0.00	47.29	1033.31	307.23	0.0235
				SLE Q.P.		4097.84			0.00			0.00	45.72	998.93	297.01	0.0227
Camp.	0.30	16.64	9.42	5320.00	178.82	15020.66	18263.85	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7248.26			-113.75			1.41	77.99	1591.99	532.53	
				SLE Freq.		6592.97			-103.42			1.28	70.94	1448.06	484.38	0.0342
				SLE Q.P.		6373.84			-99.98			1.24	68.58	1399.93	468.29	0.0331
219	0.61	18.71	6.49			15020.66	20249.27	0.32	-25.49	-8214.46	0.21					
				SLE Rare		10169.58			-17.25			0.25	109.45	1994.95	552.80	
				SLE Freq.		9249.82			-15.68			0.23	99.55	1814.52	502.80	0.0359
				SLE Q.P.		8942.53			-15.16			0.22	96.24	1754.24	486.10	0.0347

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	Staffe
Trave 209 8816 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	14958.99	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8816 8818 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11722.56	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8818 8820 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7768.19	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8820 8822 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3912.75	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8822 8824 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3951.25	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8824 8826 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7806.68	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8826 8828 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11761.06	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8828 219 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14997.48	7069.46	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 387 Nodi 219 8830 8832 8834 8836 8844 8846 8848 225*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
219	0.13	18.71	6.49			15079.63	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10204.81			-17.25			0.25	109.83	2001.86	554.71	
				SLE Freq.		9281.46			-15.68			0.23	99.89	1820.73	504.52	0.0360
				SLE Q.P.		8974.27			-15.16			0.22	96.58	1760.47	487.82	0.0348
Camp.	0.43	16.64	9.42	5320.00	178.82	15079.63	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7294.16			-113.76			1.41	78.49	1602.07	535.90	
				SLE Freq.		6634.97			-103.42			1.28	71.39	1457.29	487.47	0.0344
				SLE Q.P.		6415.85			-99.98			1.24	69.04	1409.16	471.37	0.0333
8830	0.73	14.91	9.42			11916.80	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4716.52			0.00			0.00	52.62	1149.74	341.85	
				SLE Freq.		4291.25			0.00			0.00	47.88	1046.08	311.02	0.0238
				SLE Q.P.		4150.11			0.00			0.00	46.30	1011.67	300.80	0.0230
Trave Sez. 2 Rett. 40x40 [cm]																
8830	0.00	14.23	9.42			6728.45	15895.23	0.26	0.00	-11119.63	0.22					
				SLE Rare		4553.18			0.00			0.00	51.61	1160.31	327.73	
				SLE Freq.		4142.70			0.00			0.00	46.96	1055.71	298.18	0.0236
				SLE Q.P.		4006.49			0.00			0.00	45.41	1020.99	288.38	0.0228
Camp.	0.37	12.04	9.42	5320.00	183.71	6728.45	13724.81	0.24	-510.51	-11115.81	0.22					
				SLE Rare		1856.10			-124.31			1.60	22.31	554.42	129.45	
				SLE Freq.		1690.34			-113.02			1.46	20.31	504.91	117.89	0.0106
				SLE Q.P.		1635.72			-109.26			1.41	19.66	488.59	114.08	0.0103
8832	0.74	9.86	9.42			2905.00	11540.97	0.22	-510.51	-11110.82	0.22					
				SLE Rare		0.00			-345.85			4.54	0.00	22.24	130.53	
				SLE Freq.		0.00			-310.07			4.07	0.00	19.94	117.03	0.0132
				SLE Q.P.		0.00			-298.15			3.91	0.00	19.17	112.53	0.0127
Trave Sez. 2 Rett. 40x40 [cm]																
8832	0.00	9.42	9.42			0.00	11109.65	0.22	-3461.36	-11109.65	0.22					
				SLE Rare		0.00			-577.08			7.60	0.00	37.48	217.70	
				SLE Freq.		0.00			-520.51			6.86	0.00	33.80	196.36	0.0221
				SLE Q.P.		0.00			-501.66			6.61	0.00	32.58	189.25	0.0213
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5076.13	-11109.65	0.22					
				SLE Rare		0.00			-2242.83			29.55	0.00	145.66	846.09	
				SLE Freq.		0.00			-2035.34			26.81	0.00	132.18	767.82	0.0864
				SLE Q.P.		0.00			-1966.11			25.90	0.00	127.69	741.70	0.0834

8834	0.72	9.42	9.42			0.00	11109.65	0.22	-5076.13	-11109.65	0.22					
				SLE Rare		0.00			-3435.91			45.26	0.00	223.14	1296.17	
				SLE Freq.		0.00			-3120.57			41.11	0.00	202.66	1177.21	0.1324
				SLE Q.P.		0.00			-3015.28			39.72	0.00	195.82	1137.49	0.1279
Trave Sez. 2 Rett. 40x40 [cm]																
8834	0.00	9.42	9.42			0.00	11109.65	0.22	-6435.87	-11109.65	0.22					
				SLE Rare		0.00			-3603.18			47.47	0.00	234.00	1359.27	
				SLE Freq.		0.00			-3273.02			43.12	0.00	212.56	1234.72	0.1389
				SLE Q.P.		0.00			-3162.79			41.66	0.00	205.40	1193.14	0.1342
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6753.34	-11109.65	0.22					
				SLE Rare		0.00			-4332.90			57.08	0.00	281.39	1634.55	
				SLE Freq.		0.00			-3936.98			51.86	0.00	255.68	1485.20	0.1691
				SLE Q.P.		0.00			-3804.72			50.12	0.00	247.09	1435.30	0.1614
8836	0.74	9.42	9.42			0.00	11109.65	0.22	-6753.34	-11109.65	0.22					
				SLE Rare		0.00			-4571.39			60.22	0.00	296.88	1724.52	
				SLE Freq.		0.00			-4154.35			54.73	0.00	269.80	1567.20	0.1845
				SLE Q.P.		0.00			-4014.93			52.89	0.00	260.74	1514.60	0.1747
Trave Sez. 2 Rett. 40x40 [cm]																
8836	0.00	9.42	9.42			0.00	11109.65	0.22	-6762.88	-11109.65	0.22					
				SLE Rare		0.00			-4577.81			60.30	0.00	297.30	1726.94	
				SLE Freq.		0.00			-4160.62			54.81	0.00	270.20	1569.56	0.1850
				SLE Q.P.		0.00			-4021.17			52.97	0.00	261.15	1516.96	0.1751
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6762.88	-11109.65	0.22					
				SLE Rare		0.00			-4325.08			56.98	0.00	280.88	1631.60	
				SLE Freq.		0.00			-3931.38			51.79	0.00	255.32	1483.09	0.1687
				SLE Q.P.		0.00			-3799.64			50.05	0.00	246.76	1433.39	0.1612
8844	0.74	9.42	9.42			0.00	11109.65	0.22	-6424.71	-11109.65	0.22					
				SLE Rare		0.00			-3581.15			47.18	0.00	232.57	1350.96	
				SLE Freq.		0.00			-3255.55			42.89	0.00	211.43	1228.13	0.1381
				SLE Q.P.		0.00			-3146.39			41.45	0.00	204.34	1186.95	0.1335
Trave Sez. 2 Rett. 40x40 [cm]																
8844	0.00	9.42	9.42			0.00	11109.65	0.22	-5062.91	-11109.65	0.22					
				SLE Rare		0.00			-3427.86			45.16	0.00	222.62	1293.14	
				SLE Freq.		0.00			-3116.50			41.05	0.00	202.39	1175.68	0.1322
				SLE Q.P.		0.00			-3012.19			39.68	0.00	195.62	1136.33	0.1278
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5062.91	-11109.65	0.22					
				SLE Rare		0.00			-2221.11			29.26	0.00	144.25	837.90	
				SLE Freq.		0.00			-2019.62			26.60	0.00	131.16	761.89	0.0857
				SLE Q.P.		0.00			-1951.92			25.71	0.00	126.76	736.35	0.0828
8846	0.72	9.42	9.42			0.00	11109.65	0.22	-3428.67	-11109.65	0.22					
				SLE Rare		0.00			-541.67			7.14	0.00	35.18	204.34	
				SLE Freq.		0.00			-493.00			6.49	0.00	32.02	185.98	0.0209
				SLE Q.P.		0.00			-476.21			6.27	0.00	30.93	179.65	0.0202
Trave Sez. 2 Rett. 40x40 [cm]																
8846	0.00	9.86	9.42			2960.16	11540.95	0.22	-476.04	-11110.82	0.22					
				SLE Rare		0.00			-324.28			4.26	0.00	20.85	122.39	
				SLE Freq.		0.00			-295.64			3.88	0.00	19.01	111.58	0.0126
				SLE Q.P.		0.00			-285.64			3.75	0.00	18.37	107.81	0.0121
Camp.	0.37	12.04	9.42	5320.00	183.71	6804.16	13724.79	0.24	-476.04	-11115.81	0.22					
				SLE Rare		1890.52			-124.31			1.60	22.72	564.70	131.85	
				SLE Freq.		1718.38			-113.02			1.46	20.65	513.28	119.84	0.0108
				SLE Q.P.		1661.00			-109.26			1.41	19.96	496.14	115.84	0.0104
8848	0.74	14.23	9.42			6804.16	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4601.63			0.00			0.00	52.16	1172.66	331.21	
				SLE Freq.		4182.93			0.00			0.00	47.41	1065.96	301.08	0.0238

				SLE Q.P.		4043.37			0.00			0.00	45.83	1030.39	291.03	0.0230
Trave Sez. 2 Rett. 40x40 [cm]																
8848	0.00	14.91	9.42			11990.38	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4748.58			0.00			0.00	52.98	1157.56	344.17	
				SLE Freq.		4315.95			0.00			0.00	48.15	1052.10	312.82	0.0239
				SLE Q.P.		4171.74			0.00			0.00	46.54	1016.95	302.36	0.0231
Camp.	0.30	16.64	9.42	5320.00	178.82	15165.99	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7337.72			-113.76			1.41	78.95	1611.64	539.10	
				SLE Freq.		6669.67			-103.42			1.28	71.77	1464.91	490.02	0.0346
				SLE Q.P.		6446.98			-99.98			1.24	69.37	1416.00	473.66	0.0334
225	0.61	18.71	6.49			15165.99	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10259.87			-17.25			0.25	110.42	2012.66	557.71	
				SLE Freq.		9326.15			-15.68			0.23	100.37	1829.49	506.95	0.0362
				SLE Q.P.		9014.91			-15.16			0.22	97.02	1768.44	490.03	0.0350

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 219 8830 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	14948.22	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8830 8832 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11711.80	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8832 8834 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7757.43	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8834 8836 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3902.00	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8836 8844 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3959.85	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8844 8846 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7815.28	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8846 8848 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11769.65	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8848 225 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	15006.09	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 388 Nodi 225 8847 8845 8843 8835 8833 8831 8829 218*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
225	0.12	18.71	6.49			15052.30	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10183.13			-17.25			0.25	109.59	1997.61	553.53	
				SLE Freq.		9256.47			-15.68			0.23	99.62	1815.82	503.16	0.0359
				SLE Q.P.		8947.58			-15.16			0.22	96.30	1755.23	486.37	0.0347
Camp.	0.43	16.64	9.42	5320.00	178.82	15052.30	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7269.11			-113.76			1.41	78.22	1596.57	534.06	
				SLE Freq.		6607.37			-103.42			1.28	71.10	1451.23	485.44	0.0343
				SLE Q.P.		6386.79			-99.98			1.24	68.72	1402.78	469.24	0.0331
8847	0.73	14.91	9.42			11885.40	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4688.10			0.00			0.00	52.30	1142.82	339.79	
				SLE Freq.		4261.04			0.00			0.00	47.54	1038.71	308.84	0.0236
				SLE Q.P.		4118.69			0.00			0.00	45.95	1004.01	298.52	0.0228
Trave Sez. 2 Rett. 40x40 [cm]																
8847	0.00	14.23	9.42			6693.76	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4527.08			0.00			0.00	51.31	1153.66	325.85	
				SLE Freq.		4114.48			0.00			0.00	46.64	1048.52	296.15	0.0234
				SLE Q.P.		3976.95			0.00			0.00	45.08	1013.47	286.25	0.0226
Camp.	0.37	12.04	9.42	5320.00	183.71	6693.76	13724.80	0.24	-557.71	-11115.81	0.22					
				SLE Rare		1825.91			-124.31			1.60	21.94	545.40	127.34	

				SLE Freq.		1658.95			-113.02			1.46	19.94	495.53	115.70	0.0104
				SLE Q.P.		1603.30			-109.26			1.41	19.27	478.91	111.82	0.0101
8845	0.74	9.86	9.42			2863.82	11540.96	0.22	-557.71	-11110.82	0.22					
				SLE Rare		0.00			-379.43			4.98	0.00	24.40	143.21	
				SLE Freq.		0.00			-346.06			4.54	0.00	22.25	130.61	0.0147
				SLE Q.P.		0.00			-334.66			4.39	0.00	21.52	126.31	0.0142
Trave Sez. 2 Rett. 40x40 [cm]																
8845	0.00	9.42	9.42			0.00	11109.65	0.22	-3510.83	-11109.65	0.22					
				SLE Rare		0.00			-607.63			8.00	0.00	39.46	229.22	
				SLE Freq.		0.00			-553.66			7.29	0.00	35.96	208.86	0.0235
				SLE Q.P.		0.00			-535.37			7.05	0.00	34.77	201.96	0.0227
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5131.64	-11109.65	0.22					
				SLE Rare		0.00			-2277.30			30.00	0.00	147.89	859.09	
				SLE Freq.		0.00			-2071.43			27.29	0.00	134.53	781.43	0.0879
				SLE Q.P.		0.00			-2002.52			26.38	0.00	130.05	755.44	0.0850
8843	0.72	9.42	9.42			0.00	11109.65	0.22	-5131.64	-11109.65	0.22					
				SLE Rare		0.00			-3474.29			45.77	0.00	225.63	1310.65	
				SLE Freq.		0.00			-3159.46			41.62	0.00	205.18	1191.88	0.1341
				SLE Q.P.		0.00			-3054.24			40.23	0.00	198.35	1152.19	0.1296
Trave Sez. 2 Rett. 40x40 [cm]																
8843	0.00	9.42	9.42			0.00	11109.65	0.22	-6491.37	-11109.65	0.22					
				SLE Rare		0.00			-3636.97			47.91	0.00	236.20	1372.02	
				SLE Freq.		0.00			-3307.45			43.57	0.00	214.80	1247.71	0.1403
				SLE Q.P.		0.00			-3197.33			42.12	0.00	207.64	1206.17	0.1357
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6815.13	-11109.65	0.22					
				SLE Rare		0.00			-4370.67			57.58	0.00	283.84	1648.80	
				SLE Freq.		0.00			-3974.27			52.35	0.00	258.10	1499.26	0.1718
				SLE Q.P.		0.00			-3841.87			50.61	0.00	249.50	1449.32	0.1630
8835	0.74	9.42	9.42			0.00	11109.65	0.22	-6815.13	-11109.65	0.22					
				SLE Rare		0.00			-4613.15			60.77	0.00	299.59	1740.28	
				SLE Freq.		0.00			-4194.49			55.26	0.00	272.40	1582.34	0.1874
				SLE Q.P.		0.00			-4054.68			53.41	0.00	263.32	1529.60	0.1775
Trave Sez. 2 Rett. 40x40 [cm]																
8835	0.00	9.42	9.42			0.00	11109.65	0.22	-6815.98	-11109.65	0.22					
				SLE Rare		0.00			-4613.77			60.78	0.00	299.63	1740.51	
				SLE Freq.		0.00			-4195.13			55.26	0.00	272.44	1582.58	0.1874
				SLE Q.P.		0.00			-4055.32			53.42	0.00	263.36	1529.84	0.1775
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6815.98	-11109.65	0.22					
				SLE Rare		0.00			-4365.20			57.50	0.00	283.49	1646.74	
				SLE Freq.		0.00			-3968.74			52.28	0.00	257.74	1497.18	0.1714
				SLE Q.P.		0.00			-3836.40			50.54	0.00	249.15	1447.25	0.1628
8833	0.74	9.42	9.42			0.00	11109.65	0.22	-6484.32	-11109.65	0.22					
				SLE Rare		0.00			-3625.62			47.76	0.00	235.46	1367.74	
				SLE Freq.		0.00			-3295.75			43.42	0.00	214.04	1243.30	0.1398
				SLE Q.P.		0.00			-3185.75			41.97	0.00	206.89	1201.80	0.1352
Trave Sez. 2 Rett. 40x40 [cm]																
8833	0.00	9.42	9.42			0.00	11109.65	0.22	-5118.15	-11109.65	0.22					
				SLE Rare		0.00			-3464.40			45.64	0.00	224.99	1306.92	
				SLE Freq.		0.00			-3149.32			41.49	0.00	204.53	1188.06	0.1336
				SLE Q.P.		0.00			-3044.22			40.10	0.00	197.70	1148.41	0.1292
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5118.15	-11109.65	0.22					
				SLE Rare		0.00			-2261.64			29.79	0.00	146.88	853.19	
				SLE Freq.		0.00			-2055.42			27.08	0.00	133.49	775.39	0.0872
				SLE Q.P.		0.00			-1986.68			26.17	0.00	129.02	749.46	0.0843
8831	0.72	9.42	9.42			0.00	11109.65	0.22	-3490.06	-11109.65	0.22					

				SLE Rare		0.00			-586.21			7.72	0.00	38.07	221.14	
				SLE Freq.		0.00			-531.89			7.01	0.00	34.54	200.65	0.0226
				SLE Q.P.		0.00			-513.79			6.77	0.00	33.37	193.82	0.0218
Trave Sez. 2 Rett. 40x40 [cm]																
8831	0.00	9.86	9.42			2898.28	11540.97	0.22	-531.16	-11110.82	0.22					
				SLE Rare		0.00			-359.94			4.72	0.00	23.15	135.85	
				SLE Freq.		0.00			-326.30			4.28	0.00	20.98	123.15	0.0139
				SLE Q.P.		0.00			-315.08			4.13	0.00	20.26	118.92	0.0134
Camp.	0.37	12.04	9.42	5320.00	183.71	6735.91	13724.81	0.24	-531.16	-11115.81	0.22					
				SLE Rare		1851.00			-124.31			1.60	22.25	552.89	129.09	
				SLE Freq.		1683.49			-113.02			1.46	20.23	502.86	117.41	0.0106
				SLE Q.P.		1627.82			-109.26			1.41	19.56	486.23	113.53	0.0102
8829	0.74	14.23	9.42			6735.91	15895.23	0.26	0.00	-11119.63	0.22					
				SLE Rare		4558.09			0.00			0.00	51.66	1161.56	328.08	
				SLE Freq.		4144.93			0.00			0.00	46.98	1056.27	298.34	0.0236
				SLE Q.P.		4007.36			0.00			0.00	45.42	1021.22	288.44	0.0228
Trave Sez. 2 Rett. 40x40 [cm]																
8829	0.00	14.91	9.42			11931.77	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4716.03			0.00			0.00	52.62	1149.62	341.81	
				SLE Freq.		4288.42			0.00			0.00	47.85	1045.39	310.82	0.0237
				SLE Q.P.		4146.02			0.00			0.00	46.26	1010.67	300.50	0.0230
Camp.	0.30	16.64	9.42	5320.00	178.82	15103.39	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7301.86			-113.76			1.41	78.57	1603.76	536.47	
				SLE Freq.		6639.57			-103.42			1.28	71.44	1458.30	487.81	0.0344
				SLE Q.P.		6418.93			-99.98			1.24	69.07	1409.84	471.60	0.0333
218	0.61	18.71	6.49			15103.39	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10220.71			-17.25			0.25	110.00	2004.98	555.58	
				SLE Freq.		9293.49			-15.68			0.23	100.02	1823.09	505.18	0.0360
				SLE Q.P.		8984.53			-15.16			0.22	96.70	1762.48	488.38	0.0349

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 225 8847 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	14966.52	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8847 8845 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11730.09	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8845 8843 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7775.72	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8843 8835 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3920.28	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8835 8833 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3941.90	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8833 8831 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7797.33	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8831 8829 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11751.71	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8829 218 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14988.12	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 389 Nodi 218 8827 8825 8823 8821 8819 8817 8815 209*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
218	0.13	18.71	6.49			15207.15	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10296.50			-17.25			0.25	110.82	2019.85	559.70	
				SLE Freq.		9369.27			-15.68			0.23	100.84	1837.95	509.29	0.0363
				SLE Q.P.		9060.21			-15.16			0.22	97.51	1777.33	492.50	0.0351

Camp.	0.43	16.64	9.42	5320.00	178.82	15207.15	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7368.14			-113.75			1.41	79.28	1618.32	541.34	
				SLE Freq.		6705.91			-103.42			1.28	72.16	1472.87	492.68	0.0348
				SLE Q.P.		6485.20			-99.98			1.24	69.78	1424.39	476.47	0.0336
8827	0.73	14.91	9.42			12026.05	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4772.80			0.00			0.00	53.25	1163.46	345.93	
				SLE Freq.		4345.31			0.00			0.00	48.48	1059.25	314.94	0.0241
				SLE Q.P.		4202.88			0.00			0.00	46.89	1024.53	304.62	0.0233
Trave Sez. 2 Rett. 40x40 [cm]																
8827	0.00	14.23	9.42			6836.29	15895.24	0.26	0.00	-11119.63	0.22					
				SLE Rare		4630.63			0.00			0.00	52.49	1180.05	333.30	
				SLE Freq.		4217.02			0.00			0.00	47.80	1074.64	303.53	0.0240
				SLE Q.P.		4079.34			0.00			0.00	46.24	1039.56	293.62	0.0232
Camp.	0.37	12.04	9.42	5320.00	183.71	6836.29	13724.81	0.24	-467.17	-11115.81	0.22					
				SLE Rare		1911.91			-124.31			1.60	22.98	571.09	133.34	
				SLE Freq.		1744.04			-113.02			1.46	20.96	520.94	121.63	0.0110
				SLE Q.P.		1688.29			-109.26			1.41	20.29	504.29	117.74	0.0106
8825	0.74	9.86	9.42			2983.32	11540.97	0.22	-467.17	-11110.82	0.22					
				SLE Rare		0.00			-313.52			4.11	0.00	20.16	118.33	
				SLE Freq.		0.00			-279.05			3.66	0.00	17.94	105.32	0.0119
				SLE Q.P.		0.00			-267.56			3.51	0.00	17.21	100.98	0.0114
Trave Sez. 2 Rett. 40x40 [cm]																
8825	0.00	9.42	9.42			0.00	11109.65	0.22	-3424.52	-11109.65	0.22					
				SLE Rare		0.00			-527.95			6.95	0.00	34.29	199.17	
				SLE Freq.		0.00			-473.00			6.23	0.00	30.72	178.44	0.0201
				SLE Q.P.		0.00			-454.69			5.99	0.00	29.53	171.53	0.0193
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5066.24	-11109.65	0.22					
				SLE Rare		0.00			-2214.09			29.17	0.00	143.79	835.25	
				SLE Freq.		0.00			-2007.36			26.44	0.00	130.36	757.26	0.0852
				SLE Q.P.		0.00			-1938.45			25.54	0.00	125.89	731.26	0.0822
8823	0.72	9.42	9.42			0.00	11109.65	0.22	-5066.24	-11109.65	0.22					
				SLE Rare		0.00			-3427.55			45.15	0.00	222.60	1293.02	
				SLE Freq.		0.00			-3111.97			40.99	0.00	202.10	1173.97	0.1320
				SLE Q.P.		0.00			-3006.77			39.61	0.00	195.27	1134.28	0.1276
Trave Sez. 2 Rett. 40x40 [cm]																
8823	0.00	9.42	9.42			0.00	11109.65	0.22	-6432.24	-11109.65	0.22					
				SLE Rare		0.00			-3577.94			47.13	0.00	232.36	1349.75	
				SLE Freq.		0.00			-3247.85			42.78	0.00	210.93	1225.23	0.1378
				SLE Q.P.		0.00			-3137.82			41.34	0.00	203.78	1183.72	0.1331
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6777.79	-11109.65	0.22					
				SLE Rare		0.00			-4328.43			57.02	0.00	281.10	1632.87	
				SLE Freq.		0.00			-3931.57			51.79	0.00	255.33	1483.16	0.1688
				SLE Q.P.		0.00			-3799.29			50.05	0.00	246.74	1433.25	0.1612
8821	0.74	9.42	9.42			0.00	11109.65	0.22	-6777.79	-11109.65	0.22					
				SLE Rare		0.00			-4587.71			60.44	0.00	297.94	1730.68	
				SLE Freq.		0.00			-4169.26			54.92	0.00	270.76	1572.82	0.1856
				SLE Q.P.		0.00			-4029.50			53.08	0.00	261.69	1520.10	0.1757
Trave Sez. 2 Rett. 40x40 [cm]																
8821	0.00	9.42	9.42			0.00	11109.65	0.22	-6763.88	-11109.65	0.22					
				SLE Rare		0.00			-4578.22			60.31	0.00	297.32	1727.10	
				SLE Freq.		0.00			-4159.92			54.80	0.00	270.16	1569.30	0.1849
				SLE Q.P.		0.00			-4020.22			52.96	0.00	261.09	1516.60	0.1750
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6763.88	-11109.65	0.22					
				SLE Rare		0.00			-4346.27			57.25	0.00	282.26	1639.60	
				SLE Freq.		0.00			-3951.18			52.05	0.00	256.60	1490.55	0.1701

				SLE Q.P.		0.00			-3818.85			50.31	0.00	248.01	1440.63	0.1620
8819	0.74	9.42	9.42			0.00	11109.65	0.22	-6453.80	-11109.65	0.22					
				SLE Rare		0.00			-3624.05			47.74	0.00	235.36	1367.15	
				SLE Freq.		0.00			-3295.83			43.42	0.00	214.04	1243.33	0.1398
				SLE Q.P.		0.00			-3185.75			41.97	0.00	206.89	1201.80	0.1352
Trave Sez. 2 Rett. 40x40 [cm]																
8819	0.00	9.42	9.42			0.00	11109.65	0.22	-5097.89	-11109.65	0.22					
				SLE Rare		0.00			-3452.72			45.48	0.00	224.23	1302.51	
				SLE Freq.		0.00			-3139.60			41.36	0.00	203.90	1184.39	0.1332
				SLE Q.P.		0.00			-3034.50			39.97	0.00	197.07	1144.74	0.1288
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5097.89	-11109.65	0.22					
				SLE Rare		0.00			-2267.06			29.86	0.00	147.23	855.23	
				SLE Freq.		0.00			-2062.83			27.17	0.00	133.97	778.19	0.0875
				SLE Q.P.		0.00			-1993.99			26.27	0.00	129.50	752.22	0.0846
8817	0.72	9.42	9.42			0.00	11109.65	0.22	-3491.60	-11109.65	0.22					
				SLE Rare		0.00			-608.73			8.02	0.00	39.53	229.64	
				SLE Freq.		0.00			-556.31			7.33	0.00	36.13	209.86	0.0236
				SLE Q.P.		0.00			-538.05			7.09	0.00	34.94	202.98	0.0228
Trave Sez. 2 Rett. 40x40 [cm]																
8817	0.00	9.86	9.42			2863.11	11540.96	0.22	-544.01	-11110.82	0.22					
				SLE Rare		0.00			-372.82			4.89	0.00	23.98	140.71	
				SLE Freq.		0.00			-341.35			4.48	0.00	21.95	128.83	0.0145
				SLE Q.P.		0.00			-330.05			4.33	0.00	21.22	124.57	0.0140
Camp.	0.37	12.04	9.42	5320.00	183.71	6678.66	13724.80	0.24	-544.01	-11115.81	0.22					
				SLE Rare		1822.41			-124.31			1.60	21.90	544.35	127.10	
				SLE Freq.		1654.15			-113.02			1.46	19.88	494.09	115.36	0.0104
				SLE Q.P.		1598.06			-109.26			1.41	19.21	477.34	111.45	0.0101
8815	0.74	14.23	9.42			6678.66	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4512.60			0.00			0.00	51.15	1149.97	324.81	
				SLE Freq.		4098.57			0.00			0.00	46.46	1044.46	295.00	0.0233
				SLE Q.P.		3960.56			0.00			0.00	44.89	1009.29	285.07	0.0226
Trave Sez. 2 Rett. 40x40 [cm]																
8815	0.00	14.91	9.42			11866.45	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4681.94			0.00			0.00	52.24	1141.31	339.34	
				SLE Freq.		4253.31			0.00			0.00	47.45	1036.83	308.27	0.0236
				SLE Q.P.		4110.44			0.00			0.00	45.86	1002.00	297.92	0.0228
Camp.	0.30	16.64	9.42	5320.00	178.82	15024.43	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7253.96			-113.76			1.41	78.05	1593.24	532.95	
				SLE Freq.		6590.55			-103.42			1.28	70.92	1447.53	484.21	0.0342
				SLE Q.P.		6369.42			-99.98			1.24	68.54	1398.96	467.96	0.0330
209	0.61	18.71	6.49			15024.43	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10159.00			-17.25			0.25	109.34	1992.87	552.22	
				SLE Freq.		9230.57			-15.68			0.23	99.34	1810.74	501.76	0.0358
				SLE Q.P.		8921.09			-15.16			0.22	96.01	1750.03	484.93	0.0346

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 218 8827 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	15031.26	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8827 8825 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11794.85	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8825 8823 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7840.47	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8823 8821 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3985.04	8004.72	37247.76	36621.00	ø 10 2br. 12.5'

Trave 8821 8819 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3879.75	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8819 8817 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7735.19	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8817 8815 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11689.56	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 8815 209 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14925.99	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 390 Nodi 309 10559 10561 10563 10565 10567 10569 10571 319*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
309	0.13	18.71	6.49			15277.90	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10331.52			-17.25			0.25	111.19	2026.72	561.60	
				SLE Freq.		9401.15			-15.68			0.23	101.18	1844.21	511.03	0.0365
				SLE Q.P.		9091.64			-15.16			0.22	97.85	1783.49	494.20	0.0353
Camp.	0.43	16.64	9.42	5320.00	178.82	15277.90	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7421.28			-113.76			1.41	79.85	1629.99	545.24	
				SLE Freq.		6755.64			-103.42			1.28	72.69	1483.79	496.34	0.0351
				SLE Q.P.		6534.60			-99.98			1.24	70.31	1435.24	480.10	0.0339
10559	0.73	14.91	9.42			12114.51	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4844.06			0.00			0.00	54.04	1180.84	351.09	
				SLE Freq.		4412.90			0.00			0.00	49.23	1075.73	319.84	0.0244
				SLE Q.P.		4270.24			0.00			0.00	47.64	1040.96	309.50	0.0236
Trave Sez. 2 Rett. 40x40 [cm]																
10559	0.00	14.23	9.42			6962.29	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4705.29			0.00			0.00	53.33	1199.07	338.67	
				SLE Freq.		4288.11			0.00			0.00	48.60	1092.76	308.65	0.0244
				SLE Q.P.		4150.35			0.00			0.00	47.04	1057.66	298.73	0.0236
Camp.	0.37	12.04	9.42	5320.00	183.71	6962.29	13724.80	0.24	-283.59	-11115.81	0.22					
				SLE Rare		2008.74			-124.31			1.60	24.14	600.01	140.09	
				SLE Freq.		1836.97			-113.02			1.46	22.08	548.70	128.11	0.0116
				SLE Q.P.		1781.29			-109.26			1.41	21.41	532.07	124.23	0.0112
10561	0.74	9.86	9.42			3138.00	11540.96	0.22	-283.59	-11110.82	0.22					
				SLE Rare		0.00			-196.13			2.57	0.00	12.61	74.02	
				SLE Freq.		0.00			-164.46			2.16	0.00	10.58	62.07	0.0070
				SLE Q.P.		0.00			-152.72			2.00	0.00	9.82	57.64	0.0065
Trave Sez. 2 Rett. 40x40 [cm]																
10561	0.00	9.42	9.42			0.00	11109.65	0.22	-3212.55	-11109.65	0.22					
				SLE Rare		0.00			-410.99			5.41	0.00	26.69	155.04	
				SLE Freq.		0.00			-358.64			4.72	0.00	23.29	135.29	0.0152
				SLE Q.P.		0.00			-339.92			4.48	0.00	22.08	128.23	0.0144
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-4829.65	-11109.65	0.22					
				SLE Rare		0.00			-2077.33			27.37	0.00	134.91	783.66	
				SLE Freq.		0.00			-1871.84			24.66	0.00	121.56	706.14	0.0794
				SLE Q.P.		0.00			-1802.38			23.74	0.00	117.05	679.94	0.0765
10563	0.72	9.42	9.42			0.00	11109.65	0.22	-4829.65	-11109.65	0.22					
				SLE Rare		0.00			-3270.99			43.09	0.00	212.43	1233.96	
				SLE Freq.		0.00			-2955.31			38.93	0.00	191.93	1114.87	0.1254
				SLE Q.P.		0.00			-2849.41			37.54	0.00	185.05	1074.92	0.1209
Trave Sez. 2 Rett. 40x40 [cm]																
10563	0.00	9.42	9.42			0.00	11109.65	0.22	-6175.45	-11109.65	0.22					
				SLE Rare		0.00			-3427.19			45.15	0.00	222.57	1292.88	
				SLE Freq.		0.00			-3096.73			40.79	0.00	201.11	1168.22	0.1314
				SLE Q.P.		0.00			-2985.85			39.33	0.00	193.91	1126.39	0.1267

Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6495.34	-11109.65	0.22					
				SLE Rare		0.00			-4157.50			54.77	0.00	270.00	1568.39	
				SLE Freq.		0.00			-3758.89			49.52	0.00	244.11	1418.01	0.1595
				SLE Q.P.		0.00			-3625.60			47.76	0.00	235.46	1367.73	0.1538
10565	0.74	9.42	9.42			0.00	11109.65	0.22	-6495.34	-11109.65	0.22					
				SLE Rare		0.00			-4396.58			57.92	0.00	285.53	1658.58	
				SLE Freq.		0.00			-3974.45			52.36	0.00	258.11	1499.33	0.1718
				SLE Q.P.		0.00			-3833.62			50.50	0.00	248.97	1446.20	0.1627
Trave Sez. 2 Rett. 40x40 [cm]																
10565	0.00	9.42	9.42			0.00	11109.65	0.22	-6498.84	-11109.65	0.22					
				SLE Rare		0.00			-4399.04			57.95	0.00	285.69	1659.51	
				SLE Freq.		0.00			-3976.91			52.39	0.00	258.27	1500.26	0.1720
				SLE Q.P.		0.00			-3836.04			50.53	0.00	249.12	1447.12	0.1628
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6498.84	-11109.65	0.22					
				SLE Rare		0.00			-4146.91			54.63	0.00	269.31	1564.39	
				SLE Freq.		0.00			-3746.16			49.35	0.00	243.29	1413.21	0.1590
				SLE Q.P.		0.00			-3612.58			47.59	0.00	234.61	1362.82	0.1533
10567	0.74	9.42	9.42			0.00	11109.65	0.22	-6163.10	-11109.65	0.22					
				SLE Rare		0.00			-3403.56			44.84	0.00	221.04	1283.97	
				SLE Freq.		0.00			-3069.11			40.43	0.00	199.32	1157.80	0.1302
				SLE Q.P.		0.00			-2957.63			38.96	0.00	192.08	1115.74	0.1255
Trave Sez. 2 Rett. 40x40 [cm]																
10567	0.00	9.42	9.42			0.00	11109.65	0.22	-4807.61	-11109.65	0.22					
				SLE Rare		0.00			-3252.94			42.85	0.00	211.26	1227.15	
				SLE Freq.		0.00			-2933.30			38.64	0.00	190.50	1106.57	0.1245
				SLE Q.P.		0.00			-2826.75			37.24	0.00	183.58	1066.37	0.1199
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-4807.61	-11109.65	0.22					
				SLE Rare		0.00			-2046.48			26.96	0.00	132.90	772.02	
				SLE Freq.		0.00			-1835.24			24.18	0.00	119.19	692.33	0.0779
				SLE Q.P.		0.00			-1764.82			23.25	0.00	114.61	665.77	0.0749
10569	0.72	9.42	9.42			0.00	11109.65	0.22	-3175.30	-11109.65	0.22					
				SLE Rare		0.00			-367.34			4.84	0.00	23.86	138.58	
				SLE Freq.		0.00			-307.43			4.05	0.00	19.97	115.98	0.0130
				SLE Q.P.		0.00			-287.46			3.79	0.00	18.67	108.44	0.0122
Trave Sez. 2 Rett. 40x40 [cm]																
10569	0.00	9.86	9.42			3212.95	11540.97	0.22	-237.55	-11110.82	0.22					
				SLE Rare		0.00			-158.82			2.08	0.00	10.21	59.94	
				SLE Freq.		0.00			-119.82			1.57	0.00	7.71	45.22	0.0051
				SLE Q.P.		0.00			-106.82			1.40	0.00	6.87	40.32	0.0045
Camp.	0.37	12.04	9.42	5320.00	183.71	7055.70	13724.81	0.24	-237.55	-11115.81	0.22					
				SLE Rare		2066.69			-124.31			1.60	24.84	617.32	144.13	
				SLE Freq.		1896.10			-113.02			1.46	22.79	566.36	132.24	0.0119
				SLE Q.P.		1842.07			-109.26			1.41	22.14	550.23	128.47	0.0116
10571	0.74	14.23	9.42			7055.70	15895.24	0.26	0.00	-11119.63	0.22					
				SLE Rare		4778.03			0.00			0.00	54.16	1217.61	343.91	
				SLE Freq.		4362.22			0.00			0.00	49.44	1111.65	313.98	0.0248
				SLE Q.P.		4226.44			0.00			0.00	47.91	1077.04	304.21	0.0241
Trave Sez. 2 Rett. 40x40 [cm]																
10571	0.00	14.91	9.42			12214.93	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4907.14			0.00			0.00	54.75	1196.21	355.66	
				SLE Freq.		4477.52			0.00			0.00	49.96	1091.48	324.53	0.0248
				SLE Q.P.		4336.76			0.00			0.00	48.38	1057.17	314.32	0.0240
Camp.	0.30	16.64	9.42	5320.00	178.82	15389.70	18263.85	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7496.45			-113.75			1.41	80.66	1646.50	550.76	
				SLE Freq.		6832.50			-103.42			1.28	73.52	1500.67	501.98	0.0354

				SLE Q.P.		6613.61			-99.98			1.24	71.16	1452.59	485.90	0.0343
319	0.61	18.71	6.49			15389.70	20249.27	0.32	-25.49	-8214.46	0.21					
				SLE Rare		10418.77			-17.25			0.25	112.13	2043.83	566.34	
				SLE Freq.		9490.25			-15.68			0.23	102.14	1861.68	515.87	0.0368
				SLE Q.P.		9183.15			-15.16			0.22	98.83	1801.44	499.18	0.0356

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	Staffe
Trave 309 10559 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	14953.96	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10559 10561 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11717.53	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10561 10563 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7763.16	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10563 10565 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3907.72	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10565 10567 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3956.28	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10567 10569 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7811.71	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10569 10571 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11766.09	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10571 319 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	15002.50	7069.46	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 391 Nodi 319 10573 10575 10577 10579 10581 10583 10585 325*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
319	0.13	18.71	6.49			14448.89	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		9781.22			-17.25			0.25	105.27	1918.76	531.69	
				SLE Freq.		8859.69			-15.68			0.23	95.35	1737.99	481.59	0.0344
				SLE Q.P.		8551.43			-15.16			0.22	92.03	1677.52	464.84	0.0332
Camp.	0.43	16.64	9.42	5320.00	178.82	14448.89	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		6925.05			-113.76			1.41	74.51	1521.00	508.78	
				SLE Freq.		6267.75			-103.42			1.28	67.44	1376.63	460.49	0.0325
				SLE Q.P.		6047.69			-99.98			1.24	65.07	1328.30	444.32	0.0314
10573	0.73	14.91	9.42			11344.63	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4401.91			0.00			0.00	49.11	1073.05	319.04	
				SLE Freq.		3978.57			0.00			0.00	44.39	969.85	288.36	0.0220
				SLE Q.P.		3836.64			0.00			0.00	42.80	935.26	278.08	0.0212
Trave Sez. 2 Rett. 40x40 [cm]																
10573	0.00	14.23	9.42			6266.30	15895.23	0.26	0.00	-11119.63	0.22					
				SLE Rare		4243.34			0.00			0.00	48.10	1081.35	305.43	
				SLE Freq.		3834.98			0.00			0.00	43.47	977.29	276.03	0.0218
				SLE Q.P.		3697.97			0.00			0.00	41.92	942.37	266.17	0.0211
Camp.	0.37	12.04	9.42	5320.00	183.71	6266.30	13724.81	0.24	-778.43	-11115.81	0.22					
				SLE Rare		1612.84			-124.31			1.60	19.38	481.76	112.48	
				SLE Freq.		1449.27			-113.02			1.46	17.42	432.90	101.07	0.0091
				SLE Q.P.		1394.02			-109.26			1.41	16.75	416.39	97.22	0.0088
10575	0.74	9.86	9.42			2537.32	11540.97	0.22	-778.43	-11110.82	0.22					
				SLE Rare		0.00			-524.85			6.89	0.00	33.75	198.09	
				SLE Freq.		0.00			-485.51			6.37	0.00	31.22	183.25	0.0206
				SLE Q.P.		0.00			-473.88			6.22	0.00	30.47	178.86	0.0201
Trave Sez. 2 Rett. 40x40 [cm]																
10575	0.00	9.42	9.42			0.00	11109.65	0.22	-3602.38	-11109.65	0.22					
				SLE Rare		0.00			-742.21			9.78	0.00	48.20	279.99	

				SLE Freq.		0.00			-682.48			8.99	0.00	44.32	257.46	0.0290
				SLE Q.P.		0.00			-663.89			8.75	0.00	43.11	250.45	0.0282
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5125.83	-11109.65	0.22					
				SLE Rare		0.00			-2341.02			30.84	0.00	152.03	883.13	
				SLE Freq.		0.00			-2132.16			28.09	0.00	138.47	804.34	0.0905
				SLE Q.P.		0.00			-2063.08			27.18	0.00	133.98	778.28	0.0875
10577	0.72	9.42	9.42			0.00	11109.65	0.22	-5125.83	-11109.65	0.22					
				SLE Rare		0.00			-3467.84			45.68	0.00	225.21	1308.22	
				SLE Freq.		0.00			-3152.09			41.52	0.00	204.71	1189.10	0.1337
				SLE Q.P.		0.00			-3046.83			40.14	0.00	197.87	1149.40	0.1293
Trave Sez. 2 Rett. 40x40 [cm]																
10577	0.00	9.42	9.42			0.00	11109.65	0.22	-6356.22	-11109.65	0.22					
				SLE Rare		0.00			-3617.13			47.65	0.00	234.91	1364.54	
				SLE Freq.		0.00			-3286.44			43.29	0.00	213.43	1239.79	0.1394
				SLE Q.P.		0.00			-3176.21			41.84	0.00	206.27	1198.20	0.1348
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6588.60	-11109.65	0.22					
				SLE Rare		0.00			-4280.96			56.39	0.00	278.02	1614.96	
				SLE Freq.		0.00			-3883.84			51.16	0.00	252.23	1465.15	0.1654
				SLE Q.P.		0.00			-3751.46			49.42	0.00	243.63	1415.21	0.1592
10579	0.74	9.42	9.42			0.00	11109.65	0.22	-6588.60	-11109.65	0.22					
				SLE Rare		0.00			-4453.58			58.67	0.00	289.23	1680.08	
				SLE Freq.		0.00			-4034.66			53.15	0.00	262.02	1522.05	0.1760
				SLE Q.P.		0.00			-3895.01			51.31	0.00	252.95	1469.36	0.1662
Trave Sez. 2 Rett. 40x40 [cm]																
10579	0.00	9.42	9.42			0.00	11109.65	0.22	-6567.74	-11109.65	0.22					
				SLE Rare		0.00			-4444.74			58.55	0.00	288.65	1676.74	
				SLE Freq.		0.00			-4025.61			53.03	0.00	261.44	1518.63	0.1754
				SLE Q.P.		0.00			-3885.89			51.19	0.00	252.36	1465.92	0.1655
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6567.74	-11109.65	0.22					
				SLE Rare		0.00			-4126.13			54.35	0.00	267.96	1556.55	
				SLE Freq.		0.00			-3730.12			49.14	0.00	242.25	1407.16	0.1583
				SLE Q.P.		0.00			-3597.96			47.40	0.00	233.66	1357.30	0.1527
10581	0.74	9.42	9.42			0.00	11109.65	0.22	-6136.73	-11109.65	0.22					
				SLE Rare		0.00			-3316.30			43.69	0.00	215.37	1251.05	
				SLE Freq.		0.00			-2988.04			39.36	0.00	194.05	1127.22	0.1268
				SLE Q.P.		0.00			-2878.29			37.92	0.00	186.93	1085.82	0.1221
Trave Sez. 2 Rett. 40x40 [cm]																
10581	0.00	9.42	9.42			0.00	11109.65	0.22	-4659.73	-11109.65	0.22					
				SLE Rare		0.00			-3154.72			41.56	0.00	204.88	1190.09	
				SLE Freq.		0.00			-2840.91			37.42	0.00	184.50	1071.71	0.1205
				SLE Q.P.		0.00			-2735.99			36.04	0.00	177.68	1032.13	0.1161
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-4659.73	-11109.65	0.22					
				SLE Rare		0.00			-1883.05			24.81	0.00	122.29	710.37	
				SLE Freq.		0.00			-1679.04			22.12	0.00	109.04	633.41	0.0712
				SLE Q.P.		0.00			-1610.58			21.22	0.00	104.60	607.58	0.0683
10583	0.72	9.42	9.42			0.00	11109.65	0.22	-2935.97	-11109.65	0.22					
				SLE Rare		0.00			-138.70			1.83	0.00	9.01	52.32	
				SLE Freq.		0.00			-87.43			1.15	0.00	5.68	32.98	0.0037
				SLE Q.P.		0.00			-69.73			0.92	0.00	4.53	26.30	0.0030
Trave Sez. 2 Rett. 40x40 [cm]																
10583	0.00	9.86	9.42			3677.96	11540.95	0.22	0.00	-11110.82	0.22					
				SLE Rare		139.73			0.00			0.00	1.81	50.52	9.22	
				SLE Freq.		122.97			0.00			0.00	1.59	44.46	8.11	0.0009
				SLE Q.P.		117.06			0.00			0.00	1.52	42.32	7.72	0.0008
Camp.	0.37	12.04	9.42	5320.00	183.71	7619.42	13724.79	0.24	-183.71	-11115.81	0.22					

				SLE Rare		2372.25			-124.31			1.60	28.51	708.59	165.44	
				SLE Freq.		2185.55			-113.02			1.46	26.27	652.82	152.42	0.0137
				SLE Q.P.		2129.28			-109.26			1.41	25.59	636.02	148.50	0.0134
10585	0.74	14.23	9.42			7619.42	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		5152.02			0.00			0.00	58.40	1312.92	370.83	
				SLE Freq.		4716.83			0.00			0.00	53.46	1202.02	339.51	0.0269
				SLE Q.P.		4578.53			0.00			0.00	51.90	1166.77	329.55	0.0261
Trave Sez. 2 Rett. 40x40 [cm]																
10585	0.00	14.91	9.42			12875.38	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		5274.05			0.00			0.00	58.84	1285.65	382.26	
				SLE Freq.		4825.88			0.00			0.00	53.84	1176.40	349.77	0.0267
				SLE Q.P.		4682.86			0.00			0.00	52.25	1141.54	339.41	0.0259
Camp.	0.30	16.64	9.42	5320.00	178.82	16111.42	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7919.38			-113.76			1.41	85.21	1739.39	581.84	
				SLE Freq.		7234.21			-103.42			1.28	77.84	1588.90	531.50	0.0375
				SLE Q.P.		7012.84			-99.98			1.24	75.46	1540.28	515.23	0.0364
325	0.61	18.71	6.49			16111.42	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10897.73			-17.25			0.25	117.29	2137.79	592.38	
				SLE Freq.		9945.31			-15.68			0.23	107.04	1950.95	540.61	0.0386
				SLE Q.P.		9635.51			-15.16			0.22	103.70	1890.18	523.77	0.0374

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 319 10573 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	14682.24	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10573 10575 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11445.82	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10575 10577 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7491.45	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10577 10579 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3636.02	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10579 10581 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	4234.25	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10581 10583 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	8089.69	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10583 10585 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	12044.06	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10585 325 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	15280.49	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 392 Nodi 325 10584 10582 10580 10578 10576 10574 10572 318*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 2 Rett. 40x40 [cm]																
325	0.12	18.71	6.49			15084.51	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10204.60			-17.25			0.25	109.83	2001.82	554.70	
				SLE Freq.		9275.81			-15.68			0.23	99.83	1819.62	504.21	0.0360
				SLE Q.P.		8966.21			-15.16			0.22	96.50	1758.89	487.39	0.0348
Camp.	0.43	16.64	9.42	5320.00	178.82	15084.51	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		7289.95			-113.76			1.41	78.44	1601.14	535.59	
				SLE Freq.		6626.30			-103.42			1.28	71.30	1455.38	486.83	0.0344
				SLE Q.P.		6405.09			-99.98			1.24	68.92	1406.80	470.58	0.0332
10584	0.73	14.91	9.42			11916.79	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4708.31			0.00			0.00	52.53	1147.74	341.25	
				SLE Freq.		4279.56			0.00			0.00	47.75	1043.23	310.18	0.0237
				SLE Q.P.		4136.65			0.00			0.00	46.15	1008.39	299.82	0.0229
Trave Sez. 2 Rett. 40x40 [cm]																

10584	0.00	14.23	9.42			6725.69	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4548.75			0.00			0.00	51.56	1159.18	327.41	
				SLE Freq.		4134.52			0.00			0.00	46.86	1053.62	297.59	0.0235
				SLE Q.P.		3996.44			0.00			0.00	45.30	1018.43	287.65	0.0228
Camp.	0.37	12.04	9.42	5320.00	183.71	6725.69	13724.80	0.24	-528.04	-11115.81	0.22					
				SLE Rare		1846.81			-124.31			1.60	22.20	551.64	128.80	
				SLE Freq.		1678.49			-113.02			1.46	20.17	501.37	117.06	0.0106
				SLE Q.P.		1622.38			-109.26			1.41	19.50	484.61	113.15	0.0102
10582	0.74	9.86	9.42			2894.43	11540.96	0.22	-528.04	-11110.82	0.22					
				SLE Rare		0.00			-358.96			4.71	0.00	23.08	135.48	
				SLE Freq.		0.00			-326.90			4.29	0.00	21.02	123.38	0.0139
				SLE Q.P.		0.00			-315.87			4.14	0.00	20.31	119.22	0.0134
Trave Sez. 2 Rett. 40x40 [cm]																
10582	0.00	9.42	9.42			0.00	11109.65	0.22	-3481.57	-11109.65	0.22					
				SLE Rare		0.00			-586.48			7.73	0.00	38.09	221.24	
				SLE Freq.		0.00			-533.76			7.03	0.00	34.66	201.36	0.0226
				SLE Q.P.		0.00			-515.82			6.80	0.00	33.50	194.59	0.0219
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5103.50	-11109.65	0.22					
				SLE Rare		0.00			-2256.80			29.73	0.00	146.56	851.36	
				SLE Freq.		0.00			-2051.94			27.03	0.00	133.26	774.08	0.0871
				SLE Q.P.		0.00			-1983.31			26.13	0.00	128.80	748.19	0.0842
10580	0.72	9.42	9.42			0.00	11109.65	0.22	-5103.50	-11109.65	0.22					
				SLE Rare		0.00			-3454.44			45.51	0.00	224.34	1303.16	
				SLE Freq.		0.00			-3140.38			41.37	0.00	203.95	1184.68	0.1332
				SLE Q.P.		0.00			-3035.37			39.99	0.00	197.13	1145.07	0.1288
Trave Sez. 2 Rett. 40x40 [cm]																
10580	0.00	9.42	9.42			0.00	11109.65	0.22	-6465.26	-11109.65	0.22					
				SLE Rare		0.00			-3617.19			47.65	0.00	234.91	1364.56	
				SLE Freq.		0.00			-3288.34			43.32	0.00	213.55	1240.50	0.1395
				SLE Q.P.		0.00			-3178.40			41.87	0.00	206.41	1199.03	0.1349
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6790.86	-11109.65	0.22					
				SLE Rare		0.00			-4351.87			57.33	0.00	282.62	1641.71	
				SLE Freq.		0.00			-3955.57			52.11	0.00	256.89	1492.21	0.1705
				SLE Q.P.		0.00			-3823.27			50.36	0.00	248.29	1442.30	0.1622
10578	0.74	9.42	9.42			0.00	11109.65	0.22	-6790.86	-11109.65	0.22					
				SLE Rare		0.00			-4595.50			60.54	0.00	298.45	1733.62	
				SLE Freq.		0.00			-4176.21			55.01	0.00	271.22	1575.44	0.1861
				SLE Q.P.		0.00			-4036.42			53.17	0.00	262.14	1522.71	0.1762
Trave Sez. 2 Rett. 40x40 [cm]																
10578	0.00	9.42	9.42			0.00	11109.65	0.22	-6792.90	-11109.65	0.22					
				SLE Rare		0.00			-4596.90			60.56	0.00	298.54	1734.15	
				SLE Freq.		0.00			-4177.52			55.03	0.00	271.30	1575.94	0.1862
				SLE Q.P.		0.00			-4037.70			53.19	0.00	262.22	1523.19	0.1763
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6792.90	-11109.65	0.22					
				SLE Rare		0.00			-4349.30			57.29	0.00	282.46	1640.74	
				SLE Freq.		0.00			-3951.88			52.06	0.00	256.65	1490.82	0.1702
				SLE Q.P.		0.00			-3819.41			50.31	0.00	248.04	1440.84	0.1621
10576	0.74	9.42	9.42			0.00	11109.65	0.22	-6462.87	-11109.65	0.22					
				SLE Rare		0.00			-3610.49			47.56	0.00	234.48	1362.03	
				SLE Freq.		0.00			-3279.69			43.20	0.00	212.99	1237.24	0.1392
				SLE Q.P.		0.00			-3169.42			41.75	0.00	205.83	1195.64	0.1345
Trave Sez. 2 Rett. 40x40 [cm]																
10576	0.00	9.42	9.42			0.00	11109.65	0.22	-5100.34	-11109.65	0.22					
				SLE Rare		0.00			-3450.77			45.46	0.00	224.10	1301.78	
				SLE Freq.		0.00			-3134.61			41.29	0.00	203.57	1182.51	0.1330

				SLE Q.P.		0.00			-3029.22			39.90	0.00	196.73	1142.75	0.1285
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5100.34	-11109.65	0.22					
				SLE Rare		0.00			-2248.77			29.62	0.00	146.04	848.33	
				SLE Freq.		0.00			-2041.31			26.89	0.00	132.57	770.07	0.0866
				SLE Q.P.		0.00			-1972.16			25.98	0.00	128.08	743.98	0.0837
10574	0.72	9.42	9.42			0.00	11109.65	0.22	-3473.51	-11109.65	0.22					
				SLE Rare		0.00			-574.08			7.56	0.00	37.28	216.57	
				SLE Freq.		0.00			-518.27			6.83	0.00	33.66	195.51	0.0220
				SLE Q.P.		0.00			-499.66			6.58	0.00	32.45	188.49	0.0212
Trave Sez. 2 Rett. 40x40 [cm]																
10574	0.00	9.86	9.42			2911.53	11540.97	0.22	-518.72	-11110.82	0.22					
				SLE Rare		0.00			-349.69			4.59	0.00	22.49	131.98	
				SLE Freq.		0.00			-314.49			4.13	0.00	20.22	118.70	0.0134
				SLE Q.P.		0.00			-302.76			3.97	0.00	19.47	114.27	0.0129
Camp.	0.37	12.04	9.42	5320.00	183.71	6747.98	13724.81	0.24	-518.72	-11115.81	0.22					
				SLE Rare		1861.96			-124.31			1.60	22.38	556.17	129.86	
				SLE Freq.		1695.81			-113.02			1.46	20.38	506.54	118.27	0.0107
				SLE Q.P.		1640.57			-109.26			1.41	19.72	490.04	114.42	0.0103
10572	0.74	14.23	9.42			6747.98	15895.23	0.26	0.00	-11119.63	0.22					
				SLE Rare		4568.38			0.00			0.00	51.78	1164.18	328.82	
				SLE Freq.		4156.83			0.00			0.00	47.12	1059.31	299.20	0.0237
				SLE Q.P.		4019.77			0.00			0.00	45.56	1024.38	289.33	0.0229
Trave Sez. 2 Rett. 40x40 [cm]																
10572	0.00	14.91	9.42			11939.07	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		4723.80			0.00			0.00	52.70	1151.52	342.38	
				SLE Freq.		4297.83			0.00			0.00	47.95	1047.68	311.50	0.0238
				SLE Q.P.		4155.93			0.00			0.00	46.37	1013.09	301.22	0.0230
Camp.	0.30	16.64	9.42	5320.00	178.82	15109.96	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7309.09			-113.76			1.41	78.65	1605.35	537.00	
				SLE Freq.		6648.64			-103.42			1.28	71.54	1460.29	488.47	0.0345
				SLE Q.P.		6428.56			-99.98			1.24	69.17	1411.95	472.31	0.0334
318	0.61	18.71	6.49			15109.96	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10227.39			-17.25			0.25	110.07	2006.29	555.94	
				SLE Freq.		9302.21			-15.68			0.23	100.11	1824.80	505.65	0.0361
				SLE Q.P.		8993.88			-15.16			0.22	96.80	1764.31	488.89	0.0349

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 325 10584 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	14970.24	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10584 10582 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11733.81	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10582 10580 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7779.44	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10580 10578 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3924.00	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10578 10576 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3938.60	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10576 10574 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7794.04	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10574 10572 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11748.41	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10572 318 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14984.82	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 393 Nodi 318 10570 10568 10566 10564 10562 10560 10558 309*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
318	0.13	18.71	6.49			16172.44	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		10946.34			-17.25			0.25	117.81	2147.32	595.02	
				SLE Freq.		9995.47			-15.68			0.23	107.58	1960.79	543.33	0.0388
				SLE Q.P.		9686.97			-15.16			0.22	104.26	1900.28	526.56	0.0376
Camp.	0.43	16.64	9.42	5320.00	178.82	16172.44	18263.84	0.28	-168.10	-11122.91	0.22					
				SLE Rare		7960.46			-113.75			1.41	85.66	1748.41	584.85	
				SLE Freq.		7276.73			-103.42			1.28	78.30	1598.24	534.62	0.0378
				SLE Q.P.		7056.54			-99.98			1.24	75.93	1549.88	518.44	0.0366
10570	0.73	14.91	9.42			12929.36	16566.54	0.26	0.00	-11120.64	0.22					
				SLE Rare		5307.61			0.00			0.00	59.22	1293.83	384.69	
				SLE Freq.		4860.77			0.00			0.00	54.23	1184.91	352.30	0.0269
				SLE Q.P.		4718.80			0.00			0.00	52.65	1150.30	342.01	0.0261
Trave Sez. 2 Rett. 40x40 [cm]																
10570	0.00	14.23	9.42			7669.71	15895.24	0.26	0.00	-11119.63	0.22					
				SLE Rare		5192.03			0.00			0.00	58.85	1323.11	373.71	
				SLE Freq.		4758.07			0.00			0.00	53.93	1212.52	342.47	0.0271
				SLE Q.P.		4620.82			0.00			0.00	52.38	1177.55	332.60	0.0263
Camp.	0.37	12.04	9.42	5320.00	183.71	7669.71	13724.81	0.24	-183.71	-11115.81	0.22					
				SLE Rare		2403.03			-124.31			1.60	28.88	717.79	167.59	
				SLE Freq.		2217.43			-113.02			1.46	26.65	662.35	154.65	0.0140
				SLE Q.P.		2162.05			-109.26			1.41	25.98	645.81	150.78	0.0136
10568	0.74	9.86	9.42			3716.79	11540.97	0.22	0.00	-11110.82	0.22					
				SLE Rare		162.38			0.00			0.00	2.10	58.70	10.71	
				SLE Freq.		147.02			0.00			0.00	1.90	53.15	9.70	0.0010
				SLE Q.P.		140.32			0.00			0.00	1.82	50.73	9.26	0.0010
Trave Sez. 2 Rett. 40x40 [cm]																
10568	0.00	9.42	9.42			0.00	11109.65	0.22	-2919.79	-11109.65	0.22					
				SLE Rare		0.00			-116.43			1.53	0.00	7.56	43.92	
				SLE Freq.		0.00			-60.87			0.80	0.00	3.95	22.96	0.0026
				SLE Q.P.		0.00			-42.35			0.56	0.00	2.75	15.98	0.0018
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-4652.84	-11109.65	0.22					
				SLE Rare		0.00			-1868.65			24.62	0.00	121.36	704.93	
				SLE Freq.		0.00			-1661.39			21.89	0.00	107.90	626.75	0.0705
				SLE Q.P.		0.00			-1592.30			20.98	0.00	103.41	600.68	0.0676
10566	0.72	9.42	9.42			0.00	11109.65	0.22	-4652.84	-11109.65	0.22					
				SLE Rare		0.00			-3148.19			41.47	0.00	204.45	1187.63	
				SLE Freq.		0.00			-2832.17			37.31	0.00	183.93	1068.41	0.1202
				SLE Q.P.		0.00			-2726.82			35.92	0.00	177.09	1028.67	0.1157
Trave Sez. 2 Rett. 40x40 [cm]																
10566	0.00	9.42	9.42			0.00	11109.65	0.22	-6134.53	-11109.65	0.22					
				SLE Rare		0.00			-3305.51			43.54	0.00	214.67	1246.98	
				SLE Freq.		0.00			-2975.10			39.19	0.00	193.21	1122.33	0.1262
				SLE Q.P.		0.00			-2864.96			37.74	0.00	186.06	1080.78	0.1216
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6575.23	-11109.65	0.22					
				SLE Rare		0.00			-4123.38			54.32	0.00	267.78	1555.51	
				SLE Freq.		0.00			-3726.27			49.09	0.00	242.00	1405.71	0.1581
				SLE Q.P.		0.00			-3593.90			47.34	0.00	233.40	1355.77	0.1525
10564	0.74	9.42	9.42			0.00	11109.65	0.22	-6575.23	-11109.65	0.22					
				SLE Rare		0.00			-4450.02			58.62	0.00	289.00	1678.74	
				SLE Freq.		0.00			-4030.97			53.10	0.00	261.78	1520.65	0.1758
				SLE Q.P.		0.00			-3891.22			51.26	0.00	252.71	1467.94	0.1659

Trave Sez. 2 Rett. 40x40 [cm]																
10564	0.00	9.42	9.42			0.00	11109.65	0.22	-6592.30	-11109.65	0.22					
				SLE Rare		0.00			-4454.90			58.69	0.00	289.31	1680.58	
				SLE Freq.		0.00			-4036.09			53.17	0.00	262.12	1522.59	0.1761
				SLE Q.P.		0.00			-3896.46			51.33	0.00	253.05	1469.91	0.1663
Camp.	0.37	9.42	9.42	5320.00	181.48	0.00	11109.65	0.22	-6592.30	-11109.65	0.22					
				SLE Rare		0.00			-4290.32			56.52	0.00	278.63	1618.49	
				SLE Freq.		0.00			-3894.59			51.30	0.00	252.93	1469.21	0.1661
				SLE Q.P.		0.00			-3762.39			49.56	0.00	244.34	1419.34	0.1596
10562	0.74	9.42	9.42			0.00	11109.65	0.22	-6367.74	-11109.65	0.22					
				SLE Rare		0.00			-3635.58			47.89	0.00	236.11	1371.50	
				SLE Freq.		0.00			-3306.49			43.56	0.00	214.73	1247.35	0.1403
				SLE Q.P.		0.00			-3196.59			42.11	0.00	207.60	1205.89	0.1356
Trave Sez. 2 Rett. 40x40 [cm]																
10562	0.00	9.42	9.42			0.00	11109.65	0.22	-5143.87	-11109.65	0.22					
				SLE Rare		0.00			-3482.17			45.87	0.00	226.14	1313.62	
				SLE Freq.		0.00			-3167.60			41.73	0.00	205.71	1194.95	0.1344
				SLE Q.P.		0.00			-3062.73			40.35	0.00	198.90	1155.39	0.1300
Camp.	0.36	9.42	9.42	5320.00	174.63	0.00	11109.65	0.22	-5143.87	-11109.65	0.22					
				SLE Rare		0.00			-2365.02			31.16	0.00	153.59	892.19	
				SLE Freq.		0.00			-2156.78			28.41	0.00	140.07	813.63	0.0915
				SLE Q.P.		0.00			-2088.24			27.51	0.00	135.62	787.77	0.0886
10560	0.72	9.42	9.42			0.00	11109.65	0.22	-3632.30	-11109.65	0.22					
				SLE Rare		0.00			-775.20			10.21	0.00	50.34	292.44	
				SLE Freq.		0.00			-716.22			9.43	0.00	46.51	270.19	0.0304
				SLE Q.P.		0.00			-698.32			9.20	0.00	45.35	263.44	0.0296
Trave Sez. 2 Rett. 40x40 [cm]																
10560	0.00	9.86	9.42			2497.66	11540.96	0.22	-813.48	-11110.82	0.22					
				SLE Rare		0.00			-552.56			7.25	0.00	35.53	208.55	
				SLE Freq.		0.00			-514.12			6.75	0.00	33.06	194.04	0.0218
				SLE Q.P.		0.00			-503.21			6.60	0.00	32.36	189.92	0.0214
Camp.	0.37	12.04	9.42	5320.00	183.71	6216.84	13724.80	0.24	-813.48	-11115.81	0.22					
				SLE Rare		1581.12			-124.31			1.60	19.00	472.28	110.27	
				SLE Freq.		1412.25			-113.02			1.46	16.97	421.84	98.49	0.0089
				SLE Q.P.		1355.96			-109.26			1.41	16.30	405.03	94.57	0.0085
10558	0.74	14.23	9.42			6216.84	15895.21	0.26	0.00	-11119.63	0.22					
				SLE Rare		4203.54			0.00			0.00	47.65	1071.21	302.56	
				SLE Freq.		3788.82			0.00			0.00	42.95	965.52	272.71	0.0216
				SLE Q.P.		3650.58			0.00			0.00	41.38	930.30	262.76	0.0208
Trave Sez. 2 Rett. 40x40 [cm]																
10558	0.00	14.91	9.42			11293.56	16566.52	0.26	0.00	-11120.64	0.22					
				SLE Rare		4368.81			0.00			0.00	48.74	1064.98	316.65	
				SLE Freq.		3939.40			0.00			0.00	43.95	960.31	285.52	0.0218
				SLE Q.P.		3796.26			0.00			0.00	42.35	925.41	275.15	0.0210
Camp.	0.30	16.64	9.42	5320.00	178.82	14391.77	18263.83	0.28	-168.11	-11122.91	0.22					
				SLE Rare		6885.35			-113.76			1.41	74.09	1512.28	505.87	
				SLE Freq.		6221.10			-103.42			1.28	66.94	1366.39	457.06	0.0323
				SLE Q.P.		5999.68			-99.98			1.24	64.56	1317.75	440.80	0.0311
309	0.61	18.71	6.49			14391.77	20249.27	0.32	-25.49	-8214.47	0.21					
				SLE Rare		9734.92			-17.25			0.25	104.77	1909.68	529.17	
				SLE Freq.		8805.57			-15.68			0.23	94.77	1727.37	478.65	0.0342
				SLE Q.P.		8495.79			-15.16			0.22	91.44	1666.60	461.81	0.0330

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	Staffe
Trave 318 10570 Sez. 2 Rett. 40x40 [cm]							
0.13	0.73	0.61	15312.67	7069.47	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10570 10568 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	12076.25	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10568 10566 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	8121.87	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10566 10564 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	4266.44	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10564 10562 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	3608.41	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10562 10560 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7463.85	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10560 10558 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	11418.22	8004.72	37247.76	36621.00	ø 10 2br. 12.5'
Trave 10558 309 Sez. 2 Rett. 40x40 [cm]							
0.00	0.61	0.61	14654.65	7069.47	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 5 Nodi 241 7022*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
241	0.13	6.03	6.03			0.00	7803.06	0.15	-2753.83	-7803.06	0.15					
				SLE Rare		0.00			-1689.03			24.07	0.00	144.44	915.97	
				SLE Freq.		0.00			-1674.66			23.86	0.00	143.21	908.17	0.0985
				SLE Q.P.		0.00			-1677.35			23.90	0.00	143.44	909.63	0.0986
Camp.	2.13	6.03	6.03	520.00	587.03	1881.80	7803.06	0.15	-587.03	-7803.06	0.15					
				SLE Rare		583.48			-451.56			6.43	8.31	316.42	244.88	
				SLE Freq.		515.75			-451.56			6.43	7.35	279.69	244.88	0.0266
				SLE Q.P.		493.20			-451.56			6.43	7.03	267.47	244.88	0.0266
7022	4.13	6.03	6.03			6617.23	7803.06	0.15	0.00	-7803.06	0.15					
				SLE Rare		4459.39			0.00			0.00	63.54	2418.34	381.35	
				SLE Freq.		4268.80			0.00			0.00	60.83	2314.98	365.05	0.0396
				SLE Q.P.		4222.08			0.00			0.00	60.16	2289.65	361.06	0.0392

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 241 7022 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	1510.77	7037.02	38935.73	63800.94	142.96	5004.46	2832.32	ø 10 2br. 7.5'
0.52	3.72	3.20	3174.77	7037.02	38935.73	38280.56	142.96	5004.46	2832.32	ø 10 2br. 12.5'
3.72	4.13	0.40	3382.77	7037.02	38935.73	63800.94	142.96	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 558 Nodi 3552 3683 4120*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 7 Rett. 30x80 [cm]																
3552	0.13	8.04	8.04			952.74	22578.91	0.08	-949.50	-22578.91	0.08					
				SLE Rare		340.11			0.00			0.00	1.36	61.54	14.54	
				SLE Freq.		257.20			0.00			0.00	1.03	46.54	11.00	0.0010
				SLE Q.P.		229.56			0.00			0.00	0.92	41.54	9.82	0.0009
Camp.	0.99	8.04	8.04	780.00	168.19	940.59	22578.91	0.08	-949.50	-22578.91	0.08					
				SLE Rare		82.00			-127.79			0.51	0.33	14.84	23.12	
				SLE Freq.		21.96			-127.79			0.51	0.09	5.47	23.12	0.0021
				SLE Q.P.		1.94			-127.79			0.51	0.01	5.47	23.12	0.0021
3683	1.86	8.04	8.04			817.74	22578.91	0.08	-920.39	-22578.91	0.08					
				SLE Rare		273.80			0.00			0.00	1.09	49.54	11.71	
				SLE Freq.		236.63			0.00			0.00	0.94	42.81	10.12	0.0009

				SLE Q.P.		224.23			0.00			0.00	0.89	40.57	9.59	0.0009
Trave Sez. 7 Rett. 30x80 [cm]																
3683	0.00	8.04	8.04			0.00	22578.91	0.08	-2756.79	-22578.91	0.08					
				SLE Rare		0.00			-1150.74			4.59	0.00	49.21	208.21	
				SLE Freq.		0.00			-1100.42			4.39	0.00	47.06	199.10	0.0179
				SLE Q.P.		0.00			-1083.13			4.32	0.00	46.32	195.98	0.0176
Camp.	2.95	8.04	8.04	780.00	1772.17	4662.47	22578.91	0.08	-1860.82	-22578.91	0.08					
				SLE Rare		2185.05			-1361.76			5.43	8.72	395.35	246.39	
				SLE Freq.		2097.09			-1361.76			5.43	8.37	379.44	246.39	0.0221
				SLE Q.P.		2068.36			-1361.76			5.43	8.25	374.24	246.39	0.0221
4120	5.90	8.04	10.05			316.36	22577.11	0.08	-14862.22	-28043.51	0.09					
				SLE Rare		0.00			-8293.23			30.58	0.00	340.37	1209.57	
				SLE Freq.		0.00			-8101.26			29.87	0.00	332.49	1181.57	0.0971
				SLE Q.P.		0.00			-8049.75			29.68	0.00	330.37	1174.06	0.0965

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 3552 3683 Sez. 7 Rett. 30x80 [cm]										
0.13	1.86	1.73	799.57	9231.02	91905.48	33235.49	337.40	11601.62	6485.85	ø 10 2br. 12.5'
Trave 3683 4120 Sez. 7 Rett. 30x80 [cm]										
0.00	0.80	0.80	1710.92	9231.02	91905.48	33235.49	465.16	11601.62	6485.85	ø 10 2br. 12.5'
0.80	5.10	4.30	12368.77	9231.02	63383.09	51930.45	465.16	11601.62	4053.66	ø 10 2br. 20.0'
5.10	5.90	0.80	12339.12	9943.82	91905.48	33235.49	465.16	11601.62	6485.85	ø 10 2br. 12.5'

Travata: *Travata 560 Nodi 11545 11601 11603 11605 11607 11609*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 2 Rett. 40x40 [cm]																
11545	0.12	12.57	12.57			12134.27	14241.09	0.24	-23.94	-14241.09	0.24					
				SLE Rare		8186.13			-16.21			0.19	93.85	2355.31	539.33	
				SLE Freq.		7724.88			-15.33			0.18	88.56	2222.60	508.95	0.0517
				SLE Q.P.		7609.88			-15.11			0.17	87.24	2189.52	501.37	0.0509
Camp.	0.43	12.57	12.57	4996.24	167.94	12134.27	14241.09	0.24	-157.87	-14241.09	0.24					
				SLE Rare		4914.21			-106.93			1.23	56.34	1413.92	323.77	
				SLE Freq.		4637.86			-101.09			1.16	53.17	1334.41	305.56	0.0310
				SLE Q.P.		4569.07			-99.63			1.14	52.38	1314.61	301.03	0.0306
11601	0.73	12.57	12.57			8576.79	14241.09	0.24	0.00	-14241.09	0.24					
				SLE Rare		1955.35			0.00			0.00	22.42	562.59	128.83	
				SLE Freq.		1846.77			0.00			0.00	21.17	531.35	121.67	0.0124
				SLE Q.P.		1819.91			0.00			0.00	20.86	523.63	119.90	0.0122
Trave Sez. 2 Rett. 40x40 [cm]																
11601	0.00	12.57	12.57			2306.07	14241.09	0.24	-2100.37	-14241.09	0.24					
				SLE Rare		1557.60			0.00			0.00	17.86	448.15	102.62	
				SLE Freq.		1471.65			0.00			0.00	16.87	423.42	96.96	0.0098
				SLE Q.P.		1450.44			0.00			0.00	16.63	417.32	95.56	0.0097
Camp.	0.37	12.57	12.57	4999.34	172.63	2306.06	14241.09	0.24	-5474.20	-14241.09	0.24					
				SLE Rare		0.00			-1300.25			14.91	0.00	85.67	374.11	
				SLE Freq.		0.00			-1225.05			14.04	0.00	80.71	352.47	0.0358
				SLE Q.P.		0.00			-1206.86			13.84	0.00	79.51	347.24	0.0353
11603	0.74	12.57	12.57			0.00	14241.09	0.24	-5474.20	-14241.09	0.24					
				SLE Rare		0.00			-3690.38			42.31	0.00	243.14	1061.80	
				SLE Freq.		0.00			-3479.61			39.89	0.00	229.25	1001.16	0.1017
				SLE Q.P.		0.00			-3427.34			39.29	0.00	225.81	986.12	0.1001
Trave Sez. 2 Rett. 40x40 [cm]																
11603	0.00	12.57	12.57			0.00	14241.09	0.24	-8389.37	-14241.09	0.24					
				SLE Rare		0.00			-4020.45			46.09	0.00	264.88	1156.76	
				SLE Freq.		0.00			-3790.97			43.46	0.00	249.76	1090.74	0.1108

				SLE Q.P.		0.00			-3734.08			42.81	0.00	246.02	1074.37	0.1091
Camp.	0.36	12.57	12.57	4994.58	163.95	0.00	14241.09	0.24	-9884.61	-14241.09	0.24					
				SLE Rare		0.00			-5565.13			63.80	0.00	366.65	1601.20	
				SLE Freq.		0.00			-5248.90			60.18	0.00	345.82	1510.22	0.1805
				SLE Q.P.		0.00			-5170.14			59.27	0.00	340.63	1487.55	0.1767
11605	0.72	12.57	12.57			0.00	14241.09	0.24	-9884.61	-14241.09	0.24					
				SLE Rare		0.00			-6665.61			76.42	0.00	439.16	1917.83	
				SLE Freq.		0.00			-6286.93			72.08	0.00	414.21	1808.88	0.2311
				SLE Q.P.		0.00			-6192.36			70.99	0.00	407.98	1781.67	0.2265
Trave Sez. 2 Rett. 40x40 [cm]																
11605	0.00	12.57	12.57			0.00	14241.09	0.24	-10594.36	-14241.09	0.24					
				SLE Rare		0.00			-6808.68			78.06	0.00	448.58	1959.00	
				SLE Freq.		0.00			-6421.93			73.62	0.00	423.10	1847.72	0.2377
				SLE Q.P.		0.00			-6325.40			72.52	0.00	416.74	1819.95	0.2330
Camp.	0.37	12.57	12.57	4999.63	170.55	0.00	14241.09	0.24	-10604.38	-14241.09	0.24					
				SLE Rare		0.00			-7141.50			81.87	0.00	470.51	2054.76	
				SLE Freq.		0.00			-6736.66			77.23	0.00	443.84	1938.27	0.2530
				SLE Q.P.		0.00			-6635.41			76.07	0.00	437.17	1909.14	0.2481
11607	0.74	12.57	12.57			0.00	14241.09	0.24	-10604.38	-14241.09	0.24					
				SLE Rare		0.00			-7012.24			80.39	0.00	461.99	2017.57	
				SLE Freq.		0.00			-6614.58			75.83	0.00	435.79	1903.15	0.2470
				SLE Q.P.		0.00			-6515.05			74.69	0.00	429.24	1874.51	0.2422
Trave Sez. 2 Rett. 40x40 [cm]																
11607	0.00	12.57	12.57			0.00	14241.09	0.24	-10215.19	-14241.09	0.24					
				SLE Rare		0.00			-6889.21			78.98	0.00	453.89	1982.17	
				SLE Freq.		0.00			-6498.58			74.50	0.00	428.15	1869.77	0.2414
				SLE Q.P.		0.00			-6400.84			73.38	0.00	421.71	1841.65	0.2366
Camp.	0.34	12.57	12.57	4996.78	170.45	0.00	14241.09	0.24	-10215.19	-14241.09	0.24					
				SLE Rare		0.00			-6042.62			69.27	0.00	398.11	1738.58	
				SLE Freq.		0.00			-5700.66			65.35	0.00	375.58	1640.20	0.2025
				SLE Q.P.		0.00			-5615.10			64.37	0.00	369.95	1615.58	0.1984
11609	0.69	12.57	12.57			0.00	14241.09	0.24	-9149.69	-14241.09	0.24					
				SLE Rare		0.00			-4794.85			54.97	0.00	315.90	1379.58	
				SLE Freq.		0.00			-4523.50			51.86	0.00	298.03	1301.50	0.1452
				SLE Q.P.		0.00			-4455.61			51.08	0.00	293.55	1281.97	0.1419

Da [m]	**A [m]**	**Dx [m]**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**V_{Rcd} [kg]**	**V_{Rd} [kg]**	**Staffe**
Trave 11545 11601 Sez. 2 Rett. 40x40 [cm]							
0.12	0.73	0.61	16704.63	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11601 11603 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	12325.00	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11603 11605 Sez. 2 Rett. 40x40 [cm]							
0.00	0.72	0.72	7220.24	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11605 11607 Sez. 2 Rett. 40x40 [cm]							
0.00	0.74	0.74	2253.87	8810.34	37247.76	36621.00	ø 10 2br. 12.5'
Trave 11607 11609 Sez. 2 Rett. 40x40 [cm]							
0.00	0.69	0.69	6229.71	8810.34	37247.76	36621.00	ø 10 2br. 12.5'

Travata: *Travata 57 Nodi 2788 103*

Nodo	**x [m]**	**A_{fe} [cm²]**	**A_{fi} [cm²]**	**q_T [kg/m]**	**M_{rif} [kgm]**	**M_{de} [kgm]**	**M_{re} [kgm]**	**x/d**	**M_{di} [kgm]**	**M_{ri} [kgm]**	**x/d**	**σ_{be} [kg/cm²]**	**σ_{bi} [kg/cm²]**	**σ_{fe} [kg/cm²]**	**σ_{fi} [kg/cm²]**	**w mm**
Trave Sez. 1 Rett. 40x40 [cm]																
2788	0.13	6.03	6.03			3084.74	7803.06	0.15	-513.14	-7803.06	0.15					
				SLE Rare		942.10			0.00			0.00	13.42	510.90	80.56	
				SLE Freq.		894.54			0.00			0.00	12.75	485.11	76.50	0.0083
				SLE Q.P.		877.22			0.00			0.00	12.50	475.72	75.02	0.0081

Camp.	1.77	6.03	6.03	520.00	409.58	522.93	7803.06	0.15	-1146.62	-7803.06	0.15					
				SLE Rare		0.00			-582.93			8.31	0.00	49.85	316.12	
				SLE Freq.		0.00			-567.54			8.09	0.00	48.53	307.78	0.0334
				SLE Q.P.		0.00			-562.51			8.02	0.00	48.10	305.05	0.0331
103	3.42	4.12	5.68			91.19	5628.58	0.13	-2350.34	-7381.73	0.14					
				SLE Rare		0.00			-1006.64			15.10	0.00	61.54	543.67	
				SLE Freq.		0.00			-924.89			13.87	0.00	56.54	499.51	0.0558
				SLE Q.P.		0.00			-896.39			13.44	0.00	54.80	484.12	0.0541

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 2788 103 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	2307.00	7037.02	38935.73	63800.94	133.54	5004.46	2832.32	ø 10 2br. 7.5'
0.52	3.03	2.50	2147.00	7037.02	38935.73	38280.56	133.54	5004.46	2832.32	ø 10 2br. 12.5'
3.03	3.42	0.40	1147.00	6895.68	38935.73	63800.94	133.54	5004.46	2299.93	ø 10 2br. 7.5'

Travata: *Travata 6 Nodi 248 7431*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
248	0.13	6.03	6.03			40.98	7803.06	0.15	-2823.28	-7803.06	0.15					
				SLE Rare		0.00			-1765.55			25.16	0.00	150.98	957.46	
				SLE Freq.		0.00			-1723.10			24.55	0.00	147.35	934.44	0.1013
				SLE Q.P.		0.00			-1708.95			24.35	0.00	146.14	926.77	0.1005
Camp.	2.13	6.03	6.03	520.00	587.03	1860.96	7803.06	0.15	-587.03	-7803.06	0.15					
				SLE Rare		558.78			-451.56			6.43	7.96	303.03	244.88	
				SLE Freq.		497.40			-451.56			6.43	7.09	269.74	244.88	0.0266
				SLE Q.P.		476.96			-451.56			6.43	6.80	258.66	244.88	0.0266
7431	4.13	6.03	6.03			6618.10	7803.06	0.15	0.00	-7803.06	0.15					
				SLE Rare		4475.93			0.00			0.00	63.78	2427.31	382.76	
				SLE Freq.		4282.52			0.00			0.00	61.02	2322.42	366.22	0.0397
				SLE Q.P.		4225.86			0.00			0.00	60.21	2291.70	361.38	0.0392

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 248 7431 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	1524.37	7037.02	38935.73	63800.94	149.81	5004.46	2832.32	ø 10 2br. 7.5'
0.52	3.72	3.20	3188.37	7037.02	38935.73	38280.56	149.81	5004.46	2832.32	ø 10 2br. 12.5'
3.72	4.13	0.40	3396.37	7037.02	38935.73	63800.94	149.81	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 61 Nodi 2808 108*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
2808	0.13	6.03	6.03			1969.20	7803.06	0.15	-1296.96	-7803.06	0.15					
				SLE Rare		0.00			-248.25			3.54	0.00	21.23	134.62	
				SLE Freq.		0.00			-193.61			2.76	0.00	16.56	104.99	0.0114
				SLE Q.P.		0.00			-175.40			2.50	0.00	15.00	95.12	0.0103
Camp.	1.77	6.03	6.03	520.00	409.58	237.03	7803.06	0.15	-881.87	-7803.06	0.15					
				SLE Rare		0.00			-547.93			7.81	0.00	46.86	297.14	
				SLE Freq.		0.00			-532.66			7.59	0.00	45.55	288.86	0.0313
				SLE Q.P.		0.00			-527.63			7.52	0.00	45.12	286.13	0.0310
108	3.42	6.03	6.03			1158.55	7803.06	0.15	-1266.83	-7803.06	0.15					
				SLE Rare		263.64			0.00			0.00	3.76	142.97	22.55	
				SLE Freq.		242.09			0.00			0.00	3.45	131.28	20.70	0.0022
				SLE Q.P.		234.90			0.00			0.00	3.35	127.39	20.09	0.0022

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 2808 108 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	1640.61	7037.02	38935.73	63800.94	453.83	5004.46	2832.32	ø 10 2br. 7.5'
0.52	3.03	2.50	1480.61	7037.02	38935.73	38280.56	453.83	5004.46	2832.32	ø 10 2br. 12.5'
3.03	3.42	0.40	1404.09	7037.02	38935.73	63800.94	453.83	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 66 Nodi 5866 208*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
5866	0.13	6.03	6.03			5650.66	7803.06	0.15	0.00	-7803.06	0.15					
				SLE Rare		3851.34			0.00			0.00	54.88	2088.59	329.35	
				SLE Freq.		3682.88			0.00			0.00	52.48	1997.24	314.95	0.0342
				SLE Q.P.		3626.15			0.00			0.00	51.67	1966.47	310.09	0.0336
Camp.	1.77	6.03	6.03	520.00	409.58	1481.46	7803.06	0.15	-798.57	-7803.06	0.15					
				SLE Rare		182.63			-315.06			4.49	2.60	99.04	170.86	
				SLE Freq.		163.66			-315.06			4.49	2.33	88.75	170.86	0.0185
				SLE Q.P.		157.34			-315.06			4.49	2.24	85.32	170.86	0.0185
208	3.42	6.03	6.03			0.00	7803.06	0.15	-3638.38	-7803.06	0.15					
				SLE Rare		0.00			-2401.44			34.22	0.00	205.36	1302.31	
				SLE Freq.		0.00			-2269.20			32.33	0.00	194.05	1230.60	0.1335
				SLE Q.P.		0.00			-2224.47			31.70	0.00	190.23	1206.34	0.1308

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 5866 208 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	3672.86	7037.02	38935.73	63800.94	277.48	5004.46	2832.32	ø 10 2br. 7.5'
0.52	3.03	2.50	3464.86	7037.02	38935.73	38280.56	277.48	5004.46	2832.32	ø 10 2br. 12.5'
3.03	3.42	0.40	2164.86	7037.02	38935.73	63800.94	277.48	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 71 Nodi 8924 308*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 40x40 [cm]																
8924	0.13	6.03	6.03			2067.68	7803.06	0.15	0.00	-7803.06	0.15					
				SLE Rare		1394.50			0.00			0.00	19.87	756.24	119.25	
				SLE Freq.		1348.14			0.00			0.00	19.21	731.10	115.29	0.0125
				SLE Q.P.		1331.88			0.00			0.00	18.98	722.28	113.90	0.0124
Camp.	1.77	6.03	6.03	520.00	407.28	545.33	7803.06	0.15	-407.28	-7803.06	0.15					
				SLE Rare		126.01			-313.29			4.46	1.80	68.33	169.90	
				SLE Freq.		126.41			-313.29			4.46	1.80	68.55	169.90	0.0184
				SLE Q.P.		126.43			-313.29			4.46	1.80	68.56	169.90	0.0184
308	3.41	6.03	6.03			578.67	7803.06	0.15	-273.76	-7803.06	0.15					
				SLE Rare		35.67			-63.18			0.90	0.51	19.35	34.26	
				SLE Freq.		57.62			-23.22			0.33	0.82	31.25	12.59	0.0014
				SLE Q.P.		64.93			-11.66			0.17	0.93	35.21	6.33	0.0007

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 8924 308 Sez. 1 Rett. 40x40 [cm]										
0.13	0.52	0.40	1550.52	7037.02	38935.73	63800.94	532.66	5004.46	2832.32	ø 10 2br. 7.5'
0.52	3.01	2.49	1342.52	7037.02	38935.73	38280.56	532.66	5004.46	2832.32	ø 10 2br. 12.5'
3.01	3.41	0.40	578.68	7037.02	38935.73	63800.94	532.66	5004.46	2832.32	ø 10 2br. 7.5'

Travata: *Travata 8 Nodi 341 9596*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
341	0.13	10.05	8.04			15722.78	16275.79	0.14	0.00	-13229.71	0.13					

				SLE Rare		10859.01			0.00			0.00	80.92	2740.28	694.95	
				SLE Freq.		10825.76			0.00			0.00	80.67	2731.89	692.82	0.0623
				SLE Q.P.		10814.67			0.00			0.00	80.59	2729.09	692.11	0.0623
Camp.	2.13	8.04	8.04	650.00	740.46	6804.99	13228.33	0.13	-740.46	-13228.33	0.13					
				SLE Rare		2714.81			-569.59			4.61	21.97	849.49	178.23	
				SLE Freq.		2855.69			-569.59			4.61	23.11	893.58	183.84	0.0193
				SLE Q.P.		2902.66			-569.59			4.61	23.49	908.27	186.87	0.0196
9596	4.14	8.04	8.04			0.00	13228.33	0.13	-5165.11	-13228.33	0.13					
				SLE Rare		0.00			-3405.74			27.56	0.00	219.25	1065.70	
				SLE Freq.		0.00			-3090.72			25.01	0.00	198.97	967.12	0.1014
				SLE Q.P.		0.00			-2985.71			24.16	0.00	192.21	934.26	0.0980

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 341 9596 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	6460.01	8701.28	50188.84	61680.39	114.40	6941.10	4694.74	ø 10 2br. 10.0'
0.63	3.64	3.02	6135.01	8701.28	50188.84	41120.26	114.40	6941.10	4173.10	ø 10 2br. 15.0'
3.64	4.14	0.50	4172.48	8701.28	50188.84	61680.39	114.40	6941.10	4173.10	ø 10 2br. 10.0'

Travata: *Travata 9 Nodi 348 9810*

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 5 Rett. 40x50 [cm]																
348	0.13	8.04	8.04			9937.26	13228.33	0.13	0.00	-13228.33	0.13					
				SLE Rare		6910.20			0.00			0.00	55.91	2162.28	444.86	
				SLE Freq.		6847.57			0.00			0.00	55.40	2142.68	440.83	0.0462
				SLE Q.P.		6826.69			0.00			0.00	55.23	2136.15	439.49	0.0461
Camp.	2.15	8.04	8.04	650.00	752.90	3698.08	13228.33	0.13	-1057.05	-13228.33	0.13					
				SLE Rare		1246.73			-579.15			4.69	10.09	390.11	181.22	
				SLE Freq.		1394.40			-579.15			4.69	11.28	436.32	181.22	0.0190
				SLE Q.P.		1443.62			-579.15			4.69	11.68	451.73	181.22	0.0190
9810	4.18	8.04	8.04			436.80	13228.33	0.13	-4866.20	-13228.33	0.13					
				SLE Rare		0.00			-2356.97			19.07	0.00	151.74	737.52	
				SLE Freq.		0.00			-1999.00			16.17	0.00	128.69	625.51	0.0656
				SLE Q.P.		0.00			-1879.67			15.21	0.00	121.01	588.17	0.0617

Da [m]	A [m]	Dx [m]	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 348 9810 Sez. 5 Rett. 40x50 [cm]										
0.13	0.63	0.50	4622.67	8701.28	50188.84	61680.39	303.73	6941.10	4173.10	ø 10 2br. 10.0'
0.63	3.68	3.05	4297.67	8701.28	50188.84	41120.26	303.73	6941.10	4173.10	ø 10 2br. 15.0'
3.68	4.18	0.50	2395.15	8701.28	50188.84	61680.39	303.73	6941.10	4173.10	ø 10 2br. 10.0'

Verifiche pilastri

Modalità di verifica
I pilastri vengono verificati (a discrezione dell'utente) secondo una delle seguenti modalità:
Presso-tenso flessione deviata.
Presso-tenso flessione retta. In tale caso viene svolta prima la verifica a presso-tenso flessione considerando come azioni agenti lo sforzo normale ed il momento M_x agente sulla sezione poi, disgiuntamente, considerando come azioni agenti lo sforzo normale e l'altro momento M_y. A discrezione dell'operatore tali momenti (a favore della sicurezza) possono essere incrementati di un fattore di amplificazione anch'esso a discrezione dell'utente.
Le verifiche vengono effettuate nella sezione di sommità e in quella di base in tutte le combinazioni di carico.
Nelle stampe si riportano (per le due sezioni di verifica succitate) le sollecitazioni relative alla combinazione di carico critica. Le sollecitazioni di verifica alle estremità sono valutate ad una ascissa di spunto definita dall'utente.
Sezioni Impiegate:

Sez. Num.	Info	Dimensioni	Criterio	Calcestruzzo	γ_M	F.C.	f_{ck} [kg/cm²]	f_{cd} [kg/cm²]	σ_{RARE} [kg/cm²]	σ_{FREQ} [kg/cm²]	σ_{QP} [kg/cm²]	Acciaio	γ_M	F.C.	f_{yk} [kg/cm²]	f_{yd} [kg/cm²]	σ_{yRARE} [kg/cm²]	σ_{yFREQ} [kg/cm²]	σ_{yQP} [kg/cm²]	Copr. [cm]	Verifica	cotg θ
1	Rett	B 40 [cm]	Verpil	C32/40	1.5	1.0	320.000	181.300	192.000	320.000	144.000	B 450	1.1	1.0	4500.00	3913.00	3600.00	4500.00	4500.00	5.00	Deviata	2.5

	.	H 100 [cm]			0	0						C	5	0	0	0	0	0	0			
2	Rett.	B 100 [cm] H 40 [cm]	Verpil	C32/40	1.50	1.00	320.000	181.300	192.000	320.000	144.000	B 450 C	1.15	1.00	4500.000	3913.000	3600.000	4500.000	4500.000	5.00	Deviata	2.5
5	Rett.	B 30 [cm] H 30 [cm]	Verpil	C32/40	1.50	1.00	320.000	181.300	192.000	320.000	144.000	B 450 C	1.15	1.00	4500.000	3913.000	3600.000	4500.000	4500.000	5.00	Deviata	2.5

Verifiche Pilastri:

N.B. Nella formula (7.4.28) del punto 7.4.6.2.2. TU2008 nel calcolo di A_{st} è stato inclusa l'area totale delle staffe in entrambe le direzioni. La formula (7.4.28) del punto 7.4.6.2.2. TU2008 in "CDB" viene applicata alle sole regioni critiche terminali. Fattore di sovraresistenza $\gamma_{R,d\ (Nuovi)}$=1.10

Pilastro: **1/2752** / L 1.60[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 160.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
1	1	-56045.91	-7566.93	-70.49	0.09
2752	1	-53640.91	-7769.93	-271.31	0.09

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.12	1.73	488.10	86297.23	108.55	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
1	Ft. 16	-36665.68	-5589.88	-41.62	-27.71
	$\sigma_{s,c}$15	-38854.57	-5598.85	-45.77	-220.69
	$\sigma_{cls,Max}$15	-38854.57	-5598.85	-45.77	-15.76
	$\sigma_{cls,Med}$15	-38854.57	-5598.85	-45.77	-8.51
2752	Ft. 16	-34815.68	-5359.30	-181.56	-20.95
	$\sigma_{s,c}$15	-37004.57	-5511.83	-190.04	-217.78
	$\sigma_{cls,Max}$15	-37004.57	-5511.83	-190.04	-15.71
	$\sigma_{cls,Med}$15	-37004.57	-5511.83	-190.04	-8.11
Combinazioni Frequenti					
1	Ft. 19	-35595.24	-5598.70	-38.58	-24.14
	$\sigma_{s,c}$18	-36313.12	-5602.10	-39.91	-212.21
	$\sigma_{cls,Max}$18	-36313.12	-5602.10	-39.91	-15.19
	$\sigma_{cls,Med}$18	-36313.12	-5602.10	-39.91	-7.95
2752	Ft. 19	-33745.24	-5267.49	-177.67	-19.06
	$\sigma_{s,c}$18	-34463.12	-5316.92	-180.47	-205.94
	$\sigma_{cls,Max}$18	-34463.12	-5316.92	-180.47	-14.88
	$\sigma_{cls,Med}$18	-34463.12	-5316.92	-180.47	-7.55
Combinazioni Quasi Permanenti					
1	Ft. 21	-35524.73	-5601.14	-38.24	-23.88
	$\sigma_{s,c}$21	-35524.73	-5601.14	-38.24	-209.55
	$\sigma_{cls,Max}$21	-35524.73	-5601.14	-38.24	-15.01
	$\sigma_{cls,Med}$21	-35524.73	-5601.14	-38.24	-7.78
2752	Ft. 21	-33674.73	-5259.02	-177.45	-18.97
	$\sigma_{s,c}$21	-33674.73	-5259.02	-177.45	-202.31
	$\sigma_{cls,Max}$21	-33674.73	-5259.02	-177.45	-14.62
	$\sigma_{cls,Med}$21	-33674.73	-5259.02	-177.45	-7.38

Pilastro: **2752/101** / L 2.25[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 25.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
2752	1	-129173.42	-8269.65	288.16	0.17
101	1	-125923.42	-2549.46	-249.38	0.15

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	2288.07	86297.23	233.31	61956.98	ø 10 2br.x4br./15.0
1.13	1.38	2288.07	64722.92	233.31	46467.73	ø 10 2br.x4br./20.0
1.38	2.38	2288.07	86297.23	233.31	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
2752	Ft. 16	-83675.04	-5559.23	147.88	-179.28
	$\sigma_{s,c}$15	-89006.65	-5776.21	179.93	-392.64
	$\sigma_{cls,Max}$15	-89006.65	-5776.21	179.93	-27.41
	$\sigma_{cls,Med}$15	-89006.65	-5776.21	179.93	-19.50
101	Ft. 16	-81175.04	-1620.45	-144.85	-235.59
	$\sigma_{s,c}$15	-86506.65	-1696.73	-159.80	-317.06
	$\sigma_{cls,Max}$15	-86506.65	-1696.73	-159.80	-21.62
	$\sigma_{cls,Med}$15	-86506.65	-1696.73	-159.80	-18.95
Combinazioni Frequenti					
2752	Ft. 19	-81046.41	-5423.17	134.92	-173.28
	$\sigma_{s,c}$18	-82794.25	-5493.30	145.53	-366.51
	$\sigma_{cls,Max}$18	-82794.25	-5493.30	145.53	-25.58
	$\sigma_{cls,Med}$20	-82804.91	-5423.75	160.72	-18.14
101	Ft. 19	-78546.41	-1536.76	-133.40	-228.69
	$\sigma_{s,c}$20	-80304.91	-1573.19	-147.45	-294.27
	$\sigma_{cls,Max}$20	-80304.91	-1573.19	-147.45	-20.07
	$\sigma_{cls,Med}$20	-80304.91	-1573.19	-147.45	-17.59
Combinazioni Quasi Permanenti					
2752	Ft. 21	-80870.26	-5409.98	134.46	-172.93
	$\sigma_{s,c}$21	-80870.26	-5409.98	134.46	-358.47
	$\sigma_{cls,Max}$21	-80870.26	-5409.98	134.46	-25.01
	$\sigma_{cls,Med}$22	-80879.38	-5351.22	147.46	-17.72
101	Ft. 22	-78379.38	-1535.25	-140.02	-227.95
	$\sigma_{s,c}$22	-78379.38	-1535.25	-140.02	-287.08
	$\sigma_{cls,Max}$22	-78379.38	-1535.25	-140.02	-19.57
	$\sigma_{cls,Med}$22	-78379.38	-1535.25	-140.02	-17.17

Pilastro: **101/201** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
101	1	-94710.27	-361.09	-89.03	0.11
201	1	-90225.27	321.23	182.62	0.11

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	267.39	86297.23	79.38	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	267.39	64722.92	79.38	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	267.39	86297.23	79.38	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
101	Ft. 16	-61983.15	-293.87	-50.43	-197.24
	$\sigma_{s,c}$15	-65391.04	-224.43	-57.51	-220.34
	$\sigma_{cls,Max}$15	-65391.04	-224.43	-57.51	-14.80
	$\sigma_{cls,Med}$15	-65391.04	-224.43	-57.51	-14.32
201	Ft. 16	-58533.15	349.72	134.74	-182.31
	$\sigma_{s,c}$15	-61941.04	259.04	126.19	-211.76
	$\sigma_{cls,Max}$15	-61941.04	259.04	126.19	-14.31
	$\sigma_{cls,Med}$15	-61941.04	259.04	126.19	-13.57
Combinazioni Frequenti					
101	Ft. 19	-59996.95	-258.06	-46.87	-191.41
	$\sigma_{s,c}$20	-61109.92	-240.27	-51.59	-206.35
	$\sigma_{cls,Max}$20	-61109.92	-240.27	-51.59	-13.86
	$\sigma_{cls,Med}$20	-61109.92	-240.27	-51.59	-13.39
201	Ft. 19	-56546.95	342.32	128.60	-176.10
	$\sigma_{s,c}$18	-57653.59	310.79	125.44	-198.50
	$\sigma_{cls,Max}$18	-57653.59	310.79	125.44	-13.43
	$\sigma_{cls,Med}$20	-57659.92	291.24	122.05	-12.63
Combinazioni Quasi Permanenti					
101	Ft. 22	-59826.49	-251.65	-48.62	-190.90
	$\sigma_{s,c}$22	-59826.49	-251.65	-48.62	-202.22
	$\sigma_{cls,Max}$22	-59826.49	-251.65	-48.62	-13.58
	$\sigma_{cls,Med}$22	-59826.49	-251.65	-48.62	-13.10
201	Ft. 21	-56371.04	334.53	126.74	-175.70
	$\sigma_{s,c}$21	-56371.04	334.53	126.74	-194.71
	$\sigma_{cls,Max}$21	-56371.04	334.53	126.74	-13.18
	$\sigma_{cls,Med}$22	-56376.49	318.28	123.78	-12.35

Pilastro: **201/301** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
201	1	-59007.14	2491.64	239.10	0.08
301	2	-52295.00	6297.54	-1921.78	0.09

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1126.29	86297.23	632.92	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	1126.29	64722.92	632.92	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	1126.29	86297.23	632.92	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
201	Ft. 16	-39334.52	1669.10	176.89	-96.31

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-40819.28	1722.31	161.75	-167.43
	$\sigma_{cls,Max}$15	-40819.28	1722.31	161.75	-11.65
	$\sigma_{cls,Med}$15	-40819.28	1722.31	161.75	-8.94
301	Ft. 16	-35884.52	4249.57	-1292.34	-6.57
	$\sigma_{s,c}$16	-35884.52	4249.57	-1292.34	-228.94
	$\sigma_{cls,Max}$16	-35884.52	4249.57	-1292.34	-17.51
	$\sigma_{cls,Med}$15	-37369.28	3954.20	-1224.19	-8.22
Combinazioni Frequenti					
201	Ft. 19	-37989.57	1615.62	166.09	-93.11
	$\sigma_{s,c}$18	-38455.18	1632.13	160.49	-158.15
	$\sigma_{cls,Max}$18	-38455.18	1632.13	160.49	-11.02
	$\sigma_{cls,Med}$20	-38458.46	1616.79	159.30	-8.42
301	Ft. 19	-34539.57	3988.71	-1213.48	-9.18
	$\sigma_{s,c}$19	-34539.57	3988.71	-1213.48	-217.60
	$\sigma_{cls,Max}$19	-34539.57	3988.71	-1213.48	-16.61
	$\sigma_{cls,Med}$20	-35008.46	3873.79	-1189.16	-7.73
Combinazioni Quasi Permanenti					
201	Ft. 21	-37813.70	1608.23	162.81	-92.75
	$\sigma_{s,c}$21	-37813.70	1608.23	162.81	-155.72
	$\sigma_{cls,Max}$21	-37813.70	1608.23	162.81	-10.85
	$\sigma_{cls,Med}$22	-37816.55	1595.58	161.80	-8.28
301	Ft. 21	-34363.70	3914.36	-1192.46	-10.58
	$\sigma_{s,c}$22	-34366.55	3910.95	-1194.12	-215.09
	$\sigma_{cls,Max}$22	-34366.55	3910.95	-1194.12	-16.40
	$\sigma_{cls,Med}$22	-34366.55	3910.95	-1194.12	-7.62

Pilastro: **301/11526** / L 4.05[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 205.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
301	2	-24263.93	8496.06	-2899.40	0.10
11526	2	-18673.93	1268.83	-14413.90	0.51

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1680.75	86297.23	2677.79	61956.98	ø 10 2br.x4br./15.0
1.13	3.18	1680.75	64722.92	2677.79	46467.73	ø 10 2br.x4br./20.0
3.18	4.18	1680.75	86297.23	2677.79	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
301	Ft. 16	-16888.81	5735.44	-1951.51	253.85
	$\sigma_{s,c}$16	-16888.81	5735.44	-1951.51	-271.17
	$\sigma_{cls,Max}$16	-16888.81	5735.44	-1951.51	-23.58
	$\sigma_{cls,Med}$16	-16888.81	5735.44	-1951.51	-7.91
11526	Ft. 16	-12588.81	856.41	-9721.04	1627.37
	$\sigma_{s,c}$16	-12588.81	856.41	-9721.04	-404.23
	$\sigma_{cls,Max}$16	-12588.81	856.41	-9721.04	-62.55
	$\sigma_{cls,Med}$16	-12588.81	856.41	-9721.04	-29.96

Combinazioni Frequenti					
301	Ft. 19	-16172.88	5419.98	-1834.60	234.65
	$\sigma_{s,c}$19	-16172.88	5419.98	-1834.60	-255.42
	$\sigma_{cls,Max}$19	-16172.88	5419.98	-1834.60	-22.16
	$\sigma_{cls,Med}$19	-16172.88	5419.98	-1834.60	-7.44
11526	Ft. 19	-11872.88	808.69	-9170.69	1535.36
	$\sigma_{s,c}$19	-11872.88	808.69	-9170.69	-381.36
	$\sigma_{cls,Max}$19	-11872.88	808.69	-9170.69	-59.01
	$\sigma_{cls,Med}$19	-11872.88	808.69	-9170.69	-28.26
Combinazioni Quasi Permanenti					
301	Ft. 22	-15994.69	5343.21	-1805.52	229.99
	$\sigma_{s,c}$22	-15994.69	5343.21	-1805.52	-251.55
	$\sigma_{cls,Max}$22	-15994.69	5343.21	-1805.52	-21.81
	$\sigma_{cls,Med}$22	-15994.69	5343.21	-1805.52	-7.32
11526	Ft. 22	-11694.69	795.86	-9035.00	1512.67
	$\sigma_{s,c}$22	-11694.69	795.86	-9035.00	-375.67
	$\sigma_{cls,Max}$22	-11694.69	795.86	-9035.00	-58.14
	$\sigma_{cls,Med}$22	-11694.69	795.86	-9035.00	-27.84

Pilastro: **3/103** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
3	1	-205194.16	5428.93	932.88	0.25
103	1	-199539.16	-5044.41	-166.07	0.24

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	5395.94	86297.23	486.28	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	5395.94	64722.92	486.28	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	5395.94	86297.23	486.28	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
3	Ft. 17	-131284.55	3631.70	616.89	-352.31
	$\sigma_{s,c}$15	-144771.75	3615.93	624.88	-554.68
	$\sigma_{cls,Max}$15	-144771.75	3615.93	624.88	-38.33
	$\sigma_{cls,Med}$15	-144771.75	3615.93	624.88	-31.71
103	Ft. 17	-126934.55	-3540.42	-102.42	-355.88
	$\sigma_{s,c}$15	-140421.75	-3603.97	-91.60	-523.22
	$\sigma_{cls,Max}$15	-140421.75	-3603.97	-91.60	-35.63
	$\sigma_{cls,Med}$15	-140421.75	-3603.97	-91.60	-30.76
Combinazioni Frequenti					
3	Ft. 20	-129029.48	3653.12	577.89	-345.79
	$\sigma_{s,c}$18	-138417.27	3471.40	579.51	-529.99
	$\sigma_{cls,Max}$18	-138417.27	3471.40	579.51	-36.61
	$\sigma_{cls,Med}$18	-138417.27	3471.40	579.51	-30.32
103	Ft. 20	-124679.48	-3440.84	-90.41	-350.48
	$\sigma_{s,c}$18	-134067.25	-3413.97	-78.04	-498.81
	$\sigma_{cls,Max}$18	-134067.25	-3413.97	-78.04	-33.95
	$\sigma_{cls,Med}$18	-134067.25	-3413.97	-78.04	-29.37
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
3	Ft. 22	-128277.80	3660.26	564.89	-343.62
	$\sigma_{s,c}$21	-136300.23	3419.84	564.40	-521.71
	$\sigma_{cls,Max}$21	-136300.23	3419.84	564.40	-36.03
	$\sigma_{cls,Med}$21	-136300.23	3419.84	564.40	-29.85
103	Ft. 22	-123927.81	-3407.65	-86.41	-348.68
	$\sigma_{s,c}$21	-131950.23	-3349.83	-73.60	-490.66
	$\sigma_{cls,Max}$21	-131950.23	-3349.83	-73.60	-33.39
	$\sigma_{cls,Med}$21	-131950.23	-3349.83	-73.60	-28.90

Pilastro: **103/203** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
103	1	-168908.78	12914.13	-282.57	0.23
203	1	-164423.78	-676.76	-80.44	0.19

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3977.05	86297.23	136.73	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	3977.05	64722.92	136.73	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	3977.05	86297.23	136.73	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
103	Ft. 17	-104902.09	8799.50	-236.48	-193.20
	$\sigma_{s,c}$15	-118607.50	8847.07	-203.64	-540.88
	$\sigma_{cls,Max}$15	-118607.50	8847.07	-203.64	-37.86
	$\sigma_{cls,Med}$15	-118607.50	8847.07	-203.64	-25.98
203	Ft. 17	-101452.09	-720.75	29.90	-320.58
	$\sigma_{s,c}$15	-115157.50	-586.55	-55.65	-389.72
	$\sigma_{cls,Max}$15	-115157.50	-586.55	-55.65	-26.15
	$\sigma_{cls,Med}$15	-115157.50	-586.55	-55.65	-25.22
Combinazioni Frequenti					
103	Ft. 20	-103734.69	8404.00	-219.80	-196.37
	$\sigma_{s,c}$18	-113309.78	8424.19	-195.17	-516.29
	$\sigma_{cls,Max}$18	-113309.78	8424.19	-195.17	-36.14
	$\sigma_{cls,Med}$18	-113309.78	8424.19	-195.17	-24.82
203	Ft. 20	-100284.69	-645.37	7.80	-318.68
	$\sigma_{s,c}$18	-109859.78	-549.28	-61.11	-371.88
	$\sigma_{cls,Max}$18	-109859.78	-549.28	-61.11	-24.96
	$\sigma_{cls,Med}$18	-109859.78	-549.28	-61.11	-24.06
Combinazioni Quasi Permanenti					
103	Ft. 22	-103345.55	8272.17	-214.24	-197.42
	$\sigma_{s,c}$21	-111544.40	8282.35	-192.62	-508.08
	$\sigma_{cls,Max}$21	-111544.40	8282.35	-192.62	-35.56
	$\sigma_{cls,Med}$21	-111544.40	8282.35	-192.62	-24.43
203	Ft. 22	-99895.55	-620.24	0.44	-318.05
	$\sigma_{s,c}$21	-108094.40	-535.95	-62.70	-365.91
	$\sigma_{cls,Max}$21	-108094.40	-535.95	-62.70	-24.56

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-108094.40	-535.95	-62.70	-23.68

Pilastro: **203/303** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
203	1	-136432.98	25764.36	-169.67	0.25
303	1	-131947.98	-62250.62	21.56	0.50

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	25511.59	86297.23	588.19	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	25511.59	64722.92	588.19	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	25511.59	86297.23	588.19	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
203	Ft. 17	-81123.62	17298.68	-88.46	31.99
	$\sigma_{s,c}$15	-95171.22	17679.37	-150.95	-607.44
	$\sigma_{cls,Max}$15	-95171.22	17679.37	-150.95	-43.82
	$\sigma_{cls,Med}$15	-95171.22	17679.37	-150.95	-21.66
303	Ft. 17	-77673.62	-40965.40	-138.12	1428.40
	$\sigma_{s,c}$15	-91721.22	-42706.96	80.21	-1213.34
	$\sigma_{cls,Max}$15	-91721.22	-42706.96	80.21	-94.40
	$\sigma_{cls,Med}$15	-91721.22	-42706.96	80.21	-46.97
Combinazioni Frequenti					
203	Ft. 20	-80966.55	16693.48	-112.26	19.27
	$\sigma_{s,c}$18	-90836.41	16854.90	-169.18	-580.27
	$\sigma_{cls,Max}$18	-90836.41	16854.90	-169.18	-41.89
	$\sigma_{cls,Med}$18	-90836.41	16854.90	-169.18	-20.66
303	Ft. 20	-77516.55	-40312.05	-64.32	1377.26
	$\sigma_{s,c}$18	-87386.41	-41183.44	130.69	-1172.52
	$\sigma_{cls,Max}$18	-87386.41	-41183.44	130.69	-91.43
	$\sigma_{cls,Med}$18	-87386.41	-41183.44	130.69	-45.33
Combinazioni Quasi Permanenti					
203	Ft. 22	-80914.18	16491.74	-120.19	15.22
	$\sigma_{s,c}$21	-89391.63	16579.57	-175.25	-571.20
	$\sigma_{cls,Max}$21	-89391.63	16579.57	-175.25	-41.24
	$\sigma_{cls,Med}$21	-89391.63	16579.57	-175.25	-20.33
303	Ft. 22	-77464.18	-40094.28	-39.72	1360.29
	$\sigma_{s,c}$21	-85941.63	-40673.18	147.79	-1158.87
	$\sigma_{cls,Max}$21	-85941.63	-40673.18	147.79	-90.43
	$\sigma_{cls,Med}$21	-85941.63	-40673.18	147.79	-44.78

Pilastro: **4/104** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
4	1	-198690.97	7956.59	1004.22	0.25

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
104	1	-193035.97	-5413.84	-507.52	0.24

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	6597.25	86297.23	543.60	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	6597.25	64722.92	543.60	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	6597.25	86297.23	543.60	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
4	Ft. 17	-126944.55	5377.00	669.00	-307.84
	$\sigma_{s,c}$15	-140099.03	5352.00	681.32	-569.52
	$\sigma_{cls,Max}$15	-140099.03	5352.00	681.32	-39.70
	$\sigma_{cls,Med}$15	-140099.03	5352.00	681.32	-30.69
104	Ft. 17	-122594.55	-3776.19	-330.56	-330.50
	$\sigma_{s,c}$15	-135749.03	-3842.04	-341.96	-519.73
	$\sigma_{cls,Max}$15	-135749.03	-3842.04	-341.96	-35.72
	$\sigma_{cls,Med}$15	-135749.03	-3842.04	-341.96	-29.73
Combinazioni Frequenti					
4	Ft. 20	-124681.88	5336.99	620.25	-302.62
	$\sigma_{s,c}$18	-133873.91	5149.55	631.60	-544.17
	$\sigma_{cls,Max}$18	-133873.91	5149.55	631.60	-37.91
	$\sigma_{cls,Med}$18	-133873.91	5149.55	631.60	-29.32
104	Ft. 20	-120331.88	-3672.57	-307.24	-325.51
	$\sigma_{s,c}$18	-129523.88	-3647.22	-318.59	-495.35
	$\sigma_{cls,Max}$18	-129523.88	-3647.22	-318.59	-34.03
	$\sigma_{cls,Med}$18	-129523.88	-3647.22	-318.59	-28.37
Combinazioni Quasi Permanenti					
4	Ft. 22	-123927.66	5323.66	603.99	-300.87
	$\sigma_{s,c}$21	-131799.38	5079.70	615.07	-535.69
	$\sigma_{cls,Max}$21	-131799.38	5079.70	615.07	-37.32
	$\sigma_{cls,Med}$21	-131799.38	5079.70	615.07	-28.87
104	Ft. 22	-119577.66	-3638.03	-299.47	-323.84
	$\sigma_{s,c}$21	-127449.38	-3581.85	-310.89	-487.22
	$\sigma_{cls,Max}$21	-127449.38	-3581.85	-310.89	-33.47
	$\sigma_{cls,Med}$21	-127449.38	-3581.85	-310.89	-27.92

Pilastro: **104/204** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
104	1	-163753.84	13268.65	-24.85	0.23
204	1	-159268.84	-783.90	-336.96	0.19

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4113.79	86297.23	132.88	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	4113.79	64722.92	132.88	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	4113.79	86297.23	132.88	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
104	Ft. 17	-101554.31	9045.18	-14.40	-185.25
	$\sigma_{s,c}$15	-114890.45	9090.00	-11.12	-526.51
	$\sigma_{cls,Max}$15	-114890.45	9090.00	-11.12	-36.73
	$\sigma_{cls,Med}$15	-114890.45	9090.00	-11.12	-25.16
204	Ft. 17	-98104.31	-806.36	-244.95	-301.34
	$\sigma_{s,c}$15	-111440.45	-668.18	-233.42	-384.50
	$\sigma_{cls,Max}$15	-111440.45	-668.18	-233.42	-26.02
	$\sigma_{cls,Med}$15	-111440.45	-668.18	-233.42	-24.41
Combinazioni Frequenti					
104	Ft. 20	-100327.93	8639.43	-16.99	-187.77
	$\sigma_{s,c}$18	-109678.24	8659.47	-13.16	-502.41
	$\sigma_{cls,Max}$18	-109678.24	8659.47	-13.16	-35.05
	$\sigma_{cls,Med}$18	-109678.24	8659.47	-13.16	-24.02
204	Ft. 20	-96877.93	-738.93	-238.59	-298.62
	$\sigma_{s,c}$18	-106228.24	-640.79	-224.30	-366.63
	$\sigma_{cls,Max}$18	-106228.24	-640.79	-224.30	-24.81
	$\sigma_{cls,Med}$18	-106228.24	-640.79	-224.30	-23.27
Combinazioni Quasi Permanenti					
104	Ft. 22	-99919.14	8504.18	-17.85	-188.62
	$\sigma_{s,c}$21	-107940.93	8515.11	-13.95	-494.37
	$\sigma_{cls,Max}$21	-107940.93	8515.11	-13.95	-34.49
	$\sigma_{cls,Med}$21	-107940.93	8515.11	-13.95	-23.64
204	Ft. 22	-96469.14	-716.46	-236.46	-297.71
	$\sigma_{s,c}$21	-104490.93	-630.81	-221.17	-360.66
	$\sigma_{cls,Max}$21	-104490.93	-630.81	-221.17	-24.41
	$\sigma_{cls,Med}$21	-104490.93	-630.81	-221.17	-22.89

Pilastro: **204/304** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
204	1	-132132.05	26592.94	-137.48	0.25
304	3	-107227.00	-61632.93	188.85	0.53

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	26301.84	86297.23	394.94	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	26301.84	64722.92	394.94	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	26301.84	86297.23	394.94	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
204	Ft. 17	-78448.80	17826.46	-114.80	60.56
	$\sigma_{s,c}$15	-92062.16	18222.61	-95.04	-605.91
	$\sigma_{cls,Max}$15	-92062.16	18222.61	-95.04	-43.78
	$\sigma_{cls,Med}$15	-92062.16	18222.61	-95.04	-21.73
304	Ft. 17	-74998.80	-42310.09	122.21	1592.87
	$\sigma_{s,c}$15	-88612.16	-43987.08	21.34	-1242.69
	$\sigma_{cls,Max}$15	-88612.16	-43987.08	21.34	-97.28

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-88612.16	-43987.08	21.34	-48.58
Combinazioni Frequenti					
204	Ft. 20	-78189.70	17189.99	-132.65	45.55
	$\sigma_{s,c}$18	-87785.55	17363.69	-106.34	-578.07
	$\sigma_{cls,Max}$18	-87785.55	17363.69	-106.34	-41.79
	$\sigma_{cls,Med}$18	-87785.55	17363.69	-106.34	-20.71
304	Ft. 20	-74739.70	-41568.46	163.82	1543.31
	$\sigma_{s,c}$18	-84335.55	-42397.26	50.50	-1198.86
	$\sigma_{cls,Max}$18	-84335.55	-42397.26	50.50	-94.03
	$\sigma_{cls,Med}$18	-84335.55	-42397.26	50.50	-46.86
Combinazioni Quasi Permanenti					
204	Ft. 22	-78103.35	16977.84	-138.60	40.77
	$\sigma_{s,c}$21	-86359.85	17077.13	-110.06	-568.78
	$\sigma_{cls,Max}$21	-86359.85	17077.13	-110.06	-41.12
	$\sigma_{cls,Med}$21	-86359.85	17077.13	-110.06	-20.37
304	Ft. 22	-74653.35	-41321.25	177.69	1526.83
	$\sigma_{s,c}$21	-82909.85	-41865.45	60.19	-1184.19
	$\sigma_{cls,Max}$22	-74653.35	-41321.25	177.69	-92.98
	$\sigma_{cls,Med}$21	-82909.85	-41865.45	60.19	-46.28

Pilastro: **5/105** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
5	1	-200486.84	9341.96	1226.13	0.26
105	1	-194831.84	-6206.06	-671.36	0.24

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	7184.53	86297.23	520.02	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	7184.53	64722.92	520.02	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	7184.53	86297.23	520.02	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
5	Ft. 17	-127543.62	5843.88	821.64	-297.32
	$\sigma_{s,c}$15	-141367.73	6284.39	830.04	-593.67
	$\sigma_{cls,Max}$15	-141367.73	6284.39	830.04	-41.64
	$\sigma_{cls,Med}$15	-141367.73	6284.39	830.04	-30.96
105	Ft. 17	-123193.62	-4112.18	-449.64	-323.19
	$\sigma_{s,c}$15	-137017.73	-4370.73	-453.39	-536.09
	$\sigma_{cls,Max}$15	-137017.73	-4370.73	-453.39	-37.03
	$\sigma_{cls,Med}$15	-137017.73	-4370.73	-453.39	-30.01
Combinazioni Frequenti					
5	Ft. 20	-125279.05	5784.07	764.62	-292.67
	$\sigma_{s,c}$18	-135111.11	6060.80	771.06	-567.58
	$\sigma_{cls,Max}$18	-135111.11	6060.80	771.06	-39.79
	$\sigma_{cls,Med}$18	-135111.11	6060.80	771.06	-29.59
105	Ft. 20	-120929.05	-4004.50	-422.15	-318.38

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-130761.11	-4170.19	-424.14	-511.32
	$\sigma_{cls,Max}$18	-130761.11	-4170.19	-424.14	-35.31
	$\sigma_{cls,Med}$18	-130761.11	-4170.19	-424.14	-28.64
Combinazioni Quasi Permanenti					
5	Ft. 22	-124524.20	5764.14	745.61	-291.12
	$\sigma_{s,c}$21	-133025.53	5983.98	751.39	-558.84
	$\sigma_{cls,Max}$21	-133025.53	5983.98	751.39	-39.18
	$\sigma_{cls,Med}$21	-133025.53	5983.98	751.39	-29.14
105	Ft. 22	-120174.20	-3968.61	-412.99	-316.78
	$\sigma_{s,c}$21	-128675.54	-4102.91	-414.38	-503.06
	$\sigma_{cls,Max}$21	-128675.54	-4102.91	-414.38	-34.74
	$\sigma_{cls,Med}$21	-128675.54	-4102.91	-414.38	-28.18

Pilastro: **105/205** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
105	1	-165555.42	12987.47	8.42	0.23
205	1	-161070.42	-1351.36	-393.03	0.19

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4170.42	86297.23	133.64	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	4170.42	64722.92	133.64	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	4170.42	86297.23	133.64	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
105	Ft. 17	-102250.45	8822.25	-2.56	-191.56
	$\sigma_{s,c}$15	-116164.18	8910.88	8.04	-527.67
	$\sigma_{cls,Max}$15	-116164.18	8910.88	8.04	-36.77
	$\sigma_{cls,Med}$15	-116164.18	8910.88	8.04	-25.44
205	Ft. 17	-98800.45	-1174.82	-239.85	-297.76
	$\sigma_{s,c}$15	-112714.18	-1053.44	-267.40	-396.06
	$\sigma_{cls,Max}$15	-112714.18	-1053.44	-267.40	-26.90
	$\sigma_{cls,Med}$15	-112714.18	-1053.44	-267.40	-24.69
Combinazioni Frequenti					
105	Ft. 20	-101026.79	8411.31	-8.10	-194.08
	$\sigma_{s,c}$18	-110924.20	8476.29	2.69	-503.18
	$\sigma_{cls,Max}$18	-110924.20	8476.29	2.69	-35.05
	$\sigma_{cls,Med}$18	-110924.20	8476.29	2.69	-24.30
205	Ft. 20	-97576.79	-1082.33	-226.99	-295.67
	$\sigma_{s,c}$18	-107474.20	-1000.20	-252.51	-377.50
	$\sigma_{cls,Max}$18	-107474.20	-1000.20	-252.51	-25.63
	$\sigma_{cls,Med}$18	-107474.20	-1000.20	-252.51	-23.54
Combinazioni Quasi Permanenti					
105	Ft. 22	-100618.90	8274.33	-9.94	-194.93
	$\sigma_{s,c}$21	-109177.15	8330.63	0.88	-495.00
	$\sigma_{cls,Max}$21	-109177.15	8330.63	0.88	-34.48

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-109177.15	8330.63	0.88	-23.91
205	Ft. 22	-97168.90	-1051.50	-222.71	-294.97
	$\sigma_{s,c}$21	-105727.15	-981.74	-247.59	-371.30
	$\sigma_{cls,Max}$21	-105727.15	-981.74	-247.59	-25.21
	$\sigma_{cls,Med}$21	-105727.15	-981.74	-247.59	-23.16

Pilastro: **205/305** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
205	1	-133815.16	26141.15	-3.69	0.25
305	1	-129330.13	-63748.16	-422.31	0.52

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	26054.87	86297.23	484.01	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	26054.87	64722.92	484.01	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	26054.87	86297.23	484.01	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
205	Ft. 17	-79217.19	17250.48	13.31	37.53
	$\sigma_{s,c}$15	-93259.50	17924.24	-1.11	-600.92
	$\sigma_{cls,Max}$15	-93259.50	17924.24	-1.11	-43.27
	$\sigma_{cls,Med}$15	-93259.50	17924.24	-1.11	-21.63
305	Ft. 17	-75767.19	-41142.17	-335.14	1497.27
	$\sigma_{s,c}$15	-89809.50	-43731.59	-289.06	-1252.13
	$\sigma_{cls,Max}$15	-89809.50	-43731.59	-289.06	-98.20
	$\sigma_{cls,Med}$15	-89809.50	-43731.59	-289.06	-48.24
Combinazioni Frequenti					
205	Ft. 20	-78962.52	16632.85	-0.86	23.19
	$\sigma_{s,c}$18	-88956.03	17085.08	-13.49	-573.39
	$\sigma_{cls,Max}$18	-88956.03	17085.08	-13.49	-41.30
	$\sigma_{cls,Med}$18	-88956.03	17085.08	-13.49	-20.63
305	Ft. 20	-75512.52	-40417.69	-290.11	1443.98
	$\sigma_{s,c}$18	-85506.03	-42168.82	-248.25	-1205.02
	$\sigma_{cls,Max}$18	-85506.03	-42168.82	-248.25	-94.59
	$\sigma_{cls,Med}$18	-85506.03	-42168.82	-248.25	-46.55
Combinazioni Quasi Permanenti					
205	Ft. 22	-78877.63	16426.97	-5.58	18.92
	$\sigma_{s,c}$21	-87520.94	16804.99	-17.73	-564.21
	$\sigma_{cls,Max}$21	-87520.94	16804.99	-17.73	-40.64
	$\sigma_{cls,Med}$21	-87520.94	16804.99	-17.73	-20.29
305	Ft. 22	-75427.63	-40176.20	-275.09	1426.28
	$\sigma_{s,c}$21	-84070.94	-41646.05	-234.45	-1189.24
	$\sigma_{cls,Max}$21	-84070.94	-41646.05	-234.45	-93.39
	$\sigma_{cls,Med}$21	-84070.94	-41646.05	-234.45	-45.99

Pilastro: **7/107** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
7	1	-210035.19	5961.96	1251.52	0.26
107	1	-204380.19	-5188.80	-813.79	0.25

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	6710.36	86297.23	479.29	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	6710.36	64722.92	479.29	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	6710.36	86297.23	479.29	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
7	Ft. 17	-133980.41	3540.97	856.21	-355.04
	$\sigma_{s,c}$15	-148106.39	3961.08	846.61	-578.33
	$\sigma_{cls,Max}$15	-148106.39	3961.08	846.61	-40.23
	$\sigma_{cls,Med}$15	-148106.39	3961.08	846.61	-32.44
107	Ft. 17	-129630.39	-3432.73	-562.51	-351.86
	$\sigma_{s,c}$15	-143756.39	-3681.38	-559.06	-550.32
	$\sigma_{cls,Max}$15	-143756.39	-3681.38	-559.06	-37.98
	$\sigma_{cls,Med}$15	-143756.39	-3681.38	-559.06	-31.49
Combinazioni Frequenti					
7	Ft. 20	-131647.36	3524.53	793.08	-349.65
	$\sigma_{s,c}$18	-141613.06	3808.76	785.17	-552.55
	$\sigma_{cls,Max}$18	-141613.06	3808.76	785.17	-38.41
	$\sigma_{cls,Med}$18	-141613.06	3808.76	785.17	-31.02
107	Ft. 20	-127297.38	-3338.09	-528.86	-346.81
	$\sigma_{s,c}$18	-137263.08	-3506.90	-525.22	-525.05
	$\sigma_{cls,Max}$18	-137263.08	-3506.90	-525.22	-36.23
	$\sigma_{cls,Med}$18	-137263.08	-3506.90	-525.22	-30.07
Combinazioni Quasi Permanenti					
7	Ft. 22	-130869.72	3519.05	772.03	-347.85
	$\sigma_{s,c}$21	-139447.44	3755.41	764.69	-543.91
	$\sigma_{cls,Max}$21	-139447.44	3755.41	764.69	-37.80
	$\sigma_{cls,Med}$21	-139447.44	3755.41	764.69	-30.54
107	Ft. 22	-126519.70	-3306.55	-517.64	-345.13
	$\sigma_{s,c}$21	-135097.44	-3448.14	-513.92	-516.62
	$\sigma_{cls,Max}$21	-135097.44	-3448.14	-513.92	-35.64
	$\sigma_{cls,Med}$21	-135097.44	-3448.14	-513.92	-29.59

Pilastro: **107/207** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
107	1	-173761.88	13142.01	354.54	0.24
207	1	-169276.88	-2186.35	-787.90	0.20

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4446.81	86297.23	344.79	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	4446.81	64722.92	344.79	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	4446.81	86297.23	344.79	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
107	Ft. 17	-107697.20	8924.68	270.23	-199.26
	$\sigma_{s,c}$15	-121947.53	9025.72	255.37	-556.42
	$\sigma_{cls,Max}$15	-121947.53	9025.72	255.37	-38.99
	$\sigma_{cls,Med}$15	-121947.53	9025.72	255.37	-26.71
207	Ft. 17	-104247.20	-1722.22	-558.12	-296.58
	$\sigma_{s,c}$15	-118497.53	-1612.42	-541.58	-432.93
	$\sigma_{cls,Max}$15	-118497.53	-1612.42	-541.58	-29.77
	$\sigma_{cls,Med}$15	-118497.53	-1612.42	-541.58	-25.96
Combinazioni Frequenti					
107	Ft. 20	-106468.72	8503.90	248.52	-202.80
	$\sigma_{s,c}$18	-116522.58	8576.77	237.82	-530.69
	$\sigma_{cls,Max}$18	-116522.58	8576.77	237.82	-37.17
	$\sigma_{cls,Med}$18	-116522.58	8576.77	237.82	-25.52
207	Ft. 20	-103018.72	-1574.67	-523.48	-296.06
	$\sigma_{s,c}$18	-113072.58	-1498.52	-511.13	-412.27
	$\sigma_{cls,Max}$18	-113072.58	-1498.52	-511.13	-28.33
	$\sigma_{cls,Med}$18	-113072.58	-1498.52	-511.13	-24.77
Combinazioni Quasi Permanenti					
107	Ft. 22	-106059.23	8363.64	241.29	-203.98
	$\sigma_{s,c}$21	-114712.45	8426.42	232.07	-522.10
	$\sigma_{cls,Max}$21	-114712.45	8426.42	232.07	-36.57
	$\sigma_{cls,Med}$21	-114712.45	8426.42	232.07	-25.13
207	Ft. 22	-102609.23	-1525.49	-511.94	-295.89
	$\sigma_{s,c}$21	-111262.45	-1459.99	-501.13	-405.38
	$\sigma_{cls,Max}$21	-111262.45	-1459.99	-501.13	-27.86
	$\sigma_{cls,Med}$21	-111262.45	-1459.99	-501.13	-24.37

Pilastro: **207/307** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
207	1	-141040.05	24301.53	84.75	0.25
307	1	-136555.05	-59031.20	-336.63	0.47

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	24154.42	86297.23	496.79	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	24154.42	64722.92	496.79	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	24154.42	86297.23	496.79	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
207	Ft. 17	-83912.56	16039.07	87.69	-7.89

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-98333.57	16701.99	77.48	-598.74
	$\sigma_{cls,Max}$15	-98333.57	16701.99	77.48	-42.97
	$\sigma_{cls,Med}$15	-98333.57	16701.99	77.48	-21.54
307	Ft. 17	-80462.56	-37977.70	-260.96	1150.65
	$\sigma_{s,c}$15	-94883.57	-40558.13	-258.59	-1166.40
	$\sigma_{cls,Max}$15	-94883.57	-40558.13	-258.59	-90.15
	$\sigma_{cls,Med}$15	-94883.57	-40558.13	-258.59	-44.36
Combinazioni Frequenti					
207	Ft. 20	-83709.47	15487.17	74.92	-18.14
	$\sigma_{s,c}$18	-93885.60	15945.73	65.55	-571.37
	$\sigma_{cls,Max}$18	-93885.60	15945.73	65.55	-41.00
	$\sigma_{cls,Med}$18	-93885.60	15945.73	65.55	-20.56
307	Ft. 20	-80259.47	-37377.05	-227.21	1108.80
	$\sigma_{s,c}$18	-90435.60	-39162.97	-224.83	-1124.35
	$\sigma_{cls,Max}$18	-90435.60	-39162.97	-224.83	-86.99
	$\sigma_{cls,Med}$18	-90435.60	-39162.97	-224.83	-42.87
Combinazioni Quasi Permanenti					
207	Ft. 22	-83641.78	15303.20	70.66	-21.42
	$\sigma_{s,c}$21	-92400.70	15693.17	61.46	-562.23
	$\sigma_{cls,Max}$21	-92400.70	15693.17	61.46	-40.34
	$\sigma_{cls,Med}$21	-92400.70	15693.17	61.46	-20.24
307	Ft. 22	-80191.78	-37176.84	-215.96	1094.92
	$\sigma_{s,c}$21	-88950.70	-38696.68	-213.44	-1110.29
	$\sigma_{cls,Max}$21	-88950.70	-38696.68	-213.44	-85.93
	$\sigma_{cls,Med}$21	-88950.70	-38696.68	-213.44	-42.37

Pilastro: **8/108** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
8	1	-151707.09	709.11	1936.88	0.19
108	1	-146052.09	-2944.67	1488.17	0.18

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4395.76	86297.23	383.77	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	4395.76	64722.92	383.77	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	4395.76	86297.23	383.77	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
8	Ft. 17	-98749.59	113.15	1427.16	-277.19
	$\sigma_{s,c}$15	-107792.35	312.47	1453.60	-405.51
	$\sigma_{cls,Max}$15	-107792.35	312.47	1453.60	-28.75
	$\sigma_{cls,Med}$15	-107792.35	312.47	1453.60	-23.61
108	Ft. 17	-94399.59	-1943.57	959.88	-247.82
	$\sigma_{s,c}$15	-103442.35	-2109.53	1001.42	-406.23
	$\sigma_{cls,Max}$15	-103442.35	-2109.53	1001.42	-28.60
	$\sigma_{cls,Med}$15	-103442.35	-2109.53	1001.42	-22.66

Combinazioni Frequenti					
8	Ft. 20	-97004.30	129.19	1389.27	-272.40
	$\sigma_{s,c}$18	-103346.41	275.06	1404.23	-388.72
	$\sigma_{cls,Max}$18	-103346.41	275.06	1404.23	-27.57
	$\sigma_{cls,Med}$18	-103346.41	275.06	1404.23	-22.64
108	Ft. 20	-92654.30	-1880.84	903.77	-244.90
	$\sigma_{s,c}$18	-98996.41	-1997.91	935.56	-387.70
	$\sigma_{cls,Max}$18	-98996.41	-1997.91	935.56	-27.27
	$\sigma_{cls,Med}$18	-98996.41	-1997.91	935.56	-21.68
Combinazioni Quasi Permanenti					
8	Ft. 22	-96422.53	134.54	1376.64	-270.80
	$\sigma_{s,c}$21	-101870.65	259.87	1388.97	-383.14
	$\sigma_{cls,Max}$21	-101870.65	259.87	1388.97	-27.17
	$\sigma_{cls,Med}$21	-101870.65	259.87	1388.97	-22.31
108	Ft. 22	-92072.53	-1859.93	885.07	-243.93
	$\sigma_{s,c}$21	-97520.65	-1960.17	912.97	-381.51
	$\sigma_{cls,Max}$21	-97520.65	-1960.17	912.97	-26.82
	$\sigma_{cls,Med}$21	-97520.65	-1960.17	912.97	-21.36

Pilastro: **108/208** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
108	1	-123213.10	9508.06	-5140.20	0.20
208	1	-118728.10	-2728.02	3747.45	0.17

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	3617.08	86297.23	2576.13	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	3617.08	64722.92	2576.13	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	3617.08	86297.23	2576.13	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
108	Ft. 17	-77916.91	6581.29	-3530.11	-35.38
	$\sigma_{s,c}$15	-87121.22	6578.47	-3620.69	-509.05
	$\sigma_{cls,Max}$15	-87121.22	6578.47	-3620.69	-39.24
	$\sigma_{cls,Med}$15	-87121.22	6578.47	-3620.69	-19.11
208	Ft. 17	-74466.91	-2141.58	2660.22	-125.01
	$\sigma_{s,c}$15	-83671.22	-1982.50	2654.00	-391.76
	$\sigma_{cls,Max}$15	-83671.22	-1982.50	2654.00	-29.50
	$\sigma_{cls,Med}$15	-83671.22	-1982.50	2654.00	-18.33
Combinazioni Frequenti					
108	Ft. 20	-76993.01	6261.30	-3376.44	-42.83
	$\sigma_{s,c}$18	-83449.74	6259.64	-3440.22	-486.02
	$\sigma_{cls,Max}$18	-83449.74	6259.64	-3440.22	-37.44
	$\sigma_{cls,Med}$18	-83449.74	6259.64	-3440.22	-18.30
208	Ft. 20	-73543.01	-1977.42	2521.15	-129.08
	$\sigma_{s,c}$18	-79999.74	-1864.78	2516.14	-373.39
	$\sigma_{cls,Max}$18	-79999.74	-1864.78	2516.14	-28.10
	$\sigma_{cls,Med}$18	-79999.74	-1864.78	2516.14	-17.52
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
108	Ft. 22	-76685.04	6154.64	-3325.21	-45.28
	$\sigma_{s,c}$21	-82231.26	6153.23	-3379.67	-478.35
	$\sigma_{cls,Max}$21	-82231.26	6153.23	-3379.67	-36.84
	$\sigma_{cls,Med}$21	-82231.26	6153.23	-3379.67	-18.03
208	Ft. 22	-73235.04	-1922.70	2474.80	-130.44
	$\sigma_{s,c}$21	-78781.26	-1825.72	2469.85	-367.27
	$\sigma_{cls,Max}$21	-78781.26	-1825.72	2469.85	-27.63
	$\sigma_{cls,Med}$21	-78781.26	-1825.72	2469.85	-17.26

Pilastro: **208/308** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
208	1	-98858.44	15332.07	-5298.15	0.20
308	1	-94373.45	-39099.13	7004.54	0.38

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	15783.13	86297.23	3565.98	61956.98	ø 10 2br.x4br./15.0
1.13	2.33	15779.36	64722.92	3565.98	46467.73	ø 10 2br.x4br./20.0
2.33	3.33	15774.84	86297.23	3565.98	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
208	Ft. 17	-59944.38	10107.93	-3341.40	108.17
	$\sigma_{s,c}$15	-69391.53	10557.76	-3641.54	-529.45
	$\sigma_{cls,Max}$15	-69391.53	10557.76	-3641.54	-41.72
	$\sigma_{cls,Med}$15	-69391.53	10557.76	-3641.54	-16.95
308	Ft. 15	-65941.53	-26874.83	4760.48	975.04
	$\sigma_{s,c}$15	-65941.53	-26874.83	4760.48	-1026.64
	$\sigma_{cls,Max}$15	-65941.53	-26874.83	4760.48	-85.87
	$\sigma_{cls,Med}$15	-65941.53	-26874.83	4760.48	-31.54
Combinazioni Frequenti					
208	Ft. 20	-59750.65	9766.46	-3236.33	94.48
	$\sigma_{s,c}$18	-66380.41	10082.71	-3451.68	-504.80
	$\sigma_{cls,Max}$18	-66380.41	10082.71	-3451.68	-39.75
	$\sigma_{cls,Med}$18	-66380.41	10082.71	-3451.68	-16.18
308	Ft. 18	-62930.41	-25966.84	4525.11	951.07
	$\sigma_{s,c}$18	-62930.41	-25966.84	4525.11	-988.47
	$\sigma_{cls,Max}$18	-62930.41	-25966.84	4525.11	-82.70
	$\sigma_{cls,Med}$18	-62930.41	-25966.84	4525.11	-30.43
Combinazioni Quasi Permanenti					
208	Ft. 22	-59686.07	9652.64	-3201.31	90.04
	$\sigma_{s,c}$21	-65381.03	9923.89	-3387.46	-496.55
	$\sigma_{cls,Max}$21	-65381.03	9923.89	-3387.46	-39.09
	$\sigma_{cls,Med}$21	-65381.03	9923.89	-3387.46	-15.93
308	Ft. 21	-61931.03	-25664.06	4444.62	942.84
	$\sigma_{s,c}$21	-61931.03	-25664.06	4444.62	-975.62
	$\sigma_{cls,Max}$21	-61931.03	-25664.06	4444.62	-81.63

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-61931.03	-25664.06	4444.62	-30.06

Pilastro: **9/2751** / L 1.50[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 150.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
9	1	-56952.68	-7976.43	79.80	0.09
2751	1	-54677.68	-8208.12	235.15	0.09

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.63	512.36	86297.23	88.77	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
9	Ft. 16	-37232.60	-5916.79	45.54	-24.10
	$\sigma_{s,c}$15	-39495.04	-5900.86	51.22	-227.91
	$\sigma_{cls,Max}$15	-39495.04	-5900.86	51.22	-16.30
	$\sigma_{cls,Med}$15	-39495.04	-5900.86	51.22	-8.65
2751	Ft. 16	-35482.60	-5689.74	157.61	-18.50
	$\sigma_{s,c}$15	-37745.04	-5832.13	164.13	-224.63
	$\sigma_{cls,Max}$15	-37745.04	-5832.13	164.13	-16.20
	$\sigma_{cls,Med}$15	-37745.04	-5832.13	164.13	-8.27
Combinazioni Frequenti					
9	Ft. 19	-36156.21	-5928.77	41.91	-20.48
	$\sigma_{s,c}$18	-36899.24	-5923.69	43.74	-219.52
	$\sigma_{cls,Max}$18	-36899.24	-5923.69	43.74	-15.74
	$\sigma_{cls,Med}$18	-36899.24	-5923.69	43.74	-8.08
2751	Ft. 19	-34406.21	-5602.64	154.95	-16.47
	$\sigma_{s,c}$18	-35149.24	-5648.74	157.11	-212.88
	$\sigma_{cls,Max}$18	-35149.24	-5648.74	157.11	-15.37
	$\sigma_{cls,Med}$18	-35149.24	-5648.74	157.11	-7.70
Combinazioni Quasi Permanenti					
9	Ft. 21	-36089.54	-5930.14	41.55	-20.25
	$\sigma_{s,c}$21	-36089.54	-5930.14	41.55	-216.89
	$\sigma_{cls,Max}$21	-36089.54	-5930.14	41.55	-15.56
	$\sigma_{cls,Med}$21	-36089.54	-5930.14	41.55	-7.90
2751	Ft. 21	-34339.54	-5594.44	154.85	-16.39
	$\sigma_{s,c}$21	-34339.54	-5594.44	154.85	-209.26
	$\sigma_{cls,Max}$21	-34339.54	-5594.44	154.85	-15.12
	$\sigma_{cls,Med}$21	-34339.54	-5594.44	154.85	-7.52

Pilastro: **2751/109** / L 2.35[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 35.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
2751	1	-127916.02	-8756.68	-486.15	0.17
109	1	-124536.02	-2593.19	289.12	0.15

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2370.57	86297.23	310.60	61956.98	ø 10 2br.x4br./15.0
1.13	1.48	2370.57	64722.92	310.60	46467.73	ø 10 2br.x4br./20.0
1.48	2.48	2370.57	86297.23	310.60	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
2751	Ft. 16	-82807.24	-5928.24	-289.51	-165.89
	$\sigma_{s,c}$15	-88175.63	-6137.15	-327.54	-400.51
	$\sigma_{cls,Max}$15	-88175.63	-6137.15	-327.54	-28.16
	$\sigma_{cls,Med}$15	-88175.63	-6137.15	-327.54	-19.31
109	Ft. 16	-80207.24	-1660.30	173.14	-230.86
	$\sigma_{s,c}$15	-85575.63	-1734.58	189.54	-315.56
	$\sigma_{cls,Max}$15	-85575.63	-1734.58	189.54	-21.56
	$\sigma_{cls,Med}$15	-85575.63	-1734.58	189.54	-18.74
Combinazioni Frequenti					
2751	Ft. 19	-80235.09	-5800.08	-272.02	-160.09
	$\sigma_{s,c}$18	-81997.59	-5867.70	-284.53	-374.43
	$\sigma_{cls,Max}$18	-81997.59	-5867.70	-284.53	-26.33
	$\sigma_{cls,Med}$20	-82010.02	-5785.49	-294.62	-17.96
109	Ft. 19	-77635.09	-1577.60	160.43	-224.16
	$\sigma_{s,c}$20	-79410.02	-1611.63	173.61	-292.79
	$\sigma_{cls,Max}$20	-79410.02	-1611.63	173.61	-20.00
	$\sigma_{cls,Med}$20	-79410.02	-1611.63	173.61	-17.39
Combinazioni Quasi Permanenti					
2751	Ft. 21	-80073.16	-5787.97	-271.02	-159.79
	$\sigma_{s,c}$21	-80073.16	-5787.97	-271.02	-366.38
	$\sigma_{cls,Max}$21	-80073.16	-5787.97	-271.02	-25.76
	$\sigma_{cls,Med}$22	-80083.52	-5719.45	-279.24	-17.54
109	Ft. 22	-77483.52	-1575.07	165.54	-223.54
	$\sigma_{s,c}$22	-77483.52	-1575.07	165.54	-285.60
	$\sigma_{cls,Max}$22	-77483.52	-1575.07	165.54	-19.51
	$\sigma_{cls,Med}$22	-77483.52	-1575.07	165.54	-16.97

Pilastro: **109/209** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
109	1	-93329.19	-419.92	96.38	0.11
209	1	-88844.19	308.31	-159.74	0.10

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	281.87	86297.23	74.32	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	281.87	64722.92	74.32	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	281.87	86297.23	74.32	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
109	Ft. 16	-61021.41	-345.81	54.08	-193.11

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-64465.78	-274.25	62.54	-218.28
	$\sigma_{cls,Max}$15	-64465.78	-274.25	62.54	-14.67
	$\sigma_{cls,Med}$15	-64465.78	-274.25	62.54	-14.12
209	Ft. 16	-57571.41	341.46	-117.39	-179.83
	$\sigma_{s,c}$15	-61015.78	250.21	-108.75	-208.02
	$\sigma_{cls,Max}$15	-61015.78	250.21	-108.75	-14.04
	$\sigma_{cls,Med}$15	-61015.78	250.21	-108.75	-13.36
Combinazioni Frequenti					
109	Ft. 19	-59092.27	-311.58	49.76	-187.47
	$\sigma_{s,c}$20	-60220.99	-290.72	55.25	-204.37
	$\sigma_{cls,Max}$20	-60220.99	-290.72	55.25	-13.74
	$\sigma_{cls,Med}$20	-60220.99	-290.72	55.25	-13.19
209	Ft. 19	-55642.28	336.44	-111.50	-173.76
	$\sigma_{s,c}$18	-56763.48	304.80	-108.32	-194.93
	$\sigma_{cls,Max}$18	-56763.48	304.80	-108.32	-13.17
	$\sigma_{cls,Med}$20	-56771.00	284.38	-106.05	-12.43
Combinazioni Quasi Permanenti					
109	Ft. 22	-58936.95	-303.80	51.67	-187.03
	$\sigma_{s,c}$22	-58936.95	-303.80	51.67	-200.25
	$\sigma_{cls,Max}$22	-58936.95	-303.80	51.67	-13.46
	$\sigma_{cls,Med}$22	-58936.95	-303.80	51.67	-12.91
209	Ft. 21	-55480.70	329.10	-109.69	-173.41
	$\sigma_{s,c}$21	-55480.70	329.10	-109.69	-191.16
	$\sigma_{cls,Max}$21	-55480.70	329.10	-109.69	-12.93
	$\sigma_{cls,Med}$22	-55486.96	312.10	-107.79	-12.15

Pilastro: **209/309** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
209	1	-57636.71	2461.95	-235.13	0.07
309	2	-50869.82	6252.92	1922.77	0.09

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1121.74	86297.23	632.17	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	1121.74	64722.92	632.17	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	1121.74	86297.23	632.17	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
209	Ft. 16	-38381.82	1646.98	-174.21	-93.62
	$\sigma_{s,c}$15	-39903.08	1699.66	-158.81	-163.96
	$\sigma_{cls,Max}$15	-39903.08	1699.66	-158.81	-11.41
	$\sigma_{cls,Med}$15	-39903.08	1699.66	-158.81	-8.74
309	Ft. 16	-34931.82	4221.38	1293.56	-3.62
	$\sigma_{s,c}$16	-34931.82	4221.38	1293.56	-225.54
	$\sigma_{cls,Max}$16	-34931.82	4221.38	1293.56	-17.28
	$\sigma_{cls,Med}$15	-36453.08	3927.55	1225.46	-8.04

Combinazioni Frequenti					
209	Ft. 19	-37094.55	1595.10	-163.67	-90.58
	$\sigma_{s,c}$18	-37574.73	1611.48	-158.00	-154.84
	$\sigma_{cls,Max}$18	-37574.73	1611.48	-158.00	-10.79
	$\sigma_{cls,Med}$20	-37578.64	1596.03	-156.86	-8.23
309	Ft. 19	-33644.55	3963.55	1214.84	-6.42
	$\sigma_{s,c}$19	-33644.55	3963.55	1214.84	-214.40
	$\sigma_{cls,Max}$19	-33644.55	3963.55	1214.84	-16.40
	$\sigma_{cls,Med}$20	-34128.64	3848.71	1190.14	-7.56
Combinazioni Quasi Permanenti					
209	Ft. 21	-36933.13	1588.00	-160.43	-90.27
	$\sigma_{s,c}$21	-36933.13	1588.00	-160.43	-152.42
	$\sigma_{cls,Max}$21	-36933.13	1588.00	-160.43	-10.63
	$\sigma_{cls,Med}$22	-36936.40	1575.13	-159.50	-8.09
309	Ft. 21	-33483.13	3889.94	1193.86	-7.88
	$\sigma_{s,c}$21	-33483.13	3889.94	1193.86	-211.93
	$\sigma_{cls,Max}$21	-33483.13	3889.94	1193.86	-16.19
	$\sigma_{cls,Med}$22	-33486.40	3886.11	1195.12	-7.45

Pilastro: **309/11527** / L 4.05[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 205.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
309	2	-22845.02	8436.50	2886.80	0.10
11527	2	-17255.02	1267.51	14331.44	0.52

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	1667.21	86297.23	2661.54	61956.98	ø 10 2br.x4br./15.0
1.13	3.18	1667.21	64722.92	2661.54	46467.73	ø 10 2br.x4br./20.0
3.18	4.18	1667.21	86297.23	2661.54	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
309	Ft. 16	-15942.36	5694.55	1942.17	269.01
	$\sigma_{s,c}$16	-15942.36	5694.55	1942.17	-270.59
	$\sigma_{cls,Max}$16	-15942.36	5694.55	1942.17	-23.70
	$\sigma_{cls,Med}$16	-15942.36	5694.55	1942.17	-7.92
11527	Ft. 16	-11642.36	856.23	9665.09	1642.51
	$\sigma_{s,c}$16	-11642.36	856.23	9665.09	-397.37
	$\sigma_{cls,Max}$16	-11642.36	856.23	9665.09	-62.24
	$\sigma_{cls,Med}$16	-11642.36	856.23	9665.09	-29.79
Combinazioni Frequenti					
309	Ft. 19	-15284.85	5381.35	1825.22	248.50
	$\sigma_{s,c}$19	-15284.85	5381.35	1825.22	-254.80
	$\sigma_{cls,Max}$19	-15284.85	5381.35	1825.22	-22.26
	$\sigma_{cls,Med}$19	-15284.85	5381.35	1825.22	-7.45
11527	Ft. 19	-10984.85	808.93	9117.73	1549.49
	$\sigma_{s,c}$19	-10984.85	808.93	9117.73	-374.92
	$\sigma_{cls,Max}$19	-10984.85	808.93	9117.73	-58.71
	$\sigma_{cls,Med}$19	-10984.85	808.93	9117.73	-28.11
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
309	Ft. 22	-15121.31	5305.24	1796.42	243.56
	$\sigma_{s,c}$22	-15121.31	5305.24	1796.42	-250.94
	$\sigma_{cls,Max}$22	-15121.31	5305.24	1796.42	-21.90
	$\sigma_{cls,Med}$22	-15121.31	5305.24	1796.42	-7.33
11527	Ft. 22	-10821.31	796.14	8982.83	1526.55
	$\sigma_{s,c}$22	-10821.31	796.14	8982.83	-369.33
	$\sigma_{cls,Max}$22	-10821.31	796.14	8982.83	-57.84
	$\sigma_{cls,Med}$22	-10821.31	796.14	8982.83	-27.69

Pilastro: **10/2768** / L 2.58[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 57.5/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
10	1	-95103.69	-2673.70	-11509.43	0.16
2768	1	-91431.19	-524.81	-6019.57	0.12

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	781.06	61956.98	1943.31	86297.23	ø 10 4br.x2br./15.0
1.13	1.70	781.06	46467.73	1943.31	64722.92	ø 10 4br.x2br./20.0
1.70	2.70	781.06	61956.98	1943.31	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
10	Ft. 16	-61951.40	-1703.45	-8050.78	-17.11
	$\sigma_{s,c}$15	-65789.57	-1825.97	-8258.40	-409.56
	$\sigma_{cls,Max}$15	-65789.57	-1825.97	-8258.40	-30.86
	$\sigma_{cls,Med}$15	-65789.57	-1825.97	-8258.40	-14.53
2768	Ft. 16	-59126.40	-394.33	-4212.34	-112.82
	$\sigma_{s,c}$15	-62964.59	-391.92	-4300.99	-289.69
	$\sigma_{cls,Max}$15	-62964.59	-391.92	-4300.99	-20.52
	$\sigma_{cls,Med}$15	-62964.59	-391.92	-4300.99	-13.79
Combinazioni Frequenti					
10	Ft. 19	-60102.13	-1641.76	-7956.04	-14.45
	$\sigma_{s,c}$18	-61361.88	-1681.88	-8024.37	-386.72
	$\sigma_{cls,Max}$18	-61361.88	-1681.88	-8024.37	-29.14
	$\sigma_{cls,Med}$18	-61361.88	-1681.88	-8024.37	-13.60
2768	Ft. 19	-57277.13	-397.35	-4148.45	-107.69
	$\sigma_{s,c}$18	-58536.88	-396.62	-4176.82	-273.26
	$\sigma_{cls,Max}$18	-58536.88	-396.62	-4176.82	-19.41
	$\sigma_{cls,Med}$18	-58536.88	-396.62	-4176.82	-12.82
Combinazioni Quasi Permanenti					
10	Ft. 21	-59984.23	-1637.45	-7950.76	-14.28
	$\sigma_{s,c}$21	-59984.23	-1637.45	-7950.76	-379.62
	$\sigma_{cls,Max}$21	-59984.23	-1637.45	-7950.76	-28.60
	$\sigma_{cls,Med}$21	-59984.23	-1637.45	-7950.76	-13.31
2768	Ft. 21	-57159.23	-397.80	-4141.34	-107.40
	$\sigma_{s,c}$21	-57159.23	-397.80	-4141.34	-268.19
	$\sigma_{cls,Max}$21	-57159.23	-397.80	-4141.34	-19.07

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-57159.23	-397.80	-4141.34	-12.52

Pilastro: **2768/110** / L 1.28[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 127.5
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
2768	1	-126768.68	1772.09	-3583.22	0.16
110	1	-124786.18	812.47	-1053.33	0.15

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.40	668.72	61956.98	1658.94	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
2768	Ft. 16	-81933.72	1061.78	-2529.80	-194.04
	$\sigma_{s,c}$15	-87289.59	1177.40	-2554.81	-366.04
	$\sigma_{cls,Max}$15	-87289.59	1177.40	-2554.81	-26.20
	$\sigma_{cls,Med}$15	-87289.59	1177.40	-2554.81	-19.12
110	Ft. 16	-80408.72	535.98	-684.78	-235.93
	$\sigma_{s,c}$15	-85764.59	569.22	-688.16	-311.15
	$\sigma_{cls,Max}$15	-85764.59	569.22	-688.16	-21.52
	$\sigma_{cls,Med}$15	-85764.59	569.22	-688.16	-18.79
Combinazioni Frequenti					
2768	Ft. 19	-79365.85	1006.43	-2483.41	-188.12
	$\sigma_{s,c}$20	-81119.88	1070.73	-2440.73	-340.51
	$\sigma_{cls,Max}$20	-81119.88	1070.73	-2440.73	-24.36
	$\sigma_{cls,Med}$18	-81124.16	1044.39	-2490.44	-17.77
110	Ft. 19	-77840.85	524.93	-635.76	-228.65
	$\sigma_{s,c}$20	-79594.88	530.63	-648.05	-288.99
	$\sigma_{cls,Max}$18	-79599.16	536.01	-635.24	-19.99
	$\sigma_{cls,Med}$18	-79599.16	536.01	-635.24	-17.43
Combinazioni Quasi Permanenti					
2768	Ft. 22	-79200.31	1024.51	-2435.49	-187.78
	$\sigma_{s,c}$22	-79200.31	1024.51	-2435.49	-332.64
	$\sigma_{cls,Max}$22	-79200.31	1024.51	-2435.49	-23.78
	$\sigma_{cls,Med}$21	-79203.94	1002.95	-2475.54	-17.35
110	Ft. 22	-77675.31	520.48	-637.11	-228.22
	$\sigma_{s,c}$22	-77675.31	520.48	-637.11	-282.18
	$\sigma_{cls,Max}$21	-77678.94	524.94	-625.86	-19.52
	$\sigma_{cls,Med}$21	-77678.94	524.94	-625.86	-17.01

Pilastro: **110/210** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
110	1	-93543.24	453.46	1117.53	0.11
210	1	-89058.24	162.25	540.37	0.10

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	87.60	61956.98	191.35	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	87.60	46467.73	191.35	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	87.60	61956.98	191.35	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
110	Ft. 16	-61185.00	296.48	642.66	-181.08
	$\sigma_{s,c}$15	-64622.48	314.40	777.65	-235.04
	$\sigma_{cls,Max}$15	-64622.48	314.40	777.65	-16.17
	$\sigma_{cls,Med}$15	-64622.48	314.40	777.65	-14.15
210	Ft. 16	-57735.00	126.61	479.24	-177.82
	$\sigma_{s,c}$15	-61172.48	115.03	403.36	-211.24
	$\sigma_{cls,Max}$15	-61172.48	115.03	403.36	-14.29
	$\sigma_{cls,Med}$15	-61172.48	115.03	403.36	-13.40
Combinazioni Frequenti					
110	Ft. 19	-59256.82	288.24	647.30	-174.93
	$\sigma_{s,c}$18	-60375.67	294.13	694.01	-219.07
	$\sigma_{cls,Max}$18	-60375.67	294.13	694.01	-15.06
	$\sigma_{cls,Med}$18	-60375.67	294.13	694.01	-13.22
210	Ft. 19	-55806.82	122.25	465.43	-171.85
	$\sigma_{s,c}$18	-56925.67	118.10	438.79	-197.96
	$\sigma_{cls,Max}$18	-56925.67	118.10	438.79	-13.41
	$\sigma_{cls,Med}$18	-56925.67	118.10	438.79	-12.47
Combinazioni Quasi Permanenti					
110	Ft. 21	-59094.95	287.77	657.57	-174.25
	$\sigma_{s,c}$21	-59094.95	287.77	657.57	-214.07
	$\sigma_{cls,Max}$21	-59094.95	287.77	657.57	-14.72
	$\sigma_{cls,Med}$21	-59094.95	287.77	657.57	-12.94
210	Ft. 21	-55644.95	120.55	457.34	-171.51
	$\sigma_{s,c}$21	-55644.95	120.55	457.34	-194.14
	$\sigma_{cls,Max}$21	-55644.95	120.55	457.34	-13.16
	$\sigma_{cls,Med}$21	-55644.95	120.55	457.34	-12.19

Pilastro: **210/310** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
210	1	-57792.81	231.35	2804.86	0.08
310	2	-51031.43	-1957.22	6206.98	0.09

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	641.14	61956.98	1014.81	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	641.14	46467.73	1014.81	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	641.14	61956.98	1014.81	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
210	Ft. 16	-38497.20	172.64	1868.83	-90.42
	$\sigma_{s,c}$15	-40014.79	157.08	1934.80	-168.11

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Max}$15	-40014.79	157.08	1934.80	-11.73
	$\sigma_{cls,Med}$15	-40014.79	157.08	1934.80	-8.76
310	Ft. 16	-35047.20	-1316.17	4185.06	-3.88
	$\sigma_{s,c}$16	-35047.20	-1316.17	4185.06	-226.04
	$\sigma_{cls,Max}$16	-35047.20	-1316.17	4185.06	-17.33
	$\sigma_{cls,Med}$15	-36564.79	-1250.06	3889.96	-8.06
Combinazioni Frequenti					
210	Ft. 19	-37208.93	162.24	1809.59	-87.49
	$\sigma_{s,c}$18	-37687.81	156.52	1830.30	-158.74
	$\sigma_{cls,Max}$18	-37687.81	156.52	1830.30	-11.09
	$\sigma_{cls,Med}$18	-37687.81	156.52	1830.30	-8.25
310	Ft. 19	-33758.93	-1236.32	3924.53	-6.76
	$\sigma_{s,c}$19	-33758.93	-1236.32	3924.53	-214.82
	$\sigma_{cls,Max}$19	-33758.93	-1236.32	3924.53	-16.44
	$\sigma_{cls,Med}$18	-34237.81	-1210.77	3813.79	-7.59
Combinazioni Quasi Permanenti					
210	Ft. 21	-37047.05	159.02	1801.88	-87.19
	$\sigma_{s,c}$21	-37047.05	159.02	1801.88	-156.25
	$\sigma_{cls,Max}$21	-37047.05	159.02	1801.88	-10.92
	$\sigma_{cls,Med}$21	-37047.05	159.02	1801.88	-8.11
310	Ft. 22	-33595.17	-1216.45	3848.93	-8.21
	$\sigma_{s,c}$22	-33595.17	-1216.45	3848.93	-212.34
	$\sigma_{cls,Max}$22	-33595.17	-1216.45	3848.93	-16.24
	$\sigma_{cls,Med}$21	-33597.05	-1215.24	3850.28	-7.47

Pilastro: **310/11540** / L 4.05[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 205.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
310	2	-22925.90	-2955.41	8526.16	0.11
11540	2	-17335.90	-14449.27	1228.93	0.52

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2672.99	61956.98	1697.03	86297.23	ø 10 4br.x2br./15.0
1.13	3.18	2672.99	46467.73	1697.03	64722.92	ø 10 4br.x2br./20.0
3.18	4.18	2672.99	61956.98	1697.03	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
310	Ft. 16	-15997.75	-1991.35	5756.69	277.96
	$\sigma_{s,c}$16	-15997.75	-1991.35	5756.69	-275.41
	$\sigma_{cls,Max}$16	-15997.75	-1991.35	5756.69	-24.19
	$\sigma_{cls,Med}$16	-15997.75	-1991.35	5756.69	-8.08
11540	Ft. 16	-11697.75	-9746.57	828.53	1656.11
	$\sigma_{s,c}$16	-11697.75	-9746.57	828.53	-399.08
	$\sigma_{cls,Max}$16	-11697.75	-9746.57	828.53	-62.65
	$\sigma_{cls,Med}$16	-11697.75	-9746.57	828.53	-30.04
Combinazioni Frequenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
310	Ft. 19	-15338.05	-1874.18	5441.45	257.26
	$\sigma_{s,c}$19	-15338.05	-1874.18	5441.45	-259.54
	$\sigma_{cls,Max}$19	-15338.05	-1874.18	5441.45	-22.74
	$\sigma_{cls,Med}$19	-15338.05	-1874.18	5441.45	-7.60
11540	Ft. 19	-11038.05	-9196.53	781.11	1562.61
	$\sigma_{s,c}$19	-11038.05	-9196.53	781.11	-376.54
	$\sigma_{cls,Max}$19	-11038.05	-9196.53	781.11	-59.11
	$\sigma_{cls,Med}$19	-11038.05	-9196.53	781.11	-28.35
Combinazioni Quasi Permanenti					
310	Ft. 21	-15173.19	-1843.49	5365.23	252.08
	$\sigma_{s,c}$21	-15173.19	-1843.49	5365.23	-255.57
	$\sigma_{cls,Max}$21	-15173.19	-1843.49	5365.23	-22.37
	$\sigma_{cls,Med}$21	-15173.19	-1843.49	5365.23	-7.48
11540	Ft. 21	-10873.19	-9059.37	769.24	1539.30
	$\sigma_{s,c}$21	-10873.19	-9059.37	769.24	-370.91
	$\sigma_{cls,Max}$21	-10873.19	-9059.37	769.24	-58.23
	$\sigma_{cls,Med}$21	-10873.19	-9059.37	769.24	-27.93

Pilastro: **11/111** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
11	1	-155415.00	-801.25	6929.96	0.20
111	1	-149760.00	-139.99	-67.03	0.17

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	168.66	61956.98	1608.51	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	168.66	46467.73	1608.51	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	168.66	61956.98	1608.51	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
11	Ft. 16	-102217.15	-597.89	5048.04	-234.25
	$\sigma_{s,c}$15	-106965.41	-597.05	5153.69	-454.73
	$\sigma_{cls,Max}$15	-106965.41	-597.05	5153.69	-31.91
	$\sigma_{cls,Med}$15	-106965.41	-597.05	5153.69	-23.43
111	Ft. 16	-97867.15	-60.05	-123.10	-317.62
	$\sigma_{s,c}$15	-102615.41	-74.19	-52.64	-340.37
	$\sigma_{cls,Max}$15	-102615.41	-74.19	-52.64	-22.79
	$\sigma_{cls,Med}$15	-102615.41	-74.19	-52.64	-22.48
Combinazioni Frequenti					
11	Ft. 19	-98662.66	-599.10	5082.16	-221.97
	$\sigma_{s,c}$18	-100177.43	-598.86	5119.77	-431.93
	$\sigma_{cls,Max}$18	-100177.43	-598.86	5119.77	-30.39
	$\sigma_{cls,Med}$18	-100177.43	-598.86	5119.77	-21.94
111	Ft. 19	-94312.66	-45.95	-111.10	-306.59
	$\sigma_{s,c}$20	-95817.50	-62.39	-86.80	-318.22
	$\sigma_{cls,Max}$20	-95817.50	-62.39	-86.80	-21.30

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$18	-95827.43	-50.34	-86.39	-20.99
Combinazioni Quasi Permanenti					
11	Ft. 21	-98254.72	-599.30	5096.50	-220.39
	$\sigma_{s,c}$21	-98254.72	-599.30	5096.50	-425.25
	$\sigma_{cls,Max}$21	-98254.72	-599.30	5096.50	-29.94
	$\sigma_{cls,Med}$21	-98254.72	-599.30	5096.50	-21.52
111	Ft. 22	-93895.93	-53.93	-104.42	-305.07
	$\sigma_{s,c}$22	-93895.93	-53.93	-104.42	-311.92
	$\sigma_{cls,Max}$22	-93895.93	-53.93	-104.42	-20.87
	$\sigma_{cls,Med}$21	-93904.72	-44.01	-103.76	-20.57

Pilastro: **111/211** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
111	1	-118437.56	-120.74	-2405.46	0.14
211	1	-113952.56	-179.36	-2136.17	0.14

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	19.54	61956.98	104.87	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	19.54	46467.73	104.87	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	19.54	61956.98	104.87	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
111	Ft. 16	-78592.18	-73.51	-1560.42	-230.35
	$\sigma_{s,c}$15	-81417.33	-77.54	-1634.47	-296.70
	$\sigma_{cls,Max}$15	-81417.33	-77.54	-1634.47	-20.16
	$\sigma_{cls,Med}$15	-81417.33	-77.54	-1634.47	-17.83
211	Ft. 16	-75142.18	-115.48	-1601.96	-217.00
	$\sigma_{s,c}$15	-77967.33	-113.65	-1473.51	-283.88
	$\sigma_{cls,Max}$15	-77967.33	-113.65	-1473.51	-19.32
	$\sigma_{cls,Med}$15	-77967.33	-113.65	-1473.51	-17.08
Combinazioni Frequenti					
111	Ft. 19	-75678.07	-68.02	-1501.05	-221.93
	$\sigma_{s,c}$20	-76545.26	-71.78	-1522.58	-278.68
	$\sigma_{cls,Max}$20	-76545.26	-71.78	-1522.58	-18.93
	$\sigma_{cls,Med}$18	-76551.78	-69.22	-1524.54	-16.77
211	Ft. 19	-72228.08	-104.50	-1518.33	-209.15
	$\sigma_{s,c}$18	-73101.78	-103.49	-1471.15	-267.53
	$\sigma_{cls,Max}$18	-73101.78	-103.49	-1471.15	-18.21
	$\sigma_{cls,Med}$18	-73101.78	-103.49	-1471.15	-16.01
Combinazioni Quasi Permanenti					
111	Ft. 22	-75264.23	-69.31	-1492.36	-220.67
	$\sigma_{s,c}$22	-75264.23	-69.31	-1492.36	-273.90
	$\sigma_{cls,Max}$22	-75264.23	-69.31	-1492.36	-18.60
	$\sigma_{cls,Med}$21	-75269.99	-67.16	-1493.88	-16.49
211	Ft. 21	-71820.00	-102.10	-1492.17	-208.31

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}21$	-71820.00	-102.10	-1492.17	-263.62
	$\sigma_{cls,Max}21$	-71820.00	-102.10	-1492.17	-17.96
	$\sigma_{cls,Med}21$	-71820.00	-102.10	-1492.17	-15.73

Pilastro: **211/311** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
211	1	-82601.05	-262.76	-4657.11	0.11
311	1	-78116.05	-1078.26	-4655.72	0.11

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	250.04	61956.98	108.66	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	250.04	46467.73	108.66	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	250.04	61956.98	108.66	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
211	Ft. 16	-55848.71	-177.09	-3164.70	-126.09
	$\sigma_{s,c}15$	-56750.01	-175.89	-3179.82	-244.06
	$\sigma_{cls,Max}15$	-56750.01	-175.89	-3179.82	-17.04
	$\sigma_{cls,Med}15$	-56750.01	-175.89	-3179.82	-12.43
311	Ft. 16	-52398.71	-757.55	-3377.52	-92.81
	$\sigma_{s,c}16$	-52398.71	-757.55	-3377.52	-251.50
	$\sigma_{cls,Max}16$	-52398.71	-757.55	-3377.52	-18.23
	$\sigma_{cls,Med}15$	-53300.01	-724.92	-3141.79	-11.67
Combinazioni Frequenti					
211	Ft. 19	-53575.94	-166.90	-3028.04	-121.19
	$\sigma_{s,c}18$	-53808.36	-166.13	-3028.54	-231.61
	$\sigma_{cls,Max}18$	-53808.36	-166.13	-3028.54	-16.17
	$\sigma_{cls,Med}18$	-53808.36	-166.13	-3028.54	-11.79
311	Ft. 19	-50125.94	-712.11	-3166.99	-90.23
	$\sigma_{s,c}19$	-50125.94	-712.11	-3166.99	-239.15
	$\sigma_{cls,Max}19$	-50125.94	-712.11	-3166.99	-17.32
	$\sigma_{cls,Med}18$	-50358.36	-699.30	-3078.44	-11.03
Combinazioni Quasi Permanenti					
211	Ft. 21	-53167.87	-164.70	-3000.81	-120.36
	$\sigma_{s,c}21$	-53167.87	-164.70	-3000.81	-229.01
	$\sigma_{cls,Max}21$	-53167.87	-164.70	-3000.81	-15.99
	$\sigma_{cls,Med}21$	-53167.87	-164.70	-3000.81	-11.65
311	Ft. 22	-49714.51	-701.36	-3109.04	-90.17
	$\sigma_{s,c}22$	-49714.51	-701.36	-3109.04	-236.50
	$\sigma_{cls,Max}22$	-49714.51	-701.36	-3109.04	-17.12
	$\sigma_{cls,Med}21$	-49717.87	-700.46	-3107.17	-10.89

Pilastro: **311/11541** / L 4.05[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 205.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
311	2	-48007.27	-2222.93	-7717.95	0.10
11541	2	-42417.27	4804.64	4080.63	0.11

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1634.32	61956.98	2743.86	86297.23	ø 10 4br.x2br./15.0
1.13	3.18	1634.32	46467.73	2743.86	64722.92	ø 10 4br.x2br./20.0
3.18	4.18	1634.32	61956.98	2743.86	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
311	Ft. 16	-32909.46	-1498.81	-5213.24	33.52
	$\sigma_{s,c}$16	-32909.46	-1498.81	-5213.24	-245.91
	$\sigma_{cls,Max}$16	-32909.46	-1498.81	-5213.24	-19.18
	$\sigma_{cls,Med}$16	-32909.46	-1498.81	-5213.24	-7.92
11541	Ft. 16	-28609.46	3240.85	2754.81	118.41
	$\sigma_{s,c}$16	-28609.46	3240.85	2754.81	-267.38
	$\sigma_{cls,Max}$16	-28609.46	3240.85	2754.81	-23.21
	$\sigma_{cls,Med}$16	-28609.46	3240.85	2754.81	-9.43
Combinazioni Frequenti					
311	Ft. 19	-31289.73	-1412.87	-4934.90	30.79
	$\sigma_{s,c}$19	-31289.73	-1412.87	-4934.90	-232.89
	$\sigma_{cls,Max}$19	-31289.73	-1412.87	-4934.90	-18.15
	$\sigma_{cls,Med}$19	-31289.73	-1412.87	-4934.90	-7.51
11541	Ft. 19	-26989.73	3056.69	2601.40	111.71
	$\sigma_{s,c}$19	-26989.73	3056.69	2601.40	-252.27
	$\sigma_{cls,Max}$19	-26989.73	3056.69	2601.40	-21.90
	$\sigma_{cls,Med}$19	-26989.73	3056.69	2601.40	-8.89
Combinazioni Quasi Permanenti					
311	Ft. 22	-30883.28	-1391.37	-4869.86	30.22
	$\sigma_{s,c}$21	-30884.69	-1391.11	-4870.32	-229.72
	$\sigma_{cls,Max}$22	-30883.28	-1391.37	-4869.86	-17.90
	$\sigma_{cls,Med}$21	-30884.69	-1391.11	-4870.32	-7.41
11541	Ft. 21	-26584.69	3010.38	2563.20	110.01
	$\sigma_{s,c}$21	-26584.69	3010.38	2563.20	-248.48
	$\sigma_{cls,Max}$21	-26584.69	3010.38	2563.20	-21.57
	$\sigma_{cls,Med}$22	-26583.28	3010.56	2561.16	-8.76

Pilastro: **12/112** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
12	1	-274036.53	-3241.90	-489.57	0.32
112	1	-268381.53	-2275.31	-5094.71	0.35

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2434.41	86297.23	1523.67	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	2434.41	64722.92	1523.67	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	2434.41	86297.23	1523.67	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
12	Ft. 17	-181895.03	-2268.46	-391.63	-548.06
	$\sigma_{s,c}$15	-192961.11	-2317.68	-433.16	-685.67
	$\sigma_{cls,Max}$15	-192961.11	-2317.68	-433.16	-46.62
	$\sigma_{cls,Med}$15	-192961.11	-2317.68	-433.16	-42.27
112	Ft. 17	-177545.03	-1570.73	-3494.99	-446.45
	$\sigma_{s,c}$15	-188611.11	-1634.65	-3546.14	-759.23
	$\sigma_{cls,Max}$15	-188611.11	-1634.65	-3546.14	-54.96
	$\sigma_{cls,Med}$15	-188611.11	-1634.65	-3546.14	-41.31
Combinazioni Frequenti					
12	Ft. 20	-178299.59	-2037.96	-411.94	-539.37
	$\sigma_{s,c}$18	-185875.13	-2071.21	-444.12	-658.70
	$\sigma_{cls,Max}$18	-185875.13	-2071.21	-444.12	-44.79
	$\sigma_{cls,Med}$18	-185875.13	-2071.21	-444.12	-40.71
112	Ft. 20	-173949.59	-1567.63	-3336.82	-439.72
	$\sigma_{s,c}$18	-181525.13	-1609.75	-3366.86	-729.84
	$\sigma_{cls,Max}$18	-181525.13	-1609.75	-3366.86	-52.79
	$\sigma_{cls,Med}$18	-181525.13	-1609.75	-3366.86	-39.76
Combinazioni Quasi Permanenti					
12	Ft. 22	-177101.13	-1961.13	-418.72	-536.47
	$\sigma_{s,c}$21	-183543.98	-1990.95	-450.35	-649.93
	$\sigma_{cls,Max}$21	-183543.98	-1990.95	-450.35	-44.20
	$\sigma_{cls,Med}$21	-183543.98	-1990.95	-450.35	-40.20
112	Ft. 22	-172751.13	-1566.60	-3284.09	-437.48
	$\sigma_{s,c}$21	-179193.98	-1601.13	-3305.46	-720.09
	$\sigma_{cls,Max}$21	-179193.98	-1601.13	-3305.46	-52.06
	$\sigma_{cls,Med}$21	-179193.98	-1601.13	-3305.46	-39.25

Pilastro: **112/212** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
112	1	-215225.78	5736.70	11540.07	0.35
212	1	-210740.78	-720.03	-9871.84	0.33

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1878.48	86297.23	6206.35	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	1878.48	64722.92	6206.35	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	1878.48	86297.23	6206.35	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
112	Ft. 17	-139390.78	3955.36	8021.58	-138.08
	$\sigma_{s,c}$15	-150822.02	3962.16	8143.76	-819.41
	$\sigma_{cls,Max}$15	-150822.02	3962.16	8143.76	-64.63
	$\sigma_{cls,Med}$15	-150822.02	3962.16	8143.76	-33.04
212	Ft. 17	-135940.78	-597.37	-6946.50	-215.88
	$\sigma_{s,c}$15	-147372.02	-574.54	-6972.77	-715.41
	$\sigma_{cls,Max}$15	-147372.02	-574.54	-6972.77	-55.76

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-147372.02	-574.54	-6972.77	-32.28
Combinazioni Frequenti					
112	Ft. 20	-137901.94	3767.30	7672.03	-147.39
	$\sigma_{s,c}$18	-145752.66	3771.18	7749.61	-787.09
	$\sigma_{cls,Max}$18	-145752.66	3771.18	7749.61	-61.99
	$\sigma_{cls,Med}$18	-145752.66	3771.18	7749.61	-31.92
212	Ft. 20	-134451.94	-549.10	-6607.75	-222.56
	$\sigma_{s,c}$18	-142302.66	-539.90	-6618.25	-686.91
	$\sigma_{cls,Max}$18	-142302.66	-539.90	-6618.25	-53.45
	$\sigma_{cls,Med}$18	-142302.66	-539.90	-6618.25	-31.17
Combinazioni Quasi Permanenti					
112	Ft. 22	-137405.64	3704.61	7555.51	-150.50
	$\sigma_{s,c}$21	-144091.05	3707.73	7616.72	-776.37
	$\sigma_{cls,Max}$21	-144091.05	3707.73	7616.72	-61.11
	$\sigma_{cls,Med}$21	-144091.05	3707.73	7616.72	-31.56
212	Ft. 22	-133955.64	-533.01	-6494.83	-224.78
	$\sigma_{s,c}$21	-140641.05	-528.33	-6498.62	-677.46
	$\sigma_{cls,Max}$21	-140641.05	-528.33	-6498.62	-52.68
	$\sigma_{cls,Med}$21	-140641.05	-528.33	-6498.62	-30.81

Pilastro: **212/312** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
212	1	-162945.28	8838.80	12776.35	0.32
312	1	-158460.28	-25273.21	-18645.58	0.48

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	9887.54	86297.23	9107.81	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	9887.54	64722.92	9107.81	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	9887.54	86297.23	9107.81	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
212	Ft. 17	-101062.25	5970.69	8426.17	70.07
	$\sigma_{s,c}$15	-113259.74	6064.25	8895.76	-767.28
	$\sigma_{cls,Max}$15	-113259.74	6064.25	8895.76	-62.85
	$\sigma_{cls,Med}$15	-113259.74	6064.25	8895.76	-27.56
312	Ft. 17	-97612.25	-16603.35	-11770.18	734.01
	$\sigma_{s,c}$15	-109809.74	-17275.05	-12888.43	-1215.33
	$\sigma_{cls,Max}$15	-109809.74	-17275.05	-12888.43	-105.75
	$\sigma_{cls,Med}$15	-109809.74	-17275.05	-12888.43	-39.35
Combinazioni Frequenti					
212	Ft. 20	-101649.80	5781.69	8204.72	50.39
	$\sigma_{s,c}$18	-110072.38	5832.69	8518.63	-739.40
	$\sigma_{cls,Max}$18	-110072.38	5832.69	8518.63	-60.46
	$\sigma_{cls,Med}$18	-110072.38	5832.69	8518.63	-26.58
312	Ft. 20	-98199.80	-16415.64	-11661.41	705.08

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-106622.38	-16834.21	-12424.01	-1176.38
	$\sigma_{cls,Max}$18	-106622.38	-16834.21	-12424.01	-102.22
	$\sigma_{cls,Med}$18	-106622.38	-16834.21	-12424.01	-37.99
Combinazioni Quasi Permanenti					
212	Ft. 22	-101845.66	5718.69	8130.91	44.07
	$\sigma_{s,c}$21	-109033.76	5755.60	8389.94	-730.06
	$\sigma_{cls,Max}$21	-109033.76	5755.60	8389.94	-59.65
	$\sigma_{cls,Med}$21	-109033.76	5755.60	8389.94	-26.25
312	Ft. 22	-98395.66	-16353.07	-11625.15	695.56
	$\sigma_{s,c}$21	-105583.76	-16689.39	-12264.02	-1163.16
	$\sigma_{cls,Max}$21	-105583.76	-16689.39	-12264.02	-101.01
	$\sigma_{cls,Med}$21	-105583.76	-16689.39	-12264.02	-37.52

Pilastro: **13/113** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
13	1	-424599.03	-4050.00	1514.75	0.50
113	1	-418944.03	-2685.18	-1246.57	0.49

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2926.03	86297.23	694.73	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	2926.03	64722.92	694.73	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	2926.03	86297.23	694.73	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
13	Ft. 16	-286137.50	-2420.21	962.96	-869.89
	$\sigma_{s,c}$15	-297391.91	-2723.37	1032.75	-1054.49
	$\sigma_{cls,Max}$15	-297391.91	-2723.37	1032.75	-71.96
	$\sigma_{cls,Med}$15	-297391.91	-2723.37	1032.75	-65.14
113	Ft. 17	-282632.31	-2304.98	-893.15	-862.48
	$\sigma_{s,c}$15	-293041.91	-1970.86	-845.83	-1021.94
	$\sigma_{cls,Max}$15	-293041.91	-1970.86	-845.83	-69.45
	$\sigma_{cls,Med}$15	-293041.91	-1970.86	-845.83	-64.19
Combinazioni Frequenti					
13	Ft. 19	-282377.81	-2316.51	939.53	-859.98
	$\sigma_{s,c}$18	-286128.94	-2417.48	962.79	-1010.25
	$\sigma_{cls,Max}$18	-286128.94	-2417.48	962.79	-68.88
	$\sigma_{cls,Med}$18	-286128.94	-2417.48	962.79	-62.67
113	Ft. 20	-277227.31	-2261.44	-845.79	-846.94
	$\sigma_{s,c}$18	-281778.94	-1940.55	-789.03	-982.63
	$\sigma_{cls,Max}$18	-281778.94	-1940.55	-789.03	-66.75
	$\sigma_{cls,Med}$18	-281778.94	-1940.55	-789.03	-61.72
Combinazioni Quasi Permanenti					
13	Ft. 21	-282376.09	-2315.97	939.50	-859.98
	$\sigma_{s,c}$21	-282376.09	-2315.97	939.50	-995.52
	$\sigma_{cls,Max}$21	-282376.09	-2315.97	939.50	-67.85

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-282376.09	-2315.97	939.50	-61.85
113	Ft. 22	-275425.63	-2246.92	-830.00	-841.76
	$\sigma_{s,c}$21	-278026.09	-1930.63	-770.11	-969.54
	$\sigma_{cls,Max}$22	-275425.63	-2246.92	-830.00	-65.88
	$\sigma_{cls,Med}$21	-278026.09	-1930.63	-770.11	-60.90

Pilastro: **113/213** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
113	1	-340744.88	8962.85	975.05	0.42
213	1	-336259.88	300.16	-962.18	0.39

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2510.92	86297.23	561.52	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	2510.92	64722.92	561.52	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	2510.92	86297.23	561.52	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
113	Ft. 17	-227230.89	6093.92	630.17	-626.85
	$\sigma_{s,c}$15	-237594.34	6233.69	666.36	-903.78
	$\sigma_{cls,Max}$15	-237594.34	6233.69	666.36	-62.12
	$\sigma_{cls,Med}$15	-237594.34	6233.69	666.36	-52.04
213	Ft. 17	-223780.91	526.01	-500.97	-710.70
	$\sigma_{s,c}$15	-234144.36	61.95	-659.60	-791.28
	$\sigma_{cls,Max}$15	-234144.36	61.95	-659.60	-53.52
	$\sigma_{cls,Med}$15	-234144.36	61.95	-659.60	-51.29
Combinazioni Frequenti					
113	Ft. 20	-224807.92	5843.91	599.99	-623.93
	$\sigma_{s,c}$18	-229275.38	5951.13	620.57	-870.37
	$\sigma_{cls,Max}$18	-229275.38	5951.13	620.57	-59.79
	$\sigma_{cls,Med}$18	-229275.38	5951.13	620.57	-50.22
213	Ft. 20	-221357.94	569.64	-482.51	-702.61
	$\sigma_{s,c}$18	-225825.39	59.93	-622.91	-762.75
	$\sigma_{cls,Max}$18	-225825.39	59.93	-622.91	-51.57
	$\sigma_{cls,Med}$18	-225825.39	59.93	-622.91	-49.46
Combinazioni Quasi Permanenti					
113	Ft. 22	-224000.30	5760.57	589.93	-622.96
	$\sigma_{s,c}$21	-226503.48	5856.38	604.90	-859.22
	$\sigma_{cls,Max}$21	-226503.48	5856.38	604.90	-59.01
	$\sigma_{cls,Med}$21	-226503.48	5856.38	604.90	-49.61
213	Ft. 22	-220550.31	584.18	-476.36	-699.91
	$\sigma_{s,c}$21	-223053.50	59.65	-610.33	-753.24
	$\sigma_{cls,Max}$21	-223053.50	59.65	-610.33	-50.92
	$\sigma_{cls,Med}$21	-223053.50	59.65	-610.33	-48.86

Pilastro: **213/313** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
213	1	-259643.44	15915.69	863.61	0.35
313	3	-239710.31	-46932.66	-3028.28	0.46

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	18548.65	86297.23	1262.32	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	18548.65	64722.92	1262.32	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	18548.65	86297.23	1262.32	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
213	Ft. 17	-169485.78	11742.26	878.67	-336.83
	$\sigma_{s,c}$15	-179784.53	10979.27	569.92	-788.40
	$\sigma_{cls,Max}$15	-179784.53	10979.27	569.92	-55.16
	$\sigma_{cls,Med}$15	-179784.53	10979.27	569.92	-39.38
313	Ft. 17	-166035.78	-32247.54	-2014.76	61.74
	$\sigma_{s,c}$17	-166035.78	-32247.54	-2014.76	-1145.61
	$\sigma_{cls,Max}$17	-166035.78	-32247.54	-2014.76	-84.63
	$\sigma_{cls,Med}$17	-166035.78	-32247.54	-2014.76	-38.98
Combinazioni Frequenti					
213	Ft. 20	-170033.05	11411.90	830.87	-345.55
	$\sigma_{s,c}$20	-170033.05	11411.90	830.87	-771.74
	$\sigma_{cls,Max}$20	-170033.05	11411.90	830.87	-54.42
	$\sigma_{cls,Med}$18	-174378.67	10553.12	512.42	-38.19
313	Ft. 20	-166583.05	-31886.15	-1920.02	48.11
	$\sigma_{s,c}$20	-166583.05	-31886.15	-1920.02	-1136.97
	$\sigma_{cls,Max}$20	-166583.05	-31886.15	-1920.02	-83.84
	$\sigma_{cls,Med}$20	-166583.05	-31886.15	-1920.02	-38.79
Combinazioni Quasi Permanenti					
213	Ft. 22	-170215.42	11301.79	814.94	-348.46
	$\sigma_{s,c}$22	-170215.42	11301.79	814.94	-770.04
	$\sigma_{cls,Max}$22	-170215.42	11301.79	814.94	-54.27
	$\sigma_{cls,Med}$21	-172577.42	10411.03	493.11	-37.80
313	Ft. 22	-166765.42	-31765.69	-1888.44	43.65
	$\sigma_{s,c}$22	-166765.42	-31765.69	-1888.44	-1134.12
	$\sigma_{cls,Max}$22	-166765.42	-31765.69	-1888.44	-83.58
	$\sigma_{cls,Med}$22	-166765.42	-31765.69	-1888.44	-38.73

Pilastro: **14/114** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
14	1	-427889.94	-3449.63	1072.97	0.50
114	1	-422234.94	-3646.94	-538.80	0.50

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3745.87	86297.23	536.86	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	3745.87	64722.92	536.86	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	3745.87	86297.23	536.86	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
14	Ft. 16	-287982.44	-2056.83	677.55	-890.97
	$\sigma_{s,c}$15	-299498.66	-2321.93	727.85	-1045.14
	$\sigma_{cls,Max}$15	-299498.66	-2321.93	727.85	-70.92
	$\sigma_{cls,Med}$15	-299498.66	-2321.93	727.85	-65.60
114	Ft. 17	-284633.69	-2938.71	-301.79	-877.50
	$\sigma_{s,c}$15	-295148.66	-2621.04	-360.77	-1024.07
	$\sigma_{cls,Max}$15	-295148.66	-2621.04	-360.77	-69.15
	$\sigma_{cls,Med}$15	-295148.66	-2621.04	-360.77	-64.65
Combinazioni Frequenti					
14	Ft. 19	-284145.19	-1965.77	660.40	-880.40
	$\sigma_{s,c}$18	-287984.00	-2054.04	677.15	-1001.32
	$\sigma_{cls,Max}$18	-287984.00	-2054.04	677.15	-67.89
	$\sigma_{cls,Med}$18	-287984.00	-2054.04	677.15	-63.08
114	Ft. 20	-279014.97	-2863.23	-276.60	-861.08
	$\sigma_{s,c}$18	-283634.00	-2548.42	-335.36	-984.24
	$\sigma_{cls,Max}$18	-283634.00	-2548.42	-335.36	-66.45
	$\sigma_{cls,Med}$18	-283634.00	-2548.42	-335.36	-62.13
Combinazioni Quasi Permanenti					
14	Ft. 21	-284145.50	-1965.22	660.32	-880.41
	$\sigma_{s,c}$21	-284145.50	-1965.22	660.32	-986.72
	$\sigma_{cls,Max}$21	-284145.50	-1965.22	660.32	-66.88
	$\sigma_{cls,Med}$21	-284145.50	-1965.22	660.32	-62.24
114	Ft. 22	-277142.06	-2838.07	-268.21	-855.60
	$\sigma_{s,c}$21	-279795.50	-2524.41	-326.98	-970.97
	$\sigma_{cls,Max}$21	-279795.50	-2524.41	-326.98	-65.55
	$\sigma_{cls,Med}$21	-279795.50	-2524.41	-326.98	-61.28

Pilastro: **114/214** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
114	1	-343397.63	10129.83	-39.58	0.43
214	1	-338912.63	557.17	-353.20	0.39

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2774.69	86297.23	239.51	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	2774.69	64722.92	239.51	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	2774.69	86297.23	239.51	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
114	Ft. 17	-228826.06	6951.11	-24.97	-637.32

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-239281.45	7073.47	-27.71	-902.75
	$\sigma_{cls,Max}$15	-239281.45	7073.47	-27.71	-61.47
	$\sigma_{cls,Med}$15	-239281.45	7073.47	-27.71	-52.41
214	Ft. 17	-225376.06	587.67	-347.73	-719.80
	$\sigma_{s,c}$15	-235831.45	202.53	-241.21	-785.82
	$\sigma_{cls,Max}$15	-235831.45	202.53	-241.21	-52.70
	$\sigma_{cls,Med}$15	-235831.45	202.53	-241.21	-51.66
Combinazioni Frequenti					
114	Ft. 20	-226212.66	6654.04	-30.33	-633.42
	$\sigma_{s,c}$18	-230749.83	6745.50	-32.27	-869.50
	$\sigma_{cls,Max}$18	-230749.83	6745.50	-32.27	-59.20
	$\sigma_{cls,Med}$18	-230749.83	6745.50	-32.27	-50.54
214	Ft. 20	-222762.66	632.91	-336.56	-710.83
	$\sigma_{s,c}$18	-227299.83	182.17	-227.27	-757.01
	$\sigma_{cls,Max}$18	-227299.83	182.17	-227.27	-50.76
	$\sigma_{cls,Med}$18	-227299.83	182.17	-227.27	-49.79
Combinazioni Quasi Permanenti					
114	Ft. 22	-225341.53	6555.02	-32.11	-632.12
	$\sigma_{s,c}$21	-227905.66	6635.53	-33.90	-858.40
	$\sigma_{cls,Max}$21	-227905.66	6635.53	-33.90	-58.44
	$\sigma_{cls,Med}$21	-227905.66	6635.53	-33.90	-49.92
214	Ft. 22	-221891.53	647.99	-332.83	-707.84
	$\sigma_{s,c}$22	-221891.53	647.99	-332.83	-750.22
	$\sigma_{cls,Max}$22	-221891.53	647.99	-332.83	-50.51
	$\sigma_{cls,Med}$21	-224455.66	175.87	-222.54	-49.16

Pilastro: **214/314** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
214	1	-261765.52	18469.23	-116.15	0.36
314	3	-241721.63	-53391.14	1324.40	0.49

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	21120.12	86297.23	542.20	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	21120.12	64722.92	542.20	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	21120.12	86297.23	542.20	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
214	Ft. 17	-170753.22	13390.16	-369.74	-330.23
	$\sigma_{s,c}$15	-181125.81	12720.81	-83.04	-805.81
	$\sigma_{cls,Max}$15	-181125.81	12720.81	-83.04	-56.07
	$\sigma_{cls,Med}$15	-181125.81	12720.81	-83.04	-39.67
314	Ft. 17	-167303.22	-36700.61	885.46	117.91
	$\sigma_{s,c}$17	-167303.22	-36700.61	885.46	-1195.50
	$\sigma_{cls,Max}$17	-167303.22	-36700.61	885.46	-87.62
	$\sigma_{cls,Med}$17	-167303.22	-36700.61	885.46	-42.20

Combinazioni Frequenti					
214	Ft. 20	-171117.67	12981.32	-392.26	-337.40
	$\sigma_{s,c}$20	-171117.67	12981.32	-392.26	-787.03
	$\sigma_{cls,Max}$20	-171117.67	12981.32	-392.26	-55.22
	$\sigma_{cls,Med}$18	-175534.97	12181.47	-97.91	-38.45
314	Ft. 20	-167667.67	-36174.58	928.62	104.12
	$\sigma_{s,c}$20	-167667.67	-36174.58	928.62	-1187.39
	$\sigma_{cls,Max}$20	-167667.67	-36174.58	928.62	-86.99
	$\sigma_{cls,Med}$20	-167667.67	-36174.58	928.62	-41.83
Combinazioni Quasi Permanenti					
214	Ft. 22	-171239.16	12845.04	-399.77	-339.79
	$\sigma_{s,c}$22	-171239.16	12845.04	-399.77	-785.43
	$\sigma_{cls,Max}$22	-171239.16	12845.04	-399.77	-55.10
	$\sigma_{cls,Med}$21	-173671.00	12001.70	-102.84	-38.04
314	Ft. 22	-167789.16	-35999.24	943.01	99.62
	$\sigma_{s,c}$22	-167789.16	-35999.24	943.01	-1184.71
	$\sigma_{cls,Max}$22	-167789.16	-35999.24	943.01	-86.79
	$\sigma_{cls,Med}$22	-167789.16	-35999.24	943.01	-41.70

Pilastro: **15/115** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
15	1	-430299.28	-2427.89	1099.63	0.50
115	1	-424644.28	-4301.11	-881.64	0.50

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	4408.46	86297.23	549.09	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	4408.46	64722.92	549.09	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	4408.46	86297.23	549.09	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
15	Ft. 17	-283617.47	-898.82	721.02	-894.19
	$\sigma_{s,c}$15	-301246.25	-1636.48	743.17	-1040.16
	$\sigma_{cls,Max}$15	-301246.25	-1636.48	743.17	-70.48
	$\sigma_{cls,Med}$15	-301246.25	-1636.48	743.17	-65.98
115	Ft. 17	-279267.47	-3272.95	-578.99	-845.58
	$\sigma_{s,c}$15	-296896.25	-3058.50	-602.92	-1044.67
	$\sigma_{cls,Max}$15	-296896.25	-3058.50	-602.92	-70.88
	$\sigma_{cls,Med}$15	-296896.25	-3058.50	-602.92	-65.03
Combinazioni Frequenti					
15	Ft. 20	-277999.59	-789.46	663.77	-879.34
	$\sigma_{s,c}$18	-289696.56	-1403.56	685.58	-996.57
	$\sigma_{cls,Max}$18	-289696.56	-1403.56	685.58	-67.47
	$\sigma_{cls,Med}$18	-289696.56	-1403.56	685.58	-63.45
115	Ft. 20	-273649.59	-3182.92	-539.29	-829.86
	$\sigma_{s,c}$18	-285346.56	-2969.94	-561.98	-1003.97
	$\sigma_{cls,Max}$18	-285346.56	-2969.94	-561.98	-68.10
	$\sigma_{cls,Med}$18	-285346.56	-2969.94	-561.98	-62.50
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
15	Ft. 22	-276126.94	-753.01	644.69	-874.39
	$\sigma_{s,c}$21	-285847.47	-1326.40	666.37	-982.05
	$\sigma_{cls,Max}$21	-285847.47	-1326.40	666.37	-66.47
	$\sigma_{cls,Med}$21	-285847.47	-1326.40	666.37	-62.61
115	Ft. 22	-271776.94	-3152.91	-526.05	-824.62
	$\sigma_{s,c}$21	-281497.47	-2940.63	-548.38	-990.41
	$\sigma_{cls,Max}$21	-281497.47	-2940.63	-548.38	-67.18
	$\sigma_{cls,Med}$21	-281497.47	-2940.63	-548.38	-61.66

Pilastro: **115/215** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
115	1	-345693.22	9831.19	504.02	0.43
215	1	-341208.22	314.28	-660.07	0.40

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2779.85	86297.23	422.41	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	2779.85	64722.92	422.41	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	2779.85	86297.23	422.41	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
115	Ft. 17	-223073.31	6819.28	308.12	-611.57
	$\sigma_{s,c}$15	-240938.33	6885.74	358.68	-915.65
	$\sigma_{cls,Max}$15	-240938.33	6885.74	358.68	-62.68
	$\sigma_{cls,Med}$15	-240938.33	6885.74	358.68	-52.77
215	Ft. 17	-219623.33	-78.52	-383.57	-708.09
	$\sigma_{s,c}$15	-237488.34	36.98	-460.53	-795.53
	$\sigma_{cls,Max}$15	-237488.34	36.98	-460.53	-53.57
	$\sigma_{cls,Med}$15	-237488.34	36.98	-460.53	-52.02
Combinazioni Frequenti					
115	Ft. 20	-220472.55	6522.58	278.02	-608.83
	$\sigma_{s,c}$18	-232378.55	6560.73	330.59	-881.32
	$\sigma_{cls,Max}$18	-232378.55	6560.73	330.59	-60.30
	$\sigma_{cls,Med}$18	-232378.55	6560.73	330.59	-50.90
215	Ft. 20	-217022.56	-16.76	-350.22	-701.62
	$\sigma_{s,c}$18	-228928.56	27.82	-429.54	-766.27
	$\sigma_{cls,Max}$18	-228928.56	27.82	-429.54	-51.58
	$\sigma_{cls,Med}$18	-228928.56	27.82	-429.54	-50.14
Combinazioni Quasi Permanenti					
115	Ft. 22	-219605.63	6423.69	267.99	-607.92
	$\sigma_{s,c}$21	-229525.97	6451.87	321.28	-869.87
	$\sigma_{cls,Max}$21	-229525.97	6451.87	321.28	-59.50
	$\sigma_{cls,Med}$21	-229525.97	6451.87	321.28	-50.27
215	Ft. 22	-216155.64	3.83	-339.10	-699.33
	$\sigma_{s,c}$21	-226075.98	25.12	-419.26	-756.53
	$\sigma_{cls,Max}$21	-226075.98	25.12	-419.26	-50.92

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-226075.98	25.12	-419.26	-49.52

Pilastro: **215/315** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
215	1	-263762.69	18514.22	304.46	0.36
315	1	-259277.72	-50501.65	-859.62	0.49

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	20004.60	86297.23	692.42	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	20004.60	64722.92	692.42	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	20004.60	86297.23	692.42	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
215	Ft. 17	-164366.19	12765.24	208.64	-324.59
	$\sigma_{s,c}$15	-182562.31	12766.45	220.42	-815.65
	$\sigma_{cls,Max}$15	-182562.31	12766.45	220.42	-56.89
	$\sigma_{cls,Med}$15	-182562.31	12766.45	220.42	-39.99
315	Ft. 17	-160916.19	-34396.08	-662.63	83.25
	$\sigma_{s,c}$15	-179112.31	-34830.39	-603.50	-1181.73
	$\sigma_{cls,Max}$15	-179112.31	-34830.39	-603.50	-85.75
	$\sigma_{cls,Med}$15	-179112.31	-34830.39	-603.50	-41.85
Combinazioni Frequenti					
215	Ft. 20	-164762.33	12360.95	181.55	-333.37
	$\sigma_{s,c}$18	-176957.63	12226.15	192.91	-787.52
	$\sigma_{cls,Max}$18	-176957.63	12226.15	192.91	-54.89
	$\sigma_{cls,Med}$18	-176957.63	12226.15	192.91	-38.76
315	Ft. 20	-161312.33	-33857.46	-617.21	66.54
	$\sigma_{s,c}$18	-173507.63	-33717.72	-549.94	-1143.16
	$\sigma_{cls,Max}$18	-173507.63	-33717.72	-549.94	-82.92
	$\sigma_{cls,Med}$18	-173507.63	-33717.72	-549.94	-40.52
Combinazioni Quasi Permanenti					
215	Ft. 22	-164894.39	12226.18	172.52	-336.29
	$\sigma_{s,c}$21	-175089.95	12046.06	183.80	-778.15
	$\sigma_{cls,Max}$21	-175089.95	12046.06	183.80	-54.22
	$\sigma_{cls,Med}$21	-175089.95	12046.06	183.80	-38.35
315	Ft. 22	-161444.39	-33677.93	-602.07	61.10
	$\sigma_{s,c}$21	-171639.95	-33346.05	-532.24	-1130.29
	$\sigma_{cls,Max}$21	-171639.95	-33346.05	-532.24	-81.97
	$\sigma_{cls,Med}$21	-171639.95	-33346.05	-532.24	-40.08

Pilastro: **16/116** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
16	1	-396836.94	1504.00	1177.97	0.47

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
116	1	-391181.94	-3546.69	284.83	0.46

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5957.86	86297.23	473.18	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	5957.86	64722.92	473.18	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	5957.86	86297.23	473.18	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
16	Ft. 17	-261338.50	1714.88	784.64	-805.62
	$\sigma_{s,c}$15	-278513.91	1280.93	811.65	-961.84
	$\sigma_{cls,Max}$15	-278513.91	1280.93	811.65	-65.28
	$\sigma_{cls,Med}$15	-278513.91	1280.93	811.65	-61.00
116	Ft. 17	-256988.50	-2729.71	215.09	-792.85
	$\sigma_{s,c}$15	-274163.91	-2610.51	203.97	-949.96
	$\sigma_{cls,Max}$15	-274163.91	-2610.51	203.97	-64.03
	$\sigma_{cls,Med}$15	-274163.91	-2610.51	203.97	-60.05
Combinazioni Frequenti					
16	Ft. 20	-256195.36	1764.83	743.05	-789.23
	$\sigma_{s,c}$18	-267903.38	1416.19	761.83	-927.60
	$\sigma_{cls,Max}$18	-267903.38	1416.19	761.83	-62.96
	$\sigma_{cls,Med}$18	-267903.38	1416.19	761.83	-58.68
116	Ft. 20	-251845.36	-2676.48	206.85	-777.08
	$\sigma_{s,c}$18	-263553.38	-2564.04	196.25	-914.09
	$\sigma_{cls,Max}$18	-263553.38	-2564.04	196.25	-61.62
	$\sigma_{cls,Med}$18	-263553.38	-2564.04	196.25	-57.73
Combinazioni Quasi Permanenti					
16	Ft. 22	-254480.97	1781.48	729.19	-783.77
	$\sigma_{s,c}$21	-264376.78	1464.69	745.58	-916.29
	$\sigma_{cls,Max}$21	-264376.78	1464.69	745.58	-62.20
	$\sigma_{cls,Med}$21	-264376.78	1464.69	745.58	-57.91
116	Ft. 22	-250130.97	-2658.74	204.11	-771.83
	$\sigma_{s,c}$21	-260026.86	-2550.39	193.38	-902.19
	$\sigma_{cls,Max}$21	-260026.86	-2550.39	193.38	-60.82
	$\sigma_{cls,Med}$21	-260026.86	-2550.39	193.38	-56.95

Pilastro: **116/216** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
116	1	-315802.41	6588.05	-1837.59	0.39
216	1	-311317.41	-493.65	1093.57	0.37

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2052.67	86297.23	938.83	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	2052.67	64722.92	938.83	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	2052.67	86297.23	938.83	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
116	Ft. 17	-203402.45	4528.95	-1269.71	-553.81
	$\sigma_{s,c}$15	-220681.31	4595.46	-1285.99	-841.13
	$\sigma_{cls,Max}$15	-220681.31	4595.46	-1285.99	-58.36
	$\sigma_{cls,Med}$15	-220681.31	4595.46	-1285.99	-48.34
216	Ft. 17	-199952.47	-453.26	767.21	-625.13
	$\sigma_{s,c}$15	-217231.33	-433.95	781.77	-745.69
	$\sigma_{cls,Max}$15	-217231.33	-433.95	781.77	-50.68
	$\sigma_{cls,Med}$15	-217231.33	-433.95	781.77	-47.58
Combinazioni Frequenti					
116	Ft. 20	-201116.63	4327.17	-1215.45	-551.33
	$\sigma_{s,c}$18	-212906.02	4372.65	-1224.20	-809.98
	$\sigma_{cls,Max}$18	-212906.02	4372.65	-1224.20	-56.17
	$\sigma_{cls,Med}$18	-212906.02	4372.65	-1224.20	-46.63
216	Ft. 20	-197666.64	-411.78	724.97	-619.64
	$\sigma_{s,c}$18	-209456.03	-421.85	739.83	-718.61
	$\sigma_{cls,Max}$18	-209456.03	-421.85	739.83	-48.83
	$\sigma_{cls,Med}$18	-209456.03	-421.85	739.83	-45.88
Combinazioni Quasi Permanenti					
116	Ft. 22	-200354.69	4259.91	-1197.36	-550.50
	$\sigma_{s,c}$21	-210323.20	4298.16	-1203.24	-799.60
	$\sigma_{cls,Max}$21	-210323.20	4298.16	-1203.24	-55.44
	$\sigma_{cls,Med}$21	-210323.20	4298.16	-1203.24	-46.07
216	Ft. 22	-196904.70	-397.95	710.90	-617.81
	$\sigma_{s,c}$21	-206873.22	-417.55	725.52	-709.60
	$\sigma_{cls,Max}$21	-206873.22	-417.55	725.52	-48.21
	$\sigma_{cls,Med}$21	-206873.22	-417.55	725.52	-45.31

Pilastro: **216/316** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
216	1	-238351.94	11438.07	-2920.44	0.32
316	1	-233866.94	-31586.13	4473.69	0.39

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	12470.78	86297.23	2143.23	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	12470.78	64722.92	2143.23	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	12470.78	86297.23	2143.23	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
216	Ft. 17	-147946.06	8045.52	-1961.90	-292.07
	$\sigma_{s,c}$15	-165419.33	7996.66	-2005.30	-738.08
	$\sigma_{cls,Max}$15	-165419.33	7996.66	-2005.30	-52.92
	$\sigma_{cls,Med}$15	-165419.33	7996.66	-2005.30	-36.23
316	Ft. 17	-144496.06	-21989.57	2985.43	-17.75
	$\sigma_{s,c}$15	-161969.33	-22096.19	3048.69	-990.67
	$\sigma_{cls,Max}$15	-161969.33	-22096.19	3048.69	-73.45

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-161969.33	-22096.19	3048.69	-35.58
Combinazioni Frequenti					
216	Ft. 20	-148493.70	7782.77	-1921.58	-299.45
	$\sigma_{s,c}$18	-160425.95	7683.69	-1931.35	-714.21
	$\sigma_{cls,Max}$18	-160425.95	7683.69	-1931.35	-51.18
	$\sigma_{cls,Med}$18	-160425.95	7683.69	-1931.35	-35.14
316	Ft. 20	-145043.70	-21632.38	2973.62	-26.39
	$\sigma_{s,c}$18	-156975.95	-21476.03	2959.56	-961.29
	$\sigma_{cls,Max}$18	-156975.95	-21476.03	2959.56	-71.28
	$\sigma_{cls,Med}$18	-156975.95	-21476.03	2959.56	-34.49
Combinazioni Quasi Permanenti					
216	Ft. 22	-148676.23	7695.19	-1908.14	-301.91
	$\sigma_{s,c}$21	-158769.16	7581.33	-1906.30	-706.29
	$\sigma_{cls,Max}$21	-158769.16	7581.33	-1906.30	-50.61
	$\sigma_{cls,Med}$21	-158769.16	7581.33	-1906.30	-34.78
316	Ft. 22	-145226.23	-21513.31	2969.69	-29.25
	$\sigma_{s,c}$21	-155319.16	-21275.27	2929.11	-951.60
	$\sigma_{cls,Max}$21	-155319.16	-21275.27	2929.11	-70.56
	$\sigma_{cls,Med}$21	-155319.16	-21275.27	2929.11	-34.13

Pilastro: **17/117** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
17	1	-321057.34	3581.52	956.95	0.38
117	1	-315402.34	-5195.23	1378.98	0.38

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	7112.53	86297.23	604.45	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	7112.53	64722.92	604.45	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	7112.53	86297.23	604.45	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
17	Ft. 17	-212390.52	2661.16	682.38	-632.58
	$\sigma_{s,c}$15	-226093.70	2577.53	655.05	-805.83
	$\sigma_{cls,Max}$15	-226093.70	2577.53	655.05	-54.93
	$\sigma_{cls,Med}$15	-226093.70	2577.53	655.05	-49.52
117	Ft. 17	-208040.52	-3638.29	935.95	-594.24
	$\sigma_{s,c}$15	-221743.70	-3699.43	998.58	-820.82
	$\sigma_{cls,Max}$15	-221743.70	-3699.43	998.58	-56.52
	$\sigma_{cls,Med}$15	-221743.70	-3699.43	998.58	-48.57
Combinazioni Frequenti					
17	Ft. 20	-207965.47	2703.09	613.46	-619.54
	$\sigma_{s,c}$18	-217474.02	2618.41	593.40	-776.22
	$\sigma_{cls,Max}$18	-217474.02	2618.41	593.40	-52.89
	$\sigma_{cls,Med}$18	-217474.02	2618.41	593.40	-47.63
117	Ft. 20	-203615.47	-3556.72	935.67	-581.04

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-213124.02	-3584.43	980.87	-790.06
	$\sigma_{cls,Max}$18	-213124.02	-3584.43	980.87	-54.43
	$\sigma_{cls,Med}$18	-213124.02	-3584.43	980.87	-46.68
Combinazioni Quasi Permanenti					
17	Ft. 22	-206490.47	2717.07	590.49	-615.20
	$\sigma_{s,c}$21	-214629.16	2634.33	573.33	-766.50
	$\sigma_{cls,Max}$21	-214629.16	2634.33	573.33	-52.22
	$\sigma_{cls,Med}$21	-214629.16	2634.33	573.33	-47.01
117	Ft. 22	-202140.47	-3529.53	935.58	-576.64
	$\sigma_{s,c}$21	-210279.16	-3547.79	974.51	-779.91
	$\sigma_{cls,Max}$21	-210279.16	-3547.79	974.51	-53.74
	$\sigma_{cls,Med}$21	-210279.16	-3547.79	974.51	-46.06

Pilastro: **117/217** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
117	1	-251591.84	7310.14	-4095.38	0.33
217	1	-247106.84	-3736.65	3231.81	0.31

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3205.96	86297.23	2123.82	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	3205.96	64722.92	2123.82	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	3205.96	86297.23	2123.82	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
117	Ft. 17	-162653.69	5050.67	-2829.55	-361.77
	$\sigma_{s,c}$15	-176457.50	5098.94	-2921.00	-756.08
	$\sigma_{cls,Max}$15	-176457.50	5098.94	-2921.00	-54.65
	$\sigma_{cls,Med}$15	-176457.50	5098.94	-2921.00	-38.65
217	Ft. 17	-159203.69	-2694.18	2283.85	-406.34
	$\sigma_{s,c}$15	-173007.50	-2636.72	2322.52	-685.43
	$\sigma_{cls,Max}$15	-173007.50	-2636.72	2322.52	-48.82
	$\sigma_{cls,Med}$15	-173007.50	-2636.72	2322.52	-37.89
Combinazioni Frequenti					
117	Ft. 20	-160658.38	4799.56	-2758.13	-361.60
	$\sigma_{s,c}$18	-170250.77	4831.26	-2820.95	-728.13
	$\sigma_{cls,Max}$18	-170250.77	4831.26	-2820.95	-52.62
	$\sigma_{cls,Med}$18	-170250.77	4831.26	-2820.95	-37.29
217	Ft. 20	-157208.38	-2539.70	2215.25	-404.50
	$\sigma_{s,c}$18	-166800.77	-2500.26	2239.54	-660.17
	$\sigma_{cls,Max}$18	-166800.77	-2500.26	2239.54	-47.01
	$\sigma_{cls,Med}$18	-166800.77	-2500.26	2239.54	-36.54
Combinazioni Quasi Permanenti					
117	Ft. 22	-159993.28	4715.86	-2734.33	-361.54
	$\sigma_{s,c}$21	-168207.92	4742.24	-2787.03	-718.88
	$\sigma_{cls,Max}$21	-168207.92	4742.24	-2787.03	-51.95

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-168207.92	4742.24	-2787.03	-36.84
217	Ft. 22	-156543.28	-2488.21	2192.39	-403.88
	$\sigma_{s,c}$21	-164757.92	-2454.71	2211.48	-651.82
	$\sigma_{cls,Max}$21	-164757.92	-2454.71	2211.48	-46.42
	$\sigma_{cls,Med}$21	-164757.92	-2454.71	2211.48	-36.09

Pilastro: **217/317** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
217	1	-187906.27	9004.36	-4907.47	0.27
317	1	-183421.27	-24971.75	6552.80	0.33

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	11552.82	86297.23	3321.82	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	11552.82	64722.92	3321.82	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	11552.82	86297.23	3321.82	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
217	Ft. 17	-116774.39	6173.14	-3146.75	-182.59
	$\sigma_{s,c}$15	-130923.05	6307.18	-3432.61	-642.52
	$\sigma_{cls,Max}$15	-130923.05	6307.18	-3432.61	-47.87
	$\sigma_{cls,Med}$15	-130923.05	6307.18	-3432.61	-28.68
317	Ft. 17	-113324.39	-16754.97	3933.80	36.17
	$\sigma_{s,c}$15	-127473.05	-17471.82	4544.77	-853.34
	$\sigma_{cls,Max}$15	-127473.05	-17471.82	4544.77	-65.30
	$\sigma_{cls,Med}$15	-127473.05	-17471.82	4544.77	-28.93
Combinazioni Frequenti					
217	Ft. 20	-117172.96	5967.16	-3129.82	-187.80
	$\sigma_{s,c}$18	-127021.21	6042.82	-3336.49	-622.31
	$\sigma_{cls,Max}$18	-127021.21	6042.82	-3336.49	-46.37
	$\sigma_{cls,Med}$18	-127021.21	6042.82	-3336.49	-27.82
317	Ft. 20	-113722.96	-16501.91	4008.38	32.54
	$\sigma_{s,c}$18	-123571.21	-16948.14	4450.53	-829.01
	$\sigma_{cls,Max}$18	-123571.21	-16948.14	4450.53	-63.48
	$\sigma_{cls,Med}$18	-123571.21	-16948.14	4450.53	-28.08
Combinazioni Quasi Permanenti					
217	Ft. 22	-117305.81	5898.50	-3124.18	-189.54
	$\sigma_{s,c}$21	-125744.27	5956.68	-3302.93	-615.64
	$\sigma_{cls,Max}$21	-125744.27	5956.68	-3302.93	-45.87
	$\sigma_{cls,Med}$21	-125744.27	5956.68	-3302.93	-27.54
317	Ft. 22	-113855.81	-16417.55	4033.24	31.34
	$\sigma_{s,c}$21	-122294.27	-16781.11	4416.10	-821.00
	$\sigma_{cls,Max}$21	-122294.27	-16781.11	4416.10	-62.88
	$\sigma_{cls,Med}$21	-122294.27	-16781.11	4416.10	-27.79

Pilastro: **18/118** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
18	1	-155324.53	-718.77	-6522.06	0.20
118	1	-149669.53	-141.15	160.58	0.17

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	250.23	61956.98	1536.24	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	250.23	46467.73	1536.24	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	250.23	61956.98	1536.24	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
18	Ft. 16	-102158.61	-541.65	-4757.54	-240.59
	$\sigma_{s,c}$15	-106909.52	-540.60	-4837.03	-447.57
	$\sigma_{cls,Max}$15	-106909.52	-540.60	-4837.03	-31.31
	$\sigma_{cls,Med}$15	-106909.52	-540.60	-4837.03	-23.42
118	Ft. 16	-97808.61	-58.95	197.89	-316.24
	$\sigma_{s,c}$15	-102559.52	-74.23	124.70	-341.36
	$\sigma_{cls,Max}$15	-102559.52	-74.23	124.70	-22.86
	$\sigma_{cls,Med}$15	-102559.52	-74.23	124.70	-22.46
Combinazioni Frequenti					
18	Ft. 19	-98609.85	-540.71	-4805.46	-228.18
	$\sigma_{s,c}$18	-100125.74	-540.31	-4834.52	-425.23
	$\sigma_{cls,Max}$18	-100125.74	-540.31	-4834.52	-29.82
	$\sigma_{cls,Med}$18	-100125.74	-540.31	-4834.52	-21.93
118	Ft. 19	-94259.85	-44.34	187.77	-305.21
	$\sigma_{s,c}$20	-95765.70	-62.42	158.20	-319.21
	$\sigma_{cls,Max}$20	-95765.70	-62.42	158.20	-21.38
	$\sigma_{cls,Med}$18	-95775.74	-49.11	162.19	-20.98
Combinazioni Quasi Permanenti					
18	Ft. 21	-98203.28	-540.44	-4820.85	-226.60
	$\sigma_{s,c}$21	-98203.28	-540.44	-4820.85	-418.70
	$\sigma_{cls,Max}$21	-98203.28	-540.44	-4820.85	-29.39
	$\sigma_{cls,Med}$21	-98203.28	-540.44	-4820.85	-21.51
118	Ft. 22	-93844.80	-53.37	177.63	-303.73
	$\sigma_{s,c}$22	-93844.80	-53.37	177.63	-312.93
	$\sigma_{cls,Max}$22	-93844.80	-53.37	177.63	-20.95
	$\sigma_{cls,Med}$21	-93853.28	-42.37	180.63	-20.56

Pilastro: **118/218** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
118	1	-118356.78	-134.30	2492.58	0.14
218	1	-113871.78	-170.29	2150.21	0.14

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	13.00	61956.98	124.66	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	13.00	46467.73	124.66	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	13.00	61956.98	124.66	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
118	Ft. 16	-78539.88	-82.14	1631.31	-228.75
	$\sigma_{s,c}$15	-81367.48	-86.27	1703.20	-297.94
	$\sigma_{cls,Max}$15	-81367.48	-86.27	1703.20	-20.26
	$\sigma_{cls,Med}$15	-81367.48	-86.27	1703.20	-17.82
218	Ft. 16	-75089.88	-109.35	1615.77	-216.80
	$\sigma_{s,c}$15	-77917.48	-107.57	1484.28	-283.70
	$\sigma_{cls,Max}$15	-77917.48	-107.57	1484.28	-19.30
	$\sigma_{cls,Med}$15	-77917.48	-107.57	1484.28	-17.07
Combinazioni Frequenti					
118	Ft. 19	-75630.99	-76.47	1574.29	-220.30
	$\sigma_{s,c}$18	-76505.72	-77.70	1597.11	-279.96
	$\sigma_{cls,Max}$18	-76505.72	-77.70	1597.11	-19.04
	$\sigma_{cls,Med}$18	-76505.72	-77.70	1597.11	-16.76
218	Ft. 19	-72180.99	-98.42	1534.02	-208.93
	$\sigma_{s,c}$18	-73055.72	-97.43	1485.86	-267.43
	$\sigma_{cls,Max}$18	-73055.72	-97.43	1485.86	-18.20
	$\sigma_{cls,Med}$18	-73055.72	-97.43	1485.86	-16.00
Combinazioni Quasi Permanenti					
118	Ft. 22	-75218.22	-77.88	1562.67	-219.09
	$\sigma_{s,c}$21	-75224.16	-75.58	1567.45	-275.19
	$\sigma_{cls,Max}$22	-75218.22	-77.88	1562.67	-18.71
	$\sigma_{cls,Med}$21	-75224.16	-75.58	1567.45	-16.48
218	Ft. 21	-71774.16	-96.04	1508.04	-208.09
	$\sigma_{s,c}$21	-71774.16	-96.04	1508.04	-263.54
	$\sigma_{cls,Max}$21	-71774.16	-96.04	1508.04	-17.95
	$\sigma_{cls,Med}$21	-71774.16	-96.04	1508.04	-15.72

Pilastro: **218/318** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
218	1	-82522.39	-267.47	4672.04	0.11
318	1	-78037.39	-1064.69	4628.93	0.11

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	244.72	61956.98	95.51	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	244.72	46467.73	95.51	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	244.72	61956.98	95.51	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
218	Ft. 16	-55796.63	-180.13	3180.64	-125.56

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-56700.26	-178.95	3193.08	-244.21
	$\sigma_{cls,Max}$15	-56700.26	-178.95	3193.08	-17.05
	$\sigma_{cls,Med}$15	-56700.26	-178.95	3193.08	-12.42
318	Ft. 16	-52346.63	-748.36	3357.90	-93.25
	$\sigma_{s,c}$16	-52346.63	-748.36	3357.90	-250.72
	$\sigma_{cls,Max}$16	-52346.63	-748.36	3357.90	-18.17
	$\sigma_{cls,Med}$15	-53250.26	-715.82	3121.93	-11.66
Combinazioni Frequenti					
218	Ft. 19	-53528.41	-169.80	3046.60	-120.63
	$\sigma_{s,c}$18	-53761.79	-169.04	3046.26	-231.84
	$\sigma_{cls,Max}$18	-53761.79	-169.04	3046.26	-16.19
	$\sigma_{cls,Med}$18	-53761.79	-169.04	3046.26	-11.78
318	Ft. 19	-50078.41	-703.28	3147.91	-90.67
	$\sigma_{s,c}$19	-50078.41	-703.28	3147.91	-238.40
	$\sigma_{cls,Max}$19	-50078.41	-703.28	3147.91	-17.26
	$\sigma_{cls,Med}$18	-50311.79	-690.50	3059.30	-11.02
Combinazioni Quasi Permanenti					
218	Ft. 21	-53121.44	-167.58	3019.72	-119.81
	$\sigma_{s,c}$21	-53121.44	-167.58	3019.72	-229.26
	$\sigma_{cls,Max}$21	-53121.44	-167.58	3019.72	-16.01
	$\sigma_{cls,Med}$21	-53121.44	-167.58	3019.72	-11.64
318	Ft. 22	-49667.87	-692.64	3089.57	-90.61
	$\sigma_{s,c}$22	-49667.87	-692.64	3089.57	-235.76
	$\sigma_{cls,Max}$22	-49667.87	-692.64	3089.57	-17.06
	$\sigma_{cls,Med}$21	-49671.44	-691.71	3088.19	-10.88

Pilastro: **318/11544** / L 4.05[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 205.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
318	2	-47927.55	-2213.25	7690.58	0.10
11544	2	-42337.55	4726.50	-4065.89	0.11

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1613.90	61956.98	2734.06	86297.23	ø 10 4br.x2br./15.0
1.13	3.18	1613.90	46467.73	2734.06	64722.92	ø 10 4br.x2br./20.0
3.18	4.18	1613.90	61956.98	2734.06	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
318	Ft. 16	-32857.50	-1492.14	5194.98	33.03
	$\sigma_{s,c}$16	-32857.50	-1492.14	5194.98	-245.15
	$\sigma_{cls,Max}$16	-32857.50	-1492.14	5194.98	-19.11
	$\sigma_{cls,Med}$16	-32857.50	-1492.14	5194.98	-7.90
11544	Ft. 16	-28557.50	3188.28	-2746.73	113.12
	$\sigma_{s,c}$16	-28557.50	3188.28	-2746.73	-264.34
	$\sigma_{cls,Max}$16	-28557.50	3188.28	-2746.73	-22.88
	$\sigma_{cls,Med}$16	-28557.50	3188.28	-2746.73	-9.29

Combinazioni Frequenti					
318	Ft. 19	-31241.57	-1406.51	4918.11	30.33
	$\sigma_{s,c}$19	-31241.57	-1406.51	4918.11	-232.18
	$\sigma_{cls,Max}$19	-31241.57	-1406.51	4918.11	-18.09
	$\sigma_{cls,Med}$19	-31241.57	-1406.51	4918.11	-7.50
11544	Ft. 19	-26941.57	3007.22	-2594.73	106.75
	$\sigma_{s,c}$19	-26941.57	3007.22	-2594.73	-249.43
	$\sigma_{cls,Max}$19	-26941.57	3007.22	-2594.73	-21.58
	$\sigma_{cls,Med}$19	-26941.57	3007.22	-2594.73	-8.76
Combinazioni Quasi Permanenti					
318	Ft. 21	-30837.46	-1384.83	4853.83	29.76
	$\sigma_{s,c}$21	-30837.46	-1384.83	4853.83	-229.02
	$\sigma_{cls,Max}$21	-30837.46	-1384.83	4853.83	-17.84
	$\sigma_{cls,Med}$21	-30837.46	-1384.83	4853.83	-7.40
11544	Ft. 21	-26537.46	2961.70	-2556.87	105.14
	$\sigma_{s,c}$21	-26537.46	2961.70	-2556.87	-245.69
	$\sigma_{cls,Max}$21	-26537.46	2961.70	-2556.87	-21.26
	$\sigma_{cls,Med}$22	-26535.96	2961.98	-2554.68	-8.63

Pilastro: **19/2767** / L 2.46[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 46.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
19	1	-96602.53	-2831.20	11385.35	0.16
2767	1	-93079.53	-502.64	6082.99	0.13

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	883.99	61956.98	1956.59	86297.23	ø 10 4br.x2br./15.0
1.13	1.58	883.99	46467.73	1956.59	64722.92	ø 10 4br.x2br./20.0
1.58	2.58	883.99	61956.98	1956.59	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
19	Ft. 16	-62941.54	-1796.55	8031.33	-17.70
	$\sigma_{s,c}$15	-66788.22	-1929.31	8189.80	-415.01
	$\sigma_{cls,Max}$15	-66788.22	-1929.31	8189.80	-31.33
	$\sigma_{cls,Med}$15	-66788.22	-1929.31	8189.80	-14.75
2767	Ft. 16	-60231.54	-388.82	4286.65	-115.41
	$\sigma_{s,c}$15	-64078.22	-379.86	4355.26	-293.85
	$\sigma_{cls,Max}$15	-64078.22	-379.86	4355.26	-20.80
	$\sigma_{cls,Med}$15	-64078.22	-379.86	4355.26	-14.04
Combinazioni Frequenti					
19	Ft. 19	-61038.16	-1728.47	7957.31	-14.71
	$\sigma_{s,c}$18	-62298.97	-1771.90	8009.41	-392.43
	$\sigma_{cls,Max}$18	-62298.97	-1771.90	8009.41	-29.62
	$\sigma_{cls,Med}$18	-62298.97	-1771.90	8009.41	-13.81
2767	Ft. 19	-58328.16	-394.91	4231.75	-109.86
	$\sigma_{s,c}$18	-59588.97	-392.03	4253.52	-277.83
	$\sigma_{cls,Max}$18	-59588.97	-392.03	4253.52	-19.72
	$\sigma_{cls,Med}$18	-59588.97	-392.03	4253.52	-13.05
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
19	Ft. 21	-60909.65	-1723.54	7952.93	-14.51
	$\sigma_{s,c}$21	-60909.65	-1723.54	7952.93	-385.46
	$\sigma_{cls,Max}$21	-60909.65	-1723.54	7952.93	-29.09
	$\sigma_{cls,Med}$21	-60909.65	-1723.54	7952.93	-13.52
2767	Ft. 21	-58199.65	-395.55	4225.13	-109.52
	$\sigma_{s,c}$21	-58199.65	-395.55	4225.13	-272.91
	$\sigma_{cls,Max}$21	-58199.65	-395.55	4225.13	-19.40
	$\sigma_{cls,Med}$21	-58199.65	-395.55	4225.13	-12.75

Pilastro: **2767/119** / L 1.39[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 139.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
2767	1	-128256.59	1781.79	3818.82	0.17
119	1	-126124.59	738.28	1000.33	0.15

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.52	679.70	61956.98	1718.59	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
2767	Ft. 16	-82985.16	1057.62	2710.73	-194.66
	$\sigma_{s,c}$15	-88305.45	1180.68	2728.46	-372.32
	$\sigma_{cls,Max}$15	-88305.45	1180.68	2728.46	-26.65
	$\sigma_{cls,Med}$15	-88305.45	1180.68	2728.46	-19.34
119	Ft. 16	-81345.16	488.47	645.13	-241.17
	$\sigma_{s,c}$15	-86665.45	517.47	649.71	-311.83
	$\sigma_{cls,Max}$15	-86665.45	517.47	649.71	-21.49
	$\sigma_{cls,Med}$15	-86665.45	517.47	649.71	-18.98
Combinazioni Frequenti					
2767	Ft. 19	-80363.52	996.50	2669.01	-188.68
	$\sigma_{s,c}$18	-82107.72	1036.83	2673.68	-346.48
	$\sigma_{cls,Max}$20	-82100.27	1069.06	2609.10	-24.78
	$\sigma_{cls,Med}$18	-82107.72	1036.83	2673.68	-17.98
119	Ft. 19	-78723.52	479.18	595.81	-233.66
	$\sigma_{s,c}$18	-80467.72	488.86	595.69	-289.67
	$\sigma_{cls,Max}$18	-80467.72	488.86	595.69	-19.98
	$\sigma_{cls,Med}$18	-80467.72	488.86	595.69	-17.63
Combinazioni Quasi Permanenti					
2767	Ft. 21	-80188.04	992.34	2661.60	-188.36
	$\sigma_{s,c}$21	-80188.04	992.34	2661.60	-338.56
	$\sigma_{cls,Max}$22	-80181.83	1018.84	2607.69	-24.19
	$\sigma_{cls,Med}$21	-80188.04	992.34	2661.60	-17.56
119	Ft. 22	-78541.83	474.62	595.82	-233.21
	$\sigma_{s,c}$21	-78548.04	479.26	585.93	-282.90
	$\sigma_{cls,Max}$21	-78548.04	479.26	585.93	-19.51
	$\sigma_{cls,Med}$21	-78548.04	479.26	585.93	-17.20

Pilastro: **119/219** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
119	1	-94865.25	391.77	-1183.91	0.11
219	1	-90380.25	170.65	-567.18	0.11

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	67.34	61956.98	202.17	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	67.34	46467.73	202.17	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	67.34	61956.98	202.17	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
119	Ft. 16	-62107.30	257.27	-694.26	-184.51
	$\sigma_{s,c}$15	-65509.48	272.16	-827.95	-237.43
	$\sigma_{cls,Max}$15	-65509.48	272.16	-827.95	-16.29
	$\sigma_{cls,Med}$15	-65509.48	272.16	-827.95	-14.35
219	Ft. 16	-58657.30	131.76	-498.73	-180.37
	$\sigma_{s,c}$15	-62059.47	120.24	-420.61	-214.60
	$\sigma_{cls,Max}$15	-62059.47	120.24	-420.61	-14.52
	$\sigma_{cls,Med}$15	-62059.47	120.24	-420.61	-13.59
Combinazioni Frequenti					
119	Ft. 19	-60124.80	250.56	-699.77	-178.12
	$\sigma_{s,c}$18	-61229.59	255.47	-746.06	-221.50
	$\sigma_{cls,Max}$18	-61229.59	255.47	-746.06	-15.19
	$\sigma_{cls,Med}$18	-61229.59	255.47	-746.06	-13.41
219	Ft. 19	-56674.80	127.55	-485.11	-174.21
	$\sigma_{s,c}$18	-57779.59	123.43	-457.71	-201.25
	$\sigma_{cls,Max}$18	-57779.59	123.43	-457.71	-13.64
	$\sigma_{cls,Med}$18	-57779.59	123.43	-457.71	-12.66
Combinazioni Quasi Permanenti					
119	Ft. 21	-59949.25	250.20	-710.13	-177.39
	$\sigma_{s,c}$21	-59949.25	250.20	-710.13	-216.54
	$\sigma_{cls,Max}$21	-59949.25	250.20	-710.13	-14.85
	$\sigma_{cls,Med}$21	-59949.25	250.20	-710.13	-13.13
219	Ft. 21	-56499.25	125.88	-476.91	-173.82
	$\sigma_{s,c}$21	-56499.25	125.88	-476.91	-197.43
	$\sigma_{cls,Max}$21	-56499.25	125.88	-476.91	-13.39
	$\sigma_{cls,Med}$21	-56499.25	125.88	-476.91	-12.38

Pilastro: **219/319** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
219	1	-59104.56	220.81	-2845.20	0.08
319	2	-52395.95	-1943.74	-6198.18	0.09

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	634.21	61956.98	999.56	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	634.21	46467.73	999.56	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	634.21	61956.98	999.56	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
219	Ft. 16	-39409.95	165.15	-1900.61	-93.14
	$\sigma_{s,c}$15	-40892.35	149.50	-1964.28	-171.24
	$\sigma_{cls,Max}$15	-40892.35	149.50	-1964.28	-11.94
	$\sigma_{cls,Med}$15	-40892.35	149.50	-1964.28	-8.96
319	Ft. 16	-35959.95	-1307.38	-4176.97	-7.60
	$\sigma_{s,c}$16	-35959.95	-1307.38	-4176.97	-228.44
	$\sigma_{cls,Max}$16	-35959.95	-1307.38	-4176.97	-17.47
	$\sigma_{cls,Med}$15	-37442.35	-1241.16	-3881.73	-8.23
Combinazioni Frequenti					
219	Ft. 19	-38066.63	155.12	-1842.40	-90.00
	$\sigma_{s,c}$18	-38531.48	149.38	-1862.34	-161.81
	$\sigma_{cls,Max}$18	-38531.48	149.38	-1862.34	-11.29
	$\sigma_{cls,Med}$18	-38531.48	149.38	-1862.34	-8.44
319	Ft. 19	-34616.63	-1227.85	-3915.93	-10.22
	$\sigma_{s,c}$19	-34616.63	-1227.85	-3915.93	-217.09
	$\sigma_{cls,Max}$19	-34616.63	-1227.85	-3915.93	-16.58
	$\sigma_{cls,Med}$18	-35081.48	-1202.27	-3805.12	-7.74
Combinazioni Quasi Permanenti					
219	Ft. 21	-37890.94	151.96	-1834.74	-89.65
	$\sigma_{s,c}$21	-37890.94	151.96	-1834.74	-159.34
	$\sigma_{cls,Max}$21	-37890.94	151.96	-1834.74	-11.12
	$\sigma_{cls,Med}$21	-37890.94	151.96	-1834.74	-8.30
319	Ft. 22	-34438.32	-1208.00	-3840.92	-11.58
	$\sigma_{s,c}$22	-34438.32	-1208.00	-3840.92	-214.59
	$\sigma_{cls,Max}$22	-34438.32	-1208.00	-3840.92	-16.37
	$\sigma_{cls,Med}$21	-34440.94	-1206.83	-3841.56	-7.63

Pilastro: **319/11545** / L 4.05[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 205.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
319	2	-24284.23	-2954.66	-8527.49	0.11
11545	2	-18694.23	-14444.13	-1229.03	0.51

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2671.97	61956.98	1697.31	86297.23	ø 10 4br.x2br./15.0
1.13	3.18	2671.97	46467.73	1697.31	64722.92	ø 10 4br.x2br./20.0
3.18	4.18	2671.97	61956.98	1697.31	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
319	Ft. 16	-16904.00	-1991.80	-5758.49	259.92

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$16	-16904.00	-1991.80	-5758.49	-274.31
	$\sigma_{cls,Max}$16	-16904.00	-1991.80	-5758.49	-23.91
	$\sigma_{cls,Med}$16	-16904.00	-1991.80	-5758.49	-8.00
11545	Ft. 16	-12604.00	-9744.57	-827.62	1630.47
	$\sigma_{s,c}$16	-12604.00	-9744.57	-827.62	-403.90
	$\sigma_{cls,Max}$16	-12604.00	-9744.57	-827.62	-62.61
	$\sigma_{cls,Med}$16	-12604.00	-9744.57	-827.62	-30.03
Combinazioni Frequenti					
319	Ft. 19	-16188.44	-1875.00	-5443.76	240.70
	$\sigma_{s,c}$19	-16188.44	-1875.00	-5443.76	-258.57
	$\sigma_{cls,Max}$19	-16188.44	-1875.00	-5443.76	-22.49
	$\sigma_{cls,Med}$19	-16188.44	-1875.00	-5443.76	-7.53
11545	Ft. 19	-11888.44	-9195.32	-779.77	1538.66
	$\sigma_{s,c}$19	-11888.44	-9195.32	-779.77	-381.06
	$\sigma_{cls,Max}$19	-11888.44	-9195.32	-779.77	-59.07
	$\sigma_{cls,Med}$19	-11888.44	-9195.32	-779.77	-28.34
Combinazioni Quasi Permanenti					
319	Ft. 21	-16009.60	-1844.38	-5367.63	235.89
	$\sigma_{s,c}$21	-16009.60	-1844.38	-5367.63	-254.63
	$\sigma_{cls,Max}$21	-16009.60	-1844.38	-5367.63	-22.13
	$\sigma_{cls,Med}$21	-16009.60	-1844.38	-5367.63	-7.42
11545	Ft. 21	-11709.60	-9058.33	-767.81	1515.77
	$\sigma_{s,c}$21	-11709.60	-9058.33	-767.81	-375.36
	$\sigma_{cls,Max}$21	-11709.60	-9058.33	-767.81	-58.19
	$\sigma_{cls,Med}$21	-11709.60	-9058.33	-767.81	-27.91

Pilastro: **20/120** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
20	1	-155298.28	8778.86	-522.60	0.21
120	1	-149643.28	901.75	193.33	0.17

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1812.60	86297.23	166.10	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	1812.60	64722.92	166.10	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	1812.60	86297.23	166.10	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
20	Ft. 16	-102128.80	6382.31	-314.37	-221.15
	$\sigma_{s,c}$15	-106882.80	6490.10	-346.80	-468.36
	$\sigma_{cls,Max}$15	-106882.80	6490.10	-346.80	-32.77
	$\sigma_{cls,Med}$15	-106882.80	6490.10	-346.80	-23.41
120	Ft. 16	-97778.80	490.81	103.28	-309.94
	$\sigma_{s,c}$15	-102532.80	603.75	126.11	-350.76
	$\sigma_{cls,Max}$15	-102532.80	603.75	126.11	-23.64
	$\sigma_{cls,Med}$15	-102532.80	603.75	126.11	-22.46

Combinazioni Frequenti					
20	Ft. 19	-98573.23	6424.90	-293.03	-209.45
	$\sigma_{s,c}$18	-100089.92	6463.54	-303.48	-444.23
	$\sigma_{cls,Max}$18	-100089.92	6463.54	-303.48	-31.11
	$\sigma_{cls,Med}$20	-100093.48	6193.15	-304.15	-21.92
120	Ft. 19	-94223.23	482.86	96.76	-298.60
	$\sigma_{s,c}$20	-95743.48	525.32	105.76	-326.52
	$\sigma_{cls,Max}$20	-95743.48	525.32	105.76	-21.98
	$\sigma_{cls,Med}$20	-95743.48	525.32	105.76	-20.97
Combinazioni Quasi Permanenti					
20	Ft. 21	-98165.45	6441.15	-290.85	-207.91
	$\sigma_{s,c}$21	-98165.45	6441.15	-290.85	-437.14
	$\sigma_{cls,Max}$21	-98165.45	6441.15	-290.85	-30.62
	$\sigma_{cls,Med}$22	-98168.75	6215.99	-289.93	-21.50
120	Ft. 22	-93818.75	492.13	97.51	-297.09
	$\sigma_{s,c}$22	-93818.75	492.13	97.51	-319.40
	$\sigma_{cls,Max}$22	-93818.75	492.13	97.51	-21.49
	$\sigma_{cls,Med}$22	-93818.75	492.13	97.51	-20.55

Pilastro: **120/220** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
120	1	-118289.37	-1474.80	-97.51	0.14
220	1	-113804.37	-1807.29	-61.28	0.14

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	176.27	86297.23	10.50	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	176.27	64722.92	10.50	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	176.27	86297.23	10.50	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
120	Ft. 16	-78484.70	-966.03	-73.41	-239.73
	$\sigma_{s,c}$15	-81312.52	-1002.85	-69.97	-285.78
	$\sigma_{cls,Max}$15	-81312.52	-1002.85	-69.97	-19.31
	$\sigma_{cls,Med}$15	-81312.52	-1002.85	-69.97	-17.81
220	Ft. 16	-75034.70	-1397.77	-53.61	-221.96
	$\sigma_{s,c}$15	-77862.52	-1250.83	-40.34	-277.56
	$\sigma_{cls,Max}$15	-77862.52	-1250.83	-40.34	-18.77
	$\sigma_{cls,Med}$15	-77862.52	-1250.83	-40.34	-17.05
Combinazioni Frequenti					
120	Ft. 19	-75570.43	-924.52	-72.43	-230.86
	$\sigma_{s,c}$18	-76445.05	-935.78	-71.21	-268.73
	$\sigma_{cls,Max}$18	-76445.05	-935.78	-71.21	-18.16
	$\sigma_{cls,Med}$20	-76448.77	-934.61	-69.55	-16.74
220	Ft. 19	-72120.43	-1322.42	-48.76	-213.77
	$\sigma_{s,c}$18	-72995.05	-1269.16	-44.02	-261.99
	$\sigma_{cls,Max}$18	-72995.05	-1269.16	-44.02	-17.74
	$\sigma_{cls,Med}$20	-72998.77	-1251.48	-44.87	-15.99
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
120	Ft. 21	-75162.50	-918.47	-71.99	-229.63
	$\sigma_{s,c}$21	-75162.50	-918.47	-71.99	-264.26
	$\sigma_{cls,Max}$21	-75162.50	-918.47	-71.99	-17.86
	$\sigma_{cls,Med}$22	-75165.84	-917.64	-70.78	-16.46
220	Ft. 21	-71712.50	-1296.70	-46.84	-212.91
	$\sigma_{s,c}$21	-71712.50	-1296.70	-46.84	-258.31
	$\sigma_{cls,Max}$21	-71712.50	-1296.70	-46.84	-17.50
	$\sigma_{cls,Med}$22	-71715.84	-1281.87	-47.74	-15.71

Pilastro: **220/320** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
220	1	-82507.01	-4260.50	-184.16	0.11
320	1	-78022.01	-4718.43	-1086.37	0.11

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	235.12	86297.23	273.22	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	235.12	64722.92	273.22	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	235.12	86297.23	273.22	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
220	Ft. 16	-55779.97	-2911.98	-131.41	-131.45
	$\sigma_{s,c}$15	-56683.25	-2909.59	-124.63	-237.79
	$\sigma_{cls,Max}$15	-56683.25	-2909.59	-124.63	-16.51
	$\sigma_{cls,Med}$15	-56683.25	-2909.59	-124.63	-12.42
320	Ft. 16	-52329.97	-3423.19	-765.59	-91.58
	$\sigma_{s,c}$16	-52329.97	-3423.19	-765.59	-252.28
	$\sigma_{cls,Max}$16	-52329.97	-3423.19	-765.59	-18.30
	$\sigma_{cls,Med}$15	-53233.25	-3185.30	-731.89	-11.66
Combinazioni Frequenti					
220	Ft. 19	-53506.99	-2783.55	-124.17	-126.32
	$\sigma_{s,c}$18	-53740.09	-2778.30	-121.59	-225.88
	$\sigma_{cls,Max}$18	-53740.09	-2778.30	-121.59	-15.69
	$\sigma_{cls,Med}$20	-53742.79	-2762.92	-121.14	-11.77
320	Ft. 19	-50056.99	-3212.86	-720.60	-88.99
	$\sigma_{s,c}$19	-50056.99	-3212.86	-720.60	-239.94
	$\sigma_{cls,Max}$19	-50056.99	-3212.86	-720.60	-17.39
	$\sigma_{cls,Med}$20	-50292.79	-3119.15	-708.17	-11.02
Combinazioni Quasi Permanenti					
220	Ft. 21	-53099.02	-2756.82	-122.21	-125.48
	$\sigma_{s,c}$21	-53099.02	-2756.82	-122.21	-223.44
	$\sigma_{cls,Max}$21	-53099.02	-2756.82	-122.21	-15.52
	$\sigma_{cls,Med}$22	-53101.41	-2744.02	-121.88	-11.63
320	Ft. 21	-49649.02	-3152.94	-708.97	-89.00
	$\sigma_{s,c}$21	-49649.02	-3152.94	-708.97	-237.25
	$\sigma_{cls,Max}$21	-49649.02	-3152.94	-708.97	-17.19

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$22	-49651.41	-3149.10	-709.65	-10.88

Pilastro: **320/11569** / L 4.05[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 205.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
320	2	-47965.20	-7695.34	-2212.28	0.10
11569	2	-42375.20	3998.20	4800.87	0.11

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2719.43	86297.23	1630.96	61956.98	ø 10 2br.x4br./15.0
1.13	3.18	2719.43	64722.92	1630.96	46467.73	ø 10 2br.x4br./20.0
3.18	4.18	2719.43	86297.23	1630.96	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
320	Ft. 16	-32879.70	-5197.17	-1491.56	32.95
	$\sigma_{s,c}$16	-32879.70	-5197.17	-1491.56	-245.23
	$\sigma_{cls,Max}$16	-32879.70	-5197.17	-1491.56	-19.12
	$\sigma_{cls,Med}$16	-32879.70	-5197.17	-1491.56	-7.91
11569	Ft. 16	-28579.70	2697.42	3238.09	116.72
	$\sigma_{s,c}$16	-28579.70	2697.42	3238.09	-265.86
	$\sigma_{cls,Max}$16	-28579.70	2697.42	3238.09	-23.08
	$\sigma_{cls,Med}$16	-28579.70	2697.42	3238.09	-9.41
Combinazioni Frequenti					
320	Ft. 19	-31259.90	-4919.50	-1405.98	30.25
	$\sigma_{s,c}$19	-31259.90	-4919.50	-1405.98	-232.23
	$\sigma_{cls,Max}$19	-31259.90	-4919.50	-1405.98	-18.09
	$\sigma_{cls,Med}$19	-31259.90	-4919.50	-1405.98	-7.50
11569	Ft. 19	-26959.90	2544.58	3054.15	110.06
	$\sigma_{s,c}$19	-26959.90	2544.58	3054.15	-250.77
	$\sigma_{cls,Max}$19	-26959.90	2544.58	3054.15	-21.77
	$\sigma_{cls,Med}$19	-26959.90	2544.58	3054.15	-8.87
Combinazioni Quasi Permanenti					
320	Ft. 21	-30854.91	-4854.91	-1384.23	29.67
	$\sigma_{s,c}$21	-30854.91	-4854.91	-1384.23	-229.06
	$\sigma_{cls,Max}$21	-30854.91	-4854.91	-1384.23	-17.84
	$\sigma_{cls,Med}$21	-30854.91	-4854.91	-1384.23	-7.40
11569	Ft. 21	-26554.91	2506.48	3007.86	108.37
	$\sigma_{s,c}$21	-26554.91	2506.48	3007.86	-246.98
	$\sigma_{cls,Max}$21	-26554.91	2506.48	3007.86	-21.44
	$\sigma_{cls,Med}$21	-26554.91	2506.48	3007.86	-8.74

Pilastro: **21/121** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
21	1	-414888.25	10555.86	949.55	0.51

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
121	1	-409233.25	1166.70	-4651.81	0.51

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3703.08	86297.23	1353.18	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	3703.08	64722.92	1353.18	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	3703.08	86297.23	1353.18	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
21	Ft. 16	-279701.91	7332.98	506.09	-782.92
	$\sigma_{s,c}$15	-290335.44	7444.05	626.71	-1095.60
	$\sigma_{cls,Max}$15	-290335.44	7444.05	626.71	-75.08
	$\sigma_{cls,Med}$15	-290335.44	7444.05	626.71	-63.59
121	Ft. 17	-279594.84	1102.76	-3318.92	-794.99
	$\sigma_{s,c}$15	-285985.44	817.11	-3245.27	-1056.22
	$\sigma_{cls,Max}$15	-285985.44	817.11	-3245.27	-74.27
	$\sigma_{cls,Med}$15	-285985.44	817.11	-3245.27	-62.64
Combinazioni Frequenti					
21	Ft. 19	-276153.72	7296.28	468.43	-773.06
	$\sigma_{s,c}$18	-279698.09	7333.31	508.73	-1055.09
	$\sigma_{cls,Max}$18	-279698.09	7333.31	508.73	-72.22
	$\sigma_{cls,Med}$18	-279698.09	7333.31	508.73	-61.26
121	Ft. 20	-274497.63	968.75	-3118.24	-786.82
	$\sigma_{s,c}$20	-274497.63	968.75	-3118.24	-1016.91
	$\sigma_{cls,Max}$20	-274497.63	968.75	-3118.24	-71.53
	$\sigma_{cls,Med}$18	-275348.09	709.46	-3030.26	-60.31
Combinazioni Quasi Permanenti					
21	Ft. 21	-276152.97	7296.35	468.96	-773.04
	$\sigma_{s,c}$21	-276152.97	7296.35	468.96	-1041.57
	$\sigma_{cls,Max}$21	-276152.97	7296.35	468.96	-71.27
	$\sigma_{cls,Med}$22	-277148.56	6858.82	572.13	-60.71
121	Ft. 22	-272798.56	924.08	-3051.34	-784.10
	$\sigma_{s,c}$22	-272798.56	924.08	-3051.34	-1008.47
	$\sigma_{cls,Max}$22	-272798.56	924.08	-3051.34	-70.88
	$\sigma_{cls,Med}$22	-272798.56	924.08	-3051.34	-59.75

Pilastro: **121/221** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
121	1	-340325.84	-8052.96	7240.59	0.45
221	1	-335840.84	3868.59	-4645.09	0.43

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3455.52	86297.23	3445.13	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	3455.52	64722.92	3445.13	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	3455.52	86297.23	3445.13	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
121	Ft. 17	-231069.52	-5561.59	5030.11	-508.19
	$\sigma_{s,c}$15	-237147.05	-5694.16	5087.38	-1034.13
	$\sigma_{cls,Max}$15	-237147.05	-5694.16	5087.38	-75.76
	$\sigma_{cls,Med}$15	-237147.05	-5694.16	5087.38	-51.94
221	Ft. 16	-225607.25	2460.26	-3077.19	-603.10
	$\sigma_{s,c}$15	-233697.05	2706.02	-3264.34	-915.92
	$\sigma_{cls,Max}$15	-233697.05	2706.02	-3264.34	-65.27
	$\sigma_{cls,Med}$15	-233697.05	2706.02	-3264.34	-51.19
Combinazioni Frequenti					
121	Ft. 19	-226358.81	-5308.36	4711.81	-506.98
	$\sigma_{s,c}$18	-229055.36	-5404.18	4806.52	-993.87
	$\sigma_{cls,Max}$18	-229055.36	-5404.18	4806.52	-72.71
	$\sigma_{cls,Med}$18	-229055.36	-5404.18	4806.52	-50.17
221	Ft. 19	-222908.81	2376.62	-3017.55	-597.50
	$\sigma_{s,c}$18	-225605.36	2458.49	-3080.02	-879.43
	$\sigma_{cls,Max}$18	-225605.36	2458.49	-3080.02	-62.58
	$\sigma_{cls,Med}$18	-225605.36	2458.49	-3080.02	-49.42
Combinazioni Quasi Permanenti					
121	Ft. 21	-226358.44	-5307.90	4712.40	-506.97
	$\sigma_{s,c}$22	-227709.11	-5221.38	4695.02	-982.91
	$\sigma_{cls,Max}$22	-227709.11	-5221.38	4695.02	-71.82
	$\sigma_{cls,Med}$22	-227709.11	-5221.38	4695.02	-49.88
221	Ft. 21	-222908.44	2376.27	-3018.11	-597.49
	$\sigma_{s,c}$21	-222908.44	2376.27	-3018.11	-867.25
	$\sigma_{cls,Max}$21	-222908.44	2376.27	-3018.11	-61.69
	$\sigma_{cls,Med}$22	-224259.11	1877.55	-2868.01	-49.12

Pilastro: **221/321** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
221	1	-262639.06	-5893.15	3718.98	0.34
321	3	-249718.78	23596.25	-7730.81	0.40

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	8841.84	86297.23	3466.88	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	8841.84	64722.92	3466.88	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	8841.84	86297.23	3466.88	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
221	Ft. 17	-176200.45	-4872.40	2905.14	-406.79
	$\sigma_{s,c}$17	-176200.45	-4872.40	2905.14	-751.03
	$\sigma_{cls,Max}$17	-176200.45	-4872.40	2905.14	-54.25
	$\sigma_{cls,Med}$15	-181823.97	-4195.77	2564.52	-39.83
321	Ft. 17	-172750.45	16269.49	-5270.35	-133.79
	$\sigma_{s,c}$17	-172750.45	16269.49	-5270.35	-1001.36
	$\sigma_{cls,Max}$17	-172750.45	16269.49	-5270.35	-75.66

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-178373.97	13548.82	-4332.18	-39.07
Combinazioni Frequenti					
221	Ft. 20	-176423.81	-4833.35	2773.01	-412.37
	$\sigma_{s,c}$20	-176423.81	-4833.35	2773.01	-746.92
	$\sigma_{cls,Max}$20	-176423.81	-4833.35	2773.01	-53.82
	$\sigma_{cls,Med}$18	-176452.44	-4058.49	2393.04	-38.65
321	Ft. 20	-172973.81	16233.85	-5095.80	-140.66
	$\sigma_{s,c}$20	-172973.81	16233.85	-5095.80	-995.96
	$\sigma_{cls,Max}$20	-172973.81	16233.85	-5095.80	-75.10
	$\sigma_{cls,Med}$18	-173002.44	13059.67	-4058.75	-37.89
Combinazioni Quasi Permanenti					
221	Ft. 22	-176498.27	-4820.34	2728.97	-414.23
	$\sigma_{s,c}$22	-176498.27	-4820.34	2728.97	-745.55
	$\sigma_{cls,Max}$22	-176498.27	-4820.34	2728.97	-53.68
	$\sigma_{cls,Med}$22	-176498.27	-4820.34	2728.97	-38.66
321	Ft. 22	-173048.27	16221.97	-5037.62	-142.95
	$\sigma_{s,c}$22	-173048.27	16221.97	-5037.62	-994.15
	$\sigma_{cls,Max}$22	-173048.27	16221.97	-5037.62	-74.91
	$\sigma_{cls,Med}$22	-173048.27	16221.97	-5037.62	-37.90

Pilastro: **22/122** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
22	1	-456133.72	10040.43	1048.00	0.56
122	1	-450478.72	839.35	-200.69	0.52

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4353.43	86297.23	418.76	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	4353.43	64722.92	418.76	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	4353.43	86297.23	418.76	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
22	Ft. 16	-306816.53	6889.00	661.51	-874.32
	$\sigma_{s,c}$15	-318941.78	7028.15	709.64	-1185.42
	$\sigma_{cls,Max}$15	-318941.78	7028.15	709.64	-81.09
	$\sigma_{cls,Med}$15	-318941.78	7028.15	709.64	-69.86
122	Ft. 16	-302466.53	544.12	-106.47	-981.47
	$\sigma_{s,c}$15	-314591.78	632.83	-120.07	-1047.77
	$\sigma_{cls,Max}$15	-314591.78	632.83	-120.07	-70.10
	$\sigma_{cls,Med}$15	-314591.78	632.83	-120.07	-68.91
Combinazioni Frequenti					
22	Ft. 19	-302783.72	6845.73	645.16	-862.30
	$\sigma_{s,c}$18	-306825.84	6892.22	661.19	-1141.85
	$\sigma_{cls,Max}$18	-306825.84	6892.22	661.19	-78.10
	$\sigma_{cls,Med}$18	-306825.84	6892.22	661.19	-67.21
122	Ft. 19	-298433.72	515.74	-101.60	-968.84

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-302475.84	545.35	-106.12	-1006.09
	$\sigma_{cls,Max}$18	-302475.84	545.35	-106.12	-67.29
	$\sigma_{cls,Med}$18	-302475.84	545.35	-106.12	-66.25
Combinazioni Quasi Permanenti					
22	Ft. 21	-302785.59	6846.38	645.10	-862.30
	$\sigma_{s,c}$21	-302785.59	6846.38	645.10	-1127.32
	$\sigma_{cls,Max}$21	-302785.59	6846.38	645.10	-77.11
	$\sigma_{cls,Med}$22	-303057.88	6447.50	621.07	-66.38
122	Ft. 22	-298707.88	760.37	-59.02	-967.10
	$\sigma_{s,c}$22	-298707.88	760.37	-59.02	-995.73
	$\sigma_{cls,Max}$22	-298707.88	760.37	-59.02	-66.58
	$\sigma_{cls,Med}$22	-298707.88	760.37	-59.02	-65.43

Pilastro: **122/222** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
122	1	-368615.94	-8253.38	-674.42	0.45
222	1	-364130.94	4427.30	-70.25	0.43

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3675.56	86297.23	376.44	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	3675.56	64722.92	376.44	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	3675.56	86297.23	376.44	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
122	Ft. 16	-247562.30	-5492.73	-460.46	-708.88
	$\sigma_{s,c}$15	-256630.67	-5786.56	-477.64	-953.01
	$\sigma_{cls,Max}$15	-256630.67	-5786.56	-477.64	-65.11
	$\sigma_{cls,Med}$15	-256630.67	-5786.56	-477.64	-56.21
222	Ft. 16	-244112.30	2774.32	-36.95	-755.48
	$\sigma_{s,c}$15	-253180.67	3055.42	-40.85	-883.11
	$\sigma_{cls,Max}$15	-253180.67	3055.42	-40.85	-59.46
	$\sigma_{cls,Med}$15	-253180.67	3055.42	-40.85	-55.46
Combinazioni Frequenti					
122	Ft. 19	-244547.63	-5391.98	-453.93	-700.83
	$\sigma_{s,c}$18	-247570.70	-5489.82	-459.63	-917.82
	$\sigma_{cls,Max}$18	-247570.70	-5489.82	-459.63	-62.69
	$\sigma_{cls,Med}$18	-247570.70	-5489.82	-459.63	-54.23
222	Ft. 19	-241097.63	2678.11	-36.22	-747.17
	$\sigma_{s,c}$18	-244120.70	2771.72	-37.54	-848.60
	$\sigma_{cls,Max}$18	-244120.70	2771.72	-37.54	-57.11
	$\sigma_{cls,Med}$18	-244120.70	2771.72	-37.54	-53.47
Combinazioni Quasi Permanenti					
122	Ft. 21	-244549.31	-5391.39	-453.77	-700.85
	$\sigma_{s,c}$21	-244549.31	-5391.39	-453.77	-906.09
	$\sigma_{cls,Max}$21	-244549.31	-5391.39	-453.77	-61.88

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$22	-245048.83	-5298.94	-390.33	-53.67
222	Ft. 21	-241099.31	2677.59	-36.34	-747.18
	$\sigma_{s,c}$22	-241598.83	2165.91	-252.60	-837.24
	$\sigma_{cls,Max}$22	-241598.83	2165.91	-252.60	-56.49
	$\sigma_{cls,Med}$22	-241598.83	2165.91	-252.60	-52.92

Pilastro: **222/322** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
222	1	-283783.69	-5987.50	-98.65	0.34
322	3	-268404.53	24854.95	1887.86	0.39

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	9232.91	86297.23	724.46	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	9232.91	64722.92	724.46	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	9232.91	86297.23	724.46	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
222	Ft. 17	-189013.27	-4978.52	-417.97	-526.28
	$\sigma_{s,c}$15	-196276.05	-4304.45	-76.05	-717.70
	$\sigma_{cls,Max}$17	-189013.27	-4978.52	-417.97	-49.08
	$\sigma_{cls,Med}$15	-196276.05	-4304.45	-76.05	-42.99
322	Ft. 17	-185563.27	17178.29	1274.83	-288.13
	$\sigma_{s,c}$17	-185563.27	17178.29	1274.83	-931.21
	$\sigma_{cls,Max}$17	-185563.27	17178.29	1274.83	-66.59
	$\sigma_{cls,Med}$15	-192826.05	14553.18	157.54	-42.24
Combinazioni Frequenti					
222	Ft. 20	-189013.58	-4967.50	-442.35	-525.68
	$\sigma_{s,c}$20	-189013.58	-4967.50	-442.35	-716.33
	$\sigma_{cls,Max}$20	-189013.58	-4967.50	-442.35	-49.14
	$\sigma_{cls,Med}$18	-190226.55	-4194.99	-93.94	-41.67
322	Ft. 20	-185563.58	17201.20	1319.91	-286.32
	$\sigma_{s,c}$20	-185563.58	17201.20	1319.91	-933.02
	$\sigma_{cls,Max}$20	-185563.58	17201.20	1319.91	-66.76
	$\sigma_{cls,Med}$18	-186776.55	14089.14	185.81	-40.91
Combinazioni Quasi Permanenti					
222	Ft. 22	-189013.70	-4963.83	-450.47	-525.48
	$\sigma_{s,c}$22	-189013.70	-4963.83	-450.47	-716.53
	$\sigma_{cls,Max}$22	-189013.70	-4963.83	-450.47	-49.16
	$\sigma_{cls,Med}$22	-189013.70	-4963.83	-450.47	-41.40
322	Ft. 22	-185563.70	17208.84	1334.94	-285.72
	$\sigma_{s,c}$22	-185563.70	17208.84	1334.94	-933.63
	$\sigma_{cls,Max}$22	-185563.70	17208.84	1334.94	-66.82
	$\sigma_{cls,Med}$22	-185563.70	17208.84	1334.94	-40.64

Pilastro: **23/123** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
23	1	-463480.13	11544.75	798.91	0.57
123	1	-457825.13	-94.79	-1118.68	0.53

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5174.99	86297.23	539.24	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	5174.99	64722.92	539.24	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	5174.99	86297.23	539.24	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm^2]
Combinazioni Rare					
23	Ft. 17	-314564.16	8292.29	562.17	-879.99
	$\sigma_{s,c}$15	-324253.31	8050.86	540.50	-1214.22
	$\sigma_{cls,Max}$15	-324253.31	8050.86	540.50	-82.99
	$\sigma_{cls,Med}$15	-324253.31	8050.86	540.50	-71.02
123	Ft. 16	-307635.19	-51.43	-732.79	-986.59
	$\sigma_{s,c}$15	-319903.31	9.71	-782.53	-1076.10
	$\sigma_{cls,Max}$15	-319903.31	9.71	-782.53	-72.64
	$\sigma_{cls,Med}$15	-319903.31	9.71	-782.53	-70.07
Combinazioni Frequenti					
23	Ft. 20	-308451.69	8237.35	506.32	-862.58
	$\sigma_{s,c}$18	-311970.72	7864.64	489.71	-1169.21
	$\sigma_{cls,Max}$18	-311970.72	7864.64	489.71	-79.90
	$\sigma_{cls,Med}$18	-311970.72	7864.64	489.71	-68.33
123	Ft. 20	-304101.69	-289.66	-759.21	-970.24
	$\sigma_{s,c}$18	-307620.72	-49.90	-731.22	-1034.77
	$\sigma_{cls,Max}$18	-307620.72	-49.90	-731.22	-69.83
	$\sigma_{cls,Med}$18	-307620.72	-49.90	-731.22	-67.38
Combinazioni Quasi Permanenti					
23	Ft. 22	-306414.22	8219.03	487.70	-856.78
	$\sigma_{s,c}$22	-306414.22	8219.03	487.70	-1156.68
	$\sigma_{cls,Max}$22	-306414.22	8219.03	487.70	-79.13
	$\sigma_{cls,Med}$21	-307878.97	7802.16	472.88	-67.44
123	Ft. 22	-302064.22	-321.08	-742.17	-963.58
	$\sigma_{s,c}$22	-302064.22	-321.08	-742.17	-1021.30
	$\sigma_{cls,Max}$22	-302064.22	-321.08	-742.17	-68.99
	$\sigma_{cls,Med}$21	-303528.97	-70.03	-714.38	-66.48

Pilastro: **123/223** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
123	1	-375793.78	-8861.09	1091.09	0.46
223	1	-371308.78	4344.35	-932.04	0.44

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3973.85	86297.23	619.87	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	3973.85	64722.92	619.87	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	3973.85	86297.23	619.87	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
123	Ft. 17	-252157.05	-6123.01	694.49	-706.22
	$\sigma_{s,c}$15	-261793.89	-6183.17	792.14	-986.47
	$\sigma_{cls,Max}$15	-261793.89	-6183.17	792.14	-67.77
	$\sigma_{cls,Med}$15	-261793.89	-6183.17	792.14	-57.34
223	Ft. 17	-248707.05	3392.27	-416.31	-748.40
	$\sigma_{s,c}$15	-258343.89	2995.88	-670.80	-919.14
	$\sigma_{cls,Max}$15	-258343.89	2995.88	-670.80	-62.57
	$\sigma_{cls,Med}$15	-258343.89	2995.88	-670.80	-56.59
Combinazioni Frequenti					
123	Ft. 20	-249120.19	-5857.35	643.78	-702.20
	$\sigma_{s,c}$18	-252577.02	-5870.80	744.58	-949.56
	$\sigma_{cls,Max}$18	-252577.02	-5870.80	744.58	-65.20
	$\sigma_{cls,Med}$18	-252577.02	-5870.80	744.58	-55.32
223	Ft. 20	-245670.19	3062.65	-366.12	-745.41
	$\sigma_{s,c}$18	-249127.02	2713.34	-629.07	-882.91
	$\sigma_{cls,Max}$18	-249127.02	2713.34	-629.07	-60.06
	$\sigma_{cls,Med}$18	-249127.02	2713.34	-629.07	-54.57
Combinazioni Quasi Permanenti					
123	Ft. 22	-248107.88	-5768.80	626.87	-700.86
	$\sigma_{s,c}$21	-249506.81	-5767.16	729.08	-937.29
	$\sigma_{cls,Max}$21	-249506.81	-5767.16	729.08	-64.34
	$\sigma_{cls,Med}$21	-249506.81	-5767.16	729.08	-54.65
223	Ft. 22	-244657.88	2952.78	-349.39	-744.41
	$\sigma_{s,c}$21	-246056.81	2619.51	-615.42	-870.85
	$\sigma_{cls,Max}$21	-246056.81	2619.51	-615.42	-59.22
	$\sigma_{cls,Med}$21	-246056.81	2619.51	-615.42	-53.89

Pilastro: **223/323** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
223	1	-289956.81	-5798.93	908.08	0.35
323	1	-285471.81	20081.36	-1891.80	0.39

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	7501.54	86297.23	1460.43	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	7501.54	64722.92	1460.43	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	7501.54	86297.23	1460.43	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
223	Ft. 17	-191078.72	-3326.90	1018.02	-540.99

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-200700.17	-4167.22	663.10	-748.66
	$\sigma_{cls,Max}$15	-200700.17	-4167.22	663.10	-51.41
	$\sigma_{cls,Med}$15	-200700.17	-4167.22	663.10	-43.96
323	Ft. 17	-187628.72	10611.91	-2494.20	-363.53
	$\sigma_{s,c}$15	-197250.17	13947.43	-1356.71	-919.37
	$\sigma_{cls,Max}$15	-197250.17	13947.43	-1356.71	-65.32
	$\sigma_{cls,Med}$15	-197250.17	13947.43	-1356.71	-43.20
Combinazioni Frequenti					
223	Ft. 20	-191115.70	-3316.53	977.65	-542.56
	$\sigma_{s,c}$18	-194536.58	-4069.00	615.74	-725.30
	$\sigma_{cls,Max}$18	-194536.58	-4069.00	615.74	-49.78
	$\sigma_{cls,Med}$18	-194536.58	-4069.00	615.74	-42.61
323	Ft. 19	-189035.97	13381.11	-1253.73	-362.32
	$\sigma_{s,c}$18	-191086.58	13521.85	-1277.86	-889.65
	$\sigma_{cls,Max}$18	-191086.58	13521.85	-1277.86	-63.17
	$\sigma_{cls,Med}$18	-191086.58	13521.85	-1277.86	-41.85
Combinazioni Quasi Permanenti					
223	Ft. 22	-191128.03	-3313.07	964.20	-543.09
	$\sigma_{s,c}$21	-192483.83	-4036.16	600.49	-717.53
	$\sigma_{cls,Max}$21	-192483.83	-4036.16	600.49	-49.24
	$\sigma_{cls,Med}$21	-192483.83	-4036.16	600.49	-42.16
323	Ft. 21	-189033.83	13380.50	-1252.56	-362.36
	$\sigma_{s,c}$21	-189033.83	13380.50	-1252.56	-879.79
	$\sigma_{cls,Max}$22	-187678.03	10666.79	-2432.83	-62.57
	$\sigma_{cls,Med}$21	-189033.83	13380.50	-1252.56	-41.40

Pilastro: **24/124** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
24	1	-270944.38	14122.91	8431.76	0.40
124	1	-265289.41	-1583.73	1201.98	0.31

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5380.24	86297.23	2303.07	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	5380.24	64722.92	2303.07	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	5380.24	86297.23	2303.07	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
24	Ft. 16	-183997.23	9865.45	5877.80	-256.17
	$\sigma_{s,c}$15	-191123.88	10112.00	6036.41	-985.38
	$\sigma_{cls,Max}$15	-191123.88	10112.00	6036.41	-74.38
	$\sigma_{cls,Med}$15	-191123.88	10112.00	6036.41	-41.86
124	Ft. 17	-179901.77	-1085.07	1060.75	-539.58
	$\sigma_{s,c}$15	-186773.88	-1151.88	792.58	-657.70
	$\sigma_{cls,Max}$15	-186773.88	-1151.88	792.58	-44.96
	$\sigma_{cls,Med}$15	-186773.88	-1151.88	792.58	-40.91

Combinazioni Frequenti					
24	Ft. 19	-181486.52	9752.37	5799.17	-252.27
	$\sigma_{s,c}$18	-183857.39	9833.48	5851.15	-951.05
	$\sigma_{cls,Max}$18	-183857.39	9833.48	5851.15	-71.83
	$\sigma_{cls,Med}$18	-183857.39	9833.48	5851.15	-40.27
124	Ft. 20	-176182.77	-1140.23	914.97	-531.09
	$\sigma_{s,c}$18	-179507.39	-1160.21	697.03	-630.93
	$\sigma_{cls,Max}$18	-179507.39	-1160.21	697.03	-43.06
	$\sigma_{cls,Med}$18	-179507.39	-1160.21	697.03	-39.32
Combinazioni Quasi Permanenti					
24	Ft. 21	-181458.55	9745.97	5793.84	-252.46
	$\sigma_{s,c}$21	-181458.55	9745.97	5793.84	-939.92
	$\sigma_{cls,Max}$21	-181458.55	9745.97	5793.84	-71.01
	$\sigma_{cls,Med}$21	-181458.55	9745.97	5793.84	-39.75
124	Ft. 22	-174943.11	-1158.61	866.37	-528.27
	$\sigma_{s,c}$21	-177108.55	-1165.06	662.56	-622.03
	$\sigma_{cls,Max}$22	-174943.11	-1158.61	866.37	-42.61
	$\sigma_{cls,Med}$21	-177108.55	-1165.06	662.56	-38.79

Pilastro: **124/224** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
124	1	-202871.34	-7031.11	-11337.66	0.34
224	1	-198386.34	2276.87	9096.05	0.31

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	2772.61	86297.23	5966.94	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	2772.61	64722.92	5966.94	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	2772.61	86297.23	5966.94	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
124	Ft. 17	-136053.86	-4856.46	-8017.94	-112.22
	$\sigma_{s,c}$15	-142477.66	-4947.80	-7980.00	-802.92
	$\sigma_{cls,Max}$15	-142477.66	-4947.80	-7980.00	-63.52
	$\sigma_{cls,Med}$15	-142477.66	-4947.80	-7980.00	-31.24
224	Ft. 17	-132603.86	1873.95	6489.18	-198.59
	$\sigma_{s,c}$15	-139027.66	1610.92	6425.63	-687.54
	$\sigma_{cls,Max}$15	-139027.66	1610.92	6425.63	-53.46
	$\sigma_{cls,Med}$15	-139027.66	1610.92	6425.63	-30.45
Combinazioni Frequenti					
124	Ft. 20	-134574.58	-4672.67	-7635.37	-122.77
	$\sigma_{s,c}$18	-137486.36	-4720.36	-7574.28	-769.88
	$\sigma_{cls,Max}$18	-137486.36	-4720.36	-7574.28	-60.81
	$\sigma_{cls,Med}$18	-137486.36	-4720.36	-7574.28	-30.12
224	Ft. 20	-131124.58	1671.61	6131.97	-208.40
	$\sigma_{s,c}$18	-134036.34	1445.21	6078.13	-657.38
	$\sigma_{cls,Max}$18	-134036.34	1445.21	6078.13	-51.02
	$\sigma_{cls,Med}$18	-134036.34	1445.21	6078.13	-29.36
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
124	Ft. 22	-134081.48	-4611.40	-7507.84	-126.24
	$\sigma_{s,c}$21	-135841.58	-4645.27	-7437.86	-758.91
	$\sigma_{cls,Max}$21	-135841.58	-4645.27	-7437.86	-59.91
	$\sigma_{cls,Med}$21	-135841.58	-4645.27	-7437.86	-29.76
224	Ft. 22	-130631.48	1604.16	6012.90	-211.67
	$\sigma_{s,c}$21	-132391.56	1390.21	5961.15	-647.35
	$\sigma_{cls,Max}$22	-130631.48	1604.16	6012.90	-50.27
	$\sigma_{cls,Med}$21	-132391.56	1390.21	5961.15	-29.00

Pilastro: **224/324** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
224	1	-149812.92	-6047.62	-14509.30	0.33
324	1	-145327.92	18029.87	21704.53	0.50

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	6978.98	86297.23	10496.76	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	6978.98	64722.92	10496.76	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	6978.98	86297.23	10496.76	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
224	Ft. 17	-98054.34	-3739.00	-10004.56	148.91
	$\sigma_{s,c}$15	-104376.27	-4195.87	-10041.70	-759.11
	$\sigma_{cls,Max}$15	-104376.27	-4195.87	-10041.70	-64.23
	$\sigma_{cls,Med}$15	-104376.27	-4195.87	-10041.70	-29.02
324	Ft. 17	-94604.34	10330.38	14764.45	984.07
	$\sigma_{s,c}$15	-100926.27	12307.14	14897.63	-1196.15
	$\sigma_{cls,Max}$15	-100926.27	12307.14	14897.63	-110.34
	$\sigma_{cls,Med}$15	-100926.27	12307.14	14897.63	-43.83
Combinazioni Frequenti					
224	Ft. 20	-98698.85	-3692.08	-9733.35	121.36
	$\sigma_{s,c}$18	-101323.52	-4068.03	-9613.81	-730.82
	$\sigma_{cls,Max}$18	-101323.52	-4068.03	-9613.81	-61.68
	$\sigma_{cls,Med}$20	-98698.85	-3692.08	-9733.35	-27.97
324	Ft. 20	-95248.85	10305.60	14580.05	942.41
	$\sigma_{s,c}$18	-97873.52	11911.49	14349.22	-1154.08
	$\sigma_{cls,Max}$18	-97873.52	11911.49	14349.22	-106.27
	$\sigma_{cls,Med}$20	-95248.85	10305.60	14580.05	-42.65
Combinazioni Quasi Permanenti					
224	Ft. 22	-98913.69	-3676.44	-9642.95	112.59
	$\sigma_{s,c}$21	-100321.27	-4023.97	-9468.74	-721.30
	$\sigma_{cls,Max}$22	-98913.69	-3676.44	-9642.95	-61.02
	$\sigma_{cls,Med}$22	-98913.69	-3676.44	-9642.95	-27.77
324	Ft. 22	-95463.69	10297.34	14518.58	928.68
	$\sigma_{s,c}$21	-96871.27	11775.25	14162.20	-1139.72
	$\sigma_{cls,Max}$21	-96871.27	11775.25	14162.20	-104.87

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$22	-95463.69	10297.34	14518.58	-42.45

Pilastro: **25/125** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
25	1	-155315.05	9183.00	357.25	0.21
125	1	-149660.05	1061.23	-146.61	0.17

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1881.08	86297.23	139.10	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	1881.08	64722.92	139.10	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	1881.08	86297.23	139.10	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
25	Ft. 16	-102133.63	6714.19	186.96	-219.79
	$\sigma_{s,c}$15	-106887.08	6790.34	223.82	-469.37
	$\sigma_{cls,Max}$15	-106887.08	6790.34	223.82	-32.75
	$\sigma_{cls,Med}$15	-106887.08	6790.34	223.82	-23.41
125	Ft. 16	-97783.63	600.51	-63.63	-309.42
	$\sigma_{s,c}$15	-102537.08	717.28	-89.25	-351.46
	$\sigma_{cls,Max}$15	-102537.08	717.28	-89.25	-23.66
	$\sigma_{cls,Med}$15	-102537.08	717.28	-89.25	-22.46
Combinazioni Frequenti					
25	Ft. 19	-98574.83	6780.87	162.22	-207.79
	$\sigma_{s,c}$18	-100091.24	6809.43	174.08	-445.77
	$\sigma_{cls,Max}$18	-100091.24	6809.43	174.08	-31.13
	$\sigma_{cls,Med}$20	-100096.29	6514.29	186.70	-21.92
125	Ft. 19	-94224.83	592.10	-55.51	-298.13
	$\sigma_{s,c}$20	-95746.29	634.62	-70.29	-327.19
	$\sigma_{cls,Max}$20	-95746.29	634.62	-70.29	-22.01
	$\sigma_{cls,Med}$20	-95746.29	634.62	-70.29	-20.97
Combinazioni Quasi Permanenti					
25	Ft. 21	-98166.35	6799.92	159.64	-206.22
	$\sigma_{s,c}$21	-98166.35	6799.92	159.64	-438.83
	$\sigma_{cls,Max}$21	-98166.35	6799.92	159.64	-30.64
	$\sigma_{cls,Med}$22	-98170.69	6555.24	169.67	-21.50
125	Ft. 22	-93820.69	600.96	-60.61	-296.49
	$\sigma_{s,c}$22	-93820.69	600.96	-60.61	-320.01
	$\sigma_{cls,Max}$22	-93820.69	600.96	-60.61	-21.51
	$\sigma_{cls,Med}$22	-93820.69	600.96	-60.61	-20.55

Pilastro: **125/225** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
125	1	-118306.52	-1322.56	98.71	0.14

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
225	1	-113821.52	-1793.68	80.47	0.14

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	216.26	86297.23	7.44	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	216.26	64722.92	7.44	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	216.26	86297.23	7.44	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
125	Ft. 16	-78491.36	-858.76	77.18	-241.38
	$\sigma_{s,c}$15	-81318.87	-892.08	72.16	-284.06
	$\sigma_{cls,Max}$15	-81318.87	-892.08	72.16	-19.18
	$\sigma_{cls,Med}$15	-81318.87	-892.08	72.16	-17.81
225	Ft. 16	-75041.36	-1393.32	68.65	-221.58
	$\sigma_{s,c}$15	-77868.87	-1243.33	55.03	-277.93
	$\sigma_{cls,Max}$15	-77868.87	-1243.33	55.03	-18.81
	$\sigma_{cls,Med}$15	-77868.87	-1243.33	55.03	-17.06
Combinazioni Frequenti					
125	Ft. 19	-75574.41	-816.75	77.25	-232.48
	$\sigma_{s,c}$18	-76448.83	-826.79	75.52	-267.10
	$\sigma_{cls,Max}$18	-76448.83	-826.79	75.52	-18.04
	$\sigma_{cls,Med}$20	-76453.77	-827.42	72.27	-16.75
225	Ft. 19	-72124.41	-1319.79	64.11	-213.34
	$\sigma_{s,c}$18	-72998.83	-1265.53	59.25	-262.42
	$\sigma_{cls,Max}$18	-72998.83	-1265.53	59.25	-17.79
	$\sigma_{cls,Med}$20	-73003.77	-1246.42	58.65	-15.99
Combinazioni Quasi Permanenti					
125	Ft. 21	-75165.90	-810.35	76.91	-231.26
	$\sigma_{s,c}$21	-75165.90	-810.35	76.91	-262.66
	$\sigma_{cls,Max}$21	-75165.90	-810.35	76.91	-17.74
	$\sigma_{cls,Med}$22	-75170.09	-810.52	74.27	-16.46
225	Ft. 21	-71715.90	-1294.23	62.23	-212.47
	$\sigma_{s,c}$21	-71715.90	-1294.23	62.23	-258.77
	$\sigma_{cls,Max}$21	-71715.90	-1294.23	62.23	-17.55
	$\sigma_{cls,Med}$22	-71720.09	-1278.16	61.78	-15.71

Pilastro: **225/325** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
225	1	-82521.66	-4246.78	188.37	0.11
325	1	-78036.66	-4734.53	1085.87	0.11

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	242.81	86297.23	271.88	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	242.81	64722.92	271.88	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	242.81	86297.23	271.88	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
225	Ft. 16	-55786.87	-2904.80	134.55	-131.49
	$\sigma_{s,c}$15	-56689.82	-2899.45	127.83	-237.75
	$\sigma_{cls,Max}$15	-56689.82	-2899.45	127.83	-16.51
	$\sigma_{cls,Med}$15	-56689.82	-2899.45	127.83	-12.42
325	Ft. 16	-52336.87	-3438.45	765.88	-91.35
	$\sigma_{s,c}$16	-52336.87	-3438.45	765.88	-252.56
	$\sigma_{cls,Max}$16	-52336.87	-3438.45	765.88	-18.32
	$\sigma_{cls,Med}$15	-53239.82	-3199.81	732.16	-11.66
Combinazioni Frequenti					
225	Ft. 19	-53512.00	-2777.13	127.51	-126.33
	$\sigma_{s,c}$18	-53744.92	-2770.89	124.95	-225.88
	$\sigma_{cls,Max}$18	-53744.92	-2770.89	124.95	-15.69
	$\sigma_{cls,Med}$20	-53748.38	-2754.73	124.15	-11.77
325	Ft. 19	-50062.00	-3229.14	721.21	-88.72
	$\sigma_{s,c}$19	-50062.00	-3229.14	721.21	-240.24
	$\sigma_{cls,Max}$19	-50062.00	-3229.14	721.21	-17.41
	$\sigma_{cls,Med}$20	-50298.38	-3134.09	708.36	-11.02
Combinazioni Quasi Permanenti					
225	Ft. 21	-53103.61	-2750.35	125.59	-125.49
	$\sigma_{s,c}$21	-53103.61	-2750.35	125.59	-223.46
	$\sigma_{cls,Max}$21	-53103.61	-2750.35	125.59	-15.53
	$\sigma_{cls,Med}$22	-53106.54	-2736.77	124.93	-11.63
325	Ft. 21	-49653.61	-3169.37	709.64	-88.72
	$\sigma_{s,c}$21	-49653.61	-3169.37	709.64	-237.55
	$\sigma_{cls,Max}$21	-49653.61	-3169.37	709.64	-17.21
	$\sigma_{cls,Med}$22	-49656.54	-3164.70	709.92	-10.88

Pilastro: **325/11570** / L 4.05[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 205.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
325	2	-47977.82	-7713.91	2204.07	0.10
11570	2	-42387.82	4004.79	-4782.54	0.11

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2725.28	86297.23	1624.79	61956.98	ø 10 2br.x4br./15.0
1.13	3.18	2725.28	64722.92	1624.79	46467.73	ø 10 2br.x4br./20.0
3.18	4.18	2725.28	86297.23	1624.79	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
325	Ft. 16	-32886.73	-5210.92	1486.14	32.97
	$\sigma_{s,c}$16	-32886.73	-5210.92	1486.14	-245.30
	$\sigma_{cls,Max}$16	-32886.73	-5210.92	1486.14	-19.12
	$\sigma_{cls,Med}$16	-32886.73	-5210.92	1486.14	-7.91
11570	Ft. 16	-28586.73	2699.76	-3225.95	115.41
	$\sigma_{s,c}$16	-28586.73	2699.76	-3225.95	-265.27
	$\sigma_{cls,Max}$16	-28586.73	2699.76	-3225.95	-23.01

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$16	-28586.73	2699.76	-3225.95	-9.38
Combinazioni Frequenti					
325	Ft. 19	-31265.85	-4933.22	1400.91	30.30
	$\sigma_{s,c}$19	-31265.85	-4933.22	1400.91	-232.31
	$\sigma_{cls,Max}$19	-31265.85	-4933.22	1400.91	-18.09
	$\sigma_{cls,Med}$19	-31265.85	-4933.22	1400.91	-7.50
11570	Ft. 19	-26965.85	2545.80	-3042.75	108.81
	$\sigma_{s,c}$19	-26965.85	2545.80	-3042.75	-250.20
	$\sigma_{cls,Max}$19	-26965.85	2545.80	-3042.75	-21.71
	$\sigma_{cls,Med}$19	-26965.85	2545.80	-3042.75	-8.84
Combinazioni Quasi Permanenti					
325	Ft. 21	-30860.62	-4868.56	1379.26	29.73
	$\sigma_{s,c}$21	-30860.62	-4868.56	1379.26	-229.15
	$\sigma_{cls,Max}$21	-30860.62	-4868.56	1379.26	-17.84
	$\sigma_{cls,Med}$21	-30860.62	-4868.56	1379.26	-7.40
11570	Ft. 21	-26560.62	2507.45	-2996.65	107.13
	$\sigma_{s,c}$22	-26561.95	2508.99	-2996.15	-246.43
	$\sigma_{cls,Max}$21	-26560.62	2507.45	-2996.65	-21.38
	$\sigma_{cls,Med}$21	-26560.62	2507.45	-2996.65	-8.71

Pilastro: **26/126** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
26	1	-201890.19	-1650.75	2063.27	0.25
126	1	-196235.19	-2447.19	2591.76	0.25

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	342.54	61956.98	1272.49	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	342.54	46467.73	1272.49	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	342.54	61956.98	1272.49	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
26	Ft. 16	-137111.13	-1179.32	1331.89	-391.18
	$\sigma_{s,c}$15	-142282.89	-1227.23	1549.28	-531.86
	$\sigma_{cls,Max}$15	-142282.89	-1227.23	1549.28	-37.13
	$\sigma_{cls,Med}$15	-142282.89	-1227.23	1549.28	-31.16
126	Ft. 17	-133524.56	-1722.39	1669.41	-356.60
	$\sigma_{s,c}$15	-137932.89	-1676.20	1607.88	-532.81
	$\sigma_{cls,Max}$15	-137932.89	-1676.20	1607.88	-37.72
	$\sigma_{cls,Med}$15	-137932.89	-1676.20	1607.88	-30.21
Combinazioni Frequenti					
26	Ft. 19	-135206.67	-1148.02	1245.61	-387.33
	$\sigma_{s,c}$18	-136924.36	-1163.46	1317.60	-508.43
	$\sigma_{cls,Max}$18	-136924.36	-1163.46	1317.60	-35.46
	$\sigma_{cls,Med}$18	-136924.36	-1163.46	1317.60	-29.99
126	Ft. 20	-130475.51	-1683.74	1701.85	-347.28

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-132574.38	-1611.71	1607.19	-513.14
	$\sigma_{cls,Max}$18	-132574.38	-1611.71	1607.19	-36.33
	$\sigma_{cls,Med}$18	-132574.38	-1611.71	1607.19	-29.04
Combinazioni Quasi Permanenti					
26	Ft. 21	-135169.31	-1144.85	1242.75	-387.35
	$\sigma_{s,c}$21	-135169.31	-1144.85	1242.75	-500.85
	$\sigma_{cls,Max}$21	-135169.31	-1144.85	1242.75	-34.92
	$\sigma_{cls,Med}$21	-135169.31	-1144.85	1242.75	-29.61
126	Ft. 22	-129459.15	-1670.86	1712.66	-344.17
	$\sigma_{s,c}$21	-130819.33	-1588.61	1606.54	-506.63
	$\sigma_{cls,Max}$22	-129459.15	-1670.86	1712.66	-35.98
	$\sigma_{cls,Med}$21	-130819.33	-1588.61	1606.54	-28.65

Pilastro: **126/226** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
126	1	-166403.84	5577.38	1801.88	0.24
226	1	-161918.86	-3484.38	-4161.59	0.22

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2626.60	61956.98	1732.23	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	2626.60	46467.73	1732.23	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	2626.60	61956.98	1732.23	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
126	Ft. 17	-111999.02	3905.43	1019.84	-227.05
	$\sigma_{s,c}$15	-116647.26	3929.45	1005.95	-524.71
	$\sigma_{cls,Max}$15	-116647.26	3929.45	1005.95	-39.65
	$\sigma_{cls,Med}$15	-116647.26	3929.45	1005.95	-25.55
226	Ft. 17	-108549.02	-2476.27	-2765.80	-232.62
	$\sigma_{s,c}$15	-113197.26	-2483.56	-2771.22	-496.25
	$\sigma_{cls,Max}$15	-113197.26	-2483.56	-2771.22	-36.41
	$\sigma_{cls,Med}$15	-113197.26	-2483.56	-2771.22	-24.79
Combinazioni Frequenti					
126	Ft. 20	-110254.52	3782.46	977.41	-225.93
	$\sigma_{s,c}$18	-112485.81	3774.25	937.00	-504.97
	$\sigma_{cls,Max}$18	-112485.81	3774.25	937.00	-38.14
	$\sigma_{cls,Med}$18	-112485.81	3774.25	937.00	-24.64
226	Ft. 20	-106804.52	-2403.74	-2633.24	-231.37
	$\sigma_{s,c}$18	-109035.81	-2399.18	-2560.00	-476.44
	$\sigma_{cls,Max}$18	-109035.81	-2399.18	-2560.00	-34.96
	$\sigma_{cls,Med}$18	-109035.81	-2399.18	-2560.00	-23.88
Combinazioni Quasi Permanenti					
126	Ft. 22	-109673.02	3741.47	963.27	-225.55
	$\sigma_{s,c}$21	-111127.86	3721.90	915.02	-498.48
	$\sigma_{cls,Max}$21	-111127.86	3721.90	915.02	-37.64

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-111127.86	3721.90	915.02	-24.34
226	Ft. 22	-106223.02	-2379.56	-2589.05	-230.95
	$\sigma_{s,c}$21	-107677.86	-2370.66	-2489.84	-469.92
	$\sigma_{cls,Max}$21	-107677.86	-2370.66	-2489.84	-34.48
	$\sigma_{cls,Med}$21	-107677.86	-2370.66	-2489.84	-23.59

Pilastro: **226/326** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
226	1	-126246.29	4680.22	4870.72	0.19
326	1	-121761.29	-8336.76	-8273.79	0.23

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3787.02	61956.98	3810.00	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	3787.02	46467.73	3810.00	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	3787.02	61956.98	3810.00	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
226	Ft. 17	-82914.46	3271.30	3219.45	-115.69
	$\sigma_{s,c}$15	-87898.00	3245.11	3361.09	-447.00
	$\sigma_{cls,Max}$15	-87898.00	3245.11	3361.09	-34.10
	$\sigma_{cls,Med}$15	-87898.00	3245.11	3361.09	-19.25
326	Ft. 17	-79464.46	-5728.71	-4763.10	10.30
	$\sigma_{s,c}$15	-84448.00	-5722.75	-5487.67	-554.24
	$\sigma_{cls,Max}$15	-84448.00	-5722.75	-5487.67	-44.62
	$\sigma_{cls,Med}$15	-84448.00	-5722.75	-5487.67	-19.62
Combinazioni Frequenti					
226	Ft. 20	-82798.83	3271.64	2981.97	-119.18
	$\sigma_{s,c}$18	-85240.85	3165.32	3153.80	-432.34
	$\sigma_{cls,Max}$18	-85240.85	3165.32	3153.80	-33.00
	$\sigma_{cls,Med}$18	-85240.85	3165.32	3153.80	-18.67
326	Ft. 20	-79348.83	-5760.53	-4438.82	5.71
	$\sigma_{s,c}$18	-81790.85	-5578.05	-5100.56	-534.23
	$\sigma_{cls,Max}$18	-81790.85	-5578.05	-5100.56	-43.04
	$\sigma_{cls,Med}$18	-81790.85	-5578.05	-5100.56	-18.99
Combinazioni Quasi Permanenti					
226	Ft. 22	-82760.28	3271.75	2902.81	-120.35
	$\sigma_{s,c}$21	-84383.02	3136.37	3086.29	-427.50
	$\sigma_{cls,Max}$21	-84383.02	3136.37	3086.29	-32.63
	$\sigma_{cls,Med}$21	-84383.02	3136.37	3086.29	-18.48
326	Ft. 22	-79310.28	-5771.14	-4330.73	4.19
	$\sigma_{s,c}$21	-80933.02	-5525.29	-4979.85	-527.62
	$\sigma_{cls,Max}$21	-80933.02	-5525.29	-4979.85	-42.51
	$\sigma_{cls,Med}$21	-80933.02	-5525.29	-4979.85	-18.78

Pilastro: **27/127** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
27	1	-367118.34	5043.93	1097.77	0.44
127	1	-361463.34	-2732.52	-5626.94	0.46

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2898.18	86297.23	1581.82	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	2898.18	64722.92	1581.82	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	2898.18	86297.23	1581.82	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
27	Ft. 17	-242719.73	3165.19	810.96	-719.89
	$\sigma_{s,c}$15	-256831.34	3416.33	727.44	-922.85
	$\sigma_{cls,Max}$15	-256831.34	3416.33	727.44	-62.96
	$\sigma_{cls,Med}$15	-256831.34	3416.33	727.44	-56.25
127	Ft. 17	-238369.73	-1703.19	-3952.21	-629.58
	$\sigma_{s,c}$15	-252481.34	-1833.71	-3931.60	-984.60
	$\sigma_{cls,Max}$15	-252481.34	-1833.71	-3931.60	-70.46
	$\sigma_{cls,Med}$15	-252481.34	-1833.71	-3931.60	-55.30
Combinazioni Frequenti					
27	Ft. 20	-238349.55	3211.19	671.22	-709.22
	$\sigma_{s,c}$18	-247533.28	3438.29	599.17	-888.58
	$\sigma_{cls,Max}$18	-247533.28	3438.29	599.17	-60.53
	$\sigma_{cls,Med}$18	-247533.28	3438.29	599.17	-54.22
127	Ft. 20	-233999.55	-1702.31	-3717.35	-622.71
	$\sigma_{s,c}$18	-243183.28	-1810.22	-3681.42	-945.71
	$\sigma_{cls,Max}$18	-243183.28	-1810.22	-3681.42	-67.57
	$\sigma_{cls,Med}$18	-243183.28	-1810.22	-3681.42	-53.27
Combinazioni Quasi Permanenti					
27	Ft. 22	-236892.81	3226.52	624.64	-705.67
	$\sigma_{s,c}$21	-244434.94	3445.08	555.76	-877.13
	$\sigma_{cls,Max}$21	-244434.94	3445.08	555.76	-59.72
	$\sigma_{cls,Med}$21	-244434.94	3445.08	555.76	-53.54
127	Ft. 22	-232542.81	-1702.02	-3639.06	-620.42
	$\sigma_{s,c}$21	-240084.94	-1802.41	-3597.64	-932.73
	$\sigma_{cls,Max}$21	-240084.94	-1802.41	-3597.64	-66.61
	$\sigma_{cls,Med}$21	-240084.94	-1802.41	-3597.64	-52.59

Pilastro: **127/227** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
127	1	-308344.63	-505.67	7487.65	0.42
227	1	-303859.63	1763.43	-2859.40	0.37

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1190.30	86297.23	2999.15	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	1190.30	64722.92	2999.15	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	1190.30	86297.23	2999.15	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
127	Ft. 17	-200360.64	-310.90	5164.98	-488.89
	$\sigma_{s,c}$15	-214863.95	-314.78	5251.47	-878.15
	$\sigma_{cls,Max}$15	-214863.95	-314.78	5251.47	-64.60
	$\sigma_{cls,Med}$15	-214863.95	-314.78	5251.47	-47.06
227	Ft. 17	-196910.64	1030.60	-1846.58	-571.35
	$\sigma_{s,c}$15	-211413.95	1127.39	-1986.44	-776.24
	$\sigma_{cls,Max}$15	-211413.95	1127.39	-1986.44	-54.22
	$\sigma_{cls,Med}$15	-211413.95	1127.39	-1986.44	-46.31
Combinazioni Frequenti					
127	Ft. 20	-197965.83	-296.06	4927.78	-488.81
	$\sigma_{s,c}$18	-207506.84	-286.77	4977.33	-844.80
	$\sigma_{cls,Max}$18	-207506.84	-286.77	4977.33	-62.05
	$\sigma_{cls,Med}$18	-207506.84	-286.77	4977.33	-45.45
227	Ft. 20	-194515.83	957.63	-1776.75	-566.90
	$\sigma_{s,c}$18	-204056.84	1025.23	-1889.30	-747.31
	$\sigma_{cls,Max}$18	-204056.84	1025.23	-1889.30	-52.16
	$\sigma_{cls,Med}$18	-204056.84	1025.23	-1889.30	-44.70
Combinazioni Quasi Permanenti					
127	Ft. 22	-197167.56	-291.11	4848.71	-488.79
	$\sigma_{s,c}$21	-205055.03	-277.68	4885.41	-833.67
	$\sigma_{cls,Max}$21	-205055.03	-277.68	4885.41	-61.21
	$\sigma_{cls,Med}$21	-205055.03	-277.68	4885.41	-44.91
227	Ft. 22	-193717.56	933.30	-1753.47	-565.42
	$\sigma_{s,c}$21	-201605.03	991.46	-1856.43	-737.65
	$\sigma_{cls,Max}$21	-201605.03	991.46	-1856.43	-51.47
	$\sigma_{cls,Med}$21	-201605.03	991.46	-1856.43	-44.16

Pilastro: **227/327** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
227	1	-236265.77	6674.04	-736.95	0.29
327	1	-231780.77	-14520.55	-865.10	0.31

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	6143.36	86297.23	664.82	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	6143.36	64722.92	664.82	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	6143.36	86297.23	664.82	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
227	Ft. 17	-148673.63	4210.36	-417.29	-406.33

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-163610.38	4497.40	-565.32	-629.09
	$\sigma_{cls,Max}$15	-163610.38	4497.40	-565.32	-43.38
	$\sigma_{cls,Med}$15	-163610.38	4497.40	-565.32	-35.84
327	Ft. 17	-145223.63	-8810.47	-1001.75	-301.15
	$\sigma_{s,c}$15	-160160.38	-9846.80	-538.16	-704.39
	$\sigma_{cls,Max}$15	-160160.38	-9846.80	-538.16	-49.32
	$\sigma_{cls,Med}$15	-160160.38	-9846.80	-538.16	-35.08
Combinazioni Frequenti					
227	Ft. 20	-148720.58	4069.91	-426.36	-408.49
	$\sigma_{s,c}$18	-158707.02	4307.70	-582.38	-610.42
	$\sigma_{cls,Max}$18	-158707.02	4307.70	-582.38	-42.12
	$\sigma_{cls,Med}$18	-158707.02	4307.70	-582.38	-34.76
327	Ft. 20	-145270.58	-8689.22	-887.94	-306.91
	$\sigma_{s,c}$18	-155257.02	-9586.14	-415.32	-680.11
	$\sigma_{cls,Max}$18	-155257.02	-9586.14	-415.32	-47.52
	$\sigma_{cls,Med}$18	-155257.02	-9586.14	-415.32	-34.01
Combinazioni Quasi Permanenti					
227	Ft. 22	-148736.22	4023.10	-429.39	-409.21
	$\sigma_{s,c}$21	-157072.80	4244.48	-588.47	-604.21
	$\sigma_{cls,Max}$21	-157072.80	4244.48	-588.47	-41.71
	$\sigma_{cls,Med}$21	-157072.80	4244.48	-588.47	-34.40
327	Ft. 22	-145286.22	-8648.81	-850.00	-308.83
	$\sigma_{s,c}$21	-153622.80	-9498.76	-373.63	-671.99
	$\sigma_{cls,Max}$21	-153622.80	-9498.76	-373.63	-46.91
	$\sigma_{cls,Med}$21	-153622.80	-9498.76	-373.63	-33.65

Pilastro: **28/128** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
28	1	-384865.41	4968.87	924.90	0.46
128	1	-379210.41	-3503.44	48.98	0.45

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3996.68	86297.23	338.33	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	3996.68	64722.92	338.33	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	3996.68	86297.23	338.33	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
28	Ft. 17	-254790.03	3125.79	628.30	-766.00
	$\sigma_{s,c}$15	-269147.66	3318.56	622.48	-958.37
	$\sigma_{cls,Max}$15	-269147.66	3318.56	622.48	-65.19
	$\sigma_{cls,Med}$15	-269147.66	3318.56	622.48	-58.95
128	Ft. 17	-250440.03	-2178.80	51.13	-785.56
	$\sigma_{s,c}$15	-264797.66	-2310.56	57.10	-909.61
	$\sigma_{cls,Max}$15	-264797.66	-2310.56	57.10	-61.12
	$\sigma_{cls,Med}$15	-264797.66	-2310.56	57.10	-58.00

Combinazioni Frequenti					
28	Ft. 20	-249710.78	3174.74	588.25	-749.79
	$\sigma_{s,c}$18	-259041.78	3369.80	577.34	-924.57
	$\sigma_{cls,Max}$18	-259041.78	3369.80	577.34	-62.90
	$\sigma_{cls,Med}$18	-259041.78	3369.80	577.34	-56.74
128	Ft. 20	-245360.78	-2168.96	57.14	-768.84
	$\sigma_{s,c}$18	-254691.78	-2279.73	63.89	-876.12
	$\sigma_{cls,Max}$18	-254691.78	-2279.73	63.89	-58.89
	$\sigma_{cls,Med}$18	-254691.78	-2279.73	63.89	-55.79
Combinazioni Quasi Permanenti					
28	Ft. 22	-248017.69	3191.06	574.90	-744.38
	$\sigma_{s,c}$21	-255671.84	3386.36	562.34	-913.30
	$\sigma_{cls,Max}$21	-255671.84	3386.36	562.34	-62.13
	$\sigma_{cls,Med}$21	-255671.84	3386.36	562.34	-56.00
128	Ft. 22	-243667.69	-2165.69	59.14	-763.27
	$\sigma_{s,c}$21	-251321.84	-2269.64	66.10	-864.95
	$\sigma_{cls,Max}$21	-251321.84	-2269.64	66.10	-58.14
	$\sigma_{cls,Med}$21	-251321.84	-2269.64	66.10	-55.05

Pilastro: **128/228** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
128	1	-311503.41	-2008.62	-1009.11	0.37
228	1	-307018.41	2949.53	33.55	0.36

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	1437.14	86297.23	447.92	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	1437.14	64722.92	447.92	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	1437.14	86297.23	447.92	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
128	Ft. 17	-202217.34	-1260.93	-633.26	-623.62
	$\sigma_{s,c}$15	-216927.66	-1304.36	-710.45	-756.66
	$\sigma_{cls,Max}$15	-216927.66	-1304.36	-710.45	-51.49
	$\sigma_{cls,Med}$15	-216927.66	-1304.36	-710.45	-47.51
228	Ft. 17	-198767.34	1812.85	-117.30	-619.67
	$\sigma_{s,c}$15	-213477.66	1912.88	27.49	-733.55
	$\sigma_{cls,Max}$15	-213477.66	1912.88	27.49	-49.27
	$\sigma_{cls,Med}$15	-213477.66	1912.88	27.49	-46.76
Combinazioni Frequenti					
128	Ft. 20	-199584.36	-1224.55	-609.45	-616.32
	$\sigma_{s,c}$18	-209294.84	-1238.44	-681.80	-729.59
	$\sigma_{cls,Max}$18	-209294.84	-1238.44	-681.80	-49.64
	$\sigma_{cls,Med}$18	-209294.84	-1238.44	-681.80	-45.84
228	Ft. 20	-196134.36	1689.30	-115.89	-613.08
	$\sigma_{s,c}$18	-205844.84	1754.67	29.48	-705.95
	$\sigma_{cls,Max}$18	-205844.84	1754.67	29.48	-47.41
	$\sigma_{cls,Med}$18	-205844.84	1754.67	29.48	-45.09
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
128	Ft. 22	-198706.70	-1212.42	-601.51	-613.89
	$\sigma_{s,c}$21	-206749.36	-1216.95	-672.39	-720.58
	$\sigma_{cls,Max}$21	-206749.36	-1216.95	-672.39	-49.02
	$\sigma_{cls,Med}$21	-206749.36	-1216.95	-672.39	-45.29
228	Ft. 22	-195256.70	1648.11	-115.42	-610.89
	$\sigma_{s,c}$21	-203299.36	1702.36	30.25	-696.75
	$\sigma_{cls,Max}$21	-203299.36	1702.36	30.25	-46.79
	$\sigma_{cls,Med}$21	-203299.36	1702.36	30.25	-44.53

Pilastro: **228/328** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
228	1	-239258.11	4992.11	129.06	0.29
328	1	-234773.11	-7863.61	56.25	0.29

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3726.30	86297.23	386.77	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	3726.30	64722.92	386.77	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	3726.30	86297.23	386.77	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
228	Ft. 17	-150403.48	3043.69	16.01	-443.86
	$\sigma_{s,c}$15	-165597.03	3273.24	81.42	-600.20
	$\sigma_{cls,Max}$15	-165597.03	3273.24	81.42	-40.69
	$\sigma_{cls,Med}$15	-165597.03	3273.24	81.42	-36.27
328	Ft. 17	-146953.48	-4579.51	441.70	-393.86
	$\sigma_{s,c}$15	-162147.03	-5208.12	54.24	-619.65
	$\sigma_{cls,Max}$15	-162147.03	-5208.12	54.24	-42.30
	$\sigma_{cls,Med}$15	-162147.03	-5208.12	54.24	-35.52
Combinazioni Frequenti					
228	Ft. 20	-150165.28	2924.73	-16.35	-445.01
	$\sigma_{s,c}$18	-160405.98	3126.95	54.12	-579.89
	$\sigma_{cls,Max}$18	-160405.98	3126.95	54.12	-39.28
	$\sigma_{cls,Med}$18	-160405.98	3126.95	54.12	-35.13
328	Ft. 20	-146715.28	-4491.04	486.59	-393.10
	$\sigma_{s,c}$18	-156955.98	-5120.59	86.64	-602.20
	$\sigma_{cls,Max}$18	-156955.98	-5120.59	86.64	-41.15
	$\sigma_{cls,Med}$18	-156955.98	-5120.59	86.64	-34.38
Combinazioni Quasi Permanenti					
228	Ft. 22	-150085.88	2885.08	-27.14	-445.06
	$\sigma_{s,c}$21	-158674.50	3078.29	44.98	-573.11
	$\sigma_{cls,Max}$21	-158674.50	3078.29	44.98	-38.81
	$\sigma_{cls,Med}$21	-158674.50	3078.29	44.98	-34.76
328	Ft. 22	-146635.88	-4461.55	501.55	-392.84
	$\sigma_{s,c}$21	-155224.50	-5090.71	97.61	-596.37
	$\sigma_{cls,Max}$21	-155224.50	-5090.71	97.61	-40.77

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-155224.50	-5090.71	97.61	-34.00

Pilastro: **29/129** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
29	1	-393946.25	6697.88	674.20	0.47
129	1	-388291.25	-4800.67	-1171.42	0.46

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4883.23	86297.23	487.91	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	4883.23	64722.92	487.91	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	4883.23	86297.23	487.91	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
29	Ft. 16	-265366.34	4463.25	406.13	-785.94
	$\sigma_{s,c}$15	-275679.84	4477.24	454.30	-993.44
	$\sigma_{cls,Max}$15	-275679.84	4477.24	454.30	-67.54
	$\sigma_{cls,Med}$15	-275679.84	4477.24	454.30	-60.38
129	Ft. 16	-261016.31	-3089.28	-768.02	-782.61
	$\sigma_{s,c}$15	-271329.84	-3162.93	-821.71	-969.34
	$\sigma_{cls,Max}$15	-271329.84	-3162.93	-821.71	-66.12
	$\sigma_{cls,Med}$15	-271329.84	-3162.93	-821.71	-59.43
Combinazioni Frequenti					
29	Ft. 19	-261910.31	4461.03	389.33	-775.16
	$\sigma_{s,c}$18	-265347.53	4465.77	405.36	-957.75
	$\sigma_{cls,Max}$18	-265347.53	4465.77	405.36	-65.11
	$\sigma_{cls,Med}$20	-265644.72	4265.56	453.19	-58.19
129	Ft. 19	-257560.31	-3063.16	-748.29	-772.31
	$\sigma_{s,c}$20	-261294.70	-2965.41	-832.45	-933.48
	$\sigma_{cls,Max}$20	-261294.70	-2965.41	-832.45	-63.71
	$\sigma_{cls,Med}$20	-261294.70	-2965.41	-832.45	-57.23
Combinazioni Quasi Permanenti					
29	Ft. 21	-261906.55	4461.53	389.17	-775.14
	$\sigma_{s,c}$22	-263941.31	4262.98	434.99	-950.75
	$\sigma_{cls,Max}$22	-263941.31	4262.98	434.99	-64.64
	$\sigma_{cls,Med}$22	-263941.31	4262.98	434.99	-57.81
129	Ft. 21	-257556.55	-3062.83	-747.91	-772.32
	$\sigma_{s,c}$22	-259591.31	-2950.26	-814.35	-927.06
	$\sigma_{cls,Max}$22	-259591.31	-2950.26	-814.35	-63.26
	$\sigma_{cls,Med}$22	-259591.31	-2950.26	-814.35	-56.86

Pilastro: **129/229** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
129	1	-320954.22	-3076.38	1167.39	0.38

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
229	1	-316469.22	3150.27	-906.41	0.37

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1804.83	86297.23	601.10	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	1804.83	64722.92	601.10	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	1804.83	86297.23	601.10	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
129	Ft. 16	-215838.58	-1902.14	806.33	-652.38
	$\sigma_{s,c}$15	-223685.80	-1998.32	854.42	-794.79
	$\sigma_{cls,Max}$15	-223685.80	-1998.32	854.42	-54.32
	$\sigma_{cls,Med}$15	-223685.80	-1998.32	854.42	-48.99
229	Ft. 16	-212388.58	1862.38	-621.15	-647.58
	$\sigma_{s,c}$15	-220235.80	2032.54	-660.80	-777.86
	$\sigma_{cls,Max}$15	-220235.80	2032.54	-660.80	-52.97
	$\sigma_{cls,Med}$15	-220235.80	2032.54	-660.80	-48.24
Combinazioni Frequenti					
129	Ft. 19	-213206.94	-1866.79	787.80	-644.90
	$\sigma_{s,c}$18	-215822.13	-1898.73	803.75	-765.71
	$\sigma_{cls,Max}$18	-215822.13	-1898.73	803.75	-52.30
	$\sigma_{cls,Med}$20	-216423.38	-1867.05	708.81	-47.40
229	Ft. 19	-209756.94	1803.04	-606.08	-640.39
	$\sigma_{s,c}$18	-212372.13	1859.67	-619.23	-747.87
	$\sigma_{cls,Max}$18	-212372.13	1859.67	-619.23	-50.90
	$\sigma_{cls,Med}$20	-212973.38	1786.19	-312.13	-46.65
Combinazioni Quasi Permanenti					
129	Ft. 21	-213203.64	-1866.10	787.29	-644.92
	$\sigma_{s,c}$22	-215537.69	-1846.68	691.19	-760.35
	$\sigma_{cls,Max}$22	-215537.69	-1846.68	691.19	-51.81
	$\sigma_{cls,Med}$22	-215537.69	-1846.68	691.19	-47.21
229	Ft. 21	-209753.64	1802.50	-605.70	-640.40
	$\sigma_{s,c}$21	-209753.64	1802.50	-605.70	-737.90
	$\sigma_{cls,Max}$21	-209753.64	1802.50	-605.70	-50.21
	$\sigma_{cls,Med}$22	-212087.69	1744.48	-295.16	-46.45

Pilastro: **229/329** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
229	1	-247396.88	5254.18	1107.75	0.30
329	3	-236677.88	-7397.16	-4627.60	0.31

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3909.62	86297.23	1891.87	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	3909.62	64722.92	1891.87	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	3909.62	86297.23	1891.87	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
229	Ft. 17	-167237.09	3201.66	1334.28	-454.64
	$\sigma_{s,c}$15	-171393.11	3444.53	806.54	-645.12
	$\sigma_{cls,Max}$17	-167237.09	3201.66	1334.28	-45.04
	$\sigma_{cls,Med}$15	-171393.11	3444.53	806.54	-37.54
329	Ft. 17	-163787.09	-4915.14	-3199.38	-355.95
	$\sigma_{s,c}$17	-163787.09	-4915.14	-3199.38	-720.30
	$\sigma_{cls,Max}$17	-163787.09	-4915.14	-3199.38	-52.55
	$\sigma_{cls,Med}$15	-167943.11	-5473.05	-1610.21	-36.79
Combinazioni Frequenti					
229	Ft. 20	-167044.73	3073.45	1291.13	-457.48
	$\sigma_{s,c}$20	-167044.73	3073.45	1291.13	-640.18
	$\sigma_{cls,Max}$20	-167044.73	3073.45	1291.13	-44.70
	$\sigma_{cls,Med}$20	-167044.73	3073.45	1291.13	-36.59
329	Ft. 20	-163594.73	-4809.87	-3154.13	-358.48
	$\sigma_{s,c}$20	-163594.73	-4809.87	-3154.13	-716.51
	$\sigma_{cls,Max}$20	-163594.73	-4809.87	-3154.13	-52.22
	$\sigma_{cls,Med}$20	-163594.73	-4809.87	-3154.13	-35.83
Combinazioni Quasi Permanenti					
229	Ft. 22	-166980.61	3030.72	1276.75	-458.43
	$\sigma_{s,c}$22	-166980.61	3030.72	1276.75	-638.81
	$\sigma_{cls,Max}$22	-166980.61	3030.72	1276.75	-44.58
	$\sigma_{cls,Med}$22	-166980.61	3030.72	1276.75	-36.57
329	Ft. 22	-163530.61	-4774.77	-3139.04	-359.32
	$\sigma_{s,c}$22	-163530.61	-4774.77	-3139.04	-715.24
	$\sigma_{cls,Max}$22	-163530.61	-4774.77	-3139.04	-52.12
	$\sigma_{cls,Med}$22	-163530.61	-4774.77	-3139.04	-35.82

Pilastro: **30/130** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
30	1	-235003.66	1630.77	7907.22	0.34
130	1	-229348.66	-2208.10	1010.17	0.27

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1671.74	86297.23	1585.53	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	1671.74	64722.92	1585.53	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	1671.74	86297.23	1585.53	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
30	Ft. 16	-159783.95	1038.87	5494.69	-333.18
	$\sigma_{s,c}$15	-165905.20	1031.79	5656.30	-741.90
	$\sigma_{cls,Max}$15	-165905.20	1031.79	5656.30	-56.10
	$\sigma_{cls,Med}$15	-165905.20	1031.79	5656.30	-36.34
130	Ft. 17	-156911.45	-1391.27	984.27	-461.47
	$\sigma_{s,c}$15	-161555.20	-1440.14	668.69	-575.62
	$\sigma_{cls,Max}$15	-161555.20	-1440.14	668.69	-39.39

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-161555.20	-1440.14	668.69	-35.39
Combinazioni Frequenti					
30	Ft. 19	-157596.50	1043.21	5417.17	-328.39
	$\sigma_{s,c}$18	-159631.84	1040.92	5470.23	-715.52
	$\sigma_{cls,Max}$18	-159631.84	1040.92	5470.23	-54.13
	$\sigma_{cls,Med}$18	-159631.84	1040.92	5470.23	-34.96
130	Ft. 20	-153796.33	-1362.48	851.85	-455.92
	$\sigma_{s,c}$20	-153796.33	-1362.48	851.85	-554.69
	$\sigma_{cls,Max}$20	-153796.33	-1362.48	851.85	-38.19
	$\sigma_{cls,Med}$18	-155281.84	-1393.64	592.07	-34.01
Combinazioni Quasi Permanenti					
30	Ft. 21	-157566.08	1043.62	5412.28	-328.44
	$\sigma_{s,c}$21	-157566.08	1043.62	5412.28	-706.93
	$\sigma_{cls,Max}$21	-157566.08	1043.62	5412.28	-53.49
	$\sigma_{cls,Med}$21	-157566.08	1043.62	5412.28	-34.51
130	Ft. 22	-152757.95	-1352.88	807.71	-454.07
	$\sigma_{s,c}$22	-152757.95	-1352.88	807.71	-549.71
	$\sigma_{cls,Max}$22	-152757.95	-1352.88	807.71	-37.81
	$\sigma_{cls,Med}$21	-153216.08	-1378.36	564.16	-33.56

Pilastro: **130/230** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
130	1	-175839.23	-1300.47	-10723.71	0.30
230	1	-171354.23	1103.46	8867.87	0.27

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	696.79	86297.23	5767.40	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	696.79	64722.92	5767.40	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	696.79	86297.23	5767.40	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
130	Ft. 17	-119693.85	-796.07	-7656.51	-136.67
	$\sigma_{s,c}$15	-123611.20	-819.44	-7548.91	-659.68
	$\sigma_{cls,Max}$15	-123611.20	-819.44	-7548.91	-52.74
	$\sigma_{cls,Med}$15	-123611.20	-819.44	-7548.91	-27.08
230	Ft. 17	-116243.85	619.16	6354.24	-169.65
	$\sigma_{s,c}$15	-120161.20	702.91	6257.85	-605.37
	$\sigma_{cls,Max}$15	-120161.20	702.91	6257.85	-47.63
	$\sigma_{cls,Med}$15	-120161.20	702.91	6257.85	-26.32
Combinazioni Frequenti					
130	Ft. 20	-118450.63	-770.49	-7296.14	-144.46
	$\sigma_{s,c}$20	-118450.63	-770.49	-7296.14	-633.88
	$\sigma_{cls,Max}$20	-118450.63	-770.49	-7296.14	-50.73
	$\sigma_{cls,Med}$18	-119270.88	-778.93	-7169.70	-26.12
230	Ft. 20	-115000.63	567.34	6013.92	-177.24

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-115820.88	619.46	5925.40	-579.16
	$\sigma_{cls,Max}$20	-115000.63	567.34	6013.92	-45.53
	$\sigma_{cls,Med}$18	-115820.88	619.46	5925.40	-25.37
Combinazioni Quasi Permanenti					
130	Ft. 22	-118036.23	-761.96	-7176.02	-147.06
	$\sigma_{s,c}$22	-118036.23	-761.96	-7176.02	-628.56
	$\sigma_{cls,Max}$22	-118036.23	-761.96	-7176.02	-50.23
	$\sigma_{cls,Med}$22	-118036.23	-761.96	-7176.02	-25.85
230	Ft. 22	-114586.23	550.06	5900.48	-179.77
	$\sigma_{s,c}$22	-114586.23	550.06	5900.48	-573.18
	$\sigma_{cls,Max}$22	-114586.23	550.06	5900.48	-45.05
	$\sigma_{cls,Med}$22	-114586.23	550.06	5900.48	-25.10

Pilastro: **230/330** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
230	1	-133134.95	1188.22	-13246.30	0.29
330	3	-123495.54	-2500.59	19357.26	0.39

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1593.88	86297.23	9526.01	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	1593.88	64722.92	9526.01	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	1593.88	86297.23	9526.01	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
230	Ft. 17	-89411.80	648.62	-9350.76	93.21
	$\sigma_{s,c}$15	-92848.08	756.90	-9176.65	-625.70
	$\sigma_{cls,Max}$17	-89411.80	648.62	-9350.76	-54.01
	$\sigma_{cls,Med}$17	-89411.80	648.62	-9350.76	-26.49
330	Ft. 17	-85961.80	-1666.10	13297.67	634.04
	$\sigma_{s,c}$17	-85961.80	-1666.10	13297.67	-816.06
	$\sigma_{cls,Max}$17	-85961.80	-1666.10	13297.67	-79.32
	$\sigma_{cls,Med}$17	-85961.80	-1666.10	13297.67	-37.97
Combinazioni Frequenti					
230	Ft. 20	-89872.20	596.56	-9095.33	68.32
	$\sigma_{s,c}$20	-89872.20	596.56	-9095.33	-611.77
	$\sigma_{cls,Max}$20	-89872.20	596.56	-9095.33	-52.69
	$\sigma_{cls,Med}$20	-89872.20	596.56	-9095.33	-25.88
330	Ft. 20	-86422.20	-1631.39	13131.78	600.58
	$\sigma_{s,c}$20	-86422.20	-1631.39	13131.78	-808.70
	$\sigma_{cls,Max}$20	-86422.20	-1631.39	13131.78	-78.13
	$\sigma_{cls,Med}$20	-86422.20	-1631.39	13131.78	-37.42
Combinazioni Quasi Permanenti					
230	Ft. 22	-90025.65	579.21	-9010.19	60.39
	$\sigma_{s,c}$22	-90025.65	579.21	-9010.19	-608.24
	$\sigma_{cls,Max}$22	-90025.65	579.21	-9010.19	-52.26

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$22	-90025.65	579.21	-9010.19	-25.68
330	Ft. 22	-86575.65	-1619.82	13076.48	589.56
	$\sigma_{s,c}$22	-86575.65	-1619.82	13076.48	-806.24
	$\sigma_{cls,Max}$22	-86575.65	-1619.82	13076.48	-77.74
	$\sigma_{cls,Med}$22	-86575.65	-1619.82	13076.48	-37.24

Pilastro: **31/2571** / L 0.85[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 85.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
31	1	-105597.20	1870.69	6106.70	0.18
2571	1	-104167.20	4784.48	2246.73	0.14

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	0.98	4893.04	86297.23	3509.06	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
31	Ft. 17	-69732.68	1253.98	4089.78	-78.49
	$\sigma_{s,c}$15	-73685.58	1222.13	4219.97	-396.33
	$\sigma_{cls,Max}$15	-73685.58	1222.13	4219.97	-31.46
	$\sigma_{cls,Med}$15	-73685.58	1222.13	4219.97	-16.14
2571	Ft. 17	-68632.68	3260.07	1479.07	-125.12
	$\sigma_{s,c}$15	-72585.58	3193.84	1552.33	-340.11
	$\sigma_{cls,Max}$15	-72585.58	3193.84	1552.33	-25.01
	$\sigma_{cls,Med}$15	-72585.58	3193.84	1552.33	-15.90
Combinazioni Frequenti					
31	Ft. 20	-68502.51	1210.15	3970.90	-78.95
	$\sigma_{s,c}$18	-71315.76	1187.73	4059.12	-382.87
	$\sigma_{cls,Max}$18	-71315.76	1187.73	4059.12	-30.37
	$\sigma_{cls,Med}$18	-71315.76	1187.73	4059.12	-15.62
2571	Ft. 20	-67402.51	3187.25	1445.12	-123.35
	$\sigma_{s,c}$18	-70215.76	3129.70	1496.89	-329.51
	$\sigma_{cls,Max}$18	-70215.76	3129.70	1496.89	-24.23
	$\sigma_{cls,Med}$18	-70215.76	3129.70	1496.89	-15.38
Combinazioni Quasi Permanenti					
31	Ft. 22	-68092.45	1195.54	3931.28	-79.10
	$\sigma_{s,c}$21	-70536.16	1175.89	4005.90	-378.42
	$\sigma_{cls,Max}$21	-70536.16	1175.89	4005.90	-30.01
	$\sigma_{cls,Med}$21	-70536.16	1175.89	4005.90	-15.45
2571	Ft. 22	-66992.45	3162.98	1433.80	-122.76
	$\sigma_{s,c}$21	-69436.16	3106.39	1478.72	-325.99
	$\sigma_{cls,Max}$21	-69436.16	3106.39	1478.72	-23.97
	$\sigma_{cls,Med}$21	-69436.16	3106.39	1478.72	-15.21

Pilastro: **2571/131** / L 3.00[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 100.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
2571	1	-267084.78	13947.17	-1655.48	0.35
131	1	-262859.78	-8507.06	2965.05	0.34

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	10261.53	86297.23	1756.03	61956.98	ø 10 2br.x4br./15.0
1.13	2.13	10261.53	64722.92	1756.03	46467.73	ø 10 2br.x4br./20.0
2.13	3.13	10261.53	86297.23	1756.03	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
2571	Ft. 17	-175638.88	9391.30	-1089.33	-388.80
	$\sigma_{s,c}$15	-186317.06	9454.14	-1229.79	-805.91
	$\sigma_{cls,Max}$15	-186317.06	9454.14	-1229.79	-56.81
	$\sigma_{cls,Med}$15	-186317.06	9454.14	-1229.79	-40.81
131	Ft. 17	-172388.88	-5646.15	2031.19	-409.42
	$\sigma_{s,c}$15	-183067.06	-5651.72	2170.93	-762.98
	$\sigma_{cls,Max}$15	-183067.06	-5651.72	2170.93	-54.35
	$\sigma_{cls,Med}$15	-183067.06	-5651.72	2170.93	-40.10
Combinazioni Frequenti					
2571	Ft. 20	-172878.25	9231.10	-1109.07	-381.72
	$\sigma_{s,c}$18	-180515.41	9245.71	-1217.37	-783.05
	$\sigma_{cls,Max}$18	-180515.41	9245.71	-1217.37	-55.23
	$\sigma_{cls,Med}$18	-180515.41	9245.71	-1217.37	-39.54
131	Ft. 20	-169628.25	-5514.27	1993.68	-403.70
	$\sigma_{s,c}$18	-177265.41	-5488.21	2097.92	-738.92
	$\sigma_{cls,Max}$18	-177265.41	-5488.21	2097.92	-52.63
	$\sigma_{cls,Med}$18	-177265.41	-5488.21	2097.92	-38.83
Combinazioni Quasi Permanenti					
2571	Ft. 22	-171958.00	9177.70	-1115.65	-379.36
	$\sigma_{s,c}$21	-178606.50	9171.65	-1213.19	-775.43
	$\sigma_{cls,Max}$21	-178606.50	9171.65	-1213.19	-54.71
	$\sigma_{cls,Med}$21	-178606.50	9171.65	-1213.19	-39.12
131	Ft. 22	-168708.00	-5470.31	1981.18	-401.79
	$\sigma_{s,c}$21	-175356.50	-5432.16	2073.75	-730.96
	$\sigma_{cls,Max}$21	-175356.50	-5432.16	2073.75	-52.06
	$\sigma_{cls,Med}$21	-175356.50	-5432.16	2073.75	-38.41

Pilastro: **131/231** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
131	1	-222233.89	-5268.08	-3478.79	0.29
231	1	-217748.89	-1527.80	2115.57	0.27

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1140.63	86297.23	1621.55	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	1140.63	64722.92	1621.55	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	1140.63	86297.23	1621.55	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
131	Ft. 17	-143705.81	-3506.83	-2482.99	-335.80
	$\sigma_{s,c}$15	-154230.30	-3452.88	-2529.24	-643.67
	$\sigma_{cls,Max}$15	-154230.30	-3452.88	-2529.24	-46.41
	$\sigma_{cls,Med}$15	-154230.30	-3452.88	-2529.24	-33.78
231	Ft. 17	-140255.81	-1040.05	1623.57	-392.15
	$\sigma_{s,c}$15	-150780.30	-1116.02	1589.65	-564.22
	$\sigma_{cls,Max}$15	-150780.30	-1116.02	1589.65	-39.63
	$\sigma_{cls,Med}$15	-150780.30	-1116.02	1589.65	-33.03
Combinazioni Frequenti					
131	Ft. 20	-142394.59	-3365.01	-2377.40	-337.17
	$\sigma_{s,c}$18	-149935.84	-3295.25	-2411.40	-623.23
	$\sigma_{cls,Max}$18	-149935.84	-3295.25	-2411.40	-44.89
	$\sigma_{cls,Med}$18	-149935.84	-3295.25	-2411.40	-32.84
231	Ft. 20	-138944.59	-1072.00	1504.49	-391.11
	$\sigma_{s,c}$18	-146485.84	-1148.81	1486.36	-547.36
	$\sigma_{cls,Max}$18	-146485.84	-1148.81	1486.36	-38.39
	$\sigma_{cls,Med}$18	-146485.84	-1148.81	1486.36	-32.09
Combinazioni Quasi Permanenti					
131	Ft. 22	-141957.56	-3317.74	-2342.20	-337.63
	$\sigma_{s,c}$21	-148526.98	-3243.60	-2372.13	-616.51
	$\sigma_{cls,Max}$21	-148526.98	-3243.60	-2372.13	-44.39
	$\sigma_{cls,Med}$21	-148526.98	-3243.60	-2372.13	-32.53
231	Ft. 22	-138507.56	-1082.64	1464.79	-390.76
	$\sigma_{s,c}$21	-145076.98	-1158.90	1451.65	-541.79
	$\sigma_{cls,Max}$21	-145076.98	-1158.90	1451.65	-37.98
	$\sigma_{cls,Med}$21	-145076.98	-1158.90	1451.65	-31.78

Pilastro: **231/331** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
231	1	-185373.52	2608.59	-4698.03	0.25
331	1	-180888.52	-8257.31	7827.03	0.28

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4157.32	86297.23	3630.45	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	4157.32	64722.92	3630.45	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	4157.32	86297.23	3630.45	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
231	Ft. 17	-116865.87	1592.68	-3099.62	-259.31

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-127669.81	1733.76	-3354.53	-554.54
	$\sigma_{cls,Max}$15	-127669.81	1733.76	-3354.53	-41.11
	$\sigma_{cls,Med}$15	-127669.81	1733.76	-3354.53	-27.96
331	Ft. 17	-113415.87	-5200.07	4882.73	-132.24
	$\sigma_{s,c}$15	-124219.81	-5605.90	5525.82	-675.61
	$\sigma_{cls,Max}$15	-124219.81	-5605.90	5525.82	-52.35
	$\sigma_{cls,Med}$15	-124219.81	-5605.90	5525.82	-27.21
Combinazioni Frequenti					
231	Ft. 20	-116933.38	1614.88	-3078.98	-259.82
	$\sigma_{s,c}$18	-124695.10	1692.36	-3265.73	-541.26
	$\sigma_{cls,Max}$18	-124695.10	1692.36	-3265.73	-40.11
	$\sigma_{cls,Med}$18	-124695.10	1692.36	-3265.73	-27.31
331	Ft. 20	-113483.38	-5348.68	5002.81	-126.21
	$\sigma_{s,c}$18	-121245.10	-5670.17	5457.38	-664.71
	$\sigma_{cls,Max}$18	-121245.10	-5670.17	5457.38	-51.55
	$\sigma_{cls,Med}$18	-121245.10	-5670.17	5457.38	-26.56
Combinazioni Quasi Permanenti					
231	Ft. 22	-116955.89	1622.28	-3072.10	-259.99
	$\sigma_{s,c}$21	-123723.23	1676.27	-3236.19	-536.86
	$\sigma_{cls,Max}$21	-123723.23	1676.27	-3236.19	-39.78
	$\sigma_{cls,Med}$21	-123723.23	1676.27	-3236.19	-27.10
331	Ft. 22	-113505.89	-5398.22	5042.84	-124.20
	$\sigma_{s,c}$21	-120273.23	-5681.59	5435.15	-661.00
	$\sigma_{cls,Max}$21	-120273.23	-5681.59	5435.15	-51.28
	$\sigma_{cls,Med}$21	-120273.23	-5681.59	5435.15	-26.34

Pilastro: **32/2574** / L 0.85[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 85.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
32	1	-83835.78	3743.73	-349.27	0.11
2574	1	-82405.78	6070.94	1940.32	0.12

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	0.98	5219.04	86297.23	2081.45	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
32	Ft. 17	-56473.57	2582.15	-204.09	-136.82
	$\sigma_{s,c}$15	-58320.71	2552.19	-238.64	-240.95
	$\sigma_{cls,Max}$15	-58320.71	2552.19	-238.64	-16.79
	$\sigma_{cls,Med}$15	-58320.71	2552.19	-238.64	-12.77
2574	Ft. 17	-55373.57	4174.30	1266.81	-73.35
	$\sigma_{s,c}$15	-57220.71	4084.59	1331.36	-297.17
	$\sigma_{cls,Max}$15	-57220.71	4084.59	1331.36	-22.06
	$\sigma_{cls,Med}$15	-57220.71	4084.59	1331.36	-12.53
Combinazioni Frequenti					
32	Ft. 20	-55282.90	2434.68	-224.92	-134.65

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-56400.02	2413.00	-248.96	-232.69
	$\sigma_{cls,Max}$18	-56400.02	2413.00	-248.96	-16.23
	$\sigma_{cls,Med}$18	-56400.02	2413.00	-248.96	-12.35
2574	Ft. 20	-54182.90	3980.98	1262.93	-72.73
	$\sigma_{s,c}$18	-55300.02	3908.00	1304.15	-287.10
	$\sigma_{cls,Max}$18	-55300.02	3908.00	1304.15	-21.32
	$\sigma_{cls,Med}$18	-55300.02	3908.00	1304.15	-12.11
Combinazioni Quasi Permanenti					
32	Ft. 22	-54886.01	2385.52	-231.87	-133.93
	$\sigma_{s,c}$21	-55776.10	2368.58	-251.83	-230.01
	$\sigma_{cls,Max}$21	-55776.10	2368.58	-251.83	-16.04
	$\sigma_{cls,Med}$21	-55776.10	2368.58	-251.83	-12.22
2574	Ft. 22	-53786.01	3916.54	1261.64	-72.52
	$\sigma_{s,c}$21	-54676.10	3849.49	1294.53	-283.79
	$\sigma_{cls,Max}$21	-54676.10	3849.49	1294.53	-21.08
	$\sigma_{cls,Med}$21	-54676.10	3849.49	1294.53	-11.98

Pilastro: **2574/132** / L 3.00[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 100.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
2574	1	-197120.36	11546.59	-430.68	0.26
132	1	-192895.36	-14835.44	397.82	0.27

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	10719.32	86297.23	1175.66	61956.98	ø 10 2br.x4br./15.0
1.13	2.13	10719.32	64722.92	1175.66	46467.73	ø 10 2br.x4br./20.0
2.13	3.13	10719.32	86297.23	1175.66	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
2574	Ft. 17	-132358.28	7862.39	-248.16	-298.37
	$\sigma_{s,c}$15	-136949.45	7777.80	-316.31	-587.23
	$\sigma_{cls,Max}$15	-136949.45	7777.80	-316.31	-40.89
	$\sigma_{cls,Med}$15	-136949.45	7777.80	-316.31	-30.00
132	Ft. 17	-129108.29	-10040.56	206.90	-253.37
	$\sigma_{s,c}$15	-133699.45	-10012.41	263.13	-611.42
	$\sigma_{cls,Max}$15	-133699.45	-10012.41	263.13	-42.84
	$\sigma_{cls,Med}$15	-133699.45	-10012.41	263.13	-29.28
Combinazioni Frequenti					
2574	Ft. 20	-129775.25	7619.26	-325.50	-291.40
	$\sigma_{s,c}$18	-132549.47	7531.26	-371.80	-570.51
	$\sigma_{cls,Max}$18	-132549.47	7531.26	-371.80	-39.80
	$\sigma_{cls,Med}$18	-132549.47	7531.26	-371.80	-29.03
132	Ft. 20	-126525.25	-9731.63	257.12	-248.34
	$\sigma_{s,c}$18	-129299.48	-9651.80	297.95	-592.17
	$\sigma_{cls,Max}$18	-129299.48	-9651.80	297.95	-41.53
	$\sigma_{cls,Med}$18	-129299.48	-9651.80	297.95	-28.32

Combinazioni Quasi Permanenti					
2574	Ft. 22	-128914.22	7538.21	-351.28	-289.07
	$\sigma_{s,c}$21	-131119.98	7446.16	-389.45	-564.98
	$\sigma_{cls,Max}$21	-131119.98	7446.16	-389.45	-39.43
	$\sigma_{cls,Med}$21	-131119.98	7446.16	-389.45	-28.72
132	Ft. 22	-125664.22	-9628.66	273.85	-246.66
	$\sigma_{s,c}$21	-127869.98	-9529.95	308.80	-585.82
	$\sigma_{cls,Max}$21	-127869.98	-9529.95	308.80	-41.10
	$\sigma_{cls,Med}$21	-127869.98	-9529.95	308.80	-28.01

Pilastro: **132/232** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
132	1	-183501.81	2522.91	1394.53	0.22
232	1	-179016.81	-3781.11	-3320.59	0.23

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	3018.37	86297.23	1412.79	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	3018.37	64722.92	1412.79	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	3018.37	86297.23	1412.79	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
132	Ft. 17	-121996.45	1994.86	1077.04	-333.93
	$\sigma_{s,c}$15	-126742.18	2067.48	1029.10	-482.97
	$\sigma_{cls,Max}$15	-126742.18	2067.48	1029.10	-33.74
	$\sigma_{cls,Med}$15	-126742.18	2067.48	1029.10	-27.76
232	Ft. 17	-118546.45	-2887.06	-2412.01	-265.53
	$\sigma_{s,c}$15	-123292.18	-2820.07	-2353.94	-526.09
	$\sigma_{cls,Max}$15	-123292.18	-2820.07	-2353.94	-38.26
	$\sigma_{cls,Med}$15	-123292.18	-2820.07	-2353.94	-27.01
Combinazioni Frequenti					
132	Ft. 20	-120165.98	1944.31	954.75	-332.63
	$\sigma_{s,c}$18	-123009.35	2015.78	923.47	-466.50
	$\sigma_{cls,Max}$18	-123009.35	2015.78	923.47	-32.51
	$\sigma_{cls,Med}$18	-123009.35	2015.78	923.47	-26.94
232	Ft. 20	-116715.98	-2729.98	-2195.61	-268.97
	$\sigma_{s,c}$18	-119559.35	-2740.05	-2164.25	-506.48
	$\sigma_{cls,Max}$18	-119559.35	-2740.05	-2164.25	-36.72
	$\sigma_{cls,Med}$18	-119559.35	-2740.05	-2164.25	-26.19
Combinazioni Quasi Permanenti					
132	Ft. 22	-119555.83	1927.46	913.99	-332.20
	$\sigma_{s,c}$21	-121798.78	1996.41	888.46	-461.09
	$\sigma_{cls,Max}$21	-121798.78	1996.41	888.46	-32.11
	$\sigma_{cls,Med}$21	-121798.78	1996.41	888.46	-26.68
232	Ft. 22	-116105.83	-2677.62	-2123.48	-270.12
	$\sigma_{s,c}$21	-118348.78	-2711.40	-2100.87	-500.02
	$\sigma_{cls,Max}$21	-118348.78	-2711.40	-2100.87	-36.22
	$\sigma_{cls,Med}$21	-118348.78	-2711.40	-2100.87	-25.92

Pilastro: **232/332** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
232	1	-151332.33	14276.05	5285.08	0.24
332	1	-146847.33	-41081.24	-6266.63	0.38

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	16045.59	86297.23	3407.60	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	16045.59	64722.92	3407.60	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	16045.59	86297.23	3407.60	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
232	Ft. 17	-98819.20	9594.57	3756.76	-47.80
	$\sigma_{s,c}$15	-103676.54	9797.44	3696.90	-618.56
	$\sigma_{cls,Max}$15	-103676.54	9797.44	3696.90	-47.20
	$\sigma_{cls,Med}$15	-103676.54	9797.44	3696.90	-22.77
332	Ft. 17	-95369.20	-27227.31	-4413.17	508.79
	$\sigma_{s,c}$15	-100226.54	-28068.60	-4336.69	-1025.95
	$\sigma_{cls,Max}$15	-100226.54	-28068.60	-4336.69	-81.28
	$\sigma_{cls,Med}$15	-100226.54	-28068.60	-4336.69	-32.07
Combinazioni Frequenti					
232	Ft. 20	-98280.90	9444.82	3555.46	-55.13
	$\sigma_{s,c}$18	-101188.59	9460.79	3476.54	-597.83
	$\sigma_{cls,Max}$18	-101188.59	9460.79	3476.54	-45.51
	$\sigma_{cls,Med}$18	-101188.59	9460.79	3476.54	-22.19
332	Ft. 20	-94830.90	-27221.84	-4291.10	506.06
	$\sigma_{s,c}$18	-97738.59	-27494.47	-4146.75	-999.77
	$\sigma_{cls,Max}$20	-94830.90	-27221.84	-4291.10	-79.41
	$\sigma_{cls,Med}$18	-97738.59	-27494.47	-4146.75	-31.34
Combinazioni Quasi Permanenti					
232	Ft. 22	-98101.45	9394.90	3488.35	-57.54
	$\sigma_{s,c}$21	-100387.70	9344.59	3403.94	-590.97
	$\sigma_{cls,Max}$21	-100387.70	9344.59	3403.94	-44.94
	$\sigma_{cls,Med}$21	-100387.70	9344.59	3403.94	-22.01
332	Ft. 22	-94651.45	-27220.01	-4250.41	505.17
	$\sigma_{s,c}$22	-94651.45	-27220.01	-4250.41	-996.13
	$\sigma_{cls,Max}$22	-94651.45	-27220.01	-4250.41	-79.21
	$\sigma_{cls,Med}$22	-94651.45	-27220.01	-4250.41	-31.08

Pilastro: **34/134** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
34	1	-350647.66	-36.75	-3539.92	0.41
134	1	-344992.66	-2111.81	683.07	0.41

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	542.19	61956.98	2270.26	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	542.19	46467.73	2270.26	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	542.19	61956.98	2270.26	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
34	Ft. 16	-237675.83	-30.74	-2573.21	-737.82
	$\sigma_{s,c}$15	-246152.97	-34.69	-2434.87	-849.67
	$\sigma_{cls,Max}$15	-246152.97	-34.69	-2434.87	-57.12
	$\sigma_{cls,Med}$15	-246152.97	-34.69	-2434.87	-53.92
134	Ft. 16	-233325.83	-1420.52	385.87	-715.10
	$\sigma_{s,c}$17	-240417.03	-1497.39	543.18	-846.42
	$\sigma_{cls,Max}$17	-240417.03	-1497.39	543.18	-58.23
	$\sigma_{cls,Med}$15	-241802.97	-1480.80	261.36	-52.96
Combinazioni Frequenti					
34	Ft. 19	-234755.81	-27.38	-2618.42	-727.59
	$\sigma_{s,c}$20	-240394.16	-4.07	-2815.89	-836.01
	$\sigma_{cls,Max}$20	-240394.16	-4.07	-2815.89	-56.24
	$\sigma_{cls,Med}$20	-240394.16	-4.07	-2815.89	-52.65
134	Ft. 19	-230405.81	-1401.80	428.58	-705.40
	$\sigma_{s,c}$20	-236044.16	-1446.52	672.41	-832.54
	$\sigma_{cls,Max}$20	-236044.16	-1446.52	672.41	-57.27
	$\sigma_{cls,Med}$20	-236044.16	-1446.52	672.41	-51.70
Combinazioni Quasi Permanenti					
34	Ft. 21	-234736.31	-26.96	-2618.23	-727.55
	$\sigma_{s,c}$22	-238936.52	-4.66	-2845.10	-831.72
	$\sigma_{cls,Max}$22	-238936.52	-4.66	-2845.10	-55.96
	$\sigma_{cls,Med}$22	-238936.52	-4.66	-2845.10	-52.34
134	Ft. 21	-230386.31	-1402.09	428.83	-705.32
	$\sigma_{s,c}$22	-234586.52	-1429.56	715.49	-827.92
	$\sigma_{cls,Max}$22	-234586.52	-1429.56	715.49	-56.95
	$\sigma_{cls,Med}$22	-234586.52	-1429.56	715.49	-51.38

Pilastro: **134/234** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
134	1	-281369.28	3882.67	9005.36	0.36
234	1	-276884.28	-2718.17	-6146.16	0.35

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1913.29	61956.98	4594.44	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	1913.29	46467.73	4594.44	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	1913.29	61956.98	4594.44	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
134	Ft. 16	-190412.39	2616.85	5820.42	-447.15

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-196603.78	2747.62	6062.34	-832.52
	$\sigma_{cls,Max}$15	-196603.78	2747.62	6062.34	-59.71
	$\sigma_{cls,Med}$15	-196603.78	2747.62	6062.34	-43.06
234	Ft. 16	-186962.39	-1830.74	-3960.26	-491.25
	$\sigma_{s,c}$17	-192250.25	-1873.43	-4564.00	-765.89
	$\sigma_{cls,Max}$17	-192250.25	-1873.43	-4564.00	-54.01
	$\sigma_{cls,Med}$15	-193153.78	-1943.10	-4174.83	-42.31
Combinazioni Frequenti					
134	Ft. 19	-188267.14	2573.97	5738.42	-442.81
	$\sigma_{s,c}$20	-193626.63	2592.48	5963.52	-816.18
	$\sigma_{cls,Max}$20	-193626.63	2592.48	5963.52	-58.43
	$\sigma_{cls,Med}$20	-193626.63	2592.48	5963.52	-42.41
234	Ft. 19	-184817.14	-1793.99	-3889.33	-486.53
	$\sigma_{s,c}$20	-190176.63	-1755.79	-4413.85	-752.88
	$\sigma_{cls,Max}$20	-190176.63	-1755.79	-4413.85	-52.98
	$\sigma_{cls,Med}$20	-190176.63	-1755.79	-4413.85	-41.66
Combinazioni Quasi Permanenti					
134	Ft. 21	-188250.28	2574.11	5738.14	-442.75
	$\sigma_{s,c}$22	-192935.41	2552.74	5904.91	-811.69
	$\sigma_{cls,Max}$22	-192935.41	2552.74	5904.91	-58.08
	$\sigma_{cls,Med}$22	-192935.41	2552.74	5904.91	-42.26
234	Ft. 21	-184800.28	-1794.13	-3889.45	-486.47
	$\sigma_{s,c}$22	-189485.41	-1716.57	-4363.80	-748.54
	$\sigma_{cls,Max}$22	-189485.41	-1716.57	-4363.80	-52.64
	$\sigma_{cls,Med}$22	-189485.41	-1716.57	-4363.80	-41.50

Pilastro: **234/334** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
234	1	-226529.08	3785.70	8245.39	0.30
334	1	-222044.08	-6407.95	-22435.82	0.35

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3077.86	61956.98	8893.11	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	3077.86	46467.73	8893.11	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	3077.86	61956.98	8893.11	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
234	Ft. 16	-152981.52	2538.68	5572.52	-330.71
	$\sigma_{s,c}$15	-157169.58	2638.78	5832.51	-695.73
	$\sigma_{cls,Max}$15	-157169.58	2638.78	5832.51	-50.43
	$\sigma_{cls,Med}$15	-157169.58	2638.78	5832.51	-34.43
334	Ft. 15	-153719.58	-4413.50	-15408.89	-112.60
	$\sigma_{s,c}$15	-153719.58	-4413.50	-15408.89	-897.50
	$\sigma_{cls,Max}$15	-153719.58	-4413.50	-15408.89	-67.61
	$\sigma_{cls,Med}$15	-153719.58	-4413.50	-15408.89	-33.67

Combinazioni Frequenti					
234	Ft. 19	-151515.36	2506.74	5479.09	-328.44
	$\sigma_{s,c}$20	-156909.20	2635.58	4971.67	-680.69
	$\sigma_{cls,Max}$20	-156909.20	2635.58	4971.67	-49.27
	$\sigma_{cls,Med}$20	-156909.20	2635.58	4971.67	-34.37
334	Ft. 18	-149458.95	-4310.72	-14725.04	-113.06
	$\sigma_{s,c}$18	-149458.95	-4310.72	-14725.04	-869.04
	$\sigma_{cls,Max}$18	-149458.95	-4310.72	-14725.04	-65.47
	$\sigma_{cls,Med}$20	-153459.20	-4615.24	-12707.07	-33.61
Combinazioni Quasi Permanenti					
234	Ft. 21	-151500.84	2507.04	5477.69	-328.41
	$\sigma_{s,c}$22	-156946.45	2612.09	4902.12	-678.93
	$\sigma_{cls,Max}$22	-156946.45	2612.09	4902.12	-49.12
	$\sigma_{cls,Med}$22	-156946.45	2612.09	4902.12	-34.38
334	Ft. 21	-148050.84	-4276.10	-14500.21	-113.21
	$\sigma_{s,c}$21	-148050.84	-4276.10	-14500.21	-859.64
	$\sigma_{cls,Max}$21	-148050.84	-4276.10	-14500.21	-64.77
	$\sigma_{cls,Med}$22	-153496.45	-4610.48	-12624.82	-33.62

Pilastro: **35/135** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
35	1	-500885.91	-6989.38	1558.01	0.60
135	1	-495230.91	-4558.94	-5665.56	0.62

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	2171.00	86297.23	1712.83	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	2171.00	64722.92	1712.83	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	2171.00	86297.23	1712.83	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
35	Ft. 16	-337060.13	-4749.77	917.56	-1000.54
	$\sigma_{s,c}$15	-348653.41	-5049.59	1045.78	-1261.37
	$\sigma_{cls,Max}$15	-348653.41	-5049.59	1045.78	-86.18
	$\sigma_{cls,Med}$15	-348653.41	-5049.59	1045.78	-76.37
135	Ft. 17	-332765.41	-3429.42	-4005.72	-909.78
	$\sigma_{s,c}$15	-344303.41	-3069.07	-3948.82	-1307.04
	$\sigma_{cls,Max}$15	-344303.41	-3069.07	-3948.82	-92.19
	$\sigma_{cls,Med}$15	-344303.41	-3069.07	-3948.82	-75.41
Combinazioni Frequenti					
35	Ft. 20	-331639.06	-4094.91	1005.46	-990.64
	$\sigma_{s,c}$18	-337042.22	-4742.51	921.50	-1214.25
	$\sigma_{cls,Max}$18	-337042.22	-4742.51	921.50	-82.84
	$\sigma_{cls,Med}$18	-337042.22	-4742.51	921.50	-73.82
135	Ft. 20	-327289.06	-3328.26	-3780.27	-900.62
	$\sigma_{s,c}$18	-332692.22	-2987.05	-3711.85	-1260.01
	$\sigma_{cls,Max}$18	-332692.22	-2987.05	-3711.85	-88.77
	$\sigma_{cls,Med}$18	-332692.22	-2987.05	-3711.85	-72.87
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
35	Ft. 22	-329813.66	-4049.33	960.50	-986.82
	$\sigma_{s,c}$21	-333174.88	-4641.36	879.41	-1198.55
	$\sigma_{cls,Max}$21	-333174.88	-4641.36	879.41	-81.73
	$\sigma_{cls,Med}$21	-333174.88	-4641.36	879.41	-72.98
135	Ft. 22	-325463.66	-3294.54	-3705.13	-897.56
	$\sigma_{s,c}$21	-328824.88	-2959.48	-3632.39	-1244.32
	$\sigma_{cls,Max}$21	-328824.88	-2959.48	-3632.39	-87.63
	$\sigma_{cls,Med}$21	-328824.88	-2959.48	-3632.39	-72.02

Pilastro: **135/235** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
135	1	-429598.09	6640.75	6844.84	0.55
235	1	-425113.09	3162.24	-1852.97	0.50

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1525.33	86297.23	2521.11	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	1525.33	64722.92	2521.11	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	1525.33	86297.23	2521.11	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
135	Ft. 17	-286153.75	4632.65	4689.45	-715.21
	$\sigma_{s,c}$15	-297711.75	4776.38	4775.58	-1208.19
	$\sigma_{cls,Max}$15	-297711.75	4776.38	4775.58	-86.85
	$\sigma_{cls,Med}$15	-297711.75	4776.38	4775.58	-65.21
235	Ft. 17	-282703.75	2343.24	-1031.19	-857.70
	$\sigma_{s,c}$15	-294261.75	1917.02	-1251.60	-1037.98
	$\sigma_{cls,Max}$15	-294261.75	1917.02	-1251.60	-70.97
	$\sigma_{cls,Med}$15	-294261.75	1917.02	-1251.60	-64.45
Combinazioni Frequenti					
135	Ft. 20	-283238.72	4412.03	4490.50	-715.57
	$\sigma_{s,c}$18	-288590.47	4545.27	4541.78	-1167.00
	$\sigma_{cls,Max}$18	-288590.47	4545.27	4541.78	-83.79
	$\sigma_{cls,Med}$18	-288590.47	4545.27	4541.78	-63.21
235	Ft. 20	-279788.72	2463.96	-1023.11	-846.40
	$\sigma_{s,c}$18	-285140.47	1947.02	-1210.04	-1007.18
	$\sigma_{cls,Max}$18	-285140.47	1947.02	-1210.04	-68.87
	$\sigma_{cls,Med}$18	-285140.47	1947.02	-1210.04	-62.46
Combinazioni Quasi Permanenti					
135	Ft. 22	-282267.06	4338.49	4424.19	-715.69
	$\sigma_{s,c}$21	-285552.47	4468.16	4463.25	-1153.26
	$\sigma_{cls,Max}$21	-285552.47	4468.16	4463.25	-82.77
	$\sigma_{cls,Med}$21	-285552.47	4468.16	4463.25	-62.55
235	Ft. 22	-278817.06	2504.21	-1020.42	-842.64
	$\sigma_{s,c}$21	-282102.47	1957.25	-1195.70	-996.91
	$\sigma_{cls,Max}$21	-282102.47	1957.25	-1195.70	-68.17

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-282102.47	1957.25	-1195.70	-61.79

Pilastro: **235/335** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
235	1	-342251.84	17390.12	-2643.32	0.45
335	1	-337766.84	-50736.45	1845.99	0.57

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	21306.10	86297.23	1578.60	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	21306.10	64722.92	1578.60	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	21306.10	86297.23	1578.60	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
235	Ft. 17	-224005.59	12574.75	-1560.22	-480.66
	$\sigma_{s,c}$15	-235510.47	11819.89	-1920.99	-1028.22
	$\sigma_{cls,Max}$15	-235510.47	11819.89	-1920.99	-72.84
	$\sigma_{cls,Med}$15	-235510.47	11819.89	-1920.99	-51.58
335	Ft. 17	-220555.59	-37208.61	276.30	-107.23
	$\sigma_{s,c}$15	-232060.47	-34377.16	1365.18	-1368.18
	$\sigma_{cls,Max}$15	-232060.47	-34377.16	1365.18	-98.87
	$\sigma_{cls,Med}$15	-232060.47	-34377.16	1365.18	-50.83
Combinazioni Frequenti					
235	Ft. 20	-224272.77	12360.22	-1507.38	-486.72
	$\sigma_{s,c}$18	-229521.34	11492.25	-1854.98	-1001.09
	$\sigma_{cls,Max}$18	-229521.34	11492.25	-1854.98	-70.90
	$\sigma_{cls,Med}$18	-229521.34	11492.25	-1854.98	-50.27
335	Ft. 20	-220822.77	-37093.76	353.18	-107.54
	$\sigma_{s,c}$20	-220822.77	-37093.76	353.18	-1343.50
	$\sigma_{cls,Max}$18	-226071.34	-33829.86	1387.66	-96.94
	$\sigma_{cls,Med}$18	-226071.34	-33829.86	1387.66	-49.52
Combinazioni Quasi Permanenti					
235	Ft. 22	-224361.83	12288.71	-1489.76	-488.75
	$\sigma_{s,c}$21	-227526.98	11383.12	-1833.58	-992.07
	$\sigma_{cls,Max}$21	-227526.98	11383.12	-1833.58	-70.25
	$\sigma_{cls,Med}$21	-227526.98	11383.12	-1833.58	-49.84
335	Ft. 22	-220911.83	-37055.47	378.80	-107.64
	$\sigma_{s,c}$22	-220911.83	-37055.47	378.80	-1343.98
	$\sigma_{cls,Max}$22	-220911.83	-37055.47	378.80	-96.61
	$\sigma_{cls,Med}$21	-224076.98	-33647.15	1396.34	-49.08

Pilastro: **36/136** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
36	1	-509363.03	-4380.95	816.03	0.60

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
136	1	-503708.03	-7139.30	-19.65	0.60

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2939.94	86297.23	350.77	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	2939.94	64722.92	350.77	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	2939.94	86297.23	350.77	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
36	Ft. 16	-342332.31	-2997.78	500.38	-1059.79
	$\sigma_{s,c}$15	-354398.47	-3273.92	544.89	-1235.27
	$\sigma_{cls,Max}$15	-354398.47	-3273.92	544.89	-83.55
	$\sigma_{cls,Med}$15	-354398.47	-3273.92	544.89	-77.63
136	Ft. 17	-338936.69	-5067.25	47.73	-1029.18
	$\sigma_{s,c}$15	-350048.47	-4778.78	9.67	-1228.57
	$\sigma_{cls,Max}$15	-350048.47	-4778.78	9.67	-82.76
	$\sigma_{cls,Med}$15	-350048.47	-4778.78	9.67	-76.67
Combinazioni Frequenti					
36	Ft. 19	-338319.72	-2903.06	485.35	-1048.63
	$\sigma_{s,c}$18	-342342.13	-2995.01	500.18	-1189.67
	$\sigma_{cls,Max}$18	-342342.13	-2995.01	500.18	-80.41
	$\sigma_{cls,Med}$18	-342342.13	-2995.01	500.18	-74.98
136	Ft. 20	-332863.94	-4935.87	58.40	-1011.04
	$\sigma_{s,c}$18	-337992.13	-4644.69	21.00	-1187.12
	$\sigma_{cls,Max}$18	-337992.13	-4644.69	21.00	-79.99
	$\sigma_{cls,Med}$18	-337992.13	-4644.69	21.00	-74.03
Combinazioni Quasi Permanenti					
36	Ft. 22	-335189.69	-2356.72	463.78	-1047.97
	$\sigma_{s,c}$21	-338321.69	-2902.50	485.31	-1174.48
	$\sigma_{cls,Max}$21	-338321.69	-2902.50	485.31	-79.37
	$\sigma_{cls,Med}$21	-338321.69	-2902.50	485.31	-74.10
136	Ft. 22	-330839.69	-4892.08	61.96	-1004.99
	$\sigma_{s,c}$21	-333971.69	-4600.17	24.73	-1173.30
	$\sigma_{cls,Max}$21	-333971.69	-4600.17	24.73	-79.07
	$\sigma_{cls,Med}$21	-333971.69	-4600.17	24.73	-73.15

Pilastro: **136/236** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
136	1	-421154.84	4294.25	-847.79	0.50
236	1	-416669.84	4809.97	31.52	0.49

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	596.56	86297.23	392.49	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	596.56	64722.92	392.49	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	596.56	86297.23	392.49	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
136	Ft. 17	-280535.22	3188.92	-529.60	-852.70
	$\sigma_{s,c}$15	-291596.66	3234.31	-590.81	-1029.75
	$\sigma_{cls,Max}$15	-291596.66	3234.31	-590.81	-69.90
	$\sigma_{cls,Med}$15	-291596.66	3234.31	-590.81	-63.87
236	Ft. 17	-277085.22	3301.65	-166.65	-851.06
	$\sigma_{s,c}$15	-288146.66	2980.14	17.50	-996.01
	$\sigma_{cls,Max}$15	-288146.66	2980.14	17.50	-66.95
	$\sigma_{cls,Med}$15	-288146.66	2980.14	17.50	-63.11
Combinazioni Frequenti					
136	Ft. 20	-277553.03	2994.98	-513.94	-846.57
	$\sigma_{s,c}$18	-282626.31	3061.86	-568.65	-996.75
	$\sigma_{cls,Max}$18	-282626.31	3061.86	-568.65	-67.64
	$\sigma_{cls,Med}$18	-282626.31	3061.86	-568.65	-61.90
236	Ft. 20	-274103.03	3405.27	-156.27	-839.90
	$\sigma_{s,c}$18	-279176.31	2958.80	23.27	-966.38
	$\sigma_{cls,Max}$18	-279176.31	2958.80	23.27	-64.98
	$\sigma_{cls,Med}$18	-279176.31	2958.80	23.27	-61.15
Combinazioni Quasi Permanenti					
136	Ft. 22	-276558.97	2930.33	-508.72	-844.53
	$\sigma_{s,c}$21	-279634.66	3003.89	-561.38	-985.74
	$\sigma_{cls,Max}$21	-279634.66	3003.89	-561.38	-66.89
	$\sigma_{cls,Med}$21	-279634.66	3003.89	-561.38	-61.25
236	Ft. 22	-273108.97	3439.80	-152.81	-836.18
	$\sigma_{s,c}$22	-273108.97	3439.80	-152.81	-958.43
	$\sigma_{cls,Max}$22	-273108.97	3439.80	-152.81	-64.68
	$\sigma_{cls,Med}$21	-276184.66	2952.11	25.29	-60.49

Pilastro: **236/336** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
236	1	-335952.94	19796.00	495.97	0.45
336	3	-315031.75	-57324.29	740.08	0.57

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	22637.68	86297.23	522.56	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	22637.68	64722.92	522.56	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	22637.68	86297.23	522.56	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
236	Ft. 17	-220029.83	14068.96	60.75	-490.85
	$\sigma_{s,c}$15	-230987.28	13415.83	335.41	-989.03
	$\sigma_{cls,Max}$15	-230987.28	13415.83	335.41	-68.70
	$\sigma_{cls,Med}$15	-230987.28	13415.83	335.41	-50.59
336	Ft. 17	-216579.83	-38773.18	496.98	-60.35
	$\sigma_{s,c}$17	-216579.83	-38773.18	496.98	-1362.26
	$\sigma_{cls,Max}$17	-216579.83	-38773.18	496.98	-98.28

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-227537.28	-36029.30	-401.60	-49.84
Combinazioni Frequenti					
236	Ft. 20	-220067.41	13819.10	22.03	-496.30
	$\sigma_{s,c}$18	-225029.64	13023.69	297.43	-961.83
	$\sigma_{cls,Max}$18	-225029.64	13023.69	297.43	-66.77
	$\sigma_{cls,Med}$18	-225029.64	13023.69	297.43	-49.29
336	Ft. 20	-216617.41	-38655.07	541.68	-61.07
	$\sigma_{s,c}$20	-216617.41	-38655.07	541.68	-1361.83
	$\sigma_{cls,Max}$20	-216617.41	-38655.07	541.68	-98.28
	$\sigma_{cls,Med}$18	-221579.64	-35462.54	-355.72	-48.53
Combinazioni Quasi Permanenti					
236	Ft. 22	-220079.94	13735.81	9.12	-498.11
	$\sigma_{s,c}$21	-223042.31	12893.07	284.76	-952.76
	$\sigma_{cls,Max}$21	-223042.31	12893.07	284.76	-66.13
	$\sigma_{cls,Med}$21	-223042.31	12893.07	284.76	-48.85
336	Ft. 22	-216629.94	-38615.70	556.58	-61.31
	$\sigma_{s,c}$22	-216629.94	-38615.70	556.58	-1361.69
	$\sigma_{cls,Max}$22	-216629.94	-38615.70	556.58	-98.29
	$\sigma_{cls,Med}$22	-216629.94	-38615.70	556.58	-48.23

Pilastro: **37/137** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
37	1	-518288.88	-2018.15	643.19	0.60
137	1	-512633.88	-9208.57	-976.31	0.62

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4161.79	86297.23	462.89	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	4161.79	64722.92	462.89	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	4161.79	86297.23	462.89	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
37	Ft. 17	-347755.88	-1893.78	455.37	-1097.10
	$\sigma_{s,c}$15	-360758.81	-1712.34	430.35	-1226.98
	$\sigma_{cls,Max}$15	-360758.81	-1712.34	430.35	-82.59
	$\sigma_{cls,Med}$15	-360758.81	-1712.34	430.35	-79.02
137	Ft. 17	-343405.88	-5810.02	-708.55	-1010.69
	$\sigma_{s,c}$15	-356408.81	-6123.64	-680.52	-1292.80
	$\sigma_{cls,Max}$15	-356408.81	-6123.64	-680.52	-88.05
	$\sigma_{cls,Med}$15	-356408.81	-6123.64	-680.52	-78.07
Combinazioni Frequenti					
37	Ft. 20	-341664.38	-1852.56	402.68	-1079.43
	$\sigma_{s,c}$18	-348474.25	-1520.64	381.28	-1181.92
	$\sigma_{cls,Max}$18	-348474.25	-1520.64	381.28	-79.50
	$\sigma_{cls,Med}$18	-348474.25	-1520.64	381.28	-76.33
137	Ft. 20	-337314.38	-5614.82	-658.29	-995.47

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-344124.25	-5913.89	-628.71	-1247.36
	$\sigma_{cls,Max}$18	-344124.25	-5913.89	-628.71	-84.93
	$\sigma_{cls,Med}$18	-344124.25	-5913.89	-628.71	-75.38
Combinazioni Quasi Permanenti					
37	Ft. 22	-339633.88	-1838.83	385.11	-1073.55
	$\sigma_{s,c}$21	-344381.97	-1457.16	365.02	-1166.92
	$\sigma_{cls,Max}$21	-344381.97	-1457.16	365.02	-78.47
	$\sigma_{cls,Med}$21	-344381.97	-1457.16	365.02	-75.43
137	Ft. 22	-335283.88	-5549.75	-641.54	-990.40
	$\sigma_{s,c}$21	-340031.97	-5844.29	-611.69	-1232.24
	$\sigma_{cls,Max}$21	-340031.97	-5844.29	-611.69	-83.89
	$\sigma_{cls,Med}$21	-340031.97	-5844.29	-611.69	-74.48

Pilastro: **137/237** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
137	1	-430948.16	2437.03	765.12	0.50
237	1	-426463.16	5533.49	-600.71	0.51

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	982.67	86297.23	452.00	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	982.67	64722.92	452.00	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	982.67	86297.23	452.00	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
137	Ft. 17	-285405.09	2160.67	508.33	-886.19
	$\sigma_{s,c}$15	-298526.06	2033.39	572.62	-1032.29
	$\sigma_{cls,Max}$15	-298526.06	2033.39	572.62	-69.83
	$\sigma_{cls,Med}$15	-298526.06	2033.39	572.62	-65.39
237	Ft. 16	-285883.78	3367.29	-417.68	-870.91
	$\sigma_{s,c}$15	-295076.06	3426.68	-448.34	-1039.79
	$\sigma_{cls,Max}$15	-295076.06	3426.68	-448.34	-70.44
	$\sigma_{cls,Med}$15	-295076.06	3426.68	-448.34	-64.63
Combinazioni Frequenti					
137	Ft. 20	-282414.81	2013.41	466.36	-880.11
	$\sigma_{s,c}$18	-289320.56	1924.75	533.38	-999.02
	$\sigma_{cls,Max}$18	-289320.56	1924.75	533.38	-67.55
	$\sigma_{cls,Med}$18	-289320.56	1924.75	533.38	-63.37
237	Ft. 19	-282807.00	3344.25	-405.90	-861.55
	$\sigma_{s,c}$18	-285870.56	3363.93	-416.07	-1007.49
	$\sigma_{cls,Max}$18	-285870.56	3363.93	-416.07	-68.24
	$\sigma_{cls,Med}$18	-285870.56	3363.93	-416.07	-62.62
Combinazioni Quasi Permanenti					
137	Ft. 22	-281418.13	1964.32	452.37	-878.08
	$\sigma_{s,c}$21	-286254.34	1887.88	520.66	-987.94
	$\sigma_{cls,Max}$21	-286254.34	1887.88	520.66	-66.79

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-286254.34	1887.88	520.66	-62.70
237	Ft. 22	-277968.13	2847.88	-220.63	-859.67
	$\sigma_{s,c}$21	-282804.34	3343.58	-405.58	-996.75
	$\sigma_{cls,Max}$21	-282804.34	3343.58	-405.58	-67.51
	$\sigma_{cls,Med}$21	-282804.34	3343.58	-405.58	-61.94

Pilastro: **237/337** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
237	1	-344116.41	20754.13	810.19	0.46
337	1	-339631.41	-53993.10	-1608.47	0.58

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	21665.87	86297.23	1157.34	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	21665.87	64722.92	1157.34	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	21665.87	86297.23	1157.34	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
237	Ft. 17	-223448.22	12922.78	842.21	-495.97
	$\sigma_{s,c}$15	-236726.33	14030.69	590.27	-1026.05
	$\sigma_{cls,Max}$15	-236726.33	14030.69	590.27	-71.57
	$\sigma_{cls,Med}$15	-236726.33	14030.69	590.27	-51.85
337	Ft. 16	-227180.53	-35916.68	-1080.51	-124.54
	$\sigma_{s,c}$15	-233276.33	-36538.54	-1155.29	-1400.85
	$\sigma_{cls,Max}$15	-233276.33	-36538.54	-1155.29	-101.20
	$\sigma_{cls,Med}$15	-233276.33	-36538.54	-1155.29	-51.10
Combinazioni Frequenti					
237	Ft. 20	-223576.70	12638.44	803.05	-502.29
	$\sigma_{s,c}$18	-230619.83	13581.19	538.28	-996.98
	$\sigma_{cls,Max}$18	-230619.83	13581.19	538.28	-69.49
	$\sigma_{cls,Med}$18	-230619.83	13581.19	538.28	-50.51
337	Ft. 19	-225138.23	-35714.35	-1049.97	-122.11
	$\sigma_{s,c}$18	-227169.83	-35921.81	-1074.70	-1368.13
	$\sigma_{cls,Max}$18	-227169.83	-35921.81	-1074.70	-98.81
	$\sigma_{cls,Med}$18	-227169.83	-35921.81	-1074.70	-49.76
Combinazioni Quasi Permanenti					
237	Ft. 22	-223619.52	12543.67	789.99	-504.40
	$\sigma_{s,c}$21	-228586.09	13431.54	521.50	-987.31
	$\sigma_{cls,Max}$21	-228586.09	13431.54	521.50	-68.80
	$\sigma_{cls,Med}$21	-228586.09	13431.54	521.50	-50.07
337	Ft. 21	-225136.09	-35715.38	-1048.81	-122.13
	$\sigma_{s,c}$21	-225136.09	-35715.38	-1048.81	-1357.25
	$\sigma_{cls,Max}$21	-225136.09	-35715.38	-1048.81	-98.02
	$\sigma_{cls,Med}$21	-225136.09	-35715.38	-1048.81	-49.31

Pilastro: **38/138** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 20 ø 20 Af=62.83 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 7f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
38	1	-312581.44	-7280.17	6199.02	0.37
138	1	-306926.44	-5472.30	2674.01	0.34

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4332.64	86297.23	1271.73	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	4332.64	64722.92	1271.73	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	4332.64	86297.23	1271.73	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm^2]
Combinazioni Rare					
38	Ft. 16	-211825.63	-5411.56	4354.46	-433.51
	$\sigma_{s,c}$15	-219322.41	-5652.09	4492.27	-882.69
	$\sigma_{cls,Max}$15	-219322.41	-5652.09	4492.27	-64.44
	$\sigma_{cls,Med}$15	-219322.41	-5652.09	4492.27	-44.37
138	Ft. 17	-206268.78	-3637.09	2054.33	-510.43
	$\sigma_{s,c}$15	-214972.41	-3472.28	1805.07	-758.26
	$\sigma_{cls,Max}$15	-214972.41	-3472.28	1805.07	-53.00
	$\sigma_{cls,Med}$15	-214972.41	-3472.28	1805.07	-43.49
Combinazioni Frequenti					
38	Ft. 19	-209160.52	-5289.21	4281.79	-429.41
	$\sigma_{s,c}$18	-211653.73	-5367.94	4326.80	-850.24
	$\sigma_{cls,Max}$18	-211653.73	-5367.94	4326.80	-62.06
	$\sigma_{cls,Med}$18	-211653.73	-5367.94	4326.80	-42.82
138	Ft. 20	-202525.95	-3472.92	1894.91	-506.21
	$\sigma_{s,c}$18	-207303.73	-3340.42	1703.22	-730.01
	$\sigma_{cls,Max}$18	-207303.73	-3340.42	1703.22	-50.99
	$\sigma_{cls,Med}$18	-207303.73	-3340.42	1703.22	-41.94
Combinazioni Quasi Permanenti					
38	Ft. 21	-209126.14	-5280.49	4276.25	-429.60
	$\sigma_{s,c}$21	-209126.14	-5280.49	4276.25	-839.76
	$\sigma_{cls,Max}$21	-209126.14	-5280.49	4276.25	-61.30
	$\sigma_{cls,Med}$21	-209126.14	-5280.49	4276.25	-42.31
138	Ft. 22	-201278.33	-3418.19	1841.77	-504.80
	$\sigma_{s,c}$21	-204776.14	-3294.41	1666.53	-720.57
	$\sigma_{cls,Max}$21	-204776.14	-3294.41	1666.53	-50.32
	$\sigma_{cls,Med}$21	-204776.14	-3294.41	1666.53	-41.43

Pilastro: **138/238** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 20 ø 20 Af=62.83 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 7f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
138	1	-245767.44	3096.70	-12228.20	0.35
238	1	-241282.45	2942.51	9633.84	0.32

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	567.40	86297.23	6399.22	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	567.40	64722.92	6399.22	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	567.40	86297.23	6399.22	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
138	Ft. 17	-163107.17	2428.05	-8626.25	-208.80
	$\sigma_{s,c}$15	-171500.08	2447.09	-8579.58	-805.66
	$\sigma_{cls,Max}$15	-171500.08	2447.09	-8579.58	-63.00
	$\sigma_{cls,Med}$15	-171500.08	2447.09	-8579.58	-34.70
238	Ft. 17	-159657.17	1414.19	6886.17	-264.19
	$\sigma_{s,c}$15	-168050.08	1755.25	6789.32	-732.87
	$\sigma_{cls,Max}$15	-168050.08	1755.25	6789.32	-56.18
	$\sigma_{cls,Med}$15	-168050.08	1755.25	6789.32	-34.00
Combinazioni Frequenti					
138	Ft. 20	-161636.39	2320.98	-8233.20	-217.32
	$\sigma_{s,c}$18	-166150.41	2339.19	-8170.18	-775.95
	$\sigma_{cls,Max}$18	-166150.41	2339.19	-8170.18	-60.58
	$\sigma_{cls,Med}$18	-166150.41	2339.19	-8170.18	-33.62
238	Ft. 20	-158186.39	1490.01	6519.03	-269.13
	$\sigma_{s,c}$18	-162700.41	1727.25	6438.15	-706.08
	$\sigma_{cls,Max}$18	-162700.41	1727.25	6438.15	-54.02
	$\sigma_{cls,Med}$18	-162700.41	1727.25	6438.15	-32.92
Combinazioni Quasi Permanenti					
138	Ft. 22	-161146.13	2285.29	-8102.19	-220.16
	$\sigma_{s,c}$21	-164391.23	2303.13	-8032.56	-766.09
	$\sigma_{cls,Max}$21	-164391.23	2303.13	-8032.56	-59.77
	$\sigma_{cls,Med}$21	-164391.23	2303.13	-8032.56	-33.26
238	Ft. 22	-157696.13	1515.28	6396.65	-270.77
	$\sigma_{s,c}$21	-160941.23	1718.24	6320.00	-697.20
	$\sigma_{cls,Max}$21	-160941.23	1718.24	6320.00	-53.31
	$\sigma_{cls,Med}$21	-160941.23	1718.24	6320.00	-32.56

Pilastro: **238/338** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 20 ø 20 Af=62.83 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 7f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
238	1	-193921.09	16640.29	-17127.04	0.38
338	1	-189436.09	-45845.13	27042.99	0.63

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	18111.72	86297.23	12802.91	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	18111.72	64722.92	12802.91	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	18111.72	86297.23	12802.91	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
238	Ft. 17	-125605.35	10848.54	-11669.89	207.71

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-134148.11	11221.93	-11793.25	-955.21
	$\sigma_{cls,Max}$15	-134148.11	11221.93	-11793.25	-79.00
	$\sigma_{cls,Med}$15	-134148.11	11221.93	-11793.25	-32.54
338	Ft. 17	-122155.35	-29414.36	18105.58	1345.01
	$\sigma_{s,c}$15	-130698.15	-30916.75	18464.91	-1690.53
	$\sigma_{cls,Max}$15	-130698.15	-30916.75	18464.91	-148.71
	$\sigma_{cls,Med}$15	-130698.15	-30916.75	18464.91	-51.91
Combinazioni Frequenti					
238	Ft. 20	-126300.25	10609.43	-11385.75	181.81
	$\sigma_{s,c}$18	-130794.97	10837.37	-11369.50	-924.21
	$\sigma_{cls,Max}$18	-130794.97	10837.37	-11369.50	-76.33
	$\sigma_{cls,Med}$18	-130794.97	10837.37	-11369.50	-31.50
338	Ft. 20	-122850.25	-29220.14	17894.85	1308.43
	$\sigma_{s,c}$18	-127344.95	-30298.24	17916.62	-1647.87
	$\sigma_{cls,Max}$18	-127344.95	-30298.24	17916.62	-144.85
	$\sigma_{cls,Med}$18	-127344.95	-30298.24	17916.62	-50.50
Combinazioni Quasi Permanenti					
238	Ft. 22	-126531.88	10529.73	-11291.03	173.41
	$\sigma_{s,c}$21	-129697.21	10707.47	-11225.34	-913.79
	$\sigma_{cls,Max}$21	-129697.21	10707.47	-11225.34	-75.42
	$\sigma_{cls,Med}$21	-129697.21	10707.47	-11225.34	-31.15
338	Ft. 22	-123081.88	-29155.40	17824.61	1296.30
	$\sigma_{s,c}$21	-126247.21	-30085.70	17728.63	-1633.25
	$\sigma_{cls,Max}$21	-126247.21	-30085.70	17728.63	-143.52
	$\sigma_{cls,Med}$21	-126247.21	-30085.70	17728.63	-50.01

Pilastro: **39/2575** / L 0.85[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 85.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
39	1	-255963.39	-33189.78	5422.47	0.42
2575	1	-254533.36	-3058.84	3253.13	0.32

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	0.98	27391.76	86297.23	1972.13	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
39	Ft. 17	-169654.20	-22412.00	3650.72	-74.40
	$\sigma_{s,c}$15	-178185.70	-23439.00	3722.75	-1087.37
	$\sigma_{cls,Max}$15	-178185.70	-23439.00	3722.75	-80.91
	$\sigma_{cls,Med}$15	-178185.70	-23439.00	3722.75	-39.14
2575	Ft. 17	-168554.20	-2186.36	2223.92	-447.28
	$\sigma_{s,c}$15	-177085.70	-2486.15	2223.14	-693.21
	$\sigma_{cls,Max}$15	-177085.70	-2486.15	2223.14	-49.19
	$\sigma_{cls,Med}$15	-177085.70	-2486.15	2223.14	-38.79
Combinazioni Frequenti					
39	Ft. 20	-167120.53	-22022.10	3554.40	-75.56

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-172938.11	-22693.72	3592.96	-1053.79
	$\sigma_{cls,Max}$18	-172938.11	-22693.72	3592.96	-78.39
	$\sigma_{cls,Med}$18	-172938.11	-22693.72	3592.96	-37.98
2575	Ft. 20	-166020.53	-2142.93	2153.10	-441.92
	$\sigma_{s,c}$18	-171838.11	-2355.44	2137.14	-671.09
	$\sigma_{cls,Max}$18	-171838.11	-2355.44	2137.14	-47.60
	$\sigma_{cls,Med}$18	-171838.11	-2355.44	2137.14	-37.64
Combinazioni Quasi Permanenti					
39	Ft. 22	-166275.98	-21892.13	3522.29	-75.95
	$\sigma_{s,c}$21	-171202.38	-22451.76	3549.98	-1042.76
	$\sigma_{cls,Max}$21	-171202.38	-22451.76	3549.98	-77.56
	$\sigma_{cls,Med}$21	-171202.38	-22451.76	3549.98	-37.59
2575	Ft. 22	-165175.98	-2128.45	2129.50	-440.13
	$\sigma_{s,c}$21	-170102.38	-2317.24	2108.69	-663.86
	$\sigma_{cls,Max}$21	-170102.38	-2317.24	2108.69	-47.08
	$\sigma_{cls,Med}$21	-170102.38	-2317.24	2108.69	-37.26

Pilastro: **2575/139** / L 3.00[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 100.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
2575	1	-386000.38	22820.08	1897.44	0.52
139	1	-381775.38	-17872.88	1702.45	0.50

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	13481.21	86297.23	926.12	61956.98	ø 10 2br.x4br./15.0
1.13	2.13	13481.21	64722.92	926.12	46467.73	ø 10 2br.x4br./20.0
2.13	3.13	13481.21	86297.23	926.12	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
2575	Ft. 17	-254556.34	14681.50	1331.20	-553.86
	$\sigma_{s,c}$15	-267768.56	15320.48	1261.16	-1170.48
	$\sigma_{cls,Max}$15	-267768.56	15320.48	1261.16	-82.19
	$\sigma_{cls,Med}$15	-267768.56	15320.48	1261.16	-58.65
139	Ft. 17	-251306.34	-11800.87	1187.67	-594.86
	$\sigma_{s,c}$15	-264518.56	-11971.45	1296.84	-1106.15
	$\sigma_{cls,Max}$15	-264518.56	-11971.45	1296.84	-77.35
	$\sigma_{cls,Med}$15	-264518.56	-11971.45	1296.84	-57.94
Combinazioni Frequenti					
2575	Ft. 20	-250907.95	14516.97	1272.94	-546.41
	$\sigma_{s,c}$18	-260000.88	14968.71	1200.76	-1137.28
	$\sigma_{cls,Max}$18	-260000.88	14968.71	1200.76	-79.85
	$\sigma_{cls,Med}$18	-260000.88	14968.71	1200.76	-56.95
139	Ft. 20	-247657.95	-11466.12	1133.49	-590.07
	$\sigma_{s,c}$18	-256750.88	-11533.04	1228.88	-1071.30
	$\sigma_{cls,Max}$18	-256750.88	-11533.04	1228.88	-74.87
	$\sigma_{cls,Med}$18	-256750.88	-11533.04	1228.88	-56.24

Combinazioni Quasi Permanenti					
2575	Ft. 22	-249691.81	14462.13	1253.52	-543.93
	$\sigma_{s,c}$21	-257419.97	14844.34	1180.68	-1126.13
	$\sigma_{cls,Max}$21	-257419.97	14844.34	1180.68	-79.06
	$\sigma_{cls,Med}$21	-257419.97	14844.34	1180.68	-56.38
139	Ft. 22	-246441.81	-11354.54	1115.43	-588.48
	$\sigma_{s,c}$21	-254169.97	-11384.71	1206.54	-1059.68
	$\sigma_{cls,Max}$21	-254169.97	-11384.71	1206.54	-74.04
	$\sigma_{cls,Med}$21	-254169.97	-11384.71	1206.54	-55.67

Pilastro: **139/239** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
139	1	-329136.22	-4986.03	-5180.16	0.42
239	1	-324651.22	1252.20	2957.70	0.40

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	1808.18	86297.23	2358.80	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	1808.18	64722.92	2358.80	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	1808.18	86297.23	2358.80	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
139	Ft. 17	-213885.52	-2781.69	-3681.70	-540.10
	$\sigma_{s,c}$15	-227192.30	-2970.15	-3741.12	-914.04
	$\sigma_{cls,Max}$15	-227192.30	-2970.15	-3741.12	-65.74
	$\sigma_{cls,Med}$15	-227192.30	-2970.15	-3741.12	-49.76
239	Ft. 17	-210435.52	376.49	2225.49	-614.43
	$\sigma_{s,c}$15	-223742.30	561.07	2210.54	-814.61
	$\sigma_{cls,Max}$15	-223742.30	561.07	2210.54	-56.93
	$\sigma_{cls,Med}$15	-223742.30	561.07	2210.54	-49.01
Combinazioni Frequenti					
139	Ft. 20	-212184.81	-2819.63	-3478.08	-540.37
	$\sigma_{s,c}$18	-221400.91	-2918.67	-3533.66	-887.57
	$\sigma_{cls,Max}$18	-221400.91	-2918.67	-3533.66	-63.72
	$\sigma_{cls,Med}$18	-221400.91	-2918.67	-3533.66	-48.49
239	Ft. 20	-208734.81	509.69	2024.53	-613.06
	$\sigma_{s,c}$18	-217950.91	556.18	2038.69	-790.03
	$\sigma_{cls,Max}$18	-217950.91	556.18	2038.69	-55.10
	$\sigma_{cls,Med}$18	-217950.91	556.18	2038.69	-47.74
Combinazioni Quasi Permanenti					
139	Ft. 22	-211617.92	-2832.28	-3410.20	-540.46
	$\sigma_{s,c}$21	-219477.61	-2901.21	-3464.93	-878.78
	$\sigma_{cls,Max}$21	-219477.61	-2901.21	-3464.93	-63.06
	$\sigma_{cls,Med}$21	-219477.61	-2901.21	-3464.93	-48.07
239	Ft. 22	-208167.92	554.08	1957.54	-612.60
	$\sigma_{s,c}$21	-216027.61	555.31	1981.62	-781.89
	$\sigma_{cls,Max}$21	-216027.61	555.31	1981.62	-54.49
	$\sigma_{cls,Med}$21	-216027.61	555.31	1981.62	-47.32

Pilastro: **239/339** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
239	1	-272778.47	14835.47	-5006.76	0.37
339	1	-268293.47	-40189.29	8038.46	0.48

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	15949.21	86297.23	3781.22	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	15949.21	64722.92	3781.22	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	15949.21	86297.23	3781.22	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm^2]
Combinazioni Rare					
239	Ft. 17	-173361.55	9910.33	-3276.17	-303.26
	$\sigma_{s,c}$15	-186964.98	10088.23	-3572.14	-892.93
	$\sigma_{cls,Max}$15	-186964.98	10088.23	-3572.14	-65.40
	$\sigma_{cls,Med}$15	-186964.98	10088.23	-3572.14	-40.95
339	Ft. 17	-169911.55	-26478.98	4955.29	43.91
	$\sigma_{s,c}$15	-183514.98	-27369.78	5640.94	-1236.25
	$\sigma_{cls,Max}$15	-183514.98	-27369.78	5640.94	-93.89
	$\sigma_{cls,Med}$15	-183514.98	-27369.78	5640.94	-41.72
Combinazioni Frequenti					
239	Ft. 20	-173585.33	9672.47	-3204.75	-310.16
	$\sigma_{s,c}$18	-183120.13	9669.96	-3442.04	-869.32
	$\sigma_{cls,Max}$18	-183120.13	9669.96	-3442.04	-63.60
	$\sigma_{cls,Med}$18	-183120.13	9669.96	-3442.04	-40.11
339	Ft. 20	-170135.33	-26362.97	5039.48	44.04
	$\sigma_{s,c}$18	-179670.13	-26712.07	5545.39	-1209.64
	$\sigma_{cls,Max}$18	-179670.13	-26712.07	5545.39	-91.89
	$\sigma_{cls,Med}$18	-179670.13	-26712.07	5545.39	-40.84
Combinazioni Quasi Permanenti					
239	Ft. 22	-173659.91	9593.18	-3180.94	-312.45
	$\sigma_{s,c}$21	-181844.75	9529.69	-3399.53	-861.48
	$\sigma_{cls,Max}$21	-181844.75	9529.69	-3399.53	-63.01
	$\sigma_{cls,Med}$21	-181844.75	9529.69	-3399.53	-39.83
339	Ft. 22	-170209.91	-26324.30	5067.54	44.08
	$\sigma_{s,c}$21	-178394.75	-26488.24	5515.23	-1200.76
	$\sigma_{cls,Max}$21	-178394.75	-26488.24	5515.23	-91.22
	$\sigma_{cls,Med}$21	-178394.75	-26488.24	5515.23	-40.55

Pilastro: **40/2576** / L 0.85[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 85.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
40	1	-235958.97	-15448.76	5989.47	0.34
2576	1	-234528.97	-6028.46	4753.75	0.31

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	0.98	9430.58	86297.23	1313.10	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
40	Ft. 16	-158756.64	-10677.58	4034.84	-218.59
	$\sigma_{s,c}$15	-163429.91	-10963.92	4164.08	-848.76
	$\sigma_{cls,Max}$15	-163429.91	-10963.92	4164.08	-63.29
	$\sigma_{cls,Med}$15	-163429.91	-10963.92	4164.08	-35.80
2576	Ft. 16	-157656.64	-4403.66	3157.77	-345.50
	$\sigma_{s,c}$15	-162329.91	-4510.47	3276.05	-711.33
	$\sigma_{cls,Max}$15	-162329.91	-4510.47	3276.05	-51.96
	$\sigma_{cls,Med}$15	-162329.91	-4510.47	3276.05	-35.56
Combinazioni Frequenti					
40	Ft. 19	-157201.41	-10569.83	3989.75	-216.67
	$\sigma_{s,c}$18	-158759.23	-10664.85	4032.76	-824.34
	$\sigma_{cls,Max}$18	-158759.23	-10664.85	4032.76	-61.45
	$\sigma_{cls,Med}$18	-158759.23	-10664.85	4032.76	-34.77
2576	Ft. 19	-156101.41	-4345.69	3119.23	-342.56
	$\sigma_{s,c}$18	-157659.23	-4380.52	3158.69	-690.13
	$\sigma_{cls,Max}$18	-157659.23	-4380.52	3158.69	-50.39
	$\sigma_{cls,Med}$18	-157659.23	-4380.52	3158.69	-34.53
Combinazioni Quasi Permanenti					
40	Ft. 21	-157201.92	-10567.28	3989.33	-216.73
	$\sigma_{s,c}$21	-157201.92	-10567.28	3989.33	-816.25
	$\sigma_{cls,Max}$21	-157201.92	-10567.28	3989.33	-60.85
	$\sigma_{cls,Med}$22	-157782.36	-10359.12	3974.42	-34.56
2576	Ft. 21	-156101.92	-4341.06	3119.42	-342.63
	$\sigma_{s,c}$22	-156682.36	-4153.58	3162.52	-683.33
	$\sigma_{cls,Max}$22	-156682.36	-4153.58	3162.52	-49.90
	$\sigma_{cls,Med}$22	-156682.36	-4153.58	3162.52	-34.32

Pilastro: **2576/140** / L 3.00[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 100.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
2576	1	-439374.25	22030.31	-2997.15	0.58
140	1	-435149.25	-16814.84	-4353.34	0.56

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	13793.43	86297.23	783.38	61956.98	ø 10 2br.x4br./15.0
1.13	2.13	13793.43	64722.92	783.38	46467.73	ø 10 2br.x4br./20.0
2.13	3.13	13793.43	86297.23	783.38	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
2576	Ft. 16	-294971.09	14286.09	-2126.04	-667.82
	$\sigma_{s,c}$15	-303639.94	14753.80	-2092.62	-1305.51
	$\sigma_{cls,Max}$15	-303639.94	14753.80	-2092.62	-92.04

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-303639.94	14753.80	-2092.62	-66.51
140	Ft. 17	-296208.72	-11377.85	-3202.88	-685.20
	$\sigma_{s,c}$15	-300389.94	-11180.27	-3065.23	-1267.33
	$\sigma_{cls,Max}$15	-300389.94	-11180.27	-3065.23	-89.97
	$\sigma_{cls,Med}$15	-300389.94	-11180.27	-3065.23	-65.80
Combinazioni Frequenti					
2576	Ft. 19	-292106.94	14159.83	-2137.95	-660.10
	$\sigma_{s,c}$20	-295242.53	14632.02	-2037.34	-1274.17
	$\sigma_{cls,Max}$20	-295242.53	14632.02	-2037.34	-89.87
	$\sigma_{cls,Med}$20	-295242.53	14632.02	-2037.34	-64.67
140	Ft. 20	-291992.53	-11015.45	-2958.57	-685.05
	$\sigma_{s,c}$20	-291992.53	-11015.45	-2958.57	-1233.65
	$\sigma_{cls,Max}$20	-291992.53	-11015.45	-2958.57	-87.58
	$\sigma_{cls,Med}$20	-291992.53	-11015.45	-2958.57	-63.96
Combinazioni Quasi Permanenti					
2576	Ft. 21	-292112.22	14165.97	-2138.11	-660.01
	$\sigma_{s,c}$22	-293837.13	14517.92	-2072.72	-1268.82
	$\sigma_{cls,Max}$22	-293837.13	14517.92	-2072.72	-89.53
	$\sigma_{cls,Med}$22	-293837.13	14517.92	-2072.72	-64.36
140	Ft. 22	-290587.13	-10894.66	-2877.14	-685.00
	$\sigma_{s,c}$22	-290587.13	-10894.66	-2877.14	-1224.46
	$\sigma_{cls,Max}$22	-290587.13	-10894.66	-2877.14	-86.85
	$\sigma_{cls,Med}$22	-290587.13	-10894.66	-2877.14	-63.65

Pilastro: **140/240** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
140	1	-377928.50	-5879.01	9405.66	0.51
240	1	-373443.53	789.79	-7321.03	0.49

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2043.53	86297.23	4866.44	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	2043.53	64722.92	4866.44	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	2043.53	86297.23	4866.44	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
140	Ft. 17	-255709.17	-3676.59	6710.28	-566.53
	$\sigma_{s,c}$15	-259843.77	-3586.04	6675.02	-1124.73
	$\sigma_{cls,Max}$15	-259843.77	-3586.04	6675.02	-83.24
	$\sigma_{cls,Med}$15	-259843.77	-3586.04	6675.02	-56.91
240	Ft. 17	-252259.19	448.07	-5236.48	-654.89
	$\sigma_{s,c}$15	-256393.78	284.36	-5230.07	-1013.42
	$\sigma_{cls,Max}$15	-256393.78	284.36	-5230.07	-73.58
	$\sigma_{cls,Med}$15	-256393.78	284.36	-5230.07	-56.16
Combinazioni Frequenti					
140	Ft. 19	-251208.39	-3420.17	6198.65	-572.21

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$20	-253686.75	-3602.87	6355.76	-1094.62
	$\sigma_{cls,Max}$20	-253686.75	-3602.87	6355.76	-80.87
	$\sigma_{cls,Med}$20	-253686.75	-3602.87	6355.76	-55.57
240	Ft. 19	-247758.41	222.13	-4780.98	-658.29
	$\sigma_{s,c}$20	-250236.77	510.40	-4861.35	-985.16
	$\sigma_{cls,Max}$20	-250236.77	510.40	-4861.35	-71.32
	$\sigma_{cls,Med}$20	-250236.77	510.40	-4861.35	-54.81
Combinazioni Quasi Permanenti					
140	Ft. 21	-251213.14	-3419.60	6198.61	-572.24
	$\sigma_{s,c}$22	-253012.63	-3578.30	6237.58	-1088.24
	$\sigma_{cls,Max}$22	-253012.63	-3578.30	6237.58	-80.31
	$\sigma_{cls,Med}$22	-253012.63	-3578.30	6237.58	-55.42
240	Ft. 21	-247763.16	220.97	-4781.04	-658.32
	$\sigma_{s,c}$22	-249562.64	531.18	-4736.31	-979.30
	$\sigma_{cls,Max}$22	-249562.64	531.18	-4736.31	-70.79
	$\sigma_{cls,Med}$22	-249562.64	531.18	-4736.31	-54.66

Pilastro: **240/340** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
240	1	-315278.81	11166.03	9895.89	0.45
340	3	-304904.28	-32410.68	-17418.28	0.57

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	12754.12	86297.23	8062.96	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	12754.12	64722.92	8062.96	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	12754.12	86297.23	8062.96	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
240	Ft. 17	-211231.34	7827.03	7253.56	-335.23
	$\sigma_{s,c}$17	-211231.34	7827.03	7253.56	-1052.78
	$\sigma_{cls,Max}$17	-211231.34	7827.03	7253.56	-79.86
	$\sigma_{cls,Med}$15	-215157.72	7543.69	6918.20	-47.13
340	Ft. 17	-207781.34	-22065.25	-11957.73	88.81
	$\sigma_{s,c}$17	-207781.34	-22065.25	-11957.73	-1441.09
	$\sigma_{cls,Max}$17	-207781.34	-22065.25	-11957.73	-114.17
	$\sigma_{cls,Med}$17	-207781.34	-22065.25	-11957.73	-48.59
Combinazioni Frequenti					
240	Ft. 20	-211472.03	7658.71	7005.50	-346.66
	$\sigma_{s,c}$20	-211472.03	7658.71	7005.50	-1042.93
	$\sigma_{cls,Max}$20	-211472.03	7658.71	7005.50	-78.89
	$\sigma_{cls,Med}$20	-211472.03	7658.71	7005.50	-46.32
340	Ft. 20	-208022.03	-22002.32	-11841.61	81.39
	$\sigma_{s,c}$20	-208022.03	-22002.32	-11841.61	-1436.13
	$\sigma_{cls,Max}$20	-208022.03	-22002.32	-11841.61	-113.66
	$\sigma_{cls,Med}$20	-208022.03	-22002.32	-11841.61	-48.51

Combinazioni Quasi Permanenti					
240	Ft. 22	-211552.27	7602.60	6922.82	-350.47
	$\sigma_{s,c}$22	-211552.27	7602.60	6922.82	-1039.65
	$\sigma_{cls,Max}$22	-211552.27	7602.60	6922.82	-78.56
	$\sigma_{cls,Med}$22	-211552.27	7602.60	6922.82	-46.34
340	Ft. 22	-208102.27	-21981.34	-11802.91	78.93
	$\sigma_{s,c}$22	-208102.27	-21981.34	-11802.91	-1434.48
	$\sigma_{cls,Max}$22	-208102.27	-21981.34	-11802.91	-113.49
	$\sigma_{cls,Med}$22	-208102.27	-21981.34	-11802.91	-48.49

Pilastro: **41/141** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 20 ø 20 Af=62.83 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 7f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
41	1	-261622.19	2853.80	254.69	0.28
141	1	-255967.19	-6363.34	5690.74	0.31

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	3671.00	86297.23	1659.23	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	3671.00	64722.92	1659.23	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	3671.00	86297.23	1659.23	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
41	Ft. 17	-178352.48	1723.32	84.13	-512.15
	$\sigma_{s,c}$15	-184161.09	1385.10	142.86	-584.50
	$\sigma_{cls,Max}$15	-184161.09	1385.10	142.86	-39.35
	$\sigma_{cls,Med}$15	-184161.09	1385.10	142.86	-37.26
141	Ft. 17	-174002.48	-4123.00	4078.24	-346.65
	$\sigma_{s,c}$15	-179811.09	-3998.41	4038.96	-724.08
	$\sigma_{cls,Max}$15	-179811.09	-3998.41	4038.96	-53.12
	$\sigma_{cls,Med}$15	-179811.09	-3998.41	4038.96	-36.38
Combinazioni Frequenti					
41	Ft. 20	-175657.73	1532.41	117.99	-505.95
	$\sigma_{s,c}$18	-178089.17	1250.55	173.07	-564.86
	$\sigma_{cls,Max}$18	-178089.17	1250.55	173.07	-38.05
	$\sigma_{cls,Med}$18	-178089.17	1250.55	173.07	-36.03
141	Ft. 20	-171307.73	-3953.66	3885.65	-346.65
	$\sigma_{s,c}$18	-173739.17	-3812.74	3829.26	-696.73
	$\sigma_{cls,Max}$18	-173739.17	-3812.74	3829.26	-51.05
	$\sigma_{cls,Med}$18	-173739.17	-3812.74	3829.26	-35.15
Combinazioni Quasi Permanenti					
41	Ft. 22	-174759.48	1468.77	129.28	-503.89
	$\sigma_{s,c}$21	-176081.50	1203.43	183.28	-558.33
	$\sigma_{cls,Max}$21	-176081.50	1203.43	183.28	-37.61
	$\sigma_{cls,Med}$21	-176081.50	1203.43	183.28	-35.63
141	Ft. 22	-170409.48	-3897.21	3821.45	-346.65
	$\sigma_{s,c}$22	-170409.48	-3897.21	3821.45	-687.71
	$\sigma_{cls,Max}$22	-170409.48	-3897.21	3821.45	-50.46
	$\sigma_{cls,Med}$21	-171731.50	-3751.15	3759.35	-34.75

Pilastro: **141/241** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 20 ø 20 Af=62.83 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 7f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
141	1	-216566.53	-3003.36	-12693.77	0.32
241	1	-212081.53	-1378.59	8457.30	0.28

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	606.48	86297.23	6130.74	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	606.48	64722.92	6130.74	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	606.48	86297.23	6130.74	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
141	Ft. 17	-145969.38	-1772.17	-8909.38	-158.79
	$\sigma_{s,c}$15	-151792.61	-1681.45	-8911.65	-743.55
	$\sigma_{cls,Max}$15	-151792.61	-1681.45	-8911.65	-59.07
	$\sigma_{cls,Med}$15	-151792.61	-1681.45	-8911.65	-30.71
241	Ft. 17	-142519.38	-1066.53	5985.50	-243.52
	$\sigma_{s,c}$15	-148342.61	-1120.51	6036.58	-641.53
	$\sigma_{cls,Max}$15	-148342.61	-1120.51	6036.58	-49.20
	$\sigma_{cls,Med}$15	-148342.61	-1120.51	6036.58	-30.01
Combinazioni Frequenti					
141	Ft. 20	-144691.31	-1719.45	-8379.29	-171.01
	$\sigma_{s,c}$18	-147119.31	-1616.08	-8389.57	-713.31
	$\sigma_{cls,Max}$18	-147119.31	-1616.08	-8389.57	-56.50
	$\sigma_{cls,Med}$18	-147119.31	-1616.08	-8389.57	-29.77
241	Ft. 20	-141241.31	-1047.01	5432.51	-255.88
	$\sigma_{s,c}$18	-143669.31	-1180.85	5546.40	-614.16
	$\sigma_{cls,Max}$18	-143669.31	-1180.85	5546.40	-46.88
	$\sigma_{cls,Med}$18	-143669.31	-1180.85	5546.40	-29.07
Combinazioni Quasi Permanenti					
141	Ft. 22	-144265.30	-1701.87	-8202.60	-175.08
	$\sigma_{s,c}$21	-145577.23	-1595.26	-8215.43	-703.29
	$\sigma_{cls,Max}$21	-145577.23	-1595.26	-8215.43	-55.65
	$\sigma_{cls,Med}$21	-145577.23	-1595.26	-8215.43	-29.45
241	Ft. 21	-142127.23	-1200.02	5382.88	-257.62
	$\sigma_{s,c}$21	-142127.23	-1200.02	5382.88	-605.06
	$\sigma_{cls,Max}$21	-142127.23	-1200.02	5382.88	-46.11
	$\sigma_{cls,Med}$21	-142127.23	-1200.02	5382.88	-28.76

Pilastro: **241/341** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 20 ø 20 Af=62.83 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 7f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
241	1	-176386.48	1977.39	-21424.44	0.39
341	3	-163054.36	-2687.75	37085.98	0.60

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3418.15	86297.23	17002.81	61956.98	ø 10 2br.x4br./15.0
1.13	2.33	3417.94	64722.92	17011.53	46467.73	ø 10 2br.x4br./20.0
2.33	3.33	3417.69	86297.23	17018.80	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
241	Ft. 17	-116957.84	1288.56	-14876.74	279.01
	$\sigma_{s,c}$15	-122855.94	1224.86	-14766.58	-853.28
	$\sigma_{cls,Max}$17	-116957.84	1288.56	-14876.74	-75.86
	$\sigma_{cls,Med}$17	-116957.84	1288.56	-14876.74	-36.89
341	Ft. 17	-113507.84	-1748.10	25322.35	1378.48
	$\sigma_{s,c}$15	-119405.94	-1577.01	24981.27	-1222.20
	$\sigma_{cls,Max}$17	-113507.84	-1748.10	25322.35	-126.99
	$\sigma_{cls,Med}$17	-113507.84	-1748.10	25322.35	-61.71
Combinazioni Frequenti					
241	Ft. 20	-117014.31	1202.57	-14543.26	250.12
	$\sigma_{s,c}$20	-117014.31	1202.57	-14543.26	-831.28
	$\sigma_{cls,Max}$20	-117014.31	1202.57	-14543.26	-74.20
	$\sigma_{cls,Med}$20	-117014.31	1202.57	-14543.26	-36.14
341	Ft. 20	-113564.31	-1642.50	25265.57	1368.57
	$\sigma_{s,c}$20	-113564.31	-1642.50	25265.57	-1217.56
	$\sigma_{cls,Max}$20	-113564.31	-1642.50	25265.57	-126.50
	$\sigma_{cls,Med}$20	-113564.31	-1642.50	25265.57	-61.57
Combinazioni Quasi Permanenti					
241	Ft. 22	-117033.14	1173.91	-14432.10	240.67
	$\sigma_{s,c}$22	-117033.14	1173.91	-14432.10	-826.59
	$\sigma_{cls,Max}$22	-117033.14	1173.91	-14432.10	-73.65
	$\sigma_{cls,Med}$22	-117033.14	1173.91	-14432.10	-35.89
341	Ft. 22	-113583.14	-1607.30	25246.65	1365.27
	$\sigma_{s,c}$22	-113583.14	-1607.30	25246.65	-1216.04
	$\sigma_{cls,Max}$22	-113583.14	-1607.30	25246.65	-126.33
	$\sigma_{cls,Med}$22	-113583.14	-1607.30	25246.65	-61.53

Pilastro: **42/142** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
42	1	-542401.81	5838.91	1388.11	0.64
142	1	-536746.81	1785.19	682.46	0.62

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2947.86	86297.23	533.35	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	2947.86	64722.92	533.35	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	2947.86	86297.23	533.35	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
42	Ft. 16	-365336.81	4231.14	894.94	-1102.64
	$\sigma_{s,c}$15	-376487.81	4237.67	948.65	-1336.45

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Max}$15	-376487.81	4237.67	948.65	-90.93
	$\sigma_{cls,Med}$15	-376487.81	4237.67	948.65	-82.46
142	Ft. 16	-360986.81	1121.53	495.73	-1151.91
	$\sigma_{s,c}$15	-372137.81	1245.94	509.02	-1259.24
	$\sigma_{cls,Max}$15	-372137.81	1245.94	509.02	-84.75
	$\sigma_{cls,Med}$15	-372137.81	1245.94	509.02	-81.51
Combinazioni Frequenti					
42	Ft. 19	-361590.16	4236.25	878.50	-1090.77
	$\sigma_{s,c}$18	-365306.06	4238.68	896.46	-1298.07
	$\sigma_{cls,Max}$18	-365306.06	4238.68	896.46	-88.31
	$\sigma_{cls,Med}$18	-365306.06	4238.68	896.46	-80.01
142	Ft. 19	-357240.16	1078.08	489.22	-1140.52
	$\sigma_{s,c}$18	-360956.06	1119.48	493.58	-1219.94
	$\sigma_{cls,Max}$18	-360956.06	1119.48	493.58	-82.09
	$\sigma_{cls,Med}$18	-360956.06	1119.48	493.58	-79.06
Combinazioni Quasi Permanenti					
42	Ft. 21	-361584.00	4237.75	878.81	-1090.72
	$\sigma_{s,c}$21	-361584.00	4237.75	878.81	-1285.27
	$\sigma_{cls,Max}$21	-361584.00	4237.75	878.81	-87.44
	$\sigma_{cls,Med}$22	-361742.09	4007.51	907.06	-79.23
142	Ft. 21	-357234.00	1077.66	488.79	-1140.52
	$\sigma_{s,c}$21	-357234.00	1077.66	488.79	-1206.88
	$\sigma_{cls,Max}$21	-357234.00	1077.66	488.79	-81.21
	$\sigma_{cls,Med}$22	-357392.09	1193.71	409.99	-78.28

Pilastro: **142/242** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
142	1	-461438.41	-10697.59	-2709.86	0.57
242	1	-456953.41	4167.85	2189.25	0.54

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4308.82	86297.23	1536.35	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	4308.82	64722.92	1536.35	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	4308.82	86297.23	1536.35	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
142	Ft. 17	-311272.97	-7318.17	-1989.84	-839.69
	$\sigma_{s,c}$15	-318556.50	-7428.08	-1964.01	-1230.60
	$\sigma_{cls,Max}$15	-318556.50	-7428.08	-1964.01	-85.60
	$\sigma_{cls,Med}$15	-318556.50	-7428.08	-1964.01	-69.77
242	Ft. 17	-307822.97	2536.02	1860.18	-910.70
	$\sigma_{s,c}$15	-315106.50	2923.43	1618.47	-1134.59
	$\sigma_{cls,Max}$15	-315106.50	2923.43	1618.47	-78.01
	$\sigma_{cls,Med}$15	-315106.50	2923.43	1618.47	-69.02
Combinazioni Frequenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
142	Ft. 19	-307556.31	-7013.04	-1818.28	-837.93
	$\sigma_{s,c}$18	-310298.66	-7116.41	-1853.66	-1194.86
	$\sigma_{cls,Max}$18	-310298.66	-7116.41	-1853.66	-83.04
	$\sigma_{cls,Med}$18	-310298.66	-7116.41	-1853.66	-67.97
242	Ft. 19	-304106.31	2611.28	1460.41	-909.98
	$\sigma_{s,c}$18	-306848.66	2688.88	1499.04	-1099.83
	$\sigma_{cls,Max}$18	-306848.66	2688.88	1499.04	-75.51
	$\sigma_{cls,Med}$18	-306848.66	2688.88	1499.04	-67.21
Combinazioni Quasi Permanenti					
142	Ft. 21	-307550.66	-7012.76	-1817.51	-837.94
	$\sigma_{s,c}$22	-307986.19	-6976.79	-1837.68	-1184.48
	$\sigma_{cls,Max}$22	-307986.19	-6976.79	-1837.68	-82.30
	$\sigma_{cls,Med}$22	-307986.19	-6976.79	-1837.68	-67.46
242	Ft. 21	-304100.66	2610.96	1459.76	-909.98
	$\sigma_{s,c}$22	-304536.19	2173.48	1666.34	-1089.12
	$\sigma_{cls,Max}$22	-304536.19	2173.48	1666.34	-74.90
	$\sigma_{cls,Med}$22	-304536.19	2173.48	1666.34	-66.70

Pilastro: **242/342** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
242	1	-384415.38	-14282.04	-4852.21	0.50
342	1	-379930.38	47297.50	7896.79	0.62

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	18904.77	86297.23	3695.36	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	18904.77	64722.92	3695.36	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	18904.77	86297.23	3695.36	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
242	Ft. 17	-256283.61	-10307.95	-2917.11	-580.62
	$\sigma_{s,c}$15	-263359.13	-9890.70	-3432.48	-1136.25
	$\sigma_{cls,Max}$15	-263359.13	-9890.70	-3432.48	-81.43
	$\sigma_{cls,Med}$15	-263359.13	-9890.70	-3432.48	-57.68
342	Ft. 17	-252833.61	34337.95	3957.53	-143.12
	$\sigma_{s,c}$15	-259909.11	32327.26	5492.50	-1557.46
	$\sigma_{cls,Max}$15	-259909.11	32327.26	5492.50	-115.84
	$\sigma_{cls,Med}$15	-259909.11	32327.26	5492.50	-56.97
Combinazioni Frequenti					
242	Ft. 19	-256285.56	-9455.26	-3270.90	-583.32
	$\sigma_{s,c}$18	-258047.25	-9563.59	-3309.76	-1109.54
	$\sigma_{cls,Max}$18	-258047.25	-9563.59	-3309.76	-79.45
	$\sigma_{cls,Med}$18	-258047.25	-9563.59	-3309.76	-56.52
342	Ft. 20	-253416.30	34102.54	3991.96	-147.79
	$\sigma_{s,c}$18	-254597.25	31365.23	5386.91	-1520.91
	$\sigma_{cls,Max}$18	-254597.25	31365.23	5386.91	-113.11

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$18	-254597.25	31365.23	5386.91	-55.79
Combinazioni Quasi Permanenti					
242	Ft. 21	-256280.70	-9454.87	-3269.78	-583.34
	$\sigma_{s,c}$21	-256280.70	-9454.87	-3269.78	-1100.69
	$\sigma_{cls,Max}$21	-256280.70	-9454.87	-3269.78	-78.79
	$\sigma_{cls,Med}$22	-257060.53	-10094.62	-2813.29	-56.31
342	Ft. 22	-253610.53	34024.07	4003.44	-149.35
	$\sigma_{s,c}$22	-253610.53	34024.07	4003.44	-1517.13
	$\sigma_{cls,Max}$21	-252830.70	31046.04	5353.39	-112.21
	$\sigma_{cls,Med}$22	-253610.53	34024.07	4003.44	-55.55

Pilastro: **43/143** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
43	1	-510281.50	12035.80	382.84	0.62
143	1	-504626.50	-1225.27	-730.07	0.58

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5064.98	86297.23	345.17	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	5064.98	64722.92	345.17	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	5064.98	86297.23	345.17	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
43	Ft. 16	-343562.91	8474.64	203.24	-983.70
	$\sigma_{s,c}$15	-354128.88	8535.70	238.56	-1310.71
	$\sigma_{cls,Max}$15	-354128.88	8535.70	238.56	-89.17
	$\sigma_{cls,Med}$15	-354128.88	8535.70	238.56	-77.57
143	Ft. 16	-339212.91	-826.97	-457.18	-1086.42
	$\sigma_{s,c}$15	-349778.88	-725.79	-489.14	-1176.64
	$\sigma_{cls,Max}$15	-349778.88	-725.79	-489.14	-79.13
	$\sigma_{cls,Med}$15	-349778.88	-725.79	-489.14	-76.61
Combinazioni Frequenti					
43	Ft. 19	-340052.97	8458.68	191.40	-972.80
	$\sigma_{s,c}$18	-343575.41	8479.19	203.17	-1273.98
	$\sigma_{cls,Max}$18	-343575.41	8479.19	203.17	-86.67
	$\sigma_{cls,Med}$18	-343575.41	8479.19	203.17	-75.25
143	Ft. 19	-335702.97	-860.36	-446.36	-1074.69
	$\sigma_{s,c}$18	-339225.41	-826.62	-457.00	-1142.59
	$\sigma_{cls,Max}$18	-339225.41	-826.62	-457.00	-76.84
	$\sigma_{cls,Med}$18	-339225.41	-826.62	-457.00	-74.30
Combinazioni Quasi Permanenti					
43	Ft. 21	-340055.47	8459.59	191.38	-972.80
	$\sigma_{s,c}$21	-340055.47	8459.59	191.38	-1261.72
	$\sigma_{cls,Max}$21	-340055.47	8459.59	191.38	-85.84
	$\sigma_{cls,Med}$22	-341152.31	8141.30	155.13	-74.72
143	Ft. 21	-335705.47	-860.29	-446.32	-1074.70

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$21	-335705.47	-860.29	-446.32	-1131.24
	$\sigma_{cls,Max}$21	-335705.47	-860.29	-446.32	-76.08
	$\sigma_{cls,Med}$22	-336802.31	-643.37	-374.09	-73.77

Pilastro: **143/243** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
143	1	-430411.75	-17790.05	274.55	0.55
243	1	-425926.75	7926.53	418.55	0.51

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	7454.08	86297.23	165.80	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	7454.08	64722.92	165.80	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	7454.08	86297.23	165.80	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
143	Ft. 16	-289278.16	-11700.00	198.75	-752.73
	$\sigma_{s,c}$15	-297053.72	-12239.55	208.91	-1182.82
	$\sigma_{cls,Max}$15	-297053.72	-12239.55	208.91	-81.27
	$\sigma_{cls,Med}$15	-297053.72	-12239.55	208.91	-65.07
243	Ft. 16	-285828.16	5072.75	267.07	-847.62
	$\sigma_{s,c}$15	-293603.72	5469.58	268.76	-1062.66
	$\sigma_{cls,Max}$15	-293603.72	5469.58	268.76	-72.12
	$\sigma_{cls,Med}$15	-293603.72	5469.58	268.76	-64.31
Combinazioni Frequenti					
143	Ft. 19	-286696.94	-11517.68	195.68	-747.33
	$\sigma_{s,c}$18	-289289.13	-11697.44	199.08	-1148.13
	$\sigma_{cls,Max}$18	-289289.13	-11697.44	199.08	-78.85
	$\sigma_{cls,Med}$18	-289289.13	-11697.44	199.08	-63.36
243	Ft. 19	-283246.94	4938.02	266.13	-841.38
	$\sigma_{s,c}$18	-285839.13	5070.21	266.68	-1030.55
	$\sigma_{cls,Max}$18	-285839.13	5070.21	266.68	-69.91
	$\sigma_{cls,Med}$18	-285839.13	5070.21	266.68	-62.61
Combinazioni Quasi Permanenti					
143	Ft. 21	-286699.13	-11517.17	195.75	-747.34
	$\sigma_{s,c}$22	-288154.47	-11418.82	212.80	-1140.29
	$\sigma_{cls,Max}$22	-288154.47	-11418.82	212.80	-78.29
	$\sigma_{cls,Med}$22	-288154.47	-11418.82	212.80	-63.12
243	Ft. 21	-283249.13	4937.51	266.05	-841.39
	$\sigma_{s,c}$21	-283249.13	4937.51	266.05	-1019.85
	$\sigma_{cls,Max}$21	-283249.13	4937.51	266.05	-69.17
	$\sigma_{cls,Med}$22	-284704.47	4463.72	89.26	-62.36

Pilastro: **243/343** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
243	1	-362658.63	-17937.52	633.27	0.47
343	1	-358173.63	61207.48	-2405.59	0.63

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	23719.14	86297.23	880.83	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	23719.14	64722.92	880.83	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	23719.14	86297.23	880.83	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
243	Ft. 17	-243074.44	-12808.16	43.69	-587.73
	$\sigma_{s,c}$15	-248427.00	-12444.03	429.62	-1033.43
	$\sigma_{cls,Max}$15	-248427.00	-12444.03	429.62	-71.59
	$\sigma_{cls,Med}$15	-248427.00	-12444.03	429.62	-54.41
343	Ft. 17	-239624.44	43132.64	-482.28	-64.87
	$\sigma_{s,c}$15	-244977.00	41706.09	-1638.94	-1539.77
	$\sigma_{cls,Max}$15	-244977.00	41706.09	-1638.94	-111.94
	$\sigma_{cls,Med}$15	-244977.00	41706.09	-1638.94	-54.18
Combinazioni Frequenti					
243	Ft. 19	-241503.73	-11901.42	385.05	-586.54
	$\sigma_{s,c}$18	-243237.22	-12037.19	396.11	-1008.65
	$\sigma_{cls,Max}$18	-243237.22	-12037.19	396.11	-69.83
	$\sigma_{cls,Med}$20	-243242.20	-12582.02	14.23	-53.28
343	Ft. 20	-239792.20	42777.67	-430.78	-73.42
	$\sigma_{s,c}$20	-239792.20	42777.67	-430.78	-1501.80
	$\sigma_{cls,Max}$18	-239787.22	40477.52	-1559.97	-108.97
	$\sigma_{cls,Med}$20	-239792.20	42777.67	-430.78	-53.40
Combinazioni Quasi Permanenti					
243	Ft. 21	-241505.67	-11901.50	384.99	-586.55
	$\sigma_{s,c}$22	-243298.13	-12506.64	4.41	-1004.07
	$\sigma_{cls,Max}$21	-241505.67	-11901.50	384.99	-69.25
	$\sigma_{cls,Med}$22	-243298.13	-12506.64	4.41	-53.29
343	Ft. 22	-239848.13	42659.36	-413.62	-76.24
	$\sigma_{s,c}$22	-239848.13	42659.36	-413.62	-1499.42
	$\sigma_{cls,Max}$22	-239848.13	42659.36	-413.62	-108.02
	$\sigma_{cls,Med}$22	-239848.13	42659.36	-413.62	-53.33

Pilastro: **44/144** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
44	1	-535604.00	12544.57	795.16	0.65
144	1	-529948.94	-5305.34	-684.85	0.62

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	6116.35	86297.23	438.27	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	6116.35	64722.92	438.27	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	6116.35	86297.23	438.27	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
44	Ft. 17	-354991.69	8680.72	527.75	-1007.55
	$\sigma_{s,c}$15	-371718.72	8737.71	529.74	-1381.06
	$\sigma_{cls,Max}$15	-371718.72	8737.71	529.74	-94.23
	$\sigma_{cls,Med}$15	-371718.72	8737.71	529.74	-81.42
144	Ft. 17	-350641.69	-3235.71	-460.06	-1084.48
	$\sigma_{s,c}$15	-367368.72	-3372.28	-463.21	-1276.89
	$\sigma_{cls,Max}$15	-367368.72	-3372.28	-463.21	-86.25
	$\sigma_{cls,Med}$15	-367368.72	-3372.28	-463.21	-80.47
Combinazioni Frequenti					
44	Ft. 20	-349374.94	8657.75	482.97	-990.90
	$\sigma_{s,c}$18	-360568.03	8680.25	484.66	-1342.05
	$\sigma_{cls,Max}$18	-360568.03	8680.25	484.66	-91.56
	$\sigma_{cls,Med}$18	-360568.03	8680.25	484.66	-78.98
144	Ft. 20	-345024.94	-3261.50	-425.60	-1066.70
	$\sigma_{s,c}$18	-356218.03	-3347.09	-427.86	-1238.72
	$\sigma_{cls,Max}$18	-356218.03	-3347.09	-427.86	-83.66
	$\sigma_{cls,Med}$18	-356218.03	-3347.09	-427.86	-78.02
Combinazioni Quasi Permanenti					
44	Ft. 22	-347502.69	8650.09	468.04	-985.35
	$\sigma_{s,c}$21	-356850.66	8660.70	469.60	-1329.04
	$\sigma_{cls,Max}$21	-356850.66	8660.70	469.60	-90.68
	$\sigma_{cls,Med}$21	-356850.66	8660.70	469.60	-78.16
144	Ft. 22	-343152.69	-3270.10	-414.12	-1060.77
	$\sigma_{s,c}$21	-352500.66	-3339.01	-416.11	-1226.00
	$\sigma_{cls,Max}$21	-352500.66	-3339.01	-416.11	-82.80
	$\sigma_{cls,Med}$21	-352500.66	-3339.01	-416.11	-77.21

Pilastro: **144/244** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
144	1	-453326.75	-20577.61	280.53	0.58
244	1	-448841.75	12137.27	-255.57	0.55

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	9482.57	86297.23	243.45	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	9482.57	64722.92	243.45	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	9482.57	86297.23	243.45	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
144	Ft. 17	-295931.03	-13693.76	199.15	-741.96

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-312913.47	-13971.16	209.82	-1263.29
	$\sigma_{cls,Max}$15	-312913.47	-13971.16	209.82	-86.94
	$\sigma_{cls,Med}$15	-312913.47	-13971.16	209.82	-68.54
244	Ft. 17	-292481.03	8153.67	-180.92	-821.83
	$\sigma_{s,c}$15	-309463.47	8232.52	-190.01	-1157.45
	$\sigma_{cls,Max}$15	-309463.47	8232.52	-190.01	-78.84
	$\sigma_{cls,Med}$15	-309463.47	8232.52	-190.01	-67.78
Combinazioni Frequenti					
144	Ft. 20	-293155.75	-13145.21	181.80	-742.37
	$\sigma_{s,c}$18	-304598.66	-13303.68	194.94	-1224.58
	$\sigma_{cls,Max}$18	-304598.66	-13303.68	194.94	-84.22
	$\sigma_{cls,Med}$18	-304598.66	-13303.68	194.94	-66.72
244	Ft. 20	-289705.75	7617.69	-164.91	-821.99
	$\sigma_{s,c}$18	-301148.66	7639.99	-178.05	-1120.06
	$\sigma_{cls,Max}$18	-301148.66	7639.99	-178.05	-76.23
	$\sigma_{cls,Med}$18	-301148.66	7639.99	-178.05	-65.96
Combinazioni Quasi Permanenti					
144	Ft. 22	-292230.63	-12962.36	176.02	-742.50
	$\sigma_{s,c}$21	-301826.72	-13082.00	190.04	-1211.69
	$\sigma_{cls,Max}$21	-301826.72	-13082.00	190.04	-83.32
	$\sigma_{cls,Med}$21	-301826.72	-13082.00	190.04	-66.11
244	Ft. 22	-288780.63	7439.03	-159.57	-822.04
	$\sigma_{s,c}$21	-298376.72	7443.20	-174.11	-1107.61
	$\sigma_{cls,Max}$21	-298376.72	7443.20	-174.11	-75.36
	$\sigma_{cls,Med}$21	-298376.72	7443.20	-174.11	-65.35

Pilastro: **244/344** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
244	1	-389153.50	-16404.42	559.66	0.50
344	1	-384668.50	56295.45	-1063.46	0.63

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	21072.43	86297.23	584.54	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	21072.43	64722.92	584.54	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	21072.43	86297.23	584.54	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
244	Ft. 17	-248823.91	-11057.18	356.61	-625.31
	$\sigma_{s,c}$15	-266666.84	-11494.45	387.02	-1076.47
	$\sigma_{cls,Max}$15	-266666.84	-11494.45	387.02	-74.25
	$\sigma_{cls,Med}$15	-266666.84	-11494.45	387.02	-58.41
344	Ft. 17	-245373.91	35896.71	-679.25	-197.41
	$\sigma_{s,c}$15	-263216.84	38363.37	-732.55	-1515.62
	$\sigma_{cls,Max}$15	-263216.84	38363.37	-732.55	-108.69
	$\sigma_{cls,Med}$15	-263216.84	38363.37	-732.55	-57.65

Combinazioni Frequenti					
244	Ft. 20	-248701.19	-10889.55	329.27	-628.52
	$\sigma_{s,c}$18	-260829.48	-11181.22	352.92	-1051.08
	$\sigma_{cls,Max}$18	-260829.48	-11181.22	352.92	-72.46
	$\sigma_{cls,Med}$18	-260829.48	-11181.22	352.92	-57.13
344	Ft. 20	-245251.19	35681.95	-636.39	-201.88
	$\sigma_{s,c}$18	-257379.48	37309.18	-674.48	-1477.35
	$\sigma_{cls,Max}$18	-257379.48	37309.18	-674.48	-105.88
	$\sigma_{cls,Med}$18	-257379.48	37309.18	-674.48	-56.38
Combinazioni Quasi Permanenti					
244	Ft. 22	-248660.28	-10833.67	320.16	-629.59
	$\sigma_{s,c}$21	-258883.53	-11076.60	341.67	-1042.62
	$\sigma_{cls,Max}$21	-258883.53	-11076.60	341.67	-71.86
	$\sigma_{cls,Med}$21	-258883.53	-11076.60	341.67	-56.70
344	Ft. 22	-245210.28	35610.37	-622.10	-203.37
	$\sigma_{s,c}$21	-255433.53	36958.71	-655.32	-1464.61
	$\sigma_{cls,Max}$21	-255433.53	36958.71	-655.32	-104.95
	$\sigma_{cls,Med}$21	-255433.53	36958.71	-655.32	-55.95

Pilastro: **45/145** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
45	1	-495233.84	14401.50	721.56	0.61
145	1	-489578.84	-7777.87	607.65	0.59

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	7635.61	86297.23	336.27	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	7635.61	64722.92	336.27	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	7635.61	86297.23	336.27	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
45	Ft. 16	-334185.16	9741.36	456.85	-924.10
	$\sigma_{s,c}$15	-344502.34	9841.83	491.41	-1308.49
	$\sigma_{cls,Max}$15	-344502.34	9841.83	491.41	-89.54
	$\sigma_{cls,Med}$15	-344502.34	9841.83	491.41	-75.46
145	Ft. 16	-329835.16	-4904.25	419.55	-990.11
	$\sigma_{s,c}$15	-340152.34	-5007.46	431.95	-1213.23
	$\sigma_{cls,Max}$15	-340152.34	-5007.46	431.95	-82.26
	$\sigma_{cls,Med}$15	-340152.34	-5007.46	431.95	-74.51
Combinazioni Frequenti					
45	Ft. 20	-330983.84	9913.09	481.76	-909.98
	$\sigma_{s,c}$18	-334122.53	9763.17	455.15	-1271.94
	$\sigma_{cls,Max}$18	-334122.53	9763.17	455.15	-87.05
	$\sigma_{cls,Med}$18	-334122.53	9763.17	455.15	-73.18
145	Ft. 19	-326335.59	-4876.42	417.10	-979.15
	$\sigma_{s,c}$18	-329772.53	-4911.05	421.28	-1177.21
	$\sigma_{cls,Max}$18	-329772.53	-4911.05	421.28	-79.83
	$\sigma_{cls,Med}$18	-329772.53	-4911.05	421.28	-72.23
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
45	Ft. 22	-329258.72	9881.56	473.29	-905.10
	$\sigma_{s,c}$21	-330673.06	9733.31	443.34	-1259.74
	$\sigma_{cls,Max}$21	-330673.06	9733.31	443.34	-86.22
	$\sigma_{cls,Med}$21	-330673.06	9733.31	443.34	-72.43
145	Ft. 22	-324908.72	-5031.53	341.99	-974.31
	$\sigma_{s,c}$21	-326323.06	-4877.78	417.44	-1165.21
	$\sigma_{cls,Max}$21	-326323.06	-4877.78	417.44	-79.02
	$\sigma_{cls,Med}$21	-326323.06	-4877.78	417.44	-71.48

Pilastro: **145/245** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
145	1	-416046.06	-17711.03	-2118.03	0.54
245	1	-411561.06	11117.39	1435.72	0.51

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	8406.76	86297.23	1130.28	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	8406.76	64722.92	1130.28	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	8406.76	86297.23	1130.28	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
145	Ft. 17	-279694.81	-11888.25	-1509.12	-676.48
	$\sigma_{s,c}$15	-287831.13	-11966.61	-1479.20	-1188.47
	$\sigma_{cls,Max}$15	-287831.13	-11966.61	-1479.20	-83.04
	$\sigma_{cls,Med}$15	-287831.13	-11966.61	-1479.20	-63.05
245	Ft. 17	-276244.81	7699.96	1219.05	-742.88
	$\sigma_{s,c}$15	-284381.13	7505.01	1018.49	-1089.50
	$\sigma_{cls,Max}$15	-284381.13	7505.01	1018.49	-75.13
	$\sigma_{cls,Med}$15	-284381.13	7505.01	1018.49	-62.29
Combinazioni Frequenti					
145	Ft. 20	-277216.69	-11391.46	-1440.19	-678.66
	$\sigma_{s,c}$18	-280160.31	-11365.68	-1410.26	-1151.24
	$\sigma_{cls,Max}$18	-280160.31	-11365.68	-1410.26	-80.38
	$\sigma_{cls,Med}$18	-280160.31	-11365.68	-1410.26	-61.36
245	Ft. 20	-273766.69	7221.05	1157.11	-744.54
	$\sigma_{s,c}$20	-273766.69	7221.05	1157.11	-1054.39
	$\sigma_{cls,Max}$20	-273766.69	7221.05	1157.11	-72.90
	$\sigma_{cls,Med}$18	-276710.31	6953.25	961.98	-60.61
Combinazioni Quasi Permanenti					
145	Ft. 22	-276390.69	-11225.86	-1417.22	-679.38
	$\sigma_{s,c}$21	-277612.84	-11166.63	-1386.99	-1138.88
	$\sigma_{cls,Max}$21	-277612.84	-11166.63	-1386.99	-79.49
	$\sigma_{cls,Med}$21	-277612.84	-11166.63	-1386.99	-60.81
245	Ft. 22	-272940.69	7061.41	1136.46	-745.10
	$\sigma_{s,c}$22	-272940.69	7061.41	1136.46	-1048.41
	$\sigma_{cls,Max}$22	-272940.69	7061.41	1136.46	-72.45

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-274162.84	6770.00	942.95	-60.05

Pilastro: **245/345** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
245	1	-356230.91	-10000.52	-3217.69	0.45
345	1	-351745.88	34014.40	5468.77	0.53

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	12757.95	86297.23	2517.82	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	12757.95	64722.92	2517.82	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	12757.95	86297.23	2517.82	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
245	Ft. 16	-239303.17	-6971.89	-2149.73	-603.81
	$\sigma_{s,c}$15	-244610.28	-7139.33	-2214.29	-990.89
	$\sigma_{cls,Max}$15	-244610.28	-7139.33	-2214.29	-69.86
	$\sigma_{cls,Med}$15	-244610.28	-7139.33	-2214.29	-53.58
345	Ft. 16	-235853.17	22693.07	3638.84	-287.95
	$\sigma_{s,c}$15	-241160.28	23333.89	3719.88	-1292.35
	$\sigma_{cls,Max}$15	-241160.28	23333.89	3719.88	-94.55
	$\sigma_{cls,Med}$15	-241160.28	23333.89	3719.88	-52.82
Combinazioni Frequenti					
245	Ft. 19	-237484.28	-6904.58	-2130.91	-599.53
	$\sigma_{s,c}$18	-239251.58	-6960.00	-2152.53	-968.39
	$\sigma_{cls,Max}$18	-239251.58	-6960.00	-2152.53	-68.25
	$\sigma_{cls,Med}$18	-239251.58	-6960.00	-2152.53	-52.40
345	Ft. 19	-234034.28	22432.11	3617.19	-286.93
	$\sigma_{s,c}$18	-235801.58	22644.08	3644.39	-1261.06
	$\sigma_{cls,Max}$18	-235801.58	22644.08	3644.39	-92.25
	$\sigma_{cls,Med}$18	-235801.58	22644.08	3644.39	-51.65
Combinazioni Quasi Permanenti					
245	Ft. 21	-237473.97	-6902.20	-2131.47	-599.52
	$\sigma_{s,c}$21	-237473.97	-6902.20	-2131.47	-960.93
	$\sigma_{cls,Max}$21	-237473.97	-6902.20	-2131.47	-67.72
	$\sigma_{cls,Med}$21	-237473.97	-6902.20	-2131.47	-52.02
345	Ft. 21	-234023.97	22422.31	3618.30	-287.02
	$\sigma_{s,c}$21	-234023.97	22422.31	3618.30	-1250.76
	$\sigma_{cls,Max}$21	-234023.97	22422.31	3618.30	-91.50
	$\sigma_{cls,Med}$21	-234023.97	22422.31	3618.30	-51.26

Pilastro: **46/146** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
46	1	-478094.47	15039.61	874.26	0.60

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
146	1	-472439.47	-8785.56	-1391.71	0.57

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	8013.46	86297.23	553.24	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	8013.46	64722.92	553.24	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	8013.46	86297.23	553.24	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
46	Ft. 16	-323095.34	10043.70	525.40	-880.54
	$\sigma_{s,c}$15	-332885.69	10208.69	572.09	-1278.89
	$\sigma_{cls,Max}$15	-332885.69	10208.69	572.09	-87.72
	$\sigma_{cls,Med}$15	-332885.69	10208.69	572.09	-72.91
146	Ft. 16	-318745.34	-5513.80	-895.16	-928.58
	$\sigma_{s,c}$15	-328535.69	-5670.05	-949.66	-1202.37
	$\sigma_{cls,Max}$15	-328535.69	-5670.05	-949.66	-82.25
	$\sigma_{cls,Med}$15	-328535.69	-5670.05	-949.66	-71.96
Combinazioni Frequenti					
46	Ft. 19	-319747.25	10014.90	511.46	-870.45
	$\sigma_{s,c}$20	-324919.84	10332.04	524.34	-1253.21
	$\sigma_{cls,Max}$20	-324919.84	10332.04	524.34	-85.98
	$\sigma_{cls,Med}$20	-324919.84	10332.04	524.34	-71.17
146	Ft. 19	-315397.25	-5470.47	-878.34	-918.82
	$\sigma_{s,c}$20	-320569.84	-5815.86	-866.92	-1175.95
	$\sigma_{cls,Max}$20	-320569.84	-5815.86	-866.92	-80.42
	$\sigma_{cls,Med}$20	-320569.84	-5815.86	-866.92	-70.22
Combinazioni Quasi Permanenti					
46	Ft. 21	-319729.75	10020.32	511.79	-870.29
	$\sigma_{s,c}$22	-323309.94	10268.46	506.92	-1246.33
	$\sigma_{cls,Max}$22	-323309.94	10268.46	506.92	-85.49
	$\sigma_{cls,Med}$22	-323309.94	10268.46	506.92	-70.82
146	Ft. 21	-315379.75	-5472.28	-878.62	-918.73
	$\sigma_{s,c}$22	-318959.94	-5772.70	-847.93	-1169.35
	$\sigma_{cls,Max}$22	-318959.94	-5772.70	-847.93	-79.95
	$\sigma_{cls,Med}$22	-318959.94	-5772.70	-847.93	-69.86

Pilastro: **146/246** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
146	1	-399983.34	-16804.93	1786.90	0.51
246	1	-395498.34	9840.64	-1436.30	0.49

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	7957.78	86297.23	1001.92	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	7957.78	64722.92	1001.92	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	7957.78	86297.23	1001.92	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
146	Ft. 16	-269802.56	-10750.06	1182.97	-672.97
	$\sigma_{s,c}$15	-276940.41	-11320.24	1251.35	-1134.87
	$\sigma_{cls,Max}$15	-276940.41	-11320.24	1251.35	-79.10
	$\sigma_{cls,Med}$15	-276940.41	-11320.24	1251.35	-60.66
246	Ft. 17	-270839.41	7091.05	-1139.28	-737.62
	$\sigma_{s,c}$17	-270839.41	7091.05	-1139.28	-1042.08
	$\sigma_{cls,Max}$17	-270839.41	7091.05	-1139.28	-72.03
	$\sigma_{cls,Med}$15	-273490.41	6632.99	-1011.80	-59.90
Combinazioni Frequenti					
146	Ft. 19	-267346.53	-10551.57	1160.97	-668.85
	$\sigma_{s,c}$20	-272103.72	-10911.66	1207.83	-1110.91
	$\sigma_{cls,Max}$20	-272103.72	-10911.66	1207.83	-77.38
	$\sigma_{cls,Med}$20	-272103.72	-10911.66	1207.83	-59.60
246	Ft. 20	-268653.72	6638.73	-1068.65	-740.08
	$\sigma_{s,c}$20	-268653.72	6638.73	-1068.65	-1025.25
	$\sigma_{cls,Max}$20	-268653.72	6638.73	-1068.65	-70.75
	$\sigma_{cls,Med}$20	-268653.72	6638.73	-1068.65	-58.84
Combinazioni Quasi Permanenti					
146	Ft. 21	-267330.66	-10549.83	1161.13	-668.82
	$\sigma_{s,c}$22	-271375.13	-10748.43	1183.94	-1105.08
	$\sigma_{cls,Max}$22	-271375.13	-10748.43	1183.94	-76.93
	$\sigma_{cls,Med}$22	-271375.13	-10748.43	1183.94	-59.44
246	Ft. 21	-263880.66	5939.80	-927.73	-740.31
	$\sigma_{s,c}$22	-267925.13	6487.95	-1045.11	-1019.64
	$\sigma_{cls,Max}$22	-267925.13	6487.95	-1045.11	-70.32
	$\sigma_{cls,Med}$22	-267925.13	6487.95	-1045.11	-58.68

Pilastro: **246/346** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
246	1	-342876.59	-8611.10	2436.41	0.43
346	1	-338391.59	26710.23	-4498.71	0.48

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	11141.29	86297.23	2010.18	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	11141.29	64722.92	2010.18	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	11141.29	86297.23	2010.18	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
246	Ft. 16	-230670.94	-6055.49	1601.64	-607.87
	$\sigma_{s,c}$15	-235582.13	-6163.05	1672.75	-928.03
	$\sigma_{cls,Max}$15	-235582.13	-6163.05	1672.75	-64.87
	$\sigma_{cls,Med}$15	-235582.13	-6163.05	1672.75	-51.60
346	Ft. 16	-227220.94	17922.52	-2947.14	-359.63
	$\sigma_{s,c}$15	-232132.13	18328.06	-3045.58	-1159.35
	$\sigma_{cls,Max}$15	-232132.13	18328.06	-3045.58	-84.02

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-232132.13	18328.06	-3045.58	-50.84
Combinazioni Frequenti					
246	Ft. 19	-228963.45	-6003.75	1579.95	-603.80
	$\sigma_{s,c}$18	-230598.06	-6039.05	1603.72	-907.43
	$\sigma_{cls,Max}$18	-230598.06	-6039.05	1603.72	-63.40
	$\sigma_{cls,Med}$20	-233572.73	-5363.28	1401.90	-51.16
346	Ft. 19	-225513.45	17725.74	-2917.86	-358.16
	$\sigma_{s,c}$18	-227148.06	17858.79	-2950.80	-1132.29
	$\sigma_{cls,Max}$18	-227148.06	17858.79	-2950.80	-82.03
	$\sigma_{cls,Med}$20	-230122.73	15654.94	-2311.73	-50.40
Combinazioni Quasi Permanenti					
246	Ft. 21	-228948.88	-6000.46	1580.37	-603.79
	$\sigma_{s,c}$21	-228948.88	-6000.46	1580.37	-900.64
	$\sigma_{cls,Max}$21	-228948.88	-6000.46	1580.37	-62.91
	$\sigma_{cls,Med}$22	-233653.00	-5350.20	1382.25	-51.18
346	Ft. 21	-225498.88	17712.99	-2918.60	-358.30
	$\sigma_{s,c}$21	-225498.88	17712.99	-2918.60	-1123.46
	$\sigma_{cls,Max}$21	-225498.88	17712.99	-2918.60	-81.37
	$\sigma_{cls,Med}$22	-230203.00	15684.27	-2292.39	-50.42

Pilastro: **47/147** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
47	1	-425899.25	13154.62	3700.70	0.54
147	1	-420244.25	-8372.20	1472.78	0.51

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	6732.56	86297.23	609.96	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	6732.56	64722.92	609.96	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	6732.56	86297.23	609.96	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
47	Ft. 17	-285971.22	9237.07	2553.00	-707.26
	$\sigma_{s,c}$15	-296005.56	9088.31	2517.28	-1201.27
	$\sigma_{cls,Max}$15	-296005.56	9088.31	2517.28	-84.57
	$\sigma_{cls,Med}$15	-296005.56	9088.31	2517.28	-64.84
147	Ft. 17	-281621.22	-5513.38	1019.26	-802.67
	$\sigma_{s,c}$15	-291655.56	-5431.62	1094.81	-1081.91
	$\sigma_{cls,Max}$15	-291655.56	-5431.62	1094.81	-74.34
	$\sigma_{cls,Med}$15	-291655.56	-5431.62	1094.81	-63.88
Combinazioni Frequenti					
47	Ft. 20	-281663.13	9098.05	2518.49	-696.47
	$\sigma_{s,c}$18	-287414.84	8933.01	2440.98	-1168.08
	$\sigma_{cls,Max}$18	-287414.84	8933.01	2440.98	-82.25
	$\sigma_{cls,Med}$18	-287414.84	8933.01	2440.98	-62.95
147	Ft. 20	-277313.13	-5385.20	944.22	-792.99

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-283064.84	-5259.26	1028.67	-1048.77
	$\sigma_{cls,Max}$18	-283064.84	-5259.26	1028.67	-72.03
	$\sigma_{cls,Med}$18	-283064.84	-5259.26	1028.67	-62.00
Combinazioni Quasi Permanenti					
47	Ft. 22	-280227.13	9051.72	2506.99	-692.88
	$\sigma_{s,c}$21	-284556.03	8880.03	2415.53	-1157.01
	$\sigma_{cls,Max}$21	-284556.03	8880.03	2415.53	-81.47
	$\sigma_{cls,Med}$21	-284556.03	8880.03	2415.53	-62.33
147	Ft. 22	-275877.13	-5342.47	919.21	-789.77
	$\sigma_{s,c}$21	-280206.03	-5201.92	1006.71	-1037.74
	$\sigma_{cls,Max}$21	-280206.03	-5201.92	1006.71	-71.26
	$\sigma_{cls,Med}$21	-280206.03	-5201.92	1006.71	-61.37

Pilastro: **147/247** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
147	1	-361046.97	-17847.05	-5777.01	0.49
247	1	-356561.97	7509.65	3072.01	0.44

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	7395.59	86297.23	2564.93	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	7395.59	64722.92	2564.93	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	7395.59	86297.23	2564.93	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
147	Ft. 17	-239234.73	-11935.09	-4066.08	-461.44
	$\sigma_{s,c}$15	-249532.58	-11932.78	-4122.79	-1146.18
	$\sigma_{cls,Max}$15	-249532.58	-11932.78	-4122.79	-83.24
	$\sigma_{cls,Med}$15	-249532.58	-11932.78	-4122.79	-54.66
247	Ft. 17	-235784.73	5111.05	2290.08	-618.22
	$\sigma_{s,c}$15	-246082.58	5007.98	2262.39	-962.40
	$\sigma_{cls,Max}$15	-246082.58	5007.98	2262.39	-67.63
	$\sigma_{cls,Med}$15	-246082.58	5007.98	2262.39	-53.90
Combinazioni Frequenti					
147	Ft. 20	-237120.45	-11423.04	-3852.64	-469.66
	$\sigma_{s,c}$18	-243121.72	-11334.69	-3911.97	-1108.63
	$\sigma_{cls,Max}$18	-243121.72	-11334.69	-3911.97	-80.39
	$\sigma_{cls,Med}$18	-243121.72	-11334.69	-3911.97	-53.25
247	Ft. 20	-233670.45	4698.38	2098.39	-624.12
	$\sigma_{s,c}$18	-239671.72	4528.11	2103.10	-928.42
	$\sigma_{cls,Max}$18	-239671.72	4528.11	2103.10	-65.10
	$\sigma_{cls,Med}$18	-239671.72	4528.11	2103.10	-52.50
Combinazioni Quasi Permanenti					
147	Ft. 22	-236415.69	-11252.36	-3781.50	-472.40
	$\sigma_{s,c}$21	-240989.02	-11136.71	-3841.77	-1096.15
	$\sigma_{cls,Max}$21	-240989.02	-11136.71	-3841.77	-79.44

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-240989.02	-11136.71	-3841.77	-52.78
247	Ft. 22	-232965.69	4560.82	2034.49	-626.09
	$\sigma_{s,c}$21	-237539.02	4369.25	2050.03	-917.12
	$\sigma_{cls,Max}$21	-237539.02	4369.25	2050.03	-64.26
	$\sigma_{cls,Med}$21	-237539.02	4369.25	2050.03	-52.03

Pilastro: **247/347** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
247	1	-309948.53	-14651.14	-5489.55	0.42
347	1	-305463.53	45001.19	9595.50	0.55

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	17290.53	86297.23	4372.48	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	17290.53	64722.92	4372.48	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	17290.53	86297.23	4372.48	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
247	Ft. 17	-201688.23	-9757.16	-3559.53	-389.82
	$\sigma_{s,c}$15	-212618.22	-10165.37	-3854.24	-987.45
	$\sigma_{cls,Max}$15	-212618.22	-10165.37	-3854.24	-72.04
	$\sigma_{cls,Med}$15	-212618.22	-10165.37	-3854.24	-46.57
347	Ft. 15	-209168.22	30384.39	6626.93	31.59
	$\sigma_{s,c}$15	-209168.22	30384.39	6626.93	-1401.50
	$\sigma_{cls,Max}$15	-209168.22	30384.39	6626.93	-106.58
	$\sigma_{cls,Med}$15	-209168.22	30384.39	6626.93	-47.45
Combinazioni Frequenti					
247	Ft. 20	-201587.95	-9632.13	-3454.53	-394.87
	$\sigma_{s,c}$18	-208095.75	-9968.15	-3713.07	-964.87
	$\sigma_{cls,Max}$18	-208095.75	-9968.15	-3713.07	-70.33
	$\sigma_{cls,Med}$18	-208095.75	-9968.15	-3713.07	-45.58
347	Ft. 18	-204645.75	29670.56	6478.99	29.65
	$\sigma_{s,c}$18	-204645.75	29670.56	6478.99	-1370.02
	$\sigma_{cls,Max}$18	-204645.75	29670.56	6478.99	-104.18
	$\sigma_{cls,Med}$18	-204645.75	29670.56	6478.99	-46.40
Combinazioni Quasi Permanenti					
247	Ft. 22	-201554.56	-9590.45	-3419.53	-396.56
	$\sigma_{s,c}$21	-206592.19	-9902.71	-3666.25	-957.37
	$\sigma_{cls,Max}$21	-206592.19	-9902.71	-3666.25	-69.77
	$\sigma_{cls,Med}$21	-206592.19	-9902.71	-3666.25	-45.25
347	Ft. 21	-203142.19	29435.82	6430.13	29.06
	$\sigma_{s,c}$21	-203142.19	29435.82	6430.13	-1359.61
	$\sigma_{cls,Max}$21	-203142.19	29435.82	6430.13	-103.39
	$\sigma_{cls,Med}$21	-203142.19	29435.82	6430.13	-46.06

Pilastro: **48/148** / L 4.10[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 210.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
48	1	-222696.30	18571.83	-100.95	0.31
148	1	-217041.30	-10981.62	3757.55	0.29

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	6860.19	86297.23	1533.51	61956.98	ø 10 2br.x4br./15.0
1.13	3.23	6860.19	64722.92	1533.51	46467.73	ø 10 2br.x4br./20.0
3.23	4.23	6860.19	86297.23	1533.51	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm^2]
Combinazioni Rare					
48	Ft. 17	-152582.66	12668.77	-188.16	-288.10
	$\sigma_{s,c}$15	-157786.58	12721.84	-70.94	-728.76
	$\sigma_{cls,Max}$15	-157786.58	12721.84	-70.94	-50.92
	$\sigma_{cls,Med}$15	-157786.58	12721.84	-70.94	-34.56
148	Ft. 17	-148232.66	-7205.76	2736.01	-282.12
	$\sigma_{s,c}$15	-153436.58	-7148.32	2648.39	-705.30
	$\sigma_{cls,Max}$15	-153436.58	-7148.32	2648.39	-51.31
	$\sigma_{cls,Med}$15	-153436.58	-7148.32	2648.39	-33.61
Combinazioni Frequenti					
48	Ft. 20	-151015.75	12374.43	-177.01	-288.13
	$\sigma_{s,c}$18	-153176.33	12386.28	-53.36	-707.56
	$\sigma_{cls,Max}$18	-153176.33	12386.28	-53.36	-49.43
	$\sigma_{cls,Med}$18	-153176.33	12386.28	-53.36	-33.55
148	Ft. 20	-146665.75	-7005.34	2633.89	-283.50
	$\sigma_{s,c}$18	-148826.33	-6903.29	2527.33	-682.29
	$\sigma_{cls,Max}$20	-146665.75	-7005.34	2633.89	-49.60
	$\sigma_{cls,Med}$18	-148826.33	-6903.29	2527.33	-32.60
Combinazioni Quasi Permanenti					
48	Ft. 22	-150493.47	12276.32	-173.29	-288.13
	$\sigma_{s,c}$22	-150493.47	12276.32	-173.29	-700.77
	$\sigma_{cls,Max}$22	-150493.47	12276.32	-173.29	-49.09
	$\sigma_{cls,Med}$21	-151645.58	12274.53	-47.23	-33.22
148	Ft. 22	-146143.47	-6938.53	2599.85	-283.96
	$\sigma_{s,c}$22	-146143.47	-6938.53	2599.85	-676.36
	$\sigma_{cls,Max}$22	-146143.47	-6938.53	2599.85	-49.29
	$\sigma_{cls,Med}$21	-147295.58	-6822.31	2486.80	-32.26

Pilastro: **148/248** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
148	1	-184555.64	-14555.27	-8587.53	0.31
248	1	-180070.64	-780.95	5561.75	0.25

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4082.04	86297.23	4101.24	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	4082.04	64722.92	4101.24	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	4082.04	86297.23	4101.24	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
148	Ft. 17	-125125.91	-9705.13	-6006.59	-60.16
	$\sigma_{s,c}$15	-130366.01	-9628.89	-5981.58	-776.35
	$\sigma_{cls,Max}$15	-130366.01	-9628.89	-5981.58	-60.30
	$\sigma_{cls,Med}$15	-130366.01	-9628.89	-5981.58	-28.71
248	Ft. 17	-121675.91	-506.19	3879.23	-268.08
	$\sigma_{s,c}$15	-126916.02	-635.75	3928.43	-552.36
	$\sigma_{cls,Max}$15	-126916.02	-635.75	3928.43	-41.42
	$\sigma_{cls,Med}$15	-126916.02	-635.75	3928.43	-27.80
Combinazioni Frequenti					
148	Ft. 20	-124615.45	-9337.26	-5661.38	-76.23
	$\sigma_{s,c}$18	-126824.21	-9202.87	-5636.72	-746.63
	$\sigma_{cls,Max}$18	-126824.21	-9202.87	-5636.72	-57.85
	$\sigma_{cls,Med}$18	-126824.21	-9202.87	-5636.72	-27.86
248	Ft. 20	-121165.45	-635.08	3521.32	-275.68
	$\sigma_{s,c}$18	-123374.21	-788.33	3604.38	-532.91
	$\sigma_{cls,Max}$18	-123374.21	-788.33	3604.38	-39.78
	$\sigma_{cls,Med}$18	-123374.21	-788.33	3604.38	-27.02
Combinazioni Quasi Permanenti					
148	Ft. 22	-124445.28	-9214.63	-5546.31	-81.48
	$\sigma_{s,c}$21	-125649.39	-9061.77	-5521.50	-736.77
	$\sigma_{cls,Max}$22	-124445.28	-9214.63	-5546.31	-57.05
	$\sigma_{cls,Med}$21	-125649.39	-9061.77	-5521.50	-27.59
248	Ft. 21	-122199.39	-838.02	3496.14	-276.56
	$\sigma_{s,c}$21	-122199.39	-838.02	3496.14	-526.42
	$\sigma_{cls,Max}$21	-122199.39	-838.02	3496.14	-39.24
	$\sigma_{cls,Med}$21	-122199.39	-838.02	3496.14	-26.77

Pilastro: **248/348** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
248	1	-155001.63	-8970.30	-14229.21	0.34
348	3	-142460.00	27364.57	24661.68	0.62

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.12	1.13	10655.17	86297.23	11363.51	61956.98	ø 10 2br.x4br./15.0
1.13	2.33	10656.11	64722.92	11388.37	46467.73	ø 10 2br.x4br./20.0
2.33	3.33	10656.89	86297.23	11409.09	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
248	Ft. 17	-103576.06	-6103.93	-10010.11	163.94

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-108947.16	-6256.06	-9769.38	-798.35
	$\sigma_{cls,Max}$17	-103576.06	-6103.93	-10010.11	-67.19
	$\sigma_{cls,Med}$17	-103576.06	-6103.93	-10010.11	-29.13
348	Ft. 17	-100126.06	18360.22	16805.74	1518.15
	$\sigma_{s,c}$17	-100126.06	18360.22	16805.74	-1465.65
	$\sigma_{cls,Max}$17	-100126.06	18360.22	16805.74	-138.07
	$\sigma_{cls,Med}$17	-100126.06	18360.22	16805.74	-51.47
Combinazioni Frequenti					
248	Ft. 20	-103975.77	-6006.14	-9814.58	144.03
	$\sigma_{s,c}$20	-103975.77	-6006.14	-9814.58	-785.00
	$\sigma_{cls,Max}$20	-103975.77	-6006.14	-9814.58	-66.05
	$\sigma_{cls,Med}$20	-103975.77	-6006.14	-9814.58	-28.69
348	Ft. 20	-100525.77	18075.68	16803.12	1497.78
	$\sigma_{s,c}$20	-100525.77	18075.68	16803.12	-1457.58
	$\sigma_{cls,Max}$20	-100525.77	18075.68	16803.12	-137.26
	$\sigma_{cls,Med}$20	-100525.77	18075.68	16803.12	-51.34
Combinazioni Quasi Permanenti					
248	Ft. 22	-104108.98	-5973.54	-9749.41	137.59
	$\sigma_{s,c}$22	-104108.98	-5973.54	-9749.41	-781.60
	$\sigma_{cls,Max}$22	-104108.98	-5973.54	-9749.41	-65.68
	$\sigma_{cls,Med}$22	-104108.98	-5973.54	-9749.41	-28.55
348	Ft. 22	-100658.98	17980.82	16802.24	1491.02
	$\sigma_{s,c}$22	-100658.98	17980.82	16802.24	-1454.90
	$\sigma_{cls,Max}$22	-100658.98	17980.82	16802.24	-137.00
	$\sigma_{cls,Med}$22	-100658.98	17980.82	16802.24	-51.30

Pilastro: **49/149** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
49	1	-425012.75	510.46	-7229.76	0.51
149	1	-419357.75	-1150.14	1195.99	0.49

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	447.39	61956.98	3410.46	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	447.39	46467.73	3410.46	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	447.39	61956.98	3410.46	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
49	Ft. 17	-286909.63	359.96	-5290.00	-844.67
	$\sigma_{s,c}$15	-297599.88	344.10	-5006.36	-1070.61
	$\sigma_{cls,Max}$15	-297599.88	344.10	-5006.36	-72.66
	$\sigma_{cls,Med}$15	-297599.88	344.10	-5006.36	-65.18
149	Ft. 17	-282559.63	-767.77	758.11	-891.53
	$\sigma_{s,c}$15	-293249.88	-796.81	560.31	-997.99
	$\sigma_{cls,Max}$15	-293249.88	-796.81	560.31	-67.54
	$\sigma_{cls,Med}$15	-293249.88	-796.81	560.31	-64.23

Combinazioni Frequenti					
49	Ft. 20	-281943.47	344.36	-5451.98	-826.20
	$\sigma_{s,c}$18	-287550.91	335.62	-5163.06	-1039.88
	$\sigma_{cls,Max}$18	-287550.91	335.62	-5163.06	-70.63
	$\sigma_{cls,Med}$18	-287550.91	335.62	-5163.06	-62.98
149	Ft. 20	-277593.47	-732.00	980.65	-872.71
	$\sigma_{s,c}$18	-283200.91	-764.51	752.80	-967.10
	$\sigma_{cls,Max}$18	-283200.91	-764.51	752.80	-65.48
	$\sigma_{cls,Med}$18	-283200.91	-764.51	752.80	-62.03
Combinazioni Quasi Permanenti					
49	Ft. 22	-280288.09	339.16	-5505.97	-820.04
	$\sigma_{s,c}$21	-284216.03	332.56	-5213.70	-1029.66
	$\sigma_{cls,Max}$21	-284216.03	332.56	-5213.70	-69.95
	$\sigma_{cls,Med}$21	-284216.03	332.56	-5213.70	-62.25
149	Ft. 22	-275938.09	-720.07	1054.83	-866.44
	$\sigma_{s,c}$21	-279866.03	-753.54	815.71	-956.82
	$\sigma_{cls,Max}$21	-279866.03	-753.54	815.71	-64.79
	$\sigma_{cls,Med}$21	-279866.03	-753.54	815.71	-61.30

Pilastro: **149/249** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
149	1	-344084.63	2112.47	14445.23	0.44
249	1	-339599.63	-2056.98	-10010.12	0.42

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	1307.12	61956.98	7113.62	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	1307.12	46467.73	7113.62	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	1307.12	61956.98	7113.62	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
149	Ft. 17	-229047.27	1518.18	9744.74	-544.85
	$\sigma_{s,c}$15	-239759.47	1475.26	9823.66	-995.35
	$\sigma_{cls,Max}$15	-239759.47	1475.26	9823.66	-69.79
	$\sigma_{cls,Med}$15	-239759.47	1475.26	9823.66	-52.52
249	Ft. 17	-225597.27	-1624.66	-6955.65	-575.75
	$\sigma_{s,c}$15	-236309.47	-1440.83	-6818.95	-933.77
	$\sigma_{cls,Max}$15	-236309.47	-1440.83	-6818.95	-65.11
	$\sigma_{cls,Med}$15	-236309.47	-1440.83	-6818.95	-51.76
Combinazioni Frequenti					
149	Ft. 20	-226811.45	1455.24	9456.73	-544.22
	$\sigma_{s,c}$18	-232444.23	1408.43	9430.11	-962.75
	$\sigma_{cls,Max}$18	-232444.23	1408.43	9430.11	-67.47
	$\sigma_{cls,Med}$18	-232444.23	1408.43	9430.11	-50.91
249	Ft. 20	-223361.45	-1563.57	-6691.07	-574.67
	$\sigma_{s,c}$18	-228994.23	-1375.52	-6475.22	-902.04
	$\sigma_{cls,Max}$18	-228994.23	-1375.52	-6475.22	-62.86
	$\sigma_{cls,Med}$18	-228994.23	-1375.52	-6475.22	-50.16
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
149	Ft. 22	-226066.19	1434.25	9360.73	-544.00
	$\sigma_{s,c}$21	-230018.88	1385.95	9298.84	-951.92
	$\sigma_{cls,Max}$21	-230018.88	1385.95	9298.84	-66.69
	$\sigma_{cls,Med}$21	-230018.88	1385.95	9298.84	-50.38
249	Ft. 22	-222616.19	-1543.21	-6602.88	-574.31
	$\sigma_{s,c}$21	-226568.88	-1353.56	-6360.14	-891.49
	$\sigma_{cls,Max}$22	-222616.19	-1543.21	-6602.88	-62.17
	$\sigma_{cls,Med}$21	-226568.88	-1353.56	-6360.14	-49.63

Pilastro: **249/349** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
249	1	-279726.78	2718.25	10958.40	0.36
349	1	-275241.78	-3970.95	-32068.00	0.43

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1938.90	61956.98	12471.42	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	1938.90	46467.73	12471.42	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	1938.90	61956.98	12471.42	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
249	Ft. 17	-182422.34	1580.12	7208.28	-431.18
	$\sigma_{s,c}$15	-193509.47	1877.08	7801.10	-823.10
	$\sigma_{cls,Max}$15	-193509.47	1877.08	7801.10	-58.40
	$\sigma_{cls,Med}$15	-193509.47	1877.08	7801.10	-42.39
349	Ft. 15	-190059.47	-2710.80	-22102.07	-176.68
	$\sigma_{s,c}$15	-190059.47	-2710.80	-22102.07	-1072.21
	$\sigma_{cls,Max}$15	-190059.47	-2710.80	-22102.07	-78.50
	$\sigma_{cls,Med}$15	-190059.47	-2710.80	-22102.07	-41.63
Combinazioni Frequenti					
249	Ft. 19	-187039.59	1779.62	7306.32	-438.40
	$\sigma_{s,c}$18	-188638.13	1804.46	7426.37	-798.65
	$\sigma_{cls,Max}$18	-188638.13	1804.46	7426.37	-56.62
	$\sigma_{cls,Med}$18	-188638.13	1804.46	7426.37	-41.32
349	Ft. 18	-185188.13	-2627.31	-21153.05	-178.86
	$\sigma_{s,c}$18	-185188.13	-2627.31	-21153.05	-1038.02
	$\sigma_{cls,Max}$18	-185188.13	-2627.31	-21153.05	-75.96
	$\sigma_{cls,Med}$18	-185188.13	-2627.31	-21153.05	-40.56
Combinazioni Quasi Permanenti					
249	Ft. 21	-187025.81	1779.97	7303.67	-438.39
	$\sigma_{s,c}$21	-187025.81	1779.97	7303.67	-790.57
	$\sigma_{cls,Max}$21	-187025.81	1779.97	7303.67	-56.03
	$\sigma_{cls,Med}$21	-187025.81	1779.97	7303.67	-40.97
349	Ft. 21	-183575.81	-2598.98	-20842.42	-179.54
	$\sigma_{s,c}$21	-183575.81	-2598.98	-20842.42	-1026.74
	$\sigma_{cls,Max}$21	-183575.81	-2598.98	-20842.42	-75.12

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-183575.81	-2598.98	-20842.42	-40.21

Pilastro: **52/152** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
52	1	-467297.75	362.82	-6604.49	0.56
152	1	-461642.72	-390.56	603.57	0.53

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	338.68	61956.98	3404.03	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	338.68	46467.73	3404.03	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	338.68	61956.98	3404.03	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
52	Ft. 16	-315457.16	239.84	-4911.98	-948.47
	$\sigma_{s,c}$15	-326310.94	240.38	-4692.31	-1156.50
	$\sigma_{cls,Max}$15	-326310.94	240.38	-4692.31	-78.21
	$\sigma_{cls,Med}$15	-326310.94	240.38	-4692.31	-71.47
152	Ft. 16	-311107.16	-255.42	402.04	-1007.45
	$\sigma_{s,c}$15	-321960.94	-259.48	170.01	-1068.84
	$\sigma_{cls,Max}$15	-321960.94	-259.48	170.01	-71.58
	$\sigma_{cls,Med}$15	-321960.94	-259.48	170.01	-70.52
Combinazioni Frequenti					
52	Ft. 19	-311821.53	240.24	-4981.20	-935.38
	$\sigma_{s,c}$20	-316155.59	285.18	-4902.84	-1128.00
	$\sigma_{cls,Max}$20	-316155.59	285.18	-4902.84	-76.40
	$\sigma_{cls,Med}$20	-316155.59	285.18	-4902.84	-69.25
152	Ft. 19	-307471.53	-254.86	479.31	-994.26
	$\sigma_{s,c}$20	-311805.59	-338.30	449.57	-1042.56
	$\sigma_{cls,Max}$20	-311805.59	-338.30	449.57	-69.97
	$\sigma_{cls,Med}$20	-311805.59	-338.30	449.57	-68.30
Combinazioni Quasi Permanenti					
52	Ft. 21	-311817.88	240.36	-4980.38	-935.37
	$\sigma_{s,c}$22	-314376.53	283.95	-4987.09	-1123.50
	$\sigma_{cls,Max}$22	-314376.53	283.95	-4987.09	-76.11
	$\sigma_{cls,Med}$22	-314376.53	283.95	-4987.09	-68.86
152	Ft. 21	-307467.88	-255.03	479.29	-994.24
	$\sigma_{s,c}$22	-310026.53	-336.56	544.48	-1038.21
	$\sigma_{cls,Max}$22	-310026.53	-336.56	544.48	-69.70
	$\sigma_{cls,Med}$22	-310026.53	-336.56	544.48	-67.91

Pilastro: **152/252** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
152	1	-383210.03	548.48	17809.37	0.50

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
252	1	-378725.03	-523.87	-11137.08	0.47

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	310.83	61956.98	8390.27	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	310.83	46467.73	8390.27	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	310.83	61956.98	8390.27	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
152	Ft. 16	-258252.77	359.28	11619.16	-647.01
	$\sigma_{s,c}$15	-266259.59	371.01	12109.07	-1084.67
	$\sigma_{cls,Max}$15	-266259.59	371.01	12109.07	-74.88
	$\sigma_{cls,Med}$15	-266259.59	371.01	12109.07	-58.32
252	Ft. 16	-254802.77	-347.08	-7164.94	-708.92
	$\sigma_{s,c}$15	-262809.63	-358.76	-7580.47	-998.87
	$\sigma_{cls,Max}$15	-262809.63	-358.76	-7580.47	-68.35
	$\sigma_{cls,Med}$15	-262809.63	-358.76	-7580.47	-57.56
Combinazioni Frequenti					
152	Ft. 19	-255568.70	356.27	11457.36	-640.93
	$\sigma_{s,c}$20	-259298.28	334.17	11658.74	-1053.26
	$\sigma_{cls,Max}$20	-259298.28	334.17	11658.74	-72.67
	$\sigma_{cls,Med}$20	-259298.28	334.17	11658.74	-56.80
252	Ft. 19	-252118.70	-343.73	-7028.02	-702.45
	$\sigma_{s,c}$18	-254787.14	-347.64	-7166.58	-965.39
	$\sigma_{cls,Max}$18	-254787.14	-347.64	-7166.58	-66.03
	$\sigma_{cls,Med}$20	-255848.28	-145.70	-7172.47	-56.04
Combinazioni Quasi Permanenti					
152	Ft. 21	-255565.58	356.46	11457.67	-640.91
	$\sigma_{s,c}$22	-258475.89	331.86	11539.43	-1048.54
	$\sigma_{cls,Max}$22	-258475.89	331.86	11539.43	-72.33
	$\sigma_{cls,Med}$22	-258475.89	331.86	11539.43	-56.62
252	Ft. 21	-252115.58	-343.84	-7028.35	-702.43
	$\sigma_{s,c}$22	-255025.89	-143.12	-7062.74	-957.97
	$\sigma_{cls,Max}$22	-255025.89	-143.12	-7062.74	-65.28
	$\sigma_{cls,Med}$22	-255025.89	-143.12	-7062.74	-55.86

Pilastro: **252/352** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
252	1	-313423.00	831.77	16661.66	0.41
352	1	-308938.00	-1678.20	-53154.73	0.55

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1429.39	61956.98	20236.64	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	1429.39	46467.73	20236.64	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	1429.39	61956.98	20236.64	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
252	Ft. 17	-211887.77	970.43	11496.08	-477.25
	$\sigma_{s,c}$15	-216225.52	562.76	11686.12	-919.47
	$\sigma_{cls,Max}$17	-211887.77	970.43	11496.08	-64.15
	$\sigma_{cls,Med}$15	-216225.52	562.76	11686.12	-47.36
352	Ft. 17	-208437.77	-2332.19	-35514.26	-26.83
	$\sigma_{s,c}$17	-208437.77	-2332.19	-35514.26	-1341.63
	$\sigma_{cls,Max}$17	-208437.77	-2332.19	-35514.26	-98.46
	$\sigma_{cls,Med}$15	-212775.52	-1125.58	-36320.41	-46.95
Combinazioni Frequenti					
252	Ft. 20	-212216.66	954.21	11125.22	-484.91
	$\sigma_{s,c}$20	-212216.66	954.21	11125.22	-909.57
	$\sigma_{cls,Max}$20	-212216.66	954.21	11125.22	-63.70
	$\sigma_{cls,Med}$20	-212216.66	954.21	11125.22	-46.48
352	Ft. 20	-208766.66	-2314.42	-34967.43	-38.29
	$\sigma_{s,c}$20	-208766.66	-2314.42	-34967.43	-1332.70
	$\sigma_{cls,Max}$20	-208766.66	-2314.42	-34967.43	-97.73
	$\sigma_{cls,Med}$20	-208766.66	-2314.42	-34967.43	-46.42
Combinazioni Quasi Permanenti					
252	Ft. 22	-212326.30	948.80	11001.60	-487.47
	$\sigma_{s,c}$22	-212326.30	948.80	11001.60	-907.74
	$\sigma_{cls,Max}$22	-212326.30	948.80	11001.60	-63.55
	$\sigma_{cls,Med}$22	-212326.30	948.80	11001.60	-46.51
352	Ft. 22	-208876.30	-2308.50	-34785.15	-42.07
	$\sigma_{s,c}$22	-208876.30	-2308.50	-34785.15	-1329.75
	$\sigma_{cls,Max}$22	-208876.30	-2308.50	-34785.15	-97.49
	$\sigma_{cls,Med}$22	-208876.30	-2308.50	-34785.15	-46.38

Pilastro: **53/153** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
53	1	-487052.28	-689.10	17846.66	0.62
153	1	-481397.28	-34.75	2939.85	0.56

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	516.01	61956.98	4902.80	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	516.01	46467.73	4902.80	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	516.01	61956.98	4902.80	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
53	Ft. 16	-327701.94	-505.47	11995.81	-864.38
	$\sigma_{s,c}$15	-339375.69	-527.38	12615.68	-1338.16
	$\sigma_{cls,Max}$15	-339375.69	-527.38	12615.68	-92.05
	$\sigma_{cls,Med}$15	-339375.69	-527.38	12615.68	-74.34
153	Ft. 17	-321587.97	-108.98	2121.52	-1018.42
	$\sigma_{s,c}$15	-335025.69	10.15	1855.76	-1131.41
	$\sigma_{cls,Max}$15	-335025.69	10.15	1855.76	-75.77

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-335025.69	10.15	1855.76	-73.38
Combinazioni Frequenti					
53	Ft. 20	-320170.09	-396.85	11404.02	-852.76
	$\sigma_{s,c}$18	-327672.84	-500.60	11987.51	-1288.58
	$\sigma_{cls,Max}$18	-327672.84	-500.60	11987.51	-88.61
	$\sigma_{cls,Med}$18	-327672.84	-500.60	11987.51	-71.77
153	Ft. 20	-315820.09	-99.53	2104.80	-1000.04
	$\sigma_{s,c}$18	-323322.84	4.45	1838.12	-1092.49
	$\sigma_{cls,Max}$18	-323322.84	4.45	1838.12	-73.16
	$\sigma_{cls,Med}$18	-323322.84	4.45	1838.12	-70.82
Combinazioni Quasi Permanenti					
53	Ft. 22	-318247.47	-396.70	11269.40	-848.65
	$\sigma_{s,c}$21	-323776.78	-492.48	11779.50	-1272.12
	$\sigma_{cls,Max}$21	-323776.78	-492.48	11779.50	-87.46
	$\sigma_{cls,Med}$21	-323776.78	-492.48	11779.50	-70.92
153	Ft. 22	-313897.47	-96.37	2099.23	-993.91
	$\sigma_{s,c}$21	-319426.78	3.14	1831.62	-1079.54
	$\sigma_{cls,Max}$21	-319426.78	3.14	1831.62	-72.30
	$\sigma_{cls,Med}$21	-319426.78	3.14	1831.62	-69.97

Pilastro: **153/253** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
153	1	-402401.94	601.20	-7261.28	0.48
253	1	-397916.94	-544.10	-1177.69	0.46

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	393.36	61956.98	1940.35	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	393.36	46467.73	1940.35	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	393.36	61956.98	1940.35	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
153	Ft. 17	-265442.38	399.33	-5332.31	-772.19
	$\sigma_{s,c}$15	-279044.09	400.94	-5404.15	-1017.96
	$\sigma_{cls,Max}$15	-279044.09	400.94	-5404.15	-69.28
	$\sigma_{cls,Med}$15	-279044.09	400.94	-5404.15	-61.12
253	Ft. 17	-261992.38	-239.88	-458.75	-845.65
	$\sigma_{s,c}$15	-275594.09	-367.32	-464.66	-924.76
	$\sigma_{cls,Max}$15	-275594.09	-367.32	-464.66	-62.15
	$\sigma_{cls,Med}$15	-275594.09	-367.32	-464.66	-60.36
Combinazioni Frequenti					
153	Ft. 20	-262669.88	392.68	-4970.23	-769.22
	$\sigma_{s,c}$18	-270318.69	390.80	-5072.63	-983.54
	$\sigma_{cls,Max}$18	-270318.69	390.80	-5072.63	-66.92
	$\sigma_{cls,Med}$18	-270318.69	390.80	-5072.63	-59.21
253	Ft. 20	-259219.89	-237.75	-739.18	-832.02

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-266868.69	-358.86	-555.52	-897.31
	$\sigma_{cls,Max}$18	-266868.69	-358.86	-555.52	-60.33
	$\sigma_{cls,Med}$18	-266868.69	-358.86	-555.52	-58.45
Combinazioni Quasi Permanenti					
153	Ft. 22	-261745.73	390.46	-4849.53	-768.23
	$\sigma_{s,c}$21	-267414.53	387.04	-4962.51	-972.08
	$\sigma_{cls,Max}$21	-267414.53	387.04	-4962.51	-66.13
	$\sigma_{cls,Med}$21	-267414.53	387.04	-4962.51	-58.57
253	Ft. 22	-258295.73	-237.04	-832.66	-827.48
	$\sigma_{s,c}$21	-263964.53	-355.78	-585.50	-888.16
	$\sigma_{cls,Max}$21	-263964.53	-355.78	-585.50	-59.72
	$\sigma_{cls,Med}$21	-263964.53	-355.78	-585.50	-57.82

Pilastro: **253/353** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
253	1	-319775.44	1562.90	-14684.98	0.41
353	1	-315290.44	-3364.69	31377.13	0.47

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1888.97	61956.98	13702.72	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	1888.97	46467.73	13702.72	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	1888.97	61956.98	13702.72	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
253	Ft. 17	-206320.45	1308.53	-10180.57	-469.72
	$\sigma_{s,c}$15	-220188.84	1033.93	-10023.22	-920.28
	$\sigma_{cls,Max}$15	-220188.84	1033.93	-10023.22	-64.31
	$\sigma_{cls,Med}$15	-220188.84	1033.93	-10023.22	-48.23
353	Ft. 17	-202870.45	-3011.28	22141.96	-208.56
	$\sigma_{s,c}$15	-216738.84	-2226.31	21491.14	-1134.46
	$\sigma_{cls,Max}$17	-202870.45	-3011.28	22141.96	-82.34
	$\sigma_{cls,Med}$15	-216738.84	-2226.31	21491.14	-47.47
Combinazioni Frequenti					
253	Ft. 20	-206536.16	1282.91	-10054.99	-473.30
	$\sigma_{s,c}$18	-214416.11	1003.32	-9680.37	-894.73
	$\sigma_{cls,Max}$18	-214416.11	1003.32	-9680.37	-62.51
	$\sigma_{cls,Med}$18	-214416.11	1003.32	-9680.37	-46.96
353	Ft. 20	-203086.16	-2969.72	22276.24	-208.40
	$\sigma_{s,c}$20	-203086.16	-2969.72	22276.24	-1126.09
	$\sigma_{cls,Max}$20	-203086.16	-2969.72	22276.24	-82.42
	$\sigma_{cls,Med}$18	-210966.11	-2170.78	21026.26	-46.21
Combinazioni Quasi Permanenti					
253	Ft. 22	-206608.08	1274.37	-10013.12	-474.49
	$\sigma_{s,c}$21	-212495.55	992.19	-9565.55	-886.19
	$\sigma_{cls,Max}$22	-206608.08	1274.37	-10013.12	-62.11

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-212495.55	992.19	-9565.55	-46.54
353	Ft. 22	-203158.08	-2955.87	22320.99	-208.34
	$\sigma_{s,c}$22	-203158.08	-2955.87	22320.99	-1126.62
	$\sigma_{cls,Max}$22	-203158.08	-2955.87	22320.99	-82.45
	$\sigma_{cls,Med}$21	-209045.55	-2150.39	20870.20	-45.79

Pilastro: **54/154** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
54	1	-423642.78	-1406.48	-6024.50	0.51
154	1	-417987.78	-158.80	1178.54	0.48

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	724.65	61956.98	3584.28	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	724.65	46467.73	3584.28	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	724.65	61956.98	3584.28	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
54	Ft. 16	-285166.47	-1015.10	-4220.72	-835.59
	$\sigma_{s,c}$15	-295226.13	-1050.83	-4182.85	-1071.82
	$\sigma_{cls,Max}$15	-295226.13	-1050.83	-4182.85	-73.40
	$\sigma_{cls,Med}$15	-295226.13	-1050.83	-4182.85	-64.66
154	Ft. 17	-279531.50	-232.90	447.57	-903.68
	$\sigma_{s,c}$15	-290876.13	-66.90	690.65	-969.10
	$\sigma_{cls,Max}$15	-290876.13	-66.90	690.65	-64.81
	$\sigma_{cls,Med}$15	-290876.13	-66.90	690.65	-63.71
Combinazioni Frequenti					
54	Ft. 19	-281787.69	-995.72	-4232.55	-824.91
	$\sigma_{s,c}$18	-285139.97	-1007.37	-4219.90	-1037.91
	$\sigma_{cls,Max}$18	-285139.97	-1007.37	-4219.90	-71.09
	$\sigma_{cls,Med}$18	-285139.97	-1007.37	-4219.90	-62.46
154	Ft. 20	-274616.47	-208.67	596.78	-885.86
	$\sigma_{s,c}$18	-280789.97	-65.51	770.81	-937.23
	$\sigma_{cls,Max}$18	-280789.97	-65.51	770.81	-62.69
	$\sigma_{cls,Med}$18	-280789.97	-65.51	770.81	-61.50
Combinazioni Quasi Permanenti					
54	Ft. 22	-277328.16	-846.74	-3866.96	-820.98
	$\sigma_{s,c}$21	-281782.38	-994.18	-4232.39	-1026.66
	$\sigma_{cls,Max}$21	-281782.38	-994.18	-4232.39	-70.33
	$\sigma_{cls,Med}$21	-281782.38	-994.18	-4232.39	-61.72
154	Ft. 22	-272978.16	-200.59	646.52	-879.92
	$\sigma_{s,c}$21	-277432.38	-64.21	797.41	-926.60
	$\sigma_{cls,Max}$21	-277432.38	-64.21	797.41	-61.99
	$\sigma_{cls,Med}$21	-277432.38	-64.21	797.41	-60.77

Pilastro: **154/254** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
154	1	-351276.22	1557.49	7221.41	0.43
254	1	-346791.22	-1337.34	-5336.97	0.42

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	839.08	61956.98	3640.11	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	839.08	46467.73	3640.11	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	839.08	61956.98	3640.11	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm^2]
Combinazioni Rare					
154	Ft. 17	-232303.06	1060.96	4814.40	-650.74
	$\sigma_{s,c}$15	-243660.53	1080.46	4913.19	-915.29
	$\sigma_{cls,Max}$15	-243660.53	1080.46	4913.19	-63.13
	$\sigma_{cls,Med}$15	-243660.53	1080.46	4913.19	-53.37
254	Ft. 17	-228853.06	-744.12	-3396.74	-672.67
	$\sigma_{s,c}$15	-240210.53	-931.32	-3601.31	-877.75
	$\sigma_{cls,Max}$15	-240210.53	-931.32	-3601.31	-60.22
	$\sigma_{cls,Med}$15	-240210.53	-931.32	-3601.31	-52.61
Combinazioni Frequenti					
154	Ft. 20	-229825.30	1020.85	4718.27	-645.44
	$\sigma_{s,c}$18	-236028.11	1036.30	4748.20	-886.11
	$\sigma_{cls,Max}$18	-236028.11	1036.30	4748.20	-61.10
	$\sigma_{cls,Med}$18	-236028.11	1036.30	4748.20	-51.70
254	Ft. 20	-226375.30	-711.11	-3278.37	-667.51
	$\sigma_{s,c}$18	-232578.11	-893.46	-3428.65	-848.65
	$\sigma_{cls,Max}$18	-232578.11	-893.46	-3428.65	-58.21
	$\sigma_{cls,Med}$18	-232578.11	-893.46	-3428.65	-50.94
Combinazioni Quasi Permanenti					
154	Ft. 22	-228999.38	1007.48	4686.22	-643.68
	$\sigma_{s,c}$21	-233487.95	1021.15	4693.12	-876.38
	$\sigma_{cls,Max}$21	-233487.95	1021.15	4693.12	-60.42
	$\sigma_{cls,Med}$21	-233487.95	1021.15	4693.12	-51.14
254	Ft. 22	-225549.38	-700.10	-3238.91	-665.80
	$\sigma_{s,c}$21	-230037.95	-880.53	-3370.90	-838.94
	$\sigma_{cls,Max}$21	-230037.95	-880.53	-3370.90	-57.53
	$\sigma_{cls,Med}$21	-230037.95	-880.53	-3370.90	-50.39

Pilastro: **254/354** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
254	1	-280374.88	2766.39	1309.22	0.34
354	1	-275889.88	-5130.16	-10286.97	0.37

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2973.76	61956.98	4044.27	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	2973.76	46467.73	4044.27	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	2973.76	61956.98	4044.27	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
254	Ft. 17	-181748.31	2268.98	1445.97	-501.30
	$\sigma_{s,c}$15	-193194.66	1859.35	1037.82	-710.87
	$\sigma_{cls,Max}$15	-193194.66	1859.35	1037.82	-49.70
	$\sigma_{cls,Med}$15	-193194.66	1859.35	1037.82	-42.32
354	Ft. 17	-178298.31	-4588.35	-8262.15	-304.69
	$\sigma_{s,c}$17	-178298.31	-4588.35	-8262.15	-866.91
	$\sigma_{cls,Max}$17	-178298.31	-4588.35	-8262.15	-64.50
	$\sigma_{cls,Med}$15	-189744.66	-3422.69	-7099.26	-41.56
Combinazioni Frequenti					
254	Ft. 20	-181705.25	2214.63	1328.41	-504.82
	$\sigma_{s,c}$18	-188004.17	1794.32	972.71	-690.68
	$\sigma_{cls,Max}$20	-181705.25	2214.63	1328.41	-48.71
	$\sigma_{cls,Med}$18	-188004.17	1794.32	972.71	-41.18
354	Ft. 20	-178255.25	-4521.53	-8081.56	-309.63
	$\sigma_{s,c}$20	-178255.25	-4521.53	-8081.56	-861.69
	$\sigma_{cls,Max}$20	-178255.25	-4521.53	-8081.56	-64.04
	$\sigma_{cls,Med}$18	-184554.17	-3328.19	-6826.12	-40.42
Combinazioni Quasi Permanenti					
254	Ft. 22	-181690.86	2196.52	1289.22	-505.99
	$\sigma_{s,c}$22	-181690.86	2196.52	1289.22	-687.91
	$\sigma_{cls,Max}$22	-181690.86	2196.52	1289.22	-48.60
	$\sigma_{cls,Med}$21	-186277.39	1771.44	951.33	-40.80
354	Ft. 22	-178240.86	-4499.26	-8021.36	-311.28
	$\sigma_{s,c}$22	-178240.86	-4499.26	-8021.36	-859.95
	$\sigma_{cls,Max}$22	-178240.86	-4499.26	-8021.36	-63.89
	$\sigma_{cls,Med}$21	-182827.39	-3294.33	-6735.65	-40.05

Pilastro: **55/155** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
55	1	-570150.31	368.82	-5157.67	0.67
155	1	-564495.31	-481.85	-2178.06	0.65

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	553.43	61956.98	3194.85	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	553.43	46467.73	3194.85	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	553.43	61956.98	3194.85	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
55	Ft. 16	-383493.25	212.41	-3745.26	-1191.96

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-396188.84	203.91	-3690.94	-1368.55
	$\sigma_{cls,Max}$15	-396188.84	203.91	-3690.94	-92.12
	$\sigma_{cls,Med}$15	-396188.84	203.91	-3690.94	-86.78
155	Ft. 17	-382082.66	-442.43	-1676.12	-1213.85
	$\sigma_{s,c}$15	-391838.84	-283.73	-1539.18	-1321.60
	$\sigma_{cls,Max}$15	-391838.84	-283.73	-1539.18	-88.70
	$\sigma_{cls,Med}$15	-391838.84	-283.73	-1539.18	-85.83
Combinazioni Frequenti					
55	Ft. 19	-379223.28	219.45	-3758.92	-1177.48
	$\sigma_{s,c}$18	-383453.75	216.76	-3740.66	-1327.93
	$\sigma_{cls,Max}$18	-383453.75	216.76	-3740.66	-89.44
	$\sigma_{cls,Med}$18	-383453.75	216.76	-3740.66	-83.99
155	Ft. 20	-375865.78	-439.68	-1463.67	-1196.99
	$\sigma_{s,c}$18	-379103.75	-289.04	-1385.21	-1277.41
	$\sigma_{cls,Max}$18	-379103.75	-289.04	-1385.21	-85.74
	$\sigma_{cls,Med}$18	-379103.75	-289.04	-1385.21	-83.04
Combinazioni Quasi Permanenti					
55	Ft. 22	-378143.59	335.02	-3574.77	-1173.27
	$\sigma_{s,c}$21	-379215.38	220.32	-3758.00	-1314.40
	$\sigma_{cls,Max}$21	-379215.38	220.32	-3758.00	-88.55
	$\sigma_{cls,Med}$21	-379215.38	220.32	-3758.00	-83.06
155	Ft. 22	-373793.59	-438.76	-1392.85	-1191.37
	$\sigma_{s,c}$22	-373793.59	-438.76	-1392.85	-1264.85
	$\sigma_{cls,Max}$22	-373793.59	-438.76	-1392.85	-85.07
	$\sigma_{cls,Med}$21	-374865.38	-290.19	-1333.71	-82.11

Pilastro: **155/255** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
155	1	-477160.38	134.42	7622.07	0.57
255	1	-472675.38	-138.01	-1940.68	0.55

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	362.67	61956.98	2771.81	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	362.67	46467.73	2771.81	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	362.67	61956.98	2771.81	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
155	Ft. 17	-320327.88	21.21	5230.16	-966.22
	$\sigma_{s,c}$15	-329918.25	65.78	5307.61	-1172.86
	$\sigma_{cls,Max}$15	-329918.25	65.78	5307.61	-79.21
	$\sigma_{cls,Med}$15	-329918.25	65.78	5307.61	-72.26
255	Ft. 17	-316877.88	239.19	-1441.48	-1009.92
	$\sigma_{s,c}$15	-326468.25	-75.93	-1401.75	-1097.96
	$\sigma_{cls,Max}$15	-326468.25	-75.93	-1401.75	-73.53
	$\sigma_{cls,Med}$15	-326468.25	-75.93	-1401.75	-71.51

Combinazioni Frequenti					
155	Ft. 19	-317318.06	78.25	5034.87	-957.71
	$\sigma_{s,c}$18	-320458.53	76.02	5103.14	-1138.76
	$\sigma_{cls,Max}$18	-320458.53	76.02	5103.14	-76.91
	$\sigma_{cls,Med}$18	-320458.53	76.02	5103.14	-70.19
255	Ft. 20	-313948.56	221.87	-1266.80	-1003.71
	$\sigma_{s,c}$18	-317008.53	-89.56	-1229.10	-1064.49
	$\sigma_{cls,Max}$18	-317008.53	-89.56	-1229.10	-71.29
	$\sigma_{cls,Med}$18	-317008.53	-89.56	-1229.10	-69.44
Combinazioni Quasi Permanenti					
155	Ft. 22	-316422.06	37.36	5031.25	-956.13
	$\sigma_{s,c}$21	-317311.06	78.90	5034.93	-1127.40
	$\sigma_{cls,Max}$21	-317311.06	78.90	5034.93	-76.14
	$\sigma_{cls,Med}$21	-317311.06	78.90	5034.93	-69.50
255	Ft. 22	-312972.06	216.09	-1208.57	-1001.63
	$\sigma_{s,c}$22	-312972.06	216.09	-1208.57	-1054.92
	$\sigma_{cls,Max}$22	-312972.06	216.09	-1208.57	-70.79
	$\sigma_{cls,Med}$21	-313861.06	-93.73	-1171.35	-68.75

Pilastro: **255/355** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
255	1	-387764.53	2067.10	9912.32	0.48
355	1	-383279.53	-4464.72	-39694.25	0.58

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	3101.82	61956.98	14378.72	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	3101.82	46467.73	14378.72	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	3101.82	61956.98	14378.72	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
255	Ft. 17	-256775.83	2077.49	6835.23	-665.75
	$\sigma_{s,c}$15	-266214.66	1356.12	6853.33	-1029.90
	$\sigma_{cls,Max}$17	-256775.83	2077.49	6835.23	-71.69
	$\sigma_{cls,Med}$15	-266214.66	1356.12	6853.33	-58.31
355	Ft. 17	-253325.83	-5013.11	-26466.63	-239.91
	$\sigma_{s,c}$17	-253325.83	-5013.11	-26466.63	-1424.70
	$\sigma_{cls,Max}$17	-253325.83	-5013.11	-26466.63	-105.40
	$\sigma_{cls,Med}$15	-262764.66	-2954.84	-26943.27	-57.55
Combinazioni Frequenti					
255	Ft. 20	-257114.66	2048.10	6657.70	-670.70
	$\sigma_{s,c}$20	-257114.66	2048.10	6657.70	-1018.81
	$\sigma_{cls,Max}$20	-257114.66	2048.10	6657.70	-71.44
	$\sigma_{cls,Med}$18	-259978.55	1317.95	6655.84	-56.94
355	Ft. 20	-253664.66	-4949.58	-26246.73	-246.64
	$\sigma_{s,c}$20	-253664.66	-4949.58	-26246.73	-1420.20
	$\sigma_{cls,Max}$20	-253664.66	-4949.58	-26246.73	-104.99
	$\sigma_{cls,Med}$18	-256528.55	-2874.56	-26400.36	-56.19
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
255	Ft. 22	-257227.59	2038.30	6598.52	-672.35
	$\sigma_{s,c}$22	-257227.59	2038.30	6598.52	-1017.90
	$\sigma_{cls,Max}$22	-257227.59	2038.30	6598.52	-71.36
	$\sigma_{cls,Med}$21	-257904.80	1304.09	6590.01	-56.49
355	Ft. 22	-253777.59	-4928.40	-26173.44	-248.89
	$\sigma_{s,c}$22	-253777.59	-4928.40	-26173.44	-1418.69
	$\sigma_{cls,Max}$22	-253777.59	-4928.40	-26173.44	-104.85
	$\sigma_{cls,Med}$21	-254454.80	-2845.58	-26219.02	-55.73

Pilastro: **56/156** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
56	1	-543372.06	938.98	6583.07	0.64
156	1	-537717.06	-1008.46	5112.30	0.63

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	716.59	61956.98	3255.37	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	716.59	46467.73	3255.37	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	716.59	61956.98	3255.37	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
56	Ft. 17	-364711.00	643.60	3980.25	-1112.69
	$\sigma_{s,c}$15	-376853.59	600.40	4585.58	-1332.27
	$\sigma_{cls,Max}$15	-376853.59	600.40	4585.58	-90.32
	$\sigma_{cls,Med}$15	-376853.59	600.40	4585.58	-82.54
156	Ft. 17	-360361.00	-710.46	3749.62	-1100.04
	$\sigma_{s,c}$15	-372503.59	-647.66	3578.75	-1303.01
	$\sigma_{cls,Max}$15	-372503.59	-647.66	3578.75	-88.24
	$\sigma_{cls,Med}$15	-372503.59	-647.66	3578.75	-81.59
Combinazioni Frequenti					
56	Ft. 20	-359294.47	650.71	3678.52	-1099.60
	$\sigma_{s,c}$18	-365615.94	604.87	4203.32	-1289.23
	$\sigma_{cls,Max}$18	-365615.94	604.87	4203.32	-87.39
	$\sigma_{cls,Med}$18	-365615.94	604.87	4203.32	-80.08
156	Ft. 20	-354944.47	-712.66	3746.70	-1082.22
	$\sigma_{s,c}$18	-361265.94	-643.62	3540.35	-1265.33
	$\sigma_{cls,Max}$18	-361265.94	-643.62	3540.35	-85.72
	$\sigma_{cls,Med}$18	-361265.94	-643.62	3540.35	-79.13
Combinazioni Quasi Permanenti					
56	Ft. 22	-357488.97	653.08	3577.94	-1095.24
	$\sigma_{s,c}$21	-361871.16	606.16	4075.90	-1274.89
	$\sigma_{cls,Max}$21	-361871.16	606.16	4075.90	-86.41
	$\sigma_{cls,Med}$21	-361871.16	606.16	4075.90	-79.26
156	Ft. 22	-353138.97	-713.40	3745.72	-1076.28
	$\sigma_{s,c}$21	-357521.16	-642.06	3527.56	-1252.77
	$\sigma_{cls,Max}$21	-357521.16	-642.06	3527.56	-84.88

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-357521.16	-642.06	3527.56	-78.31

Pilastro: **156/256** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
156	1	-459995.75	377.21	-10807.56	0.56
256	1	-455510.75	-542.63	-3011.63	0.53

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	489.07	61956.98	2259.69	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	489.07	46467.73	2259.69	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	489.07	61956.98	2259.69	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
156	Ft. 17	-305089.44	169.99	-7546.38	-873.53
	$\sigma_{s,c}$15	-317301.03	237.88	-7608.97	-1174.53
	$\sigma_{cls,Max}$15	-317301.03	237.88	-7608.97	-79.92
	$\sigma_{cls,Med}$15	-317301.03	237.88	-7608.97	-69.50
256	Ft. 17	-301639.44	-130.41	-1823.35	-957.07
	$\sigma_{s,c}$15	-313851.03	-358.14	-1815.30	-1072.25
	$\sigma_{cls,Max}$15	-313851.03	-358.14	-1815.30	-72.21
	$\sigma_{cls,Med}$15	-313851.03	-358.14	-1815.30	-68.74
Combinazioni Frequenti					
156	Ft. 20	-302745.88	184.63	-7134.75	-872.10
	$\sigma_{s,c}$18	-309094.09	242.82	-7193.09	-1140.92
	$\sigma_{cls,Max}$18	-309094.09	242.82	-7193.09	-77.62
	$\sigma_{cls,Med}$18	-309094.09	242.82	-7193.09	-67.70
256	Ft. 20	-299295.88	-148.51	-2085.17	-944.51
	$\sigma_{s,c}$18	-305644.09	-365.43	-1943.34	-1047.61
	$\sigma_{cls,Max}$18	-305644.09	-365.43	-1943.34	-70.60
	$\sigma_{cls,Med}$18	-305644.09	-365.43	-1943.34	-66.95
Combinazioni Quasi Permanenti					
156	Ft. 22	-301964.69	189.51	-6997.54	-871.62
	$\sigma_{s,c}$21	-306359.44	244.23	-7054.73	-1129.71
	$\sigma_{cls,Max}$21	-306359.44	244.23	-7054.73	-76.85
	$\sigma_{cls,Med}$21	-306359.44	244.23	-7054.73	-67.10
256	Ft. 22	-298514.69	-154.55	-2172.45	-940.32
	$\sigma_{s,c}$21	-302909.44	-367.71	-1985.78	-1039.39
	$\sigma_{cls,Max}$21	-302909.44	-367.71	-1985.78	-70.07
	$\sigma_{cls,Med}$21	-302909.44	-367.71	-1985.78	-66.35

Pilastro: **256/356** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
256	1	-380698.66	1616.59	-24250.65	0.51

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
356	1	-376213.66	-2081.23	67865.18	0.68

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1725.43	61956.98	26936.95	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	1725.43	46467.73	26936.95	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	1725.43	61956.98	26936.95	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
256	Ft. 17	-248321.55	1420.17	-16736.66	-496.92
	$\sigma_{s,c}$15	-260629.47	1053.84	-16628.47	-1161.82
	$\sigma_{cls,Max}$15	-260629.47	1053.84	-16628.47	-81.61
	$\sigma_{cls,Med}$15	-260629.47	1053.84	-16628.47	-57.09
356	Ft. 17	-244871.55	-2481.10	46782.02	55.92
	$\sigma_{s,c}$17	-244871.55	-2481.10	46782.02	-1657.58
	$\sigma_{cls,Max}$17	-244871.55	-2481.10	46782.02	-121.88
	$\sigma_{cls,Med}$15	-257179.45	-1344.15	46345.79	-57.72
Combinazioni Frequenti					
256	Ft. 20	-249035.94	1405.75	-16537.80	-502.98
	$\sigma_{s,c}$18	-255413.63	1019.47	-16203.48	-1136.64
	$\sigma_{cls,Max}$20	-249035.94	1405.75	-16537.80	-80.10
	$\sigma_{cls,Med}$18	-255413.63	1019.47	-16203.48	-55.94
356	Ft. 20	-245585.94	-2457.11	46568.54	47.73
	$\sigma_{s,c}$20	-245585.94	-2457.11	46568.54	-1654.85
	$\sigma_{cls,Max}$20	-245585.94	-2457.11	46568.54	-121.61
	$\sigma_{cls,Med}$20	-245585.94	-2457.11	46568.54	-56.79
Combinazioni Quasi Permanenti					
256	Ft. 22	-249274.06	1400.94	-16471.52	-505.00
	$\sigma_{s,c}$22	-249274.06	1400.94	-16471.52	-1132.99
	$\sigma_{cls,Max}$22	-249274.06	1400.94	-16471.52	-80.06
	$\sigma_{cls,Med}$21	-253675.91	1007.60	-16061.90	-55.56
356	Ft. 22	-245824.06	-2449.11	46497.38	45.02
	$\sigma_{s,c}$22	-245824.06	-2449.11	46497.38	-1653.95
	$\sigma_{cls,Max}$22	-245824.06	-2449.11	46497.38	-121.52
	$\sigma_{cls,Med}$22	-245824.06	-2449.11	46497.38	-56.78

Pilastro: **57/157** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
57	1	-260474.80	-411.16	-7189.01	0.32
157	1	-254819.83	-1282.14	4243.57	0.31

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	497.22	61956.98	6839.48	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	497.22	46467.73	6839.48	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	497.22	61956.98	6839.48	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
57	Ft. 17	-170524.08	-292.85	-4757.04	-473.13
	$\sigma_{s,c}$15	-182680.00	-337.38	-5000.56	-692.73
	$\sigma_{cls,Max}$15	-182680.00	-337.38	-5000.56	-47.45
	$\sigma_{cls,Med}$15	-182680.00	-337.38	-5000.56	-40.01
157	Ft. 17	-166174.09	-874.95	2917.99	-470.40
	$\sigma_{s,c}$15	-178330.02	-867.51	3056.43	-663.50
	$\sigma_{cls,Max}$15	-178330.02	-867.51	3056.43	-45.77
	$\sigma_{cls,Med}$15	-178330.02	-867.51	3056.43	-39.06
Combinazioni Frequenti					
57	Ft. 20	-168055.00	-281.92	-5020.28	-461.06
	$\sigma_{s,c}$18	-176380.25	-314.00	-5077.88	-672.55
	$\sigma_{cls,Max}$18	-176380.25	-314.00	-5077.88	-46.10
	$\sigma_{cls,Med}$18	-176380.25	-314.00	-5077.88	-38.63
157	Ft. 20	-163705.00	-844.79	3074.94	-460.68
	$\sigma_{s,c}$18	-172030.25	-834.32	3111.21	-642.64
	$\sigma_{cls,Max}$18	-172030.25	-834.32	3111.21	-44.35
	$\sigma_{cls,Med}$18	-172030.25	-834.32	3111.21	-37.68
Combinazioni Quasi Permanenti					
57	Ft. 22	-167231.98	-278.28	-5108.03	-457.04
	$\sigma_{s,c}$21	-174278.27	-306.34	-5103.59	-665.82
	$\sigma_{cls,Max}$21	-174278.27	-306.34	-5103.59	-45.64
	$\sigma_{cls,Med}$21	-174278.27	-306.34	-5103.59	-38.17
157	Ft. 22	-162881.98	-834.73	3127.25	-457.44
	$\sigma_{s,c}$21	-169928.27	-823.20	3129.34	-635.68
	$\sigma_{cls,Max}$21	-169928.27	-823.20	3129.34	-43.87
	$\sigma_{cls,Med}$21	-169928.27	-823.20	3129.34	-37.22

Pilastro: **157/257** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
157	1	-226174.41	2105.60	-8650.18	0.29
257	1	-221689.41	-1408.28	-3143.74	0.27

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1018.52	61956.98	1747.83	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	1018.52	46467.73	1747.83	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	1018.52	61956.98	1747.83	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
157	Ft. 17	-145849.48	1472.24	-5976.46	-334.60
	$\sigma_{s,c}$15	-158054.41	1507.59	-5874.55	-663.34
	$\sigma_{cls,Max}$15	-158054.41	1507.59	-5874.55	-46.99
	$\sigma_{cls,Med}$15	-158054.41	1507.59	-5874.55	-34.62
257	Ft. 17	-142399.48	-1021.81	-1803.59	-405.85
	$\sigma_{s,c}$15	-154604.41	-1029.94	-2050.72	-574.26
	$\sigma_{cls,Max}$15	-154604.41	-1029.94	-2050.72	-39.82

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-154604.41	-1029.94	-2050.72	-33.86
Combinazioni Frequenti					
157	Ft. 20	-144291.19	1398.71	-5483.35	-339.88
	$\sigma_{s,c}$18	-152682.08	1429.02	-5429.70	-635.91
	$\sigma_{cls,Max}$18	-152682.08	1429.02	-5429.70	-44.99
	$\sigma_{cls,Med}$18	-152682.08	1429.02	-5429.70	-33.44
257	Ft. 20	-140841.19	-961.39	-2253.40	-395.29
	$\sigma_{s,c}$18	-149232.08	-978.20	-2383.95	-560.42
	$\sigma_{cls,Max}$18	-149232.08	-978.20	-2383.95	-38.90
	$\sigma_{cls,Med}$18	-149232.08	-978.20	-2383.95	-32.69
Combinazioni Quasi Permanenti					
157	Ft. 22	-143771.75	1374.20	-5318.98	-341.65
	$\sigma_{s,c}$21	-150889.36	1402.81	-5281.53	-626.77
	$\sigma_{cls,Max}$21	-150889.36	1402.81	-5281.53	-44.32
	$\sigma_{cls,Med}$21	-150889.36	1402.81	-5281.53	-33.05
257	Ft. 22	-140321.75	-941.25	-2403.34	-391.78
	$\sigma_{s,c}$21	-147439.36	-960.95	-2494.78	-555.79
	$\sigma_{cls,Max}$21	-147439.36	-960.95	-2494.78	-38.59
	$\sigma_{cls,Med}$21	-147439.36	-960.95	-2494.78	-32.29

Pilastro: **257/357** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
257	1	-194965.16	2249.20	-26561.38	0.32
357	1	-190480.16	-2458.83	65902.23	0.53

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1364.63	61956.98	26802.28	86297.23	ø 10 4br.x2br./15.0
1.13	2.33	1364.66	46467.73	26801.51	64722.92	ø 10 4br.x2br./20.0
2.33	3.33	1364.69	61956.98	26800.58	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
257	Ft. 17	-123352.41	1458.67	-17732.34	-68.82
	$\sigma_{s,c}$15	-135651.25	1531.04	-18143.11	-791.16
	$\sigma_{cls,Max}$15	-135651.25	1531.04	-18143.11	-57.71
	$\sigma_{cls,Med}$15	-135651.25	1531.04	-18143.11	-29.71
357	Ft. 17	-119902.41	-1459.89	43473.19	882.78
	$\sigma_{s,c}$15	-132201.27	-1627.91	44906.84	-1371.75
	$\sigma_{cls,Max}$15	-132201.27	-1627.91	44906.84	-105.15
	$\sigma_{cls,Med}$15	-132201.27	-1627.91	44906.84	-48.73
Combinazioni Frequenti					
257	Ft. 20	-122591.18	1403.29	-17640.16	-69.59
	$\sigma_{s,c}$18	-131089.00	1446.98	-17819.09	-768.19
	$\sigma_{cls,Max}$18	-131089.00	1446.98	-17819.09	-56.03
	$\sigma_{cls,Med}$18	-131089.00	1446.98	-17819.09	-28.71
357	Ft. 20	-119141.18	-1429.43	43785.25	911.97

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-127638.99	-1536.47	44464.02	-1352.98
	$\sigma_{cls,Max}$18	-127638.99	-1536.47	44464.02	-103.90
	$\sigma_{cls,Med}$18	-127638.99	-1536.47	44464.02	-48.26
Combinazioni Quasi Permanenti					
257	Ft. 22	-122337.44	1384.83	-17609.44	-69.85
	$\sigma_{s,c}$21	-129566.42	1418.89	-17710.80	-760.53
	$\sigma_{cls,Max}$21	-129566.42	1418.89	-17710.80	-55.47
	$\sigma_{cls,Med}$21	-129566.42	1418.89	-17710.80	-28.38
357	Ft. 22	-118887.44	-1419.27	43889.26	921.82
	$\sigma_{s,c}$21	-126116.42	-1505.77	44316.24	-1346.73
	$\sigma_{cls,Max}$21	-126116.42	-1505.77	44316.24	-103.49
	$\sigma_{cls,Med}$21	-126116.42	-1505.77	44316.24	-48.10

Pilastro: **58/158** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
58	1	-434726.22	9.80	-6468.53	0.52
158	1	-429071.22	989.04	2449.96	0.50

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	483.01	61956.98	4242.84	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	483.01	46467.73	4242.84	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	483.01	61956.98	4242.84	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
58	Ft. 16	-293916.56	19.58	-4751.60	-887.32
	$\sigma_{s,c}$15	-303964.78	3.71	-4516.36	-1072.68
	$\sigma_{cls,Max}$15	-303964.78	3.71	-4516.36	-72.32
	$\sigma_{cls,Med}$15	-303964.78	3.71	-4516.36	-66.58
158	Ft. 16	-289566.56	652.06	1613.84	-904.24
	$\sigma_{s,c}$15	-299614.78	695.43	1442.53	-1030.11
	$\sigma_{cls,Max}$15	-299614.78	695.43	1442.53	-69.72
	$\sigma_{cls,Med}$15	-299614.78	695.43	1442.53	-65.63
Combinazioni Frequenti					
58	Ft. 19	-290526.06	23.30	-4838.63	-874.64
	$\sigma_{s,c}$20	-295232.38	-35.26	-4755.12	-1048.89
	$\sigma_{cls,Max}$20	-295232.38	-35.26	-4755.12	-70.81
	$\sigma_{cls,Med}$20	-295232.38	-35.26	-4755.12	-64.67
158	Ft. 19	-286176.06	639.36	1675.05	-892.50
	$\sigma_{s,c}$20	-290882.38	741.70	1642.06	-1006.15
	$\sigma_{cls,Max}$20	-290882.38	741.70	1642.06	-68.22
	$\sigma_{cls,Med}$20	-290882.38	741.70	1642.06	-63.71
Combinazioni Quasi Permanenti					
58	Ft. 21	-290517.56	22.97	-4840.41	-874.60
	$\sigma_{s,c}$22	-293586.00	-30.75	-4845.41	-1044.82
	$\sigma_{cls,Max}$22	-293586.00	-30.75	-4845.41	-70.55

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$22	-293586.00	-30.75	-4845.41	-64.31
158	Ft. 21	-286167.56	639.73	1675.90	-892.45
	$\sigma_{s,c}$22	-289236.00	728.72	1718.52	-1001.58
	$\sigma_{cls,Max}$22	-289236.00	728.72	1718.52	-67.91
	$\sigma_{cls,Med}$22	-289236.00	728.72	1718.52	-63.35

Pilastro: **158/258** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
158	1	-354901.31	-2061.59	14528.29	0.46
258	1	-350416.31	1617.72	-9765.92	0.43

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1066.47	61956.98	7041.80	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	1066.47	46467.73	7041.80	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	1066.47	61956.98	7041.80	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
158	Ft. 16	-239535.67	-1369.33	9426.70	-589.25
	$\sigma_{s,c}$15	-246912.45	-1445.09	9819.05	-1017.82
	$\sigma_{cls,Max}$15	-246912.45	-1445.09	9819.05	-71.25
	$\sigma_{cls,Med}$15	-246912.45	-1445.09	9819.05	-54.08
258	Ft. 16	-236085.67	1077.50	-6237.60	-639.36
	$\sigma_{s,c}$15	-243462.45	1144.98	-6605.44	-944.37
	$\sigma_{cls,Max}$15	-243462.45	1144.98	-6605.44	-65.44
	$\sigma_{cls,Med}$15	-243462.45	1144.98	-6605.44	-53.33
Combinazioni Frequenti					
158	Ft. 19	-237041.16	-1345.98	9294.53	-583.95
	$\sigma_{s,c}$20	-241300.81	-1372.62	9456.87	-991.15
	$\sigma_{cls,Max}$20	-241300.81	-1372.62	9456.87	-69.32
	$\sigma_{cls,Med}$20	-241300.81	-1372.62	9456.87	-52.85
258	Ft. 19	-233591.16	1056.22	-6114.17	-633.86
	$\sigma_{s,c}$18	-236048.83	1078.76	-6236.76	-911.88
	$\sigma_{cls,Max}$18	-236048.83	1078.76	-6236.76	-63.13
	$\sigma_{cls,Med}$20	-237850.81	928.75	-6107.94	-52.10
Combinazioni Quasi Permanenti					
158	Ft. 21	-237033.78	-1346.37	9294.24	-583.92
	$\sigma_{s,c}$22	-240547.44	-1348.06	9362.43	-986.35
	$\sigma_{cls,Max}$22	-240547.44	-1348.06	9362.43	-68.96
	$\sigma_{cls,Med}$22	-240547.44	-1348.06	9362.43	-52.69
258	Ft. 21	-233583.78	1056.47	-6114.00	-633.83
	$\sigma_{s,c}$22	-237097.44	905.52	-6016.25	-906.20
	$\sigma_{cls,Max}$22	-237097.44	905.52	-6016.25	-62.52
	$\sigma_{cls,Med}$22	-237097.44	905.52	-6016.25	-51.93

Pilastro: **258/358** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
258	1	-290911.28	-3184.87	11276.37	0.38
358	3	-281766.69	6538.78	-37543.45	0.47

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2966.15	61956.98	14177.94	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	2966.15	46467.73	14177.94	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	2966.15	61956.98	14177.94	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
258	Ft. 17	-197844.91	-2534.74	8036.79	-437.93
	$\sigma_{s,c}$17	-197844.91	-2534.74	8036.79	-862.12
	$\sigma_{cls,Max}$17	-197844.91	-2534.74	8036.79	-61.80
	$\sigma_{cls,Med}$15	-200951.30	-2195.03	7974.08	-44.02
358	Ft. 17	-194394.91	4435.43	-25649.30	-77.51
	$\sigma_{s,c}$17	-194394.91	4435.43	-25649.30	-1199.66
	$\sigma_{cls,Max}$17	-194394.91	4435.43	-25649.30	-89.61
	$\sigma_{cls,Med}$15	-197501.30	3436.78	-25408.60	-43.26
Combinazioni Frequenti					
258	Ft. 20	-198181.52	-2485.37	7755.94	-445.20
	$\sigma_{s,c}$20	-198181.52	-2485.37	7755.94	-857.06
	$\sigma_{cls,Max}$20	-198181.52	-2485.37	7755.94	-61.35
	$\sigma_{cls,Med}$20	-198181.52	-2485.37	7755.94	-43.41
358	Ft. 20	-194731.52	4402.36	-25185.01	-87.48
	$\sigma_{s,c}$20	-194731.52	4402.36	-25185.01	-1191.99
	$\sigma_{cls,Max}$20	-194731.52	4402.36	-25185.01	-88.97
	$\sigma_{cls,Med}$20	-194731.52	4402.36	-25185.01	-42.81
Combinazioni Quasi Permanenti					
258	Ft. 22	-198293.72	-2468.91	7662.33	-447.62
	$\sigma_{s,c}$22	-198293.72	-2468.91	7662.33	-855.37
	$\sigma_{cls,Max}$22	-198293.72	-2468.91	7662.33	-61.20
	$\sigma_{cls,Med}$22	-198293.72	-2468.91	7662.33	-43.43
358	Ft. 22	-194843.72	4391.34	-25030.24	-90.79
	$\sigma_{s,c}$22	-194843.72	4391.34	-25030.24	-1189.44
	$\sigma_{cls,Max}$22	-194843.72	4391.34	-25030.24	-88.76
	$\sigma_{cls,Med}$22	-194843.72	4391.34	-25030.24	-42.81

Pilastro: **59/159** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
59	1	-375124.16	2301.30	8957.90	0.46
159	1	-369469.13	4320.43	4512.29	0.46

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	959.55	61956.98	3234.41	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	959.55	46467.73	3234.41	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	959.55	61956.98	3234.41	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
59	Ft. 16	-253234.28	1691.98	6017.86	-679.75
	$\sigma_{s,c}$15	-262072.41	1691.43	6422.79	-1019.91
	$\sigma_{cls,Max}$15	-262072.41	1691.43	6422.79	-71.07
	$\sigma_{cls,Med}$15	-262072.41	1691.43	6422.79	-57.40
159	Ft. 17	-248610.45	3132.63	3060.46	-667.10
	$\sigma_{s,c}$15	-257722.41	2987.55	2946.03	-989.98
	$\sigma_{cls,Max}$15	-257722.41	2987.55	2946.03	-69.93
	$\sigma_{cls,Med}$15	-257722.41	2987.55	2946.03	-56.45
Combinazioni Frequenti					
59	Ft. 19	-250209.09	1677.50	5878.45	-672.55
	$\sigma_{s,c}$18	-253152.45	1676.81	6013.27	-983.44
	$\sigma_{cls,Max}$18	-253152.45	1676.81	6013.27	-68.55
	$\sigma_{cls,Med}$18	-253152.45	1676.81	6013.27	-55.45
159	Ft. 20	-244246.13	2947.24	3046.52	-658.89
	$\sigma_{s,c}$18	-248802.44	2813.12	2894.60	-954.28
	$\sigma_{cls,Max}$18	-248802.44	2813.12	2894.60	-67.35
	$\sigma_{cls,Med}$18	-248802.44	2813.12	2894.60	-54.50
Combinazioni Quasi Permanenti					
59	Ft. 21	-250192.73	1674.47	5877.53	-672.61
	$\sigma_{s,c}$21	-250192.73	1674.47	5877.53	-971.42
	$\sigma_{cls,Max}$21	-250192.73	1674.47	5877.53	-67.72
	$\sigma_{cls,Med}$21	-250192.73	1674.47	5877.53	-54.80
159	Ft. 22	-242791.31	2885.44	3041.87	-656.15
	$\sigma_{s,c}$21	-245842.72	2753.24	2877.31	-942.37
	$\sigma_{cls,Max}$21	-245842.72	2753.24	2877.31	-66.48
	$\sigma_{cls,Med}$21	-245842.72	2753.24	2877.31	-53.85

Pilastro: **159/259** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
159	1	-308207.28	-11115.82	-2139.85	0.45
259	1	-303722.28	8676.23	-3550.34	0.42

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5776.86	61956.98	554.45	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	5776.86	46467.73	554.45	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	5776.86	61956.98	554.45	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
159	Ft. 17	-205152.61	-7846.94	-1742.43	-395.90

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-214243.23	-7806.57	-1790.46	-981.53
	$\sigma_{cls,Max}$15	-214243.23	-7806.57	-1790.46	-74.67
	$\sigma_{cls,Med}$15	-214243.23	-7806.57	-1790.46	-46.93
259	Ft. 17	-201702.61	6179.38	-2182.52	-430.42
	$\sigma_{s,c}$15	-210793.23	6127.67	-2172.31	-923.03
	$\sigma_{cls,Max}$15	-210793.23	6127.67	-2172.31	-68.92
	$\sigma_{cls,Med}$15	-210793.23	6127.67	-2172.31	-46.17
Combinazioni Frequenti					
159	Ft. 20	-203098.70	-7465.78	-1544.05	-404.53
	$\sigma_{s,c}$18	-207631.09	-7413.29	-1634.30	-944.74
	$\sigma_{cls,Max}$18	-207631.09	-7413.29	-1634.30	-71.74
	$\sigma_{cls,Med}$18	-207631.09	-7413.29	-1634.30	-45.48
259	Ft. 20	-199648.70	5819.72	-2314.93	-432.95
	$\sigma_{s,c}$18	-204181.09	5787.36	-2137.40	-889.91
	$\sigma_{cls,Max}$18	-204181.09	5787.36	-2137.40	-66.32
	$\sigma_{cls,Med}$18	-204181.09	5787.36	-2137.40	-44.72
Combinazioni Quasi Permanenti					
159	Ft. 22	-202414.06	-7338.72	-1477.92	-407.40
	$\sigma_{s,c}$21	-205438.72	-7281.18	-1582.54	-932.49
	$\sigma_{cls,Max}$21	-205438.72	-7281.18	-1582.54	-70.76
	$\sigma_{cls,Med}$21	-205438.72	-7281.18	-1582.54	-45.00
259	Ft. 22	-198964.06	5699.83	-2359.07	-433.79
	$\sigma_{s,c}$21	-201988.72	5673.11	-2125.71	-878.88
	$\sigma_{cls,Max}$21	-201988.72	5673.11	-2125.71	-65.45
	$\sigma_{cls,Med}$21	-201988.72	5673.11	-2125.71	-44.24

Pilastro: **259/359** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
259	1	-245352.75	-13997.20	-11313.68	0.42
359	1	-240867.75	21694.31	24116.25	0.55

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	10345.37	61956.98	10560.89	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	10345.37	46467.73	10560.89	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	10345.37	61956.98	10560.89	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
259	Ft. 17	-160173.56	-9654.77	-7775.43	-89.60
	$\sigma_{s,c}$15	-169307.28	-9653.41	-7682.96	-989.44
	$\sigma_{cls,Max}$15	-169307.28	-9653.41	-7682.96	-78.36
	$\sigma_{cls,Med}$15	-169307.28	-9653.41	-7682.96	-37.35
359	Ft. 17	-156723.56	14759.85	17109.92	425.14
	$\sigma_{s,c}$15	-165857.28	14808.23	16532.29	-1357.92
	$\sigma_{cls,Max}$17	-156723.56	14759.85	17109.92	-113.56
	$\sigma_{cls,Med}$15	-165857.28	14808.23	16532.29	-45.31

Combinazioni Frequenti					
259	Ft. 20	-160406.36	-9393.13	-7687.12	-101.05
	$\sigma_{s,c}$18	-164937.36	-9272.75	-7405.47	-958.29
	$\sigma_{cls,Max}$18	-164937.36	-9272.75	-7405.47	-75.80
	$\sigma_{cls,Med}$18	-164937.36	-9272.75	-7405.47	-36.33
359	Ft. 20	-156956.36	14575.59	17194.04	410.91
	$\sigma_{s,c}$20	-156956.36	14575.59	17194.04	-1346.84
	$\sigma_{cls,Max}$20	-156956.36	14575.59	17194.04	-112.72
	$\sigma_{cls,Med}$20	-156956.36	14575.59	17194.04	-44.45
Combinazioni Quasi Permanenti					
259	Ft. 22	-160483.97	-9305.92	-7657.69	-104.80
	$\sigma_{s,c}$22	-160483.97	-9305.92	-7657.69	-949.28
	$\sigma_{cls,Max}$22	-160483.97	-9305.92	-7657.69	-75.29
	$\sigma_{cls,Med}$21	-163490.42	-9143.58	-7313.13	-35.99
359	Ft. 22	-157033.97	14514.17	17222.08	406.24
	$\sigma_{s,c}$22	-157033.97	14514.17	17222.08	-1344.46
	$\sigma_{cls,Max}$22	-157033.97	14514.17	17222.08	-112.45
	$\sigma_{cls,Med}$22	-157033.97	14514.17	17222.08	-44.33

Pilastro: **60/160** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
60	1	-321813.69	2488.57	1752.44	0.39
160	1	-316158.69	3934.26	1433.67	0.40

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	732.20	61956.98	1971.08	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	732.20	46467.73	1971.08	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	732.20	61956.98	1971.08	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
60	Ft. 16	-217570.75	1833.89	1070.17	-638.99
	$\sigma_{s,c}$15	-224962.38	1817.55	1248.22	-817.36
	$\sigma_{cls,Max}$15	-224962.38	1817.55	1248.22	-56.79
	$\sigma_{cls,Med}$15	-224962.38	1817.55	1248.22	-49.27
160	Ft. 17	-214073.67	2871.39	700.89	-600.53
	$\sigma_{s,c}$15	-220612.38	2718.55	888.59	-825.84
	$\sigma_{cls,Max}$15	-220612.38	2718.55	888.59	-58.32
	$\sigma_{cls,Med}$15	-220612.38	2718.55	888.59	-48.32
Combinazioni Frequenti					
60	Ft. 19	-215042.31	1827.26	1009.68	-631.88
	$\sigma_{s,c}$18	-217503.94	1821.40	1068.98	-790.04
	$\sigma_{cls,Max}$18	-217503.94	1821.40	1068.98	-54.94
	$\sigma_{cls,Med}$18	-217503.94	1821.40	1068.98	-47.64
160	Ft. 20	-210503.42	2687.27	775.00	-593.45
	$\sigma_{s,c}$18	-213153.94	2543.29	921.30	-796.30
	$\sigma_{cls,Max}$18	-213153.94	2543.29	921.30	-56.15
	$\sigma_{cls,Med}$18	-213153.94	2543.29	921.30	-46.69
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
60	Ft. 22	-213663.36	1617.29	1284.58	-629.53
	$\sigma_{s,c}$21	-215028.94	1824.76	1009.44	-781.04
	$\sigma_{cls,Max}$21	-215028.94	1824.76	1009.44	-54.33
	$\sigma_{cls,Med}$21	-215028.94	1824.76	1009.44	-47.10
160	Ft. 22	-209313.36	2625.89	799.70	-591.09
	$\sigma_{s,c}$21	-210678.94	2483.45	932.05	-786.44
	$\sigma_{cls,Max}$21	-210678.94	2483.45	932.05	-55.43
	$\sigma_{cls,Med}$21	-210678.94	2483.45	932.05	-46.15

Pilastro: **160/260** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
160	1	-264676.50	-10451.49	3108.47	0.39
260	1	-260191.41	7858.44	-3875.73	0.36

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5321.91	61956.98	2024.41	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	5321.91	46467.73	2024.41	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	5321.91	61956.98	2024.41	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
160	Ft. 17	-177710.55	-7360.98	1965.68	-317.55
	$\sigma_{s,c}$15	-184117.59	-7331.46	2022.82	-871.24
	$\sigma_{cls,Max}$15	-184117.59	-7331.46	2022.82	-66.81
	$\sigma_{cls,Med}$15	-184117.59	-7331.46	2022.82	-40.33
260	Ft. 17	-174260.55	5550.87	-2227.01	-359.52
	$\sigma_{s,c}$15	-180667.59	5546.62	-2537.91	-811.55
	$\sigma_{cls,Max}$15	-180667.59	5546.62	-2537.91	-60.89
	$\sigma_{cls,Med}$15	-180667.59	5546.62	-2537.91	-39.57
Combinazioni Frequenti					
160	Ft. 20	-176018.52	-7003.72	1974.58	-323.21
	$\sigma_{s,c}$18	-178550.00	-6958.81	1983.22	-840.44
	$\sigma_{cls,Max}$18	-178550.00	-6958.81	1983.22	-64.33
	$\sigma_{cls,Med}$18	-178550.00	-6958.81	1983.22	-39.11
260	Ft. 20	-172568.52	5217.77	-2194.05	-365.10
	$\sigma_{s,c}$18	-175100.00	5229.89	-2433.77	-781.48
	$\sigma_{cls,Max}$18	-175100.00	5229.89	-2433.77	-58.50
	$\sigma_{cls,Med}$18	-175100.00	5229.89	-2433.77	-38.35
Combinazioni Quasi Permanenti					
160	Ft. 22	-175454.52	-6884.63	1977.54	-325.10
	$\sigma_{s,c}$21	-176703.91	-6833.84	1969.89	-830.19
	$\sigma_{cls,Max}$21	-176703.91	-6833.84	1969.89	-63.50
	$\sigma_{cls,Med}$21	-176703.91	-6833.84	1969.89	-38.70
260	Ft. 22	-172004.52	5106.74	-2183.06	-366.96
	$\sigma_{s,c}$21	-173253.91	5123.72	-2399.03	-771.47
	$\sigma_{cls,Max}$21	-173253.91	5123.72	-2399.03	-57.71

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-173253.91	5123.72	-2399.03	-37.95

Pilastro: **260/360** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
260	1	-209565.53	-13219.00	-2206.13	0.36
360	3	-195720.41	21572.44	-5057.19	0.47

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	10139.44	61956.98	1063.35	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	10139.44	46467.73	1063.35	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	10139.44	61956.98	1063.35	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
260	Ft. 17	-138518.16	-9233.03	-862.00	-147.23
	$\sigma_{s,c}$15	-144758.25	-9106.62	-1407.00	-788.32
	$\sigma_{cls,Max}$15	-144758.25	-9106.62	-1407.00	-63.20
	$\sigma_{cls,Med}$15	-144758.25	-9106.62	-1407.00	-31.71
360	Ft. 17	-135068.16	14709.93	-3434.64	246.27
	$\sigma_{s,c}$17	-135068.16	14709.93	-3434.64	-1018.12
	$\sigma_{cls,Max}$17	-135068.16	14709.93	-3434.64	-88.73
	$\sigma_{cls,Med}$17	-135068.16	14709.93	-3434.64	-41.59
Combinazioni Frequenti					
260	Ft. 20	-138693.39	-8973.16	-884.12	-155.76
	$\sigma_{s,c}$18	-141060.86	-8734.48	-1356.68	-763.51
	$\sigma_{cls,Max}$18	-141060.86	-8734.48	-1356.68	-61.12
	$\sigma_{cls,Med}$18	-141060.86	-8734.48	-1356.68	-30.90
360	Ft. 20	-135243.39	14494.25	-3329.51	222.84
	$\sigma_{s,c}$20	-135243.39	14494.25	-3329.51	-1006.46
	$\sigma_{cls,Max}$20	-135243.39	14494.25	-3329.51	-87.40
	$\sigma_{cls,Med}$20	-135243.39	14494.25	-3329.51	-41.04
Combinazioni Quasi Permanenti					
260	Ft. 22	-138751.80	-8886.54	-891.49	-158.59
	$\sigma_{s,c}$21	-139836.53	-8608.48	-1339.93	-755.21
	$\sigma_{cls,Max}$22	-138751.80	-8886.54	-891.49	-60.52
	$\sigma_{cls,Med}$21	-139836.53	-8608.48	-1339.93	-30.63
360	Ft. 22	-135301.80	14422.35	-3294.47	215.18
	$\sigma_{s,c}$22	-135301.80	14422.35	-3294.47	-1002.59
	$\sigma_{cls,Max}$22	-135301.80	14422.35	-3294.47	-86.96
	$\sigma_{cls,Med}$22	-135301.80	14422.35	-3294.47	-40.85

Pilastro: **61/161** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
61	1	-397877.00	2040.99	-5465.51	0.48

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
161	1	-392222.00	4620.33	-2099.71	0.49

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1153.44	61956.98	3299.03	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	1153.44	46467.73	3299.03	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	1153.44	61956.98	3299.03	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
61	Ft. 16	-268682.00	1570.90	-4024.63	-766.96
	$\sigma_{s,c}$15	-277250.06	1511.72	-3948.70	-1023.59
	$\sigma_{cls,Max}$15	-277250.06	1511.72	-3948.70	-70.67
	$\sigma_{cls,Med}$15	-277250.06	1511.72	-3948.70	-60.73
161	Ft. 17	-268971.28	3424.15	-1523.69	-749.86
	$\sigma_{s,c}$15	-272900.06	3187.96	-1468.53	-1022.06
	$\sigma_{cls,Max}$15	-272900.06	3187.96	-1468.53	-72.04
	$\sigma_{cls,Med}$15	-272900.06	3187.96	-1468.53	-59.77
Combinazioni Frequenti					
61	Ft. 19	-265751.50	1576.46	-4046.48	-756.79
	$\sigma_{s,c}$18	-268605.00	1556.24	-4021.05	-997.79
	$\sigma_{cls,Max}$18	-268605.00	1556.24	-4021.05	-69.01
	$\sigma_{cls,Med}$20	-269278.63	1261.14	-3907.30	-58.98
161	Ft. 19	-261401.56	2900.86	-1257.41	-745.99
	$\sigma_{s,c}$20	-264928.63	3198.39	-1318.41	-993.74
	$\sigma_{cls,Max}$20	-264928.63	3198.39	-1318.41	-70.14
	$\sigma_{cls,Med}$20	-264928.63	3198.39	-1318.41	-58.03
Combinazioni Quasi Permanenti					
61	Ft. 21	-265736.09	1573.52	-4045.76	-756.85
	$\sigma_{s,c}$21	-265736.09	1573.52	-4045.76	-989.32
	$\sigma_{cls,Max}$21	-265736.09	1573.52	-4045.76	-68.47
	$\sigma_{cls,Med}$22	-267931.06	1297.59	-3977.87	-58.69
161	Ft. 21	-261386.16	2902.93	-1257.25	-745.88
	$\sigma_{s,c}$22	-263581.06	3123.13	-1249.99	-985.80
	$\sigma_{cls,Max}$22	-263581.06	3123.13	-1249.99	-69.51
	$\sigma_{cls,Med}$22	-263581.06	3123.13	-1249.99	-57.73

Pilastro: **161/261** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
161	1	-331636.50	-11819.45	8448.59	0.48
261	1	-327151.50	8975.78	-2343.92	0.45

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	6031.41	61956.98	3128.26	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	6031.41	46467.73	3128.26	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	6031.41	61956.98	3128.26	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
161	Ft. 17	-226443.48	-8319.08	5787.01	-384.68
	$\sigma_{s,c}$15	-229868.92	-8257.53	5892.85	-1114.32
	$\sigma_{cls,Max}$15	-229868.92	-8257.53	5892.85	-84.76
	$\sigma_{cls,Med}$15	-229868.92	-8257.53	5892.85	-50.35
261	Ft. 17	-222993.48	6254.82	-1607.07	-507.38
	$\sigma_{s,c}$15	-226418.92	6307.61	-1657.59	-971.68
	$\sigma_{cls,Max}$15	-226418.92	6307.61	-1657.59	-72.28
	$\sigma_{cls,Med}$15	-226418.92	6307.61	-1657.59	-49.59
Combinazioni Frequenti					
161	Ft. 19	-221358.42	-7697.97	5602.21	-390.75
	$\sigma_{s,c}$20	-224640.33	-7916.73	5634.69	-1082.08
	$\sigma_{cls,Max}$20	-224640.33	-7916.73	5634.69	-82.18
	$\sigma_{cls,Med}$20	-224640.33	-7916.73	5634.69	-49.20
261	Ft. 19	-217908.42	5826.55	-1436.42	-507.09
	$\sigma_{s,c}$20	-221190.33	5879.75	-1430.85	-937.18
	$\sigma_{cls,Max}$18	-220018.20	5948.27	-1492.47	-69.49
	$\sigma_{cls,Med}$20	-221190.33	5879.75	-1430.85	-48.45
Combinazioni Quasi Permanenti					
161	Ft. 21	-221345.45	-7699.24	5602.37	-390.67
	$\sigma_{s,c}$22	-224039.30	-7782.62	5583.92	-1075.00
	$\sigma_{cls,Max}$22	-224039.30	-7782.62	5583.92	-81.55
	$\sigma_{cls,Med}$22	-224039.30	-7782.62	5583.92	-49.07
261	Ft. 21	-217895.45	5827.61	-1436.97	-507.01
	$\sigma_{s,c}$22	-220589.30	5754.73	-1372.11	-930.26
	$\sigma_{cls,Max}$22	-220589.30	5754.73	-1372.11	-68.83
	$\sigma_{cls,Med}$22	-220589.30	5754.73	-1372.11	-48.32

Pilastro: **261/361** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=62.83 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
261	3	-266237.09	-15958.87	9786.19	0.41
361	3	-261752.09	26378.24	-40794.16	0.62

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	12271.63	61956.98	14770.25	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	12271.63	46467.73	14770.25	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	12271.63	61956.98	14770.25	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
261	Ft. 17	-183248.19	-10955.17	6793.77	-134.72
	$\sigma_{s,c}$17	-183248.19	-10955.17	6793.77	-977.40
	$\sigma_{cls,Max}$17	-183248.19	-10955.17	6793.77	-77.64
	$\sigma_{cls,Med}$15	-186051.33	-10496.24	6788.30	-37.69
361	Ft. 17	-179798.19	17936.89	-27769.11	697.84
	$\sigma_{s,c}$17	-179798.19	17936.89	-27769.11	-1631.69
	$\sigma_{cls,Max}$17	-179798.19	17936.89	-27769.11	-137.02

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$17	-179798.19	17936.89	-27769.11	-50.85
Combinazioni Frequenti					
261	Ft. 20	-183662.81	-10649.39	6613.04	-147.89
	$\sigma_{s,c}$20	-183662.81	-10649.39	6613.04	-966.87
	$\sigma_{cls,Max}$20	-183662.81	-10649.39	6613.04	-76.59
	$\sigma_{cls,Med}$20	-183662.81	-10649.39	6613.04	-37.26
361	Ft. 20	-180212.81	17665.23	-27515.11	668.04
	$\sigma_{s,c}$20	-180212.81	17665.23	-27515.11	-1614.37
	$\sigma_{cls,Max}$20	-180212.81	17665.23	-27515.11	-135.25
	$\sigma_{cls,Med}$20	-180212.81	17665.23	-27515.11	-50.33
Combinazioni Quasi Permanenti					
261	Ft. 22	-183801.03	-10547.47	6552.80	-152.23
	$\sigma_{s,c}$22	-183801.03	-10547.47	6552.80	-963.38
	$\sigma_{cls,Max}$22	-183801.03	-10547.47	6552.80	-76.24
	$\sigma_{cls,Med}$22	-183801.03	-10547.47	6552.80	-37.25
361	Ft. 22	-180351.03	17574.68	-27430.45	658.21
	$\sigma_{s,c}$22	-180351.03	17574.68	-27430.45	-1608.63
	$\sigma_{cls,Max}$22	-180351.03	17574.68	-27430.45	-134.67
	$\sigma_{cls,Med}$22	-180351.03	17574.68	-27430.45	-50.17

Pilastro: **62/162** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
62	1	-509900.78	312.31	9568.36	0.61
162	1	-504245.78	919.90	368.57	0.59

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	671.67	61956.98	3686.53	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	671.67	46467.73	3686.53	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	671.67	61956.98	3686.53	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
62	Ft. 16	-343372.00	229.27	5844.58	-1025.26
	$\sigma_{s,c}$15	-353773.84	200.18	6422.19	-1273.75
	$\sigma_{cls,Max}$15	-353773.84	200.18	6422.19	-86.29
	$\sigma_{cls,Med}$15	-353773.84	200.18	6422.19	-77.49
162	Ft. 17	-337783.34	728.02	620.07	-1076.49
	$\sigma_{s,c}$15	-349423.84	656.78	379.00	-1175.13
	$\sigma_{cls,Max}$15	-349423.84	656.78	379.00	-79.16
	$\sigma_{cls,Med}$15	-349423.84	656.78	379.00	-76.54
Combinazioni Frequenti					
62	Ft. 20	-337306.03	176.85	5292.58	-1016.03
	$\sigma_{s,c}$18	-343336.75	228.29	5854.82	-1231.07
	$\sigma_{cls,Max}$18	-343336.75	228.29	5854.82	-83.37
	$\sigma_{cls,Med}$18	-343336.75	228.29	5854.82	-75.20
162	Ft. 20	-332956.03	674.79	773.85	-1059.81

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-338986.75	601.43	526.37	-1141.49
	$\sigma_{cls,Max}$18	-338986.75	601.43	526.37	-76.88
	$\sigma_{cls,Med}$18	-338986.75	601.43	526.37	-74.25
Combinazioni Quasi Permanenti					
62	Ft. 22	-335696.91	186.52	5138.89	-1012.95
	$\sigma_{s,c}$21	-339863.59	237.82	5663.98	-1216.84
	$\sigma_{cls,Max}$21	-339863.59	237.82	5663.98	-82.40
	$\sigma_{cls,Med}$21	-339863.59	237.82	5663.98	-74.44
162	Ft. 22	-331346.91	657.04	825.11	-1054.25
	$\sigma_{s,c}$21	-335513.59	582.72	576.11	-1130.30
	$\sigma_{cls,Max}$21	-335513.59	582.72	576.11	-76.12
	$\sigma_{cls,Med}$21	-335513.59	582.72	576.11	-73.49

Pilastro: **162/262** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
162	1	-430452.91	-3249.56	-7586.86	0.53
262	1	-425967.91	2416.76	-3696.04	0.51

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1642.41	61956.98	1127.77	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	1642.41	46467.73	1127.77	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	1642.41	61956.98	1127.77	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
162	Ft. 17	-285474.06	-2246.52	-5241.13	-780.73
	$\sigma_{s,c}$15	-297024.66	-2242.82	-5301.44	-1133.95
	$\sigma_{cls,Max}$15	-297024.66	-2242.82	-5301.44	-79.10
	$\sigma_{cls,Med}$15	-297024.66	-2242.82	-5301.44	-65.06
262	Ft. 17	-282024.06	1553.52	-2475.62	-836.68
	$\sigma_{s,c}$15	-293574.66	1681.92	-2361.48	-1056.68
	$\sigma_{cls,Max}$15	-293574.66	1681.92	-2361.48	-72.79
	$\sigma_{cls,Med}$15	-293574.66	1681.92	-2361.48	-64.30
Combinazioni Frequenti					
162	Ft. 20	-283508.38	-2142.46	-4933.51	-782.62
	$\sigma_{s,c}$18	-289434.69	-2132.14	-4993.51	-1100.45
	$\sigma_{cls,Max}$18	-289434.69	-2132.14	-4993.51	-76.68
	$\sigma_{cls,Med}$18	-289434.69	-2132.14	-4993.51	-63.40
262	Ft. 20	-280058.38	1458.44	-2642.24	-830.52
	$\sigma_{s,c}$18	-285984.69	1584.21	-2438.23	-1029.89
	$\sigma_{cls,Max}$18	-285984.69	1584.21	-2438.23	-70.90
	$\sigma_{cls,Med}$18	-285984.69	1584.21	-2438.23	-62.64
Combinazioni Quasi Permanenti					
162	Ft. 22	-282853.19	-2107.77	-4830.97	-783.25
	$\sigma_{s,c}$21	-286909.94	-2094.99	-4891.40	-1089.30
	$\sigma_{cls,Max}$21	-286909.94	-2094.99	-4891.40	-75.88

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-286909.94	-2094.99	-4891.40	-62.84
262	Ft. 22	-279403.19	1426.75	-2697.78	-828.47
	$\sigma_{s,c}$21	-283459.94	1551.49	-2463.30	-1020.96
	$\sigma_{cls,Max}$21	-283459.94	1551.49	-2463.30	-70.27
	$\sigma_{cls,Med}$21	-283459.94	1551.49	-2463.30	-62.09

Pilastro: **262/362** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
262	1	-355230.59	-4201.93	-14602.01	0.46
362	3	-333547.84	8784.94	42294.96	0.56

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3916.83	61956.98	16656.98	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	3916.83	46467.73	16656.98	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	3916.83	61956.98	16656.98	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
262	Ft. 17	-231795.70	-3242.79	-10413.30	-488.08
	$\sigma_{s,c}$15	-243260.88	-2892.00	-10033.58	-1055.36
	$\sigma_{cls,Max}$15	-243260.88	-2892.00	-10033.58	-75.44
	$\sigma_{cls,Med}$15	-243260.88	-2892.00	-10033.58	-53.28
362	Ft. 17	-228345.70	5962.02	28994.40	-85.33
	$\sigma_{s,c}$17	-228345.70	5962.02	28994.40	-1414.76
	$\sigma_{cls,Max}$17	-228345.70	5962.02	28994.40	-106.29
	$\sigma_{cls,Med}$15	-239810.88	4957.40	27495.94	-52.53
Combinazioni Frequenti					
262	Ft. 20	-232686.36	-3169.35	-10392.34	-493.68
	$\sigma_{s,c}$20	-232686.36	-3169.35	-10392.34	-1035.31
	$\sigma_{cls,Max}$20	-232686.36	-3169.35	-10392.34	-74.48
	$\sigma_{cls,Med}$18	-238486.38	-2790.83	-9902.75	-52.24
362	Ft. 20	-229236.36	5881.25	29055.76	-89.98
	$\sigma_{s,c}$20	-229236.36	5881.25	29055.76	-1416.02
	$\sigma_{cls,Max}$20	-229236.36	5881.25	29055.76	-106.29
	$\sigma_{cls,Med}$18	-235036.38	4807.26	27192.72	-51.48
Combinazioni Quasi Permanenti					
262	Ft. 22	-232983.22	-3144.88	-10385.35	-495.55
	$\sigma_{s,c}$22	-232983.22	-3144.88	-10385.35	-1035.39
	$\sigma_{cls,Max}$22	-232983.22	-3144.88	-10385.35	-74.46
	$\sigma_{cls,Med}$21	-236899.39	-2756.62	-9859.84	-51.89
362	Ft. 22	-229533.22	5854.32	29076.22	-91.53
	$\sigma_{s,c}$22	-229533.22	5854.32	29076.22	-1416.45
	$\sigma_{cls,Max}$22	-229533.22	5854.32	29076.22	-106.29
	$\sigma_{cls,Med}$21	-233449.39	4756.28	27095.32	-51.13

Pilastro: **63/163** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
63	1	-298902.75	705.76	-6804.38	0.36
163	1	-293247.75	-477.60	3927.17	0.35

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	549.91	61956.98	7285.39	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	549.91	46467.73	7285.39	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	549.91	61956.98	7285.39	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
63	Ft. 17	-192892.52	460.20	-4505.59	-545.41
	$\sigma_{s,c}$15	-208717.89	459.52	-4746.80	-778.01
	$\sigma_{cls,Max}$15	-208717.89	459.52	-4746.80	-53.23
	$\sigma_{cls,Med}$15	-208717.89	459.52	-4746.80	-45.72
163	Ft. 17	-188542.52	-298.88	2741.69	-565.11
	$\sigma_{s,c}$15	-204367.89	-306.08	2871.83	-728.17
	$\sigma_{cls,Max}$15	-204367.89	-306.08	2871.83	-49.40
	$\sigma_{cls,Med}$15	-204367.89	-306.08	2871.83	-44.76
Combinazioni Frequenti					
63	Ft. 20	-190083.91	466.77	-4838.44	-530.53
	$\sigma_{s,c}$18	-201125.08	467.70	-4889.24	-755.65
	$\sigma_{cls,Max}$18	-201125.08	467.70	-4889.24	-51.78
	$\sigma_{cls,Med}$18	-201125.08	467.70	-4889.24	-44.05
163	Ft. 20	-185733.91	-303.94	2953.14	-552.26
	$\sigma_{s,c}$18	-196775.08	-309.84	2984.56	-705.18
	$\sigma_{cls,Max}$18	-196775.08	-309.84	2984.56	-47.90
	$\sigma_{cls,Med}$18	-196775.08	-309.84	2984.56	-43.10
Combinazioni Quasi Permanenti					
63	Ft. 22	-189147.70	468.95	-4949.38	-525.57
	$\sigma_{s,c}$21	-198592.20	470.24	-4936.67	-748.19
	$\sigma_{cls,Max}$21	-198592.20	470.24	-4936.67	-51.29
	$\sigma_{cls,Med}$21	-198592.20	470.24	-4936.67	-43.50
163	Ft. 22	-184797.70	-305.62	3023.63	-547.98
	$\sigma_{s,c}$21	-194242.20	-311.00	3021.92	-697.51
	$\sigma_{cls,Max}$21	-194242.20	-311.00	3021.92	-47.39
	$\sigma_{cls,Med}$21	-194242.20	-311.00	3021.92	-42.55

Pilastro: **163/263** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
163	1	-260403.17	-891.75	-11395.73	0.34
263	1	-255918.17	754.54	-1350.01	0.30

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	477.28	61956.98	3046.33	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	477.28	46467.73	3046.33	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	477.28	61956.98	3046.33	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
163	Ft. 17	-165108.16	-607.91	-7833.50	-394.99
	$\sigma_{s,c}$15	-181070.13	-596.36	-7740.83	-740.50
	$\sigma_{cls,Max}$15	-181070.13	-596.36	-7740.83	-51.42
	$\sigma_{cls,Med}$15	-181070.13	-596.36	-7740.83	-39.66
263	Ft. 17	-161658.16	495.05	-598.19	-505.60
	$\sigma_{s,c}$15	-177620.13	506.38	-814.95	-613.01
	$\sigma_{cls,Max}$15	-177620.13	506.38	-814.95	-41.59
	$\sigma_{cls,Med}$15	-177620.13	506.38	-814.95	-38.90
Combinazioni Frequenti					
163	Ft. 20	-163405.19	-583.53	-7222.29	-400.17
	$\sigma_{s,c}$18	-174576.84	-570.77	-7170.24	-709.02
	$\sigma_{cls,Max}$18	-174576.84	-570.77	-7170.24	-49.19
	$\sigma_{cls,Med}$18	-174576.84	-570.77	-7170.24	-38.24
263	Ft. 20	-159955.19	468.51	-1189.03	-491.18
	$\sigma_{s,c}$18	-171126.84	474.96	-1305.96	-598.71
	$\sigma_{cls,Max}$18	-171126.84	474.96	-1305.96	-40.69
	$\sigma_{cls,Med}$18	-171126.84	474.96	-1305.96	-37.48
Combinazioni Quasi Permanenti					
163	Ft. 22	-162837.55	-575.41	-7018.55	-401.90
	$\sigma_{s,c}$21	-172410.56	-562.25	-6980.34	-698.52
	$\sigma_{cls,Max}$21	-172410.56	-562.25	-6980.34	-48.45
	$\sigma_{cls,Med}$21	-172410.56	-562.25	-6980.34	-37.76
263	Ft. 22	-159387.55	459.67	-1385.97	-486.38
	$\sigma_{s,c}$21	-168960.56	464.49	-1469.11	-593.93
	$\sigma_{cls,Max}$21	-168960.56	464.49	-1469.11	-40.39
	$\sigma_{cls,Med}$21	-168960.56	464.49	-1469.11	-37.01

Pilastro: **263/363** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
263	1	-225294.52	-77.98	-27257.41	0.35
363	1	-220809.52	-60.46	65329.07	0.53

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	352.31	61956.98	26836.66	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	352.31	46467.73	26836.66	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	352.31	61956.98	26836.66	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
263	Ft. 17	-139678.56	-102.26	-18263.95	-156.92

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-155845.73	-73.95	-18634.45	-819.19
	$\sigma_{cls,Max}$15	-155845.73	-73.95	-18634.45	-58.01
	$\sigma_{cls,Med}$15	-155845.73	-73.95	-18634.45	-34.14
363	Ft. 17	-136228.56	79.83	43329.51	584.09
	$\sigma_{s,c}$15	-152395.73	-14.03	44546.78	-1308.49
	$\sigma_{cls,Max}$15	-152395.73	-14.03	44546.78	-96.87
	$\sigma_{cls,Med}$15	-152395.73	-14.03	44546.78	-48.40
Combinazioni Frequenti					
263	Ft. 20	-138951.30	-101.87	-18231.78	-155.07
	$\sigma_{s,c}$18	-150314.89	-78.19	-18386.20	-797.09
	$\sigma_{cls,Max}$18	-150314.89	-78.19	-18386.20	-56.49
	$\sigma_{cls,Med}$18	-150314.89	-78.19	-18386.20	-32.92
363	Ft. 20	-135501.30	82.91	43836.21	618.87
	$\sigma_{s,c}$18	-146864.89	-2.17	44357.28	-1295.81
	$\sigma_{cls,Max}$18	-146864.89	-2.17	44357.28	-96.20
	$\sigma_{cls,Med}$18	-146864.89	-2.17	44357.28	-48.09
Combinazioni Quasi Permanenti					
263	Ft. 22	-138708.89	-101.74	-18221.05	-154.45
	$\sigma_{s,c}$21	-148469.42	-79.72	-18303.00	-789.72
	$\sigma_{cls,Max}$21	-148469.42	-79.72	-18303.00	-55.99
	$\sigma_{cls,Med}$21	-148469.42	-79.72	-18303.00	-32.52
363	Ft. 22	-135258.89	83.93	44005.12	630.67
	$\sigma_{s,c}$21	-145019.42	2.00	44294.38	-1291.90
	$\sigma_{cls,Max}$21	-145019.42	2.00	44294.38	-96.01
	$\sigma_{cls,Med}$21	-145019.42	2.00	44294.38	-48.00

Pilastro: **64/164** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
64	1	-382053.59	475.46	-428.09	0.44
164	1	-376398.59	-319.87	1745.71	0.44

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	314.15	61956.98	3888.20	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	314.15	46467.73	3888.20	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	314.15	61956.98	3888.20	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
64	Ft. 17	-253615.89	309.16	-614.82	-813.37
	$\sigma_{s,c}$15	-267938.69	311.05	-186.96	-893.27
	$\sigma_{cls,Max}$15	-267938.69	311.05	-186.96	-59.94
	$\sigma_{cls,Med}$15	-267938.69	311.05	-186.96	-58.69
164	Ft. 17	-249265.89	-198.51	1047.15	-795.53
	$\sigma_{s,c}$15	-263588.72	-206.85	972.76	-888.52
	$\sigma_{cls,Max}$15	-263588.72	-206.85	972.76	-59.64
	$\sigma_{cls,Med}$15	-263588.72	-206.85	972.76	-57.74

Combinazioni Frequenti					
64	Ft. 20	-249192.78	306.79	-947.70	-793.47
	$\sigma_{s,c}$18	-258964.00	312.19	-592.11	-870.45
	$\sigma_{cls,Max}$18	-258964.00	312.19	-592.11	-58.49
	$\sigma_{cls,Med}$18	-258964.00	312.19	-592.11	-56.72
164	Ft. 20	-244842.78	-195.17	1226.44	-778.17
	$\sigma_{s,c}$18	-254614.00	-206.60	1140.30	-861.76
	$\sigma_{cls,Max}$18	-254614.00	-206.60	1140.30	-57.89
	$\sigma_{cls,Med}$18	-254614.00	-206.60	1140.30	-55.77
Combinazioni Quasi Permanenti					
64	Ft. 22	-247718.41	306.01	-1058.65	-786.83
	$\sigma_{s,c}$21	-255987.28	312.51	-721.94	-862.80
	$\sigma_{cls,Max}$21	-255987.28	312.51	-721.94	-58.01
	$\sigma_{cls,Med}$21	-255987.28	312.51	-721.94	-56.07
164	Ft. 22	-243368.41	-194.05	1286.21	-772.38
	$\sigma_{s,c}$21	-251637.28	-206.48	1194.06	-852.86
	$\sigma_{cls,Max}$21	-251637.28	-206.48	1194.06	-57.31
	$\sigma_{cls,Med}$21	-251637.28	-206.48	1194.06	-55.12

Pilastro: **164/264** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
164	1	-307621.88	151.18	7866.68	0.38
264	1	-303136.88	-425.13	-7396.60	0.37

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	167.05	61956.98	4424.14	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	167.05	46467.73	4424.14	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	167.05	61956.98	4424.14	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
164	Ft. 17	-200309.69	97.40	5076.67	-571.98
	$\sigma_{s,c}$15	-214689.28	109.29	5230.12	-794.39
	$\sigma_{cls,Max}$15	-214689.28	109.29	5230.12	-54.01
	$\sigma_{cls,Med}$15	-214689.28	109.29	5230.12	-47.02
264	Ft. 17	-196859.69	-293.83	-4763.78	-559.52
	$\sigma_{s,c}$15	-211239.28	-297.21	-4958.60	-784.59
	$\sigma_{cls,Max}$15	-211239.28	-297.21	-4958.60	-53.53
	$\sigma_{cls,Med}$15	-211239.28	-297.21	-4958.60	-46.27
Combinazioni Frequenti					
164	Ft. 20	-198318.11	90.23	4928.23	-568.10
	$\sigma_{s,c}$18	-208180.52	103.00	5018.06	-769.34
	$\sigma_{cls,Max}$18	-208180.52	103.00	5018.06	-52.30
	$\sigma_{cls,Med}$18	-208180.52	103.00	5018.06	-45.60
264	Ft. 20	-194868.11	-284.37	-4591.81	-556.09
	$\sigma_{s,c}$18	-204730.52	-286.72	-4694.31	-758.55
	$\sigma_{cls,Max}$18	-204730.52	-286.72	-4694.31	-51.73
	$\sigma_{cls,Med}$18	-204730.52	-286.72	-4694.31	-44.84
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
164	Ft. 22	-197654.27	87.84	4878.75	-566.80
	$\sigma_{s,c}$21	-206024.16	100.85	4947.96	-761.04
	$\sigma_{cls,Max}$21	-206024.16	100.85	4947.96	-51.73
	$\sigma_{cls,Med}$21	-206024.16	100.85	4947.96	-45.13
264	Ft. 22	-194204.27	-281.21	-4534.49	-554.95
	$\sigma_{s,c}$21	-202574.16	-283.17	-4606.35	-749.92
	$\sigma_{cls,Max}$21	-202574.16	-283.17	-4606.35	-51.14
	$\sigma_{cls,Med}$21	-202574.16	-283.17	-4606.35	-44.37

Pilastro: **264/364** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
264	1	-250445.05	427.61	4376.04	0.30
364	1	-245960.05	-253.90	-12535.08	0.32

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	256.74	61956.98	5242.89	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	256.74	46467.73	5242.89	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	256.74	61956.98	5242.89	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
264	Ft. 17	-158408.25	228.38	3005.28	-464.03
	$\sigma_{s,c}$15	-173548.61	295.92	3215.58	-632.21
	$\sigma_{cls,Max}$15	-173548.61	295.92	3215.58	-43.06
	$\sigma_{cls,Med}$15	-173548.61	295.92	3215.58	-38.01
364	Ft. 17	-154958.25	-38.23	-7500.09	-385.22
	$\sigma_{s,c}$15	-170098.61	-174.06	-8679.21	-706.37
	$\sigma_{cls,Max}$15	-170098.61	-174.06	-8679.21	-48.83
	$\sigma_{cls,Med}$15	-170098.61	-174.06	-8679.21	-37.26
Combinazioni Frequenti					
264	Ft. 20	-158752.11	219.81	2829.31	-468.31
	$\sigma_{s,c}$18	-169195.22	282.53	3024.69	-614.36
	$\sigma_{cls,Max}$18	-169195.22	282.53	3024.69	-41.82
	$\sigma_{cls,Med}$18	-169195.22	282.53	3024.69	-37.06
364	Ft. 20	-155302.11	-31.48	-7145.72	-392.36
	$\sigma_{s,c}$18	-165745.22	-164.92	-8068.50	-681.78
	$\sigma_{cls,Max}$18	-165745.22	-164.92	-8068.50	-47.07
	$\sigma_{cls,Med}$18	-165745.22	-164.92	-8068.50	-36.30
Combinazioni Quasi Permanenti					
264	Ft. 22	-158866.72	216.95	2770.66	-469.74
	$\sigma_{s,c}$21	-167755.89	278.10	2963.95	-608.49
	$\sigma_{cls,Max}$21	-167755.89	278.10	2963.95	-41.41
	$\sigma_{cls,Med}$21	-167755.89	278.10	2963.95	-36.74
364	Ft. 22	-155416.72	-29.23	-7027.59	-394.74
	$\sigma_{s,c}$21	-164305.89	-161.95	-7874.32	-673.78
	$\sigma_{cls,Max}$21	-164305.89	-161.95	-7874.32	-46.50

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-164305.89	-161.95	-7874.32	-35.99

Pilastro: **65/165** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
65	1	-448117.13	1221.26	8743.97	0.54
165	1	-442462.13	-1129.58	-3155.99	0.52

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	727.15	61956.98	4241.71	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	727.15	46467.73	4241.71	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	727.15	61956.98	4241.71	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
65	Ft. 17	-294485.34	818.27	5408.75	-853.04
	$\sigma_{s,c}$15	-311635.44	802.33	5565.74	-1140.45
	$\sigma_{cls,Max}$15	-311635.44	802.33	5565.74	-77.93
	$\sigma_{cls,Med}$15	-311635.44	802.33	5565.74	-68.26
165	Ft. 17	-290135.34	-752.56	-1941.66	-897.55
	$\sigma_{s,c}$15	-307285.44	-744.06	-1942.77	-1065.04
	$\sigma_{cls,Max}$15	-307285.44	-744.06	-1942.77	-72.20
	$\sigma_{cls,Med}$15	-307285.44	-744.06	-1942.77	-67.31
Combinazioni Frequenti					
65	Ft. 20	-290450.66	809.80	4842.99	-849.30
	$\sigma_{s,c}$18	-302520.41	796.79	4973.73	-1100.64
	$\sigma_{cls,Max}$18	-302520.41	796.79	4973.73	-75.17
	$\sigma_{cls,Med}$18	-302520.41	796.79	4973.73	-66.26
165	Ft. 20	-286100.66	-741.90	-1677.78	-888.94
	$\sigma_{s,c}$18	-298170.41	-732.83	-1688.66	-1030.58
	$\sigma_{cls,Max}$18	-298170.41	-732.83	-1688.66	-69.84
	$\sigma_{cls,Med}$18	-298170.41	-732.83	-1688.66	-65.31
Combinazioni Quasi Permanenti					
65	Ft. 22	-289105.78	806.98	4654.40	-848.06
	$\sigma_{s,c}$21	-299496.53	794.82	4770.88	-1087.32
	$\sigma_{cls,Max}$21	-299496.53	794.82	4770.88	-74.24
	$\sigma_{cls,Med}$21	-299496.53	794.82	4770.88	-65.60
165	Ft. 22	-284755.78	-738.35	-1589.82	-886.08
	$\sigma_{s,c}$21	-295146.53	-729.03	-1601.93	-1019.10
	$\sigma_{cls,Max}$21	-295146.53	-729.03	-1601.93	-69.06
	$\sigma_{cls,Med}$21	-295146.53	-729.03	-1601.93	-64.65

Pilastro: **165/265** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
165	1	-374895.16	-591.82	-4500.55	0.44

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
265	1	-370410.16	226.08	-2451.00	0.43

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	237.07	61956.98	649.38	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	237.07	46467.73	649.38	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	237.07	61956.98	649.38	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
165	Ft. 17	-242032.28	-376.38	-3067.80	-733.05
	$\sigma_{s,c}$15	-259249.73	-378.32	-3081.45	-914.21
	$\sigma_{cls,Max}$15	-259249.73	-378.32	-3081.45	-61.93
	$\sigma_{cls,Med}$15	-259249.73	-378.32	-3081.45	-56.78
265	Ft. 17	-238582.28	135.52	-1509.10	-754.87
	$\sigma_{s,c}$15	-255799.75	137.18	-1610.63	-871.14
	$\sigma_{cls,Max}$15	-255799.75	137.18	-1610.63	-58.52
	$\sigma_{cls,Med}$15	-255799.75	137.18	-1610.63	-56.03
Combinazioni Frequenti					
165	Ft. 20	-240576.78	-370.53	-2884.59	-731.45
	$\sigma_{s,c}$18	-252725.19	-366.49	-2895.74	-889.36
	$\sigma_{cls,Max}$18	-252725.19	-366.49	-2895.74	-60.22
	$\sigma_{cls,Med}$18	-252725.19	-366.49	-2895.74	-55.36
265	Ft. 20	-237126.78	132.08	-1587.76	-748.91
	$\sigma_{s,c}$18	-249275.19	125.77	-1660.49	-850.16
	$\sigma_{cls,Max}$18	-249275.19	125.77	-1660.49	-57.12
	$\sigma_{cls,Med}$18	-249275.19	125.77	-1660.49	-54.60
Combinazioni Quasi Permanenti					
165	Ft. 22	-240091.63	-368.58	-2823.52	-730.92
	$\sigma_{s,c}$21	-250563.11	-362.67	-2834.65	-881.13
	$\sigma_{cls,Max}$21	-250563.11	-362.67	-2834.65	-59.66
	$\sigma_{cls,Med}$21	-250563.11	-362.67	-2834.65	-54.88
265	Ft. 22	-236641.63	130.94	-1613.98	-746.93
	$\sigma_{s,c}$21	-247113.11	122.09	-1676.38	-843.20
	$\sigma_{cls,Max}$21	-247113.11	122.09	-1676.38	-56.65
	$\sigma_{cls,Med}$21	-247113.11	122.09	-1676.38	-54.13

Pilastro: **265/365** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
265	1	-307654.53	582.66	-3579.64	0.36
365	1	-303169.53	-675.08	8306.50	0.37

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	591.45	61956.98	5007.09	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	591.45	46467.73	5007.09	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	591.45	61956.98	5007.09	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
265	Ft. 17	-193561.80	381.72	-2546.21	-582.16
	$\sigma_{s,c}$15	-211083.89	386.89	-2552.94	-747.59
	$\sigma_{cls,Max}$15	-211083.89	386.89	-2552.94	-50.73
	$\sigma_{cls,Med}$15	-211083.89	386.89	-2552.94	-46.23
365	Ft. 17	-190111.80	-455.39	5986.05	-512.22
	$\sigma_{s,c}$15	-207633.89	-450.37	6059.79	-795.63
	$\sigma_{cls,Max}$15	-207633.89	-450.37	6059.79	-54.63
	$\sigma_{cls,Med}$15	-207633.89	-450.37	6059.79	-45.48
Combinazioni Frequenti					
265	Ft. 20	-194683.34	368.83	-2684.85	-583.99
	$\sigma_{s,c}$18	-207090.09	364.74	-2684.98	-735.92
	$\sigma_{cls,Max}$18	-207090.09	364.74	-2684.98	-49.95
	$\sigma_{cls,Med}$18	-207090.09	364.74	-2684.98	-45.36
365	Ft. 20	-191233.34	-442.58	6355.32	-510.27
	$\sigma_{s,c}$18	-203640.09	-428.06	6397.66	-787.33
	$\sigma_{cls,Max}$18	-203640.09	-428.06	6397.66	-54.11
	$\sigma_{cls,Med}$18	-203640.09	-428.06	6397.66	-44.60
Combinazioni Quasi Permanenti					
265	Ft. 22	-195057.20	364.54	-2731.07	-584.60
	$\sigma_{s,c}$21	-205770.00	357.27	-2731.25	-732.10
	$\sigma_{cls,Max}$21	-205770.00	357.27	-2731.25	-49.70
	$\sigma_{cls,Med}$21	-205770.00	357.27	-2731.25	-45.07
365	Ft. 22	-191607.20	-438.30	6478.41	-509.62
	$\sigma_{s,c}$21	-202320.00	-420.42	6519.38	-784.74
	$\sigma_{cls,Max}$21	-202320.00	-420.42	6519.38	-53.95
	$\sigma_{cls,Med}$21	-202320.00	-420.42	6519.38	-44.32

Pilastro: **66/166** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
66	1	-308173.97	1219.07	-3642.91	0.37
166	1	-302518.97	-952.18	2283.31	0.36

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	716.12	61956.98	6417.33	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	716.12	46467.73	6417.33	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	716.12	61956.98	6417.33	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
66	Ft. 17	-198520.77	816.78	-1980.91	-593.86
	$\sigma_{s,c}$15	-215028.95	801.96	-2586.39	-774.30
	$\sigma_{cls,Max}$15	-215028.95	801.96	-2586.39	-52.99
	$\sigma_{cls,Med}$15	-215028.95	801.96	-2586.39	-47.10
166	Ft. 17	-194170.77	-629.99	1481.42	-593.68
	$\sigma_{s,c}$15	-210678.95	-623.37	1764.84	-740.89
	$\sigma_{cls,Max}$15	-210678.95	-623.37	1764.84	-50.42

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-210678.95	-623.37	1764.84	-46.15
Combinazioni Frequenti					
66	Ft. 20	-195682.47	812.48	-2313.83	-579.22
	$\sigma_{s,c}$18	-207228.73	800.36	-2757.59	-751.42
	$\sigma_{cls,Max}$18	-207228.73	800.36	-2757.59	-51.50
	$\sigma_{cls,Med}$18	-207228.73	800.36	-2757.59	-45.39
166	Ft. 20	-191332.47	-626.89	1683.09	-581.15
	$\sigma_{s,c}$18	-202878.73	-618.98	1886.59	-717.11
	$\sigma_{cls,Max}$18	-202878.73	-618.98	1886.59	-48.85
	$\sigma_{cls,Med}$18	-202878.73	-618.98	1886.59	-44.44
Combinazioni Quasi Permanenti					
66	Ft. 22	-194736.39	811.05	-2424.80	-574.35
	$\sigma_{s,c}$21	-204627.45	799.70	-2815.02	-743.79
	$\sigma_{cls,Max}$21	-204627.45	799.70	-2815.02	-51.00
	$\sigma_{cls,Med}$21	-204627.45	799.70	-2815.02	-44.82
166	Ft. 22	-190386.39	-625.85	1750.31	-576.98
	$\sigma_{s,c}$21	-200277.45	-617.48	1926.97	-709.18
	$\sigma_{cls,Max}$21	-200277.45	-617.48	1926.97	-48.33
	$\sigma_{cls,Med}$21	-200277.45	-617.48	1926.97	-43.87

Pilastro: **166/266** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
166	1	-270244.03	-1151.91	-12955.61	0.35
266	1	-265759.03	751.88	-24.86	0.31

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	551.82	61956.98	3891.83	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	551.82	46467.73	3891.83	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	551.82	61956.98	3891.83	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
166	Ft. 17	-171193.88	-760.67	-8867.99	-393.21
	$\sigma_{s,c}$15	-187742.20	-761.11	-8801.62	-785.01
	$\sigma_{cls,Max}$15	-187742.20	-761.11	-8801.62	-54.77
	$\sigma_{cls,Med}$15	-187742.20	-761.11	-8801.62	-41.12
266	Ft. 17	-167743.88	495.00	352.84	-529.61
	$\sigma_{s,c}$15	-184292.20	499.86	88.51	-622.85
	$\sigma_{cls,Max}$15	-184292.20	499.86	88.51	-42.11
	$\sigma_{cls,Med}$15	-184292.20	499.86	88.51	-40.37
Combinazioni Frequenti					
166	Ft. 20	-169468.02	-734.49	-8243.94	-398.58
	$\sigma_{s,c}$18	-181035.73	-730.01	-8202.28	-752.18
	$\sigma_{cls,Max}$18	-181035.73	-730.01	-8202.28	-52.44
	$\sigma_{cls,Med}$18	-181035.73	-730.01	-8202.28	-39.65
266	Ft. 20	-166018.02	470.89	-255.80	-526.29

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-177585.73	467.51	-441.59	-605.56
	$\sigma_{cls,Max}$18	-177585.73	467.51	-441.59	-40.98
	$\sigma_{cls,Med}$18	-177585.73	467.51	-441.59	-38.90
Combinazioni Quasi Permanenti					
166	Ft. 22	-168892.73	-725.76	-8035.92	-400.37
	$\sigma_{s,c}$21	-178799.00	-719.71	-8003.10	-741.25
	$\sigma_{cls,Max}$21	-178799.00	-719.71	-8003.10	-51.66
	$\sigma_{cls,Med}$21	-178799.00	-719.71	-8003.10	-39.16
266	Ft. 22	-165442.73	462.85	-458.69	-521.34
	$\sigma_{s,c}$21	-175349.00	456.81	-617.51	-600.75
	$\sigma_{cls,Max}$21	-175349.00	456.81	-617.51	-40.68
	$\sigma_{cls,Med}$21	-175349.00	456.81	-617.51	-38.41

Pilastro: **266/366** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
266	1	-235894.92	-132.55	-25505.45	0.35
366	1	-231409.92	326.11	60226.18	0.51

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	393.27	61956.98	24849.75	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	393.27	46467.73	24849.75	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	393.27	61956.98	24849.75	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
266	Ft. 17	-146394.39	-89.05	-16801.96	-203.32
	$\sigma_{s,c}$15	-163003.56	-102.15	-17452.90	-824.28
	$\sigma_{cls,Max}$15	-163003.56	-102.15	-17452.90	-58.17
	$\sigma_{cls,Med}$15	-163003.56	-102.15	-17452.90	-35.70
366	Ft. 17	-142944.39	190.37	38817.94	319.80
	$\sigma_{s,c}$15	-159553.56	224.15	41101.88	-1247.73
	$\sigma_{cls,Max}$15	-159553.56	224.15	41101.88	-91.67
	$\sigma_{cls,Med}$15	-159553.56	224.15	41101.88	-45.38
Combinazioni Frequenti					
266	Ft. 20	-145652.86	-87.76	-16780.04	-201.28
	$\sigma_{s,c}$18	-157254.83	-103.29	-17244.41	-802.02
	$\sigma_{cls,Max}$18	-157254.83	-103.29	-17244.41	-56.65
	$\sigma_{cls,Med}$18	-157254.83	-103.29	-17244.41	-34.44
366	Ft. 20	-142202.86	189.80	39380.02	348.36
	$\sigma_{s,c}$18	-153804.83	220.32	41019.12	-1235.03
	$\sigma_{cls,Max}$18	-153804.83	220.32	41019.12	-90.97
	$\sigma_{cls,Med}$18	-153804.83	220.32	41019.12	-45.03
Combinazioni Quasi Permanenti					
266	Ft. 22	-145405.67	-87.33	-16772.73	-200.60
	$\sigma_{s,c}$21	-155337.23	-103.69	-17174.57	-794.59
	$\sigma_{cls,Max}$21	-155337.23	-103.69	-17174.57	-56.14

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-155337.23	-103.69	-17174.57	-34.02
366	Ft. 22	-141955.67	189.61	39567.38	358.13
	$\sigma_{s,c}$21	-151887.23	219.15	40993.05	-1231.01
	$\sigma_{cls,Max}$21	-151887.23	219.15	40993.05	-90.76
	$\sigma_{cls,Med}$21	-151887.23	219.15	40993.05	-44.93

Pilastro: **67/167** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
67	1	-437326.16	888.99	-3463.96	0.51
167	1	-431671.16	-1928.94	-592.69	0.51

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	744.62	61956.98	3487.63	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	744.62	46467.73	3487.63	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	744.62	61956.98	3487.63	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
67	Ft. 17	-295462.25	667.00	-2601.70	-906.97
	$\sigma_{s,c}$15	-305883.03	574.76	-2561.34	-1065.17
	$\sigma_{cls,Max}$15	-305883.03	574.76	-2561.34	-72.12
	$\sigma_{cls,Med}$15	-305883.03	574.76	-2561.34	-67.00
167	Ft. 17	-291112.25	-1412.36	-537.71	-902.73
	$\sigma_{s,c}$15	-301533.03	-1310.55	-544.68	-1041.29
	$\sigma_{cls,Max}$15	-301533.03	-1310.55	-544.68	-71.01
	$\sigma_{cls,Med}$15	-301533.03	-1310.55	-544.68	-66.05
Combinazioni Frequenti					
67	Ft. 20	-290408.47	652.93	-2883.62	-886.20
	$\sigma_{s,c}$18	-295611.41	569.57	-2838.22	-1035.78
	$\sigma_{cls,Max}$18	-295611.41	569.57	-2838.22	-70.21
	$\sigma_{cls,Med}$18	-295611.41	569.57	-2838.22	-64.75
167	Ft. 20	-286058.47	-1368.56	-291.83	-891.54
	$\sigma_{s,c}$18	-291261.41	-1266.31	-323.96	-1002.53
	$\sigma_{cls,Max}$18	-291261.41	-1266.31	-323.96	-68.34
	$\sigma_{cls,Med}$18	-291261.41	-1266.31	-323.96	-63.80
Combinazioni Quasi Permanenti					
67	Ft. 22	-288723.88	648.24	-2977.60	-879.28
	$\sigma_{s,c}$21	-292194.41	567.51	-2929.14	-1025.98
	$\sigma_{cls,Max}$21	-292194.41	567.51	-2929.14	-69.57
	$\sigma_{cls,Med}$21	-292194.41	567.51	-2929.14	-64.00
167	Ft. 22	-284373.88	-1353.96	-209.87	-887.81
	$\sigma_{s,c}$21	-287844.41	-1251.26	-251.01	-989.63
	$\sigma_{cls,Max}$21	-287844.41	-1251.26	-251.01	-67.45
	$\sigma_{cls,Med}$21	-287844.41	-1251.26	-251.01	-63.05

Pilastro: **167/267** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
167	1	-356779.78	2469.64	11962.46	0.45
267	1	-352294.78	-1938.06	-8171.82	0.43

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1277.59	61956.98	5836.02	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	1277.59	46467.73	5836.02	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	1277.59	61956.98	5836.02	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
167	Ft. 17	-237968.36	1748.59	8068.23	-594.25
	$\sigma_{s,c}$15	-248302.98	1740.00	8151.94	-1004.50
	$\sigma_{cls,Max}$15	-248302.98	1740.00	8151.94	-70.40
	$\sigma_{cls,Med}$15	-248302.98	1740.00	8151.94	-54.39
267	Ft. 17	-234518.36	-1260.99	-5559.02	-639.47
	$\sigma_{s,c}$15	-244852.98	-1374.42	-5586.65	-939.57
	$\sigma_{cls,Max}$15	-244852.98	-1374.42	-5586.65	-65.20
	$\sigma_{cls,Med}$15	-244852.98	-1374.42	-5586.65	-53.63
Combinazioni Frequenti					
167	Ft. 20	-235646.75	1658.30	7790.42	-594.04
	$\sigma_{s,c}$18	-240760.11	1650.32	7799.93	-971.11
	$\sigma_{cls,Max}$18	-240760.11	1650.32	7799.93	-68.01
	$\sigma_{cls,Med}$18	-240760.11	1650.32	7799.93	-52.73
267	Ft. 20	-232196.75	-1172.77	-5273.29	-639.32
	$\sigma_{s,c}$18	-237310.11	-1298.23	-5256.06	-906.96
	$\sigma_{cls,Max}$18	-237310.11	-1298.23	-5256.06	-62.88
	$\sigma_{cls,Med}$18	-237310.11	-1298.23	-5256.06	-51.98
Combinazioni Quasi Permanenti					
167	Ft. 22	-234872.89	1628.21	7697.81	-593.97
	$\sigma_{s,c}$21	-238252.00	1620.10	7682.90	-959.99
	$\sigma_{cls,Max}$21	-238252.00	1620.10	7682.90	-67.21
	$\sigma_{cls,Med}$21	-238252.00	1620.10	7682.90	-52.19
267	Ft. 22	-231422.89	-1143.37	-5178.04	-639.27
	$\sigma_{s,c}$21	-234802.00	-1272.61	-5145.80	-896.10
	$\sigma_{cls,Max}$21	-234802.00	-1272.61	-5145.80	-62.11
	$\sigma_{cls,Med}$21	-234802.00	-1272.61	-5145.80	-51.43

Pilastro: **267/367** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
267	1	-290907.09	3835.79	13372.06	0.38
367	1	-286422.09	-6416.88	-38896.68	0.48

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3529.77	61956.98	15150.37	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	3529.77	46467.73	15150.37	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	3529.77	61956.98	15150.37	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
267	Ft. 17	-190412.92	2971.19	9035.77	-383.29
	$\sigma_{s,c}$15	-201023.69	2632.82	9350.78	-897.17
	$\sigma_{cls,Max}$15	-201023.69	2632.82	9350.78	-64.48
	$\sigma_{cls,Med}$15	-201023.69	2632.82	9350.78	-44.03
367	Ft. 17	-186962.92	-5309.85	-25272.80	-28.75
	$\sigma_{s,c}$15	-197573.69	-4364.85	-26522.96	-1222.19
	$\sigma_{cls,Max}$15	-197573.69	-4364.85	-26522.96	-91.18
	$\sigma_{cls,Med}$15	-197573.69	-4364.85	-26522.96	-43.52
Combinazioni Frequenti					
267	Ft. 20	-190742.50	2911.43	8754.86	-390.87
	$\sigma_{s,c}$18	-195953.33	2537.29	8952.57	-870.96
	$\sigma_{cls,Max}$18	-195953.33	2537.29	8952.57	-62.55
	$\sigma_{cls,Med}$18	-195953.33	2537.29	8952.57	-42.92
367	Ft. 20	-187292.50	-5269.15	-24825.78	-39.20
	$\sigma_{s,c}$20	-187292.50	-5269.15	-24825.78	-1190.54
	$\sigma_{cls,Max}$20	-187292.50	-5269.15	-24825.78	-89.84
	$\sigma_{cls,Med}$18	-192503.33	-4236.70	-25440.27	-42.35
Combinazioni Quasi Permanenti					
267	Ft. 22	-190852.38	2891.51	8661.22	-393.39
	$\sigma_{s,c}$21	-194268.83	2504.93	8821.04	-862.25
	$\sigma_{cls,Max}$22	-190852.38	2891.51	8661.22	-62.22
	$\sigma_{cls,Med}$21	-194268.83	2504.93	8821.04	-42.55
367	Ft. 22	-187402.38	-5255.58	-24676.77	-42.65
	$\sigma_{s,c}$22	-187402.38	-5255.58	-24676.77	-1187.89
	$\sigma_{cls,Max}$22	-187402.38	-5255.58	-24676.77	-89.61
	$\sigma_{cls,Med}$21	-190818.83	-4192.94	-25083.26	-41.96

Pilastro: **68/168** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
68	1	-384948.84	-1298.78	11912.49	0.48
168	1	-379293.84	-4704.60	1038.82	0.47

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1095.58	61956.98	3925.31	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	1095.58	46467.73	3925.31	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	1095.58	61956.98	3925.31	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
68	Ft. 16	-259742.42	-1053.96	8045.42	-688.26

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-268901.63	-1081.53	8492.63	-1056.80
	$\sigma_{cls,Max}$15	-268901.63	-1081.53	8492.63	-73.20
	$\sigma_{cls,Med}$15	-268901.63	-1081.53	8492.63	-58.90
168	Ft. 17	-253096.59	-3344.42	716.62	-713.44
	$\sigma_{s,c}$15	-264551.63	-3182.46	618.19	-980.54
	$\sigma_{cls,Max}$15	-264551.63	-3182.46	618.19	-69.11
	$\sigma_{cls,Med}$15	-264551.63	-3182.46	618.19	-57.95
Combinazioni Frequenti					
68	Ft. 20	-252910.33	-797.88	7771.03	-678.45
	$\sigma_{s,c}$18	-259655.77	-1038.07	8029.00	-1017.46
	$\sigma_{cls,Max}$18	-259655.77	-1038.07	8029.00	-70.44
	$\sigma_{cls,Med}$18	-259655.77	-1038.07	8029.00	-56.87
168	Ft. 20	-248560.33	-3179.69	720.46	-703.71
	$\sigma_{s,c}$18	-255305.77	-3039.57	632.53	-945.85
	$\sigma_{cls,Max}$18	-255305.77	-3039.57	632.53	-66.64
	$\sigma_{cls,Med}$18	-255305.77	-3039.57	632.53	-55.92
Combinazioni Quasi Permanenti					
68	Ft. 22	-251398.23	-809.81	7667.19	-674.80
	$\sigma_{s,c}$21	-256588.25	-1026.23	7877.20	-1004.52
	$\sigma_{cls,Max}$21	-256588.25	-1026.23	7877.20	-69.54
	$\sigma_{cls,Med}$21	-256588.25	-1026.23	7877.20	-56.20
168	Ft. 22	-247048.23	-3124.78	721.74	-700.47
	$\sigma_{s,c}$21	-252238.25	-2990.26	636.56	-934.27
	$\sigma_{cls,Max}$21	-252238.25	-2990.26	636.56	-65.81
	$\sigma_{cls,Med}$21	-252238.25	-2990.26	636.56	-55.25

Pilastro: **168/268** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
168	1	-316033.34	9641.96	-7561.82	0.45
268	1	-311548.34	-7550.13	-55.24	0.42

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5034.07	61956.98	2193.08	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	5034.07	46467.73	2193.08	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	5034.07	61956.98	2193.08	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
168	Ft. 17	-208106.80	6822.63	-5384.87	-378.62
	$\sigma_{s,c}$15	-219622.27	6779.04	-5454.83	-1026.45
	$\sigma_{cls,Max}$15	-219622.27	6779.04	-5454.83	-77.14
	$\sigma_{cls,Med}$15	-219622.27	6779.04	-5454.83	-48.10
268	Ft. 17	-204656.80	-5409.63	289.88	-495.57
	$\sigma_{s,c}$15	-216172.27	-5336.24	180.23	-882.94
	$\sigma_{cls,Max}$15	-216172.27	-5336.24	180.23	-64.99
	$\sigma_{cls,Med}$15	-216172.27	-5336.24	180.23	-47.35

Combinazioni Frequenti					
168	Ft. 20	-205993.70	6484.23	-5096.62	-387.15
	$\sigma_{s,c}$18	-212790.06	6437.82	-5165.02	-988.41
	$\sigma_{cls,Max}$18	-212790.06	6437.82	-5165.02	-74.16
	$\sigma_{cls,Med}$18	-212790.06	6437.82	-5165.02	-46.61
268	Ft. 20	-202543.70	-5089.16	93.77	-502.03
	$\sigma_{s,c}$18	-209340.06	-5046.55	102.06	-850.00
	$\sigma_{cls,Max}$18	-209340.06	-5046.55	102.06	-62.45
	$\sigma_{cls,Med}$18	-209340.06	-5046.55	102.06	-45.85
Combinazioni Quasi Permanenti					
168	Ft. 22	-205289.34	6371.43	-5000.53	-390.00
	$\sigma_{s,c}$21	-210525.13	6322.96	-5068.53	-975.74
	$\sigma_{cls,Max}$21	-210525.13	6322.96	-5068.53	-73.17
	$\sigma_{cls,Med}$21	-210525.13	6322.96	-5068.53	-46.11
268	Ft. 22	-201839.34	-4982.33	28.40	-504.18
	$\sigma_{s,c}$21	-207075.13	-4948.97	75.90	-839.03
	$\sigma_{cls,Max}$21	-207075.13	-4948.97	75.90	-61.60
	$\sigma_{cls,Med}$21	-207075.13	-4948.97	75.90	-45.36

Pilastro: **268/368** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
268	1	-250394.30	12958.59	-11821.71	0.41
368	1	-245909.30	-20709.89	30280.17	0.57

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	9758.98	61956.98	12203.45	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	9758.98	46467.73	12203.45	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	9758.98	61956.98	12203.45	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
268	Ft. 17	-161022.80	8854.59	-7922.93	-117.27
	$\sigma_{s,c}$15	-172699.91	8904.78	-8090.76	-983.05
	$\sigma_{cls,Max}$15	-172699.91	8904.78	-8090.76	-77.14
	$\sigma_{cls,Med}$15	-172699.91	8904.78	-8090.76	-37.86
368	Ft. 17	-157572.80	-13914.08	20049.96	437.08
	$\sigma_{s,c}$15	-169249.91	-14092.58	20694.74	-1419.00
	$\sigma_{cls,Max}$15	-169249.91	-14092.58	20694.74	-117.02
	$\sigma_{cls,Med}$15	-169249.91	-14092.58	20694.74	-45.68
Combinazioni Frequenti					
268	Ft. 20	-161312.56	8625.86	-7798.59	-127.82
	$\sigma_{s,c}$18	-168222.58	8564.72	-7811.53	-952.94
	$\sigma_{cls,Max}$18	-168222.58	8564.72	-7811.53	-74.70
	$\sigma_{cls,Med}$18	-168222.58	8564.72	-7811.53	-36.86
368	Ft. 20	-157862.56	-13754.66	20087.64	423.80
	$\sigma_{s,c}$18	-164772.58	-13657.50	20210.72	-1379.82
	$\sigma_{cls,Max}$20	-157862.56	-13754.66	20087.64	-113.76
	$\sigma_{cls,Med}$18	-164772.58	-13657.50	20210.72	-44.40
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
268	Ft. 22	-161409.13	8549.61	-7757.15	-131.30
	$\sigma_{s,c}$21	-166740.53	8449.30	-7717.82	-942.86
	$\sigma_{cls,Max}$21	-166740.53	8449.30	-7717.82	-73.88
	$\sigma_{cls,Med}$21	-166740.53	8449.30	-7717.82	-36.53
368	Ft. 22	-157959.13	-13701.52	20100.20	419.43
	$\sigma_{s,c}$22	-157959.13	-13701.52	20100.20	-1368.93
	$\sigma_{cls,Max}$22	-157959.13	-13701.52	20100.20	-113.50
	$\sigma_{cls,Med}$21	-163290.53	-13508.70	20047.38	-43.96

Pilastro: **69/169** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
69	1	-308213.66	-715.92	3593.44	0.37
169	1	-302558.66	-4363.66	-2420.89	0.38

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1118.18	61956.98	2340.11	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	1118.18	46467.73	2340.11	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	1118.18	61956.98	2340.11	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
69	Ft. 16	-208404.58	-713.51	2237.47	-625.42
	$\sigma_{s,c}$15	-215582.53	-712.96	2439.64	-770.89
	$\sigma_{cls,Max}$15	-215582.53	-712.96	2439.64	-52.64
	$\sigma_{cls,Med}$15	-215582.53	-712.96	2439.64	-47.22
169	Ft. 17	-203891.73	-3133.69	-1884.27	-539.38
	$\sigma_{s,c}$15	-211232.53	-2910.38	-1689.12	-814.22
	$\sigma_{cls,Max}$15	-211232.53	-2910.38	-1689.12	-57.90
	$\sigma_{cls,Med}$15	-211232.53	-2910.38	-1689.12	-46.27
Combinazioni Frequenti					
69	Ft. 20	-204783.53	-399.16	2622.63	-617.22
	$\sigma_{s,c}$18	-208327.08	-696.16	2236.98	-743.20
	$\sigma_{cls,Max}$18	-208327.08	-696.16	2236.98	-50.74
	$\sigma_{cls,Med}$18	-208327.08	-696.16	2236.98	-45.63
169	Ft. 20	-200433.53	-2973.10	-1752.53	-535.28
	$\sigma_{s,c}$18	-203977.08	-2775.89	-1569.03	-784.14
	$\sigma_{cls,Max}$20	-200433.53	-2973.10	-1752.53	-55.82
	$\sigma_{cls,Med}$18	-203977.08	-2775.89	-1569.03	-44.68
Combinazioni Quasi Permanenti					
69	Ft. 22	-203630.80	-420.19	2552.41	-613.92
	$\sigma_{s,c}$21	-205921.50	-693.46	2169.51	-734.11
	$\sigma_{cls,Max}$21	-205921.50	-693.46	2169.51	-50.12
	$\sigma_{cls,Med}$21	-205921.50	-693.46	2169.51	-45.10
169	Ft. 22	-199280.80	-2919.57	-1708.62	-533.92
	$\sigma_{s,c}$22	-199280.80	-2919.57	-1708.62	-775.57
	$\sigma_{cls,Max}$22	-199280.80	-2919.57	-1708.62	-55.34

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-201571.50	-2729.31	-1529.18	-44.15

Pilastro: **169/269** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
169	1	-253073.00	7985.13	345.03	0.36
269	1	-248588.00	-6478.62	-3185.49	0.34

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4253.08	61956.98	1023.34	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	4253.08	46467.73	1023.34	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	4253.08	61956.98	1023.34	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
169	Ft. 17	-168962.83	5700.42	207.37	-370.40
	$\sigma_{s,c}$15	-176111.17	5613.92	232.57	-761.01
	$\sigma_{cls,Max}$15	-176111.17	5613.92	232.57	-57.19
	$\sigma_{cls,Med}$15	-176111.17	5613.92	232.57	-38.57
269	Ft. 17	-165512.83	-4629.44	-1949.64	-364.63
	$\sigma_{s,c}$15	-172661.17	-4576.35	-2155.28	-748.12
	$\sigma_{cls,Max}$15	-172661.17	-4576.35	-2155.28	-55.48
	$\sigma_{cls,Med}$15	-172661.17	-4576.35	-2155.28	-37.82
Combinazioni Frequenti					
169	Ft. 20	-167313.36	5405.36	216.17	-374.22
	$\sigma_{s,c}$18	-170697.27	5324.30	231.80	-734.00
	$\sigma_{cls,Max}$18	-170697.27	5324.30	231.80	-55.05
	$\sigma_{cls,Med}$18	-170697.27	5324.30	231.80	-37.39
269	Ft. 20	-163863.36	-4350.49	-1896.46	-368.96
	$\sigma_{s,c}$18	-167247.27	-4328.49	-2066.80	-721.00
	$\sigma_{cls,Max}$18	-167247.27	-4328.49	-2066.80	-53.38
	$\sigma_{cls,Med}$18	-167247.27	-4328.49	-2066.80	-36.63
Combinazioni Quasi Permanenti					
169	Ft. 22	-166763.52	5307.01	219.10	-375.49
	$\sigma_{s,c}$21	-168903.50	5226.40	231.56	-724.99
	$\sigma_{cls,Max}$21	-168903.50	5226.40	231.56	-54.34
	$\sigma_{cls,Med}$21	-168903.50	5226.40	231.56	-37.00
269	Ft. 22	-163313.52	-4257.50	-1878.73	-370.40
	$\sigma_{s,c}$21	-165453.50	-4244.47	-2037.10	-711.95
	$\sigma_{cls,Max}$21	-165453.50	-4244.47	-2037.10	-52.67
	$\sigma_{cls,Med}$21	-165453.50	-4244.47	-2037.10	-36.24

Pilastro: **269/369** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
269	1	-200149.95	11582.95	-1250.81	0.33

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
369	1	-195664.95	-18252.96	5146.53	0.42

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	8857.60	61956.98	1854.30	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	8857.60	46467.73	1854.30	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	8857.60	61956.98	1854.30	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
269	Ft. 17	-131248.86	8072.32	-335.13	-168.94
	$\sigma_{s,c}$15	-138302.86	7930.50	-800.46	-719.78
	$\sigma_{cls,Max}$15	-138302.86	7930.50	-800.46	-57.18
	$\sigma_{cls,Med}$15	-138302.86	7930.50	-800.46	-30.29
369	Ft. 17	-127798.85	-12713.64	1885.82	102.13
	$\sigma_{s,c}$15	-134852.86	-12373.59	3506.67	-916.54
	$\sigma_{cls,Max}$15	-134852.86	-12373.59	3506.67	-77.06
	$\sigma_{cls,Med}$17	-127798.85	-12713.64	1885.82	-36.30
Combinazioni Frequenti					
269	Ft. 20	-131393.53	7849.47	-377.61	-175.81
	$\sigma_{s,c}$18	-134680.61	7609.65	-796.05	-697.60
	$\sigma_{cls,Max}$18	-134680.61	7609.65	-796.05	-55.34
	$\sigma_{cls,Med}$18	-134680.61	7609.65	-796.05	-29.50
369	Ft. 20	-127943.53	-12526.40	1955.00	88.70
	$\sigma_{s,c}$18	-131230.61	-11956.92	3463.07	-889.37
	$\sigma_{cls,Max}$20	-127943.53	-12526.40	1955.00	-74.70
	$\sigma_{cls,Med}$20	-127943.53	-12526.40	1955.00	-35.86
Combinazioni Quasi Permanenti					
269	Ft. 22	-131441.77	7775.19	-391.77	-178.10
	$\sigma_{s,c}$21	-133481.58	7500.66	-794.11	-690.16
	$\sigma_{cls,Max}$21	-133481.58	7500.66	-794.11	-54.72
	$\sigma_{cls,Med}$21	-133481.58	7500.66	-794.11	-29.24
369	Ft. 22	-127991.77	-12463.99	1978.06	84.33
	$\sigma_{s,c}$21	-130031.57	-11814.40	3447.49	-880.17
	$\sigma_{cls,Max}$22	-127991.77	-12463.99	1978.06	-74.44
	$\sigma_{cls,Med}$22	-127991.77	-12463.99	1978.06	-35.72

Pilastro: **70/170** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
70	1	-380995.94	614.61	-4700.02	0.45
170	1	-375340.94	-4662.80	-5043.82	0.47

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1463.71	61956.98	3060.67	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	1463.71	46467.73	3060.67	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	1463.71	61956.98	3060.67	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
70	Ft. 16	-257314.88	171.75	-3654.63	-780.17
	$\sigma_{s,c}$15	-265486.50	208.65	-3567.84	-937.26
	$\sigma_{cls,Max}$15	-265486.50	208.65	-3567.84	-63.36
	$\sigma_{cls,Med}$15	-265486.50	208.65	-3567.84	-58.15
170	Ft. 17	-256000.58	-3378.60	-3524.40	-675.97
	$\sigma_{s,c}$15	-261136.50	-3102.28	-3396.08	-1012.21
	$\sigma_{cls,Max}$15	-261136.50	-3102.28	-3396.08	-71.63
	$\sigma_{cls,Med}$15	-261136.50	-3102.28	-3396.08	-57.20
Combinazioni Frequenti					
70	Ft. 19	-254498.70	174.96	-3670.24	-770.56
	$\sigma_{s,c}$20	-256526.88	526.13	-3342.90	-914.24
	$\sigma_{cls,Max}$20	-256526.88	526.13	-3342.90	-62.14
	$\sigma_{cls,Med}$18	-257219.39	187.79	-3640.85	-56.34
170	Ft. 20	-252176.88	-3220.75	-3274.97	-672.50
	$\sigma_{s,c}$20	-252176.88	-3220.75	-3274.97	-984.56
	$\sigma_{cls,Max}$20	-252176.88	-3220.75	-3274.97	-69.90
	$\sigma_{cls,Med}$18	-252869.39	-2966.09	-3178.65	-55.39
Combinazioni Quasi Permanenti					
70	Ft. 22	-255252.30	496.49	-3422.33	-766.86
	$\sigma_{s,c}$22	-255252.30	496.49	-3422.33	-910.41
	$\sigma_{cls,Max}$22	-255252.30	496.49	-3422.33	-61.87
	$\sigma_{cls,Med}$22	-255252.30	496.49	-3422.33	-55.91
170	Ft. 22	-250902.30	-3168.13	-3191.83	-671.35
	$\sigma_{s,c}$22	-250902.30	-3168.13	-3191.83	-977.34
	$\sigma_{cls,Max}$22	-250902.30	-3168.13	-3191.83	-69.34
	$\sigma_{cls,Med}$22	-250902.30	-3168.13	-3191.83	-54.96

Pilastro: **170/270** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
170	1	-319726.59	6612.25	5370.86	0.42
270	1	-315241.59	-5235.26	-182.42	0.40

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3488.62	61956.98	1619.56	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	3488.62	46467.73	1619.56	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	3488.62	61956.98	1619.56	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
170	Ft. 17	-216835.86	4765.89	3774.73	-499.06
	$\sigma_{s,c}$15	-221608.69	4650.20	3837.28	-938.80
	$\sigma_{cls,Max}$15	-221608.69	4650.20	3837.28	-68.58
	$\sigma_{cls,Med}$15	-221608.69	4650.20	3837.28	-48.54
270	Ft. 17	-213385.86	-3712.18	-306.97	-577.97
	$\sigma_{s,c}$15	-218158.69	-3702.37	-221.61	-838.17
	$\sigma_{cls,Max}$15	-218158.69	-3702.37	-221.61	-60.15

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-218158.69	-3702.37	-221.61	-47.78
Combinazioni Frequenti					
170	Ft. 20	-215089.17	4515.03	3651.38	-503.32
	$\sigma_{s,c}$20	-215089.17	4515.03	3651.38	-910.04
	$\sigma_{cls,Max}$20	-215089.17	4515.03	3651.38	-66.47
	$\sigma_{cls,Med}$18	-215437.34	4408.89	3680.68	-47.19
270	Ft. 19	-209960.61	-3427.52	-66.69	-579.70
	$\sigma_{s,c}$18	-211987.34	-3498.20	-106.49	-809.52
	$\sigma_{cls,Max}$18	-211987.34	-3498.20	-106.49	-57.98
	$\sigma_{cls,Med}$18	-211987.34	-3498.20	-106.49	-46.43
Combinazioni Quasi Permanenti					
170	Ft. 21	-213394.02	4327.11	3628.29	-504.11
	$\sigma_{s,c}$22	-214506.91	4431.41	3610.26	-904.79
	$\sigma_{cls,Max}$22	-214506.91	4431.41	3610.26	-66.02
	$\sigma_{cls,Med}$22	-214506.91	4431.41	3610.26	-46.98
270	Ft. 21	-209944.02	-3428.95	-67.47	-579.59
	$\sigma_{s,c}$22	-211056.91	-3396.63	-86.65	-802.90
	$\sigma_{cls,Max}$22	-211056.91	-3396.63	-86.65	-57.42
	$\sigma_{cls,Med}$22	-211056.91	-3396.63	-86.65	-46.23

Pilastro: **270/370** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
270	1	-261810.33	11443.51	12125.14	0.41
370	3	-250714.56	-20426.36	-41101.14	0.62

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	9428.34	61956.98	15663.24	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	9428.34	46467.73	15663.24	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	9428.34	61956.98	15663.24	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
270	Ft. 17	-175752.61	8240.40	8246.67	-180.40
	$\sigma_{s,c}$15	-180159.77	7801.79	8330.44	-976.37
	$\sigma_{cls,Max}$17	-175752.61	8240.40	8246.67	-75.84
	$\sigma_{cls,Med}$15	-180159.77	7801.79	8330.44	-39.46
370	Ft. 17	-172302.61	-13800.44	-27921.22	552.82
	$\sigma_{s,c}$17	-172302.61	-13800.44	-27921.22	-1572.41
	$\sigma_{cls,Max}$17	-172302.61	-13800.44	-27921.22	-129.30
	$\sigma_{cls,Med}$17	-172302.61	-13800.44	-27921.22	-48.42
Combinazioni Frequenti					
270	Ft. 20	-176069.20	8025.06	8056.26	-191.41
	$\sigma_{s,c}$20	-176069.20	8025.06	8056.26	-965.55
	$\sigma_{cls,Max}$20	-176069.20	8025.06	8056.26	-74.96
	$\sigma_{cls,Med}$20	-176069.20	8025.06	8056.26	-38.57
370	Ft. 20	-172619.20	-13593.53	-27663.79	526.85

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$20	-172619.20	-13593.53	-27663.79	-1556.34
	$\sigma_{cls,Max}$20	-172619.20	-13593.53	-27663.79	-127.71
	$\sigma_{cls,Med}$20	-172619.20	-13593.53	-27663.79	-48.03
Combinazioni Quasi Permanenti					
270	Ft. 22	-176174.73	7953.29	7992.79	-195.08
	$\sigma_{s,c}$22	-176174.73	7953.29	7992.79	-962.58
	$\sigma_{cls,Max}$22	-176174.73	7953.29	7992.79	-74.67
	$\sigma_{cls,Med}$22	-176174.73	7953.29	7992.79	-38.59
370	Ft. 22	-172724.73	-13524.56	-27577.98	518.31
	$\sigma_{s,c}$22	-172724.73	-13524.56	-27577.98	-1551.02
	$\sigma_{cls,Max}$22	-172724.73	-13524.56	-27577.98	-127.18
	$\sigma_{cls,Med}$22	-172724.73	-13524.56	-27577.98	-47.90

Pilastro: **71/171** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
71	1	-509076.22	1958.98	10278.25	0.62
171	1	-503421.22	-2735.51	-1355.32	0.60

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1215.73	61956.98	3665.40	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	1215.73	46467.73	3665.40	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	1215.73	61956.98	3665.40	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
71	Ft. 17	-341389.56	1381.32	6342.71	-973.95
	$\sigma_{s,c}$15	-353383.88	1270.82	6931.21	-1314.85
	$\sigma_{cls,Max}$15	-353383.88	1270.82	6931.21	-90.34
	$\sigma_{cls,Med}$15	-353383.88	1270.82	6931.21	-77.40
171	Ft. 17	-337039.56	-1938.75	-568.54	-1036.38
	$\sigma_{s,c}$15	-349033.88	-1827.66	-797.04	-1217.94
	$\sigma_{cls,Max}$15	-349033.88	-1827.66	-797.04	-83.42
	$\sigma_{cls,Med}$15	-349033.88	-1827.66	-797.04	-76.45
Combinazioni Frequenti					
71	Ft. 20	-336600.34	1344.41	5917.90	-966.34
	$\sigma_{s,c}$18	-343024.22	1246.18	6414.14	-1271.57
	$\sigma_{cls,Max}$18	-343024.22	1246.18	6414.14	-87.33
	$\sigma_{cls,Med}$18	-343024.22	1246.18	6414.14	-75.13
171	Ft. 20	-332250.34	-1881.19	-426.48	-1024.79
	$\sigma_{s,c}$18	-338674.22	-1772.88	-648.54	-1179.73
	$\sigma_{cls,Max}$18	-338674.22	-1772.88	-648.54	-80.79
	$\sigma_{cls,Med}$18	-338674.22	-1772.88	-648.54	-74.18
Combinazioni Quasi Permanenti					
71	Ft. 22	-335003.91	1332.11	5776.29	-963.80
	$\sigma_{s,c}$21	-339577.44	1237.58	6240.42	-1257.13
	$\sigma_{cls,Max}$21	-339577.44	1237.58	6240.42	-86.33

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-339577.44	1237.58	6240.42	-74.38
171	Ft. 22	-330653.91	-1862.00	-379.13	-1020.93
	$\sigma_{s,c}$21	-335227.44	-1754.30	-598.65	-1167.00
	$\sigma_{cls,Max}$21	-335227.44	-1754.30	-598.65	-79.91
	$\sigma_{cls,Med}$21	-335227.44	-1754.30	-598.65	-73.43

Pilastro: **171/271** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
171	1	-429776.75	393.60	-9128.34	0.52
271	1	-425291.75	-568.19	-2050.35	0.49

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	360.44	61956.98	2051.59	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	360.44	46467.73	2051.59	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	360.44	61956.98	2051.59	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
171	Ft. 17	-284702.88	410.18	-6249.40	-820.13
	$\sigma_{s,c}$15	-296696.50	349.55	-6319.60	-1089.29
	$\sigma_{cls,Max}$15	-296696.50	349.55	-6319.60	-74.14
	$\sigma_{cls,Med}$15	-296696.50	349.55	-6319.60	-64.99
271	Ft. 17	-281252.88	-407.22	-1406.52	-888.10
	$\sigma_{s,c}$15	-293246.50	-456.44	-1252.87	-998.48
	$\sigma_{cls,Max}$15	-293246.50	-456.44	-1252.87	-67.31
	$\sigma_{cls,Med}$15	-293246.50	-456.44	-1252.87	-64.23
Combinazioni Frequenti					
171	Ft. 20	-282807.34	354.14	-5940.35	-820.74
	$\sigma_{s,c}$18	-289200.81	313.81	-5988.64	-1058.11
	$\sigma_{cls,Max}$18	-289200.81	313.81	-5988.64	-71.96
	$\sigma_{cls,Med}$18	-289200.81	313.81	-5988.64	-63.35
271	Ft. 20	-279357.34	-350.70	-1563.44	-881.10
	$\sigma_{s,c}$18	-285750.81	-426.55	-1352.58	-974.53
	$\sigma_{cls,Max}$18	-285750.81	-426.55	-1352.58	-65.70
	$\sigma_{cls,Med}$18	-285750.81	-426.55	-1352.58	-62.59
Combinazioni Quasi Permanenti					
171	Ft. 22	-282175.56	335.46	-5837.33	-820.94
	$\sigma_{s,c}$21	-286708.09	301.41	-5878.97	-1047.74
	$\sigma_{cls,Max}$21	-286708.09	301.41	-5878.97	-71.24
	$\sigma_{cls,Med}$21	-286708.09	301.41	-5878.97	-62.80
271	Ft. 22	-278725.56	-331.86	-1615.75	-878.77
	$\sigma_{s,c}$21	-283258.09	-416.18	-1385.27	-966.55
	$\sigma_{cls,Max}$21	-283258.09	-416.18	-1385.27	-65.16
	$\sigma_{cls,Med}$21	-283258.09	-416.18	-1385.27	-62.04

Pilastro: **271/371** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
271	1	-354078.31	3137.69	-13393.12	0.45
371	1	-349593.31	-4626.15	39948.34	0.54

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	2810.84	61956.98	16240.43	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	2810.84	46467.73	16240.43	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	2810.84	61956.98	16240.43	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
271	Ft. 17	-230554.20	2491.18	-9573.71	-521.64
	$\sigma_{s,c}$15	-242559.72	2141.60	-9182.97	-1015.27
	$\sigma_{cls,Max}$15	-242559.72	2141.60	-9182.97	-71.76
	$\sigma_{cls,Med}$15	-242559.72	2141.60	-9182.97	-53.13
371	Ft. 17	-227104.20	-4079.91	28701.86	-146.89
	$\sigma_{s,c}$17	-227104.20	-4079.91	28701.86	-1345.42
	$\sigma_{cls,Max}$17	-227104.20	-4079.91	28701.86	-99.45
	$\sigma_{cls,Med}$15	-239109.72	-3140.45	27300.58	-52.37
Combinazioni Frequenti					
271	Ft. 20	-231541.98	2430.77	-9517.79	-527.73
	$\sigma_{s,c}$18	-237897.14	2057.48	-9037.21	-994.89
	$\sigma_{cls,Max}$20	-231541.98	2430.77	-9517.79	-70.72
	$\sigma_{cls,Med}$18	-237897.14	2057.48	-9037.21	-52.11
371	Ft. 20	-228091.98	-4031.48	28675.87	-152.10
	$\sigma_{s,c}$20	-228091.98	-4031.48	28675.87	-1346.70
	$\sigma_{cls,Max}$20	-228091.98	-4031.48	28675.87	-99.47
	$\sigma_{cls,Med}$18	-234447.14	-3048.12	26901.53	-51.35
Combinazioni Quasi Permanenti					
271	Ft. 22	-231871.25	2410.64	-9499.15	-529.75
	$\sigma_{s,c}$22	-231871.25	2410.64	-9499.15	-993.88
	$\sigma_{cls,Max}$22	-231871.25	2410.64	-9499.15	-70.70
	$\sigma_{cls,Med}$21	-236348.08	2028.87	-8989.18	-51.77
371	Ft. 22	-228421.25	-4015.33	28667.20	-153.84
	$\sigma_{s,c}$22	-228421.25	-4015.33	28667.20	-1347.13
	$\sigma_{cls,Max}$22	-228421.25	-4015.33	28667.20	-99.48
	$\sigma_{cls,Med}$21	-232898.08	-3016.15	26771.93	-51.01

Pilastro: **72/172** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
72	1	-288368.44	1649.03	-7908.00	0.36
172	1	-282713.44	-1701.08	3961.53	0.34

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	935.60	61956.98	6559.90	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	935.60	46467.73	6559.90	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	935.60	61956.98	6559.90	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
72	Ft. 17	-187353.86	1125.66	-5176.93	-495.07
	$\sigma_{s,c}$15	-202190.89	1081.86	-5440.92	-787.72
	$\sigma_{cls,Max}$15	-202190.89	1081.86	-5440.92	-54.72
	$\sigma_{cls,Med}$15	-202190.89	1081.86	-5440.92	-44.29
172	Ft. 17	-183003.86	-1159.55	2764.94	-519.15
	$\sigma_{s,c}$15	-197840.89	-1129.50	2889.97	-733.21
	$\sigma_{cls,Max}$15	-197840.89	-1129.50	2889.97	-50.68
	$\sigma_{cls,Med}$15	-197840.89	-1129.50	2889.97	-43.33
Combinazioni Frequenti					
72	Ft. 20	-185068.56	1110.41	-5383.08	-484.67
	$\sigma_{s,c}$18	-195399.53	1073.49	-5460.59	-765.46
	$\sigma_{cls,Max}$18	-195399.53	1073.49	-5460.59	-53.23
	$\sigma_{cls,Med}$18	-195399.53	1073.49	-5460.59	-42.80
172	Ft. 20	-180718.56	-1140.85	2894.45	-510.12
	$\sigma_{s,c}$18	-191049.53	-1110.31	2933.73	-711.01
	$\sigma_{cls,Max}$18	-191049.53	-1110.31	2933.73	-49.19
	$\sigma_{cls,Med}$18	-191049.53	-1110.31	2933.73	-41.85
Combinazioni Quasi Permanenti					
72	Ft. 22	-184306.78	1105.32	-5451.79	-481.21
	$\sigma_{s,c}$21	-193134.81	1070.65	-5467.02	-758.03
	$\sigma_{cls,Max}$21	-193134.81	1070.65	-5467.02	-52.73
	$\sigma_{cls,Med}$21	-193134.81	1070.65	-5467.02	-42.30
172	Ft. 22	-179956.78	-1134.62	2937.62	-507.11
	$\sigma_{s,c}$21	-188784.81	-1103.96	2947.97	-703.60
	$\sigma_{cls,Max}$21	-188784.81	-1103.96	2947.97	-48.69
	$\sigma_{cls,Med}$21	-188784.81	-1103.96	2947.97	-41.35

Pilastro: **172/272** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
172	1	-249188.97	-1325.54	-13074.79	0.33
272	1	-244703.97	386.12	118.58	0.28

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	496.13	61956.98	3931.22	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	496.13	46467.73	3931.22	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	496.13	61956.98	3931.22	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
172	Ft. 17	-159120.20	-823.49	-8940.67	-350.35

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-174065.03	-844.79	-8878.70	-744.00
	$\sigma_{cls,Max}$15	-174065.03	-844.79	-8878.70	-52.14
	$\sigma_{cls,Med}$15	-174065.03	-844.79	-8878.70	-38.13
272	Ft. 17	-155670.20	231.66	374.87	-497.96
	$\sigma_{s,c}$15	-170615.03	231.78	190.62	-571.05
	$\sigma_{cls,Max}$15	-170615.03	231.78	190.62	-38.37
	$\sigma_{cls,Med}$15	-170615.03	231.78	190.62	-37.37
Combinazioni Frequenti					
172	Ft. 20	-157956.98	-807.93	-8335.46	-356.93
	$\sigma_{s,c}$18	-168394.19	-816.97	-8292.07	-714.89
	$\sigma_{cls,Max}$18	-168394.19	-816.97	-8292.07	-50.06
	$\sigma_{cls,Med}$18	-168394.19	-816.97	-8292.07	-36.88
272	Ft. 20	-154506.98	227.78	-162.42	-497.73
	$\sigma_{s,c}$18	-164944.19	215.13	-270.30	-553.19
	$\sigma_{cls,Max}$18	-164944.19	215.13	-270.30	-37.17
	$\sigma_{cls,Med}$18	-164944.19	215.13	-270.30	-36.13
Combinazioni Quasi Permanenti					
172	Ft. 22	-157569.23	-802.74	-8133.73	-359.12
	$\sigma_{s,c}$21	-166503.06	-807.81	-8096.97	-705.19
	$\sigma_{cls,Max}$21	-166503.06	-807.81	-8096.97	-49.37
	$\sigma_{cls,Med}$21	-166503.06	-807.81	-8096.97	-36.47
272	Ft. 22	-154119.23	226.49	-341.52	-493.57
	$\sigma_{s,c}$21	-163053.06	209.73	-423.36	-549.31
	$\sigma_{cls,Max}$21	-163053.06	209.73	-423.36	-36.94
	$\sigma_{cls,Med}$21	-163053.06	209.73	-423.36	-35.71

Pilastro: **272/372** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
272	1	-212924.81	-249.94	-27238.68	0.33
372	1	-208439.83	1969.15	68114.13	0.55

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	643.21	61956.98	27638.49	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	643.21	46467.73	27638.49	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	643.21	61956.98	27638.49	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
272	Ft. 17	-132938.33	-90.33	-18238.09	-135.58
	$\sigma_{s,c}$15	-148048.13	-159.51	-18607.24	-795.85
	$\sigma_{cls,Max}$15	-148048.13	-159.51	-18607.24	-56.54
	$\sigma_{cls,Med}$15	-148048.13	-159.51	-18607.24	-32.43
372	Ft. 17	-129488.31	1088.08	44985.06	810.58
	$\sigma_{s,c}$15	-144598.13	1291.23	46344.25	-1402.63
	$\sigma_{cls,Max}$15	-144598.13	1291.23	46344.25	-106.37
	$\sigma_{cls,Med}$15	-144598.13	1291.23	46344.25	-50.23

Combinazioni Frequenti					
272	Ft. 20	-132794.25	-85.86	-18101.10	-137.49
	$\sigma_{s,c}$18	-143390.72	-150.60	-18269.57	-774.74
	$\sigma_{cls,Max}$18	-143390.72	-150.60	-18269.57	-55.06
	$\sigma_{cls,Med}$18	-143390.72	-150.60	-18269.57	-31.41
372	Ft. 20	-129344.23	1050.82	45246.58	825.80
	$\sigma_{s,c}$18	-139940.70	1220.06	45883.27	-1383.49
	$\sigma_{cls,Max}$18	-139940.70	1220.06	45883.27	-105.09
	$\sigma_{cls,Med}$18	-139940.70	1220.06	45883.27	-49.71
Combinazioni Quasi Permanenti					
272	Ft. 22	-132746.20	-84.37	-18055.44	-138.12
	$\sigma_{s,c}$21	-141837.44	-147.53	-18156.57	-767.69
	$\sigma_{cls,Max}$21	-141837.44	-147.53	-18156.57	-54.57
	$\sigma_{cls,Med}$21	-141837.44	-147.53	-18156.57	-31.07
372	Ft. 22	-129296.21	1038.40	45333.76	830.90
	$\sigma_{s,c}$21	-138387.45	1196.38	45729.86	-1377.17
	$\sigma_{cls,Max}$21	-138387.45	1196.38	45729.86	-104.68
	$\sigma_{cls,Med}$21	-138387.45	1196.38	45729.86	-49.54

Pilastro: **73/173** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
73	1	-395720.75	1440.81	-4449.17	0.47
173	1	-390065.75	2409.29	-1242.77	0.47

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	631.61	61956.98	3056.09	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	631.61	46467.73	3056.09	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	631.61	61956.98	3056.09	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
73	Ft. 16	-267541.19	987.39	-3575.89	-789.11
	$\sigma_{s,c}$15	-276770.41	972.22	-3398.88	-995.86
	$\sigma_{cls,Max}$15	-276770.41	972.22	-3398.88	-68.10
	$\sigma_{cls,Med}$15	-276770.41	972.22	-3398.88	-60.62
173	Ft. 16	-263191.19	1615.06	-702.93	-801.84
	$\sigma_{s,c}$15	-272420.38	1734.87	-899.73	-964.95
	$\sigma_{cls,Max}$15	-272420.38	1734.87	-899.73	-66.47
	$\sigma_{cls,Med}$15	-272420.38	1734.87	-899.73	-59.67
Combinazioni Frequenti					
73	Ft. 19	-264463.56	992.39	-3633.54	-777.90
	$\sigma_{s,c}$20	-271981.19	998.15	-3344.71	-980.06
	$\sigma_{cls,Max}$20	-271981.19	998.15	-3344.71	-67.07
	$\sigma_{cls,Med}$20	-271981.19	998.15	-3344.71	-59.57
173	Ft. 19	-260113.64	1575.21	-638.08	-794.06
	$\sigma_{s,c}$20	-267631.19	1611.61	-718.72	-942.33
	$\sigma_{cls,Max}$20	-267631.19	1611.61	-718.72	-64.79
	$\sigma_{cls,Med}$20	-267631.19	1611.61	-718.72	-58.62
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
73	Ft. 21	-264463.31	992.38	-3633.25	-777.90
	$\sigma_{s,c}$22	-270462.38	1008.63	-3413.03	-976.52
	$\sigma_{cls,Max}$22	-270462.38	1008.63	-3413.03	-66.86
	$\sigma_{cls,Med}$22	-270462.38	1008.63	-3413.03	-59.24
173	Ft. 21	-260113.39	1575.23	-638.23	-794.06
	$\sigma_{s,c}$22	-266112.38	1573.50	-648.80	-934.99
	$\sigma_{cls,Max}$22	-266112.38	1573.50	-648.80	-64.24
	$\sigma_{cls,Med}$22	-266112.38	1573.50	-648.80	-58.29

Pilastro: **173/273** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
173	3	-325398.22	-6781.43	12795.21	0.44
273	1	-320423.78	4677.05	-6287.99	0.41

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3338.82	61956.98	5528.59	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	3338.82	46467.73	5528.59	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	3338.82	61956.98	5528.59	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
173	Ft. 16	-219263.27	-4565.49	8354.88	-438.49
	$\sigma_{s,c}$17	-226428.73	-4755.60	8792.10	-1039.03
	$\sigma_{cls,Max}$17	-226428.73	-4755.60	8792.10	-76.26
	$\sigma_{cls,Med}$17	-226428.73	-4755.60	8792.10	-49.60
273	Ft. 16	-215813.27	3118.46	-4054.93	-543.53
	$\sigma_{s,c}$15	-222652.42	3305.72	-4353.55	-907.90
	$\sigma_{cls,Max}$15	-222652.42	3305.72	-4353.55	-65.07
	$\sigma_{cls,Med}$17	-222978.73	3254.92	-4347.18	-48.84
Combinazioni Frequenti					
173	Ft. 19	-216982.75	-4488.42	8231.13	-435.48
	$\sigma_{s,c}$20	-224281.98	-4541.71	8480.63	-1020.08
	$\sigma_{cls,Max}$20	-224281.98	-4541.71	8480.63	-74.70
	$\sigma_{cls,Med}$20	-224281.98	-4541.71	8480.63	-49.13
273	Ft. 19	-213532.75	3055.65	-3955.16	-539.66
	$\sigma_{s,c}$20	-220831.98	3059.77	-4042.76	-889.01
	$\sigma_{cls,Max}$20	-220831.98	3059.77	-4042.76	-63.48
	$\sigma_{cls,Med}$20	-220831.98	3059.77	-4042.76	-48.37
Combinazioni Quasi Permanenti					
173	Ft. 21	-216982.59	-4488.36	8231.12	-435.48
	$\sigma_{s,c}$22	-223566.38	-4470.42	8376.80	-1013.77
	$\sigma_{cls,Max}$22	-223566.38	-4470.42	8376.80	-74.18
	$\sigma_{cls,Med}$22	-223566.38	-4470.42	8376.80	-48.97
273	Ft. 21	-213532.59	3055.57	-3955.11	-539.67
	$\sigma_{s,c}$22	-220116.38	2994.72	-3941.28	-882.93
	$\sigma_{cls,Max}$22	-220116.38	2994.72	-3941.28	-62.98

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$22	-220116.38	2994.72	-3941.28	-48.21

Pilastro: **273/373** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
273	3	-266803.50	-6783.44	15926.77	0.38
373	3	-262318.50	11342.64	-48037.15	0.55

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5253.94	61956.98	18540.27	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	5253.94	46467.73	18540.27	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	5253.94	61956.98	18540.27	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
273	Ft. 16	-178790.64	-4516.61	10588.60	-270.54
	$\sigma_{s,c}$17	-184320.97	-4729.05	11015.68	-936.22
	$\sigma_{cls,Max}$17	-184320.97	-4729.05	11015.68	-69.77
	$\sigma_{cls,Med}$17	-184320.97	-4729.05	11015.68	-40.37
373	Ft. 17	-180870.97	7808.71	-32612.28	259.20
	$\sigma_{s,c}$17	-180870.97	7808.71	-32612.28	-1415.00
	$\sigma_{cls,Max}$17	-180870.97	7808.71	-32612.28	-110.20
	$\sigma_{cls,Med}$17	-180870.97	7808.71	-32612.28	-44.82
Combinazioni Frequenti					
273	Ft. 19	-177241.61	-4449.40	10449.42	-269.86
	$\sigma_{s,c}$20	-184517.41	-4579.97	10750.21	-927.78
	$\sigma_{cls,Max}$20	-184517.41	-4579.97	10750.21	-68.99
	$\sigma_{cls,Med}$20	-184517.41	-4579.97	10750.21	-40.42
373	Ft. 20	-181067.41	7713.72	-32227.11	243.63
	$\sigma_{s,c}$20	-181067.41	7713.72	-32227.11	-1403.45
	$\sigma_{cls,Max}$20	-181067.41	7713.72	-32227.11	-109.16
	$\sigma_{cls,Med}$20	-181067.41	7713.72	-32227.11	-44.59
Combinazioni Quasi Permanenti					
273	Ft. 21	-177241.53	-4449.46	10449.58	-269.86
	$\sigma_{s,c}$22	-184582.88	-4530.27	10661.72	-924.96
	$\sigma_{cls,Max}$22	-184582.88	-4530.27	10661.72	-68.73
	$\sigma_{cls,Med}$22	-184582.88	-4530.27	10661.72	-40.43
373	Ft. 22	-181132.88	7682.06	-32098.71	238.50
	$\sigma_{s,c}$22	-181132.88	7682.06	-32098.71	-1399.62
	$\sigma_{cls,Max}$22	-181132.88	7682.06	-32098.71	-108.82
	$\sigma_{cls,Med}$22	-181132.88	7682.06	-32098.71	-44.52

Pilastro: **74/174** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
74	1	-441579.75	534.95	13663.67	0.55

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
174	1	-435924.75	1557.73	1469.58	0.51

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	842.02	61956.98	4003.18	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	842.02	46467.73	4003.18	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	842.02	61956.98	4003.18	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
74	Ft. 16	-297652.19	383.58	9096.38	-816.95
	$\sigma_{s,c}$15	-308014.09	331.41	9578.49	-1179.21
	$\sigma_{cls,Max}$15	-308014.09	331.41	9578.49	-80.69
	$\sigma_{cls,Med}$15	-308014.09	331.41	9578.49	-67.47
174	Ft. 17	-293379.50	1149.66	1299.38	-906.08
	$\sigma_{s,c}$15	-303664.09	1136.15	993.62	-1050.09
	$\sigma_{cls,Max}$15	-303664.09	1136.15	993.62	-71.48
	$\sigma_{cls,Med}$15	-303664.09	1136.15	993.62	-66.51
Combinazioni Frequenti					
74	Ft. 19	-294198.41	400.81	8935.02	-807.69
	$\sigma_{s,c}$18	-297652.41	383.41	9095.71	-1138.92
	$\sigma_{cls,Max}$18	-297652.41	383.41	9095.71	-77.98
	$\sigma_{cls,Med}$18	-297652.41	383.41	9095.71	-65.20
174	Ft. 20	-288297.38	1036.48	1269.13	-893.48
	$\sigma_{s,c}$18	-293302.41	1019.71	977.82	-1012.08
	$\sigma_{cls,Max}$18	-293302.41	1019.71	977.82	-68.81
	$\sigma_{cls,Med}$18	-293302.41	1019.71	977.82	-64.24
Combinazioni Quasi Permanenti					
74	Ft. 22	-290953.31	399.99	8508.23	-804.04
	$\sigma_{s,c}$21	-294198.44	400.78	8934.89	-1125.49
	$\sigma_{cls,Max}$21	-294198.44	400.78	8934.89	-77.08
	$\sigma_{cls,Med}$21	-294198.44	400.78	8934.89	-64.44
174	Ft. 22	-286603.31	998.75	1259.05	-889.27
	$\sigma_{s,c}$21	-289848.44	980.89	972.52	-999.41
	$\sigma_{cls,Max}$21	-289848.44	980.89	972.52	-67.92
	$\sigma_{cls,Med}$21	-289848.44	980.89	972.52	-63.49

Pilastro: **174/274** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
174	1	-364443.22	-6722.96	-8122.28	0.48
274	1	-359958.22	6224.34	1192.75	0.46

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3752.84	61956.98	2700.01	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	3752.84	46467.73	2700.01	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	3752.84	61956.98	2700.01	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
174	Ft. 17	-242538.86	-4589.83	-5670.05	-558.11
	$\sigma_{s,c}$15	-252951.83	-4637.67	-5814.38	-1073.72
	$\sigma_{cls,Max}$15	-252951.83	-4637.67	-5814.38	-77.91
	$\sigma_{cls,Med}$15	-252951.83	-4637.67	-5814.38	-55.41
274	Ft. 17	-239088.86	4227.13	778.80	-638.32
	$\sigma_{s,c}$15	-249501.83	4325.87	1013.10	-973.93
	$\sigma_{cls,Max}$15	-249501.83	4325.87	1013.10	-70.05
	$\sigma_{cls,Med}$15	-249501.83	4325.87	1013.10	-54.65
Combinazioni Frequenti					
174	Ft. 20	-240152.95	-4389.93	-5380.53	-561.36
	$\sigma_{s,c}$18	-245258.38	-4411.07	-5514.41	-1036.33
	$\sigma_{cls,Max}$18	-245258.38	-4411.07	-5514.41	-75.10
	$\sigma_{cls,Med}$18	-245258.38	-4411.07	-5514.41	-53.72
274	Ft. 20	-236702.95	4039.07	561.21	-640.02
	$\sigma_{s,c}$18	-241808.38	4111.85	898.19	-939.97
	$\sigma_{cls,Max}$18	-241808.38	4111.85	898.19	-67.52
	$\sigma_{cls,Med}$18	-241808.38	4111.85	898.19	-52.96
Combinazioni Quasi Permanenti					
174	Ft. 22	-239357.66	-4323.29	-5284.03	-562.45
	$\sigma_{s,c}$21	-242693.80	-4335.73	-5414.40	-1023.87
	$\sigma_{cls,Max}$21	-242693.80	-4335.73	-5414.40	-74.17
	$\sigma_{cls,Med}$21	-242693.80	-4335.73	-5414.40	-53.16
274	Ft. 22	-235907.66	3976.39	488.68	-640.59
	$\sigma_{s,c}$21	-239243.80	4040.73	859.88	-928.65
	$\sigma_{cls,Max}$21	-239243.80	4040.73	859.88	-66.68
	$\sigma_{cls,Med}$21	-239243.80	4040.73	859.88	-52.40

Pilastro: **274/374** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
274	1	-293396.06	-8766.74	-10503.13	0.42
374	1	-288911.06	12754.96	26870.74	0.49

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	6238.18	61956.98	11615.68	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	6238.18	46467.73	11615.68	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	6238.18	61956.98	11615.68	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
274	Ft. 17	-191494.88	-5993.31	-7697.81	-312.59
	$\sigma_{s,c}$15	-202193.84	-6068.27	-7252.93	-975.99
	$\sigma_{cls,Max}$15	-202193.84	-6068.27	-7252.93	-73.28
	$\sigma_{cls,Med}$15	-202193.84	-6068.27	-7252.93	-44.29
374	Ft. 17	-188044.88	8609.16	19828.85	-12.01
	$\sigma_{s,c}$15	-198743.84	8705.53	18473.58	-1233.63
	$\sigma_{cls,Max}$15	-198743.84	8705.53	18473.58	-95.51

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-198743.84	8705.53	18473.58	-44.13
Combinazioni Frequenti					
274	Ft. 20	-191775.92	-5819.34	-7576.41	-321.03
	$\sigma_{s,c}$18	-197078.78	-5815.46	-6998.32	-946.98
	$\sigma_{cls,Max}$18	-197078.78	-5815.46	-6998.32	-71.02
	$\sigma_{cls,Med}$18	-197078.78	-5815.46	-6998.32	-43.17
374	Ft. 20	-188325.92	8468.24	19925.70	-16.51
	$\sigma_{s,c}$20	-188325.92	8468.24	19925.70	-1218.17
	$\sigma_{cls,Max}$20	-188325.92	8468.24	19925.70	-94.54
	$\sigma_{cls,Med}$18	-193628.78	8381.63	18071.58	-42.97
Combinazioni Quasi Permanenti					
274	Ft. 22	-191869.59	-5761.36	-7535.95	-323.84
	$\sigma_{s,c}$21	-195373.53	-5731.14	-6913.39	-937.31
	$\sigma_{cls,Max}$22	-191869.59	-5761.36	-7535.95	-70.38
	$\sigma_{cls,Med}$21	-195373.53	-5731.14	-6913.39	-42.79
374	Ft. 22	-188419.59	8421.26	19957.98	-18.00
	$\sigma_{s,c}$22	-188419.59	8421.26	19957.98	-1217.39
	$\sigma_{cls,Max}$22	-188419.59	8421.26	19957.98	-94.44
	$\sigma_{cls,Med}$21	-191923.53	8273.60	17937.38	-42.58

Pilastro: **75/175** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
75	1	-360713.09	998.88	-5971.00	0.43
175	1	-355058.09	746.36	502.50	0.41

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	722.11	61956.98	3453.33	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	722.11	46467.73	3453.33	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	722.11	61956.98	3453.33	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
75	Ft. 16	-243702.09	727.65	-4146.53	-709.72
	$\sigma_{s,c}$15	-251975.73	676.71	-4149.18	-917.27
	$\sigma_{cls,Max}$15	-251975.73	676.71	-4149.18	-62.66
	$\sigma_{cls,Med}$15	-251975.73	676.71	-4149.18	-55.19
175	Ft. 17	-238362.28	629.17	134.77	-760.92
	$\sigma_{s,c}$15	-247625.73	556.30	328.13	-836.64
	$\sigma_{cls,Max}$15	-247625.73	556.30	328.13	-56.47
	$\sigma_{cls,Med}$15	-247625.73	556.30	328.13	-54.24
Combinazioni Frequenti					
75	Ft. 19	-240944.28	744.41	-4147.08	-700.11
	$\sigma_{s,c}$18	-243702.17	727.42	-4148.02	-891.68
	$\sigma_{cls,Max}$18	-243702.17	727.42	-4148.02	-61.01
	$\sigma_{cls,Med}$18	-243702.17	727.42	-4148.02	-53.38
175	Ft. 20	-234391.14	530.74	219.92	-749.62

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$18	-239352.17	455.83	373.02	-807.00
	$\sigma_{cls,Max}$18	-239352.17	455.83	373.02	-54.39
	$\sigma_{cls,Med}$18	-239352.17	455.83	373.02	-52.43
Combinazioni Quasi Permanenti					
75	Ft. 22	-237417.42	689.21	-3759.28	-696.62
	$\sigma_{s,c}$21	-240944.30	744.36	-4147.38	-883.15
	$\sigma_{cls,Max}$21	-240944.30	744.36	-4147.38	-60.46
	$\sigma_{cls,Med}$21	-240944.30	744.36	-4147.38	-52.78
175	Ft. 22	-233067.42	497.93	248.30	-745.85
	$\sigma_{s,c}$21	-236594.30	422.32	387.85	-797.11
	$\sigma_{cls,Max}$21	-236594.30	422.32	387.85	-53.69
	$\sigma_{cls,Med}$21	-236594.30	422.32	387.85	-51.82

Pilastro: **175/275** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
175	1	-298116.84	-6319.74	2673.45	0.39
275	1	-293631.84	6095.98	-1256.00	0.39

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3598.76	61956.98	1138.97	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	3598.76	46467.73	1138.97	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	3598.76	61956.98	1138.97	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
175	Ft. 17	-197931.61	-4265.98	1885.32	-483.76
	$\sigma_{s,c}$15	-207242.59	-4311.87	1892.60	-849.03
	$\sigma_{cls,Max}$15	-207242.59	-4311.87	1892.60	-61.86
	$\sigma_{cls,Med}$15	-207242.59	-4311.87	1892.60	-45.39
275	Ft. 17	-194481.63	4032.20	-800.78	-497.60
	$\sigma_{s,c}$15	-203792.61	4194.50	-880.69	-817.41
	$\sigma_{cls,Max}$15	-203792.61	4194.50	-880.69	-59.44
	$\sigma_{cls,Med}$15	-203792.61	4194.50	-880.69	-44.64
Combinazioni Frequenti					
175	Ft. 20	-195995.78	-4094.35	1831.75	-483.74
	$\sigma_{s,c}$18	-201016.03	-4105.74	1823.29	-820.88
	$\sigma_{cls,Max}$18	-201016.03	-4105.74	1823.29	-59.74
	$\sigma_{cls,Med}$18	-201016.03	-4105.74	1823.29	-44.03
275	Ft. 20	-192545.80	3873.53	-720.81	-497.60
	$\sigma_{s,c}$18	-197566.05	3996.66	-809.11	-789.48
	$\sigma_{cls,Max}$18	-197566.05	3996.66	-809.11	-57.34
	$\sigma_{cls,Med}$18	-197566.05	3996.66	-809.11	-43.27
Combinazioni Quasi Permanenti					
175	Ft. 22	-195350.53	-4037.14	1813.90	-483.73
	$\sigma_{s,c}$21	-198940.50	-4037.26	1800.10	-811.50
	$\sigma_{cls,Max}$21	-198940.50	-4037.26	1800.10	-59.03

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-198940.50	-4037.26	1800.10	-43.57
275	Ft. 22	-191900.55	3820.64	-694.16	-497.60
	$\sigma_{s,c}$21	-195490.52	3930.98	-785.14	-780.18
	$\sigma_{cls,Max}$21	-195490.52	3930.98	-785.14	-56.64
	$\sigma_{cls,Med}$21	-195490.52	3930.98	-785.14	-42.82

Pilastro: **275/375** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
275	1	-242460.75	-8552.56	-165.68	0.35
375	1	-237975.75	12677.52	-802.19	0.38

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	6325.24	61956.98	1609.05	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	6325.24	46467.73	1609.05	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	6325.24	61956.98	1609.05	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
275	Ft. 17	-157790.66	-5969.48	316.96	-323.34
	$\sigma_{s,c}$15	-167425.86	-5893.62	-57.42	-738.51
	$\sigma_{cls,Max}$15	-167425.86	-5893.62	-57.42	-55.97
	$\sigma_{cls,Med}$15	-167425.86	-5893.62	-57.42	-36.67
375	Ft. 17	-154340.66	8935.19	-1932.46	-191.23
	$\sigma_{s,c}$15	-163975.86	8616.38	-628.67	-823.14
	$\sigma_{cls,Max}$17	-154340.66	8935.19	-1932.46	-65.41
	$\sigma_{cls,Med}$15	-163975.86	8616.38	-628.67	-35.92
Combinazioni Frequenti					
275	Ft. 20	-157861.14	-5807.91	271.57	-329.45
	$\sigma_{s,c}$18	-163154.23	-5652.51	-73.47	-717.07
	$\sigma_{cls,Max}$18	-163154.23	-5652.51	-73.47	-54.27
	$\sigma_{cls,Med}$18	-163154.23	-5652.51	-73.47	-35.74
375	Ft. 20	-154411.14	8780.48	-1867.00	-197.46
	$\sigma_{s,c}$20	-154411.14	8780.48	-1867.00	-817.19
	$\sigma_{cls,Max}$20	-154411.14	8780.48	-1867.00	-64.84
	$\sigma_{cls,Med}$18	-159704.23	8284.74	-570.23	-34.98
Combinazioni Quasi Permanenti					
275	Ft. 22	-157884.64	-5754.05	256.45	-331.49
	$\sigma_{s,c}$21	-161730.28	-5572.06	-78.64	-709.91
	$\sigma_{cls,Max}$21	-161730.28	-5572.06	-78.64	-53.70
	$\sigma_{cls,Med}$21	-161730.28	-5572.06	-78.64	-35.42
375	Ft. 22	-154434.64	8728.91	-1845.18	-199.53
	$\sigma_{s,c}$22	-154434.64	8728.91	-1845.18	-815.27
	$\sigma_{cls,Max}$22	-154434.64	8728.91	-1845.18	-64.65
	$\sigma_{cls,Med}$21	-158280.28	8174.12	-551.04	-34.67

Pilastro: **76/176** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
76	1	-450017.06	609.20	-1463.00	0.52
176	1	-444362.06	2330.93	-3402.51	0.53

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	1164.79	61956.98	2313.24	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	1164.79	46467.73	2313.24	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	1164.79	61956.98	2313.24	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
76	Ft. 16	-303723.06	461.56	-1161.87	-964.20
	$\sigma_{s,c}$15	-313463.03	387.91	-1059.93	-1059.57
	$\sigma_{cls,Max}$15	-313463.03	387.91	-1059.93	-71.27
	$\sigma_{cls,Med}$15	-313463.03	387.91	-1059.93	-68.66
176	Ft. 16	-299373.06	1528.13	-2200.99	-898.98
	$\sigma_{s,c}$15	-309113.03	1689.25	-2332.49	-1107.49
	$\sigma_{cls,Max}$15	-309113.03	1689.25	-2332.49	-76.18
	$\sigma_{cls,Med}$15	-309113.03	1689.25	-2332.49	-67.71
Combinazioni Frequenti					
76	Ft. 19	-300474.59	486.73	-1197.99	-952.14
	$\sigma_{s,c}$20	-306113.41	382.66	-1033.30	-1034.82
	$\sigma_{cls,Max}$20	-306113.41	382.66	-1033.30	-69.61
	$\sigma_{cls,Med}$20	-306113.41	382.66	-1033.30	-67.05
176	Ft. 19	-296124.59	1473.88	-2155.64	-890.78
	$\sigma_{s,c}$20	-301763.41	1631.12	-2248.15	-1080.11
	$\sigma_{cls,Max}$20	-301763.41	1631.12	-2248.15	-74.27
	$\sigma_{cls,Med}$20	-301763.41	1631.12	-2248.15	-66.10
Combinazioni Quasi Permanenti					
76	Ft. 21	-300474.22	486.86	-1198.43	-952.12
	$\sigma_{s,c}$22	-304563.22	407.34	-1097.28	-1031.56
	$\sigma_{cls,Max}$22	-304563.22	407.34	-1097.28	-69.43
	$\sigma_{cls,Med}$22	-304563.22	407.34	-1097.28	-66.71
176	Ft. 21	-296124.22	1473.77	-2155.33	-890.78
	$\sigma_{s,c}$22	-300213.22	1578.06	-2197.38	-1072.50
	$\sigma_{cls,Max}$22	-300213.22	1578.06	-2197.38	-73.69
	$\sigma_{cls,Med}$22	-300213.22	1578.06	-2197.38	-65.76

Pilastro: **176/276** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
176	1	-375532.63	-10198.20	2399.77	0.52
276	1	-371047.63	9452.12	1260.35	0.50

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5695.75	61956.98	569.07	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	5695.75	46467.73	569.07	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	5695.75	61956.98	569.07	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
176	Ft. 16	-253013.59	-6699.27	1699.05	-590.37
	$\sigma_{s,c}$15	-260219.69	-7038.62	1785.61	-1108.08
	$\sigma_{cls,Max}$15	-260219.69	-7038.62	1785.61	-82.23
	$\sigma_{cls,Med}$15	-260219.69	-7038.62	1785.61	-57.00
276	Ft. 16	-249563.59	6235.03	836.06	-607.92
	$\sigma_{s,c}$15	-256769.70	6556.80	758.66	-1064.62
	$\sigma_{cls,Max}$15	-256769.70	6556.80	758.66	-78.60
	$\sigma_{cls,Med}$15	-256769.70	6556.80	758.66	-56.24
Combinazioni Frequenti					
176	Ft. 19	-250610.53	-6584.03	1671.66	-586.59
	$\sigma_{s,c}$20	-255836.09	-6675.09	1692.69	-1080.59
	$\sigma_{cls,Max}$20	-255836.09	-6675.09	1692.69	-79.96
	$\sigma_{cls,Med}$20	-255836.09	-6675.09	1692.69	-56.04
276	Ft. 19	-247160.53	6125.54	859.94	-603.12
	$\sigma_{s,c}$20	-252386.09	6028.25	941.14	-1036.39
	$\sigma_{cls,Max}$20	-252386.09	6028.25	941.14	-76.14
	$\sigma_{cls,Med}$20	-252386.09	6028.25	941.14	-55.28
Combinazioni Quasi Permanenti					
176	Ft. 21	-250610.31	-6583.60	1671.97	-586.60
	$\sigma_{s,c}$22	-255137.14	-6574.62	1665.68	-1074.66
	$\sigma_{cls,Max}$22	-255137.14	-6574.62	1665.68	-79.45
	$\sigma_{cls,Med}$22	-255137.14	-6574.62	1665.68	-55.88
276	Ft. 21	-247160.31	6125.07	859.55	-603.14
	$\sigma_{s,c}$22	-251687.14	5934.01	980.09	-1031.73
	$\sigma_{cls,Max}$22	-251687.14	5934.01	980.09	-75.73
	$\sigma_{cls,Med}$22	-251687.14	5934.01	980.09	-55.13

Pilastro: **276/376** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
276	3	-306905.94	-11425.34	7200.68	0.45
376	3	-302420.94	16620.65	-25055.37	0.54

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	8129.27	61956.98	9349.58	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	8129.27	46467.73	9349.58	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	8129.27	61956.98	9349.58	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
276	Ft. 17	-211189.33	-7889.09	4969.44	-361.61

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$17	-211189.33	-7889.09	4969.44	-1026.12
	$\sigma_{cls,Max}$17	-211189.33	-7889.09	4969.44	-78.30
	$\sigma_{cls,Med}$15	-213154.34	-7540.29	4787.17	-46.69
376	Ft. 17	-207739.33	11299.21	-17068.42	-35.47
	$\sigma_{s,c}$17	-207739.33	11299.21	-17068.42	-1326.13
	$\sigma_{cls,Max}$17	-207739.33	11299.21	-17068.42	-104.49
	$\sigma_{cls,Med}$17	-207739.33	11299.21	-17068.42	-46.87
Combinazioni Frequenti					
276	Ft. 20	-211611.44	-7660.48	4864.76	-371.98
	$\sigma_{s,c}$20	-211611.44	-7660.48	4864.76	-1018.52
	$\sigma_{cls,Max}$20	-211611.44	-7660.48	4864.76	-77.51
	$\sigma_{cls,Med}$20	-211611.44	-7660.48	4864.76	-46.35
376	Ft. 20	-208161.44	11112.78	-16973.03	-45.73
	$\sigma_{s,c}$20	-208161.44	11112.78	-16973.03	-1319.23
	$\sigma_{cls,Max}$20	-208161.44	11112.78	-16973.03	-103.78
	$\sigma_{cls,Med}$20	-208161.44	11112.78	-16973.03	-46.81
Combinazioni Quasi Permanenti					
276	Ft. 22	-211752.13	-7584.27	4829.87	-375.44
	$\sigma_{s,c}$22	-211752.13	-7584.27	4829.87	-1015.99
	$\sigma_{cls,Max}$22	-211752.13	-7584.27	4829.87	-77.25
	$\sigma_{cls,Med}$22	-211752.13	-7584.27	4829.87	-46.38
376	Ft. 22	-208302.13	11050.63	-16941.24	-49.12
	$\sigma_{s,c}$22	-208302.13	11050.63	-16941.24	-1316.94
	$\sigma_{cls,Max}$22	-208302.13	11050.63	-16941.24	-103.54
	$\sigma_{cls,Med}$22	-208302.13	11050.63	-16941.24	-46.79

Pilastro: **77/177** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 20 ø 20 Af=62.83 [cm²] < 1f20 x 4 V + 7f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
77	1	-333299.25	2448.93	6272.60	0.37
177	1	-327644.25	3587.33	-285.27	0.36

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1104.01	61956.98	1906.85	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	1104.01	46467.73	1906.85	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	1104.01	61956.98	1906.85	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
77	Ft. 16	-226431.02	1916.33	4301.78	-565.30
	$\sigma_{s,c}$15	-232885.44	1816.90	4496.74	-828.85
	$\sigma_{cls,Max}$15	-232885.44	1816.90	4496.74	-57.89
	$\sigma_{cls,Med}$15	-232885.44	1816.90	4496.74	-47.12
177	Ft. 17	-222539.52	2608.66	18.80	-599.92
	$\sigma_{s,c}$15	-228535.44	2497.17	-159.00	-768.01
	$\sigma_{cls,Max}$15	-228535.44	2497.17	-159.00	-53.81
	$\sigma_{cls,Med}$15	-228535.44	2497.17	-159.00	-46.24

Combinazioni Frequenti					
77	Ft. 19	-224282.64	1949.87	4235.19	-558.84
	$\sigma_{s,c}$18	-226434.23	1916.74	4300.12	-809.10
	$\sigma_{cls,Max}$18	-226434.23	1916.74	4300.12	-56.65
	$\sigma_{cls,Med}$18	-226434.23	1916.74	4300.12	-45.81
177	Ft. 20	-219617.70	2371.09	37.96	-597.61
	$\sigma_{s,c}$18	-222084.23	2258.39	-141.60	-741.28
	$\sigma_{cls,Max}$18	-222084.23	2258.39	-141.60	-51.78
	$\sigma_{cls,Med}$18	-222084.23	2258.39	-141.60	-44.93
Combinazioni Quasi Permanenti					
77	Ft. 21	-224283.28	1949.95	4234.86	-558.85
	$\sigma_{s,c}$21	-224283.28	1949.95	4234.86	-802.52
	$\sigma_{cls,Max}$21	-224283.28	1949.95	4234.86	-56.23
	$\sigma_{cls,Med}$21	-224283.28	1949.95	4234.86	-45.38
177	Ft. 22	-218643.75	2291.90	44.35	-596.83
	$\sigma_{s,c}$21	-219933.28	2178.81	-136.04	-732.37
	$\sigma_{cls,Max}$21	-219933.28	2178.81	-136.04	-51.10
	$\sigma_{cls,Med}$21	-219933.28	2178.81	-136.04	-44.50

Pilastro: **177/277** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 20 ø 20 Af=62.83 [cm^2] < 1f20 x 4 V + 7f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
177	1	-275674.97	-16401.91	-6673.26	0.42
277	1	-271189.97	14021.76	-989.09	0.39

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.13	1.13	8818.45	61956.98	1647.59	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	8818.45	46467.73	1647.59	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	8818.45	61956.98	1647.59	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
177	Ft. 17	-185497.84	-11274.87	-4488.25	-168.47
	$\sigma_{s,c}$15	-191298.48	-11314.45	-4574.47	-977.53
	$\sigma_{cls,Max}$15	-191298.48	-11314.45	-4574.47	-77.64
	$\sigma_{cls,Med}$15	-191298.48	-11314.45	-4574.47	-38.71
277	Ft. 17	-182047.84	9628.76	-771.05	-263.08
	$\sigma_{s,c}$15	-187848.48	9702.04	-641.48	-859.63
	$\sigma_{cls,Max}$15	-187848.48	9702.04	-641.48	-67.45
	$\sigma_{cls,Med}$15	-187848.48	9702.04	-641.48	-38.01
Combinazioni Frequenti					
177	Ft. 20	-184543.27	-10807.74	-4323.83	-181.60
	$\sigma_{s,c}$18	-186758.53	-10781.78	-4381.37	-945.41
	$\sigma_{cls,Max}$18	-186758.53	-10781.78	-4381.37	-74.92
	$\sigma_{cls,Med}$18	-186758.53	-10781.78	-4381.37	-37.79
277	Ft. 20	-181093.27	9187.62	-863.52	-271.46
	$\sigma_{s,c}$18	-183308.53	9212.89	-702.82	-832.71
	$\sigma_{cls,Max}$18	-183308.53	9212.89	-702.82	-65.16
	$\sigma_{cls,Med}$18	-183308.53	9212.89	-702.82	-37.09
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
177	Ft. 22	-184225.08	-10652.03	-4269.02	-185.97
	$\sigma_{s,c}$21	-185245.00	-10604.43	-4317.22	-934.71
	$\sigma_{cls,Max}$21	-185245.00	-10604.43	-4317.22	-74.01
	$\sigma_{cls,Med}$21	-185245.00	-10604.43	-4317.22	-37.48
277	Ft. 22	-180775.08	9040.57	-894.35	-274.25
	$\sigma_{s,c}$21	-181795.00	9050.08	-722.95	-823.73
	$\sigma_{cls,Max}$21	-181795.00	9050.08	-722.95	-64.40
	$\sigma_{cls,Med}$21	-181795.00	9050.08	-722.95	-36.78

Pilastro: **277/377** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 20 ø 20 Af=62.83 [cm²] < 1f20 x 4 V + 7f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
277	1	-238587.27	-19586.47	-9246.66	0.42
377	3	-225124.75	30561.26	35437.94	0.63

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	14545.41	61956.98	13073.70	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	14545.41	46467.73	13073.70	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	14545.41	61956.98	13073.70	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
277	Ft. 17	-157944.75	-13423.98	-6587.49	44.84
	$\sigma_{s,c}$15	-163929.77	-13449.55	-6307.72	-996.11
	$\sigma_{cls,Max}$15	-163929.77	-13449.55	-6307.72	-81.88
	$\sigma_{cls,Med}$15	-163929.77	-13449.55	-6307.72	-36.97
377	Ft. 17	-154494.75	20782.69	24049.43	1051.98
	$\sigma_{s,c}$17	-154494.75	20782.69	24049.43	-1653.90
	$\sigma_{cls,Max}$17	-154494.75	20782.69	24049.43	-145.40
	$\sigma_{cls,Med}$17	-154494.75	20782.69	24049.43	-54.69
Combinazioni Frequenti					
277	Ft. 20	-158878.77	-13082.74	-6515.08	23.67
	$\sigma_{s,c}$20	-158878.77	-13082.74	-6515.08	-974.11
	$\sigma_{cls,Max}$20	-158878.77	-13082.74	-6515.08	-80.09
	$\sigma_{cls,Med}$20	-158878.77	-13082.74	-6515.08	-35.95
377	Ft. 20	-155428.77	20489.14	23942.09	1011.63
	$\sigma_{s,c}$20	-155428.77	20489.14	23942.09	-1638.90
	$\sigma_{cls,Max}$20	-155428.77	20489.14	23942.09	-143.59
	$\sigma_{cls,Med}$20	-155428.77	20489.14	23942.09	-54.03
Combinazioni Quasi Permanenti					
277	Ft. 22	-159190.09	-12969.00	-6490.94	16.85
	$\sigma_{s,c}$22	-159190.09	-12969.00	-6490.94	-970.42
	$\sigma_{cls,Max}$22	-159190.09	-12969.00	-6490.94	-79.68
	$\sigma_{cls,Med}$22	-159190.09	-12969.00	-6490.94	-35.79
377	Ft. 22	-155740.09	20391.29	23906.30	998.33
	$\sigma_{s,c}$22	-155740.09	20391.29	23906.30	-1633.90
	$\sigma_{cls,Max}$22	-155740.09	20391.29	23906.30	-142.99

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$22	-155740.09	20391.29	23906.30	-53.81

Pilastro: **78/178** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
78	1	-169402.06	4668.32	2012.41	0.23
178	1	-163747.06	-901.45	176.70	0.20

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	1533.66	61956.98	2163.93	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	1533.66	46467.73	2163.93	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	1533.66	61956.98	2163.93	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
78	Ft. 17	-113143.84	3240.14	1299.00	-247.41
	$\sigma_{s,c}$15	-120102.30	3379.36	1482.26	-526.35
	$\sigma_{cls,Max}$15	-120102.30	3379.36	1482.26	-39.21
	$\sigma_{cls,Med}$15	-120102.30	3379.36	1482.26	-26.31
178	Ft. 17	-108793.84	-572.70	315.25	-334.07
	$\sigma_{s,c}$15	-115752.30	-612.22	267.61	-404.16
	$\sigma_{cls,Max}$15	-115752.30	-612.22	267.61	-27.69
	$\sigma_{cls,Med}$15	-115752.30	-612.22	267.61	-25.35
Combinazioni Frequenti					
78	Ft. 20	-111881.01	3343.15	1208.57	-241.47
	$\sigma_{s,c}$18	-116560.44	3440.07	1389.46	-515.13
	$\sigma_{cls,Max}$18	-116560.44	3440.07	1389.46	-38.52
	$\sigma_{cls,Med}$18	-116560.44	3440.07	1389.46	-25.53
178	Ft. 20	-107531.01	-684.72	314.33	-326.37
	$\sigma_{s,c}$18	-112210.44	-709.58	264.56	-395.57
	$\sigma_{cls,Max}$18	-112210.44	-709.58	264.56	-27.23
	$\sigma_{cls,Med}$18	-112210.44	-709.58	264.56	-24.58
Combinazioni Quasi Permanenti					
78	Ft. 22	-111460.07	3377.49	1178.42	-239.48
	$\sigma_{s,c}$21	-115379.34	3460.21	1358.73	-511.38
	$\sigma_{cls,Max}$21	-115379.34	3460.21	1358.73	-38.28
	$\sigma_{cls,Med}$21	-115379.34	3460.21	1358.73	-25.27
178	Ft. 22	-107110.07	-722.06	314.03	-323.81
	$\sigma_{s,c}$21	-111029.34	-742.04	263.32	-392.70
	$\sigma_{cls,Max}$21	-111029.34	-742.04	263.32	-27.07
	$\sigma_{cls,Med}$21	-111029.34	-742.04	263.32	-24.32

Pilastro: **178/278** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
178	1	-139130.27	-8728.80	-9654.47	0.25

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
278	1	-134645.27	6404.60	627.59	0.21

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	4386.49	61956.98	3010.26	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	4386.49	46467.73	3010.26	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	4386.49	61956.98	3010.26	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
178	Ft. 17	-91116.63	-5937.26	-6587.92	6.50
	$\sigma_{s,c}$15	-98090.65	-6013.60	-6602.34	-624.56
	$\sigma_{cls,Max}$15	-98090.65	-6013.60	-6602.34	-49.77
	$\sigma_{cls,Med}$15	-98090.65	-6013.60	-6602.34	-22.29
278	Ft. 17	-87666.63	4404.47	617.12	-137.82
	$\sigma_{s,c}$15	-94640.65	4424.58	533.81	-460.43
	$\sigma_{cls,Max}$15	-94640.65	4424.58	533.81	-35.84
	$\sigma_{cls,Med}$15	-94640.65	4424.58	533.81	-20.73
Combinazioni Frequenti					
178	Ft. 20	-90575.77	-5711.76	-6293.28	-6.42
	$\sigma_{s,c}$18	-95258.55	-5746.97	-6300.19	-601.25
	$\sigma_{cls,Max}$18	-95258.55	-5746.97	-6300.19	-47.84
	$\sigma_{cls,Med}$18	-95258.55	-5746.97	-6300.19	-21.55
278	Ft. 20	-87125.77	4203.87	488.25	-144.53
	$\sigma_{s,c}$18	-91808.55	4198.27	430.44	-442.24
	$\sigma_{cls,Max}$18	-91808.55	4198.27	430.44	-34.35
	$\sigma_{cls,Med}$18	-91808.55	4198.27	430.44	-20.11
Combinazioni Quasi Permanenti					
178	Ft. 22	-90395.48	-5636.59	-6195.07	-10.61
	$\sigma_{s,c}$21	-94314.29	-5658.27	-6199.57	-593.50
	$\sigma_{cls,Max}$21	-94314.29	-5658.27	-6199.57	-47.20
	$\sigma_{cls,Med}$21	-94314.29	-5658.27	-6199.57	-21.31
278	Ft. 22	-86945.48	4137.01	445.30	-146.77
	$\sigma_{s,c}$21	-90864.29	4123.07	396.21	-436.18
	$\sigma_{cls,Max}$21	-90864.29	4123.07	396.21	-33.86
	$\sigma_{cls,Med}$21	-90864.29	4123.07	396.21	-19.90

Pilastro: **278/378** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
278	1	-123366.65	-7526.48	-10566.77	0.23
378	1	-118881.66	12658.99	33182.50	0.42

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5850.86	61956.98	12680.95	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	5850.86	46467.73	12680.95	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	5850.86	61956.98	12680.95	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
278	Ft. 17	-78783.62	-4970.55	-7225.32	29.43
	$\sigma_{s,c}$15	-86136.81	-5170.89	-7242.34	-570.33
	$\sigma_{cls,Max}$15	-86136.81	-5170.89	-7242.34	-45.35
	$\sigma_{cls,Med}$15	-86136.81	-5170.89	-7242.34	-19.82
378	Ft. 17	-75333.62	8065.03	21844.20	847.27
	$\sigma_{s,c}$15	-82686.81	8583.99	22371.61	-1100.67
	$\sigma_{cls,Max}$15	-82686.81	8583.99	22371.61	-94.14
	$\sigma_{cls,Med}$15	-82686.81	8583.99	22371.61	-31.96
Combinazioni Frequenti					
278	Ft. 20	-78848.68	-4797.53	-6986.92	16.71
	$\sigma_{s,c}$18	-83783.27	-4938.29	-6972.69	-550.09
	$\sigma_{cls,Max}$18	-83783.27	-4938.29	-6972.69	-43.66
	$\sigma_{cls,Med}$18	-83783.27	-4938.29	-6972.69	-19.19
378	Ft. 20	-75398.68	7850.04	21443.39	800.60
	$\sigma_{s,c}$18	-80333.27	8202.39	21682.77	-1059.63
	$\sigma_{cls,Max}$18	-80333.27	8202.39	21682.77	-90.44
	$\sigma_{cls,Med}$18	-80333.27	8202.39	21682.77	-30.75
Combinazioni Quasi Permanenti					
278	Ft. 22	-78870.37	-4739.86	-6907.45	12.59
	$\sigma_{s,c}$21	-82998.71	-4860.62	-6882.43	-543.34
	$\sigma_{cls,Max}$21	-82998.71	-4860.62	-6882.43	-43.10
	$\sigma_{cls,Med}$21	-82998.71	-4860.62	-6882.43	-18.98
378	Ft. 22	-75420.37	7778.38	21309.79	785.25
	$\sigma_{s,c}$21	-79548.71	8075.05	21452.86	-1045.93
	$\sigma_{cls,Max}$21	-79548.71	8075.05	21452.86	-89.20
	$\sigma_{cls,Med}$21	-79548.71	8075.05	21452.86	-30.35

Pilastro: **383/483** / L 4.02[m] / Sezione **5 B 30 [cm]H 30 [cm]**
Af: 4 ø 20 Af=12.57 [cm²] < 1f20 x 4 V + 0f20 x 2 B + 0f20 x 2 H >
Staffe: ø 10/15.0 x 92.0/ø 10/20.0 x 218.0/ø 10/15.0 x 92.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
383	2	-11045.76	98.23	366.91	0.07
483	2	-9796.79	-147.89	-366.30	0.07

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.05	57.64	19917.99	175.62	19917.99	ø 10/15.0
1.05	3.22	57.64	16319.03	175.62	16319.03	ø 10/20.0
3.22	4.14	57.64	19917.99	175.62	19917.99	ø 10/15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
383	Ft. 15	-7606.73	67.78	269.21	-54.00
	$\sigma_{s,c}$16	-7911.20	67.57	257.03	-157.98
	$\sigma_{cls,Max}$16	-7911.20	67.57	257.03	-13.39
	$\sigma_{cls,Med}$16	-7911.20	67.57	257.03	-7.27
483	Ft. 15	-6645.98	-101.65	-257.45	-37.36
	$\sigma_{s,c}$16	-6950.45	-103.89	-258.52	-150.45
	$\sigma_{cls,Max}$16	-6950.45	-103.89	-258.52	-13.22

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$16	-6950.45	-103.89	-258.52	-6.40
Combinazioni Frequenti					
383	Ft. 18	-7311.83	63.35	249.18	-53.62
	$\sigma_{s,c}$19	-7433.29	63.42	245.38	-149.01
	$\sigma_{cls,Max}$19	-7433.29	63.42	245.38	-12.65
	$\sigma_{cls,Med}$19	-7433.29	63.42	245.38	-6.83
483	Ft. 18	-6351.08	-94.57	-241.98	-36.73
	$\sigma_{s,c}$19	-6472.54	-95.62	-242.89	-140.26
	$\sigma_{cls,Max}$19	-6472.54	-95.62	-242.89	-12.33
	$\sigma_{cls,Med}$19	-6472.54	-95.62	-242.89	-5.96
Combinazioni Quasi Permanenti					
383	Ft. 21	-7313.42	62.57	243.81	-54.57
	$\sigma_{s,c}$21	-7313.42	62.57	243.81	-146.99
	$\sigma_{cls,Max}$21	-7313.42	62.57	243.81	-12.50
	$\sigma_{cls,Med}$22	-7330.32	60.71	209.81	-6.73
483	Ft. 21	-6352.67	-93.76	-239.58	-37.24
	$\sigma_{s,c}$21	-6352.67	-93.76	-239.58	-137.83
	$\sigma_{cls,Max}$21	-6352.67	-93.76	-239.58	-12.12
	$\sigma_{cls,Med}$21	-6352.67	-93.76	-239.58	-5.85

Pilastro: **384/484** / L 3.42[m] / Sezione **5 B 30 [cm]H 30 [cm]**
Af: 4 ø 20 Af=12.57 [cm²] < 1f20 x 4 V + 0f20 x 2 B + 0f20 x 2 H >
Staffe: ø 10/15.0 x 93.7/ø 10/20.0 x 154.7/ø 10/15.0 x 93.7
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
384	2	-15200.11	-327.95	-221.57	0.09
484	2	-14126.63	520.98	628.48	0.12

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.06	231.31	19917.99	231.62	19917.99	ø 10/15.0
1.06	2.61	231.31	16319.03	231.62	16319.03	ø 10/20.0
2.61	3.54	231.31	19917.99	231.62	19917.99	ø 10/15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
384	Ft. 17	-10003.69	-209.29	-137.75	-85.51
	$\sigma_{s,c}$16	-10870.76	-234.07	-163.33	-209.74
	$\sigma_{cls,Max}$16	-10870.76	-234.07	-163.33	-17.48
	$\sigma_{cls,Med}$16	-10870.76	-234.07	-163.33	-9.99
484	Ft. 15	-9508.37	354.42	424.94	-2.59
	$\sigma_{s,c}$16	-10045.01	373.00	449.36	-267.41
	$\sigma_{cls,Max}$16	-10045.01	373.00	449.36	-25.54
	$\sigma_{cls,Med}$16	-10045.01	373.00	449.36	-10.35
Combinazioni Frequenti					
384	Ft. 18	-9888.05	-216.33	-138.33	-82.77
	$\sigma_{s,c}$19	-10099.69	-218.78	-144.23	-193.93
	$\sigma_{cls,Max}$19	-10099.69	-218.78	-144.23	-16.12
	$\sigma_{cls,Med}$19	-10099.69	-218.78	-144.23	-9.28
484	Ft. 18	-9062.30	335.51	403.02	-3.48

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$19	-9273.94	342.95	412.70	-246.22
	$\sigma_{cls,Max}$19	-9273.94	342.95	412.70	-23.49
	$\sigma_{cls,Med}$19	-9273.94	342.95	412.70	-9.54
Combinazioni Quasi Permanenti					
384	Ft. 21	-9903.15	-215.23	-139.23	-83.01
	$\sigma_{s,c}$22	-9998.75	-209.40	-140.56	-190.57
	$\sigma_{cls,Max}$22	-9998.75	-209.40	-140.56	-15.78
	$\sigma_{cls,Med}$22	-9998.75	-209.40	-140.56	-9.19
484	Ft. 21	-9077.40	335.46	403.44	-3.69
	$\sigma_{s,c}$22	-9173.00	335.98	404.20	-242.20
	$\sigma_{cls,Max}$22	-9173.00	335.98	404.20	-23.06
	$\sigma_{cls,Med}$22	-9173.00	335.98	404.20	-9.39

Pilastro: **1361/2675 (87-187)** / L 1.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 120.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
1361	13	-21697.23	14126.29	-2109.35	0.15
2675	13	-20247.23	9521.01	1317.22	0.09

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.12	1.33	3176.05	86297.23	2597.10	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
1361	Ft. 16	-23996.86	8267.63	-1635.65	247.34
	$\sigma_{s,c}$15	-24894.03	8457.95	-1664.36	-328.72
	$\sigma_{cls,Max}$15	-24894.03	8457.95	-1664.36	-27.11
	$\sigma_{cls,Med}$15	-24894.03	8457.95	-1664.36	-9.96
2675	Ft. 16	-22546.86	5828.94	995.78	90.40
	$\sigma_{s,c}$15	-23444.03	5920.41	1013.88	-222.89
	$\sigma_{cls,Max}$15	-23444.03	5920.41	1013.88	-17.57
	$\sigma_{cls,Med}$15	-23444.03	5920.41	1013.88	-6.90
Combinazioni Frequenti					
1361	Ft. 19	-23692.08	8143.93	-1620.46	243.57
	$\sigma_{s,c}$18	-23990.94	8205.29	-1629.84	-319.87
	$\sigma_{cls,Max}$18	-23990.94	8205.29	-1629.84	-26.42
	$\sigma_{cls,Med}$18	-23990.94	8205.29	-1629.84	-9.68
2675	Ft. 19	-22242.08	5765.08	986.33	90.05
	$\sigma_{s,c}$18	-22540.94	5794.42	992.24	-217.77
	$\sigma_{cls,Max}$18	-22540.94	5794.42	992.24	-17.20
	$\sigma_{cls,Med}$18	-22540.94	5794.42	992.24	-6.74
Combinazioni Quasi Permanenti					
1361	Ft. 21	-23690.90	8131.46	-1619.30	242.73
	$\sigma_{s,c}$21	-23690.90	8131.46	-1619.30	-317.29
	$\sigma_{cls,Max}$21	-23690.90	8131.46	-1619.30	-26.22
	$\sigma_{cls,Med}$21	-23690.90	8131.46	-1619.30	-9.60
2675	Ft. 21	-22240.90	5758.18	985.62	89.73

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$21	-22240.90	5758.18	985.62	-216.26
	$\sigma_{cls,Max}$21	-22240.90	5758.18	985.62	-17.09
	$\sigma_{cls,Med}$21	-22240.90	5758.18	985.62	-6.69

Pilastro: **2675/3971(187-287)** (/ L 2.65[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 65.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
2675	1	-74953.41	-829.57	-882.20	0.09
3971	1	-71183.41	-3892.58	1173.62	0.10

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.12	1.13	1723.22	86297.23	708.90	61956.98	ø 10 2br.x4br./15.0
1.13	1.78	1723.22	64722.92	708.90	46467.73	ø 10 2br.x4br./20.0
1.78	2.78	1723.22	86297.23	708.90	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
2675	Ft. 17	-48931.49	-527.91	-582.84	-133.59
	$\sigma_{s,c}$15	-53002.02	-608.62	-631.52	-204.18
	$\sigma_{cls,Max}$15	-53002.02	-608.62	-631.52	-14.44
	$\sigma_{cls,Med}$15	-53002.02	-608.62	-631.52	-11.61
3971	Ft. 16	-48340.91	-2843.99	820.40	-86.21
	$\sigma_{s,c}$15	-50102.02	-2852.52	837.98	-237.93
	$\sigma_{cls,Max}$15	-50102.02	-2852.52	837.98	-17.33
	$\sigma_{cls,Med}$15	-50102.02	-2852.52	837.98	-10.97
Combinazioni Frequenti					
2675	Ft. 20	-48349.03	-560.18	-583.19	-131.14
	$\sigma_{s,c}$18	-51162.27	-614.72	-617.04	-197.78
	$\sigma_{cls,Max}$18	-51162.27	-614.72	-617.04	-14.00
	$\sigma_{cls,Med}$18	-51162.27	-614.72	-617.04	-11.21
3971	Ft. 20	-45449.03	-2442.09	774.68	-84.73
	$\sigma_{s,c}$18	-48262.27	-2808.02	818.02	-230.52
	$\sigma_{cls,Max}$18	-48262.27	-2808.02	818.02	-16.80
	$\sigma_{cls,Med}$18	-48262.27	-2808.02	818.02	-10.57
Combinazioni Quasi Permanenti					
2675	Ft. 22	-48154.88	-570.94	-583.31	-130.32
	$\sigma_{s,c}$21	-50562.12	-617.86	-612.52	-195.71
	$\sigma_{cls,Max}$21	-50562.12	-617.86	-612.52	-13.86
	$\sigma_{cls,Med}$21	-50562.12	-617.86	-612.52	-11.07
3971	Ft. 22	-45254.88	-2484.99	774.51	-83.40
	$\sigma_{s,c}$21	-47662.12	-2799.18	811.76	-228.21
	$\sigma_{cls,Max}$21	-47662.12	-2799.18	811.76	-16.64
	$\sigma_{cls,Med}$21	-47662.12	-2799.18	811.76	-10.44

Pilastro: **3971/7031 (287-387)** / L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
3971	1	-207128.80	1941.94	1898.57	0.25
7031	1	-202643.80	1109.91	-5614.05	0.28

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2421.83	86297.23	2326.43	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	2421.83	64722.92	2326.43	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	2421.83	86297.23	2326.43	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm^2]
Combinazioni Rare					
3971	Ft. 17	-133324.45	784.43	1479.65	-378.14
	$\sigma_{s,c}$15	-145329.61	1467.63	1330.59	-543.82
	$\sigma_{cls,Max}$15	-145329.61	1467.63	1330.59	-38.03
	$\sigma_{cls,Med}$15	-145329.61	1467.63	1330.59	-31.83
7031	Ft. 17	-129874.45	1279.52	-4184.42	-272.66
	$\sigma_{s,c}$15	-141879.61	791.94	-3991.10	-606.07
	$\sigma_{cls,Max}$15	-141879.61	791.94	-3991.10	-45.10
	$\sigma_{cls,Med}$15	-141879.61	791.94	-3991.10	-31.08
Combinazioni Frequenti					
3971	Ft. 20	-132111.05	1064.60	1323.68	-374.53
	$\sigma_{s,c}$18	-140455.89	1544.48	1217.25	-525.46
	$\sigma_{cls,Max}$18	-140455.89	1544.48	1217.25	-36.69
	$\sigma_{cls,Med}$18	-140455.89	1544.48	1217.25	-30.76
7031	Ft. 20	-128661.04	982.40	-3871.02	-283.50
	$\sigma_{s,c}$18	-137005.89	626.55	-3729.73	-579.04
	$\sigma_{cls,Max}$18	-137005.89	626.55	-3729.73	-42.97
	$\sigma_{cls,Med}$18	-137005.89	626.55	-3729.73	-30.01
Combinazioni Quasi Permanenti					
3971	Ft. 22	-131706.56	1157.98	1271.69	-373.33
	$\sigma_{s,c}$21	-138862.13	1575.92	1178.57	-519.50
	$\sigma_{cls,Max}$21	-138862.13	1575.92	1178.57	-36.26
	$\sigma_{cls,Med}$21	-138862.13	1575.92	1178.57	-30.42
7031	Ft. 22	-128256.55	883.37	-3766.55	-287.12
	$\sigma_{s,c}$21	-135412.13	570.46	-3641.89	-570.09
	$\sigma_{cls,Max}$21	-135412.13	570.46	-3641.89	-42.27
	$\sigma_{cls,Med}$21	-135412.13	570.46	-3641.89	-29.66

Pilastro: **7031/9601** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
7031	1	-155393.77	13460.75	6421.36	0.32
9601	1	-150908.77	-18788.20	-14518.86	0.43

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	9348.31	61956.98	6069.63	86297.23	ø 10 4br.x2br./15.0
1.13	2.33	9347.82	46467.73	6069.63	64722.92	ø 10 4br.x2br./20.0
2.33	3.33	9347.23	61956.98	6069.63	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
7031	Ft. 17	-96333.93	9125.33	4159.28	103.15
	$\sigma_{s,c}$15	-108198.75	9391.85	4414.56	-743.90
	$\sigma_{cls,Max}$15	-108198.75	9391.85	4414.56	-61.85
	$\sigma_{cls,Med}$15	-108198.75	9391.85	4414.56	-27.85
9601	Ft. 17	-92883.93	-12095.44	-9037.22	576.79
	$\sigma_{s,c}$15	-104748.75	-12937.61	-9810.61	-1029.68
	$\sigma_{cls,Max}$15	-104748.75	-12937.61	-9810.61	-91.20
	$\sigma_{cls,Med}$15	-104748.75	-12937.61	-9810.61	-37.39
Combinazioni Frequenti					
7031	Ft. 20	-96844.53	8805.01	4064.72	75.69
	$\sigma_{s,c}$18	-105123.29	8981.28	4265.12	-716.26
	$\sigma_{cls,Max}$18	-105123.29	8981.28	4265.12	-59.41
	$\sigma_{cls,Med}$18	-105123.29	8981.28	4265.12	-26.76
9601	Ft. 20	-93394.53	-11920.93	-8859.86	541.37
	$\sigma_{s,c}$18	-101673.29	-12500.46	-9454.23	-994.73
	$\sigma_{cls,Max}$18	-101673.29	-12500.46	-9454.23	-88.02
	$\sigma_{cls,Med}$18	-101673.29	-12500.46	-9454.23	-36.11
Combinazioni Quasi Permanenti					
7031	Ft. 22	-97014.74	8698.24	4033.21	67.02
	$\sigma_{s,c}$21	-104121.98	8843.74	4211.78	-707.02
	$\sigma_{cls,Max}$21	-104121.98	8843.74	4211.78	-58.59
	$\sigma_{cls,Med}$21	-104121.98	8843.74	4211.78	-26.40
9601	Ft. 22	-93564.74	-11862.75	-8800.74	529.78
	$\sigma_{s,c}$21	-100671.98	-12353.39	-9323.36	-982.74
	$\sigma_{cls,Max}$21	-100671.98	-12353.39	-9323.36	-86.92
	$\sigma_{cls,Med}$21	-100671.98	-12353.39	-9323.36	-35.68

Pilastro: **1587/4381 (47A-147A)** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
1587	3	-385857.84	-2273.63	-14252.03	0.49
4381	3	-380202.84	-863.56	6690.56	0.46

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	815.29	61956.98	6322.25	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	817.36	46467.73	6322.25	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	818.35	61956.98	6322.25	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
1587	Ft. 16	-260235.11	-1694.78	-9668.38	-642.95

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{s,c}$15	-267765.69	-1692.20	-9857.08	-1094.81
	$\sigma_{cls,Max}$15	-267765.69	-1692.20	-9857.08	-76.67
	$\sigma_{cls,Med}$17	-268515.84	-1595.67	-9806.88	-58.81
4381	Ft. 16	-255885.09	-466.42	4117.50	-758.53
	$\sigma_{s,c}$17	-264165.84	-612.92	4214.50	-956.36
	$\sigma_{cls,Max}$17	-264165.84	-612.92	4214.50	-65.21
	$\sigma_{cls,Med}$17	-264165.84	-612.92	4214.50	-57.86
Combinazioni Frequenti					
1587	Ft. 19	-257708.00	-1694.94	-9610.89	-635.58
	$\sigma_{s,c}$20	-264933.88	-1635.17	-9648.79	-1080.29
	$\sigma_{cls,Max}$20	-264933.88	-1635.17	-9648.79	-75.60
	$\sigma_{cls,Med}$20	-264933.88	-1635.17	-9648.79	-58.03
4381	Ft. 19	-253358.00	-443.75	4080.73	-751.55
	$\sigma_{s,c}$20	-260583.88	-529.81	4140.96	-940.74
	$\sigma_{cls,Max}$20	-260583.88	-529.81	4140.96	-64.06
	$\sigma_{cls,Med}$20	-260583.88	-529.81	4140.96	-57.08
Combinazioni Quasi Permanenti					
1587	Ft. 21	-257704.50	-1694.79	-9612.01	-635.55
	$\sigma_{s,c}$22	-263739.91	-1648.33	-9596.09	-1075.92
	$\sigma_{cls,Max}$22	-263739.91	-1648.33	-9596.09	-75.31
	$\sigma_{cls,Med}$22	-263739.91	-1648.33	-9596.09	-57.77
4381	Ft. 21	-253354.50	-443.83	4080.35	-751.54
	$\sigma_{s,c}$22	-259389.91	-502.11	4116.45	-935.54
	$\sigma_{cls,Max}$22	-259389.91	-502.11	4116.45	-63.67
	$\sigma_{cls,Med}$22	-259389.91	-502.11	4116.45	-56.82

Pilastro: **4381/7439 (147A-247A)**/ L 3.20[m] / Sezione **1 B 40 [cm]H 100 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 1f20 x 2 B + 3f20 x 2 H >
Staffe: ø 10 2br.x4br./15.0 x 100.0/ø 10 2br.x4br./20.0 x 120.0/ø 10 2br.x4br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
4381	3	-326045.69	-20301.47	3083.71	0.44
7439	3	-321560.69	5256.70	-1933.87	0.39

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	7437.46	86297.23	1465.65	61956.98	ø 10 2br.x4br./15.0
1.13	2.32	7437.46	64722.92	1465.65	46467.73	ø 10 2br.x4br./20.0
2.32	3.32	7437.46	86297.23	1465.65	61956.98	ø 10 2br.x4br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
4381	Ft. 16	-218816.42	-12939.85	2079.05	-441.13
	$\sigma_{s,c}$17	-225551.50	-13644.22	2225.21	-1035.02
	$\sigma_{cls,Max}$17	-225551.50	-13644.22	2225.21	-73.96
	$\sigma_{cls,Med}$17	-225551.50	-13644.22	2225.21	-49.40
7439	Ft. 16	-215366.42	3180.49	-1334.31	-613.12
	$\sigma_{s,c}$17	-222101.50	3537.69	-1417.94	-832.69
	$\sigma_{cls,Max}$17	-222101.50	3537.69	-1417.94	-57.76
	$\sigma_{cls,Med}$17	-222101.50	3537.69	-1417.94	-48.65

Combinazioni Frequenti					
4381	Ft. 19	-216978.64	-12710.93	2034.18	-440.26
	$\sigma_{s,c}$20	-224070.91	-13045.92	2087.42	-1015.99
	$\sigma_{cls,Max}$20	-224070.91	-13045.92	2087.42	-72.43
	$\sigma_{cls,Med}$20	-224070.91	-13045.92	2087.42	-49.08
7439	Ft. 19	-213528.64	3019.37	-1293.44	-611.02
	$\sigma_{s,c}$20	-220620.91	3083.89	-1271.81	-815.76
	$\sigma_{cls,Max}$20	-220620.91	3083.89	-1271.81	-56.38
	$\sigma_{cls,Med}$20	-220620.91	3083.89	-1271.81	-48.32
Combinazioni Quasi Permanenti					
4381	Ft. 21	-216975.47	-12709.52	2034.10	-440.28
	$\sigma_{s,c}$22	-223577.36	-12846.49	2041.49	-1009.64
	$\sigma_{cls,Max}$22	-223577.36	-12846.49	2041.49	-71.92
	$\sigma_{cls,Med}$22	-223577.36	-12846.49	2041.49	-48.97
7439	Ft. 21	-213525.47	3017.94	-1293.42	-611.03
	$\sigma_{s,c}$22	-220127.36	2932.62	-1223.10	-810.11
	$\sigma_{cls,Max}$22	-220127.36	2932.62	-1223.10	-55.92
	$\sigma_{cls,Med}$22	-220127.36	2932.62	-1223.10	-48.22

Pilastro: **7439/9808 (247A-347A)**/ L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm^2] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	**Comb**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
7439	3	-277015.28	-1356.53	-20161.63	0.38
9808	3	-272530.28	3640.00	60202.32	0.56

Verifiche a Taglio

Da [m]	**A [m]**	**V_{d12} [kg]**	**V_{Rd12} [kg]**	**V_{d13} [kg]**	**V_{Rd13} [kg]**	**Staffe**
0.12	1.13	1447.30	61956.98	23293.88	86297.23	ø 10 4br.x2br./15.0
1.13	2.33	1449.24	46467.73	23293.88	64722.92	ø 10 4br.x2br./20.0
2.33	3.33	1450.85	61956.98	23293.88	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm^2]**
Combinazioni Rare					
7439	Ft. 16	-184596.45	-695.33	-13510.93	-363.38
	$\sigma_{s,c}$17	-190081.72	-1008.71	-13952.23	-884.82
	$\sigma_{cls,Max}$17	-190081.72	-1008.71	-13952.23	-62.62
	$\sigma_{cls,Med}$17	-190081.72	-1008.71	-13952.23	-41.63
9808	Ft. 17	-186631.72	2553.13	40717.02	188.74
	$\sigma_{s,c}$17	-186631.72	2553.13	40717.02	-1387.54
	$\sigma_{cls,Max}$17	-186631.72	2553.13	40717.02	-103.35
	$\sigma_{cls,Med}$17	-186631.72	2553.13	40717.02	-47.14
Combinazioni Frequenti					
7439	Ft. 19	-183384.92	-674.23	-13403.63	-361.82
	$\sigma_{s,c}$20	-190595.25	-958.69	-13738.37	-881.42
	$\sigma_{cls,Max}$20	-190595.25	-958.69	-13738.37	-62.30
	$\sigma_{cls,Med}$20	-190595.25	-958.69	-13738.37	-41.75
9808	Ft. 20	-187145.25	2591.41	40479.51	181.28
	$\sigma_{s,c}$20	-187145.25	2591.41	40479.51	-1385.26
	$\sigma_{cls,Max}$20	-187145.25	2591.41	40479.51	-103.17
	$\sigma_{cls,Med}$20	-187145.25	2591.41	40479.51	-47.00
Combinazioni Quasi Permanenti					

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
7439	Ft. 21	-183382.00	-674.19	-13404.02	-361.81
	$\sigma_{s,c}$22	-190766.44	-942.02	-13667.09	-880.29
	$\sigma_{cls,Max}$22	-190766.44	-942.02	-13667.09	-62.19
	$\sigma_{cls,Med}$22	-190766.44	-942.02	-13667.09	-41.78
9808	Ft. 22	-187316.44	2604.17	40400.35	178.83
	$\sigma_{s,c}$22	-187316.44	2604.17	40400.35	-1384.50
	$\sigma_{cls,Max}$22	-187316.44	2604.17	40400.35	-103.11
	$\sigma_{cls,Med}$22	-187316.44	2604.17	40400.35	-46.95

Pilastro: **2000/5093(60A-160A)** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
2000	1	-80508.01	1665.64	238.40	0.11
5093	1	-74853.01	276.52	1773.81	0.09

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	608.28	61956.98	1215.30	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	608.28	46467.73	1215.30	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	608.28	61956.98	1215.30	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
2000	Ft. 17	-53488.07	977.74	303.79	-139.66
	$\sigma_{s,c}$15	-57903.11	1282.13	207.79	-234.43
	$\sigma_{cls,Max}$15	-57903.11	1282.13	207.79	-17.13
	$\sigma_{cls,Med}$15	-57903.11	1282.13	207.79	-12.68
5093	Ft. 17	-49138.07	272.67	1067.69	-135.31
	$\sigma_{s,c}$15	-53553.11	128.04	1113.42	-198.24
	$\sigma_{cls,Max}$15	-53553.11	128.04	1113.42	-13.56
	$\sigma_{cls,Med}$15	-53553.11	128.04	1113.42	-11.73
Combinazioni Frequenti					
2000	Ft. 20	-52897.30	1010.92	201.44	-138.34
	$\sigma_{s,c}$18	-56333.95	1272.50	120.15	-227.53
	$\sigma_{cls,Max}$18	-56333.95	1272.50	120.15	-16.64
	$\sigma_{cls,Med}$18	-56333.95	1272.50	120.15	-12.34
5093	Ft. 20	-48547.30	233.90	1110.43	-133.90
	$\sigma_{s,c}$18	-51983.95	99.32	1119.17	-192.26
	$\sigma_{cls,Max}$18	-51983.95	99.32	1119.17	-13.13
	$\sigma_{cls,Med}$18	-51983.95	99.32	1119.17	-11.39
Combinazioni Quasi Permanenti					
2000	Ft. 22	-52700.38	1021.98	167.32	-137.90
	$\sigma_{s,c}$21	-55831.86	1272.06	90.88	-225.39
	$\sigma_{cls,Max}$21	-55831.86	1272.06	90.88	-16.49
	$\sigma_{cls,Med}$21	-55831.86	1272.06	90.88	-12.23
5093	Ft. 22	-48350.38	220.98	1124.68	-133.43
	$\sigma_{s,c}$21	-51481.86	88.25	1121.09	-190.29
	$\sigma_{cls,Max}$21	-51481.86	88.25	1121.09	-12.99

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$21	-51481.86	88.25	1121.09	-11.28

Pilastro: **5093/8151(160A-260A** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
5093	1	-66707.32	2417.74	-1864.54	0.10
8151	1	-62222.32	-1901.04	3430.23	0.09

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.12	1.13	1322.10	61956.98	1534.72	86297.23	ø 10 4br.x2br./15.0
1.13	2.33	1320.66	46467.73	1534.72	64722.92	ø 10 4br.x2br./20.0
2.33	3.33	1318.93	61956.98	1534.72	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
5093	Ft. 17	-43294.11	1716.15	-1130.22	-69.16
	$\sigma_{s,c}$15	-47844.83	1661.63	-1169.18	-229.18
	$\sigma_{cls,Max}$15	-47844.83	1661.63	-1169.18	-17.38
	$\sigma_{cls,Med}$15	-47844.83	1661.63	-1169.18	-10.48
8151	Ft. 17	-39844.11	-1406.05	2158.83	-50.87
	$\sigma_{s,c}$15	-44394.83	-1304.23	2235.39	-223.91
	$\sigma_{cls,Max}$15	-44394.83	-1304.23	2235.39	-16.81
	$\sigma_{cls,Med}$15	-44394.83	-1304.23	2235.39	-9.72
Combinazioni Frequenti					
5093	Ft. 20	-43024.02	1656.48	-1169.74	-69.53
	$\sigma_{s,c}$18	-46593.66	1586.89	-1167.93	-222.67
	$\sigma_{cls,Max}$18	-46593.66	1586.89	-1167.93	-16.86
	$\sigma_{cls,Med}$18	-46593.66	1586.89	-1167.93	-10.21
8151	Ft. 20	-39574.02	-1346.74	2140.41	-52.17
	$\sigma_{s,c}$18	-43143.66	-1236.68	2144.50	-216.17
	$\sigma_{cls,Max}$18	-43143.66	-1236.68	2144.50	-16.20
	$\sigma_{cls,Med}$18	-43143.66	-1236.68	2144.50	-9.45
Combinazioni Quasi Permanenti					
5093	Ft. 22	-42933.99	1636.58	-1182.91	-69.65
	$\sigma_{s,c}$21	-46198.53	1561.68	-1167.56	-220.56
	$\sigma_{cls,Max}$21	-46198.53	1561.68	-1167.56	-16.69
	$\sigma_{cls,Med}$21	-46198.53	1561.68	-1167.56	-10.12
8151	Ft. 22	-39483.99	-1326.97	2134.28	-52.60
	$\sigma_{s,c}$21	-42748.53	-1213.86	2114.24	-213.65
	$\sigma_{cls,Max}$21	-42748.53	-1213.86	2114.24	-16.00
	$\sigma_{cls,Med}$21	-42748.53	-1213.86	2114.24	-9.36

Pilastro: **8151/10190(260A-360A** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
8151	1	-50526.86	-4219.90	-3508.34	0.11

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
10190	1	-46041.86	6858.75	1762.39	0.14

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	3216.16	61956.98	1936.20	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	3216.16	46467.73	1936.20	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	3216.16	61956.98	1936.20	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
8151	Ft. 17	-31590.70	-2891.40	-2207.02	46.44
	$\sigma_{s,c}$15	-36235.35	-2846.77	-2295.39	-252.27
	$\sigma_{cls,Max}$15	-36235.35	-2846.77	-2295.39	-20.66
	$\sigma_{cls,Med}$15	-36235.35	-2846.77	-2295.39	-8.89
10190	Ft. 17	-28140.71	4575.86	1122.92	259.03
	$\sigma_{s,c}$15	-32785.35	4609.08	1155.97	-303.46
	$\sigma_{cls,Max}$17	-28140.71	4575.86	1122.92	-28.65
	$\sigma_{cls,Med}$17	-28140.71	4575.86	1122.92	-13.16
Combinazioni Frequenti					
8151	Ft. 20	-31666.83	-2827.45	-2182.31	40.90
	$\sigma_{s,c}$18	-35380.45	-2737.41	-2198.22	-243.74
	$\sigma_{cls,Max}$18	-35380.45	-2737.41	-2198.22	-19.92
	$\sigma_{cls,Med}$18	-35380.45	-2737.41	-2198.22	-8.61
10190	Ft. 20	-28216.83	4498.71	1116.86	245.25
	$\sigma_{s,c}$18	-31930.45	4442.08	1103.94	-292.78
	$\sigma_{cls,Max}$20	-28216.83	4498.71	1116.86	-28.11
	$\sigma_{cls,Med}$20	-28216.83	4498.71	1116.86	-12.92
Combinazioni Quasi Permanenti					
8151	Ft. 22	-31692.21	-2806.14	-2174.07	39.12
	$\sigma_{s,c}$21	-35118.49	-2699.29	-2165.80	-240.90
	$\sigma_{cls,Max}$22	-31692.21	-2806.14	-2174.07	-19.78
	$\sigma_{cls,Med}$21	-35118.49	-2699.29	-2165.80	-8.52
10190	Ft. 22	-28242.21	4472.99	1114.84	240.71
	$\sigma_{s,c}$21	-31668.49	4383.40	1086.76	-289.12
	$\sigma_{cls,Max}$22	-28242.21	4472.99	1114.84	-27.93
	$\sigma_{cls,Med}$22	-28242.21	4472.99	1114.84	-12.83

Pilastro: **2398/5711(79-179)** / L 4.10[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 210.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
2398	1	-234534.94	-759.12	3308.35	0.28
5711	1	-228879.94	-960.25	18.64	0.27

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	677.46	61956.98	2504.10	86297.23	ø 10 4br.x2br./15.0
1.13	3.23	676.31	46467.73	2504.10	64722.92	ø 10 4br.x2br./20.0
3.23	4.23	673.90	61956.98	2504.10	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
2398	Ft. 16	-159950.27	-647.95	2485.04	-464.26
	$\sigma_{s,c}$15	-165324.45	-620.37	2385.07	-601.92
	$\sigma_{cls,Max}$15	-165324.45	-620.37	2385.07	-41.26
	$\sigma_{cls,Med}$15	-165324.45	-620.37	2385.07	-36.21
5711	Ft. 16	-155600.27	-566.87	-13.88	-492.97
	$\sigma_{s,c}$15	-160974.45	-639.42	75.09	-550.45
	$\sigma_{cls,Max}$15	-160974.45	-639.42	75.09	-37.44
	$\sigma_{cls,Med}$15	-160974.45	-639.42	75.09	-35.26
Combinazioni Frequenti					
2398	Ft. 19	-158154.00	-656.71	2518.67	-457.53
	$\sigma_{s,c}$18	-159945.25	-647.50	2485.36	-586.75
	$\sigma_{cls,Max}$18	-159945.25	-647.50	2485.36	-40.30
	$\sigma_{cls,Med}$18	-159945.25	-647.50	2485.36	-35.03
5711	Ft. 20	-155109.27	-715.08	-55.47	-485.96
	$\sigma_{s,c}$20	-155109.27	-715.08	-55.47	-533.27
	$\sigma_{cls,Max}$20	-155109.27	-715.08	-55.47	-36.38
	$\sigma_{cls,Med}$18	-155595.25	-567.22	-13.88	-34.08
Combinazioni Quasi Permanenti					
2398	Ft. 21	-158153.00	-656.62	2518.73	-457.53
	$\sigma_{s,c}$21	-158153.00	-656.62	2518.73	-581.70
	$\sigma_{cls,Max}$21	-158153.00	-656.62	2518.73	-39.98
	$\sigma_{cls,Med}$22	-158560.16	-453.08	2478.33	-34.73
5711	Ft. 22	-154210.16	-695.05	-86.98	-483.13
	$\sigma_{s,c}$22	-154210.16	-695.05	-86.98	-530.19
	$\sigma_{cls,Max}$22	-154210.16	-695.05	-86.98	-36.16
	$\sigma_{cls,Med}$22	-154210.16	-695.05	-86.98	-33.78

Pilastro: **5711/8769 (179-279)** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
5711	1	-187761.63	-4814.53	6061.99	0.26
8769	1	-183276.63	4528.45	-2123.68	0.25

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	2731.32	61956.98	2409.23	86297.23	ø 10 4br.x2br./15.0
1.13	2.32	2731.32	46467.73	2409.23	64722.92	ø 10 4br.x2br./20.0
2.32	3.32	2731.32	61956.98	2409.23	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
5711	Ft. 17	-128830.47	-3341.03	4207.75	-248.16
	$\sigma_{s,c}$15	-131666.47	-3288.55	4158.10	-605.22
	$\sigma_{cls,Max}$15	-131666.47	-3288.55	4158.10	-44.84
	$\sigma_{cls,Med}$15	-131666.47	-3288.55	4158.10	-28.84
8769	Ft. 17	-125380.47	3107.56	-1507.29	-288.43
	$\sigma_{s,c}$15	-128216.50	3106.67	-1472.83	-544.18
	$\sigma_{cls,Max}$15	-128216.50	3106.67	-1472.83	-40.09

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
	$\sigma_{cls,Med}$15	-128216.50	3106.67	-1472.83	-28.08
Combinazioni Frequenti					
5711	Ft. 20	-127535.70	-3233.13	4077.37	-249.47
	$\sigma_{s,c}$20	-127535.70	-3233.13	4077.37	-588.57
	$\sigma_{cls,Max}$20	-127535.70	-3233.13	4077.37	-43.65
	$\sigma_{cls,Med}$18	-127730.27	-3150.55	4003.66	-27.98
8769	Ft. 19	-122969.83	2928.15	-1287.72	-289.81
	$\sigma_{s,c}$20	-124085.70	3005.99	-1359.65	-525.55
	$\sigma_{cls,Max}$20	-124085.70	3005.99	-1359.65	-38.71
	$\sigma_{cls,Med}$18	-124280.27	2972.76	-1333.99	-27.22
Combinazioni Quasi Permanenti					
5711	Ft. 22	-127104.13	-3197.16	4033.91	-249.91
	$\sigma_{s,c}$22	-127104.13	-3197.16	4033.91	-585.29
	$\sigma_{cls,Max}$22	-127104.13	-3197.16	4033.91	-43.39
	$\sigma_{cls,Med}$22	-127104.13	-3197.16	4033.91	-27.84
8769	Ft. 21	-122968.95	2928.13	-1287.72	-289.80
	$\sigma_{s,c}$22	-123654.13	2972.13	-1310.44	-522.25
	$\sigma_{cls,Max}$22	-123654.13	2972.13	-1310.44	-38.44
	$\sigma_{cls,Med}$22	-123654.13	2972.13	-1310.44	-27.08

Pilastro: **8769/10528 (279-379)** / L 3.20[m] / Sezione **2 B 100 [cm]H 40 [cm]**
Af: 12 ø 20 Af=37.70 [cm²] < 1f20 x 4 V + 3f20 x 2 B + 1f20 x 2 H >
Staffe: ø 10 4br.x2br./15.0 x 100.0/ø 10 4br.x2br./20.0 x 120.0/ø 10 4br.x2br./15.0 x 100.0
Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
8769	1	-157598.31	-6881.11	4298.30	0.24
10528	3	-148720.31	10614.57	-16769.00	0.31

Verifiche a Taglio

Da [m]	A [m]	V_{d12} [kg]	V_{Rd12} [kg]	V_{d13} [kg]	V_{Rd13} [kg]	Staffe
0.13	1.13	5164.85	61956.98	6106.39	86297.23	ø 10 4br.x2br./15.0
1.13	2.33	5167.11	46467.73	6106.39	64722.92	ø 10 4br.x2br./20.0
2.33	3.33	5168.99	61956.98	6106.39	86297.23	ø 10 4br.x2br./15.0

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
8769	Ft. 17	-106761.01	-4922.28	2994.48	-145.20
	$\sigma_{s,c}$15	-109689.66	-4704.29	2994.63	-559.02
	$\sigma_{cls,Max}$17	-106761.01	-4922.28	2994.48	-43.24
	$\sigma_{cls,Med}$15	-109689.66	-4704.29	2994.63	-24.03
10528	Ft. 17	-103311.01	7173.94	-11403.93	113.73
	$\sigma_{s,c}$17	-103311.01	7173.94	-11403.93	-774.86
	$\sigma_{cls,Max}$17	-103311.01	7173.94	-11403.93	-62.54
	$\sigma_{cls,Med}$17	-103311.01	7173.94	-11403.93	-25.51
Combinazioni Frequenti					
8769	Ft. 20	-106763.16	-4809.84	2921.13	-149.98
	$\sigma_{s,c}$20	-106763.16	-4809.84	2921.13	-551.57
	$\sigma_{cls,Max}$20	-106763.16	-4809.84	2921.13	-42.78
	$\sigma_{cls,Med}$18	-106912.53	-4523.42	2891.48	-23.42
10528	Ft. 20	-103313.16	7077.91	-11275.76	105.57

Nodo	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Combinazioni Rare					
	$\sigma_{s,c}$20	-103313.16	7077.91	-11275.76	-768.20
	$\sigma_{cls,Max}$20	-103313.16	7077.91	-11275.76	-61.92
	$\sigma_{cls,Med}$20	-103313.16	7077.91	-11275.76	-25.36
Combinazioni Quasi Permanenti					
8769	Ft. 22	-106763.88	-4772.36	2896.68	-151.57
	$\sigma_{s,c}$22	-106763.88	-4772.36	2896.68	-549.98
	$\sigma_{cls,Max}$22	-106763.88	-4772.36	2896.68	-42.63
	$\sigma_{cls,Med}$22	-106763.88	-4772.36	2896.68	-23.38
10528	Ft. 22	-103313.88	7045.90	-11233.04	102.88
	$\sigma_{s,c}$22	-103313.88	7045.90	-11233.04	-765.99
	$\sigma_{cls,Max}$22	-103313.88	7045.90	-11233.04	-61.71
	$\sigma_{cls,Med}$22	-103313.88	7045.90	-11233.04	-25.31